

SIMUTECH PROJECT REPORT

HANDS-ON ASPEN AND MATLAB

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210009

OVERVIEW

- Differential equations are essential for modeling and analyzing dynamic systems.
- MATLAB provides powerful tools for numerically solving differential equations.
- This report explores the utilization of MATLAB in solving differential equations and its application in heat conduction problems in chemical engineering.
- The report also discusses the use of Aspen, a process simulation software, for solving reactor problems.
- The report is organized as follows:
 - Introduction to differential equations and MATLAB's capabilities in solving ordinary and partial differential equations.
 - Application of MATLAB in solving heat conduction problems in chemical engineering, including formulation, boundary conditions, and real-world case studies.
 - Introduction to Aspen and its role in modeling and simulating various reactor problems.
 - Practical application of Aspen for solving reactor problems, including a step-by-step guide and analysis of simulation outcomes.
 - Presentation of case studies demonstrating the combined usage of MATLAB and Aspen.

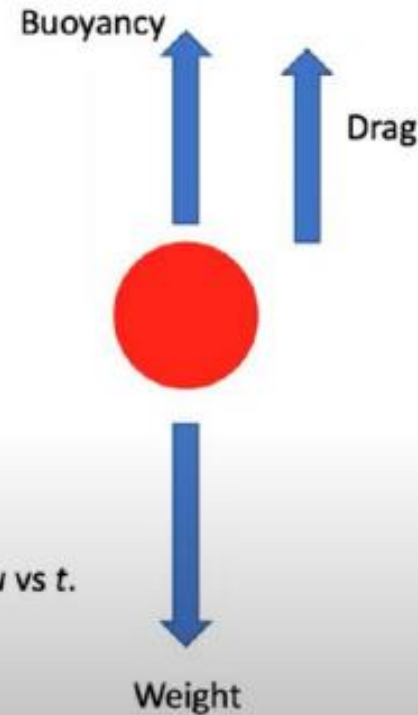
Assignment 1

$$m \frac{du}{dt} = W - F_B - F_D$$

$$m \frac{du}{dt} = mg - V\rho g - 6\pi R\eta u$$

EXERCISE:

- ☐ Fix the properties of the fluid and solid sphere.
- ☐ Do you get a terminal velocity? What will be the analytical expression for the same?
- ☐ Get the analytical answer for u vs t (assume $u = 0$ at $t = 0$)
- ☐ For the same initial velocity, numerically compute u vs t .
- ☐ Compare the analytical and numerical answers on a plot of u vs t .
 - ☐ Analytical – solid line; numerical – dashed line



ASSIGNMENT 1 : PROBLEM STATEMENT

➤ Take the value of the required properties as follows:

- Radius of sphere = 10^{-5} m
- Density of liquid = 1000 kg/m^3
- Density of sphere = 8050 kg/m^3
- Viscosity of liquid = 10^{-3} Pa.s
- Acceleration due to gravity = 9.8 m/s^2

→ To calculate analytical expression for u vs t

⇒ The equation of motion for an object falling through a viscous fluid is given by

$$m \frac{du}{dt} = mg - 6\pi\eta R u$$

where u is velocity of sphere at time t

Taking $m = \sigma V$ where σ = density of sphere
 V = Volume of sphere

$$\Rightarrow \sigma V \frac{du}{dt} = \sigma V g - 6\pi\eta R u$$

$$\Rightarrow \sigma V \frac{du}{dt} = \sigma V g - \rho V g - 6\pi\eta R u$$

$$\Rightarrow \sigma V \frac{du}{dt} = (\sigma - \rho) V g - 6\pi\eta R u$$

$$\Rightarrow \int_0^t \frac{dt}{\sigma V} = \int_0^u \frac{du}{(\sigma - \rho) V g - 6\pi\eta R u}$$

$$\Rightarrow \frac{t}{\sigma V} = \frac{\ln[(\sigma - \rho) V g - 6\pi\eta R u] \Big|_0^u}{-6\pi\eta R}$$

Numerical computation of u vs t :

To obtain the numerical solution for u vs t , we can use numerical integration techniques such as Euler's method or the Runge-Kutta method. By discretizing the time interval and approximating the derivative, we can calculate the velocity at each time step.

Comparison of analytical and numerical answers:

Plotting the analytical solution (solid line) and the numerical solution (dashed line) on the same graph will allow us to compare the two solutions and observe any differences or similarities between them.

