

# **ESc201 : Introduction to Electronics**

## **Amplifiers**

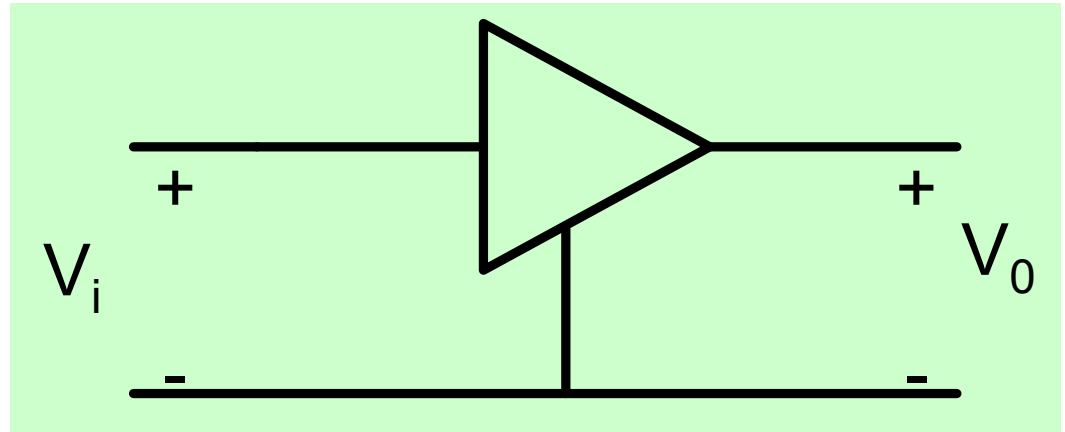
Dr. Y. S. Chauhan  
Dept. of Electrical Engineering  
IIT Kanpur

# Objective

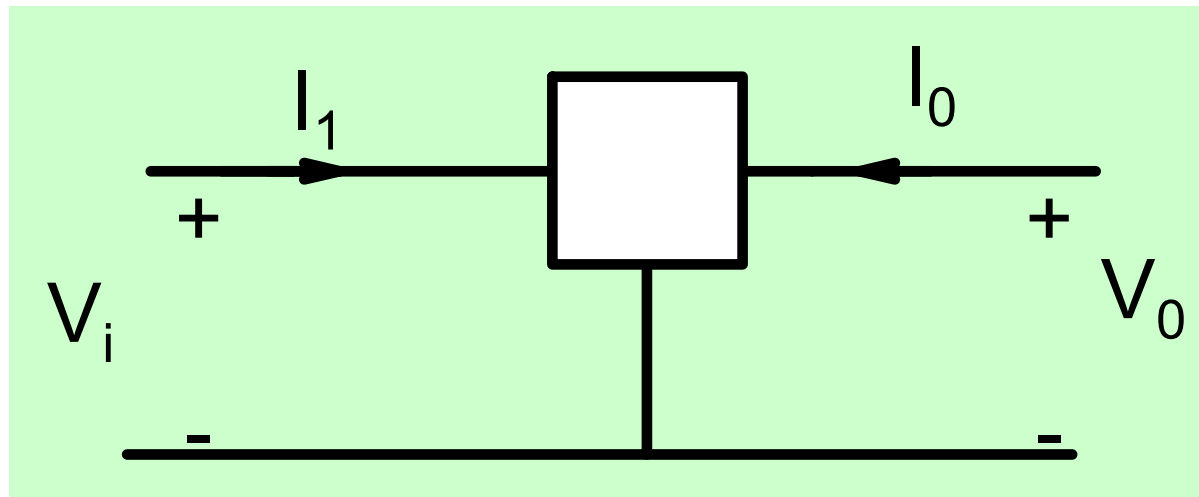
1. Learn ideal Transistor characteristics required for Voltage Amplification
2. Learn to build amplifiers using elements which have non-ideal characteristics.

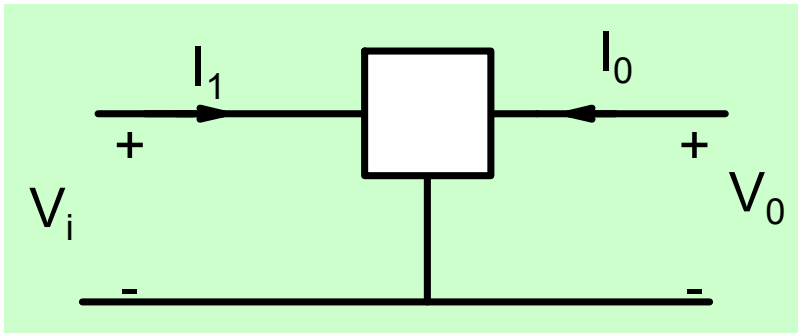
## Voltage Amplification

$$V_o = G \times V_i$$
$$G > 1$$



3-terminal unilateral linear device



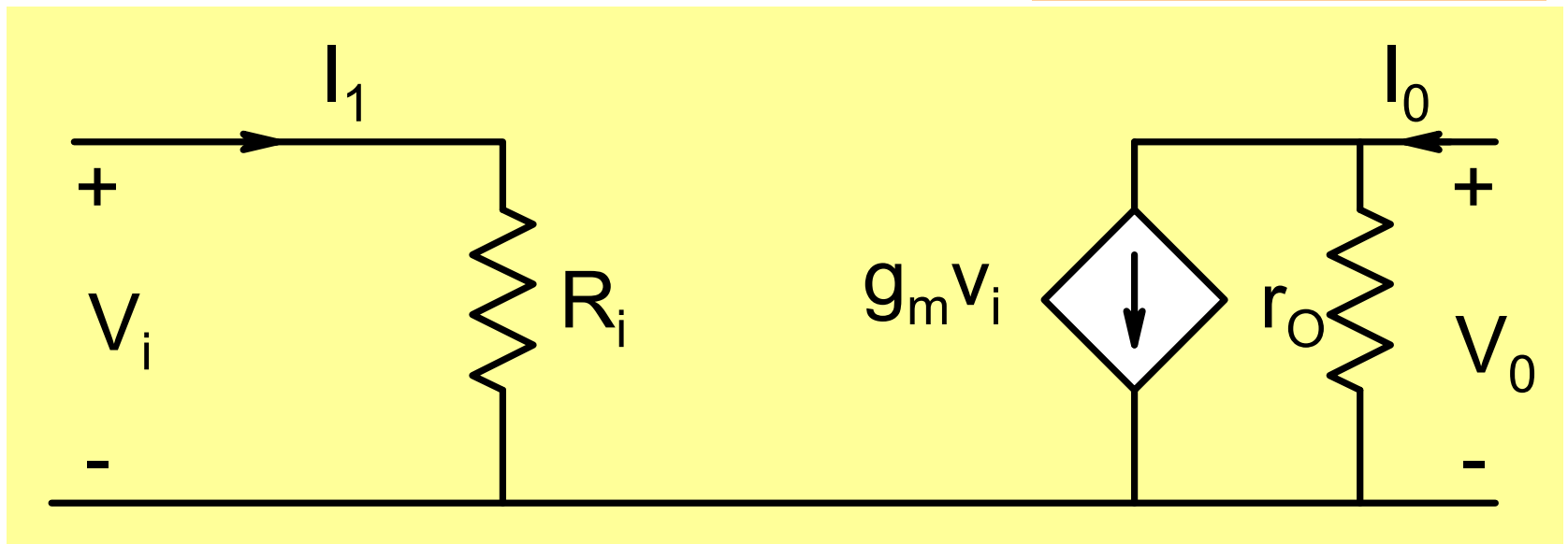


Input resistance  $R_i = V_i / I_i$   
(Ideally large)

Trans conductance

$$g_m = \left. \frac{I_o}{V_i} \right|_{V_o=0}$$

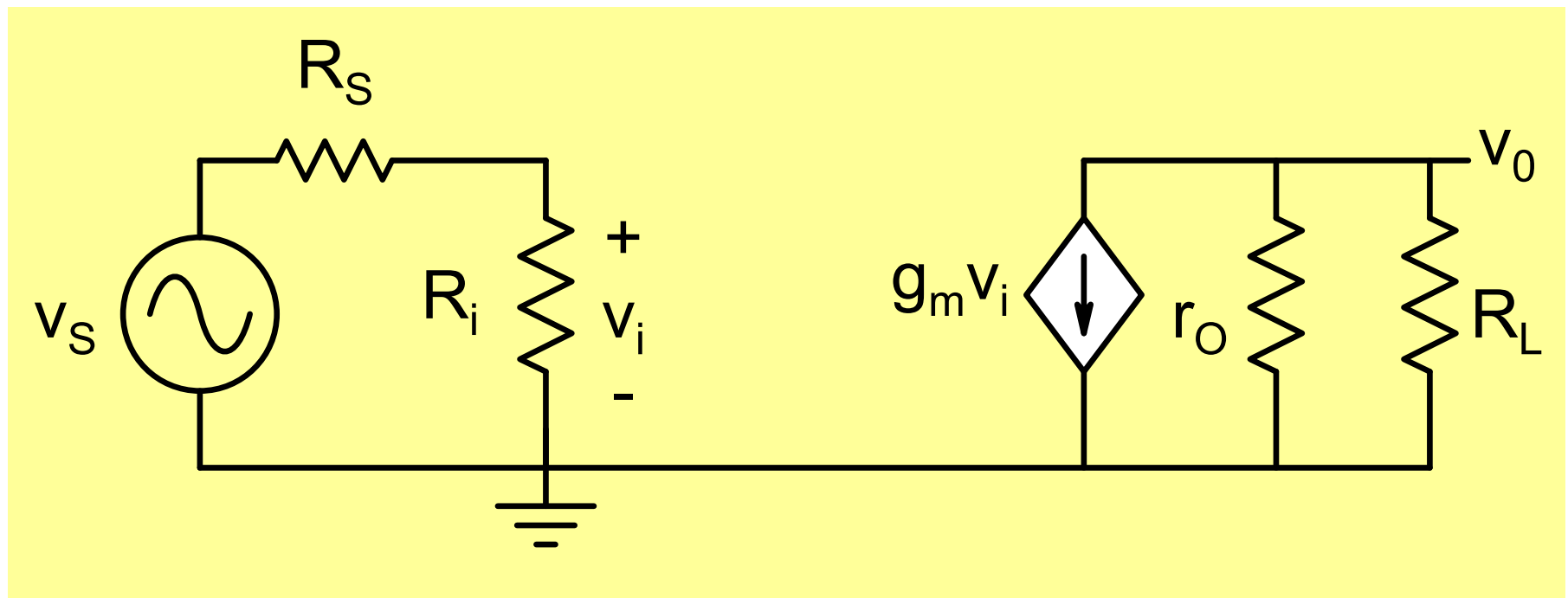
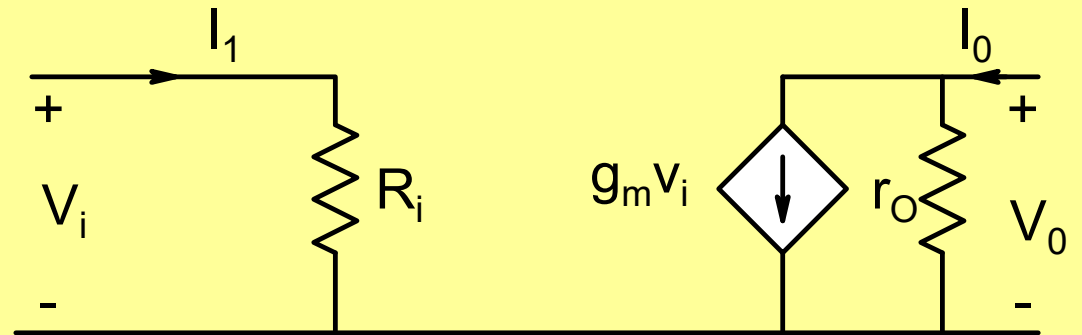
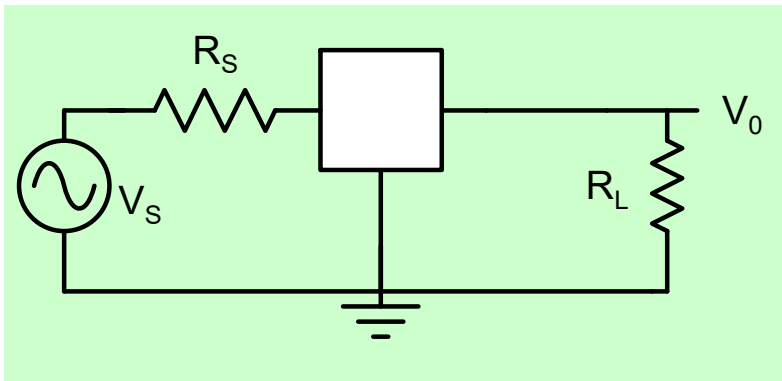
(Ideally large)

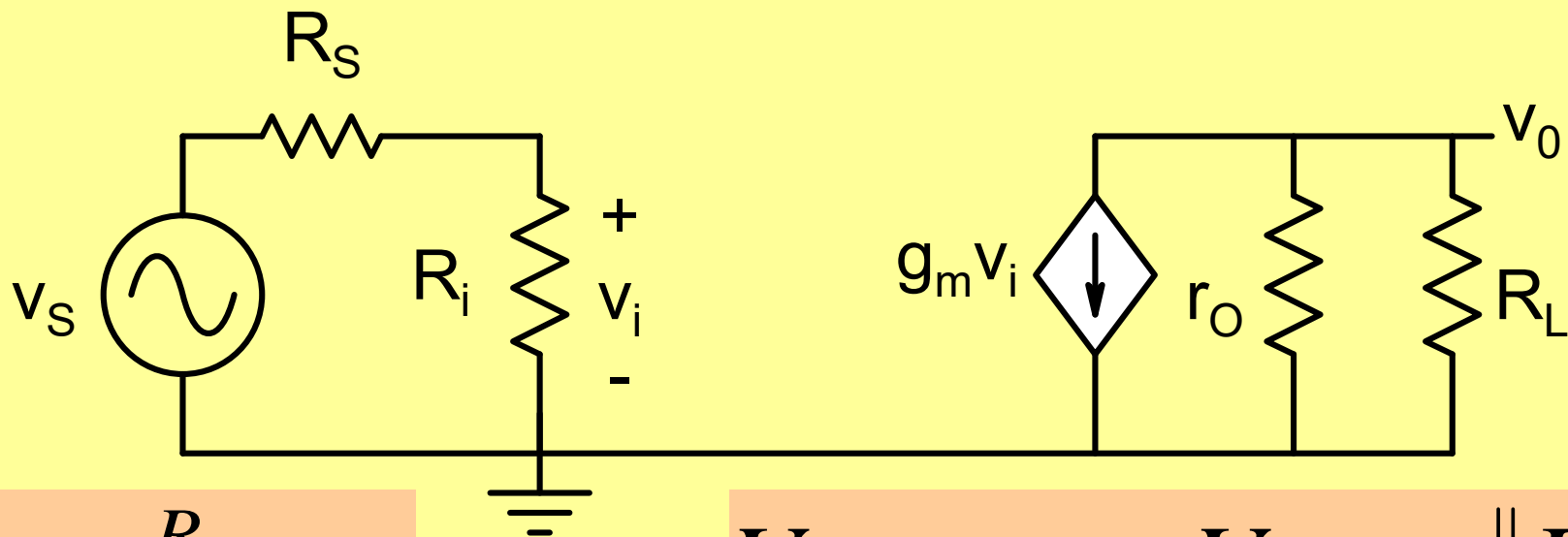


Output conductance:  $g_o = 1 / r_o = \left. \frac{I_o}{V_o} \right|_{V_i=0}$

(Ideally small)

# Voltage Amplifier





$$V_i = \frac{R_i}{R_i + R_S} V_S$$

$$V_o = -g_m V_i \times r_o \parallel R_L$$

$$A_V = \frac{V_o}{V_S} = -g_m r_o \times \frac{R_L}{r_o + R_L} \times \frac{R_i}{R_i + R_S}$$

$$|A_V| \leq g_m \times r_o$$

Necessary Condition for Voltage Amplifications

$$g_m \times r_o > 1$$

# Voltage Amplification

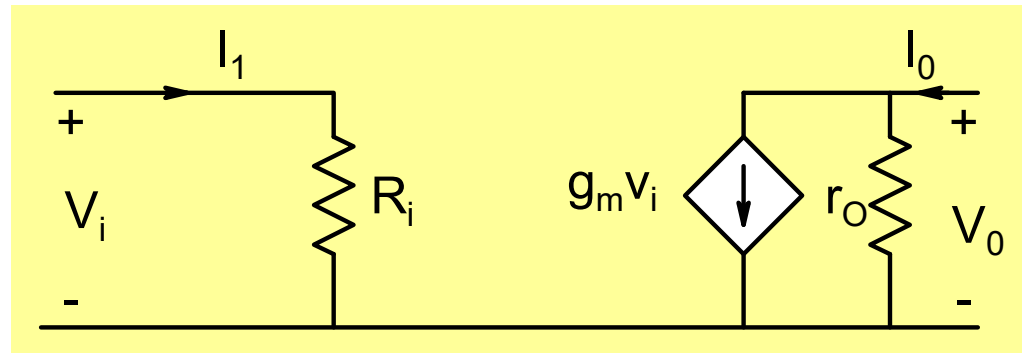
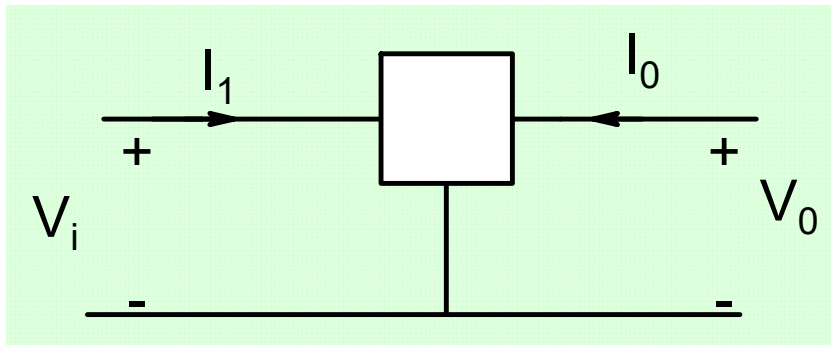
$$g_m r_o \gg 1$$

$$g_m \gg g_o$$

Trans-conductance  $\gg$  Output Conductance

$$g_m = \left. \frac{I_o}{V_i} \right|_{V_o=0}$$

$$g_o = \left. \frac{I_o}{V_o} \right|_{V_i=0}$$



Transistor

# Transistor

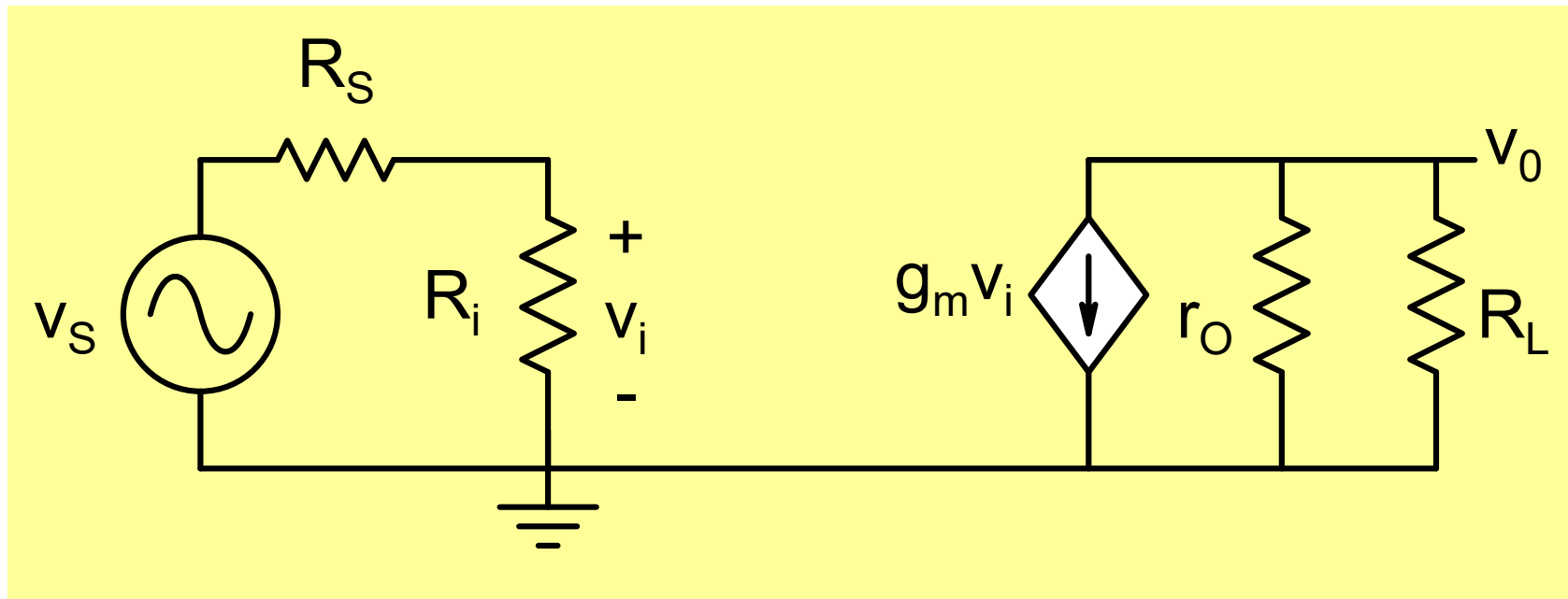
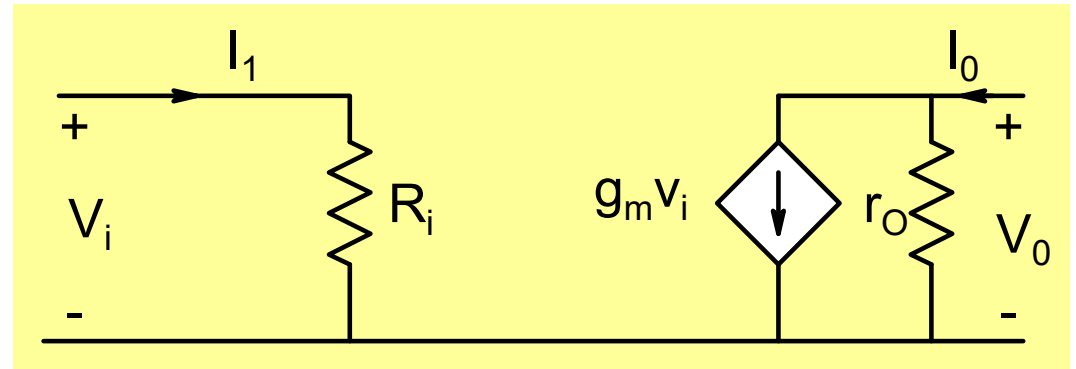
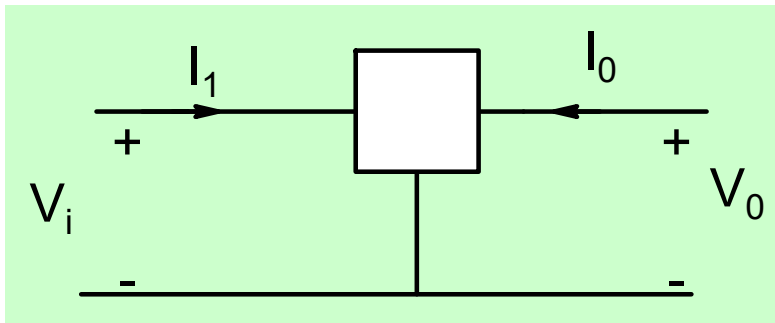
## Trans-resistor



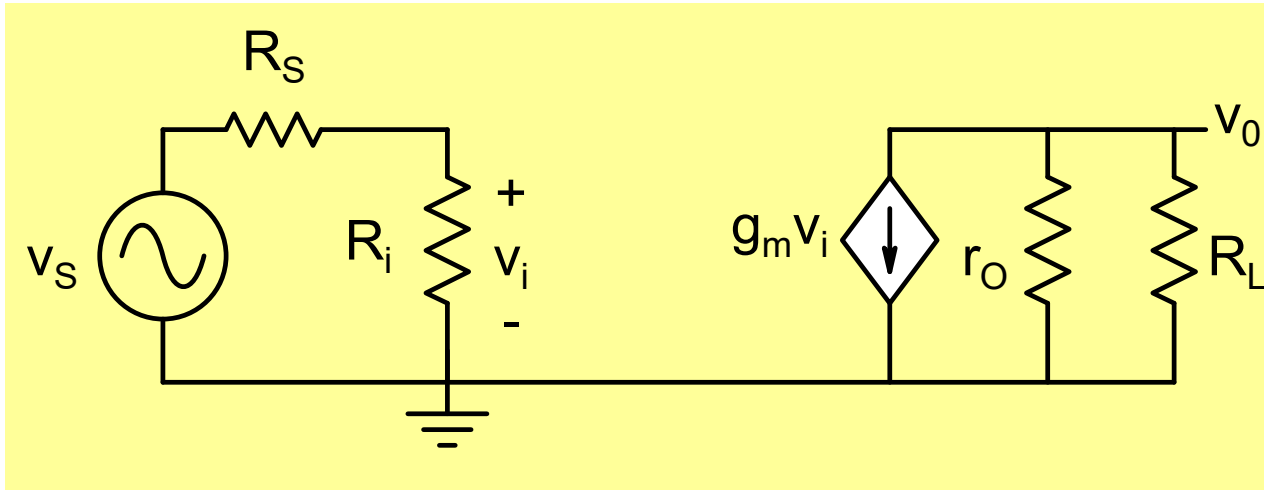
Current  $I_O$  is much more sensitive to  $V_{IN}$  than  $V_O$

- Can be used for voltage amplification
- Can be used as a switch
- Implement logic
- ...





$$A_V = \frac{V_o}{V_S} = -g_m r_o \times \frac{R_L}{r_o + R_L} \times \frac{R_i}{R_i + R_S}$$



$$A_V = \frac{V_o}{V_s} = -g_m r_o \times \frac{R_L}{r_o + R_L} \times \frac{R_i}{R_i + R_S}$$

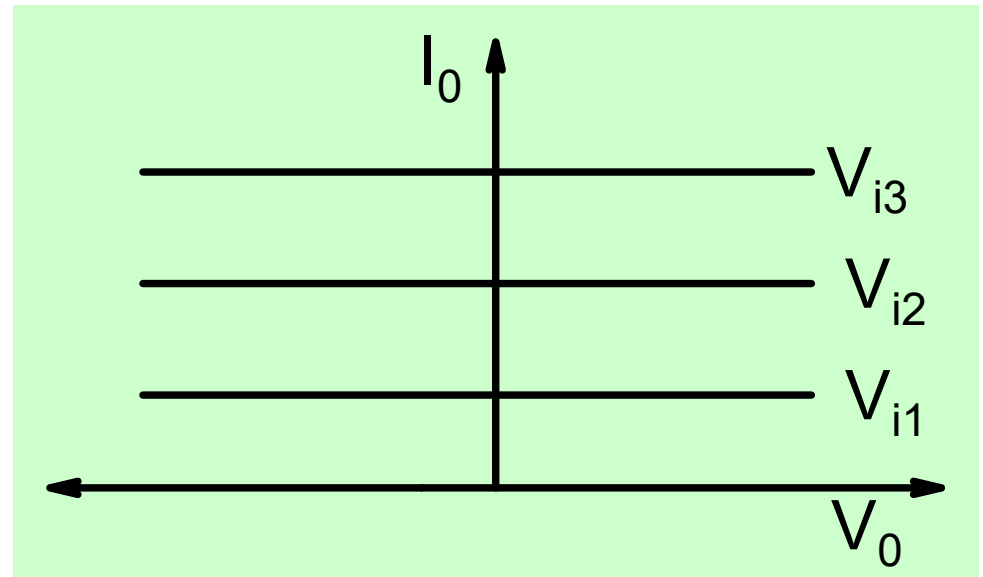
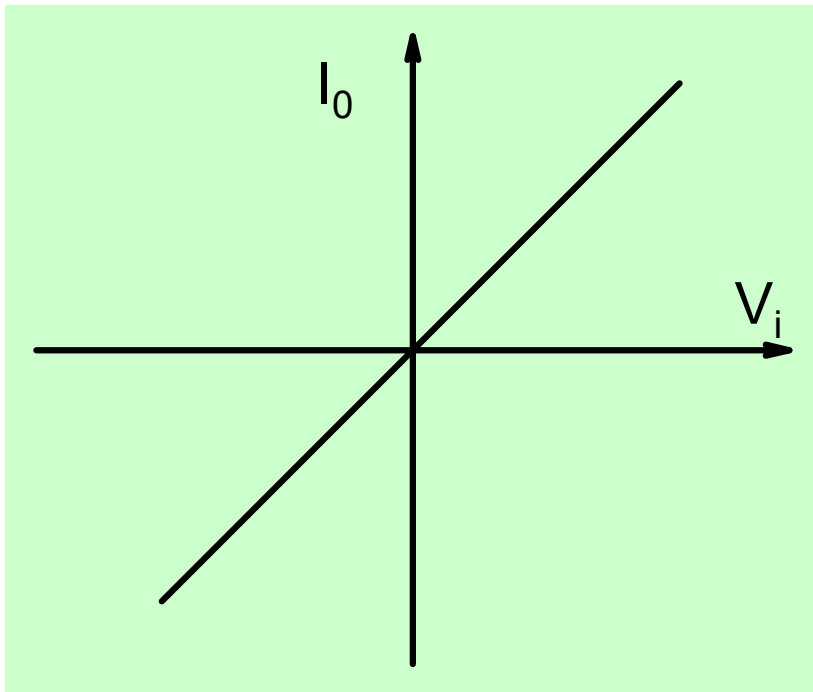
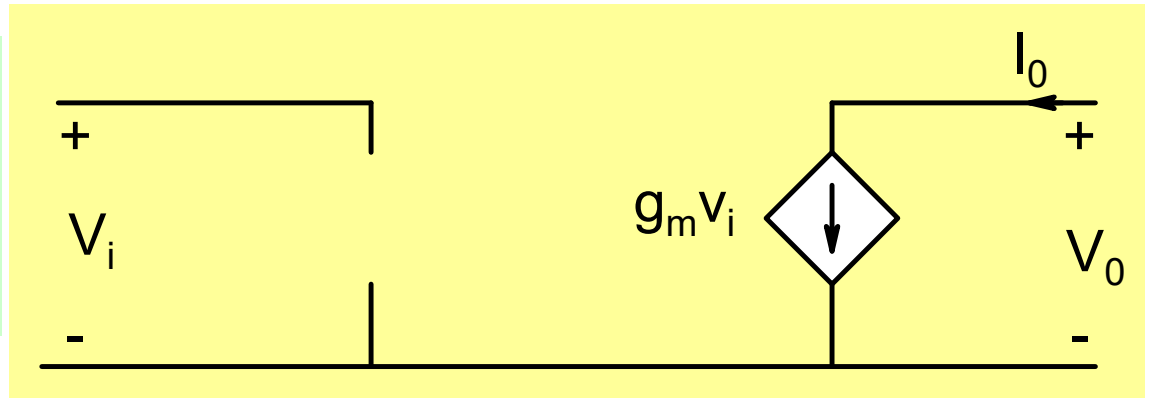
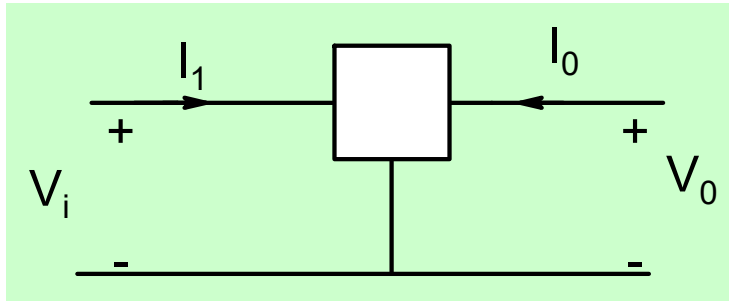
In the ideal case  $r_o$  is infinite

$$A_V = \frac{V_o}{V_s} = -g_m R_L \times \frac{R_i}{R_i + R_S}$$

We would ideally like input resistance  $R_i$  to be infinite as well !

$$A_V = -g_m R_L$$

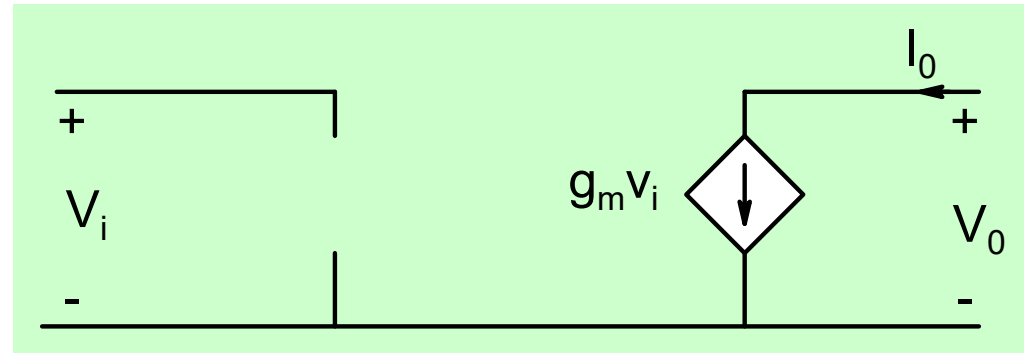
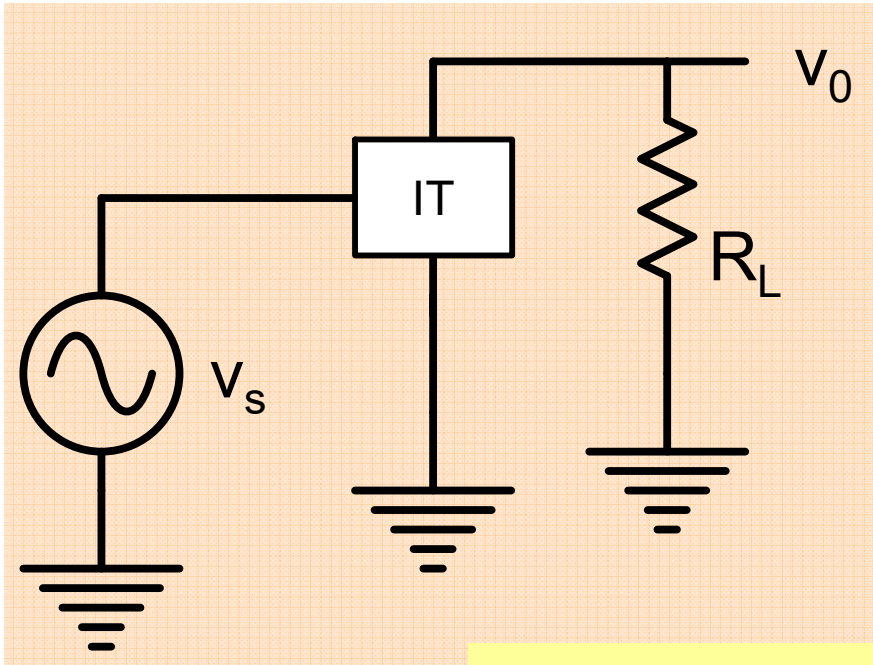
# An ideal 3-terminal device for Voltage Amplification



