1

CH: CHEMICAL ENGINEERING

EE25BTECH11042 - Nipun Dasari

c) $3\hat{i} + 4\hat{j}$

c) rank of A<n

d) A is an identity matrix

c) 1

3) The system of linear equations Ax = 0, where textbfA is an nxn matrix, has a non-trivial solution

4) A dehumidifier (shown below) is used to completely remove water vapour from air

Dehumidifier

d) $3\hat{i} + 4\hat{j}$

d) $\sqrt{2}$

(GATE CH 2009)

(GATE CH 2009)

(GATE CH 2009)

1) The direction of largest increase of the function $xy^3 - x^2$ the point (1, 1) is -

b) $3\hat{i} + 4\hat{j}$

b) $1/\sqrt{2}$

2) The modulus of the complex number is $(1+i)/\sqrt{2}$

a) $3\hat{i} + 4\hat{j}$

a) 1/2

ONLY if-

a) rank of A>n

b) rank of A=n

		Fig. 1		
a) Water is theb) Air is the Oc) BOTH water	of the following statement ONLY tie component on the component of the component of the components.			
5) Dehydrogenati tank reactor (C	CSTR) The feed is pure	ghtarrow $H_4(g) + H_2(g)$, ethane. If the reactor exit ber of degrees of freedom	is carried out in a continu stream contains unconver	
a) 1	b) 2	c) 3	d) 4	
			(GATE	CH 2009)

		D 1 1		D \
in a closed syste		following is TRUE for i	isothermally to pressure P_2 (> I internal energy (U) and Gibbs fi	-,
a) $U_1 = U_2$, G_1 ; b) $U_1 = U_2$, G_1 ; c		c) $U_1 \ U_2, G_1 =$ d) $U_1 \ U_2, G_1 =$		
•	ulent flow conditions, to elocity (V) of the fluid a	-	(GATE CH 200 op across a packed bed varies w	,
a) V^{-1}	b) V	c) $V^{3/2}$	d) V^2	
8) For a mixing ta number (<i>Re</i>) as	nk operating in the lar	ninar regime, the power	(GATE CH 200 number varies with the Reyno	,
a) $Re^{\frac{-1}{2}}$	b) $Re^{\frac{1}{2}}$	c) Re	d) Re^-1	
a) uniform temporal by negligible concepts of significant the dynamical temporal of the prandtl number a) thermal diffus by momentum disconductive results.	erature throughout the of vection at surface of the rmal resistance within the operature gradient within the operature gradient within the operature gradient within the operature gradient within the operature of a fluid is the rational to the operation of the o	e object he object n the object io of usivity usivity sistance	(GATE CH 200 umber → O indicates (GATE CH 200	
_	e penetration theory of ent (D) of the diffusing		(GATE CH 200 transfer coefficient (k) varies w	
a) D	b) $D^{\frac{-1}{2}}$	c) $D^{\frac{1}{2}}$	d) $D^{\frac{3}{2}}$	
otherwise identical The operating b) The operating c) The concentration	cal conditions. Which O line shifts towards the line shifts away from t	NE of the following state equilibrium curve		

13) For a homogeneous reaction system, where

 C_j is the concentration of j at time t N_j is the number of moles of j at time t V is the reaction volume at time t 1 is the reaction time The rate of reaction for species j is defined as

a) $\frac{dC_j}{dt}$	b) - $\frac{dC_j}{dt}$	c) $\frac{1}{V} \frac{dN_j}{dt}$	d) $-\frac{1}{V}\frac{dN_j}{dt}$	
14) The half-life of a) 0.0231 b) 0.602 c) 1.386 d) 2.0	a first order liquid phase	reaction is 30 seconds. T	(GATE CH Then the rate constant, in mi	n ⁻¹ , is
15) For a solid cata	lyzed reaction, the Thield	e modulus is proportional	(GATE CH to	2009)
 a) \$\square\$\frac{\text{intrinsic reaction}}{\text{diffusion rat}}\$ b) \$\square\$\frac{\text{diffusion rat}}{\text{intrinsic reaction}}\$ 	n rate e e n rate	c) intrinsic: reaction rate diffusion: rate diffusion rate intrinsic: reaction rate	<u>e</u> -e	
			(GATE CH	
process (<i>T</i> > 18 a) Type J therm b) Thermistor	800°C) ?	used for the measuremen	t of temperature in a combi	ustion
	and equal and unequal and unequal	of an underdamped second	(GATE CH d order system are	2009)
		is Rs. 10.0 lakhs; the into	(GATE CH ernal rate of return is 15 pe plant is	
a) 1.8	b) 2.6	c) 3.5	d) 4.3	
19) In petroleum ref	ining operations, the proc	ess used for converting par	(GATE CH affins and naphthenes to aror	
a) catalytic reformsb) catalytic crac	•	c) hydrocrackingd) alkylation		
20) The active comp	ponent of catalysts used	in steam reforming of me	(GATE CH chane to produce synthesis g	
a) Nickel	b) Iron	c) Platinum	d) Palladium	
21) The value of the	e limit		(GATE CH	2009)