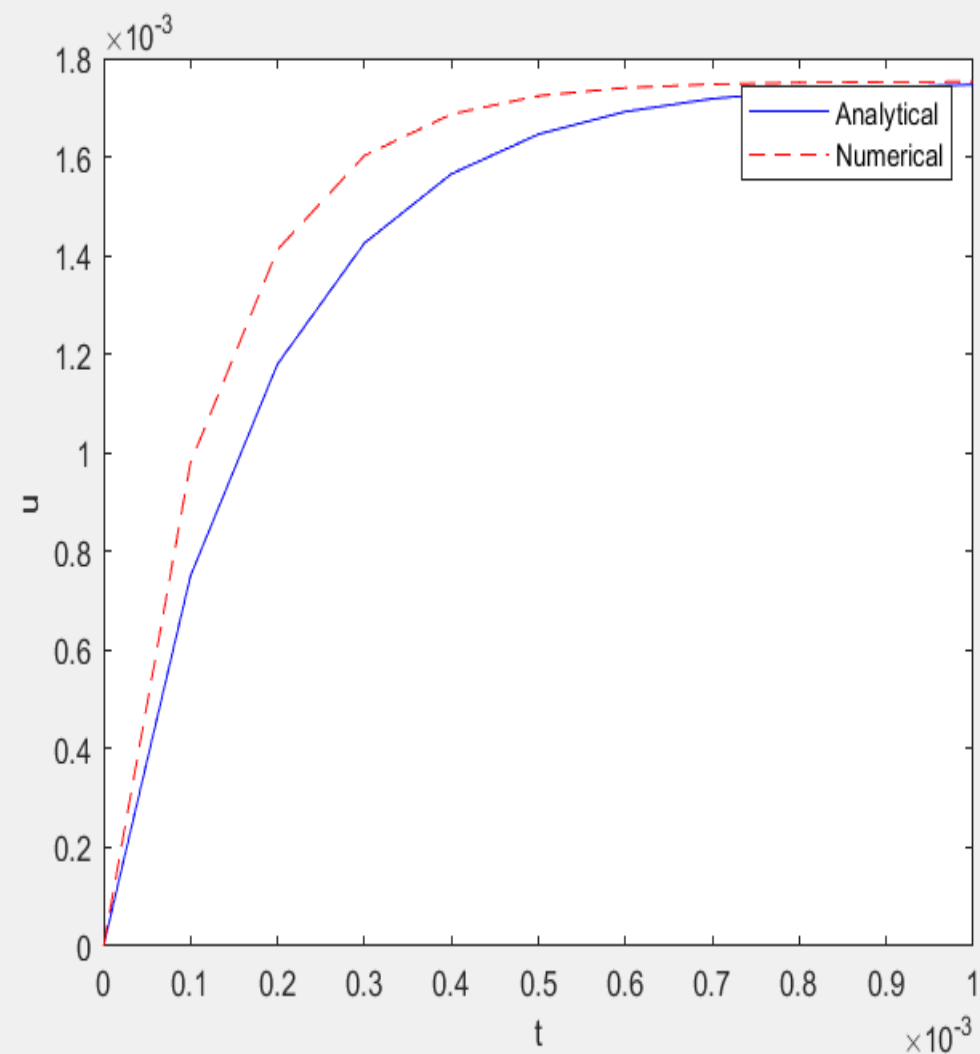
```

1 % Define the parameters
2 density = 8050; % Density of the sphere material
3 r = 0.0001; % Radius of the sphere
4 m = (4/3) * pi * r^3 * density; % Mass of the sphere
5 g = 9.8; % Acceleration due to gravity
6 mu = 0.001; % Viscosity of the fluid
7
8 % Define the time interval
9 dt = 0.0001;
10 t = 0:dt:0.001;
11
12 % Initialize arrays for storing velocity values
13 u_analytical = zeros(size(t));
14 u_numerical = zeros(size(t));
15
16 % Analytical solution
17 u_analytical = (m * g) / (6 * pi * r * mu) * (1 - exp(-(6 * pi * r * mu * t) / m));
18
19 % Numerical solution using Euler's method
20 u_numerical(1) = 0;
21 for i = 2:length(t)
22     u_numerical(i) = u_numerical(i - 1) + (((m * g) - (6 * pi * r * mu * u_numerical(i - 1))) / m) * dt;
23 end
24
25 % Plotting the results
26 plot(t, u_analytical, 'b-', t, u_numerical, 'r--');
27 xlabel('t');
28 ylabel('u');
29 legend('Analytical', 'Numerical');
30

```

Figure 1

File Edit View Insert Tools Desktop Window Help

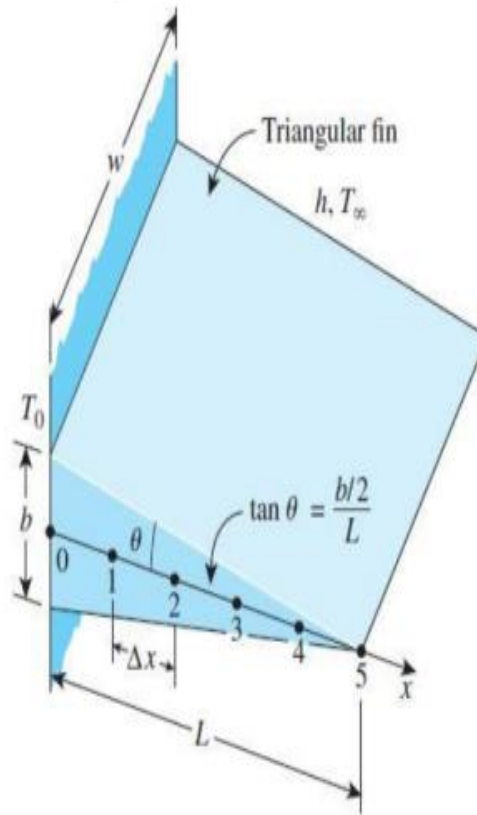


ASSIGNMENT 2: PROBLEM STATEMENT

Assignment-2

Consider an aluminum alloy fin ($k = 180 \text{ W/m}\cdot\text{K}$) of triangular cross section with length $L=20 \text{ cm}$, base thickness $b = 4 \text{ cm}$, and very large width w . The base of the fin is maintained at a temperature of $T_0 = 100^\circ\text{C}$. The fin is losing heat to the surrounding medium at $T_\infty = 25^\circ\text{C}$ with a heat transfer coefficient of $h = 15 \text{ W/m}^2\cdot\text{K}$. Using the finite difference method with 20 equally spaced nodes along the fin in the x -direction, Write a matlab program to find-

- (a) The Temperatures at the nodes
- (b) Plot the Temperature(T) vs distance from the base(x) plot.