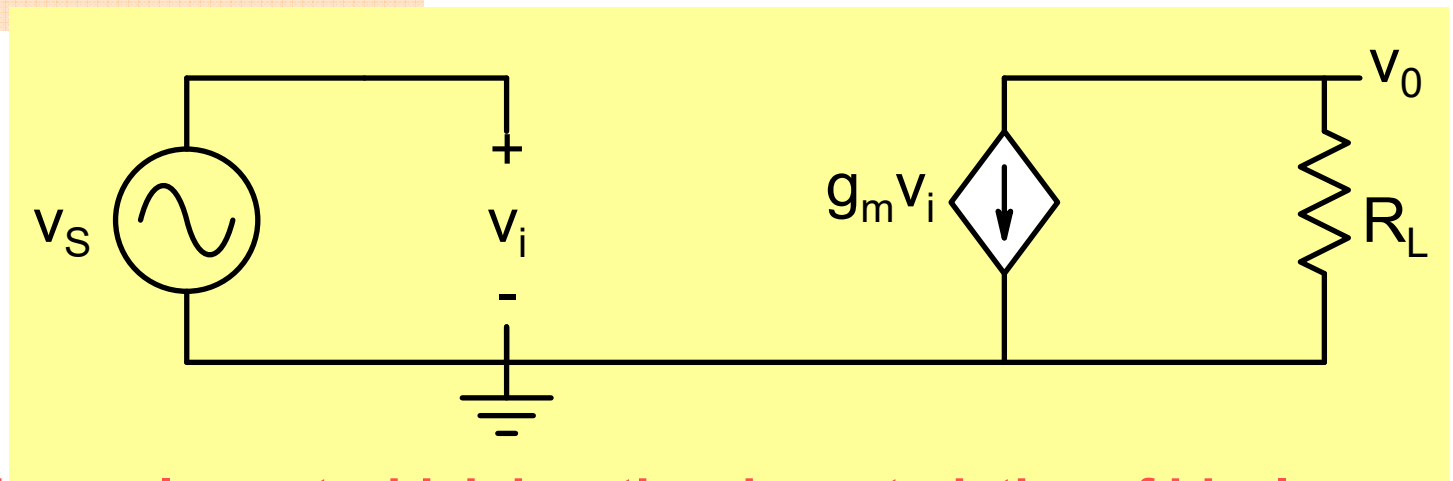
## Ideal Transistor Characteristics

# Ideal Transistor (IT)

Making a voltage amplifier with an ideal transistor is straightforward

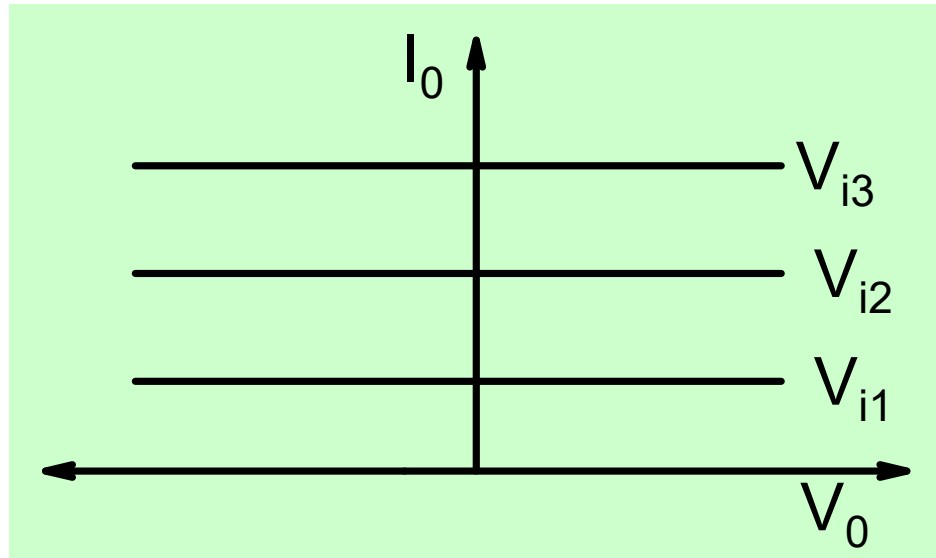
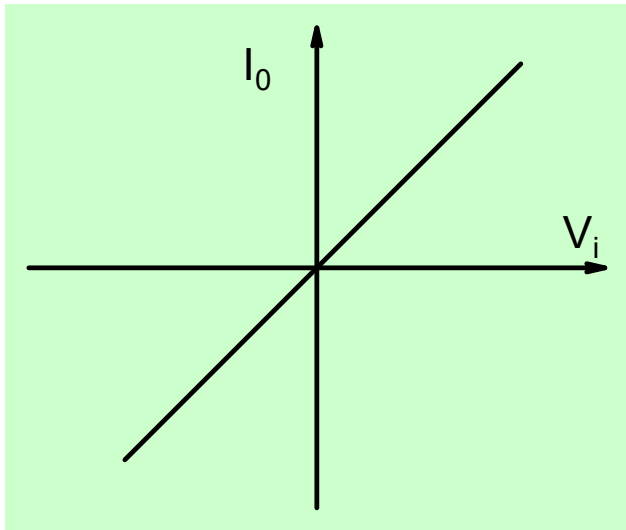


$$A_V = \frac{v_o}{v_s} = -g_m R_L$$

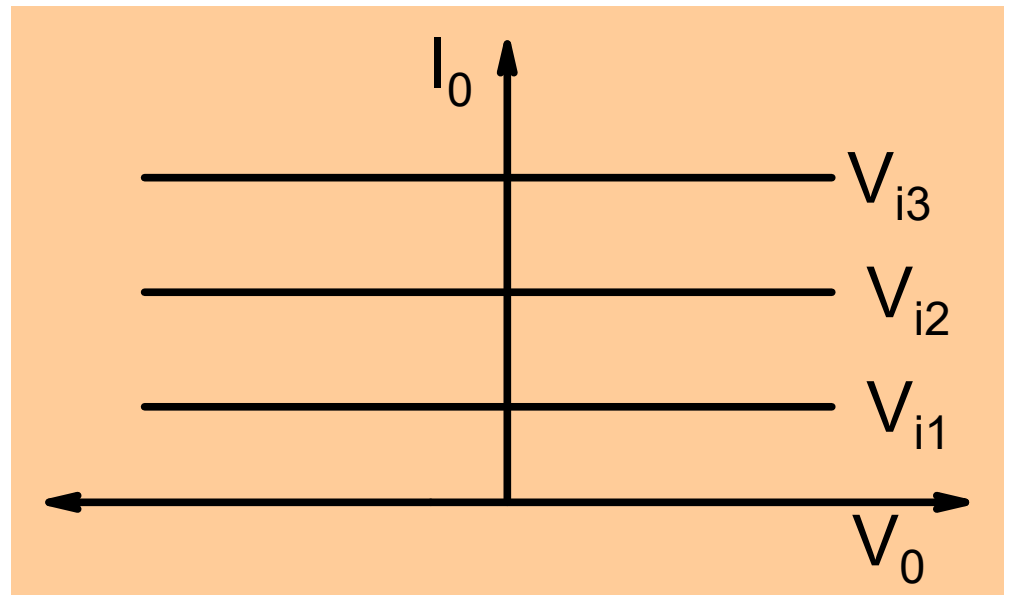
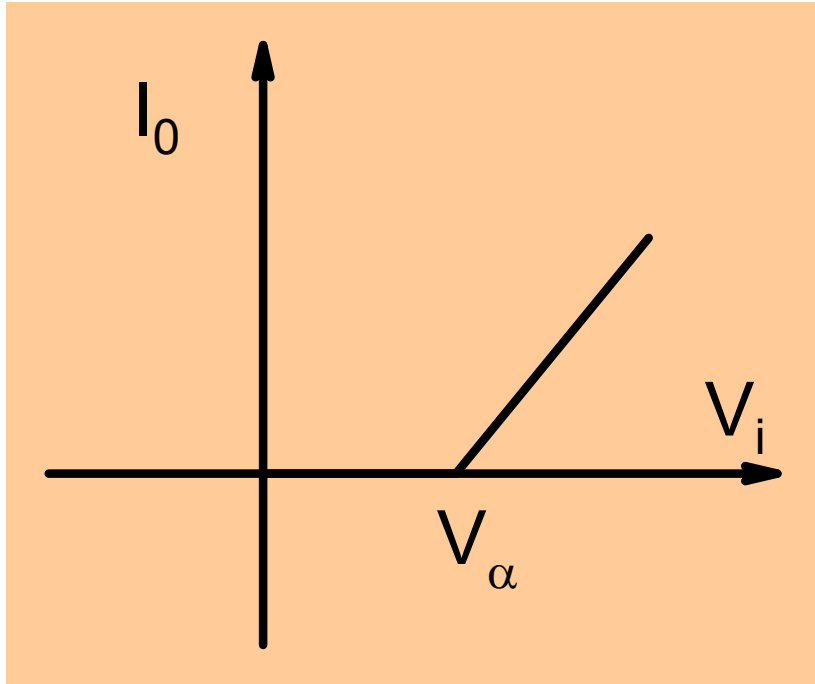


In practice there is no element which has the characteristics of ideal transistor !

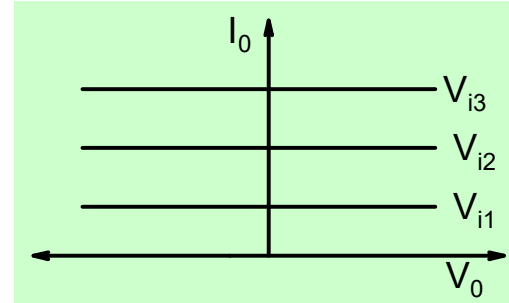
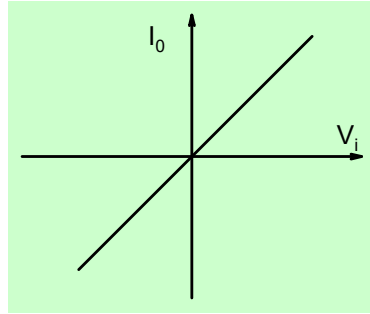
## Ideal transistor



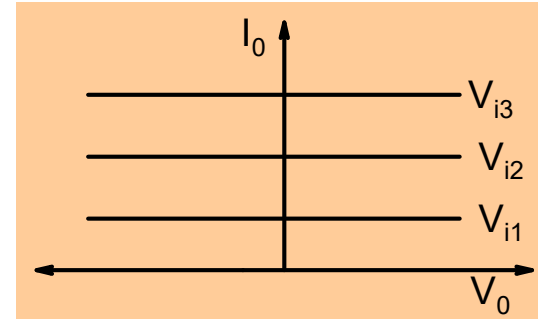
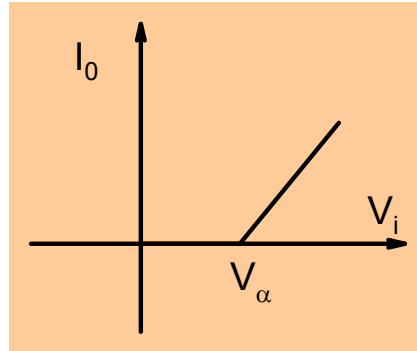
## Device X



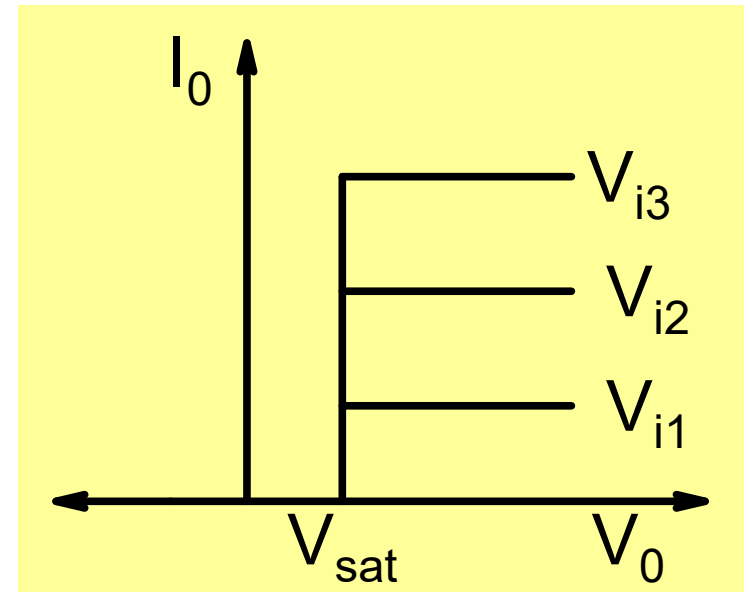
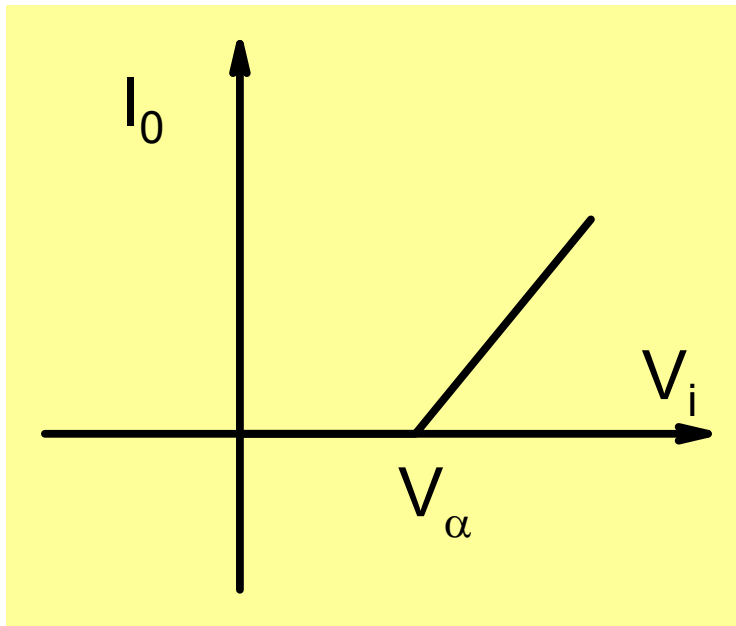
## Ideal transistor



## Device X

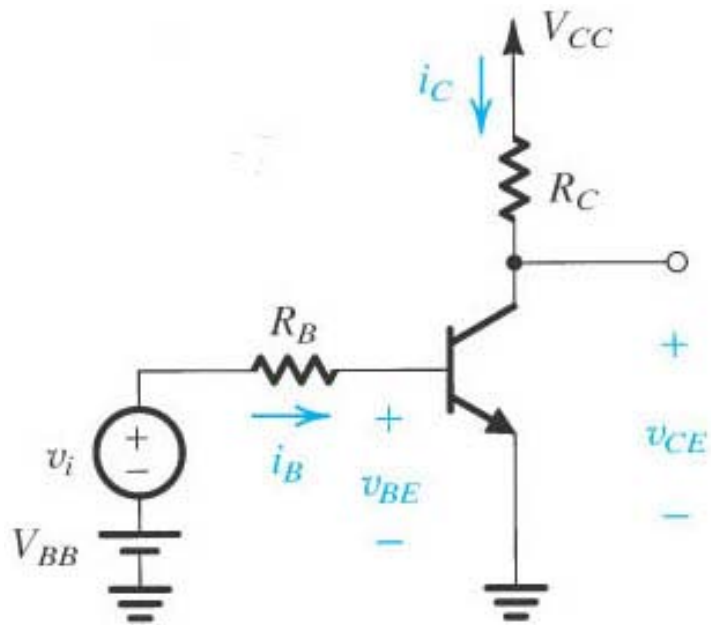


## Device Y

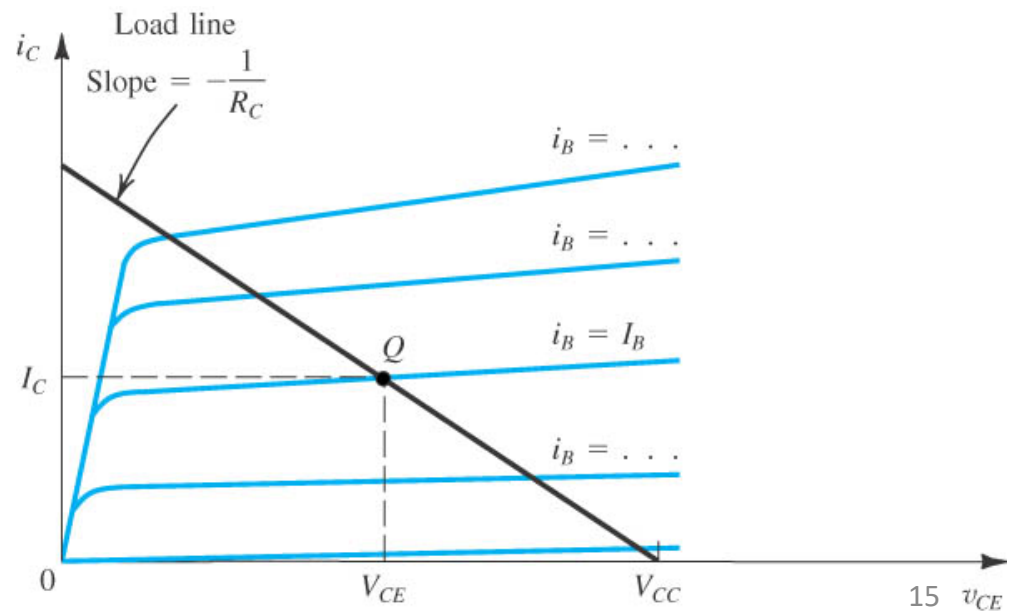
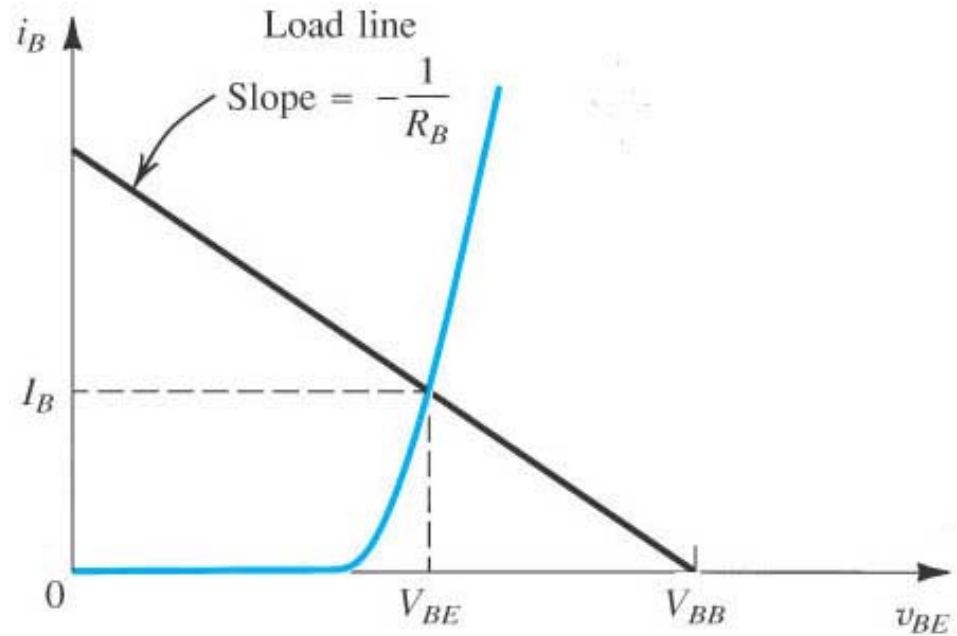


How do we use elements such as X, Y etc to make amplifiers?

# Bipolar Junction Transistor: BJT

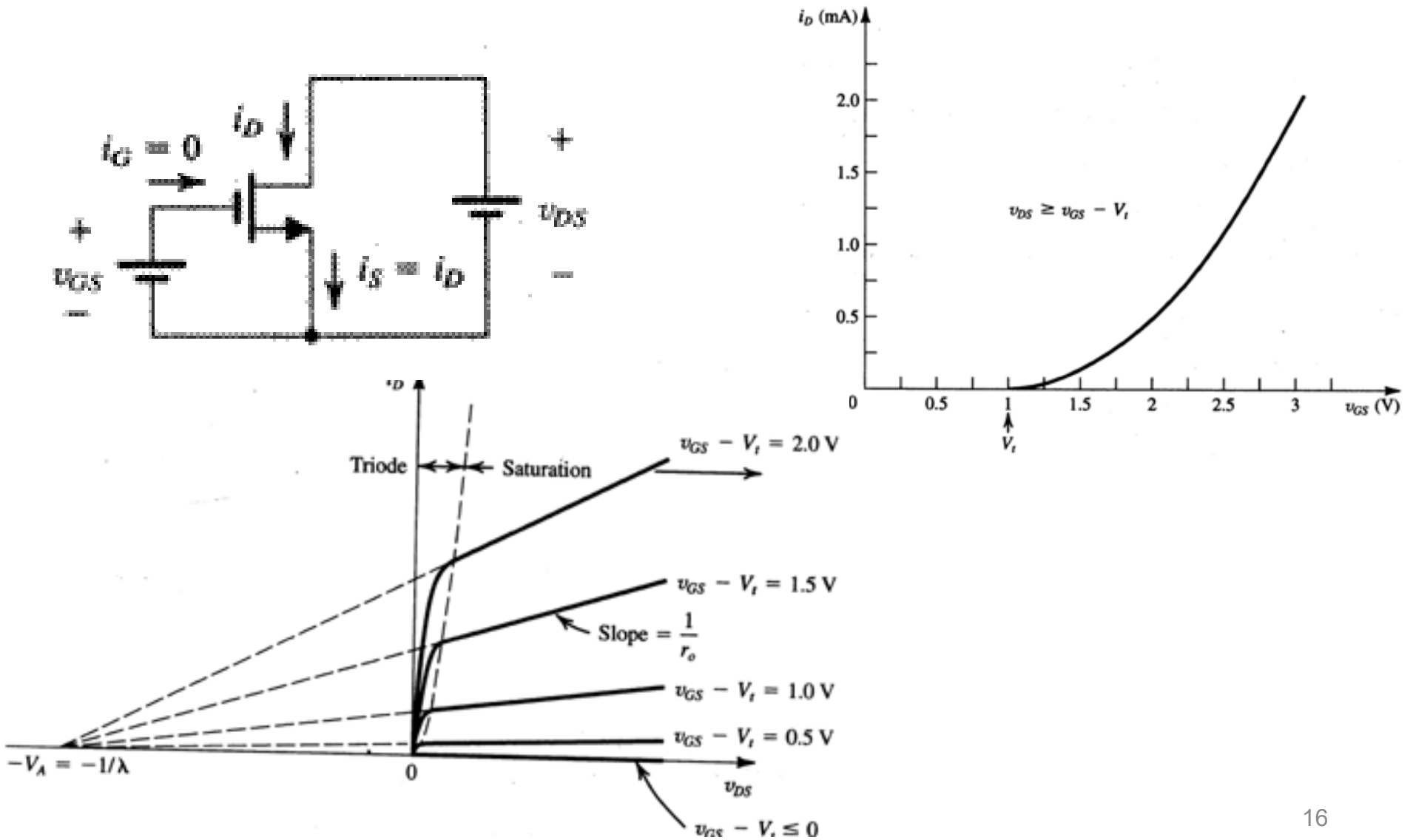


$$I_C = \beta_F I_B$$



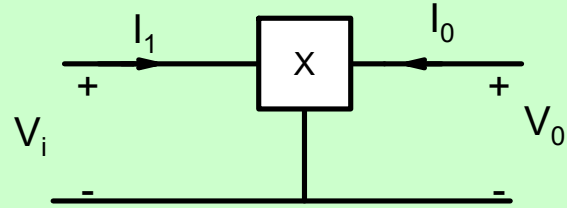
# Metal Oxide Semiconductor Field Effect Transistor

## MOSFET



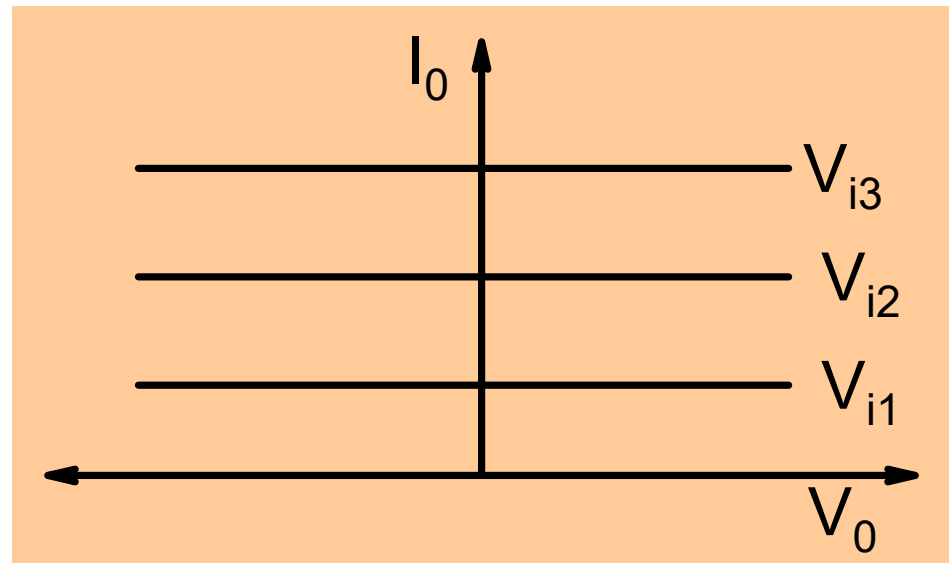
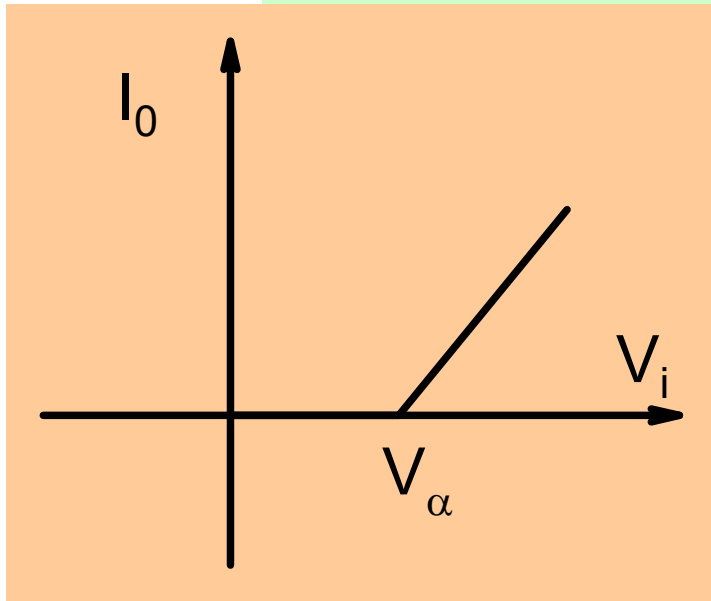


## Device X

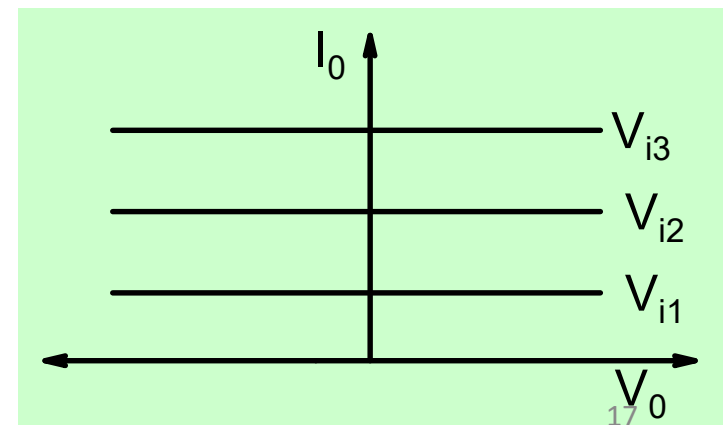
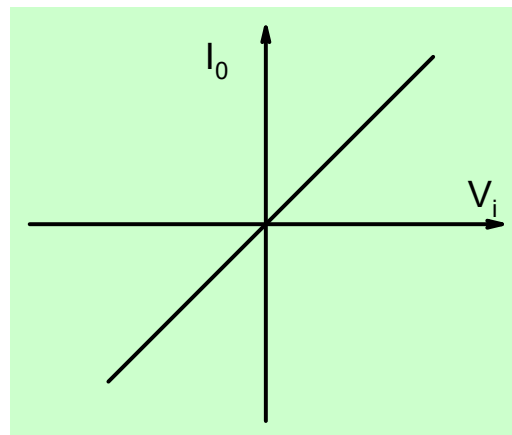


$$I_o = 0 \quad \text{for } V_i \leq V_\alpha$$

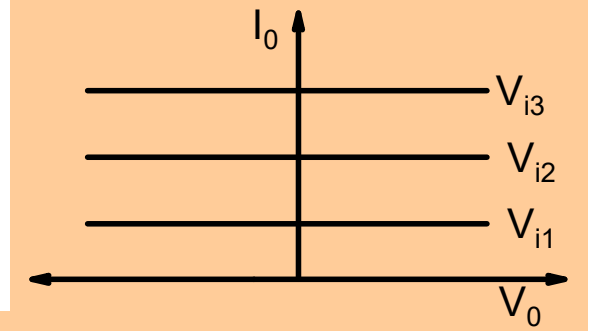
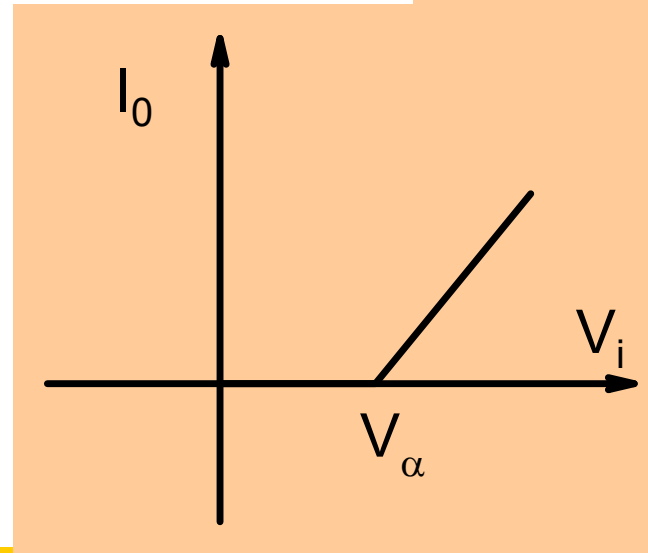
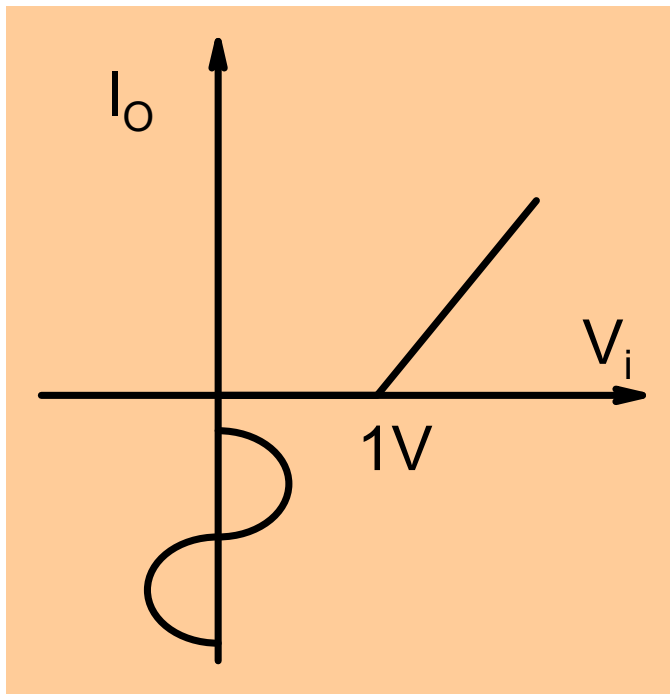
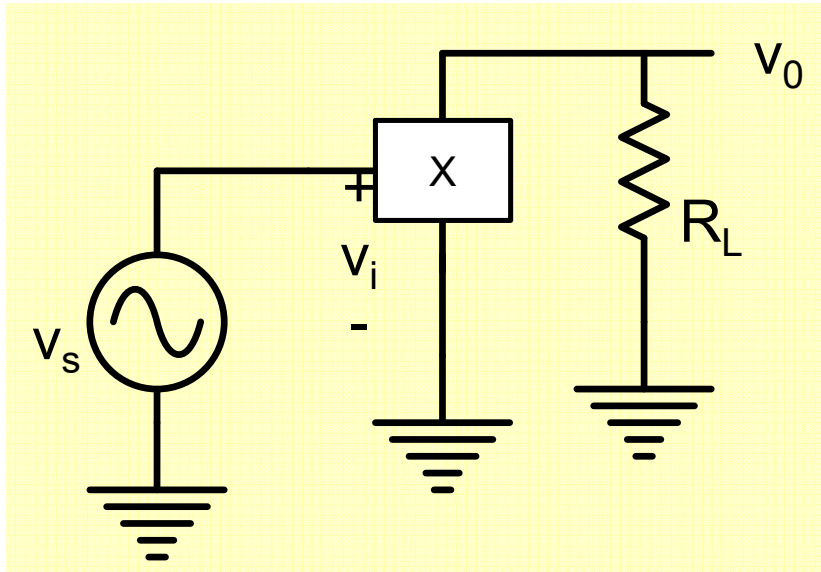
$$= g_m \times (V_i - V_\alpha) \quad \text{for } V_i > V_\alpha$$



## Ideal Characteristics



## How do we use device X to make an amplifier?



$$V_{\alpha} = 1V; g_m = 0.01\Omega^{-1}$$

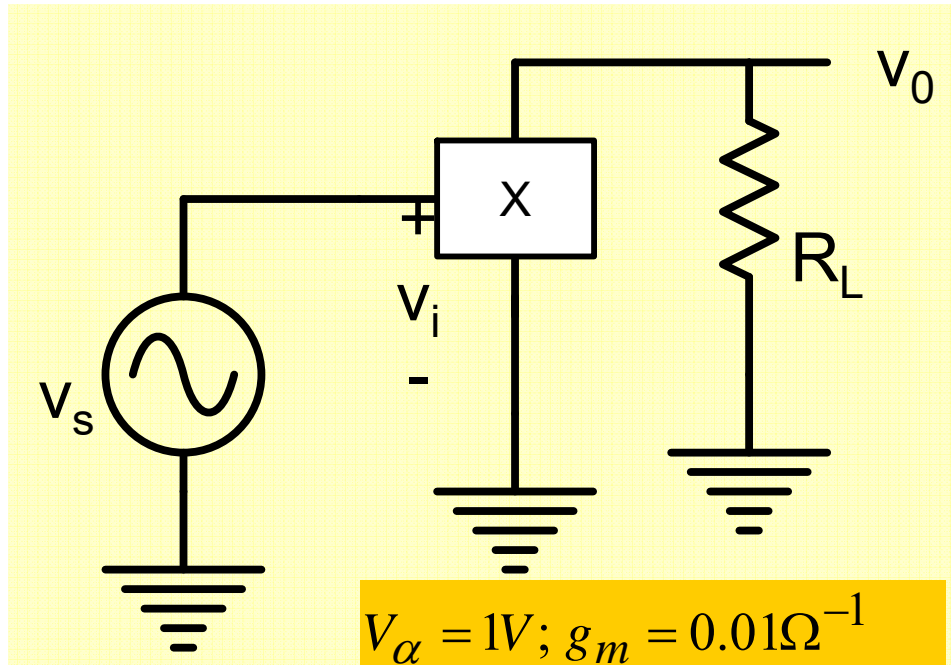
$$R_L = 1K; v_s = 0.5V \sin \omega t$$

$$I_O = 0 \Rightarrow V_O = 0$$

No Amplification

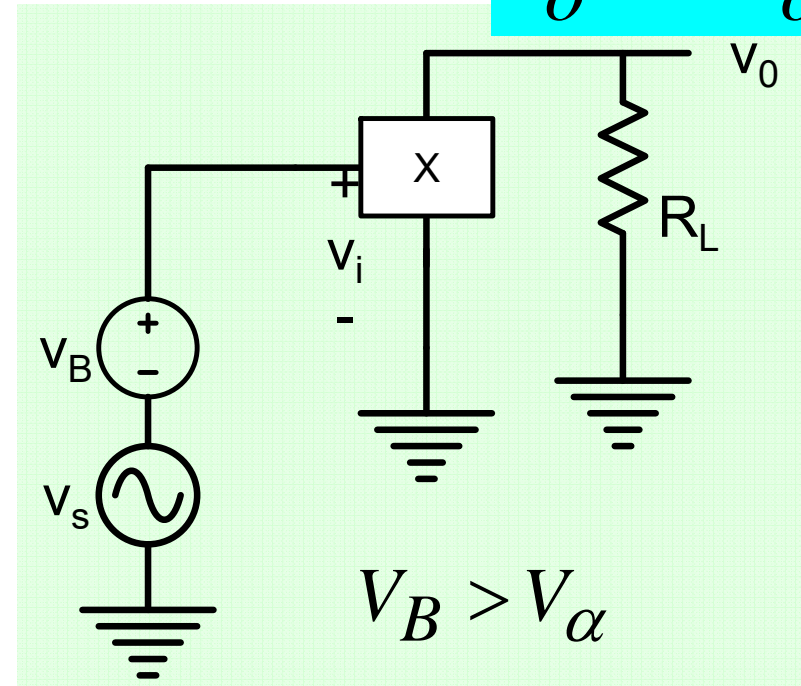
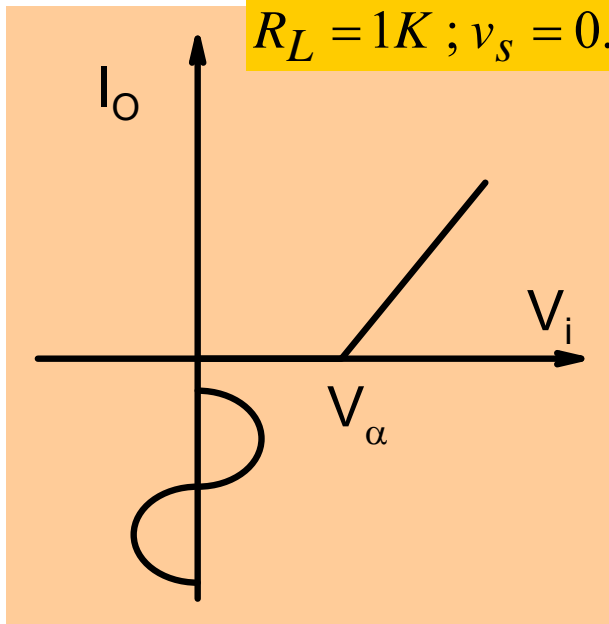
How do we use device X to make an amplifier?