 $\lim_{x \to \pi/2} \frac{\cos x}{(x - \pi/2)^3}$

	a) −∞	b) 0	c) 1	d) ∞		
				(GATE CH 2009)		
22)	The general solution of	f the differential equation				
		$\frac{d^2y}{dx^2} - \frac{a}{a}$	$\frac{dy}{dx} - 6y = 0$			
	, with C_1 and as const	tants of integration, is				
	a) $C_1e^-3x + C_2e^-2x$ b) $C_1e^3x + C_2e^-2x$		c) $C_1e^3x + C_2e^2x$ d) $C_1e^-3x + C_2e^2x$			
23)	Using the residue theor	rem, the value of integral	(counterclockwise)	(GATE CH 2009)		
		$\oint \frac{8}{3}$	$\frac{-7z}{z-4} dz$			
	around a circle with ce	entre at z=0 and radius=8	(where z is a complex r	number and $i = \sqrt{-1}$, is		
	a) -20π	b) -40π	c) -40πi	d) 40πi		
24)	(GATE CH 2009) 24) Consider the integral ∫∫ (2xi - 2yj + 5zk). n dS over the surface of a sphere of radius = 3 with center at the origin and surface unit normal n pointing away from the origin. Using the Gauss divergence theorem, the value of the integral is					
	a) -180π	b) 0	c) 90π	d) 180π		
(GATE CH 2009) 25) Using the trapezoidal rule and 4 equal intervals $(n = 4)$, the calculated value of the integral (rounded to the first $\left(\int_0^{\pi} sin\theta d\theta\right)$ is						
	a) 1.7	b) 1.9	c) 2.0	d) 2.1		
				(GATE CH 2009)		
26)	The eigenvalues of mat					
			$\begin{pmatrix} 1 & 2 \\ 5 & 3 \end{pmatrix}$	(1)		
	are 5 and -1. Then the	eigenvalues of $-2\mathbf{A} + 3\mathbf{I}$	(If is 2x2 identity matrix)) are		
	a) -7 and 5	b) 7 and -5	c) -1/7 and 1/5	d) 1/7 and - 1/5		
27)	the event of obtaining is TRUE ?	an odd number. Then wh	ich ONE of the followin	(GATE CH 2009) a or equal to 5 and S denote g about the probability (P)		
	a) $P(R/S) = 1$	b) $P(R/S) = 0$	c) $P(S/R) = 1$	d) P(S/R) = 0		

28) Pure water (*streamW*) is to be obtained from a feed containing 5 wt per cent salt using a desalination unit as shown below

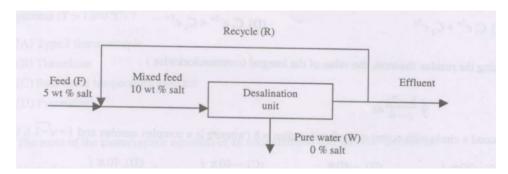


Fig. 2

If the overall recovery of pure water (through stream W) is 0.75 kg/kg feed, then the recycle ratio (R/F) is

a) 0.25

b) 0.5

c) 0.75

d) 1.0

(GATE CH 2009)

29) For a binary mixture at constant temperature and pressure, which ONE of the following relations between activity coefficient γ and mole fraction χ is thermodynamically consistent?

