

UNIVERSITÉ LIBRE DE BRUXELLES

SYNTHÈSE

Fluid mechanics II MECA-H-305

Auteur:
Enes ULUSOY

Professeur :
Gérard DEGREGZ

Année 2015 - 2016

Appel à contribution

Synthèse Open Source



Ce document est grandement inspiré de l'excellent cours donné par Gérard Degrez à l'EPB (École Polytechnique de Bruxelles), faculté de l'ULB (Université Libre de Bruxelles). Il est écrit par les auteurs susnommés avec l'aide de tous les autres étudiants et votre aide est la bienvenue ! En effet, il y a toujours moyen de

l'améliorer surtout que si le cours change, la synthèse doit être changée en conséquence. On peut retrouver le code source à l'adresse suivante

<https://github.com/nenglebert/Syntheses>

Pour contribuer à cette synthèse, il vous suffira de créer un compte sur *Github.com*. De légères modifications (petites coquilles, orthographe, ...) peuvent directement être faites sur le site ! Vous avez vu une petite faute ? Si oui, la corriger de cette façon ne prendra que quelques secondes, une bonne raison de le faire !

Pour de plus longues modifications, il est intéressant de disposer des fichiers : il vous faudra pour cela installer \LaTeX , mais aussi *git*. Si cela pose problème, nous sommes évidemment ouverts à des contributeurs envoyant leur changement par mail ou n'importe quel autre moyen.

Le lien donné ci-dessus contient aussi le README contient de plus amples informations, vous êtes invités à le lire si vous voulez faire avancer ce projet !

Licence Creative Commons

Le contenu de ce document est sous la licence Creative Commons : *Attribution-NonCommercial-ShareAlike 4.0 International (CC BY-NC-SA 4.0)*. Celle-ci vous autorise à l'exploiter pleinement, compte- tenu de trois choses :



1. *Attribution* ; si vous utilisez/modifiez ce document vous devez signaler le(s) nom(s) de(s) auteur(s).
2. *Non Commercial* ; interdiction de tirer un profit commercial de l'œuvre sans autorisation de l'auteur
3. *Share alike* ; partage de l'œuvre, avec obligation de rediffuser selon la même licence ou une licence similaire

Si vous voulez en savoir plus sur cette licence :

<http://creativecommons.org/licenses/by-nc-sa/4.0/>

Merci !

Contents

1	Generalities	1
1.1	Fundamental laws	1
1.1.1	Mass conservation equation	2

Chapter 1

Generalities

1.1 Fundamental laws

Reminder

Let's first remind the 3 basic principles of *Fluid mechanics I* :

- **Mass conservation** : *The mass of a closed system remains constant in time.*
This is much a definition of a closed system than a principle. We have to notice that related to Einstein law of relativity, $E = mc^2$, mass must vary with energy. But if we exclude nuclear reactions, our approximation is valid. Indeed, the square of light velocity has a greater impact on energy than the mass term. If the energy exchange is huge like in nuclear reaction, mass vary, but in smaller energies domain (combustion for example), the mass can be considered as constant.
- **Newton's law** : *the time rate of change of momentum of a closed system is equal to the sum of the forces applied on the system.*
- **First principle of thermodynamics** : *the time rate of change of the total energy of a closed system is equal to the sum of the power of the forces applied on the system and the thermal power provided to the system.*

Useful equations

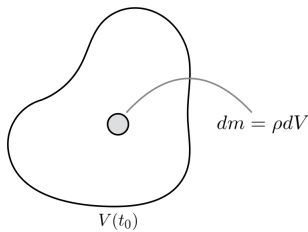


Figure 1.1

Let's consider the integral on a moving volume of a function depending on time and position $f(\vec{x}, t)$. Imagine that Figure 1.1 represents the moving volume at initial time containing mass m . An infinitesimal part of that volume contains an infinitesimal mass $dm = \rho dV$, where ρ is mass density. We deduce the expression of the total mass at any time by that of the initial time

$$M(t_0) = \int_{V(t_0)} \rho(\vec{x}, t_0) dV \quad \Rightarrow \quad M(t) = \int_{V(t)} \rho(\vec{x}, t) dV \quad (1.1)$$

