

Esc201A: Introduction to Electronics

Solution-Quiz-2A, October 2016

Total points: 15 marks

Duration: 45 minutes

1. Calculate the small signal gain v_o/v_i of the circuit in Figure 1(a) in terms of R_L , g_{m1} , and g_{m2} . Assume that both of the MOSFETS are operating in the saturation region, and that the small-signal models of the MOSFETS are as shown in Figure 1(b).

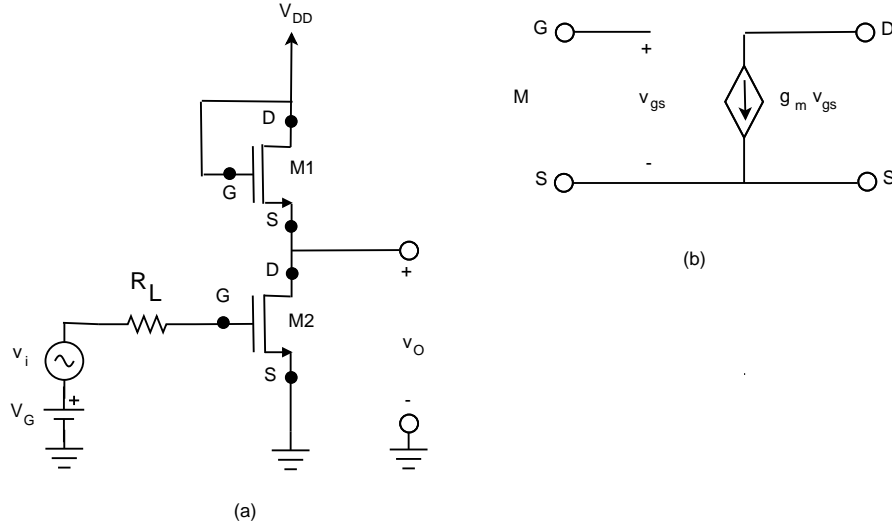


Figure 1: Figure for Problem 1

Solution: Current through MOSFET $M1$ is given by

$$i_{D1} = g_{m1}v_{gs1} = -g_{m1}v_o$$

Current through MOSFET $M2$ is given by

$$i_{D2} = g_{m2}v_{gs2} \approx g_{m2}v_i$$

The approximation can be made because current flowing into gate is nearly zero.

In the circuit we see that

$$\begin{aligned} i_{D1} &= i_{D2} \\ \implies -g_{m1}v_o &= g_{m2}v_i \end{aligned}$$

Hence, we have

$$\implies \frac{v_o}{v_i} = \frac{-g_{m2}}{g_{m1}}$$

2. Determine the expression for v_O in terms of v_I for the circuit in Figure 2. Assume that the MOSFET is operating in the saturation region with $i_{DS} = (K/2)(v_{GS} - V_t)^2$, and that $v_I > 0$.

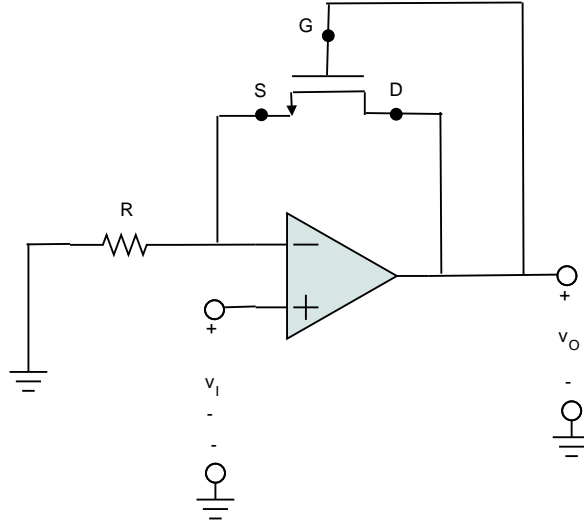


Figure 2: Figure for Problem 2

Solution: From $V_+ = V_- = v_I$, we see that $v_{DS} = v_{GS} = v_o - v_I = v_o$.