a)
$$\ln \gamma_1 = -1 + 2\chi_1 - \chi_1^2$$
, $\ln \gamma_2 = \frac{1}{2} \chi_1^2$
b) $\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$, $\ln \gamma_2 = \chi_1^2$
c) $\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$, $\ln \gamma_2 = -\frac{1}{2} \chi_1^2$
d) $\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$, $\ln \gamma_2 = -\chi_1^2$

b)
$$\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$$
, $\ln \gamma_2 = \chi_1^2$

c)
$$\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$$
, $\ln \gamma_2 = -\frac{1}{2} \chi_1^2$

d)
$$\ln \gamma_1 = -1 + \chi_1 - \chi_1^2$$
, $\ln \gamma_2 = -\chi_1^2$

(GATE CH 2009)

30) Two identical reservoirs, open at the top, are drained through pipes attached to the bottom of the tanks as shown below. The two drain pipes are of the same length, but of different diameters $D_1 > D_2$

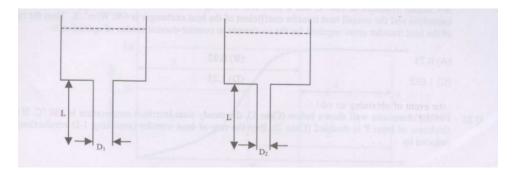


Fig. 3

Assuming the flow to be steady and laminar in both drain pipes, if the volumetric flow rate in the larger pipe is 16 times of that in the smaller pipe, the ratio D_1/D_2 is

a) 2

b) 4

c) 8

d) 16

(GATE CH 2009)

31) For an incompressible flow, the x- and y-components of the velocity vector are $v_y = 3(y+z)v_x =$ 2(x + y) where x, y, z are in metres and velocities are in m/s. Then the z-component of the velocity vector (v_z) of the flow for the boundary condition $v_z = 0$ at z = 0 is

a) 5z

b) -5z

- c) 2x+3z
- d) -2x-3z

(GATE CH 2009)

32) The terminal settling velocity mm diameter glass sphere (density: $2500 \text{kg} / m^3$) in a viscous Newtonian liquid (density: $1500 \text{kg} / m^3$) is 100 s / mu m/s. If the particle Reynolds small and the value of acceleration due to gravity is $9.81 \text{m} / s^2$ the viscosity of the liquid (in Pa.s) is

a) 100

- b) 196.2
- c) 245.3
- d) 490.5

(GATE CH 2009)

33) A well-insulated hemispherical furnace (radius = 1m) is shown below:

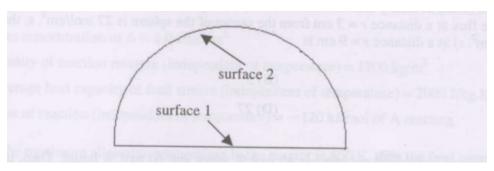


Fig. 4

The self-view factor of radiation for the curved surface 2 is

a) 1/4

b) 1/2

c) 2/3

d) 3/4

(GATE CH 2009)

34) A double-pipe heat exchanger is to be designed to heat 4 kg/s of a cold feed from 20 to $40^{\circ}C$ using a hot stream available at $160^{\circ}C$ and a flow rate of 1 kg/s. The two streams have equal specific heat capacities and the overall heat transfer coefficient of the heat exchanger is $640 \text{W} / m^2 \text{ K}$. Then the ratio of the heat transfer areas required for the co-current to counter-current modes of operation

a) 0.92

c) 1.085

b) 0.73

d) 1.25

(GATE CH 2009)

35) For the composite wall shown below (Case1), the steady state interface temperature is $180^{\circ}C$ If the thickness of layer P is doubled (Case2), then the rate of heat transfer (assuming 1-D conduction) is reduced by

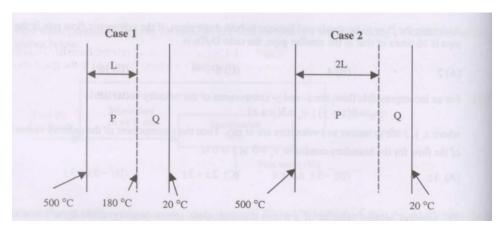


Fig. 5

a) 20%

c) 50%

b) 40%

d) 70%

(GATE CH 2009)