Editor - C:\Users\akas\Desktop\amc\AAKASH_SARAN_210009_A2\assign_2.m

```

1  A=zeros(20,20);
2  B=zeros(20,1);
3
4  for i=2:20
5      B(i,1)=-0.209;
6  end
7  B(1,1) = -1950.209;
8
9  for i=2:1:19
10     A(i,i-1)=20.5-i;
11     A(i,i)=2*(i) - 40.008;
12     A(i,i+1)=19.5-(i);
13
14 end
15 A(1,1)=2*(1) - 40.008;
16 A(1,2)=19.5-(1);
17 A(20,19)=1;
18 A(20,20)=-1.008;
19
20 A
21 B
22 maxerr = 1e-5;
23 T = zeros(1,size(A,1));
24 err1 = inf;
25 itr = 0;
26 while all(err1>maxerr)
27     T_old = T;
28     for i = 1:size(A,1)
29         sum = 0;
30         for j = 1:i-1
31             sum = sum + A(i,j)*T(j);
32         end
33         for j=i+1:size(A,1)
34             sum = sum+A(i,j)*T_old(j);
35         end
36         T(i) = (1/A(i,i)) * (B(i) - sum);
37     end
38     itr = itr + 1;
39     y(itr,:) = T;
40     err1 = abs(T_old-T);
41 end
42 for i=1:1:20
43     fprintf("T_%d is %d.\n",i,T(i));
44 end
45 x=0.01:0.01:0.2;
46 plot(x,T)

```

```

T_1 is 9.945220e+01.
T_2 is 9.890652e+01.
T_3 is 9.836296e+01.
T_4 is 9.782152e+01.
T_5 is 9.728221e+01.
T_6 is 9.674502e+01.
T_7 is 9.620997e+01.
T_8 is 9.567703e+01.
T_9 is 9.514624e+01.
T_10 is 9.461757e+01.
T_11 is 9.409103e+01.
T_12 is 9.356663e+01.
T_13 is 9.304435e+01.
T_14 is 9.252421e+01.
T_15 is 9.200621e+01.
T_16 is 9.149034e+01.
T_17 is 9.097661e+01.
T_18 is 9.046504e+01.
T_19 is 8.995571e+01.
T_20 is 8.944911e+01.

```

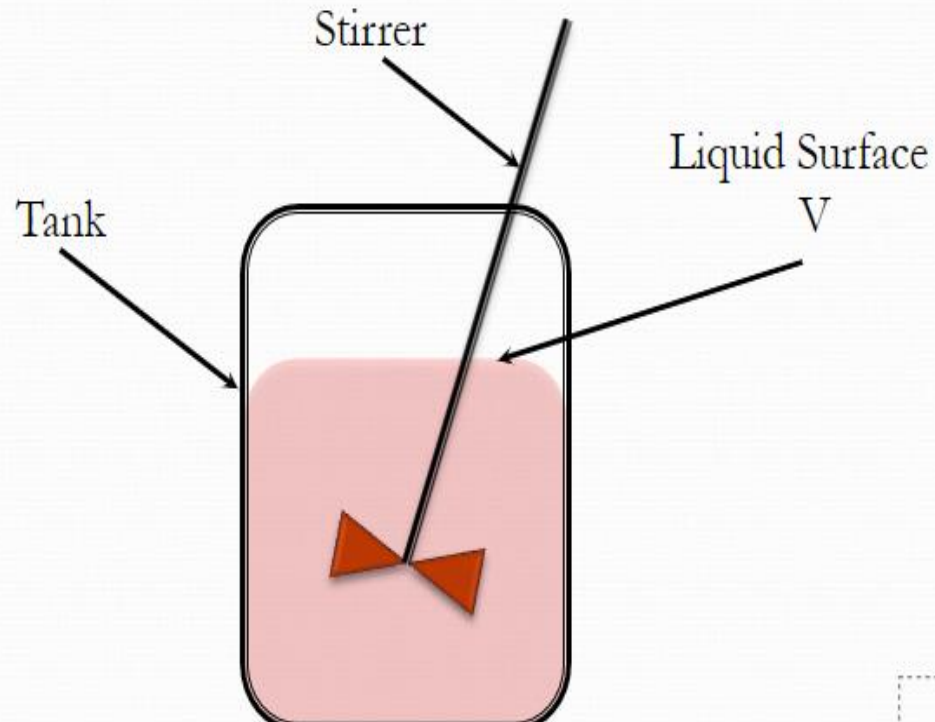

Reactors:

Batch Reactor:

Definition:

Batch Reactors are defined as reactors in which no flow of mass across the reactor boundaries, once the reactants have been charged.