We can write

$$\frac{v_I - 0}{R} = i_{DS} = \frac{K}{2} (v_{GS} - V_t)^2 = \frac{K}{2} (v_o - v_I - V_t)^2$$

$$\Rightarrow \sqrt{\frac{2v_I}{RK}} = v_o - v_I - V_t$$

or

$$v_o = \sqrt{\frac{2v_I}{RK}} + v_I + V_t$$

3. Look at the op-amp circuit shown in Figure 4. An input signal $v_i = A \sin(\omega t)$ is applied to the circuit and an output $v_o(t) = V_o \sin(\omega t + \theta)$ is observed. Determine the value of V_o and θ in terms of A, R, C_1, C_2 and ω .

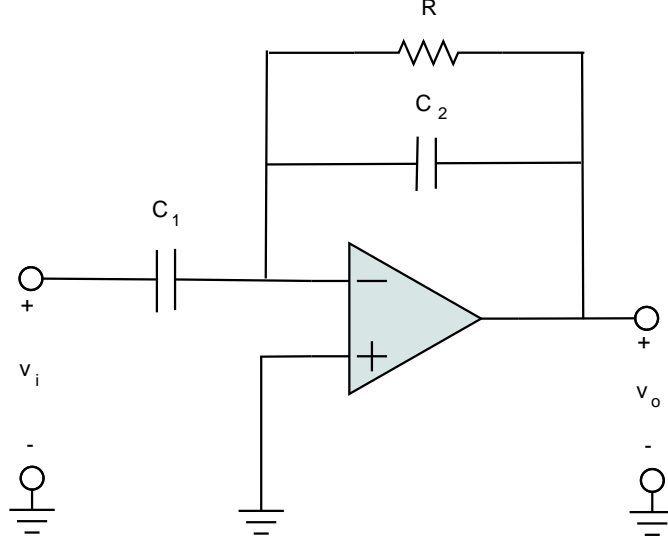


Figure 3: Figure for Problem 3

Solution: From the circuit, we can write

$$\frac{v_o(j\omega)}{v_i(j\omega)} = \frac{-Z_2(j\omega)}{Z_1(j\omega)}$$

where

$$Z_2(j\omega) = R \parallel \frac{1}{j\omega C_2} = \frac{R}{1 + j\omega C_2 R} \quad \text{and} \quad Z_1(j\omega) = \frac{1}{j\omega C_1}$$

Substituting these values,

$$\begin{aligned} \frac{v_o(j\omega)}{v_i(j\omega)} &= -\frac{j\omega C_1 R}{1 + j\omega C_2 R} = -\frac{j\omega C_1 R (1 - j\omega C_2 R)}{(1 + j\omega C_2 R)(1 - j\omega C_2 R)} = -\frac{\omega^2 R^2 C_1 C_2 + j\omega C_1 R}{1 + \omega^2 R^2 C_2^2} \\ &= -\frac{\sqrt{\omega^4 R^4 C_1^2 C_2^2 + \omega^2 C_1^2 R^2}}{(1 + \omega^2 R^2 C_2^2)} \angle \tan^{-1} \left(\frac{\omega C_1 R}{\omega^2 R^2 C_1 C_2} \right) \\ &= -\frac{\omega C_1 R \sqrt{\omega^2 R^2 C_2^2 + 1}}{(1 + \omega^2 R^2 C_2^2)} \angle \tan^{-1} \left(\frac{1}{\omega R C_2} \right) \\ &= \frac{\omega C_1 R}{\sqrt{\omega^2 R^2 C_2^2 + 1}} \angle \tan^{-1} \left(\frac{1}{\omega R C_2} \right) + \pi \end{aligned}$$

When $v_i(t) = A \sin(\omega t)$ and $v_o(t) = V_o \sin(\omega t + \theta)$, we can write

$$V_o = \frac{A\omega C_1 R}{\sqrt{\omega^2 R^2 C_2^2 + 1}}$$

and

$$\theta = \tan^{-1} \left(\frac{1}{\omega RC_2} \right) + \pi$$

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1. Calculate the small signal gain v_o/v_i of the circuit in Figure 1(a) in terms of R_L , g_{m1} , and g_{m2} . Assume that both of the MOSFETS are operating in the saturation region, and that the small-signal models of the MOSFETS are as shown in Figure 1(b).

