

# SSSRA — Variable Reference

Stacked Solar-Shade Radiator Architecture

Aaron Smith — Independent Systems Architect · February 2026

Complete definition of all variables and terms used in the thermal math framework of the Stacked Solar-Shade Radiator Architecture document. All values correspond to the nominal parameters and ranges specified in Sections 4–5 of the architecture reference document.

## Radiator Surface Properties

Symbol	Name	Definition	Nominal
$\epsilon_{\text{rad}}$	Radiator surface emissivity	Fraction of blackbody radiation emitted by the radiator coating. Clean: 0.85–0.92; degraded (21-day dust): 0.70–0.80.	0.88 (clean) 0.75 (degraded)
$\alpha_s$	Radiator solar absorptance	Fraction of incident solar flux absorbed by the radiator surface. Drives parasitic heating. Clean white coatings (AZ-93, Z-93P): 0.09–0.15; dust-degraded: 0.20–0.30.	0.12 (clean) 0.25 (degraded)
$T_{\text{rad}}$	Radiator operating temperature	Bulk temperature of the radiator panel surface during active thermal rejection. Set by the fluid loop outlet temperature.	310 K (300–320 K)
$A$	Radiator area	Total projected radiating area of the horizontal flat-plate radiator ( $\text{m}^2$ ). Sized to meet the heat rejection requirement at degraded end-of-mission conditions.	Mission-dependent

## Solar Environment

Symbol	Name	Definition	Nominal
$S$	Solar constant at 1 AU	Irradiance of the Sun at Earth–Moon distance. Provides the baseline solar flux incident on any exposed surface.	1,361 $\text{W}/\text{m}^2$
$\alpha$	Solar elevation angle	Angle of the Sun above the local horizon. At the lunar south pole, typically 1.5–15°. Determines the projected solar flux on a horizontal surface via $\sin(\alpha)$ .	6° nominal (1.5–15°)

## Fundamental Constants

Symbol	Name	Definition	Nominal
$\sigma$	Stefan-Boltzmann constant	Proportionality constant in the Stefan-Boltzmann law governing radiative heat transfer between surfaces.	$5.67 \times 10^{-8}$ $\text{W}/\text{m}^2\text{K}^4$
$T_{\text{sink}}$	Effective sink temperature	Equivalent blackbody temperature of the thermal environment seen by the radiator. Deep space provides ~4 K; contributes negligibly to the radiation balance.	~4 K

## Solar Array / Shade Tier Properties

Symbol	Name	Definition	Nominal
$\epsilon_{\text{back}}$	Array backside emissivity	Emissivity of the solar array's downward-facing surface. Uncoated: 0.75–0.85. With vacuum-deposited aluminum or gold low- $\epsilon$ coating: 0.05–0.20. Key enabler of the architecture.	0.10 (low- $\epsilon$ ) 0.82 (uncoated)
$T_{\text{array}}$	Array backside temperature	Temperature of the solar panel's underside during sunlit operation. Tracks with front-face temperature; depends on cell efficiency, substrate, and thermal coupling.	330 K (320–370 K)
$F_{\text{array}}$	View factor, radiator to array	Fraction of the radiator's upward hemisphere occupied by the solar array underside. Depends on clearance gap, panel sizing, and edge geometry.	0.30 (0.20–0.40)

## Derived Geometric Terms

Symbol	Name	Definition	Nominal
$F_{\text{space,eff}}$	Effective view factor to space	Remaining fraction of the radiator's upward hemisphere that sees deep space after the array occupies $F_{\text{array}}$ . Defined as $1 - F_{\text{array}}$ .	0.70 (0.60–0.80)

## Heat Flux & Performance Terms

Symbol	Name	Definition	Nominal
$Q_{\text{rad}}$	Gross radiative rejection	Total heat radiated by the radiator to its thermal environment before accounting for solar absorption. Governed by Stefan-Boltzmann law.	W
$Q_{\text{solar}}$	Solar parasitic load	Solar flux absorbed by the radiator surface. The primary thermal penalty eliminated by the shade configuration.	W
$q_{\text{solar}}$	Projected solar flux on horizontal surface	Solar irradiance incident on a horizontal surface at elevation angle $\alpha$ . Equal to $S \times \sin(\alpha)$ .	W/m <sup>2</sup>
$q_{\text{abs}}$	Absorbed solar flux	Net solar power absorbed per unit area: $\alpha_s \times S \times \sin(\alpha)$ . Represents the parasitic load on an unshaded radiator.	W/m <sup>2</sup>
$q_{\text{back}}$	IR backradiation from array	Infrared flux radiated downward from the array underside onto the radiator. Equal to $F_{\text{array}} \times \epsilon_{\text{back}} \times \sigma \times T_{\text{array}}^4$ .	W/m <sup>2</sup>
$q_{\text{net,unshaded}}$	Net rejection capacity (unshaded)	Heat rejection per unit area for a radiator with no shade, after subtracting solar absorption.	W/m <sup>2</sup>
$q_{\text{net,shaded}}$	Net rejection capacity (shaded)	Heat rejection per unit area for the stacked configuration, accounting for reduced view to space and IR backradiation.	W/m <sup>2</sup>
$q_{\text{net,benefit}}$	Net shade benefit	Difference in rejection performance: solar flux eliminated minus IR backradiation penalty minus view factor loss. Positive = shade improves performance.	W/m <sup>2</sup>

## Key Equations

Projected solar flux on horizontal surface

$$q_{\text{solar}} = S \times \sin(\alpha)$$

Solar parasitic absorbed by radiator

$$q_{abs} = \alpha_s \times S \times \sin(\alpha)$$

Gross radiative rejection (unshaded)

$$Q_{rad} = \epsilon_{rad} \times \sigma \times A \times (T_{rad}^4 - T_{sink}^4)$$

Net rejection per unit area (unshaded)

$$q_{net,unshaded} = \epsilon_{rad} \times \sigma \times (T_{rad}^4 - T_{sink}^4) - \alpha_s \times S \times \sin(\alpha)$$

IR backradiation from array underside

$$q_{back} = F_{array} \times \epsilon_{back} \times \sigma \times T_{array}^4$$

Effective view factor to space

$$F_{space,eff} = 1 - F_{array}$$

Net rejection per unit area (shaded)

$$q_{net,shaded} = \epsilon_{rad} \times \sigma \times T_{rad}^4 \times F_{space,eff} - q_{back}$$

Net shade benefit

$$q_{net,benefit} = q_{solar,eliminated} - q_{IR,backrad} - q_{view\ factor\ loss}$$