36) Species A is diffusing at steady state from the surface of a sphere (radius = 1cm) into a stagnant fluid. If the diffusive flux at a distance r = 3 cm from the center of the $27 \text{mol} / cm^2$ s, the diffusive flux (in $\text{mol} / cm^2 . s$) at a distance r = 9 cm is

a) 1

c) 9

b) 3

d) 27

(GATE CH 2009)

37) The feed to a binary distillation column has 40 mol % vapor and 60 mol % liquid. Then, the slope of the q-line in the McCabe-Thiele plot is

a) -1.5

b) -0.6

c) 0.6

d) 1.5

(GATE CH 2009)

38) The equilibrium moisture curve for a solid is shown below:

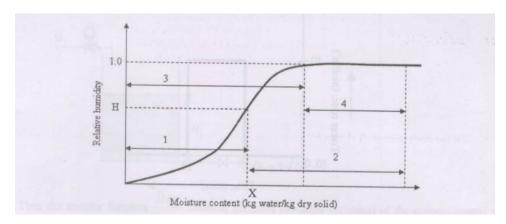


Fig. 6

The total moisture content of the solid is X and it is exposed to air of relative humidity H. In the table below. Group I lists the types of moisture, and Group II represents the region in the graph above.

	GROUP I	GROUP II
P.	Equilibrium moisture	1
Q.	Bound moisture	2
R.	Unbound moisture	3
S.	Free moisture	4

a) P-1, Q-2, R-3, S-4

c) P-1, Q-4, R-2, S-3

b) P-1, Q-3, R-4, S-2

d) P-1, Q-2, R-4, S-3

(GATE CH 2009)

- 39) The liquid-phase reaction $A \rightarrow B$ is conducted in an adiabatic plug flow reactor.
 - a) Inlet concentration of A = $4.0 kmol/m^3$
 - b) Density of reaction mixture (independent of temperature) = 1200kg/m Average heat capacity of feed stream (independent of temperature) = 2000 J/kg.K
 - c) Heat of reaction (independent of temperature)120 kJ/mol of A reacting
 - d) If the maximum allowable temperature in the reactor is 800 K, then the feed temperature (in K) should not exceed
 - a) 400

c) 600

b) 500

d) 700

(GATE CH 2009)

40) An isothermal pulse test is conducted on a reactor and the variation of the outlet tracer concentration with time is shown below:

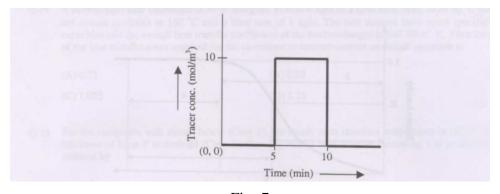


Fig. 7

The mean residence time of the fluid in the reactor (in minutes) is

a) 5.0

c) 10.0

b) 7.5

d) 15.0

(GATE CH 2009)

41) The inverse Laplace transform of is $\frac{1}{2s^2+3s+1}$

a) $e^{\frac{-t}{2}} - e^{-t}$

c) $e^{\frac{-t}{2}} - 2e^{-t}$ d) $e^{\frac{-t}{2}} - e^{-t}$

b) $2e^{\frac{-t}{2}} - e^{-t}$

(GATE CH 2009)

42) The characteristic of a closed loop system using a proportional controller with gain K_c is

$$12s^3 + 19s^2 + 8s + 1 + K_c = 0$$

At the onset of instability, the value of K_c is

a) 35/3

b) 10

c) 25/3

d) 20/3

(GATE CH 2009)

43) The block diagram for a control system is shown below:

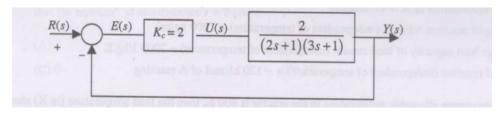


Fig. 8

For a unit step change in the set point, R(s) the steady state offset in the output Y(s) is

a) 0.2

b) 0.3

c) 0.4

- d) 0.5
- 44) For a tank of cross-sectional area $100cm^2$ and inlet flow rate $(Q_i \text{ in } cm^3/s)$, the outlet flow rate $(Q_o \text{ in } cm^3/s)$ is related to the liquid height (H in cm as) $Q_o = 3\sqrt{(H)}$ (see figure below).