$$V_o = -I_o R_L$$

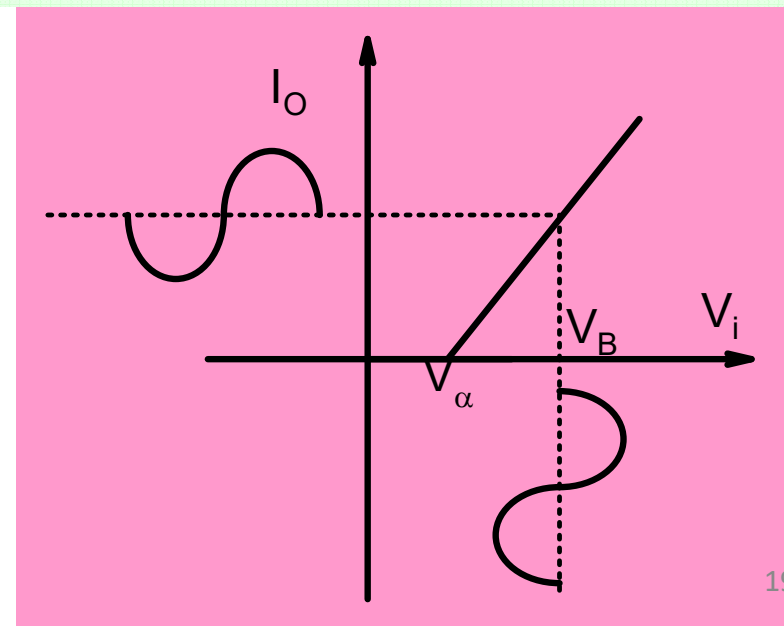


$$V_{\alpha} = 1V; g_m = 0.01\Omega^{-1}$$

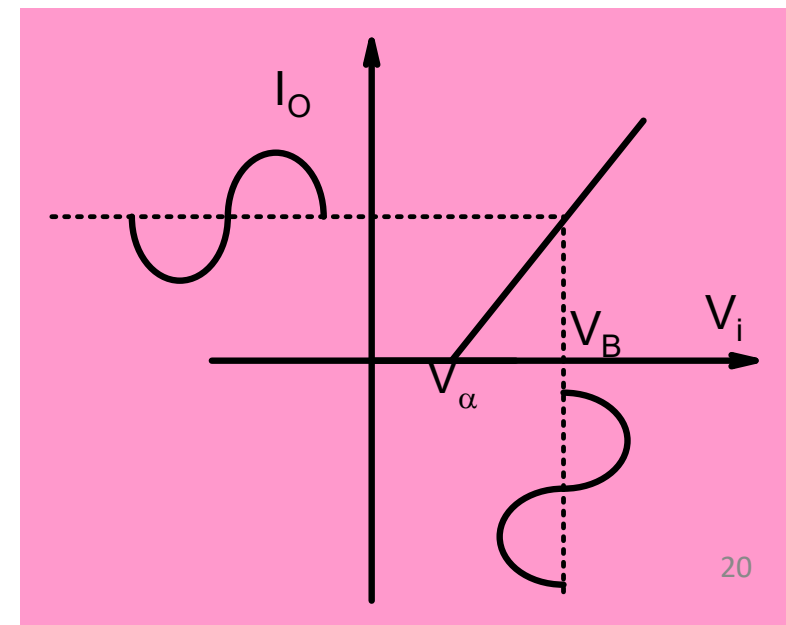
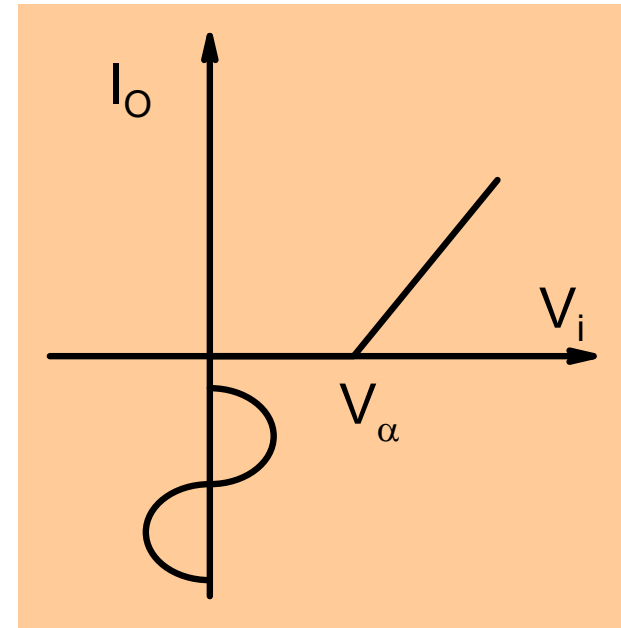
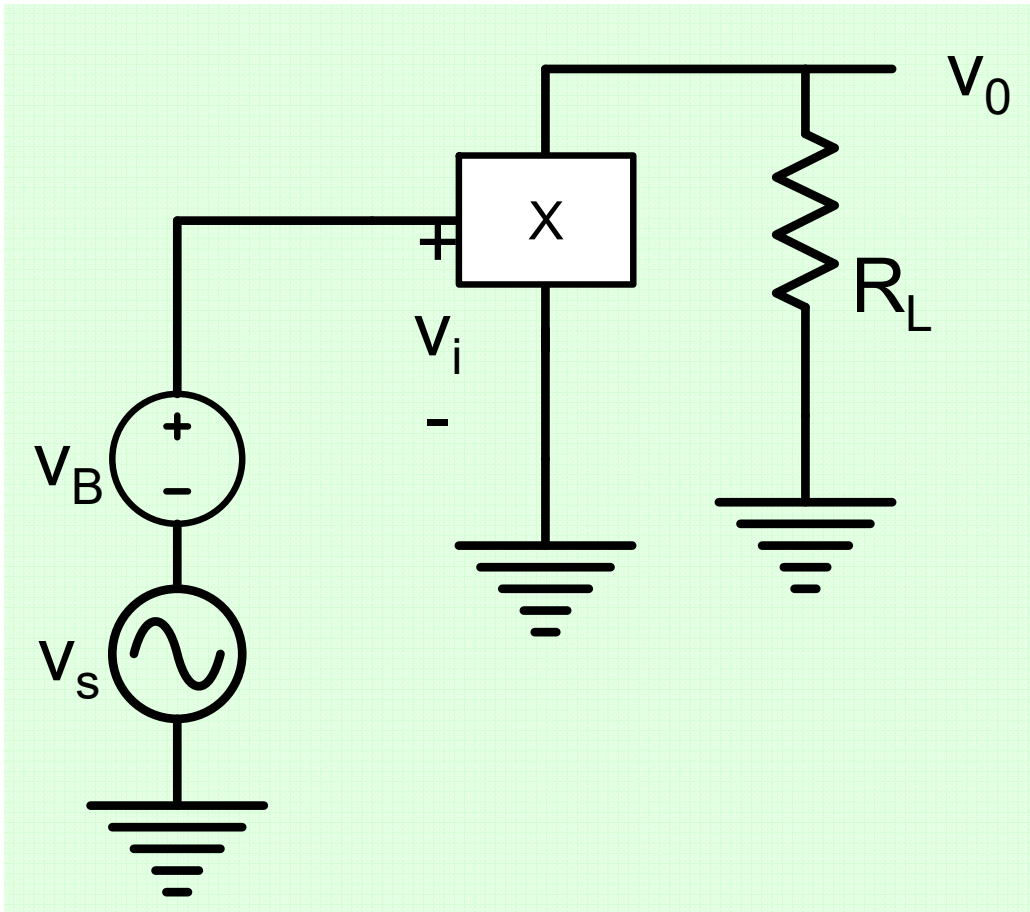
$$R_L = 1K; v_s = 0.5V \sin \omega t$$



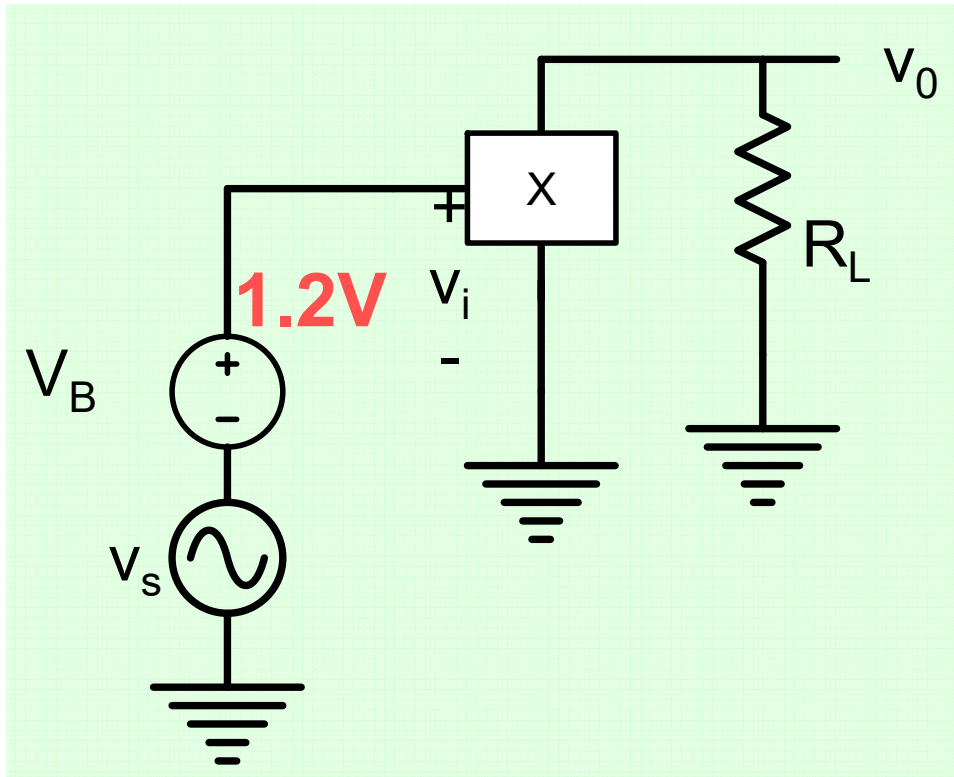
$$V_B > V_{\alpha}$$



When only a part of device characteristics is suitable for amplification, then we need to push the device into that region by applying suitable bias voltages. This process is called **BIASING**

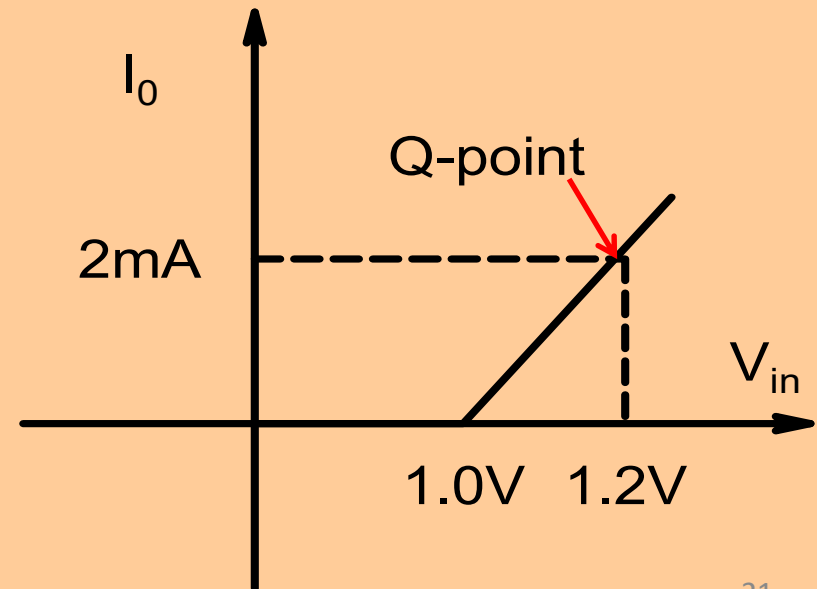


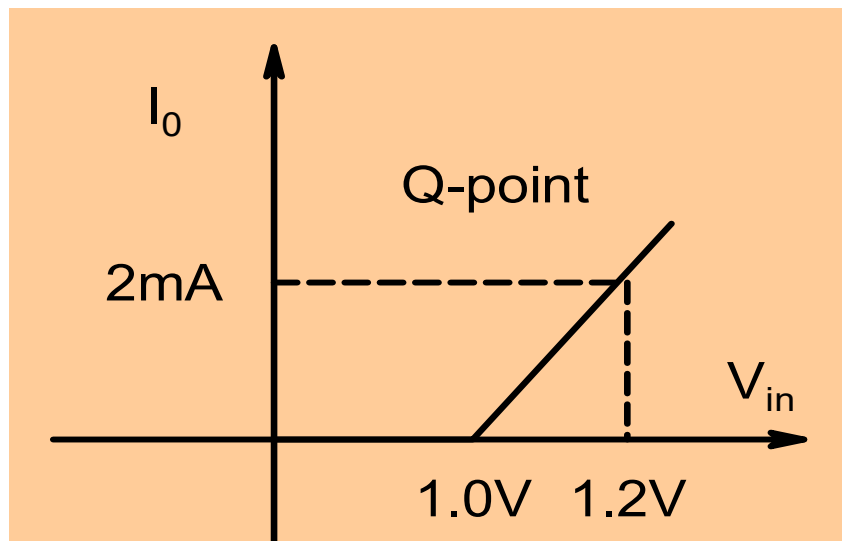
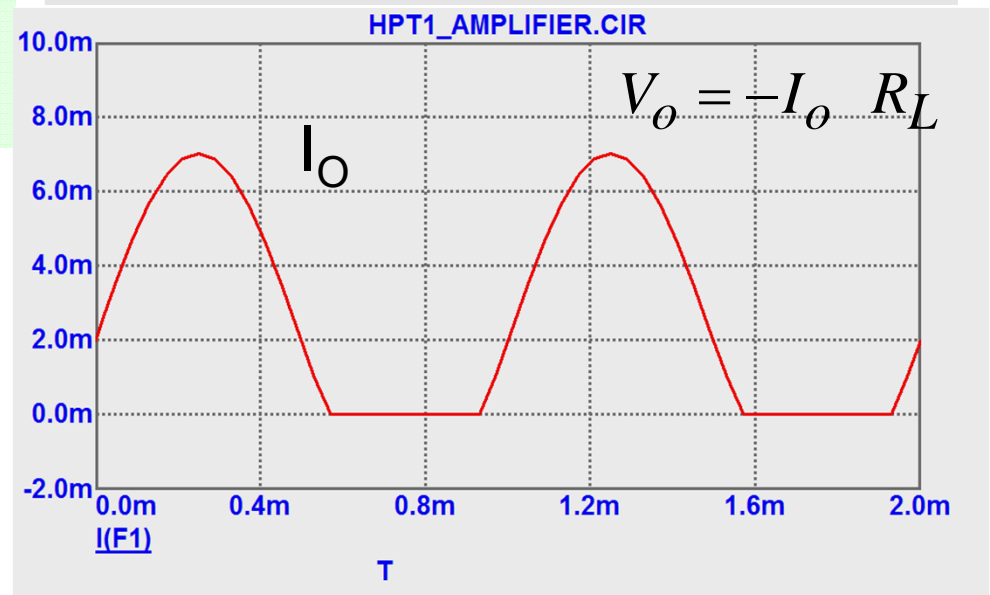
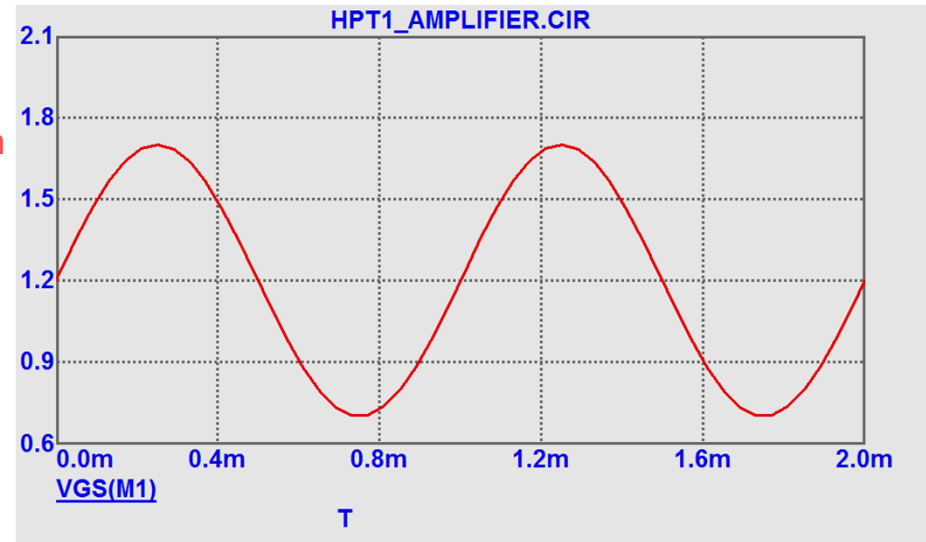
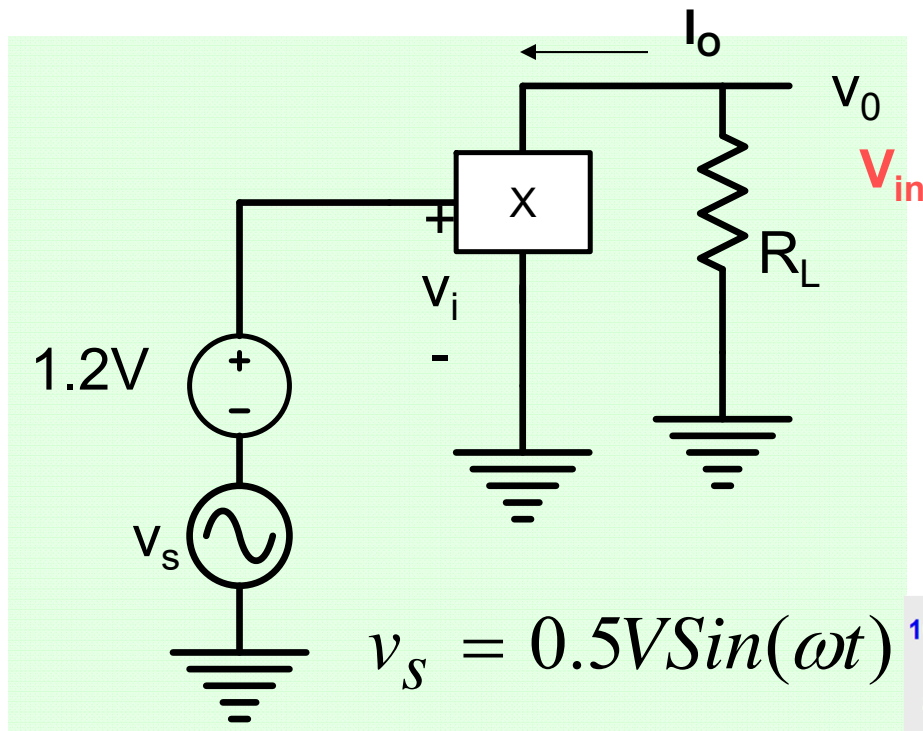
## How should one choose the bias voltage $V_B$ ?



$$v_s = 0.5V \sin \omega t$$

Quiescent point or Bias point





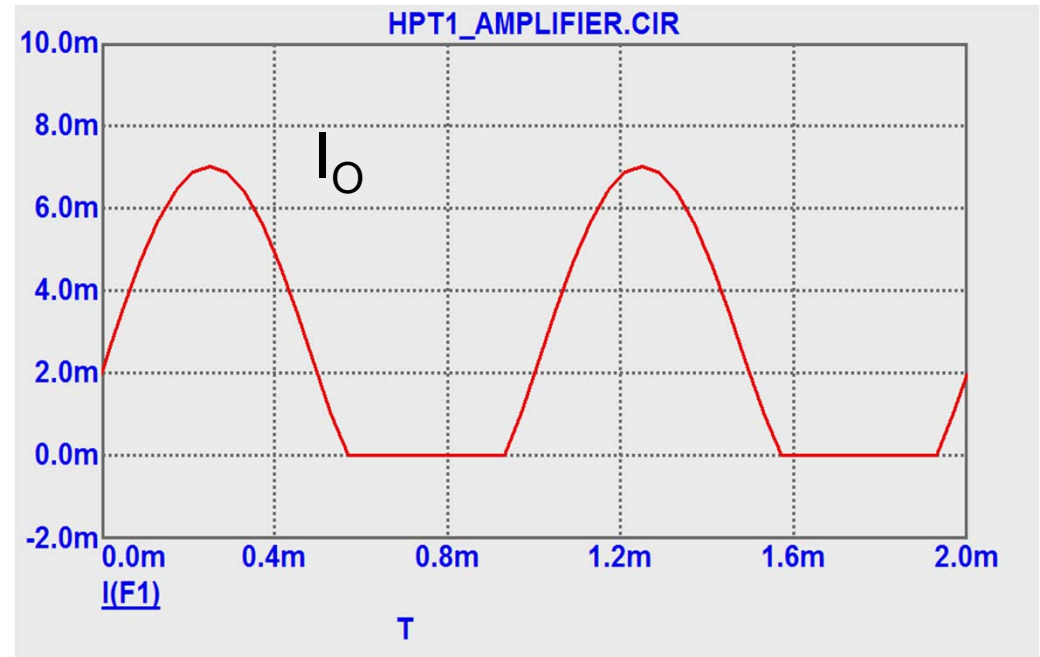
$$V_{\alpha} = 1V; g_m = 0.01\Omega^{-1}$$

$$\begin{aligned}
 I_o &= 0 && \text{for } V_i \leq V_{\alpha} \\
 &= g_m \times (V_i - V_{\alpha}) && \text{for } V_i > V_{\alpha}
 \end{aligned}$$

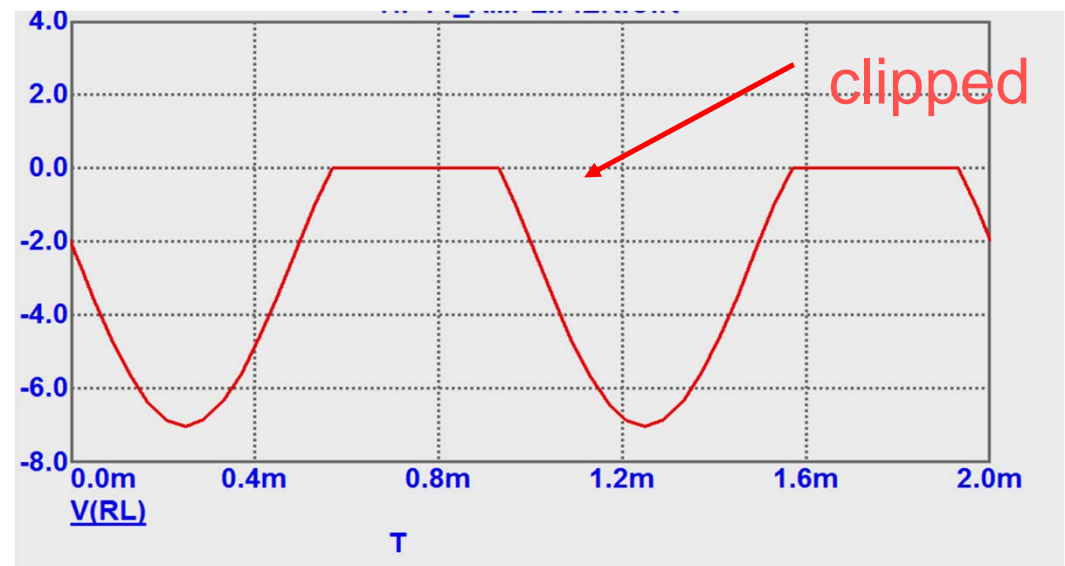
Output voltage is distorted !

$$R_L = 1\text{k}\Omega$$

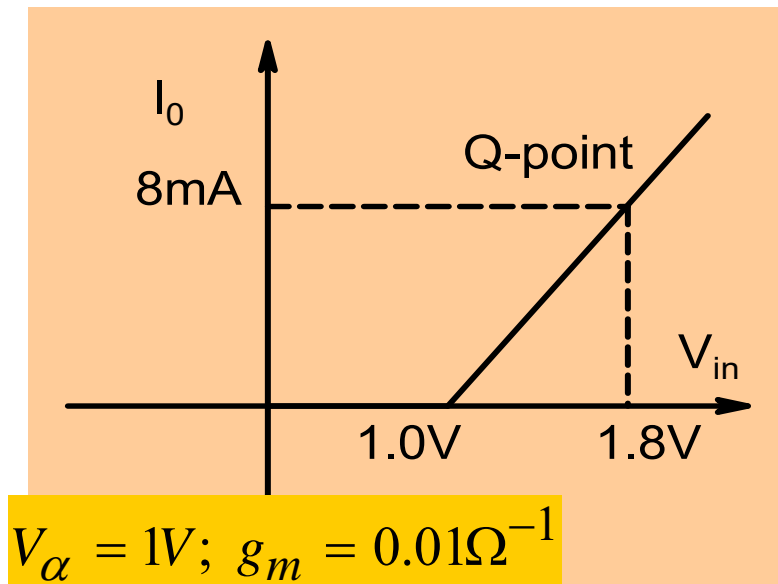
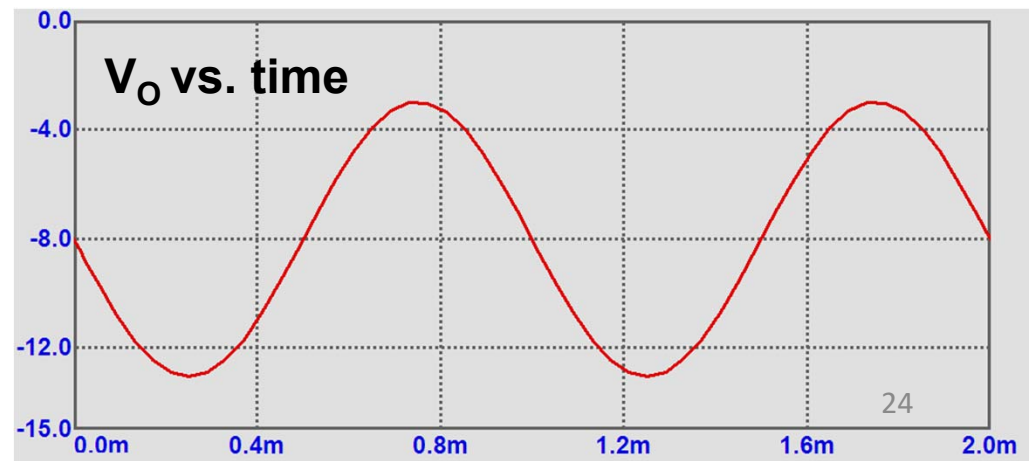
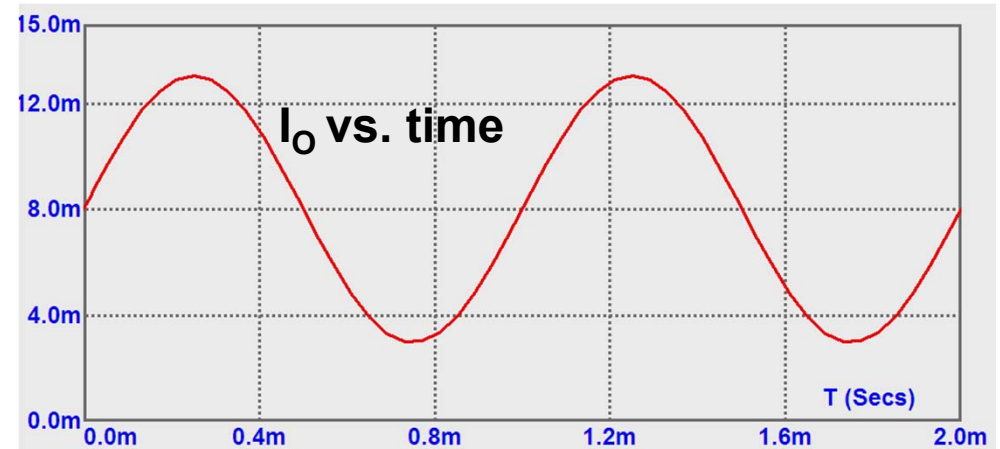
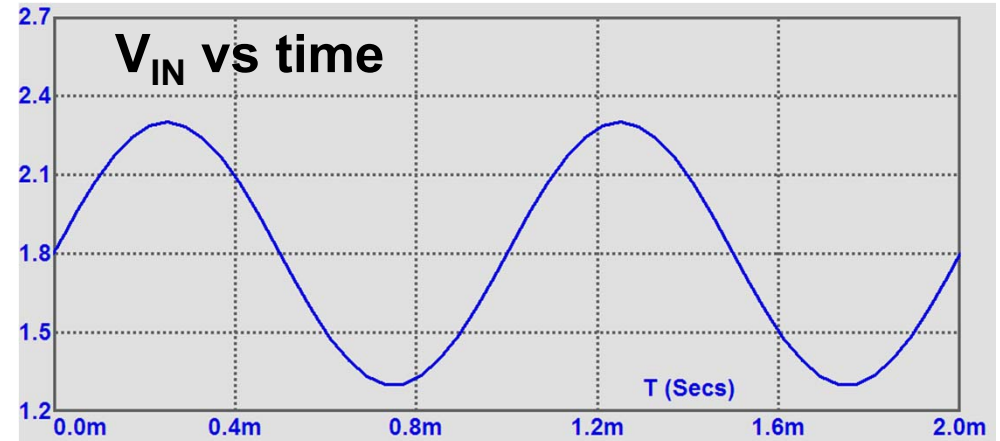
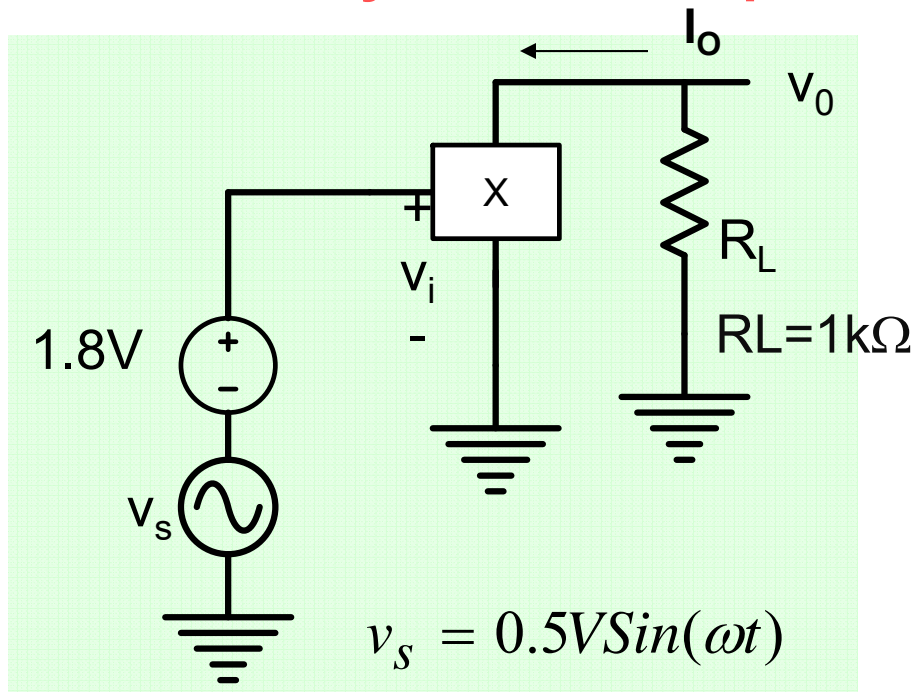
$$V_O = -I_O R_L$$