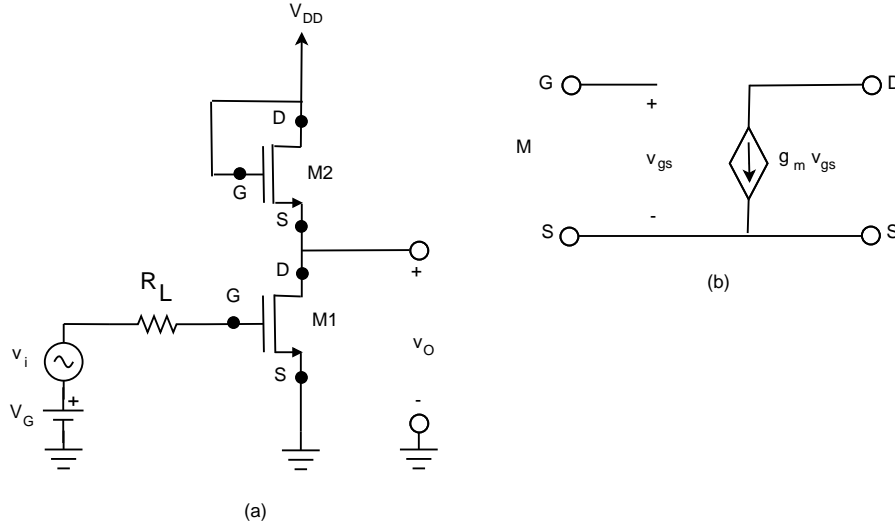


Figure 1: Figure for Problem 1

Solution: Current through MOSFET M2 is given by

$$i_{D2} = g_{m2}v_{gs2} = -g_{m2}v_o$$

Current through MOSFET M1 is given by

$$i_{D1} = g_{m1}v_{gs1} \approx g_{m1}v_i$$

The approximation can be made because current flowing into gate is nearly zero.

In the circuit we see that

$$\begin{aligned} i_{D1} &= i_{D2} \\ \implies -g_{m2}v_o &= g_{m1}v_i \end{aligned}$$

Hence, we have

$$\implies \frac{v_o}{v_i} = \frac{-g_{m1}}{g_{m2}}$$

2. Determine the expression for v_O in terms of v_I for the circuit in Figure 2. Assume that the MOSFET is operating in the saturation region with $i_{DS} = (K/2)(v_{GS} - V_t)^2$, and that $v_I < 0$.

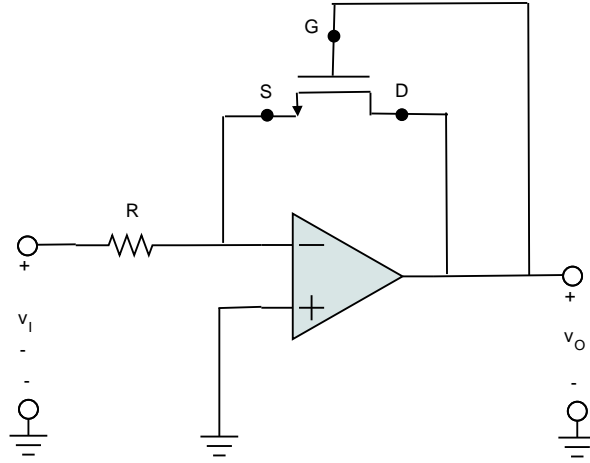


Figure 2: Figure for Problem 2

Solution: From $V_+ = V_- = 0$, we see that $v_{DS} = v_o - 0 = v_o$.