Schematic Representation of Batch Reactors:



Continuous Stirred Tank Reactor (CSTR):

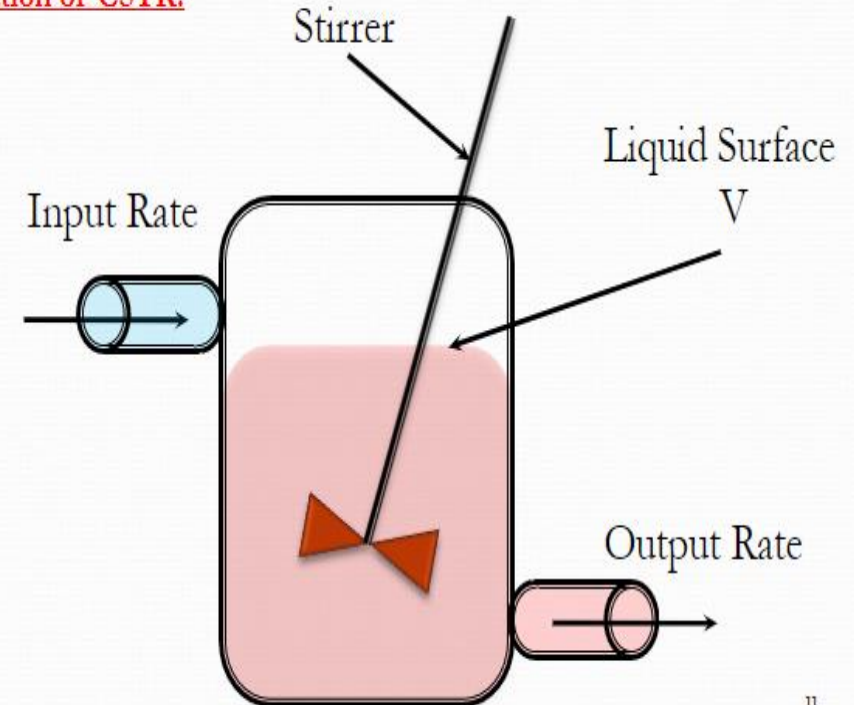
Definition:

Continuous Stirred Tank Reactors (CSTR) are defined to be flow reactors characterized by intense mixing so that the properties anywhere inside the reactor are exactly the same as that of the exit stream.

Schematic Representation of CSTR:

This model can be used to:

1. model a bed of catalyst powder, i.e. fluidized-bed reactors.
2. Slurry bubble column reactor
3. Polymerization reactors



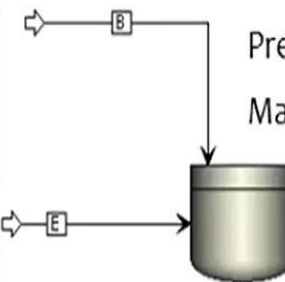
BATCH REACTOR:

Problem Description:

The specific chemistry used to illustrate the use of Aspen Plus is the reaction of ethylene (E) with benzene (B) to form ethylbenzene (EB)



Feed Condition (SI units)	Ethylene	Benzene
Temp. (K)	298	300
Pressure (atm)	15	15
Molar Flow(kmole/hr)	50	100



Reactor Spec.

Batch feed time: 1 hour

Pressure: 10 atm

Max Calculation time: 2 hrs

Rate of reaction

$$-r_A = C_E C_B (1.528 \times 10^8) e^{\frac{(-7.1129 \times 10^7)}{RT}}$$

Fluid Package

CHAO-SEA

Specific Reaction Rate Constant

$$K = K_0 \exp(-E_a/RT)$$

$$K_0 = 1.528 \times 10^8 \text{ kmol/s.m}^3$$

$$E_a = 7.1129 \times 10^7 \text{ J/kmol}$$

OBJECTIVES:

- ANALYZE: The concentration of reactants and products as a function of time.
- PLOT: The temperature profile

SOLUTION STEPS:

Components - Specifications

Select components

Component ID	Type	Component name	Alias
BENZENE	Conventional	BENZENE	C6H6
ETHYLENE	Conventional	ETHYLENE	C2H4
EB	Conventional	ETHYLBENZENE	CBH10-4

Find Elec Wizard SFE Assistant User Defined Reorder Review

Methods - Specifications

Property methods & options

Method filter: COMMON

Base method: CHAO-SEA

Henry components

Petroleum calculation options

Free-water method: STEAM-TA

Water solubility: 3

Electrolyte calculation options

Chemistry ID

☒ Use true components

Method name: CHAO-SEA

Methods Assistant...