By considering $\rho(\vec{x}, t)$ as $f(\vec{x}, t)$, the derivative of the integral is given by

Reynolds transport theorem

$$\frac{d}{dt} \int_{V(t)} f(\vec{x}, t) dV = \int_{V(t)} \frac{\partial f}{\partial t}(\vec{x}, t) dV + \oint_{S(t)=\partial V(t)} f(\vec{x}, t) \vec{b} \cdot \vec{n} dS \quad (1.2)$$

where \vec{b} is the surface displacement velocity.

The second equation that will be used in the developement is given by

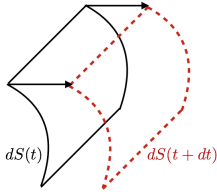
Gauss theorem

$$\oint_{S=\partial V} \vec{a} \cdot \vec{n} dS = \int_V \nabla \cdot \vec{a} dV \quad (1.3)$$

1.1.1 Mass conservation equation

If $V(t)$ is the moving volume occupied by the closed system as time varies, then by definition of a closed system $\frac{dM(t)}{dt} = 0$. The corresponding equation using Reynolds transport theorem is

$$M(t) = \int_{V(t)} \rho dV \quad \Rightarrow \quad \frac{dM(t)}{dt} = \int_{V(t)} \frac{\partial \rho}{\partial t} dV + \oint_{S(t)=\partial V(t)} \rho \vec{b} \cdot \vec{n} dS = 0 \quad (1.4)$$



We have to express that this volume is not traversed by material. There is no flux of fluid and the particles in the volume are always the same. By definition, the infinitesimal distance traveled by the surface and the fluid are

$$d\vec{x} = \vec{b} dt \quad \text{and} \quad d\vec{x}' = \vec{u} dt \quad (1.5)$$

Figure 1.2

where \vec{u} is the fluid velocity. Under which condition do we know that the fluid has not traversed the boundary? We have to define the relative displacement $d\vec{x}' - d\vec{x}$ of the fluid in regard to the fluid. For a closed system

$$\begin{aligned} (d\vec{x}' - d\vec{x}) \cdot \vec{n} = 0 & \Leftrightarrow dt(\vec{u} - \vec{b}) \cdot \vec{n} = 0 \Leftrightarrow (\vec{u} - \vec{b}) \cdot \vec{n} = 0 \\ & \Rightarrow \vec{b} \cdot \vec{n} = \vec{u} \cdot \vec{n} \end{aligned} \quad (1.6)$$

Mass conservation equation for closed systems (integral form)

$$\int_{V(t)} \frac{\partial \rho}{\partial t} dV + \oint_{S(t)=\partial V(t)} \rho \underbrace{\vec{b} \cdot \vec{n}}_{=\vec{u} \cdot \vec{n}} dS = 0 \quad (1.7)$$

How to write this equation in a different way? Let's consider now a fixed open system composed of fluid particles in the fixed volume $V_0(t) = V(t_0)$. Similarly to the previous point, the mass variation in this fixed volume is expressed like

$$M_0(t) = \int_{V_0(t)} \rho dV \quad \Rightarrow \quad \int_{V_0(t)} \frac{\partial \rho}{\partial t} dV + \oint_{S_0(t)=\partial V_0(t)} \rho \vec{b} \cdot \vec{n} dS. \quad (1.8)$$

The volume integral expresses the variable mass in the fixed volume and the surface integral is null due to the null surface velocity (since the volume is fixed). This relation enables us to write the

Mass conservation equation for fixed open systems (integral form)

$$\frac{dM_0}{dt} + \underbrace{\oint_{S_0(t)=\partial V_0(t)} \rho \vec{u} \vec{n} dS}_{\text{mass flow out of the system}} = 0 \quad (1.9)$$

