

SSSRA — Variable Reference

Stacked Solar-Shade Radiator Architecture

Aaron Smith — Independent Systems Architect · February 2026

Complete definition of all variables and terms used in the thermal math framework of the Stacked Solar-Shade Radiator Architecture document. All values correspond to the nominal parameters and ranges specified in Sections 4–5 of the architecture reference document.

Radiator Surface Properties

| Symbol | Name | Definition | Nominal |
|-------------------------|--------------------------------|---|---------------------------------|
| ϵ_{rad} | Radiator surface emissivity | Fraction of blackbody radiation emitted by the radiator coating. Clean: 0.85–0.92; degraded (21-day dust): 0.70–0.80. | 0.88 (clean) 0.75 (degraded) |
| α_{s} | Radiator solar absorptance | Fraction of incident solar flux absorbed by the radiator surface. Drives parasitic heating. Clean white coatings (AZ-93, Z-93P): 0.09–0.15; dust-degraded: 0.20–0.30. | 0.12 (clean) 0.25 (degraded) |
| T_{rad} | Radiator operating temperature | Bulk temperature of the radiator panel surface during active thermal rejection. Set by the fluid loop outlet temperature. | 310 K (300–320 K) |
| A | Radiator area | Total projected radiating area of the horizontal flat-plate radiator (m ²). Sized to meet the heat rejection requirement at degraded end-of-mission conditions. | Mission-dependent |

Solar Environment

| Symbol | Name | Definition | Nominal |
|----------|------------------------|--|-------------------------|
| S | Solar constant at 1 AU | Irradiance of the Sun at Earth–Moon distance. Provides the baseline solar flux incident on any exposed surface. | 1,361 W/m ² |
| α | Solar elevation angle | Angle of the Sun above the local horizon. At the lunar south pole, typically 1.5–15°. Determines the projected solar flux on a horizontal surface via $\sin(\alpha)$. | 6° nominal (1.5–15°) |

Fundamental Constants

| Symbol | Name | Definition | Nominal |
|-------------------|----------------------------|--|---|
| σ | Stefan-Boltzmann constant | Proportionality constant in the Stefan-Boltzmann law governing radiative heat transfer between surfaces. | $5.67 \times 10^{-8} \text{ W/m}^2\text{K}^4$ |
| T_{sink} | Effective sink temperature | Equivalent blackbody temperature of the thermal environment seen by the radiator. Deep space provides ~4 K; contributes negligibly to the radiation balance. | ~4 K |

Solar Array / Shade Tier Properties

| Symbol | Name | Definition | Nominal |
|--------------------------|--------------------------------|---|--|
| ϵ_{back} | Array backside emissivity | Emissivity of the solar array's downward-facing surface. Uncoated: 0.75–0.85. With vacuum-deposited aluminum or gold low- ϵ coating: 0.05–0.20. Key enabler of the architecture. | 0.10 (low- ϵ) 0.82 (uncoated) |
| T_{array} | Array backside temperature | Temperature of the solar panel's underside during sunlit operation. Tracks with front-face temperature; depends on cell efficiency, substrate, and thermal coupling. | 330 K (320–370 K) |
| F_{array} | View factor, radiator to array | Fraction of the radiator's upward hemisphere occupied by the solar array underside. Depends on clearance gap, panel sizing, and edge geometry. | 0.30 (0.20–0.40) |

Derived Geometric Terms

| Symbol | Name | Definition | Nominal |
|------------------------|--------------------------------|---|---------------------|
| $F_{\text{space,eff}}$ | Effective view factor to space | Remaining fraction of the radiator's upward hemisphere that sees deep space after the array occupies F_{array} . Defined as $1 - F_{\text{array}}$. | 0.70 (0.60–0.80) |

Heat Flux & Performance Terms

| Symbol | Name | Definition | Nominal |
|---------------------------|--|---|------------------|
| Q_{rad} | Gross radiative rejection | Total heat radiated by the radiator to its thermal environment before accounting for solar absorption. Governed by Stefan-Boltzmann law. | W |
| Q_{solar} | Solar parasitic load | Solar flux absorbed by the radiator surface. The primary thermal penalty eliminated by the shade configuration. | W |
| q_{solar} | Projected solar flux on horizontal surface | Solar irradiance incident on a horizontal surface at elevation angle α . Equal to $S \times \sin(\alpha)$. | W/m ² |
| q_{abs} | Absorbed solar flux | Net solar power absorbed per unit area: $\alpha_s \times S \times \sin(\alpha)$. Represents the parasitic load on an unshaded radiator. | W/m ² |
| q_{back} | IR backradiation from array | Infrared flux radiated downward from the array underside onto the radiator. Equal to $F_{\text{array}} \times \epsilon_{\text{back}} \times \sigma \times T_{\text{array}}^4$. | W/m ² |
| $q_{\text{net,unshaded}}$ | Net rejection capacity (unshaded) | Heat rejection per unit area for a radiator with no shade, after subtracting solar absorption. | W/m ² |
| $q_{\text{net,shaded}}$ | Net rejection capacity (shaded) | Heat rejection per unit area for the stacked configuration, accounting for reduced view to space and IR backradiation. | W/m ² |
| $q_{\text{net,benefit}}$ | Net shade benefit | Difference in rejection performance: solar flux eliminated minus IR backradiation penalty minus view factor loss. Positive = shade improves performance. | W/m ² |

Key Equations

Projected solar flux on horizontal surface

$$q_{\text{solar}} = S \times \sin(\alpha)$$

Solar parasitic absorbed by radiator

$$q_{\text{abs}} = \alpha_s \times S \times \sin(\alpha)$$

Gross radiative rejection (unshaded)

$$Q_{\text{rad}} = \epsilon_{\text{rad}} \times \sigma \times A \times (T_{\text{rad}}^4 - T_{\text{sink}}^4)$$

Net rejection per unit area (unshaded)

$$q_{\text{net,unshaded}} = \epsilon_{\text{rad}} \times \sigma \times (T_{\text{rad}}^4 - T_{\text{sink}}^4) - \alpha_s \times S \times \sin(\alpha)$$

IR backradiation from array underside

$$q_{\text{back}} = F_{\text{array}} \times \epsilon_{\text{back}} \times \sigma \times T_{\text{array}}^4$$

Effective view factor to space

$$F_{\text{space,eff}} = 1 - F_{\text{array}}$$

Net rejection per unit area (shaded)

$$q_{\text{net,shaded}} = \epsilon_{\text{rad}} \times \sigma \times T_{\text{rad}}^4 \times F_{\text{space,eff}} - q_{\text{back}}$$

Net shade benefit

$$q_{\text{net,benefit}} = q_{\text{solar,eliminated}} - q_{\text{IR,backrad}} - q_{\text{view factor loss}}$$