Modify

Vapor EOS: ESRK

Data set: 1

Liquid gamma: GMDKH

Data set: 1

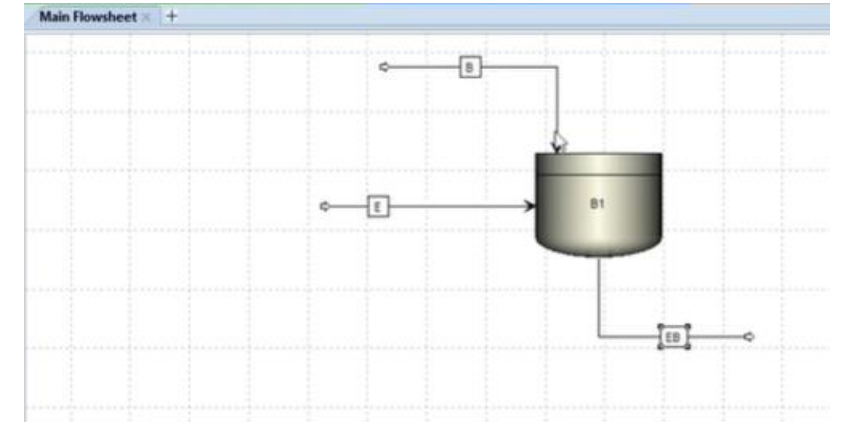
Liquid molar enthalpy: HLMX13

Liquid molar volume: VLMX20

☐ Heat of mixing

☐ Poynting correction

☐ Use liquid reference state enthalpy



Main Flowsheet - B (MATERIAL) - Input

Specifications

Flash Type: Temperature Pressure

State variables

Temperature: 300 K

Pressure: 15 atm

Vapor fraction

Total flow basis: Mole

Total flow rate: 100 kmol/hr

Solvent

Reference Temperature

Volume flow reference temperature

Component concentration reference temperature

Composition

Mole-Frac

Component	Value
BENZENE	1
ETHYLENE	
EB	

Main Flowsheet - E (MATERIAL) - Input

Specifications

Flash Type: Temperature Pressure

State variables

Temperature: 298 K

Pressure: 15 atm

Vapor fraction

Total flow basis: Mole

Total flow rate: 50 kmol/hr

Solvent

Reference Temperature

Volume flow reference temperature

Component concentration reference temperature

Composition

Mole-Frac

Component	Value
BENZENE	
ETHYLENE	1
EB	

Main Flowsheet - B1 (RBatch) - Setup

Specifications

Reactor operating specification

Temperature profile

Time	Temperature
min	K
0	300
10	400
20	430

Pressure specification

Specify reactor pressure

Reactor pressure: 10 atm

Catalyst loading: 0 kg

Valid phases

Reactor: Liquid-Only

Vent accumulator: Vapor-Only

2nd Liquid

Main Flowsheet × B1 (RBatch) - Setup × +

Specifications Kinetics Stop Criteria **Operation Times** Continuous Feeds Controllers PSD Co

Stop criteria

Criterion no.		1	
Location	Reactor		
Variable type	Time		
Stop value		2	
Unit	hr		
Component			
Substream			
Property set ID			
Approach from			

owsheet × B1 (RBatch) - Setup × +

Specifications Kinetics Stop Criteria Operation Times Continuous Feeds Controllers PSD Comments

Reaction set(s) to be included in the model

Available reaction sets

Selected reaction sets

Enter Type

POWERLAW

OK Cancel

activity

name

value

Flowsheet × R-1 (POWERLAW) × +

Stoichiometry Kinetic Equilibrium Activity Comments

Edit Reaction

Reaction No. 1 Reaction type Kinetic

Reactants	Component	Coefficient	Exponent
BENZENE		-1	1
ETHYLENE		-1	1

Products	Component	Coefficient	Exponent
EB		1	

Close

Main Flowsheet × B1 (RBatch) - Setup × +

Specifications Kinetics Stop Criteria **Operation Times** Continuous Feeds Controllers PSD Comments

Batch cycle time

Total cycle time

Batch feed time 1 hr

Down time 0 hr

Profile result time

Maximum calculation time 2 hr

Time interval between profile points 10 sec

Maximum number of profile points 722

Main Flowsheet × R-1 (POWERLAW) × +

Stoichiometry Kinetic Equilibrium Activity Comments

1) BENZENE + ETHYLENE --> EB(MIXED)

Reacting phase Liquid Rate basis Reac (vol)