Need to choose a proper value of biasing Voltage

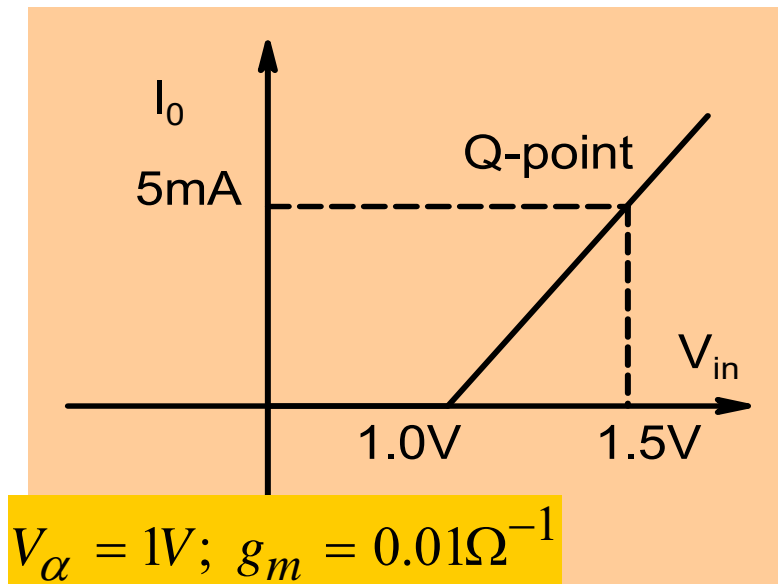
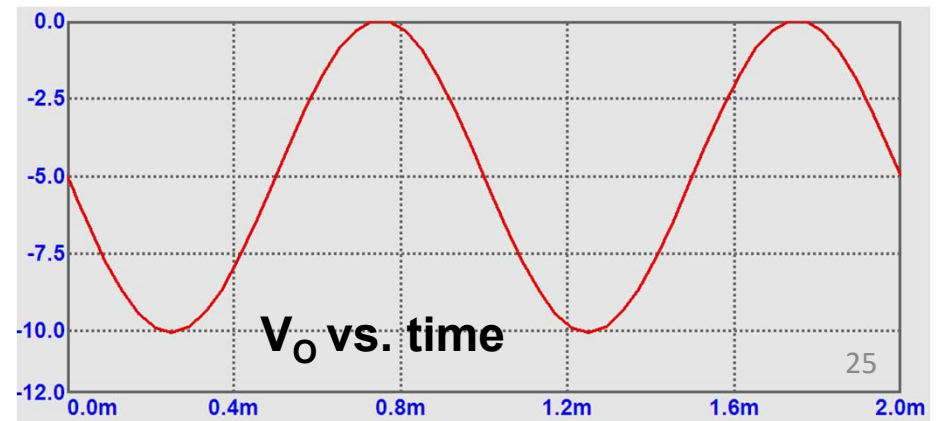
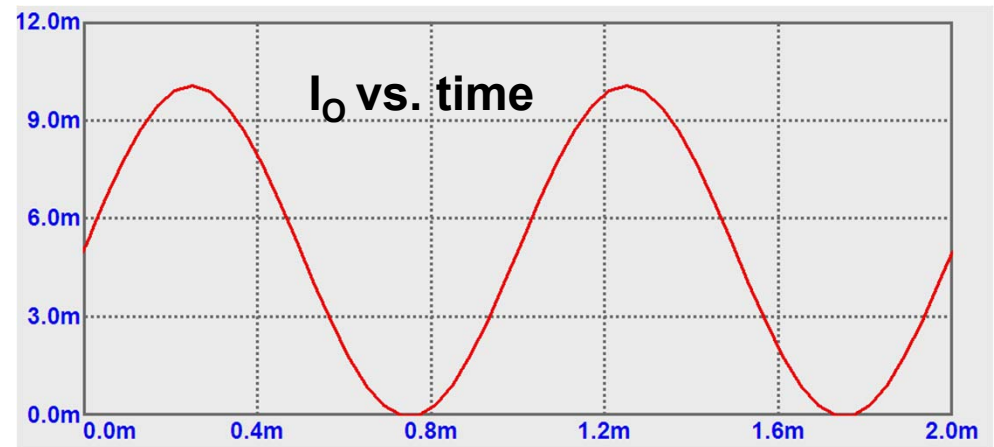
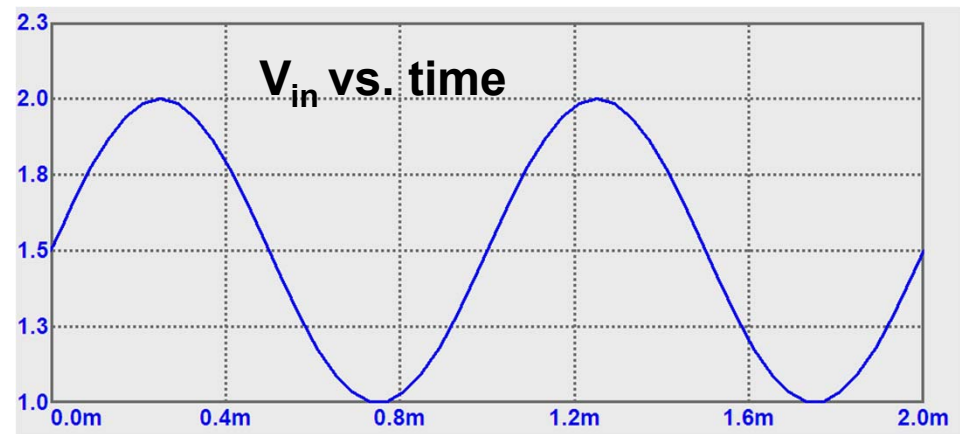
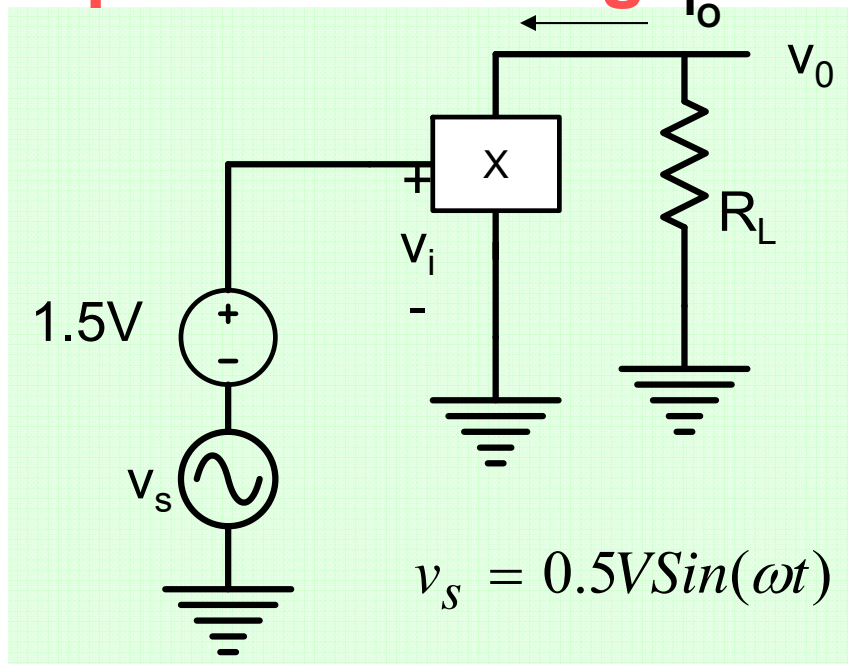


# Unnecessary Power Dissipation

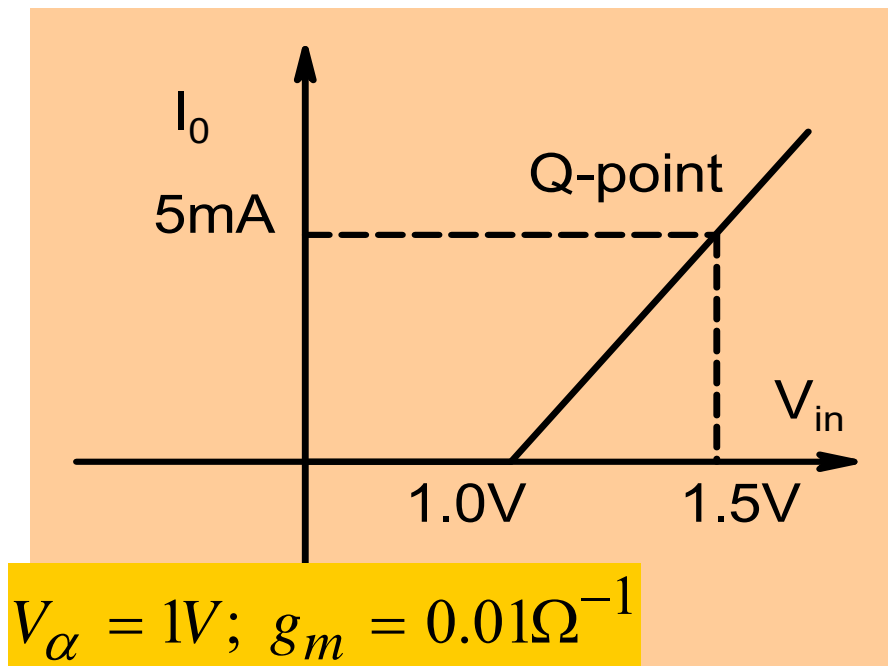
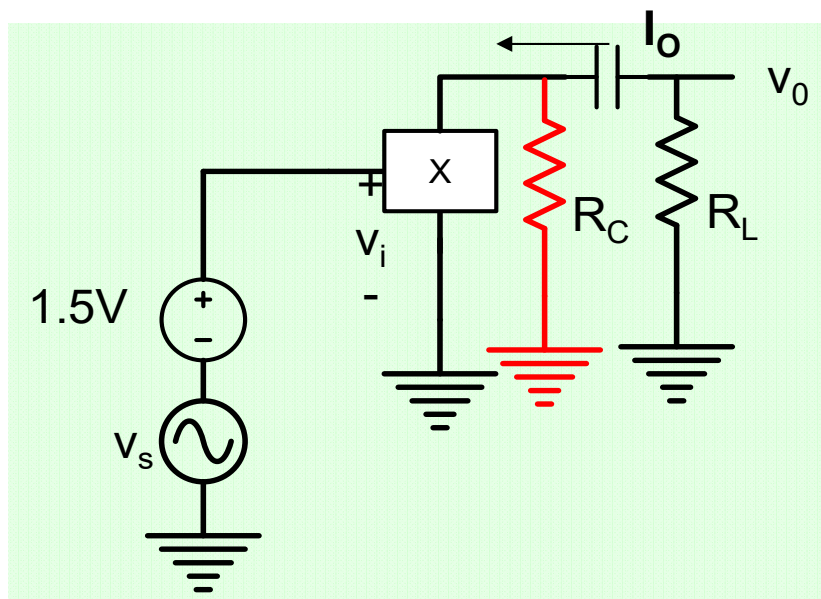
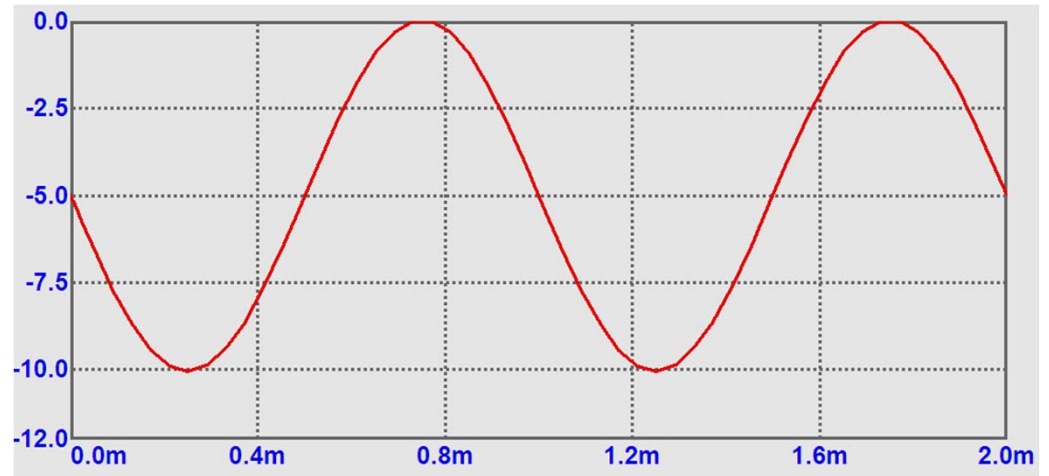
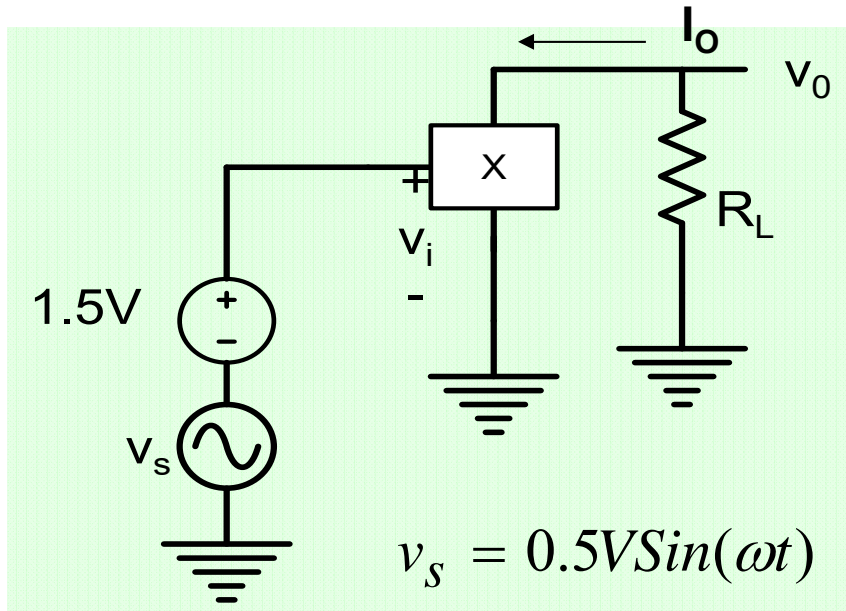


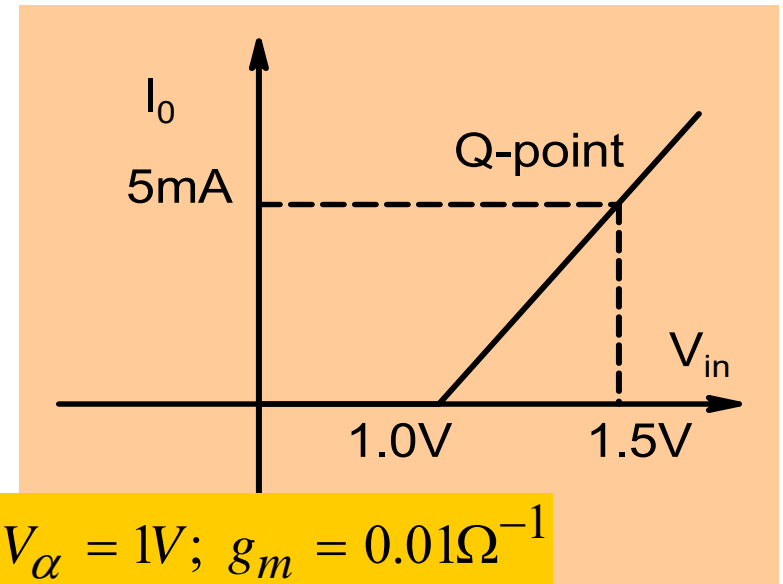
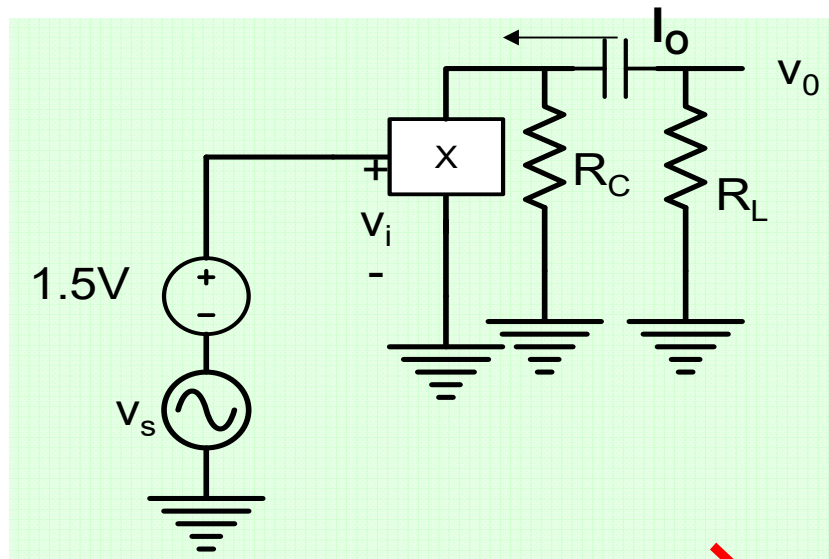


# Optimum Biasing ?



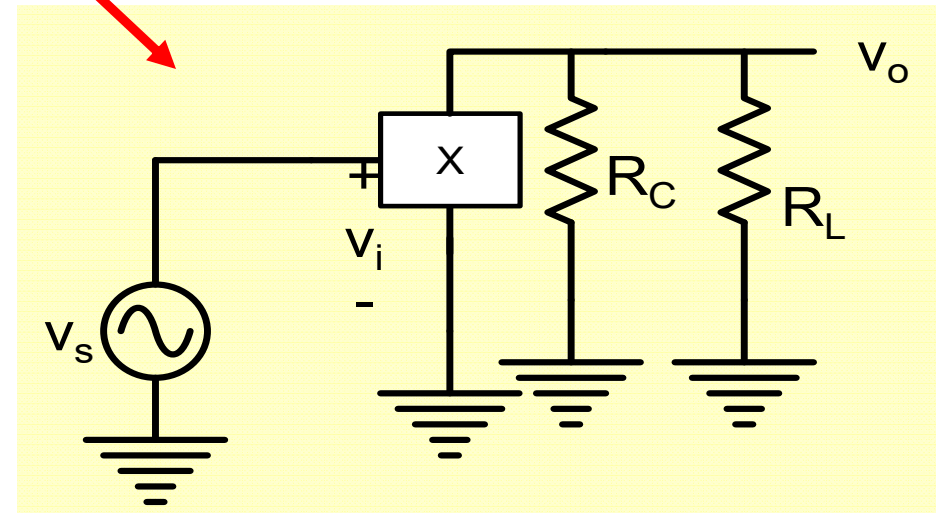
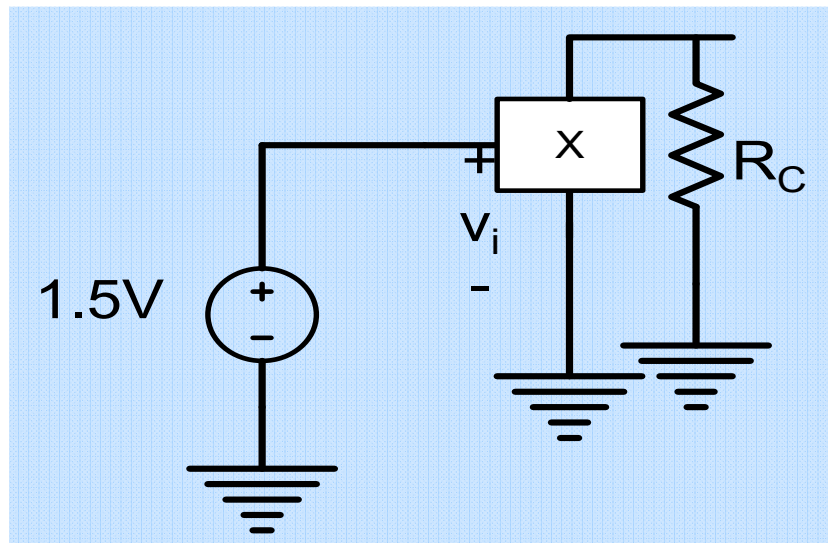
# How do we get rid of unwanted dc voltage at the output ?



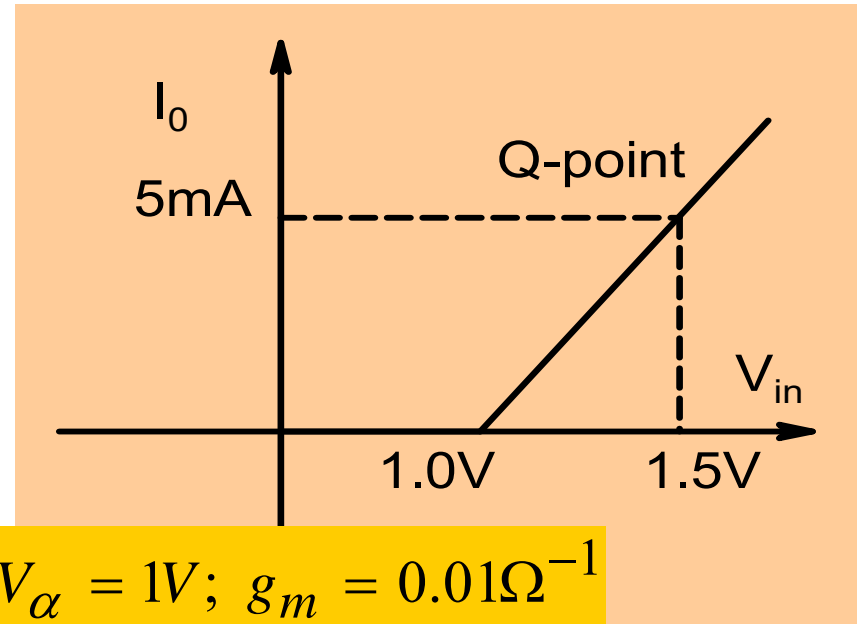
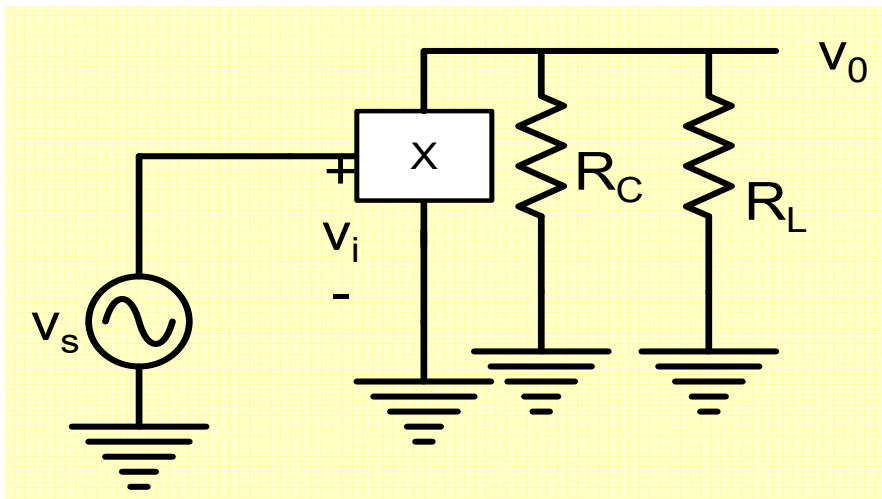


dc

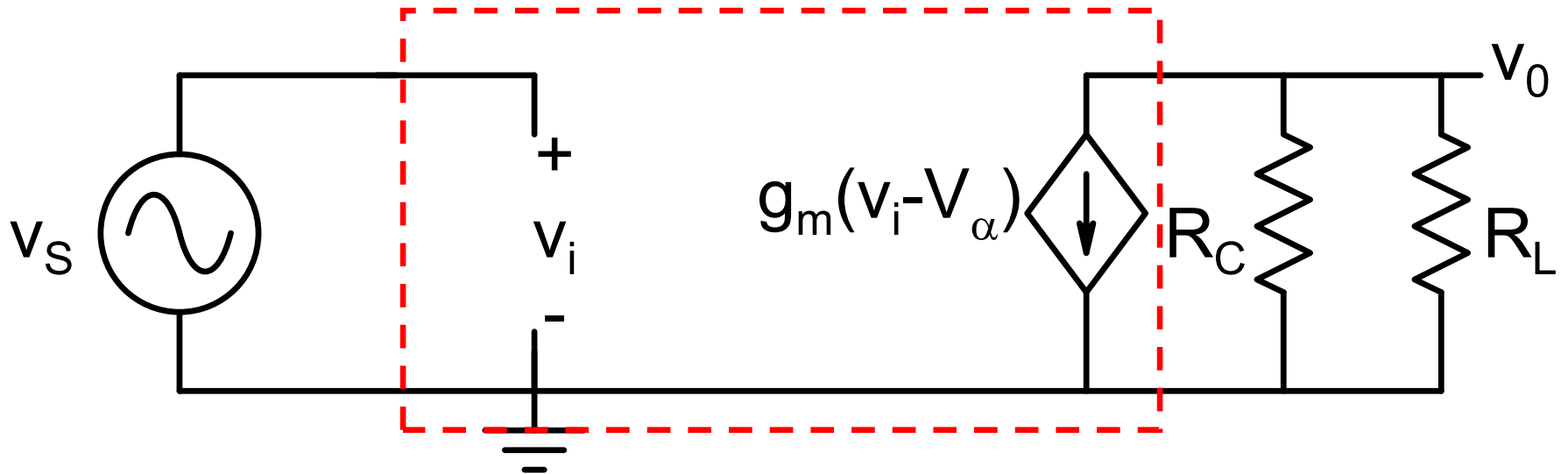
ac (signal)



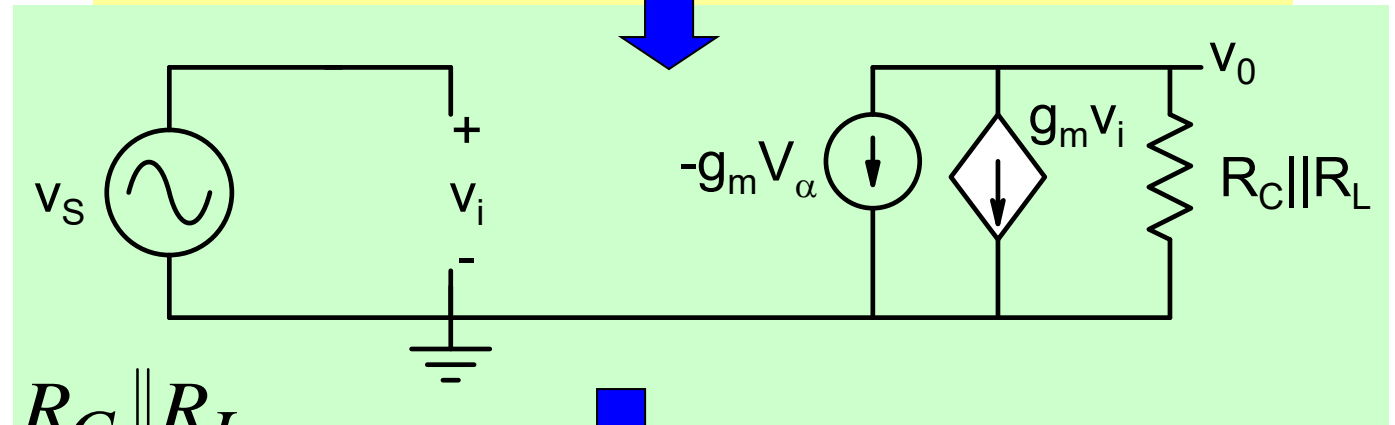
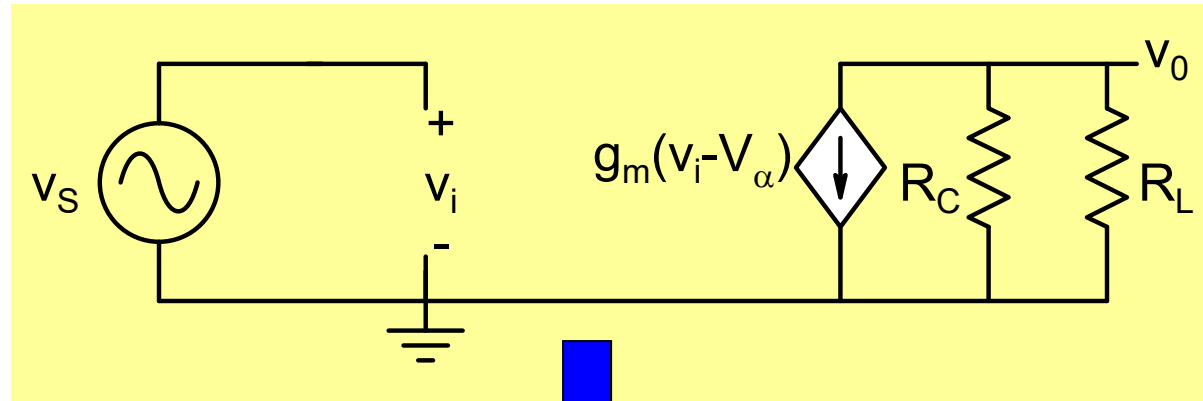
Capacitor is chosen large enough so that at the signal frequency  $1/j\omega C \sim 0$ .



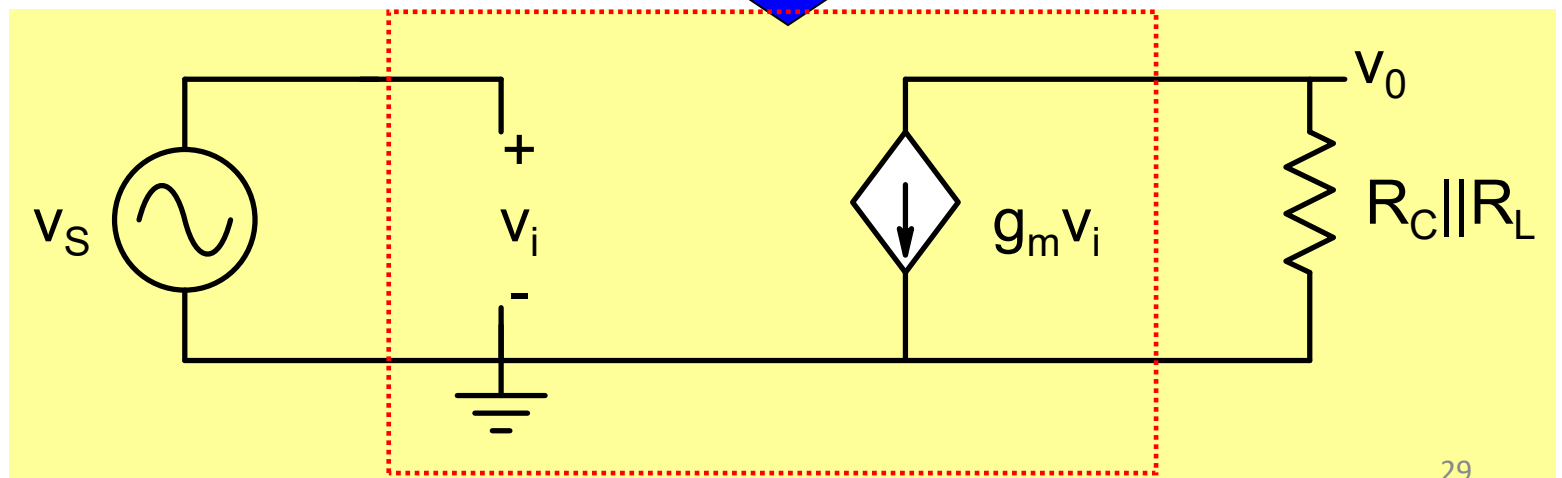
$$I_o = g_m \times (V_i - V_{\alpha}) \text{ for } V_i > V_{\alpha}$$

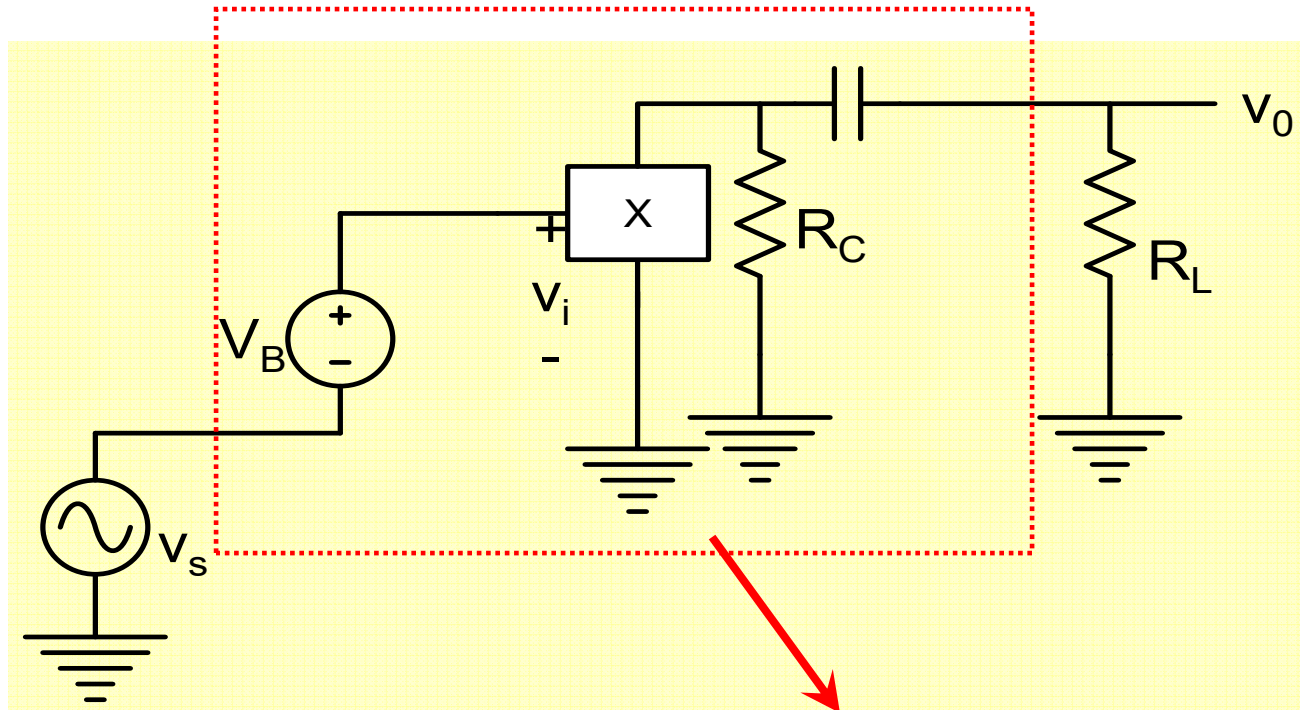
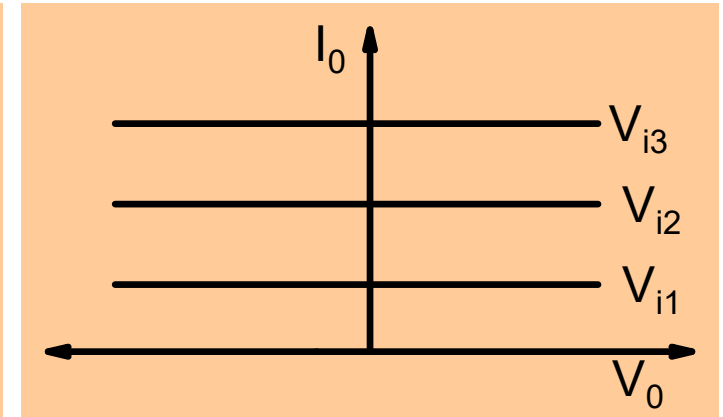
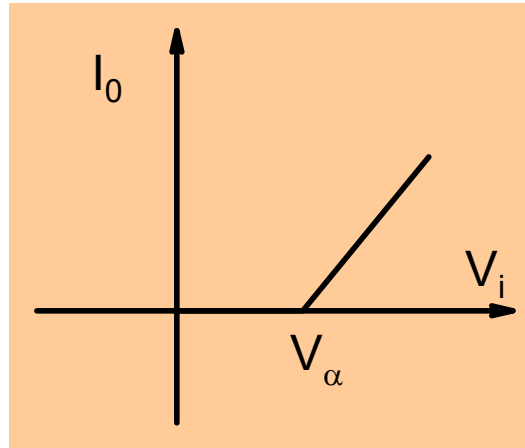
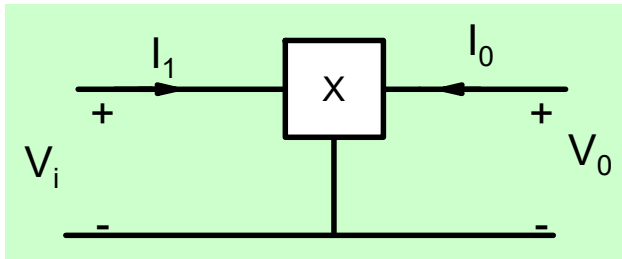


