About sensitivity analysis (MCA)

I have based my thoughts on http://www.math.uwaterloo.ca/bingalls/MMSB/Notes.pdf.

In MCA (Metabolic control analysis) the sensitivity of reaction is observed through two coefficients: concentration control coefficient,

$$C_{e_j}^{S_i} = \frac{e_j}{S_i} \frac{dS_i}{de_j},$$

where S_i is the steady state concentration of species i, and e_j is the concentration of enzyme j. Flux control coefficients are defined by

$$C_{e_j}^{J_k} = \frac{e_j}{J_k} \frac{dJ_k}{de_j},$$

where J_k is the flux through reaction k (i.e. the steady-state reaction rate k).

In this case we need to take the enzyme concentrations into account as can be seen from above formulas. We can build onto our existing very simple model and add enzyme concentrations to every reaction rate and assume the enzyme reaction occurs instantaneously compared to our time scale. (Then we'll have $k_i e_i [some\ other\ concentrations]$.)

Now to obtain the steady state concentrations of our species in the reaction we need to set the differential equations to zero. I used notation that puts a as a first concentration, b as the second and so on, until the second last is g and then p for propane. The obtained concentrations are as follows. Notice that e_i for multiple i are not the same than e(t).

$$b(t) = \frac{k_1 e_1 a^2}{k_2 [NADPH]} \tag{1}$$

$$c(t) = \frac{k_2 e_2 b(t) [NADPH]}{k_3 e_3} \tag{2}$$

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$$d(t) = \frac{k_3 e_3 c(t)}{k_4 e_4 [NADH]}$$
(2)

$$e(t) = \frac{k_4 e_4 d(t)[NADH]}{k_5 e_5 [H2O]}$$
(4)

$$f(t) = \frac{k_5 e_5 e(t)[H2O]}{k_6 e_6 [ATP][H2O][NADPH]}$$
 (5)

$$g(t) = \frac{k_6 e_6 f(t) [ATP] [H2O] [NADPH]}{k_7 e_7 [H]^2 [O2] [NADPH]^2}$$
(6)

Also, if we add a rate to propone to go away with parameter k_8 , we get further from the last differential equation:

$$p(t) = \frac{k_7 e_7 g(t) [H]^2 [O2] [NADPH]^2}{k_8}.$$

Thus, all the steady state concentrations depend on the concentration of the first species, a, which we assume constant.

The problem in this approach are fluxes. In the notes there wasn't any formal definition of that, it was just said that it is the reaction rate.

If we calculate the fluxes with steady-state reaction rates, all the coefficients $C_{e_j}^{J_k}$ lead to one since $\frac{e_j}{S_i}$ equals $1/\frac{dS_i}{de_j}$. This can not be right since according to summation theory, all the flux control coefficients should sum to one.

Another approach we tried was stoichiometric analysis. There we form matrix N so, that i, j-th component corresponds to the number of molecules of species i involved in reaction j. Now if we arrange the reaction rates as a column vector \mathbf{v} , then for the steady state holds $N\mathbf{v} = 0$. (This comes from the formula

$$\frac{d}{dt}s(t) = N\mathbf{v}.$$

However, the problem in this approach is that our matrix N is bad, and the only solution is $\mathbf{v} = \mathbf{0}$.

The conclusion is that the sensitivity analysis based on our knowledge and these simplified reactions is hard. We need either measured data, or some more information of our reactions.