Power Law kinetic expression

If To is specified Kinetic factor $= k(T/T_o)^n e^{-(E/R)(1/T-1/T_o)}$

If To is not specified Kinetic factor $= kT^n e^{-E/RT}$

k 1.528e+08

n 0

E 7.1129e+07 J/kmol

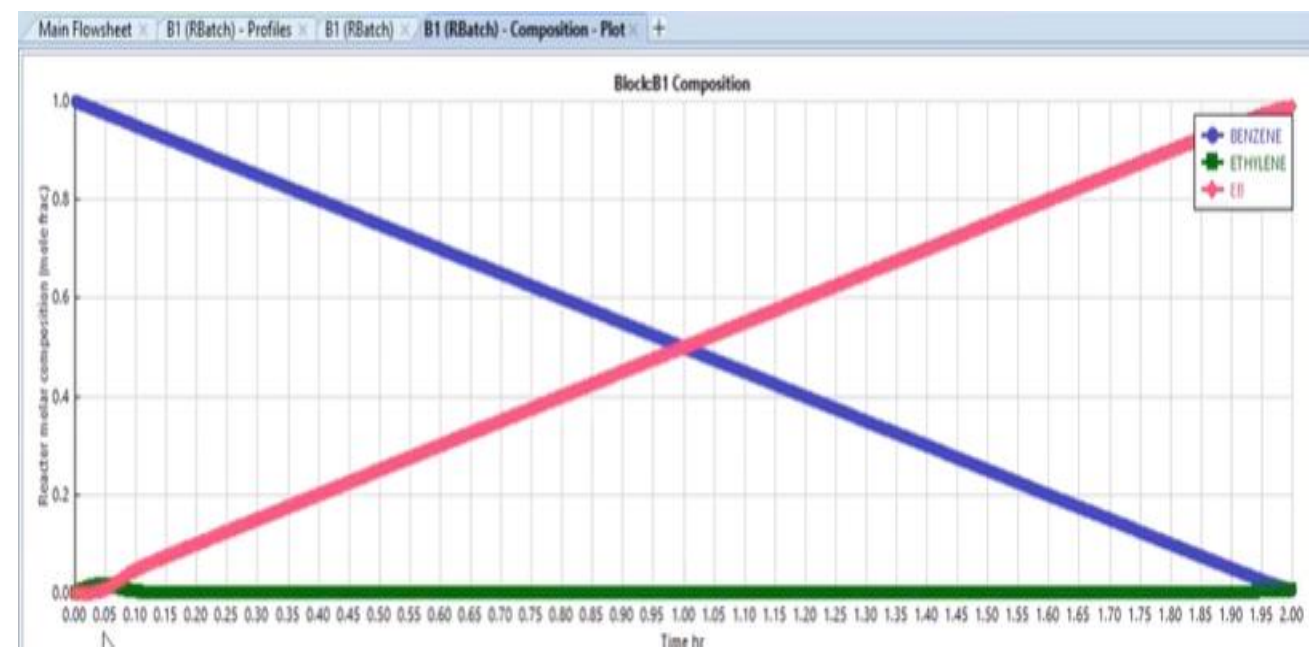
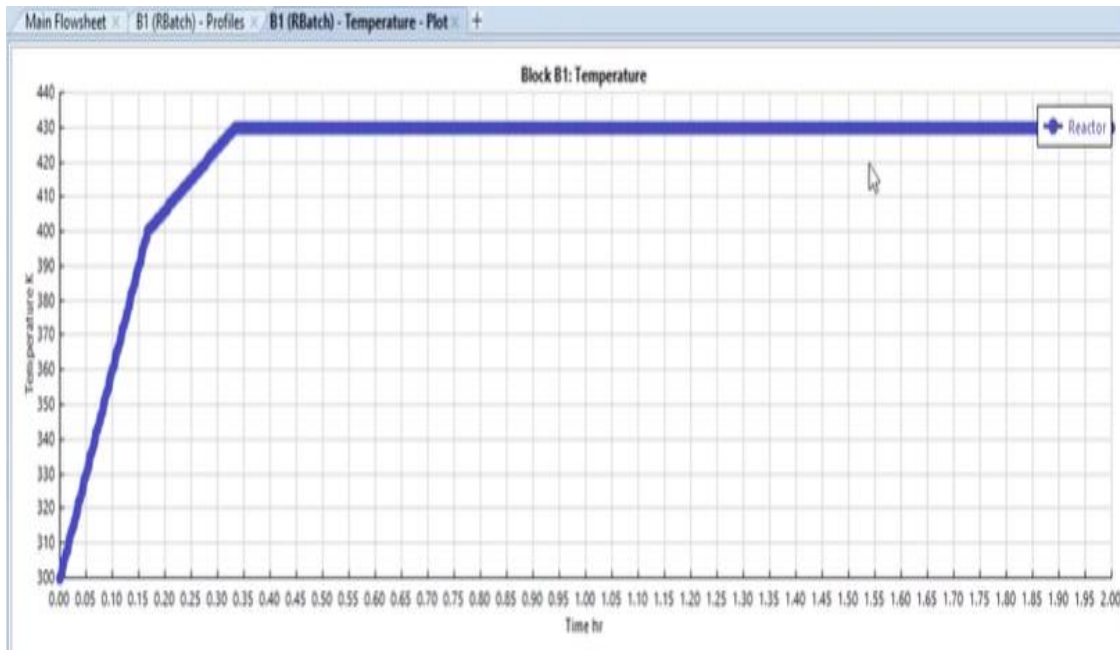
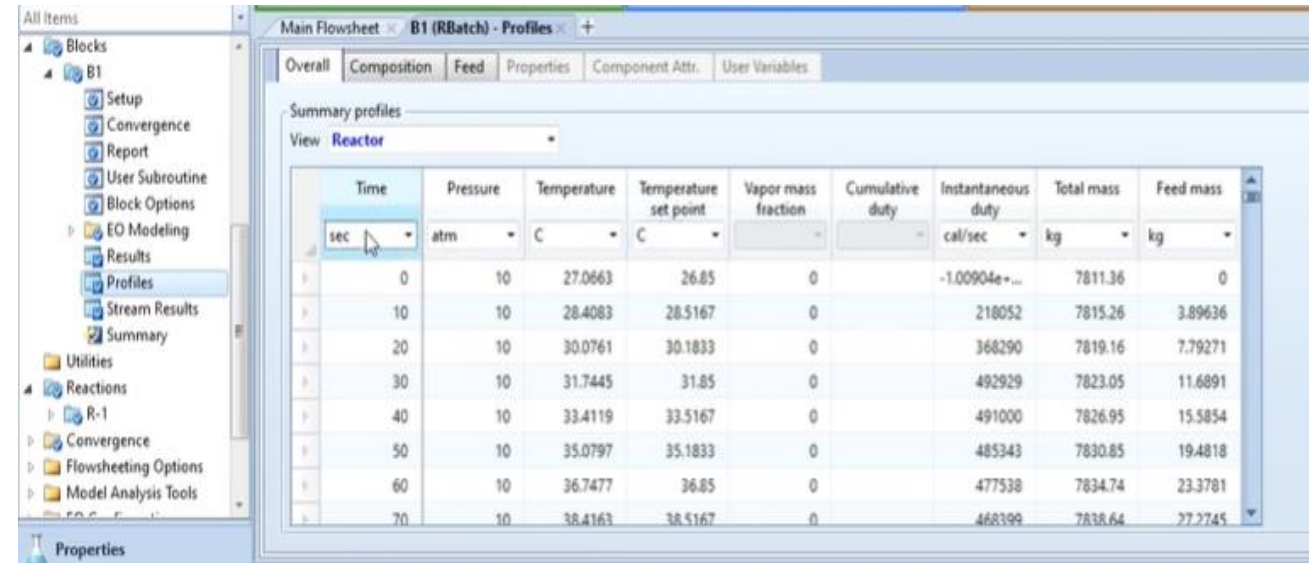
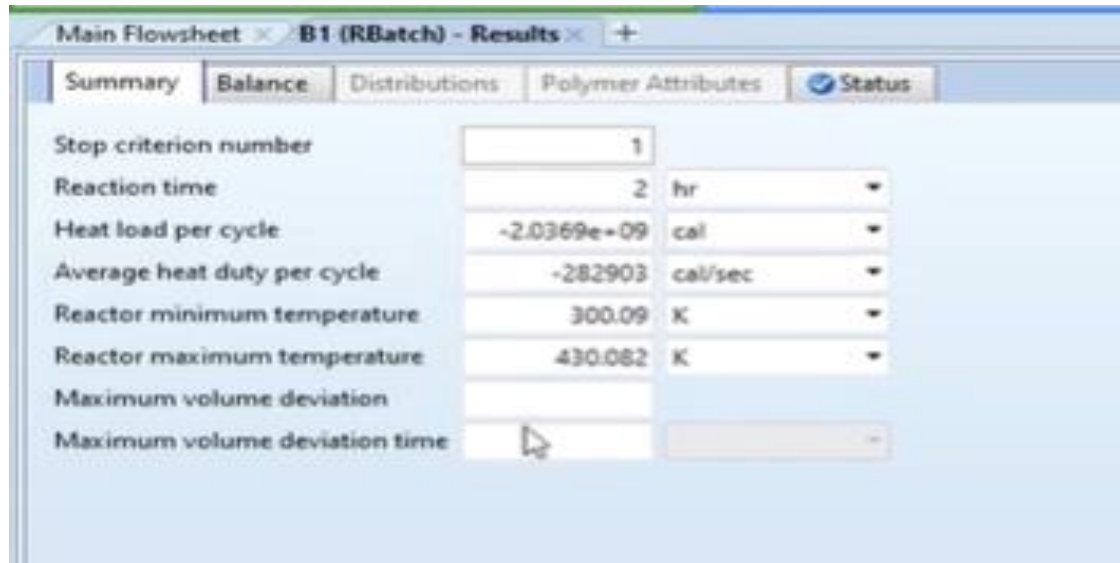
To K