# AC Analysis



$$A_V = \frac{v_o}{v_s} = -g_m R_C \parallel R_L$$

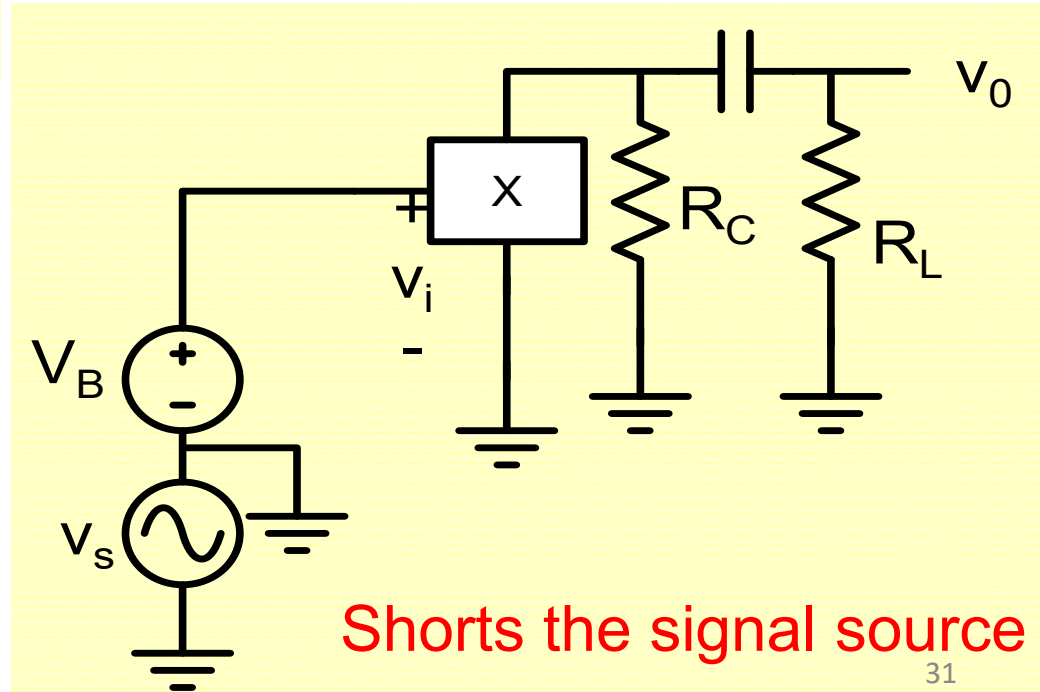
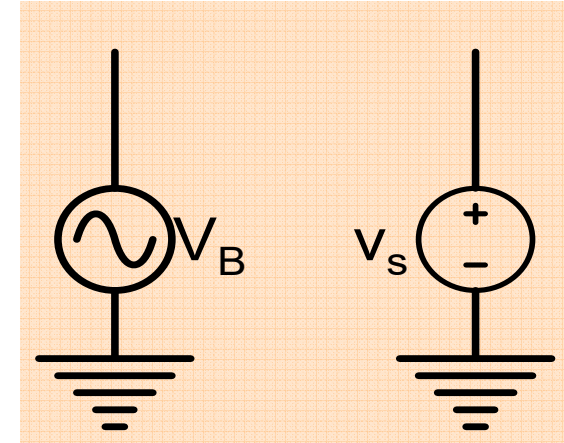
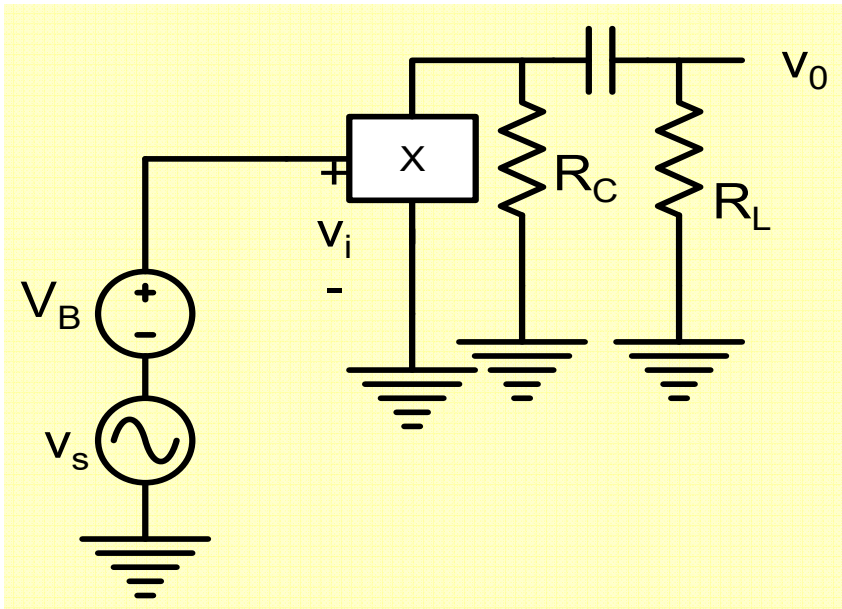




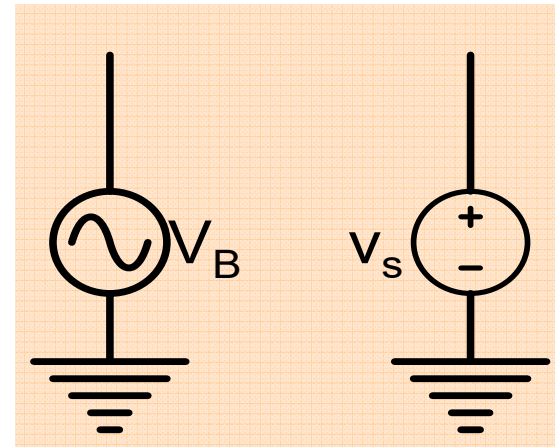
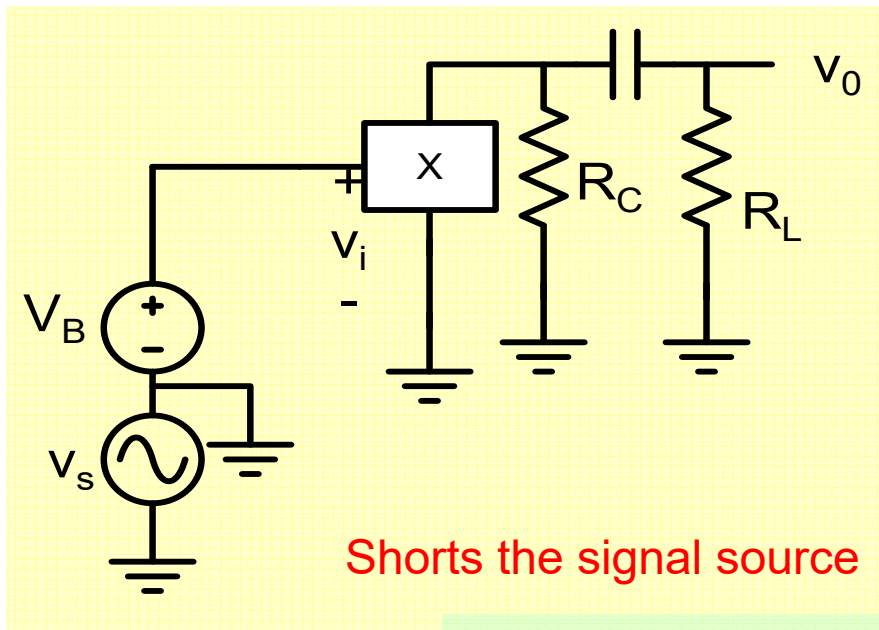
The addition of biasing network allows element  $X$  to appear as an ideal transistor to the signal source



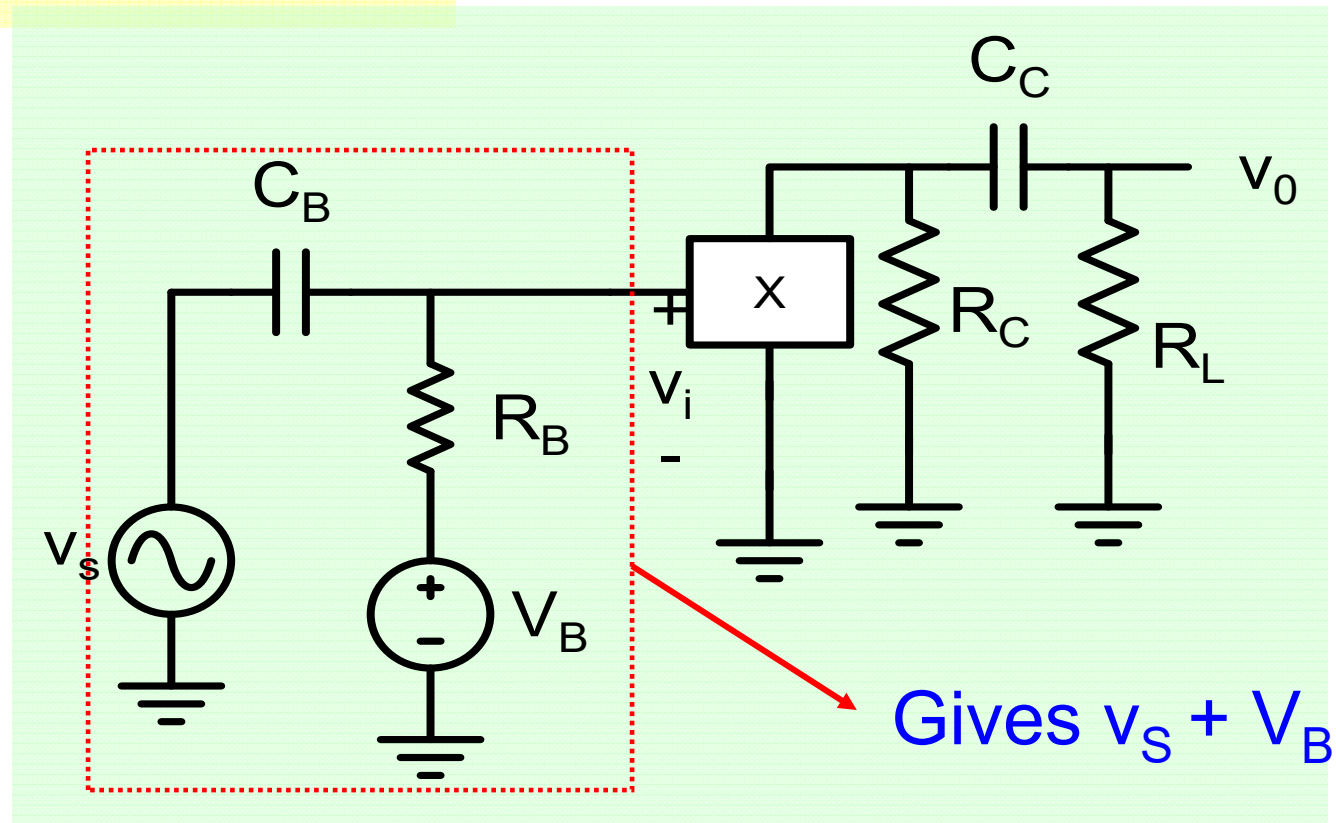
What happens if both dc voltage source and signal source have one terminal as ground?



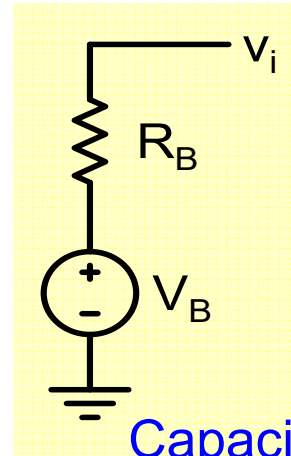
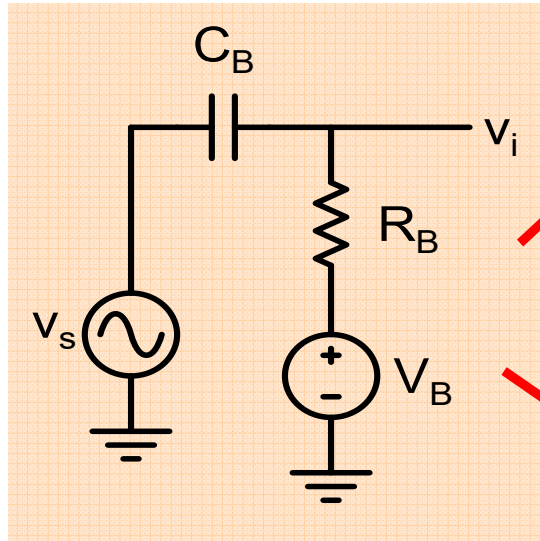
Shorts the signal source



**Solution**

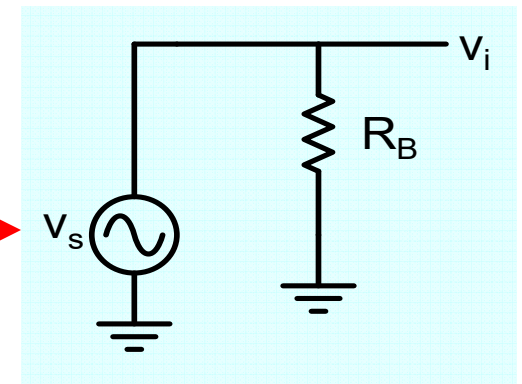
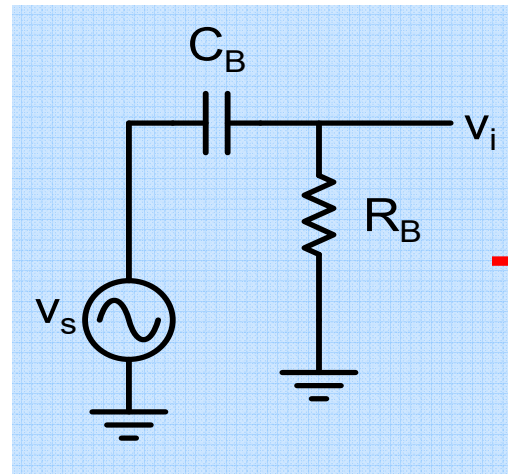






$$v_i = V_B$$

Capacitor is chosen large enough so that at the signal frequency  $1/j\omega C \sim 0$ .

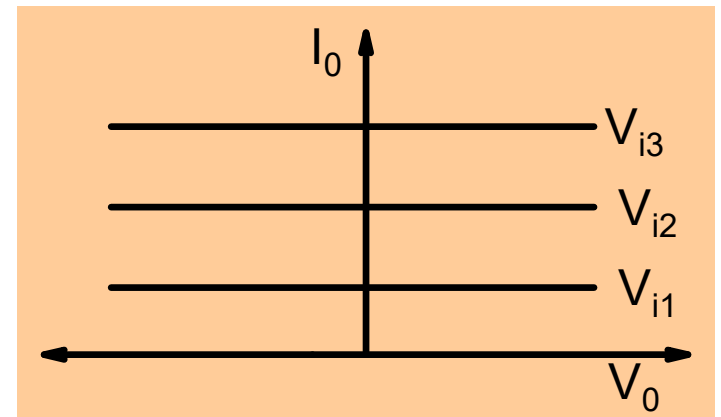
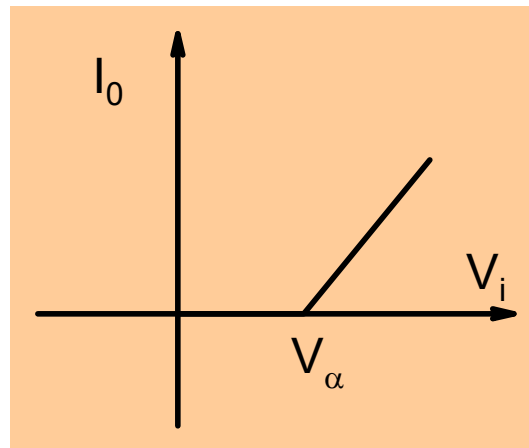
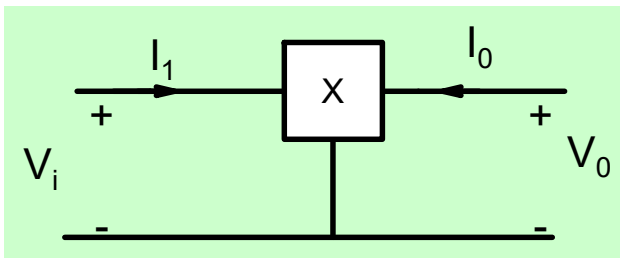
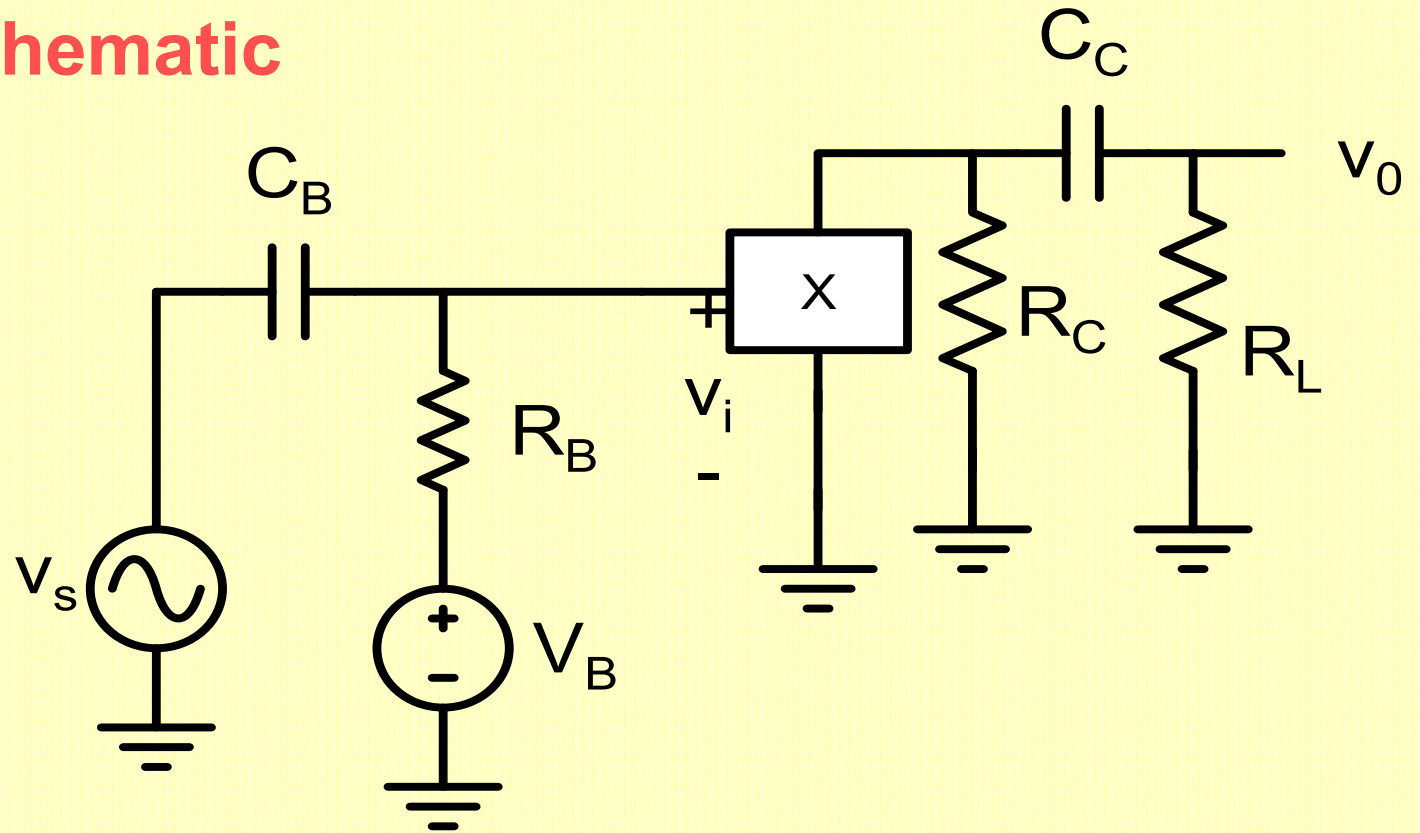


$$v_i = v_s$$

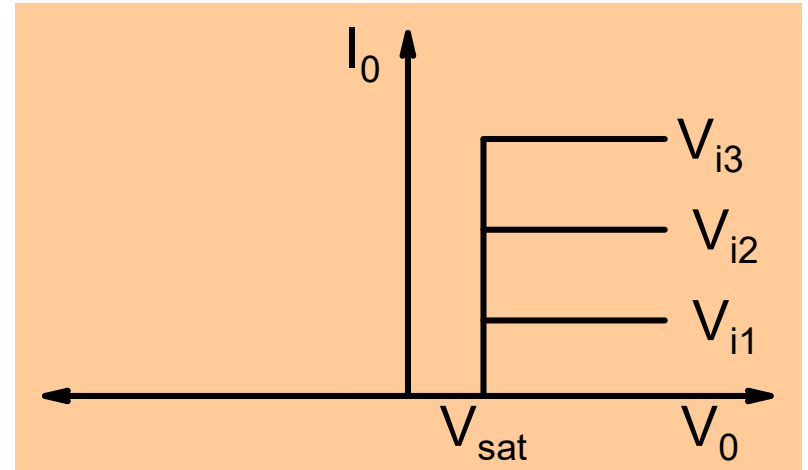
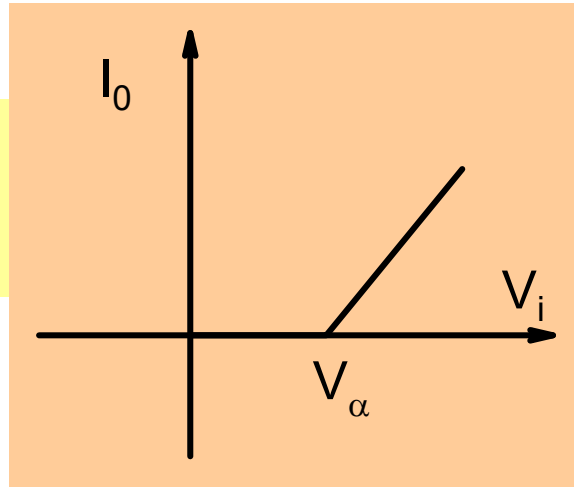
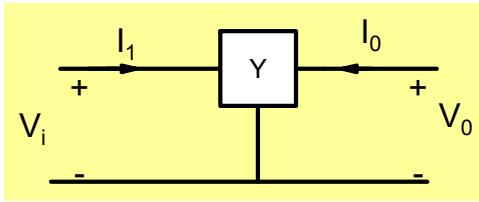
$$v_i(\text{total}) = v_s + V_B$$

Note the role of  $R_B$

# Amplifier Schematic



## Device Y

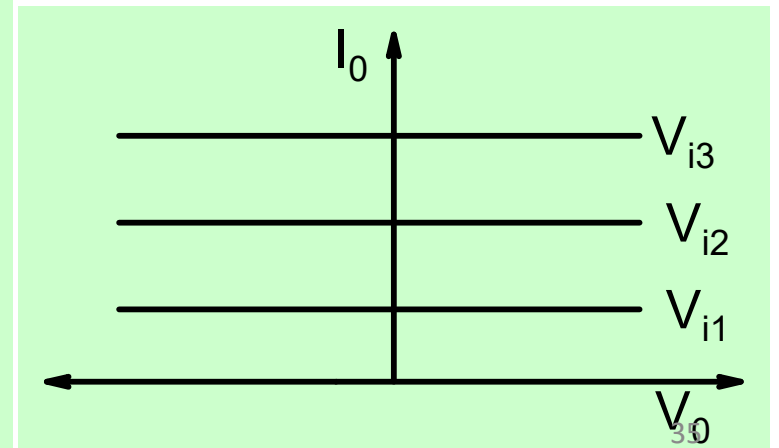
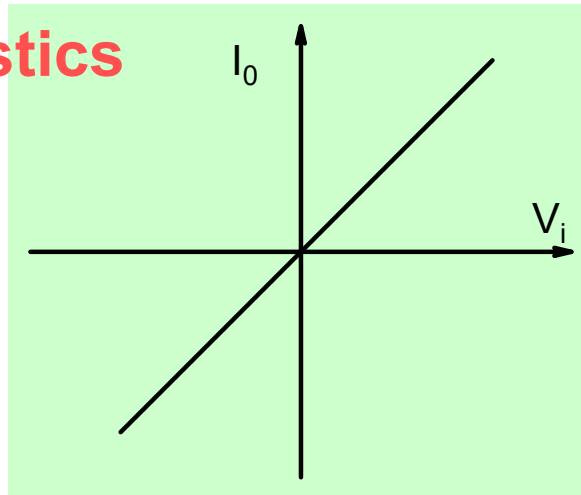


$$I_o = 0 \quad \text{for } V_o < V_{\text{sat}}$$

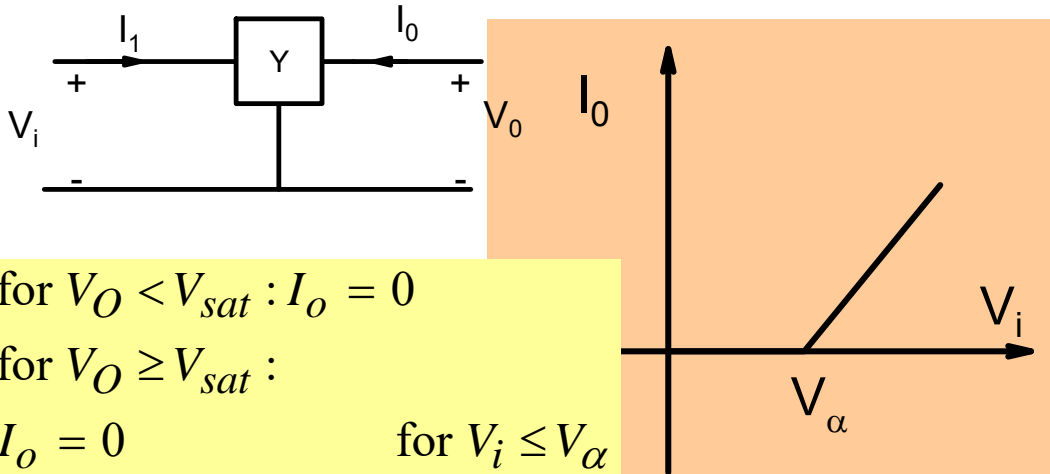
$$I_o = 0 \quad \text{for } V_i \leq V_\alpha$$

$$= g_m \times (V_i - V_\alpha) \quad \text{for } V_i > V_\alpha$$

## Ideal Characteristics



## How do we use device Y to make an amplifier?



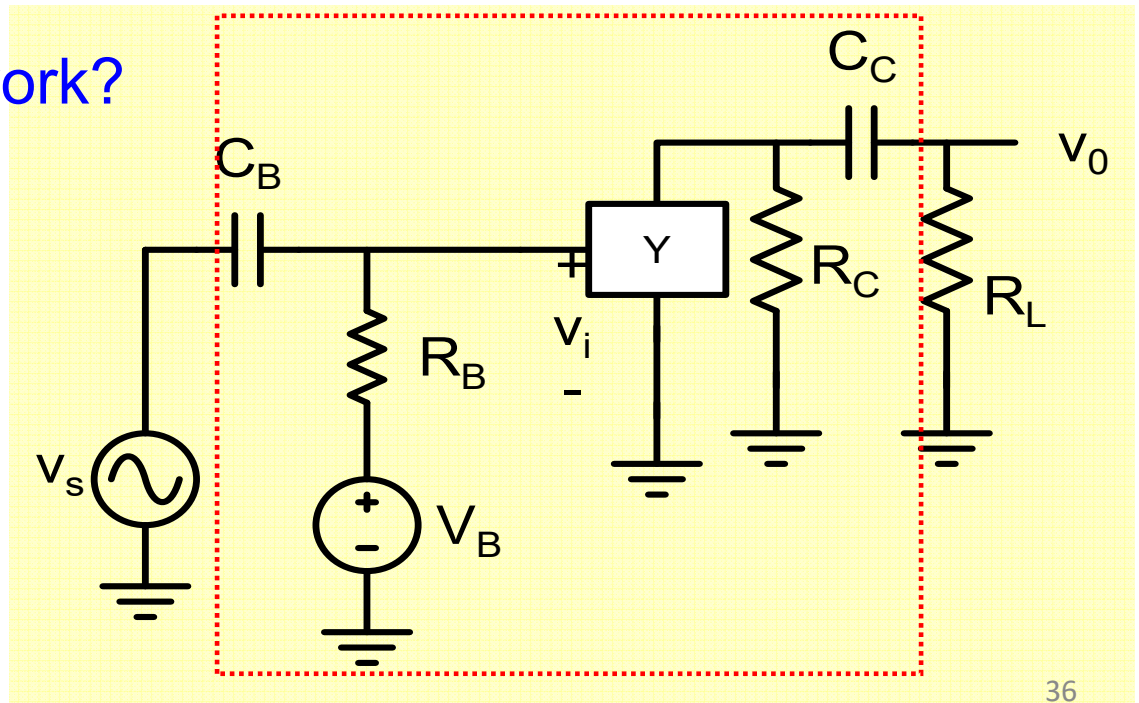
for  $V_o < V_{sat} : I_o = 0$

for  $V_o \geq V_{sat} :$

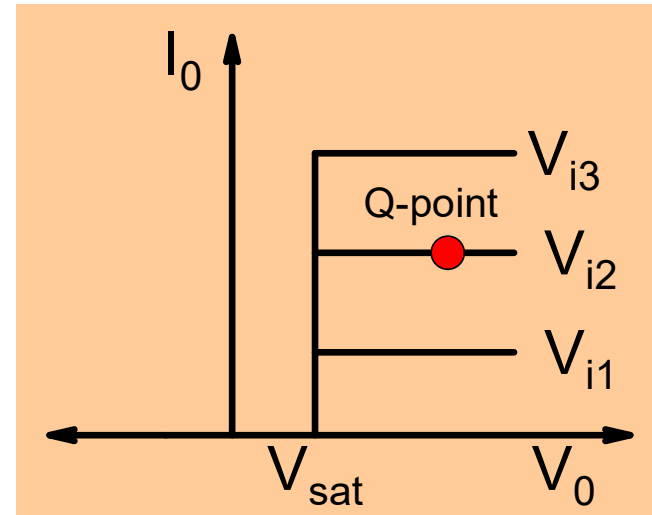
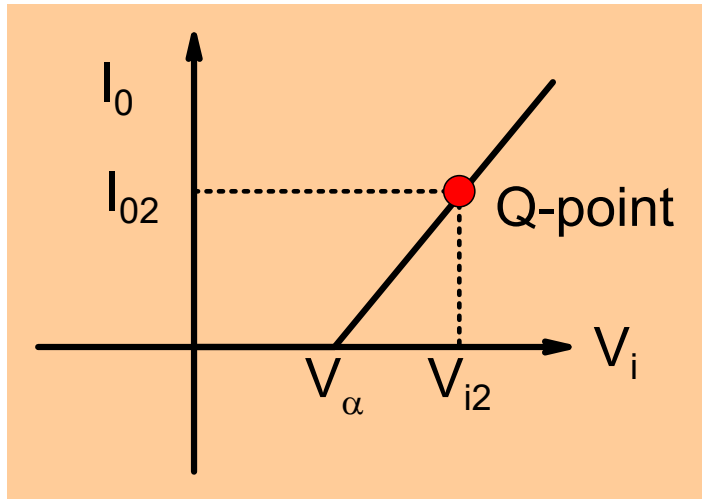
$I_o = 0$  for  $V_i \leq V_\alpha$

$= g_m \times (V_i - V_\alpha)$  for  $V_i > V_\alpha$

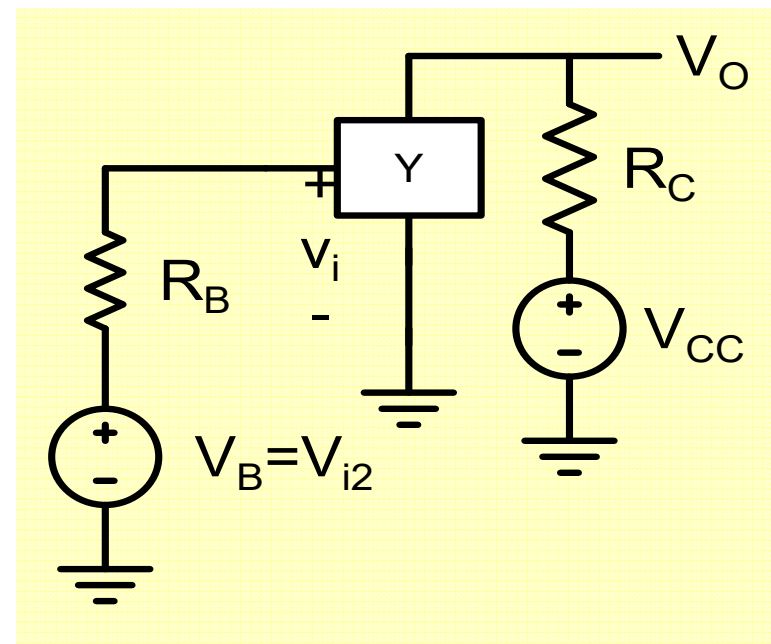
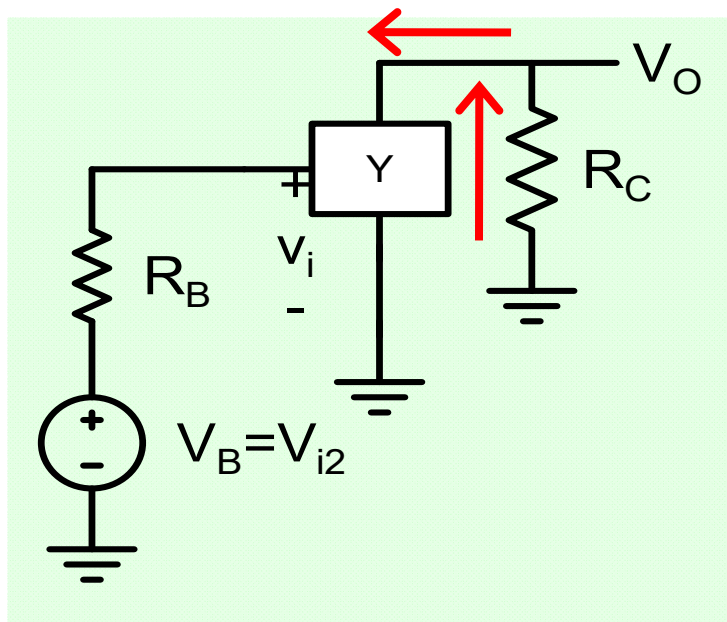
Will the earlier solution work?