We can write

$$\frac{0 - v_I}{R} = i_{DS} = \frac{K}{2} (v_{GS} - V_t)^2$$

$$\Rightarrow v_{GS} = \sqrt{\frac{-2v_I}{RK}} + V_t$$

Also, from the circuit, $v_{DS} = v_{GS} = v_o$. Thus,

$$v_o = \sqrt{\frac{-2v_I}{RK}} + V_t$$

3. Look at the op-amp circuit shown in Figure 4. An input signal $v_i = A \sin(\omega t)$ is applied to the circuit and an output $v_o(t) = V_o \sin(\omega t + \theta)$ is observed. Determine the value of V_o and θ in terms of A, R, C_A, C_B and ω .

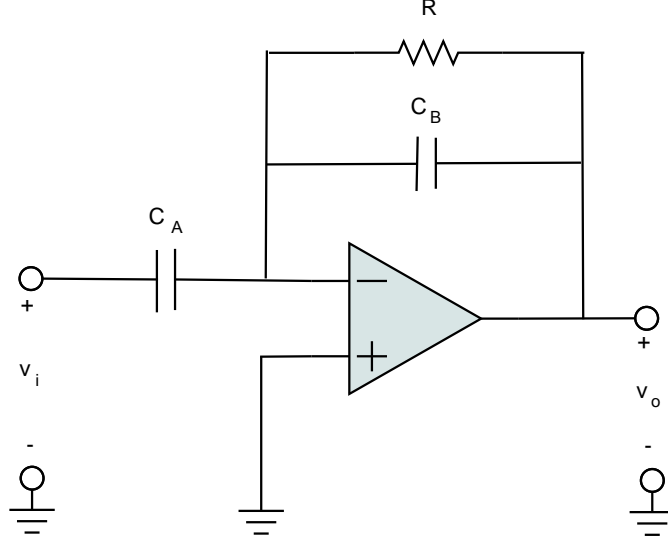


Figure 3: Figure for Problem 3

Solution: From the circuit, we can write

$$\frac{v_o(j\omega)}{v_i(j\omega)} = \frac{-Z_2(j\omega)}{Z_1(j\omega)}$$

where

$$Z_2(j\omega) = R \parallel \frac{1}{j\omega C_B} = \frac{R}{1 + j\omega C_B R} \quad \text{and} \quad Z_1(j\omega) = \frac{1}{j\omega C_A}$$

Substituting these values,

$$\begin{aligned} \frac{v_o(j\omega)}{v_i(j\omega)} &= -\frac{j\omega C_A R}{1 + j\omega C_B R} = -\frac{j\omega C_A R (1 - j\omega C_B R)}{(1 + j\omega C_B R)(1 - j\omega C_B R)} = -\frac{\omega^2 R^2 C_B C_A + j\omega C_A R}{1 + \omega^2 R^2 C_B^2} \\ &= -\frac{\sqrt{\omega^4 R^4 C_A^2 C_B^2 + \omega^2 C_A^2 R^2}}{(1 + \omega^2 R^2 C_B^2)} \angle \tan^{-1} \left(\frac{\omega C_A R}{\omega^2 R^2 C_A C_B} \right) \\ &= -\frac{\omega C_A R \sqrt{\omega^2 R^2 C_B^2 + 1}}{(1 + \omega^2 R^2 C_B^2)} \angle \tan^{-1} \left(\frac{1}{\omega R C_B} \right) \\ &= \frac{\omega C_A R}{\sqrt{\omega^2 R^2 C_B^2 + 1}} \angle \tan^{-1} \left(\frac{1}{\omega R C_B} \right) + \pi \end{aligned}$$

When $v_i(t) = A \sin(\omega t)$ and $v_o(t) = V_o \sin(\omega t + \theta)$, we can write

$$V_o = \frac{A \omega C_A R}{\sqrt{\omega^2 R^2 C_B^2 + 1}}$$

and

$$\theta = \tan^{-1} \left(\frac{1}{\omega RC_{\text{B}}} \right) + \pi$$