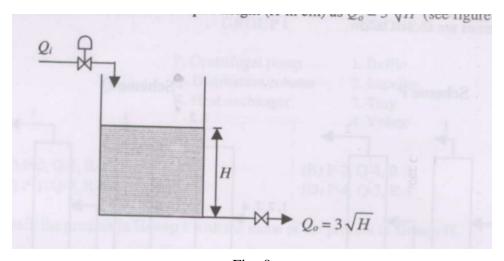


Fig. 9

Then the transfer function $\frac{H(s)}{Q(S)}$ of the process around the steady-state point, $Q_{Lx} = 18cm^3/s$ and $H_x =$ 36cm is

a) $\frac{100s+1}{1002}$

c) $\frac{3}{300s+1}$ d) $\frac{4}{400s+1}$

(GATE CH 2009)

- 45) A column costs Rs. 5.0 lakhs and has a useful life of 10 years. Using the double declining balance depreciation method, the book value of the unit at the end of five years (in lakhs of Rs.) is
 - a) 1.21

c) 1.64

b) 1.31

d) 2.05

46) An equi-molar mixture of four hydrocarbons (1, 2, 3, 4) is to be separated into high purity individual components using a sequence of simple distillation columns (one overhead and one bottom stream). Four possible schemes are shown below.

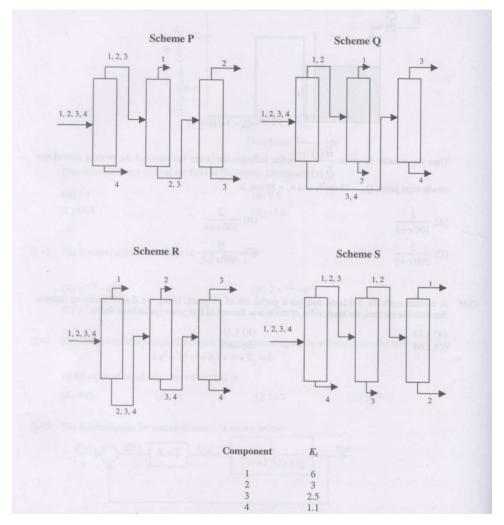


Fig. 10

Component	K_i	
1	6	
2	3	
3	2.5	
4	1.1	
4		

a) P

b) Q

c) R

d) S

47) Match the equipment in Group I to the internals in Group II

	GROUP I		GROUP II
P.	Centrifugal Pump	1.	Baffle
Q.	Distillation column	2.	Impeller
R.	Heat exchanger	3.	Tray
		4.	Volute

(GATE CH 2009)

a) P-2, Q-1, R-4	c) P-1, Q-3, R-4	
b) P-2, Q-4, R-3	d) P-4, Q-3, R-1	
		(GATE CH 2009)
48) Match the product in C	Group I with the name of the process in Group II.	,
	GROUP II GROUP II	
	P. Sodium carbonate 1. Haber	
	Q. Ammonia 2. Solvay	
	R. Sulphuric acid 3. Fischer-Tropsch	
	4. Contact	
a) P-2, Q-1, R-4	c) P-3, Q-4, R-2	
b) P-4, Q-1, R-2	d) P-2, Q-1, R-3	
		(GATE CH 2009)
49) Match the product in (Group I to the raw material in Group II.	(GAIE CH 2009)
+) Water the product in C	GROUP I GROUP II	
	P. Ethylene 1. Natural gas	
	Q. Methanol 2. Synthesis gas	
	R. Pthalic anhydride 3. Naphtha	
	4. Naphtalene	
\ D1 0 2 D 2	\ D2 01 D4	
a) P-1, Q-2, R-3	c) P-3, Q-1, R-4	
b) P-2, Q-1, R-4	d) P-3, Q-2, R-4	
		(GATE CH 2009)
50) Match the unit process	in Group I with the industry in Group II.	
	GROUP II GROUP II	
	P. Steam cracking 1. Petroleum refining	
	Q. Hydrocracking 2. Petrochemicals	
	R. Condensation 3. Polymers	
	4. Soaps and detergents	
a) P-1, Q-2, R-3	c) P-1, Q-2, R-4	
b) P-2, Q-3, R-3	d) P-2, Q-1, R-3	

Common Data for Questions 51 and 52 An ideal gas with molar heat capacity $C_p = 5/2 \times R$ (where R = 8.314 J/mol K) is compressed adiabatically from 1 bar and 300 K to pressure P_2 in a closed system. The final temperature after compression is 600 K and the mechanical efficiency of compression is 50%.