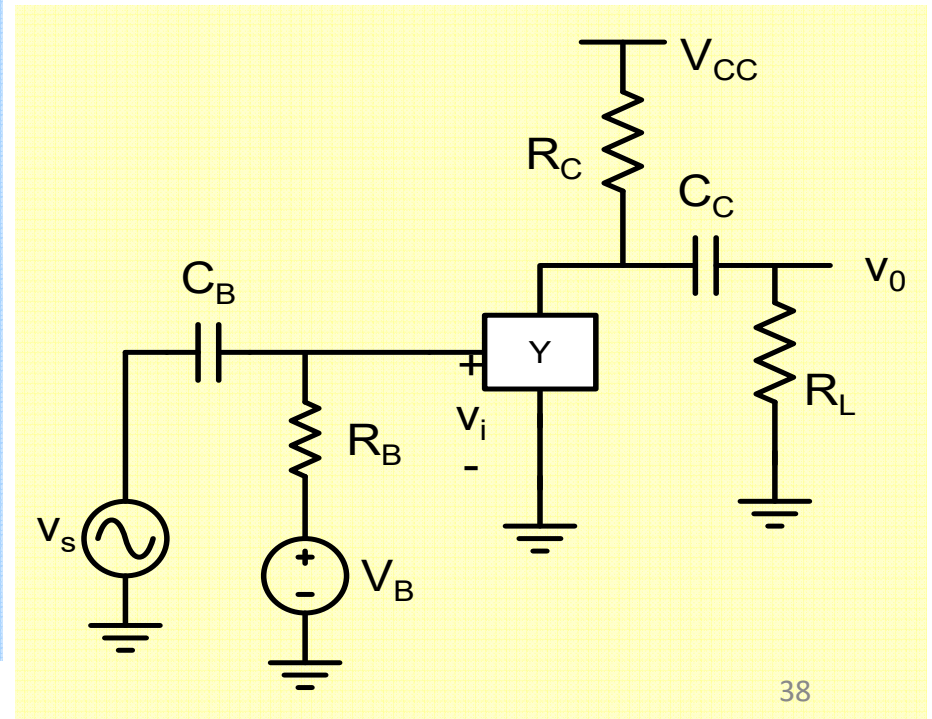
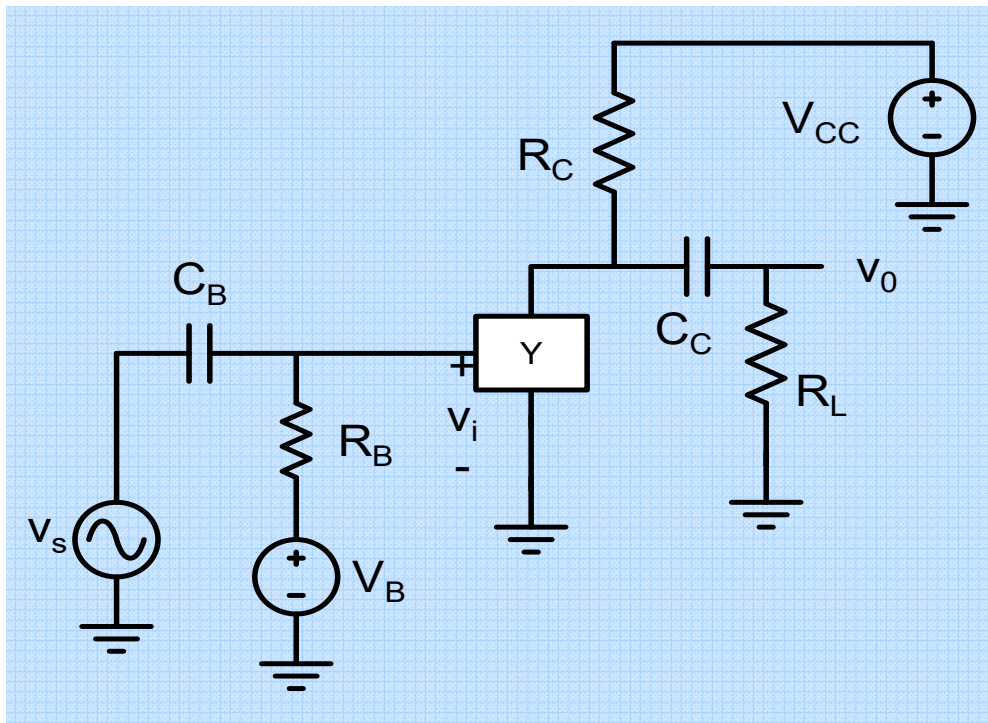
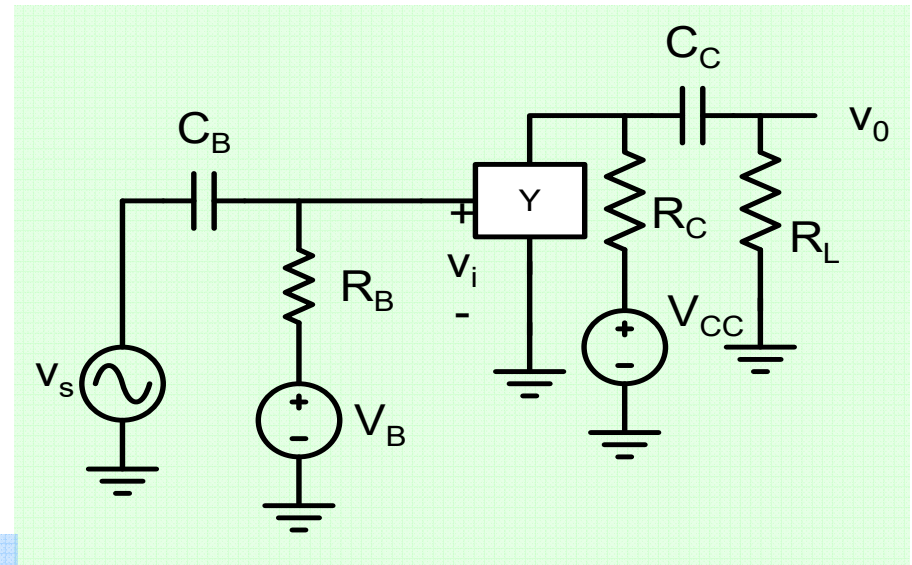
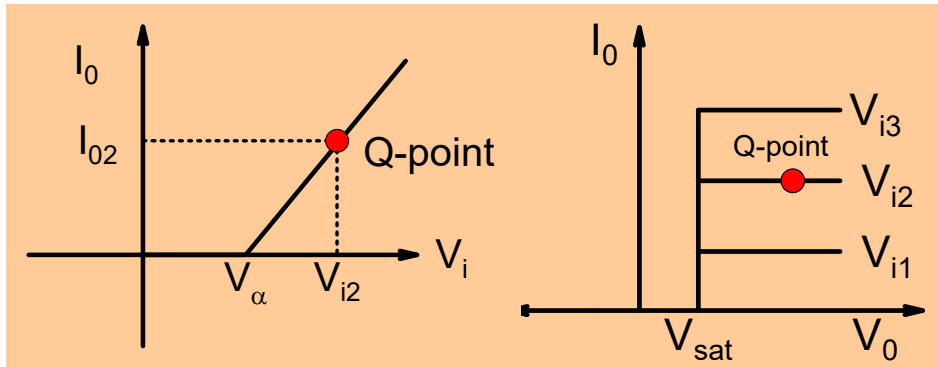
The purpose of biasing network is to operate the device in a region which resembles ideal transistor



$V_o = -ve$  which is not possible for device Y

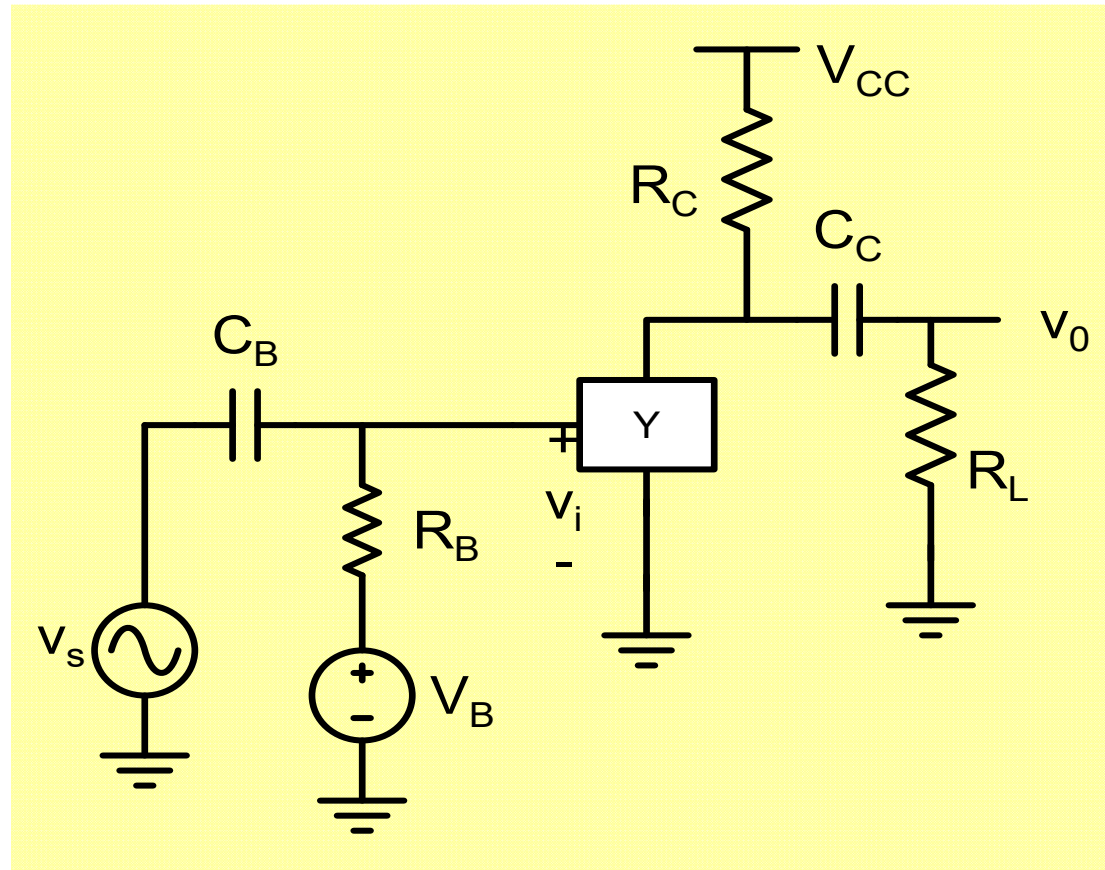
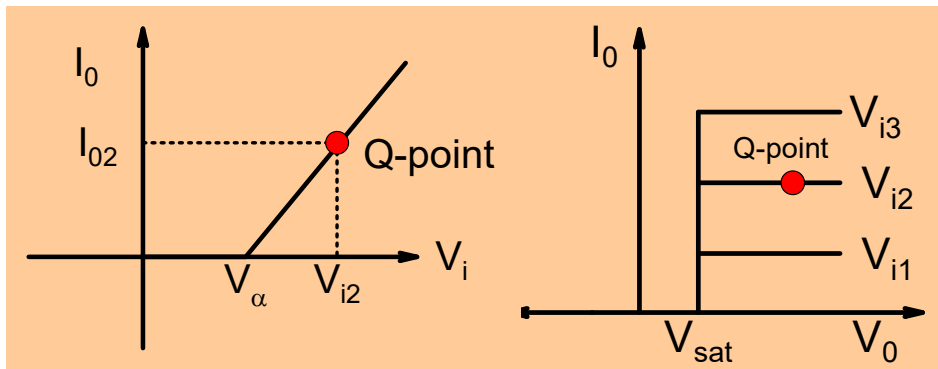


# Revised Amplifier Schematic

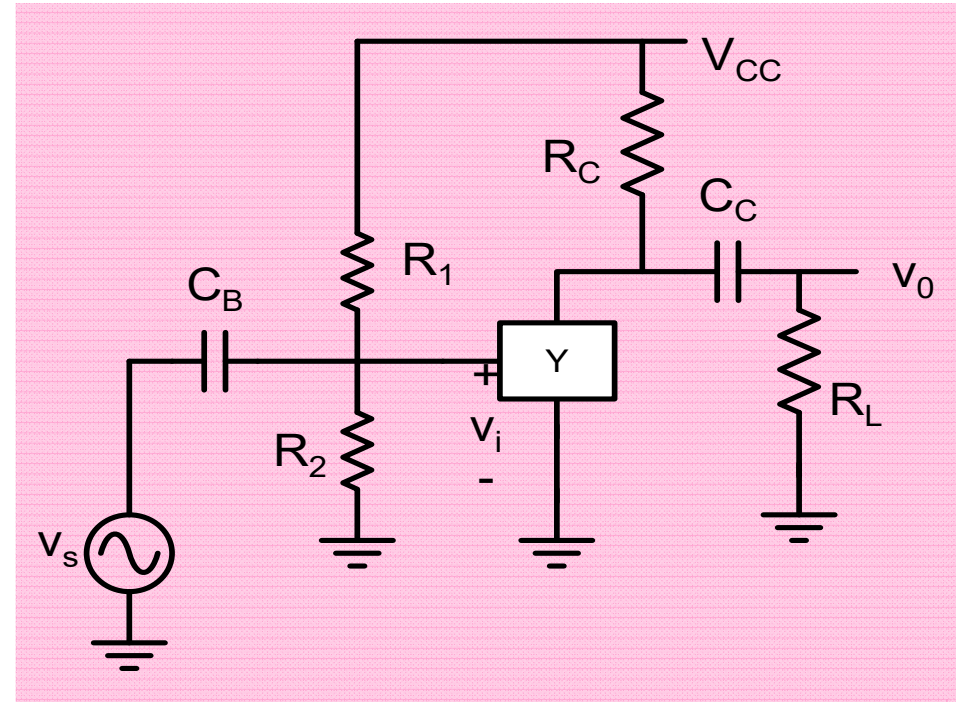
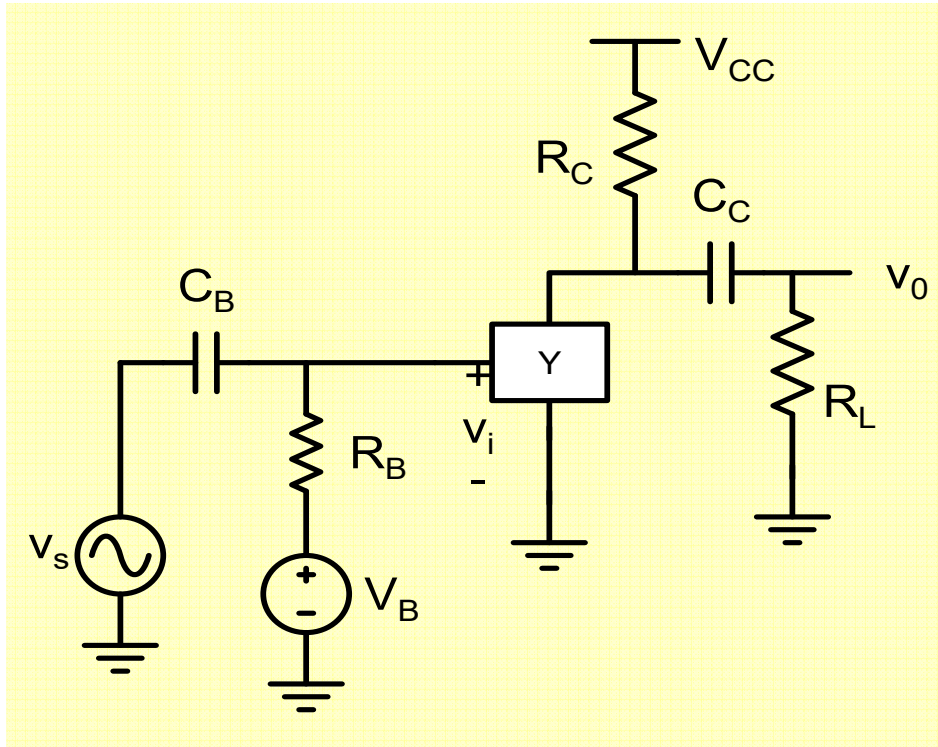




# Revised Amplifier Schematic



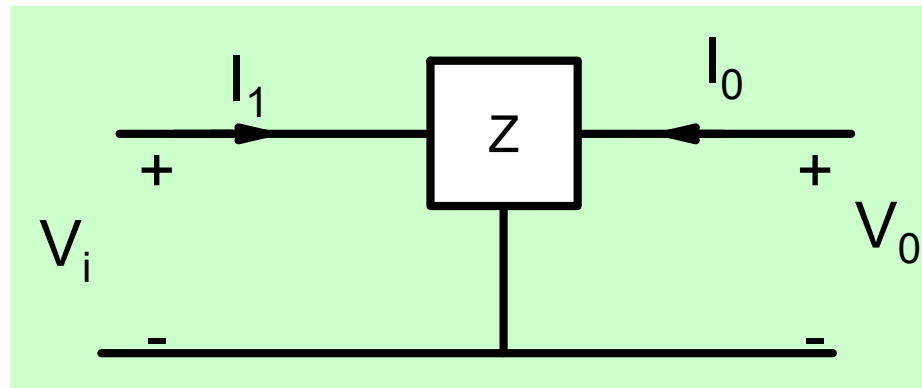
Can we amplify using one dc voltage source only?



$$V_B = V_{CC} \times \frac{R_2}{R_1 + R_2}$$



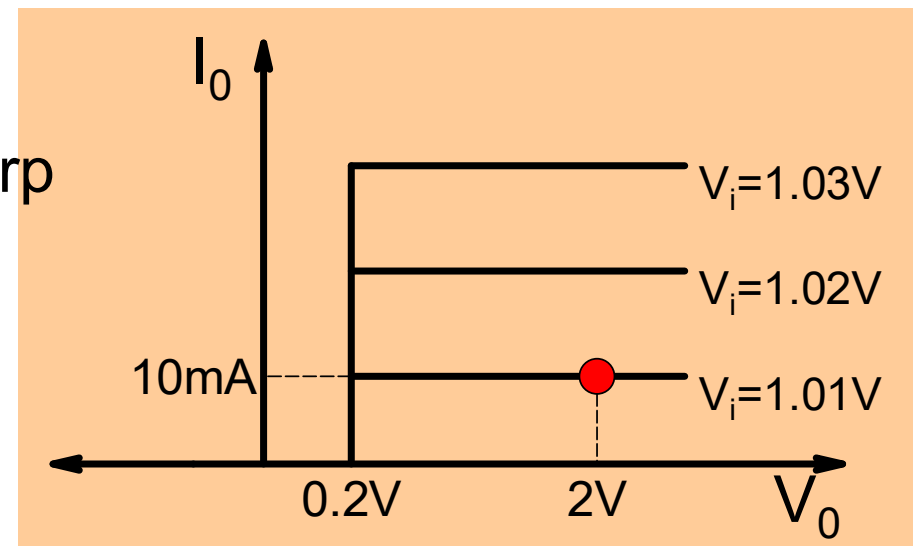
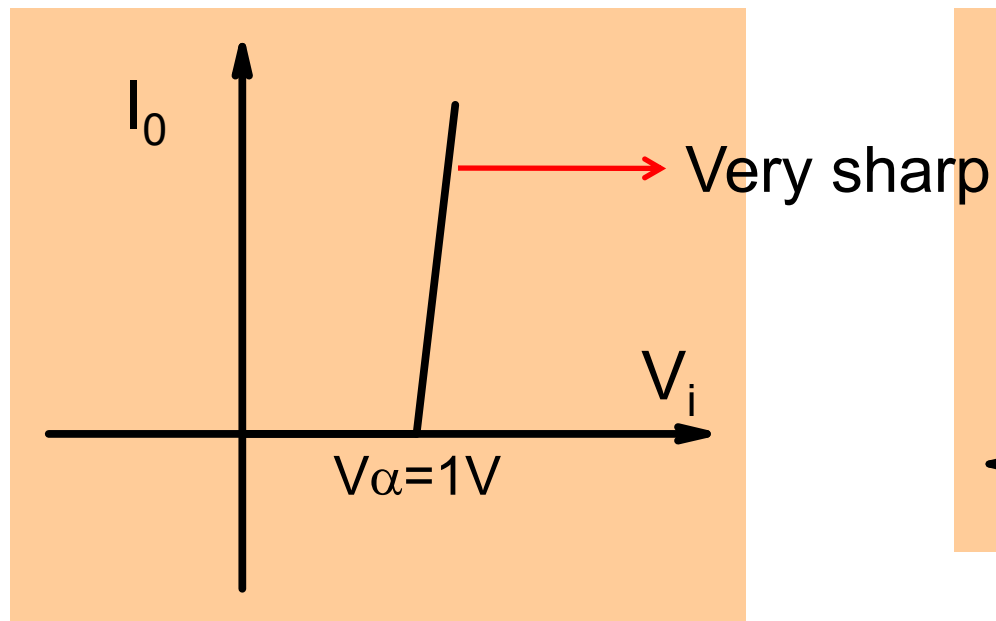
## Device Z



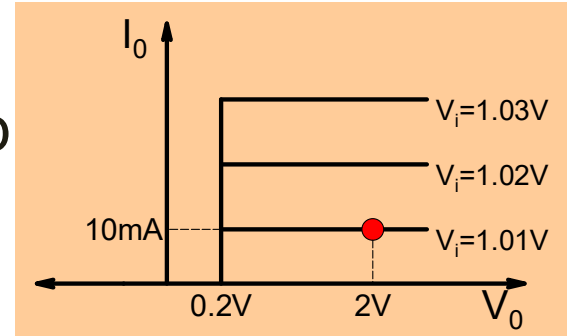
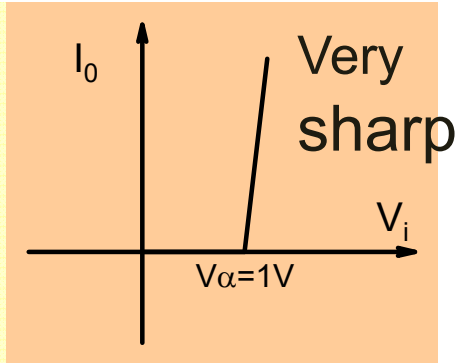
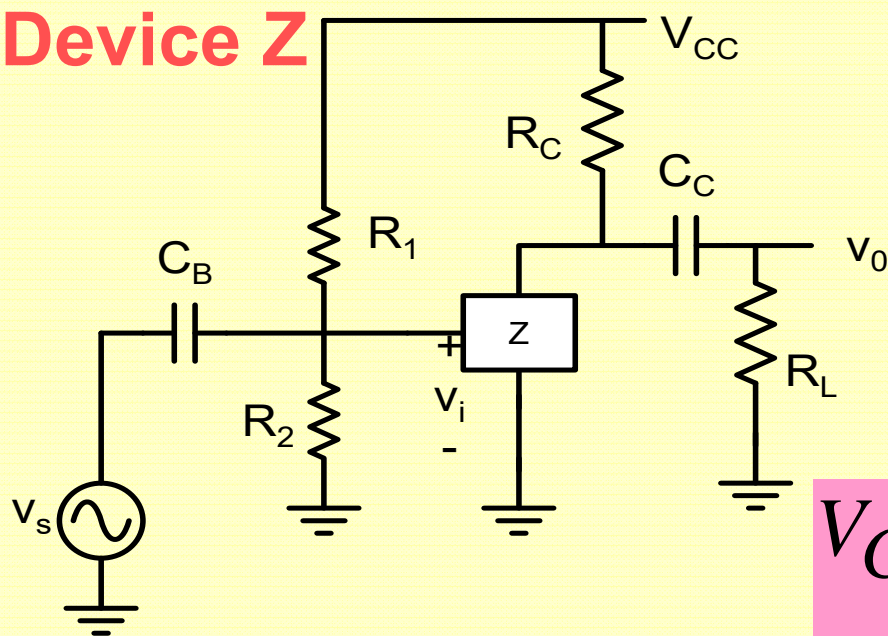
for  $V_o < 0.2V : I_o = 0$

for  $V_o \geq 0.2$ :

$I_o = 0$  for  $V_i \leq 1V$   
 $= 1 \times (V_i - 1V)$  for  $V_i > 1V$



## Device Z



$$V_{CC} = 5V; R_2 = 1K; R_1 = 3.95K$$

$$\Rightarrow V_i = 1.01 \Rightarrow I_o = 10mA$$

$$V_{CC} = 5V; R_2 = 0.99K; R_1 = 3.95K$$

$$\Rightarrow V_i = 1.002 \Rightarrow I_o = 2mA$$

$$V_{CC} = 5V; R_2 = 0.98K; R_1 = 3.95K$$

$$\Rightarrow V_i = 0.994V \Rightarrow I_o = 0$$

for  $V_o < 0.2V : I_o = 0$

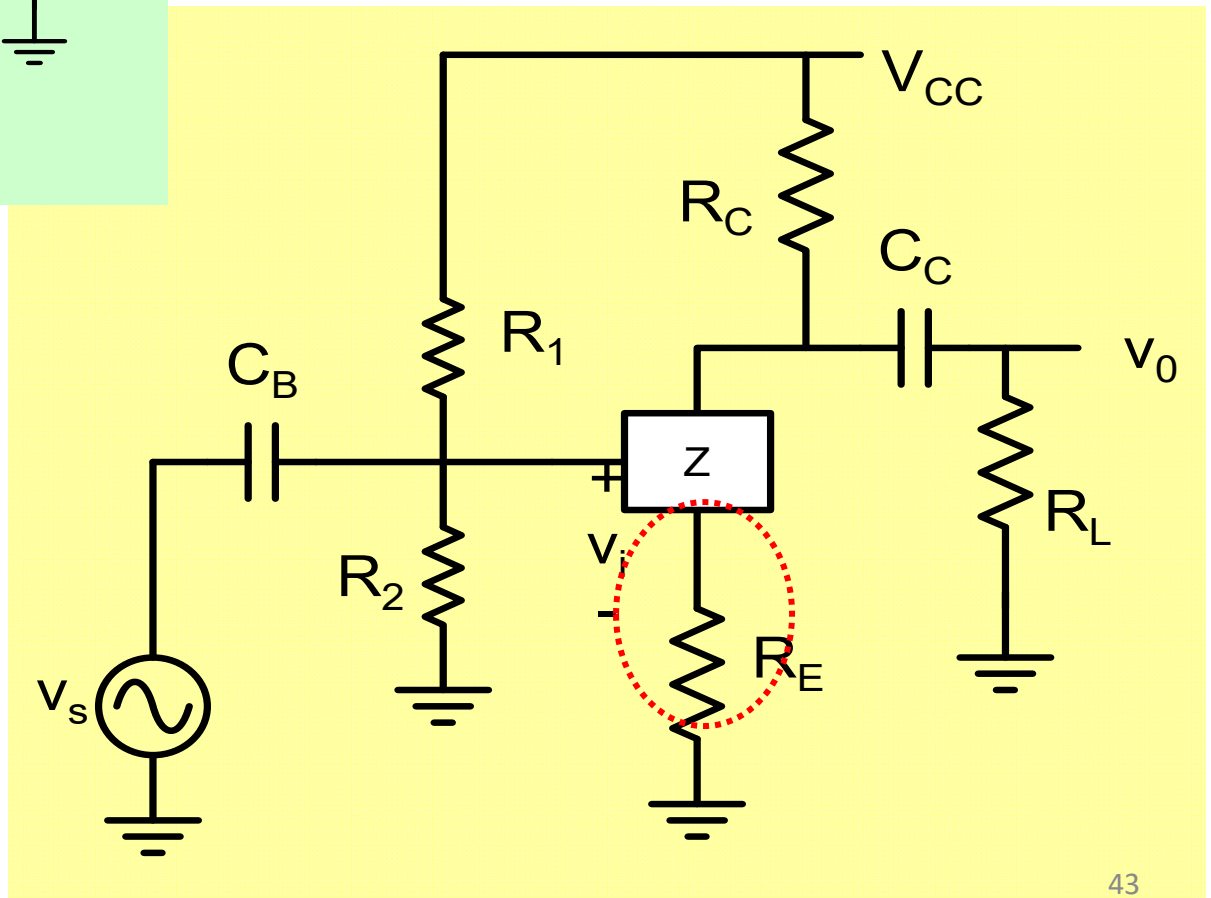
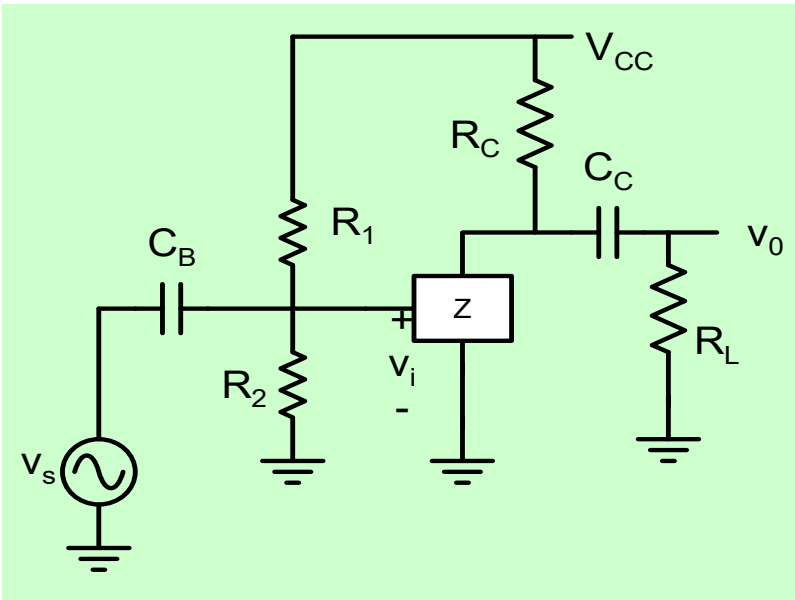
for  $V_o \geq 0.2$ :

$I_o = 0$  for  $V_i \leq 1V$

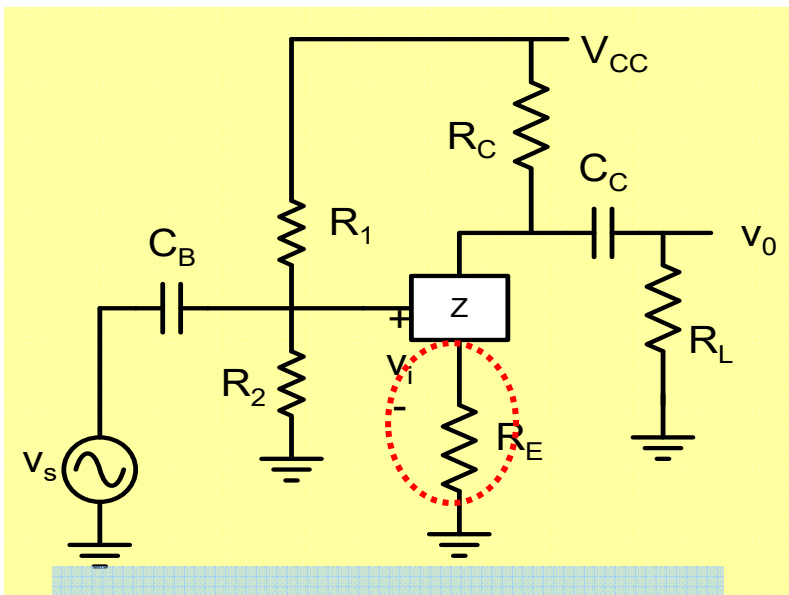
$= 1 \times (V_i - 1V)$  for  $V_i > 1V$

Circuit is very sensitive to variations in resistor values, power supply, device parameters such as  $V_{\alpha}$

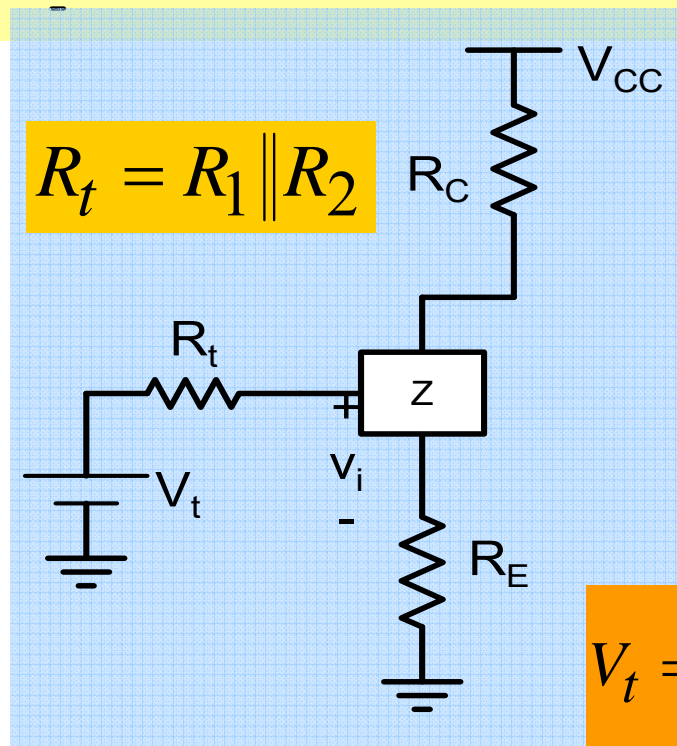
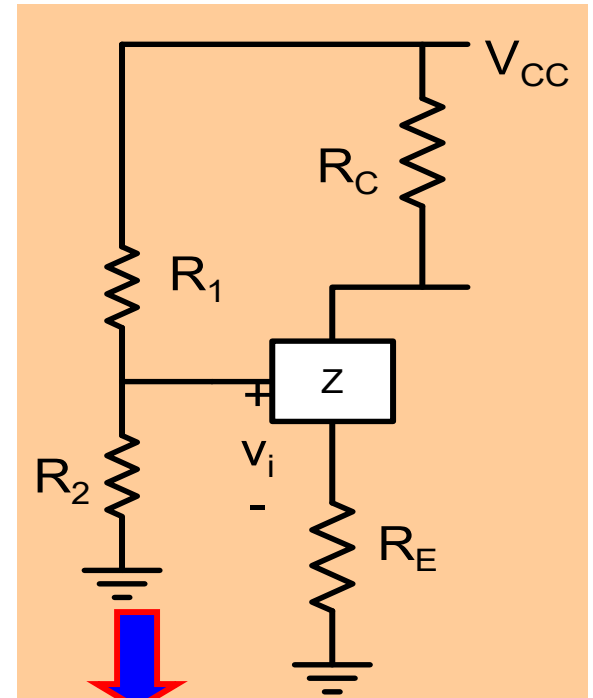
## Solution



# Solution

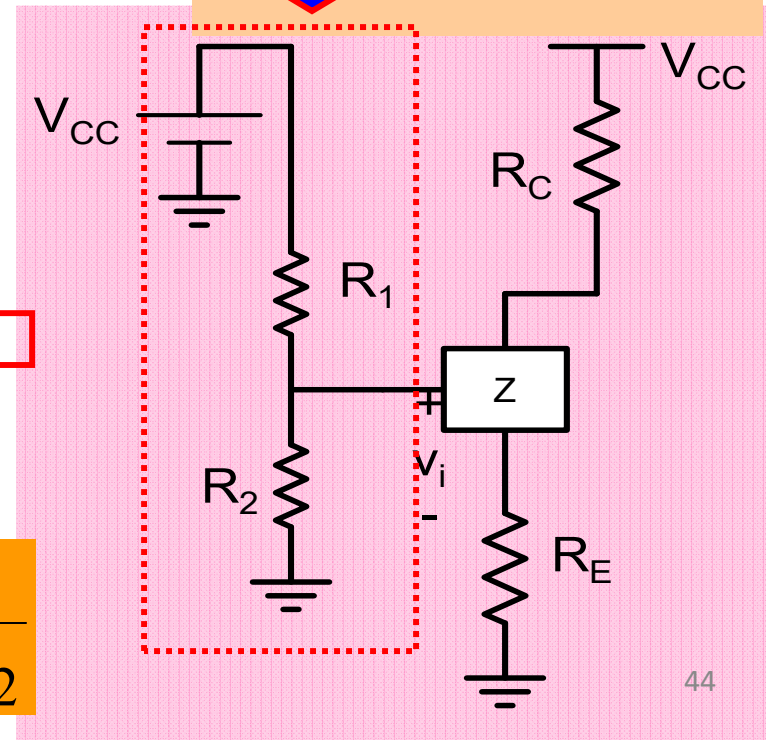


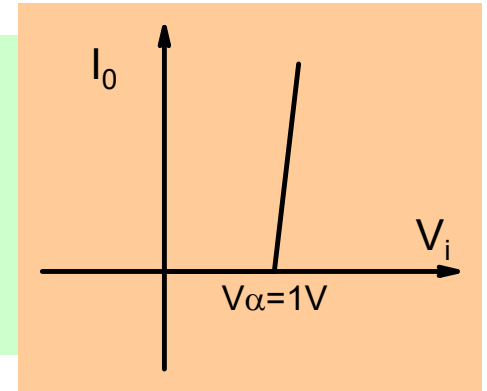
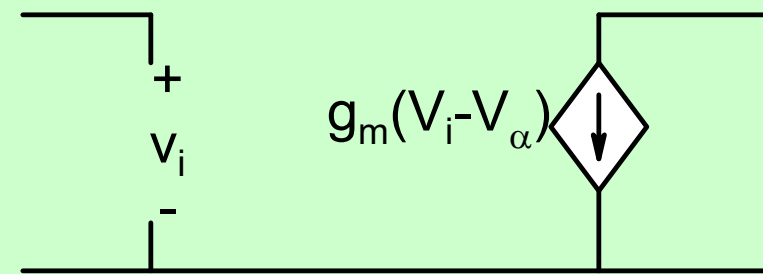
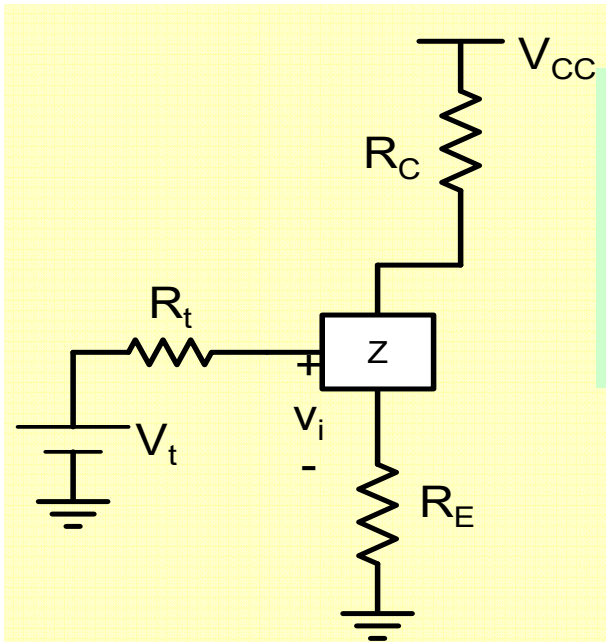
## DC Analysis



$$R_t = R_1 \parallel R_2$$

$$V_t = V_{CC} \times \frac{R_2}{R_1 + R_2}$$





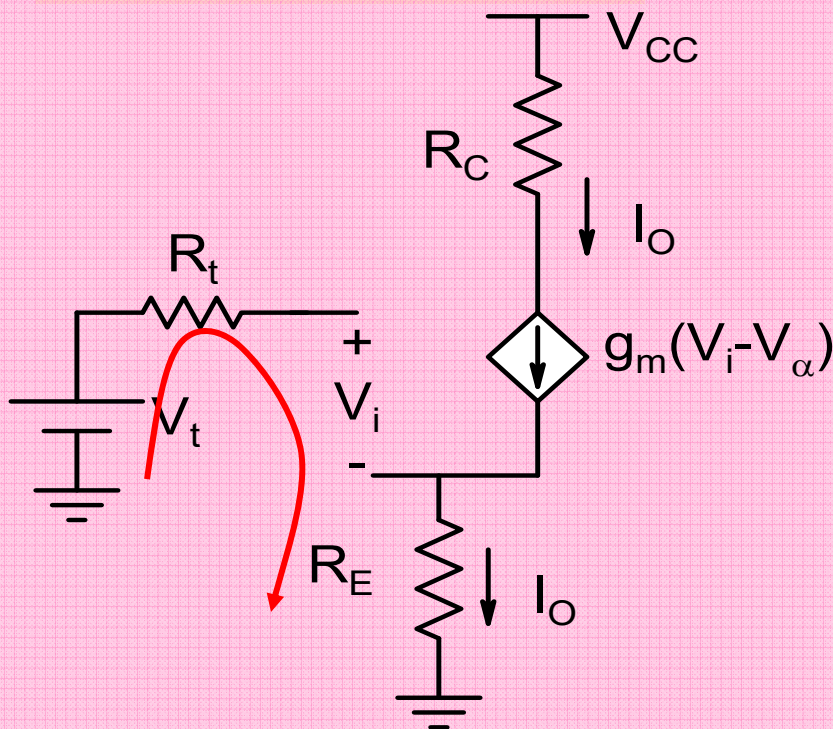
$$-V_t + 0 \times R_t + V_i + I_O R_E = 0$$