Let's finally consider an arbitrary open system containing fluid particles in a moving volume $V_*(t)$ such that $V_*(t_0) = V(t_0) = V_0$. Similarly we have using the Reynolds transport theorem

$$M_*(t) = \int_{V_*(t)} \rho dV \quad \Rightarrow \quad \frac{dM_*(t)}{dt} = \int_{V_*(t)} \frac{\partial \rho}{\partial t} dV + \oint_{S_*(t)=\partial V_*(t)} \rho \vec{b} \vec{n} dS \quad (1.10)$$

Using the definition of the volume at $t = t_0$, we can equalize the volume integral with that of (1.7) to find

Mass conservation equation for arbitrary open systems (integral form)

$$\frac{dM_*(t_0)}{dt} + \oint_{S(t_0)=\partial V(t_0)} \rho (\vec{u} - \vec{b}) \vec{n} dS = 0 \quad (1.11)$$

Let's now take (1.7) again and apply Gauss theorem

$$\begin{aligned} \int_{V(t)} \frac{\partial \rho}{\partial t} dV + \oint_{S(t)=\partial V(t)} \rho \underbrace{\vec{u} \vec{n}}_{\vec{a}} dS &= 0 \quad \text{with} \quad \oint_{S(t)} \rho \underbrace{\vec{u} \vec{n}}_{\vec{a}} dS = \int_{V(t)} \nabla \rho \vec{u} dV \\ &\Leftrightarrow \int_{V(t)} \left[\frac{\partial \rho}{\partial t} + \nabla \rho \vec{u} \right] dV \end{aligned} \quad (1.12)$$

For this last equation to be true for all systems, the integrated term must be equal to zero

Mass conservation equation (differential form (1) - divergent form)

$$\frac{\partial \rho}{\partial t} + \nabla \rho \vec{u} = 0 \quad (1.13)$$

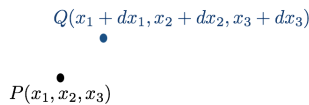
 In order to find the second differential form, let's consider 2 points Q and P as described in Figure 1.3. The difference of density between the 2 points is

Figure 1.3

$$\begin{aligned} \rho_Q(t + dt) - \rho_P(t) &= \rho(x_1 + dx_1, x_2 + dx_2, x_3 + dx_3, t + dt) - \rho(x_1, x_2, x_3) \\ &= d\rho = \frac{\partial \rho}{\partial x_1} dx_1 + \frac{\partial \rho}{\partial x_2} dx_2 + \frac{\partial \rho}{\partial x_3} dx_3 + \frac{\partial \rho}{\partial t} dt \end{aligned} \quad (1.14)$$

In general, the fluid particles at $P(t)$ and $Q(t + dt)$ are different. However, if $dx_1 = u_1 dt$, $dx_2 = u_2 dt$, $dx_3 = u_3 dt$, then the fluid particles at the 2 points are the same. By making appear these velocities in (1.14),

$$d\rho = \left(\frac{\partial \rho}{\partial x_1} u_1 + \frac{\partial \rho}{\partial x_2} u_2 + \frac{\partial \rho}{\partial x_3} u_3 + \frac{\partial \rho}{\partial t} \right) dt \quad (1.15)$$

Finally, after dividing by dt the 2 members of the equation, we obtain the definition of the time rate of change of density when I follow the fluid $\dot{\rho}$. As (1.13) can be expressed in term of indicial notation like

$$\frac{\partial \rho}{\partial t} + u_i \frac{\partial \rho}{\partial x_i} + \rho \frac{\partial u_i}{\partial x_i} = 0 \quad (1.16)$$

Replacing the sum of first and second term by $\dot{\rho}$ gives the last form

Mass conservation equation (differential form (2) - substancial form)

$$\dot{\rho} + \rho \nabla \vec{u} = 0 \quad (1.17)$$

1.1.2 Newton's second law : Momentum equation