[Ci] basis Molarity

Edit Reactions

Solids

RESULTS AND ANALYSIS:



CSTR REACTOR:

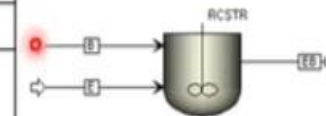
Case. RCSTR Reactor Design

Problem Description:

- The specific chemistry used to illustrate the use of Aspen Plus is the reaction of ethylene (E) with benzene (B) to form ethylbenzene (EB)



Feed Condition (SI units)	Ethylene	Benzene
Temp. (K)	298	300
Pressure (atm)	15	15
Molar Flow(kmole/hr)	50	100



Reactor Spec.

Reactor Temp 400K

Pressure: 10 atm

Reactor Volume 0.1 cum

Rate of reaction

$$-r_A = C_E C_B (1.528 \times 10^8) e^{\frac{(-7.1129 \times 10^7)}{RT}}$$

Fluid Package

CHAO-SEA

Specific Reaction Rate Constant

$$K = K_0 \exp(-E_a/RT)$$

$$K_0 = 1.528 \times 10^8 \text{ kmol/s.m}^3$$

$$E_a = 7.1129 \times 10^7 \text{ J/kmol}$$

OBJECTIVES:

- ANALYZE: as Using Design specs to analyze the volume of the reactor for 98% ethylene conversion.
- CALCULATE: The conversion of ethylene for given reaction kinetics.

SOLUTION STEPS:

Components - Specifications

Component ID	Type	Component name	Alias
B	Conventional	BENZENE	C6H6
EB	Conventional	ETHYLBENZENE	C8H10-4
E	Conventional	ETHYLENE	C2H4

Methods

Property methods & options

Method filter: COMMON

Base method: CHAO-SEA

Method name: CHAO-SEA

Method Assistant...

Model Palette

Reactors: RCSTR

Simulation

Main Flowsheet > E (MATERIAL) > Reactions

Create New ID

Enter ID: R-1

Select Type: POWERLAW

Reaction R-1 (POWERLAW) - Input

Stoichiometry: Kinetic

Reaction type: Kinetic

Reactants:

Component	Coefficient	Exponent
B	-1	1
E	-1	1

Products:

Component	Coefficient	Exponent
EB	1	1

Power Law kinetic expression

Reacting phase: Liquid

Rate basis: Reac (vol)

If To is specified: Kinetic factor = $k(T/T_o)^n e^{-(E/R)[1/T-1/T_o]}$

If To is not specified: Kinetic factor = $kT^n e^{-E/RT}$

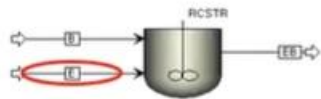
k: 1.528e+08

n: 0

E: 7.1129e+07 J/kmol

To: C

[C] basis: Molarity



Main Flowsheet > E (MATERIAL) > Specifications

Flash Type: Temperature Pressure Composition

State variables

Temperature: 298 K

Pressure: 15 atm

Vapor fraction:

Total flow basis: Mole

Total flow rate: 50 kmol/hr

Solvent:

Reference Temperature

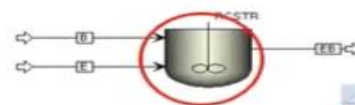
Volume flow reference temperature: C

Component concentration reference temperature: C

Component

Value

Total: 1



Main Flowsheet > E (MATERIAL) > R-1 (POWERLAW) > Control Panel > B (MATERIAL) > Specifications

Operating conditions

Pressure: 10 atm

Temperature: 400 K

Duty: cal/sec

Vapor fraction:

Holdup

Valid phases: Liquid-Only

Specification type: Reactor volume

Reactor

Volume: 0.1 cum

Phase:

Res. time: hr

Volume: l

Volume frac:

Residence time: hr

Simulation

Capital: USD Utilities: USD/Year Energy Savings: MW Exchangers - Unknown

Main Flowsheet > RCSTR (RCSTR) - Stream Results (Default) > RCSTR (RCSTR) > Design Specs

New Copy Paste Export Edit Input View Results Reconcile Reveal

Hide Active Status Description

Create New ID

Enter ID: DS-1

OK Cancel

Blocks

RCSTR

Setup

Convergence

User Subroutine

Dynamic

Block Options

EO Modeling

Results

Stream Results

Summary

Utilities

Reactions

R-1

Input

Results

EO Variables

Convergence

Flowsheeting Options

Design Specs

Calculator

Transfer

Stream Library

Define Spec Vary Fortran Declarations EO Options Comments

Active

Sampled variables (drag and drop variables from form to the grid below)

Variable Definition

New Delete Copy Paste

Selected variable

Variable Reference

Category Type

Create new variable

Enter variable name: EIN

OK Cancel

Reactions

EO input

Open variable

Description

Main Flowsheet > RCSTR (RCSTR) - Stream Results (Default) > RCSTR (RCSTR) > DS-1

Define Spec Vary Fortran Declarations EO Options Comments

Active

Sampled variables (drag and drop variables from form to the grid below)

Variable Definition

EIN Mole-Flow Stream = E Substream = MIXED Component = E Units = kmol/hr

New Delete Copy Paste Move Up Move Down View Variables

Edit selected variable

Variable EIN

Category All

Type Mole-Flow

Stream E

Substream MIXED

Component E

Units kmol/hr

Model Utility

Property Parameters

Reactions

Main Flowsheet x RCSTR (RCSTR) - Stream Results (Default) x RCSTR (RCSTR) x DS-1 x +

Define Spec Vary Fortran Declarations EO Options Comments

☒ Active

Sampled variables (drag and drop variables from form to the grid below)

Variable	Definition
EIN	Mole-Flow Stream=E Substream=MIXED Components=E Units=kmol/hr
EOUT	Mole-Flow Stream=EB Substream=MIXED Component=E Units=kmol/hr

New Delete Copy Paste Move Up Move Down View Variables

Edit selected variable

Variable: **EOUT**

Category:

- ☐ All
- ☐ Blocks
- ☒ Streams
- ☐ Model Utility
- ☐ Property Parameters
- ☐ Reactions

Reference:

Type: **Mole-Flow**

Stream: **EB**

Substream: **MIXED**

Component: **E**

Units: **kmol/hr**

Main Flowsheet x RCSTR (RCSTR) - Stream Results (Default) x RCSTR (RCSTR) x DS-1 x +

Define Spec Vary Fortran Declarations EO Options Comments

Design specification expressions

Spec: **(EIN-EOUT)/EIN**

Target: **0.98**

Tolerance: **0.001**

Main Flowsheet x RCSTR (RCSTR) - Stream Results (Default) x RCSTR (RCSTR) x DS-1 x +

Define Spec Vary Fortran Declarations EO Options Comments

Manipulated variable

Type: **Block-Var**

Block: **RCSTR**

Variable: **VOL**

Sentence: **PARAM**

Units: **cum**

Manipulated variable limits

Lower: **0.1**

Upper: **2**

Step size: **0.1**

Maximum step size:

Report labels

Line 1 Line 2 Line 3 Line 4

EO input

Open variable:

Description:

Copy Paste Clear

RESULTS AND ANALYSIS:

Material	Heat	Load	Work	Vol.% Curves	Wt.% Curves	Petroleum	Polymers	Solids
Mass Vapor Fraction								
Mass Liquid Fraction								
Mass Solid Fraction								
Molar Enthalpy								
Mass Enthalpy								
Molar Entropy								
Mass Entropy								
Molar Density								
Mass Density								
Enthalpy Flow								
Average MW								
Mole Flows								
BENZENE								
ETHYLENE								
ETHYL-01								
Mole Fractions								
Mass Flows								
Mass Fractions								
Volume Flow								

Main Flowsheet x DS-1 x Control Panel x DS-1 - Results x +

Results ☒ Status

Variable	Initial value	Final value	Units
MANIPULATED	100	511.634	L
EIN	50	50	KMOL/HR
EOUT	4.45344	0.976424	KMOL/HR

Sensitivity analysis in Aspen:

Sensitivity analysis in Aspen is a technique used to assess how changes in input variables affect the outputs of a model. It helps in understanding the sensitivity of a process or system, optimizing decisions, and evaluating risks. The process involves defining the objective, selecting input variables, specifying variable ranges, creating the Aspen model, running the sensitivity analysis, analyzing the results, interpreting the findings, and refining the analysis if necessary. It's a valuable tool for making informed decisions and improving process performance.



Thank you