Since  $I_o$  vs.  $V_i$  characteristics is very sharp,  $V_i \sim V_\alpha = 1V$

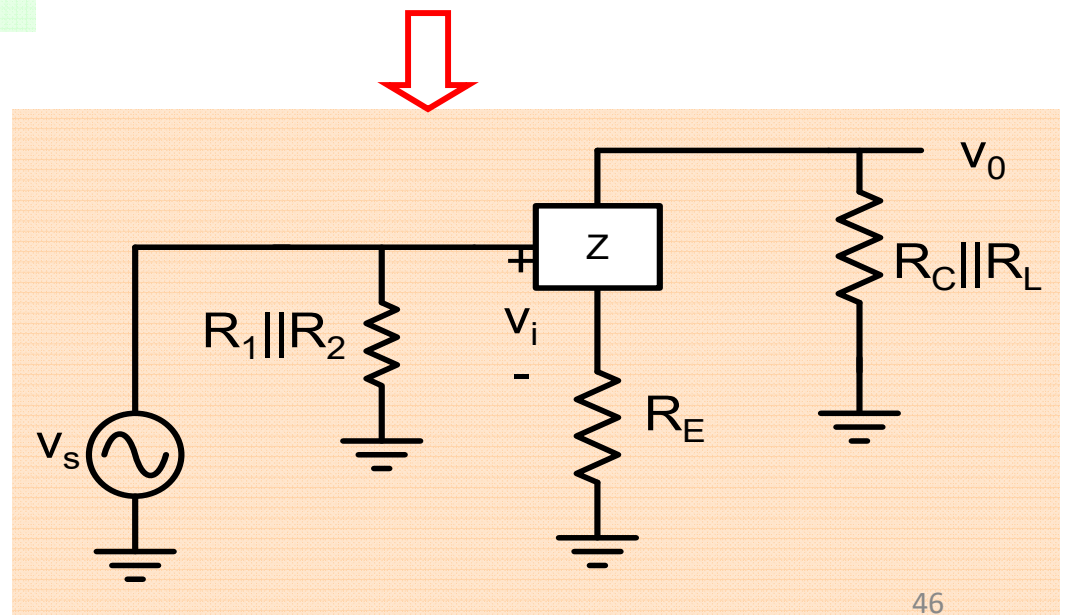
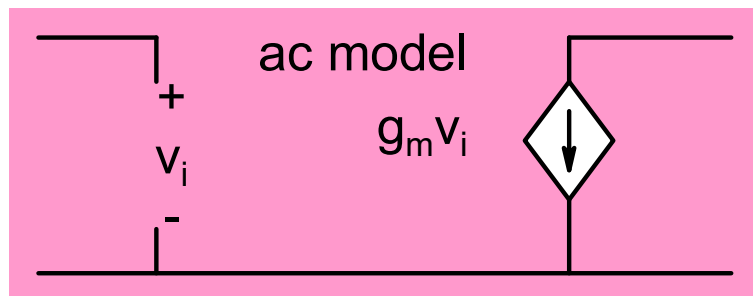
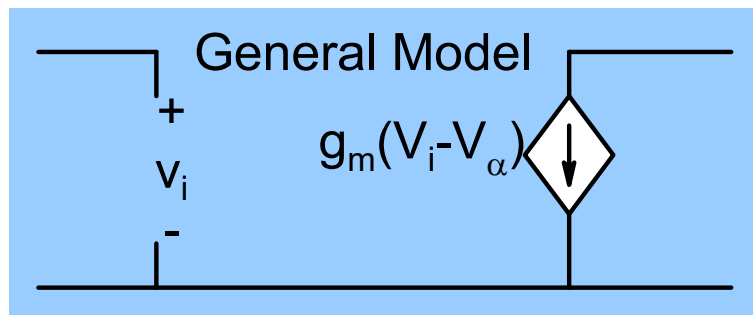
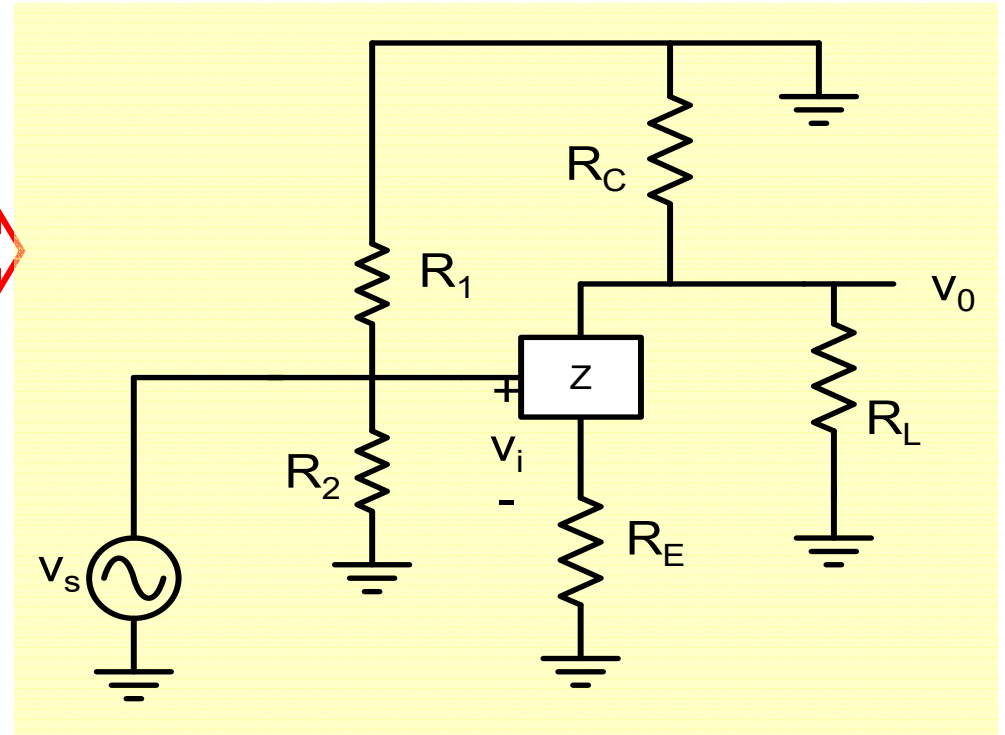
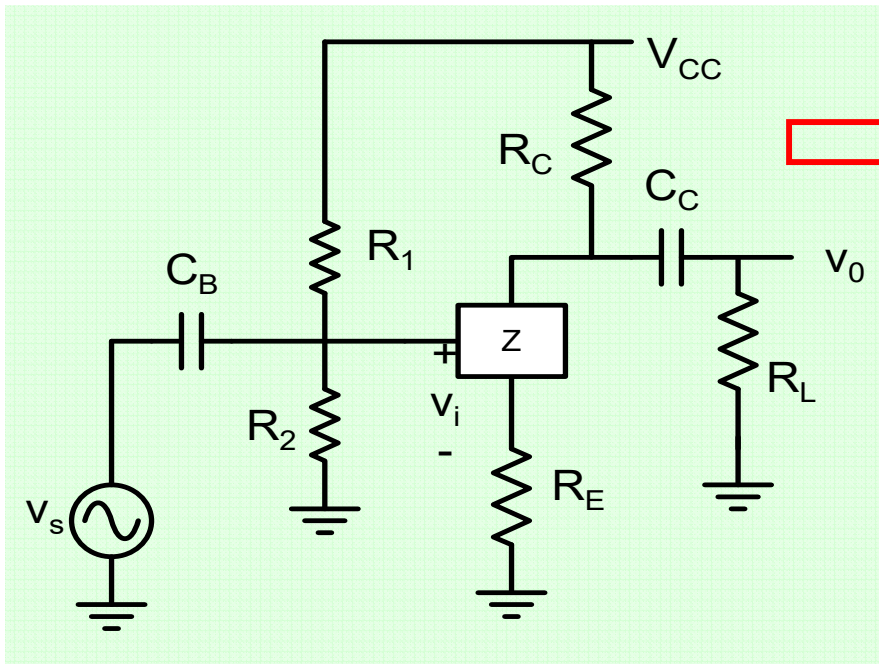
$$I_O \cong \frac{V_t - V_\alpha}{R_E}$$

If  $V_t$  changes by 1% due to variation in resistor values then the change in output current is proportional.

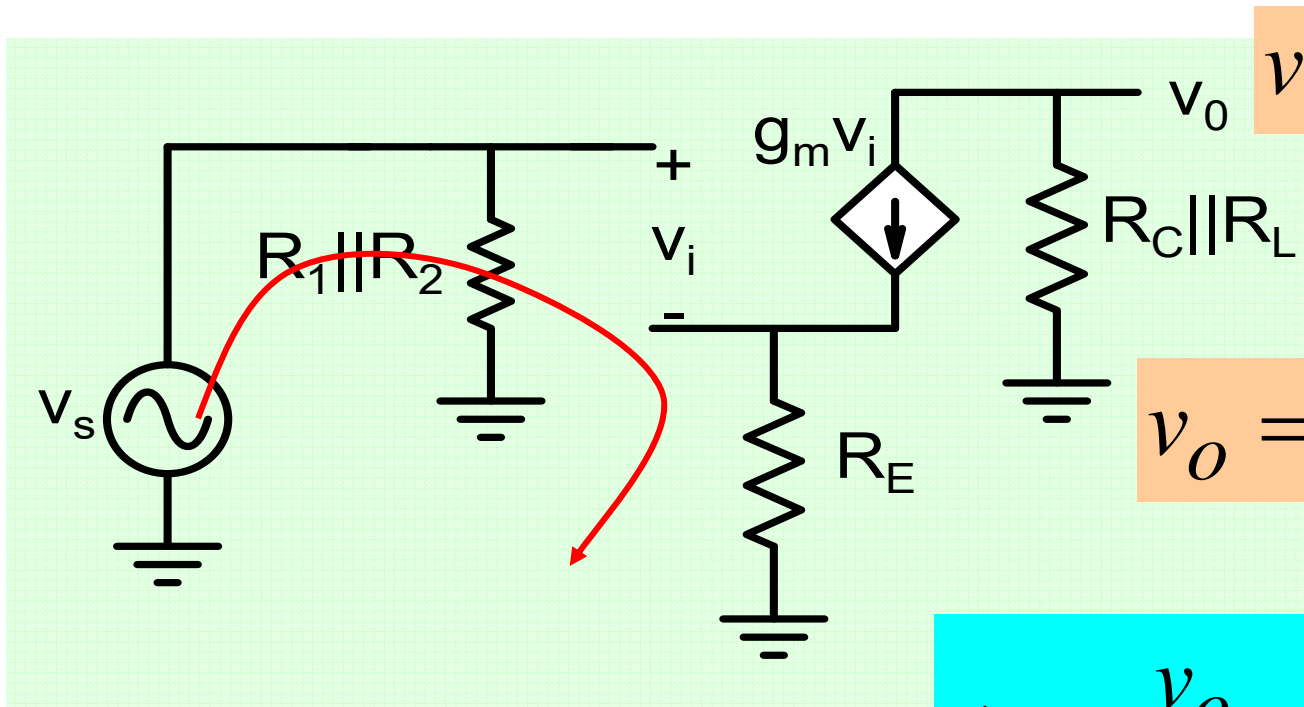
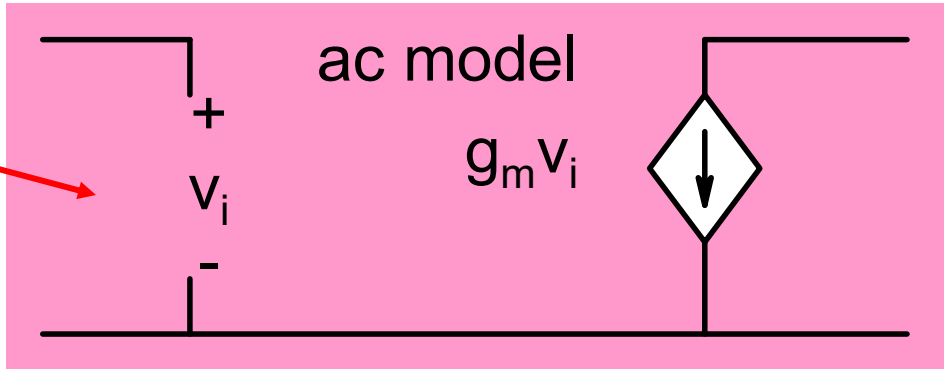
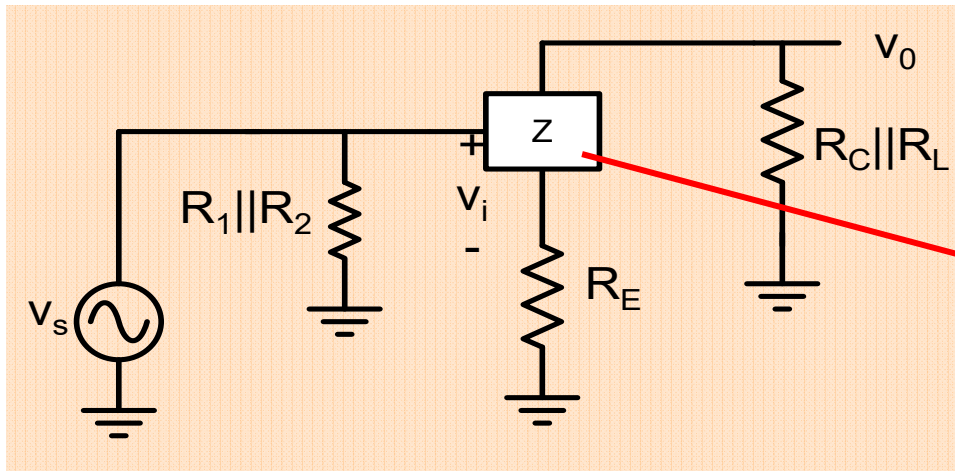
But circuit is much less sensitive to variations in circuit parameters



# AC analysis



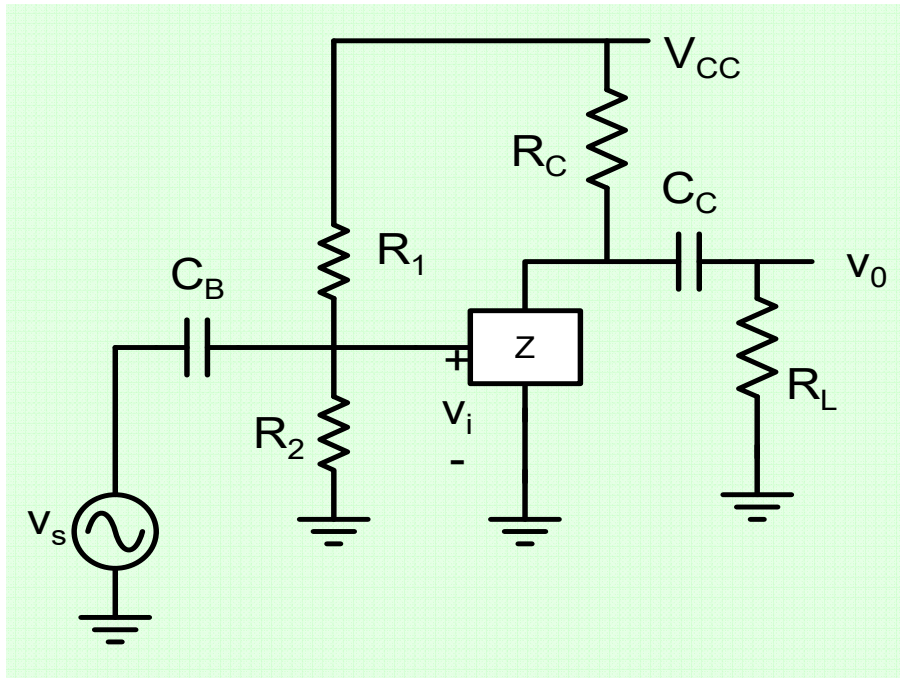




$$v_s = v_i + g_m v_i R_E$$

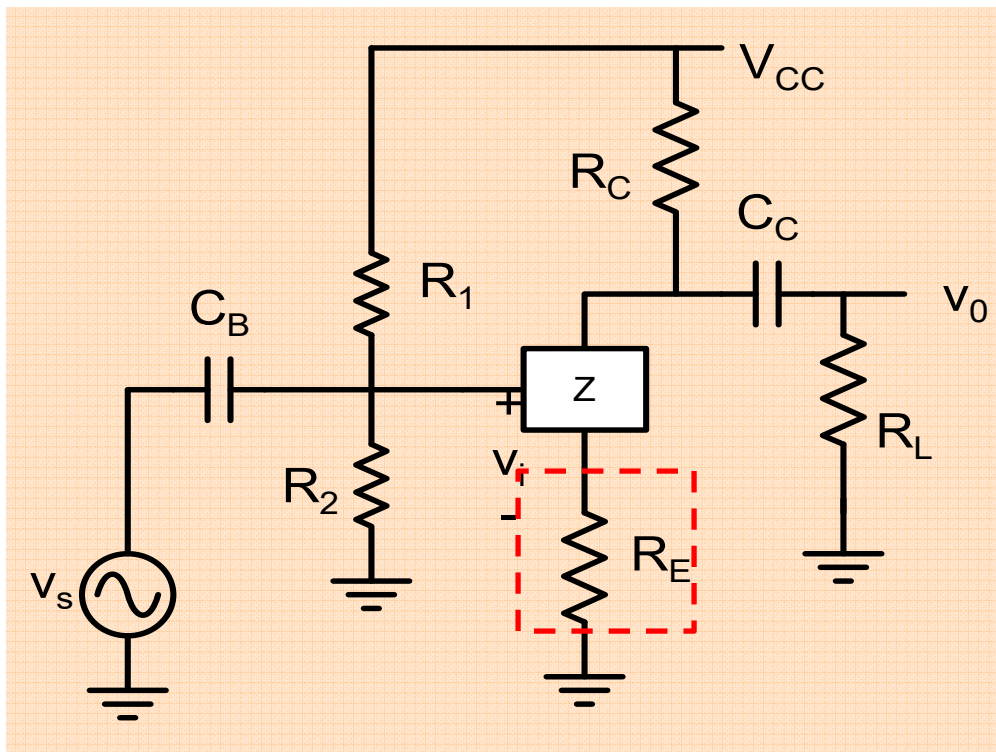
$$v_o = -g_m v_i \times R_C \parallel R_L$$

$$A_V = \frac{v_o}{v_s} = -\frac{g_m R_C \parallel R_L}{1 + g_m R_E}$$



Circuit is **very sensitive** to variations in resistor values, power supply, device parameters such as  $V_{\alpha}$

$$A_V = \frac{v_o}{v_s} = -g_m R_C \parallel R_L$$



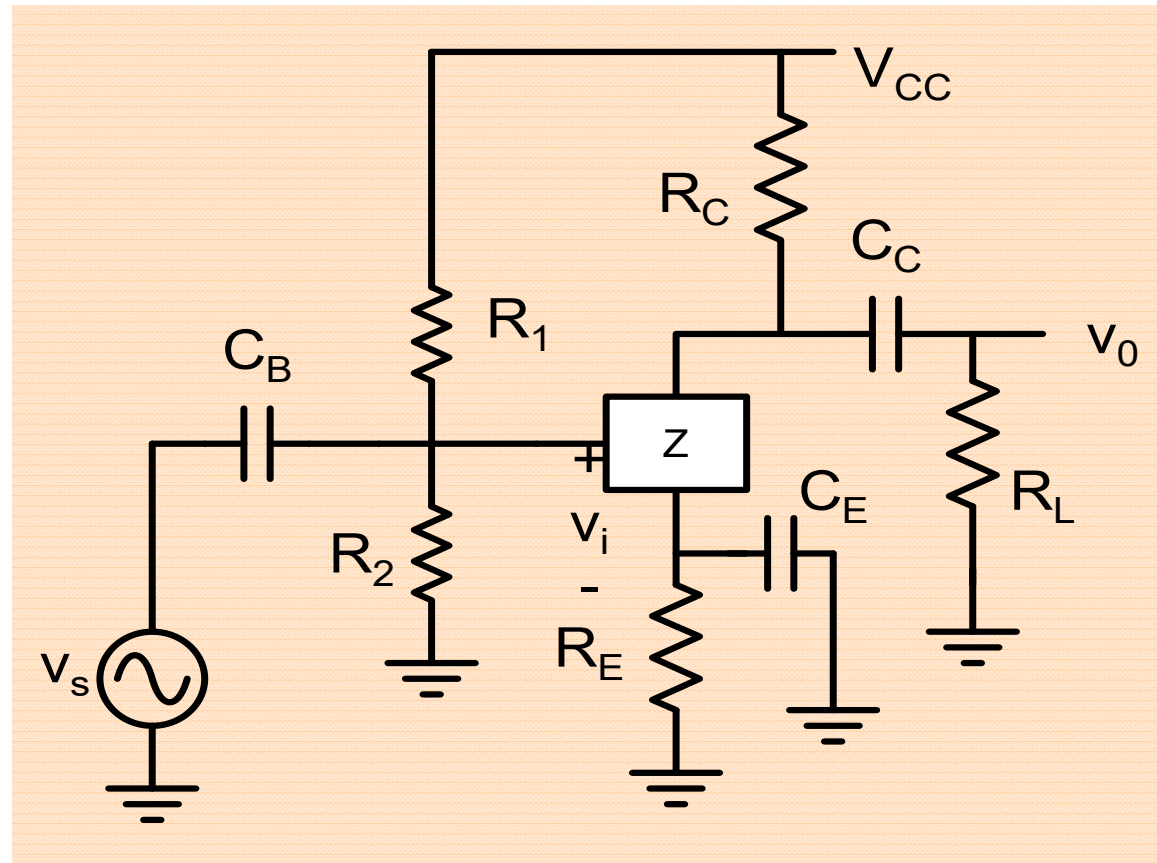
Circuit is much **less sensitive** to variations in circuit parameters

$$A_V = \frac{v_o}{v_s} = -\frac{g_m R_C \parallel R_L}{1 + g_m R_E}$$

**But gain is smaller**



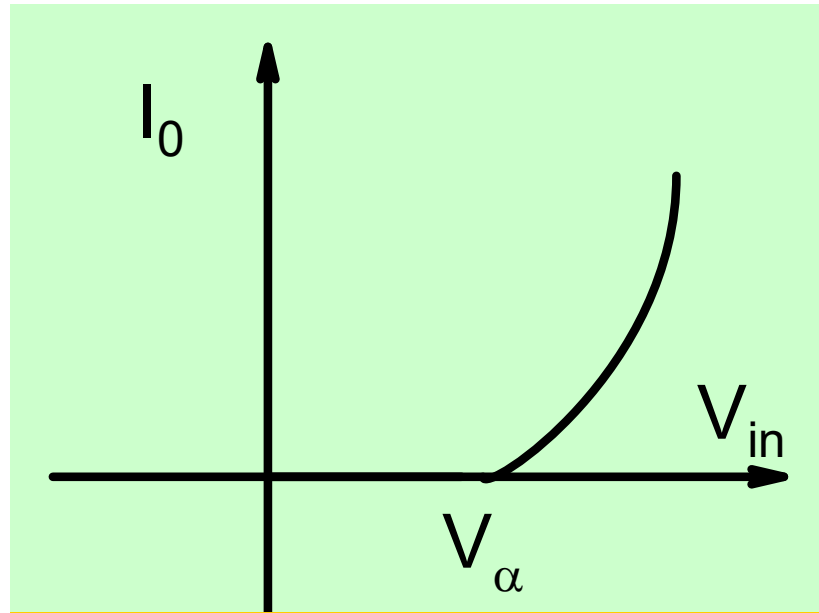
## Simple Solution



For dc, Capacitor  $C_E$  acts as open allowing  $R_E$  to reduce variations in current

For ac Capacitor  $C_E$  acts as a short circuit ( $1/j\omega C \sim 0$ ) allowing high voltage gain to be obtained

## Device Non-Linear:

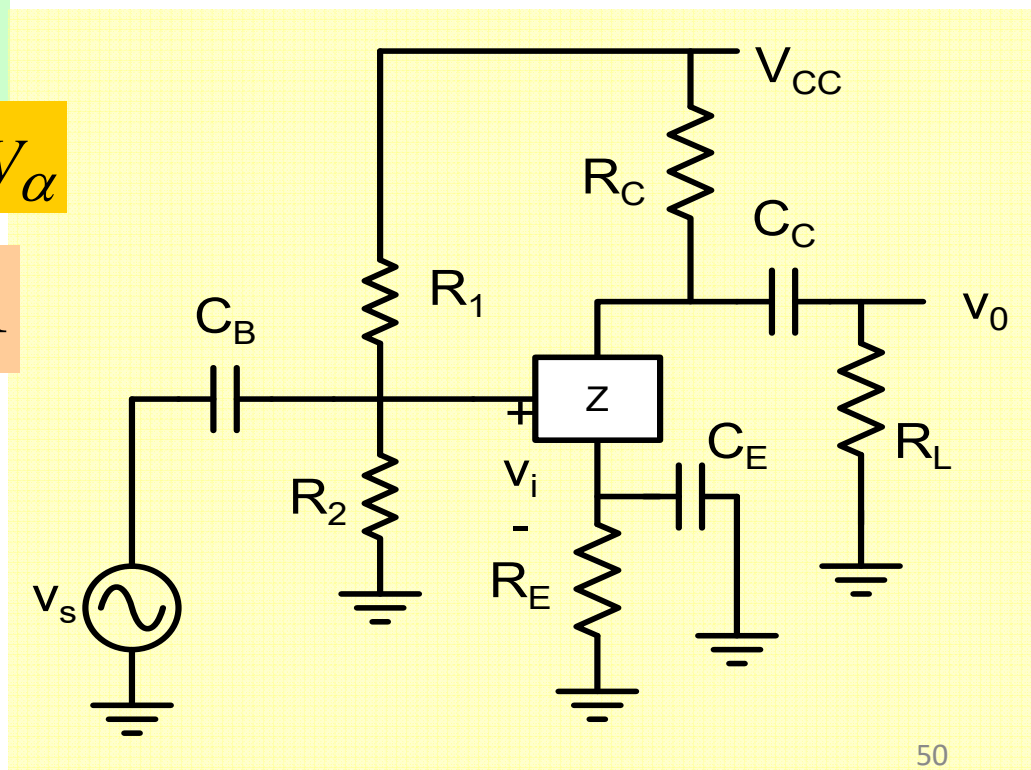
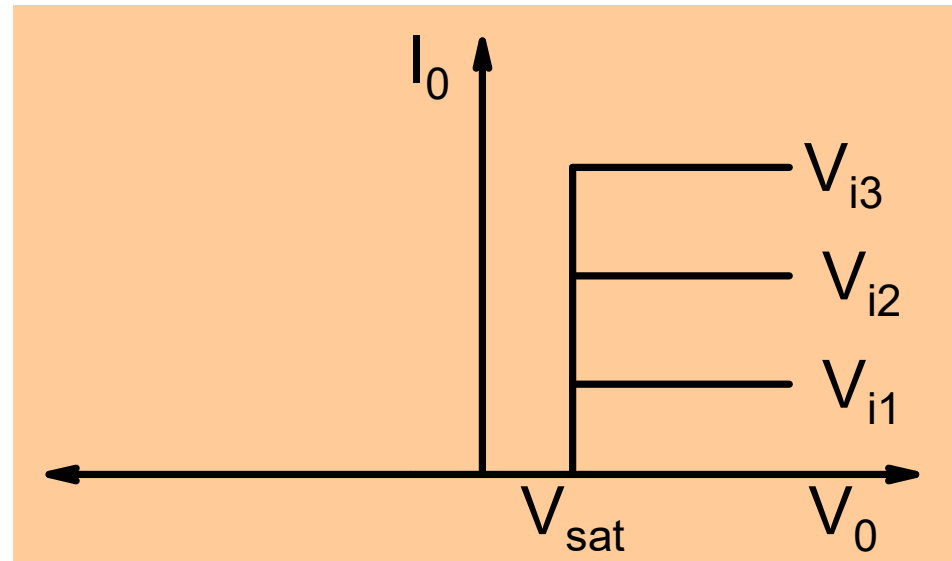


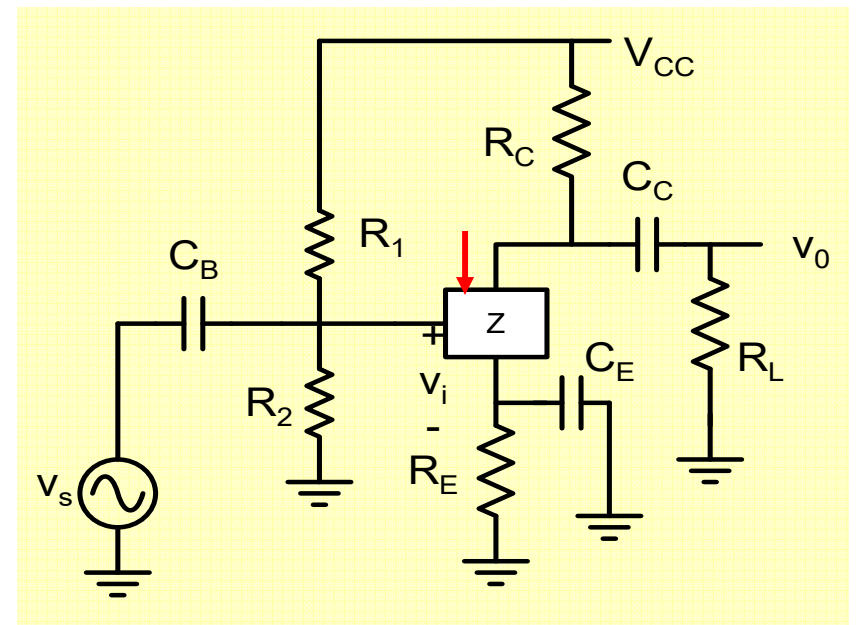
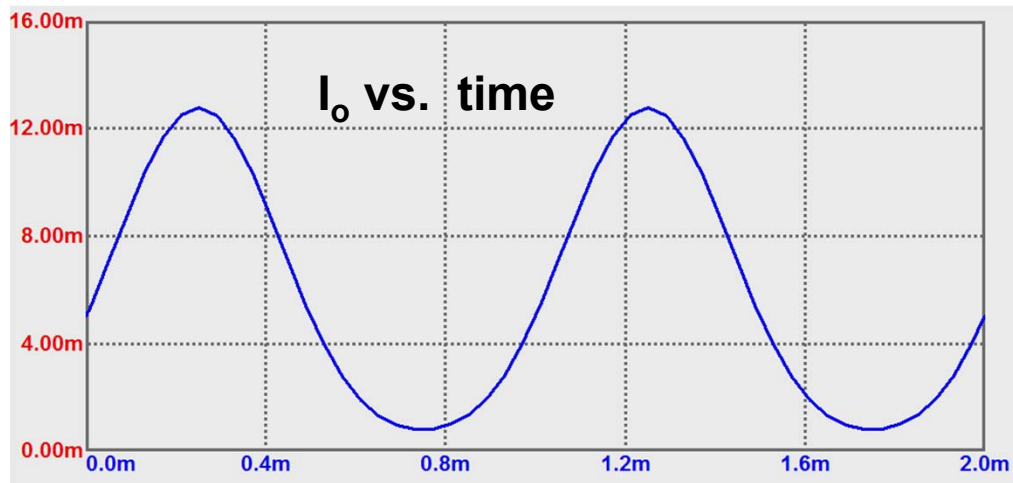
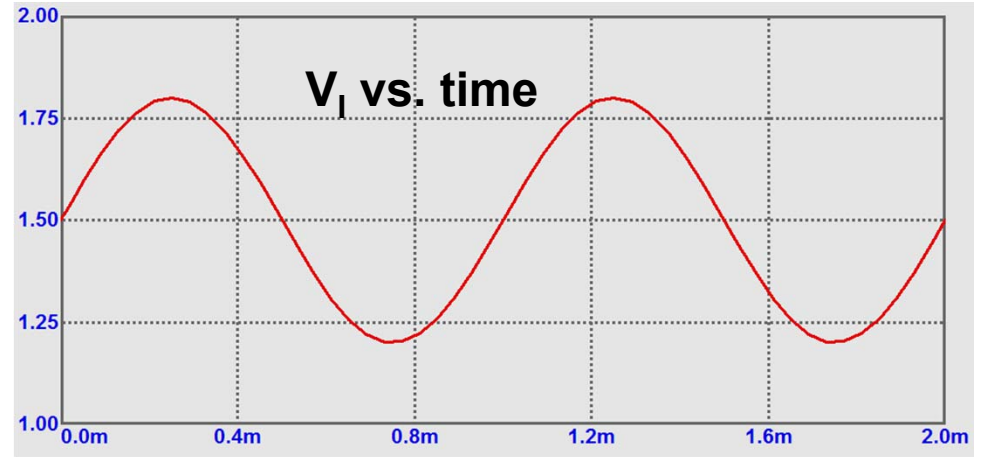
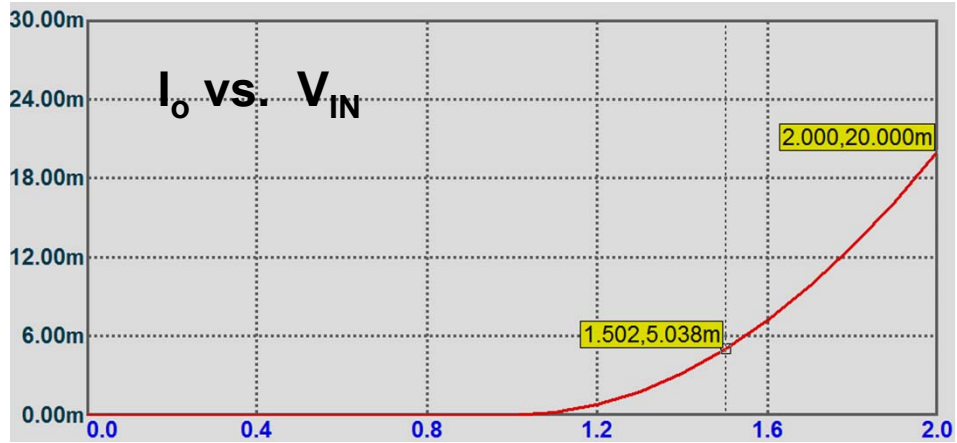
$$I_o = K \times (V_{in} - V_\alpha)^2 \text{ for } V_{in} \geq V_\alpha$$

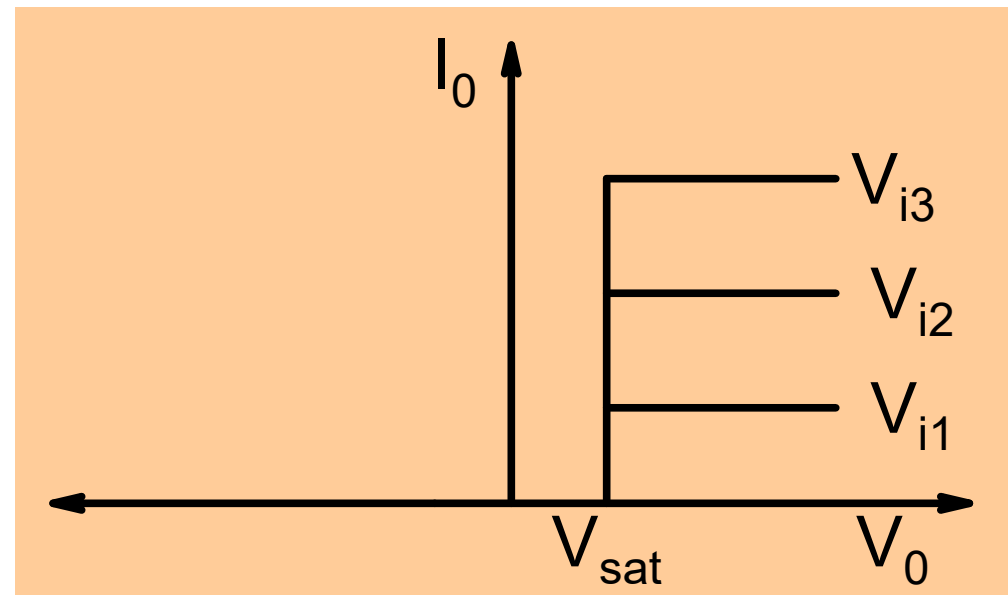
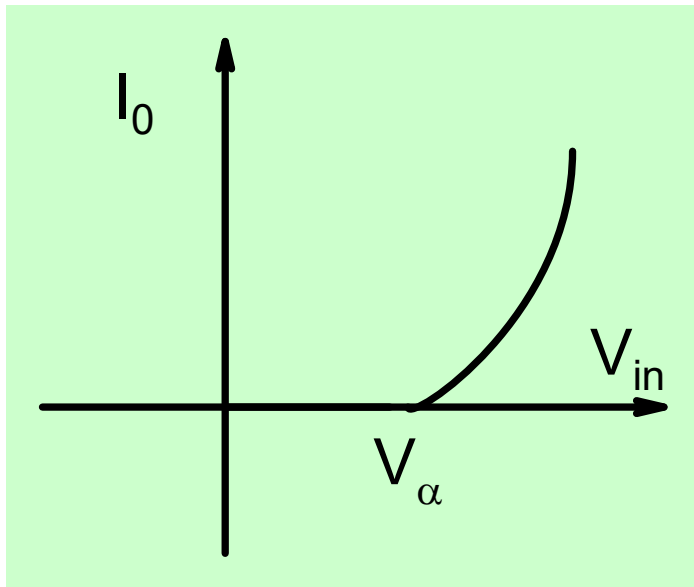
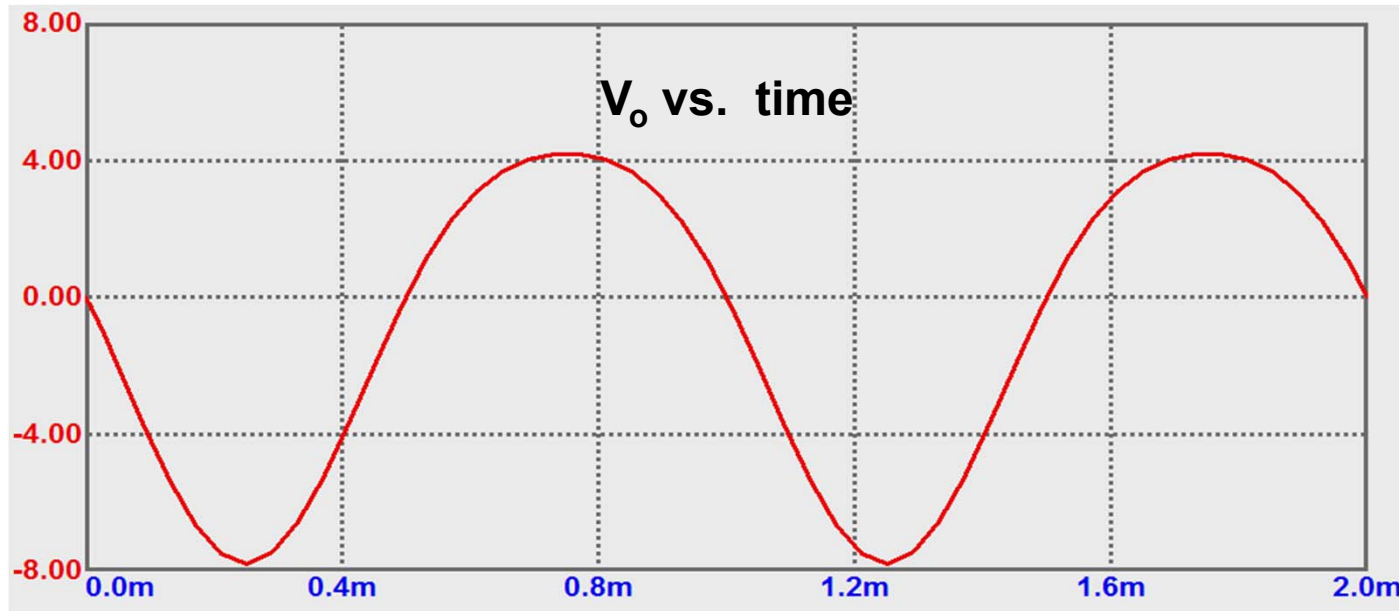
$$V_\alpha = 1.0V ; K = 0.01$$

$$V_B = 1.5V$$

$$v_s = 0.3V \sin \omega t$$



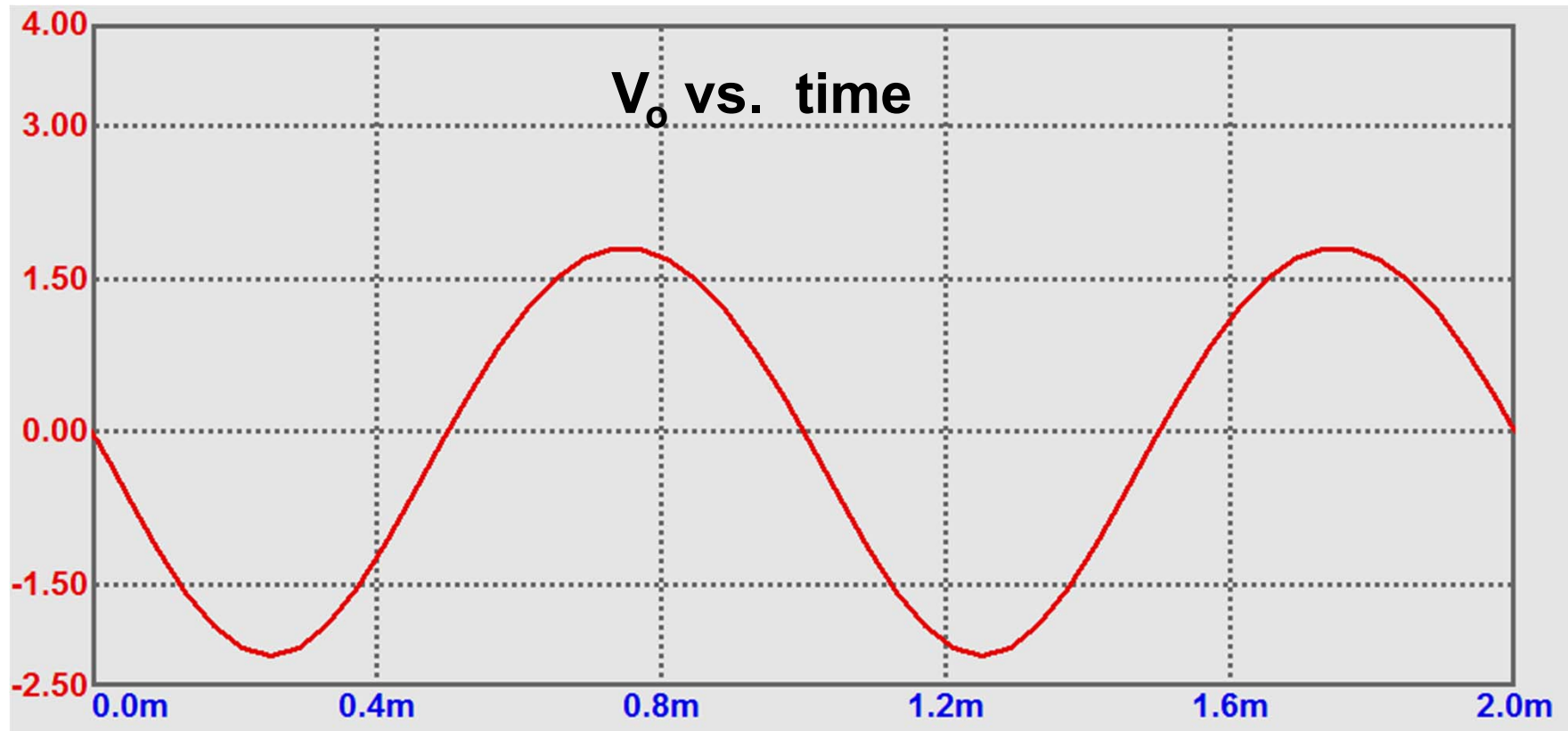




Because of Non-linearity the output waveform is distorted !

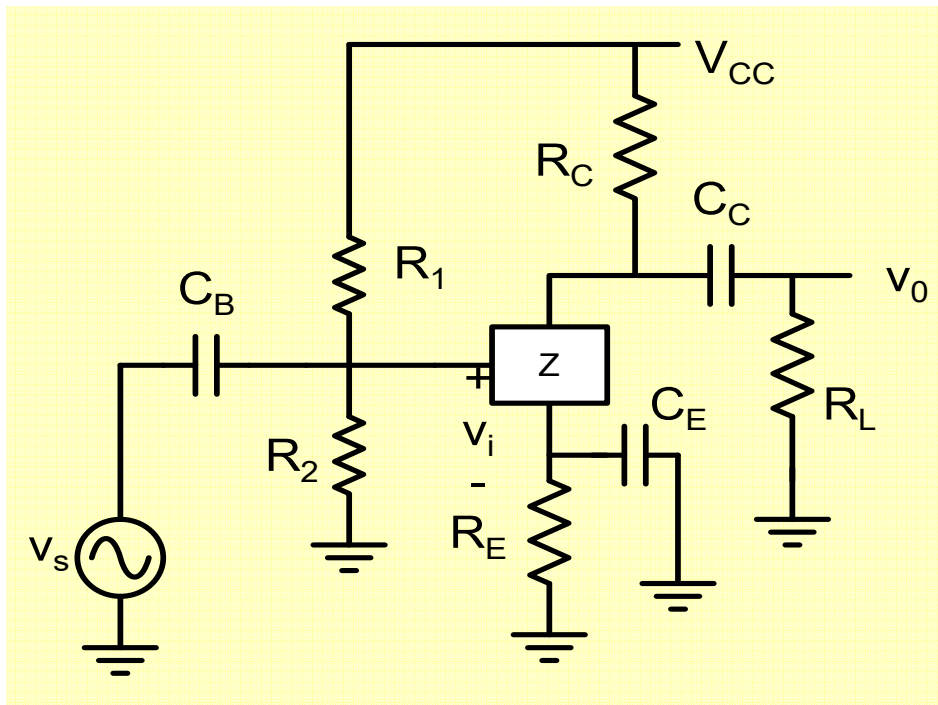
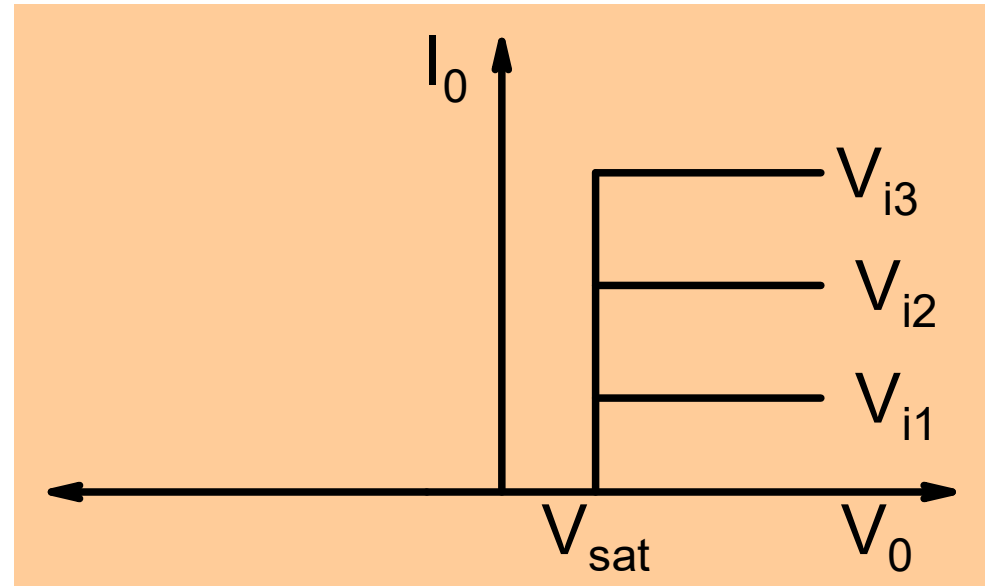
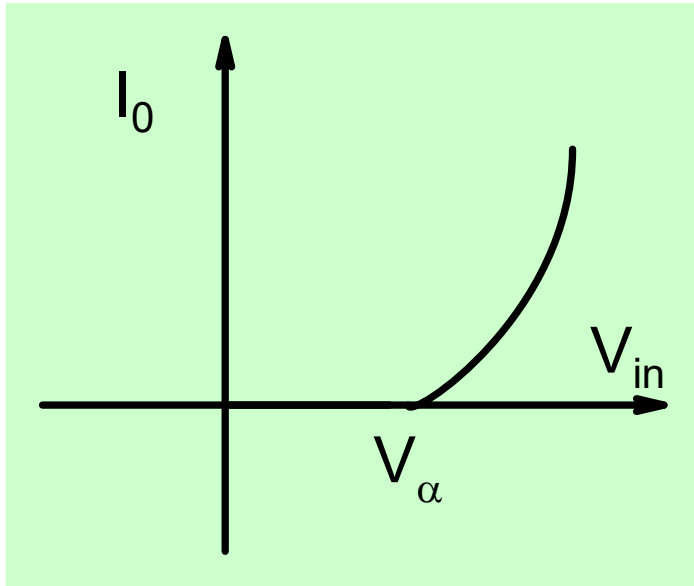
Suppose input is reduced to

$$v_s = 0.1V \sin(\omega t)$$



**Distortion is much smaller if we restrict input voltage to a small value !**

## Building Amplifiers with non-linear devices

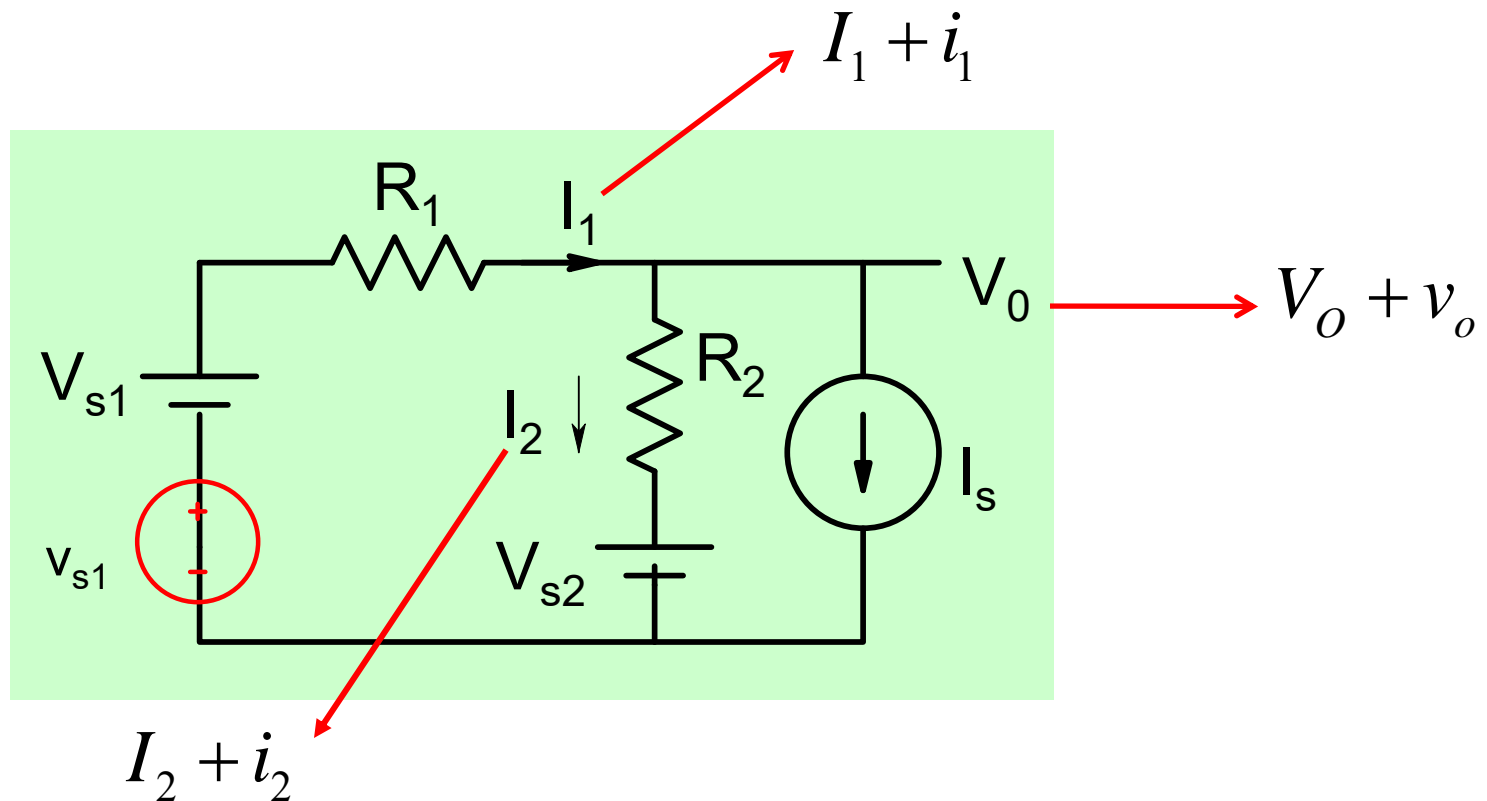


Amplifier will work properly (with small distortion only if we restrict the amplitude of input signal to small values.

How small depends on the nature of non-linearity. The stronger the non-linearity the lesser the signal amplitude.

# Appendix

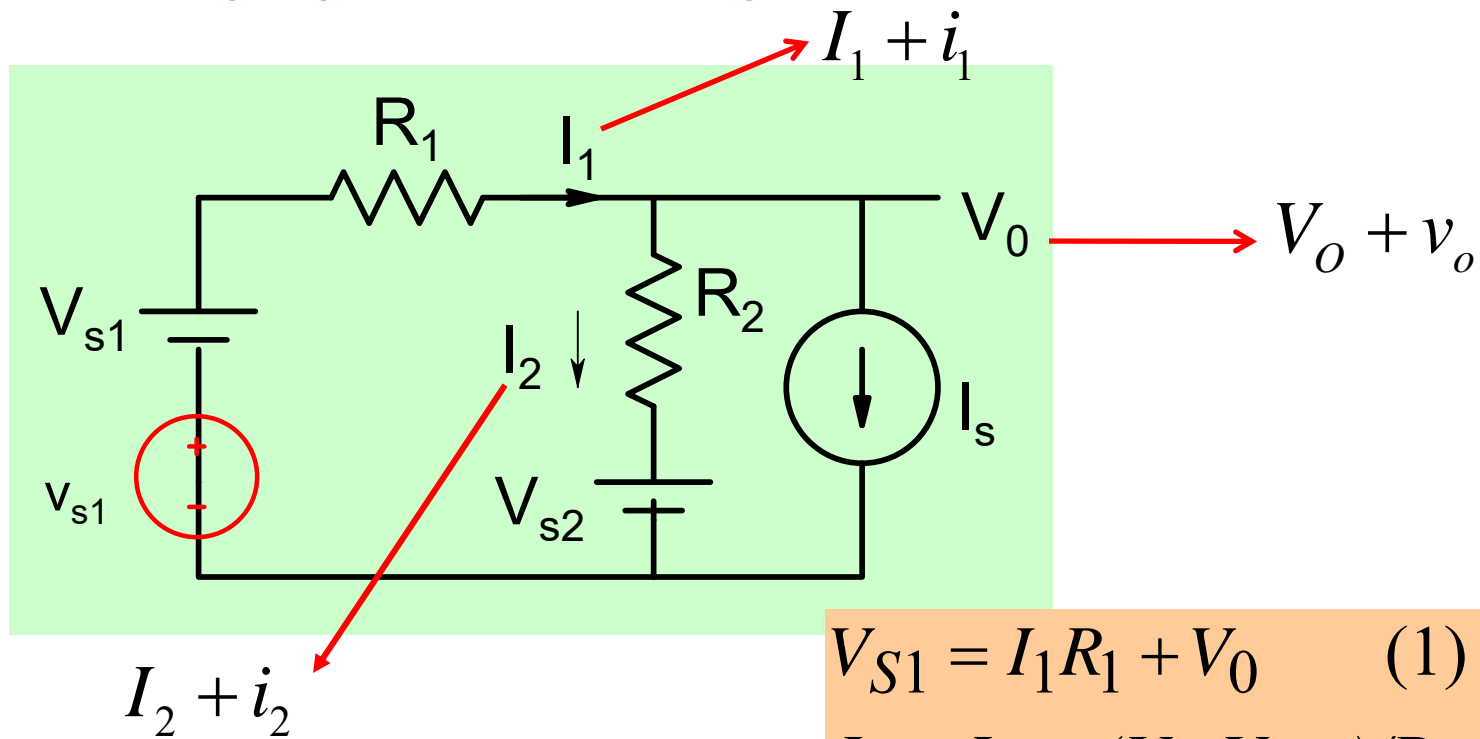
## Incremental (ac) Circuit Analysis



Incremental circuit analysis attempts to find the relationships between incremental voltages and currents  $v_{s1}$ ,  $i_1$ ,  $v_o$ .....



# Incremental (ac) Circuit Analysis



$$V_{S1} = I_1 R_1 + V_0 \quad (1)$$

$$I_1 = I_S + (V_0 - V_{S2}) / R_2 \quad (2)$$

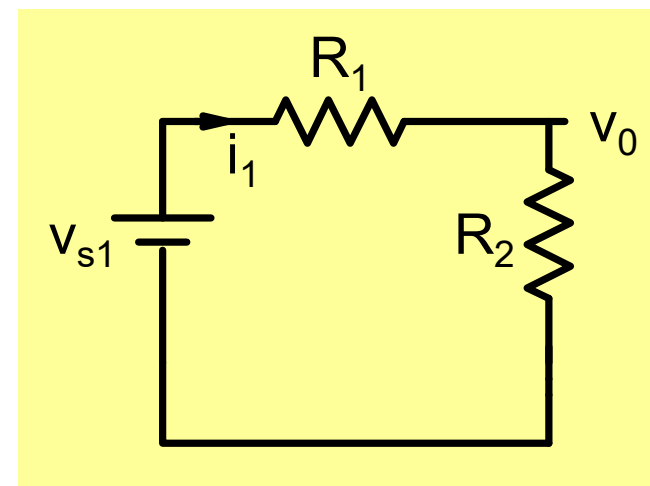
$$V_{S1} + v_{s1} = (I_1 + i_1) \times R_1 + V_0 + v_o \quad (3)$$

$$I_1 + i_1 = I_S + (V_0 + v_o - V_{S2}) / R_2 \quad (4)$$

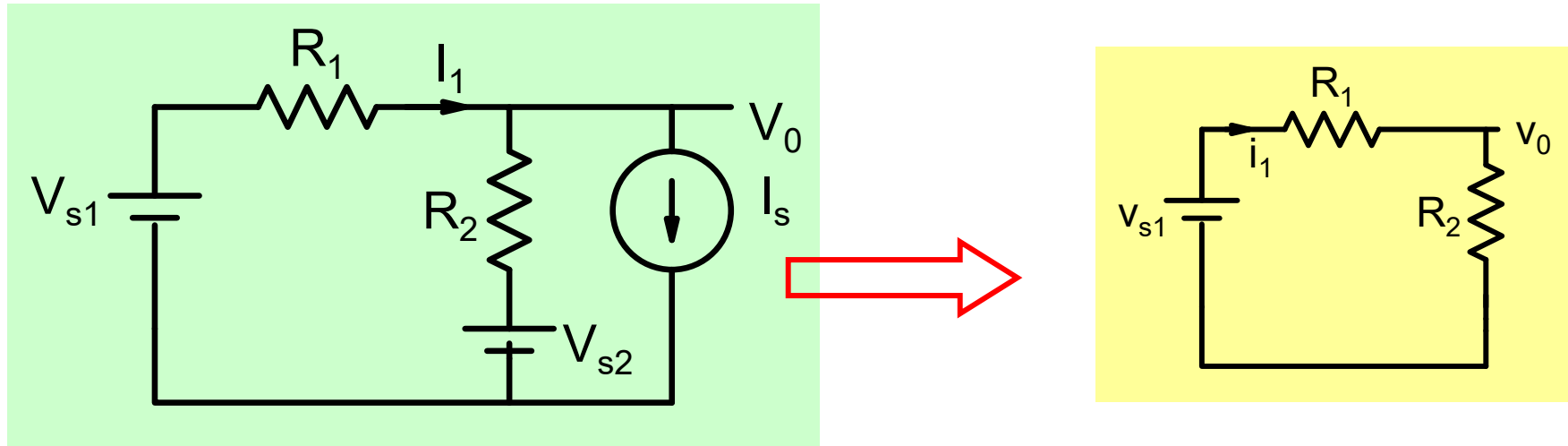
$$(3)-(1): v_{s1} = i_1 R_1 + v_o$$

$$(4)-(2): i_1 = v_o / R_2$$

$$v_{s1} = i_1 R_1 + i_1 R_2$$



## Method: Incremental equivalent circuit



Analyze incremental equivalent circuit obtained by replacing each circuit element by its increment circuit model (sometimes called ac model).

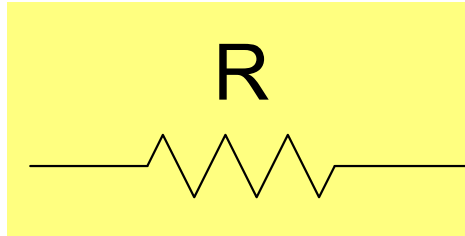
### Incremental model



$$I = f(V) \quad I + i = f(V + v)$$

Relation between  $i$  and  $v$

## Incremental (ac) Models: Resistor



$$V = I \times R$$

$$V + v = (I + i) \times R$$

$$\Rightarrow v = i \times R$$

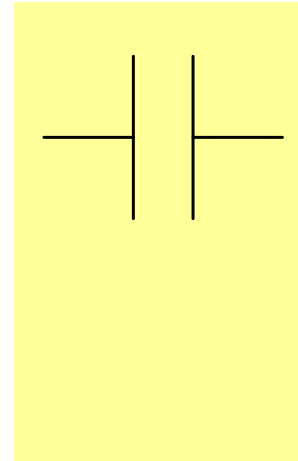
**Incremental model of a resistor is a resistor of the same magnitude**

## Incremental (ac) Models: Capacitor

$$I = C \frac{dV}{dt}$$

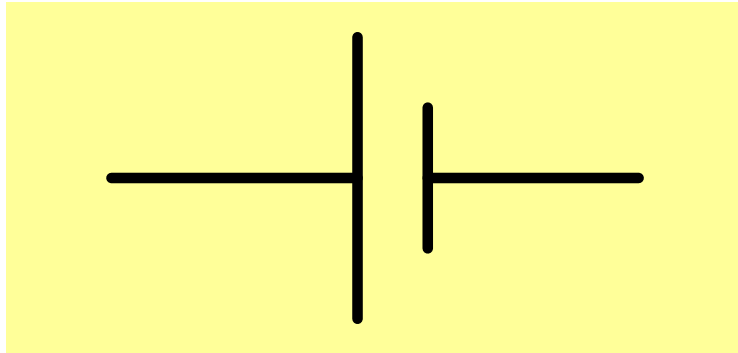
$$I + i = C \frac{d(V + v)}{dt}$$

$$i = C \times \frac{dv}{dt}$$

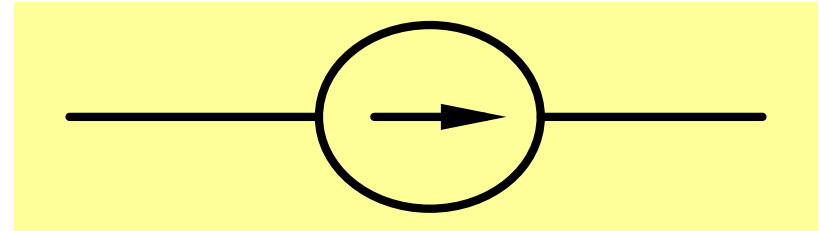


Incremental model of a capacitor is a capacitor of the same magnitude. The same holds for an inductor as well.

## Incremental (ac) Models



$$V = \text{const} \tan t$$
$$\Rightarrow v = 0$$

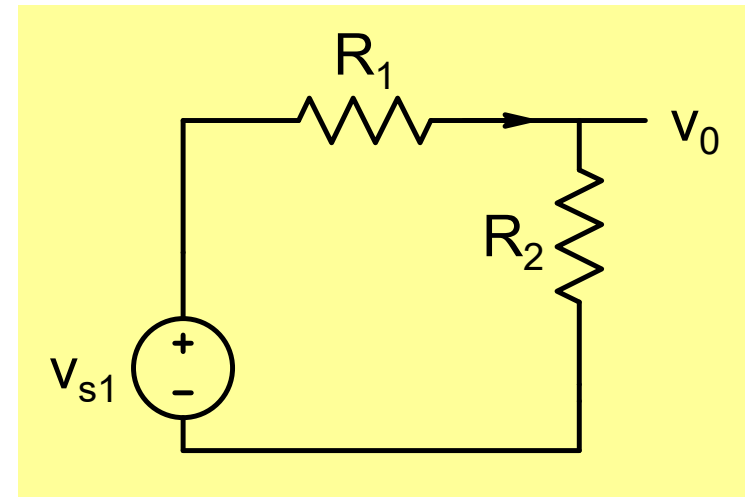
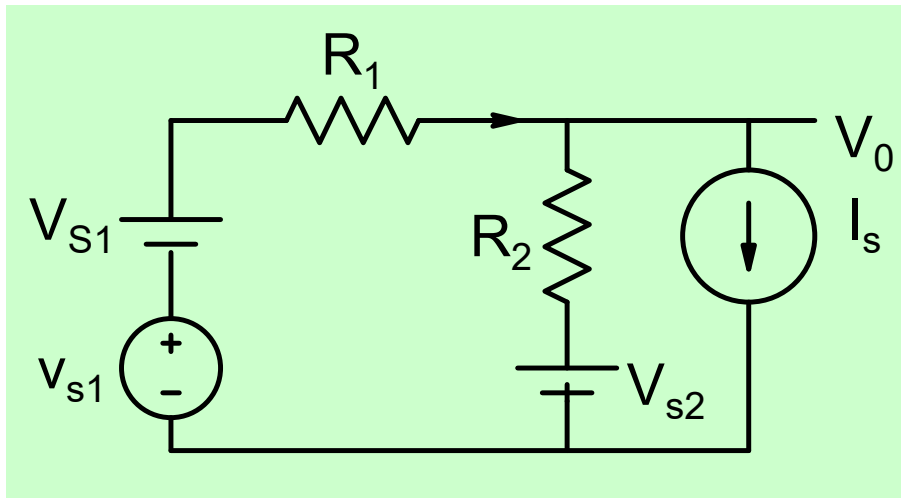


$$I = \text{const} \tan t$$
$$\Rightarrow i = 0$$

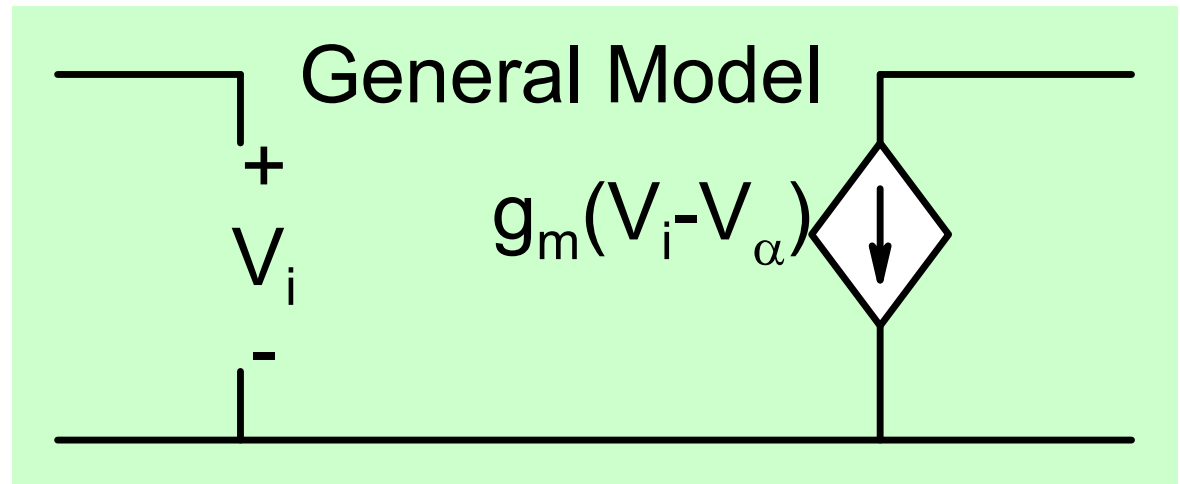
Incremental model of a constant Voltage Source is a short circuit

Incremental model of a constant current Source is an open circuit

# Incremental (ac) circuit Analysis



$$v_o = v_{s1} \times \frac{R_2}{R_1 + R_2}$$



$$I_o = g_m (V_i - V_\alpha)$$

$$I_o + i_o = g_m (V_I + v_i - V_\alpha)$$

$$i_o = g_m v_i$$