- 51) The work required for compression (in kJ / mol) is
 - a) 3.74

b) 6.24

c) 7.48

d) 12.48

(GATE CH 2009)

- 52) The final pressure P_2 (in bar) is
 - a) $2^{\frac{3}{4}}$

b) $2^{\frac{5}{4}}$

c) $2^{\frac{3}{2}}$

d) $2^{\frac{5}{2}}$

(GATE CH 2009)

Common Data for questions 53 and 54

A slab of thickness L with one side (x = 0) insulated and the other side (x = L) maintained at a constant temperature T_0 is shown below.

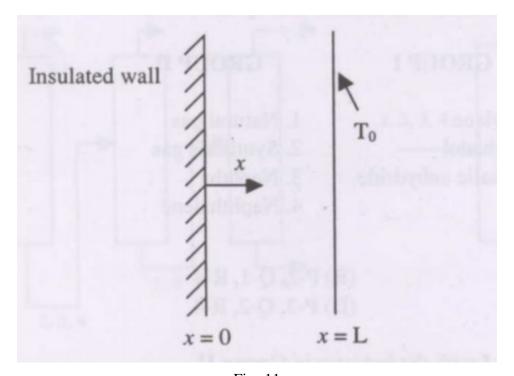


Fig. 11

A uniformly distributed internal heat source produces heat in the slab at the rate of SW / m^3 Assume the heat conduction to be steady and 1-D along the x-direction.

- 53) The maximum temperature in the slab occurs at x equal to
 - a) 0

b) L/4

c) L/2

d) L

(GATE CH 2009)

54) The heat flux at x = L is

a) 0

- b) S L/4
- c) S L/2
- d) SL

(GATE CH 2009)

Common Data for Questions 55 and 56 A flash distillation drum (see figure below) is used to separate a methanol-water mixture. The mole fraction of methanol in the feed is 0.5, and the feed flow rate is 1000 kmol/hr. The feed is preheated in a heater with heat duty Q and is subsequently flashed in the drum. The flash drum can be assumed to be an equilibrium stage, operating adiabatically. The equilibrium relation between the mole fractions of methanol in the vapor and liquid phases is $y = 4 \times 1000 \text{ kmol/hr}$. The ratio of distillate to feed flow rate is 0.5.

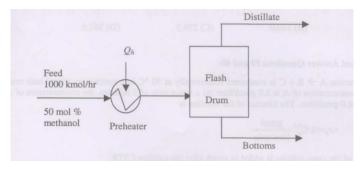


Fig. 12

- 55) The mole fraction of methanol in the distillate is
 - a) 0.2

b) 0.7

c) 0.8

d) 0.9

(GATE CH 2009)

- 56) If the enthalpy of the distillate with reference to the feed is 3000 kJ/kmol, and the enthalpy of the bottoms with reference to the feed is -1000 kJ/kmol, the heat duty of the preheater (Q in kJ / hr) is
 - a) -2×10^6
- b) -1×10^6
- c) 1×10^6
- d) 2×10^6

(GATE CH 2009)

Statement for Linked Answer Questions 57 and 58

A free jet of water is emerging from a nozzle (diameter 75 mm) attached to a pipe (diameter 225 mm) as shown below.

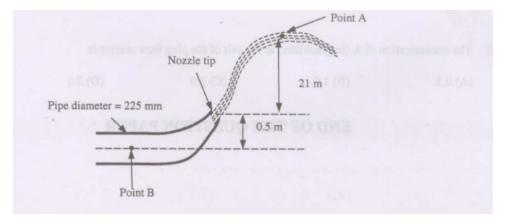


Fig. 13

The velocity of water at point A is 18 m/s. Neglect friction in the pipe and nozzle. Use g = 9.81 m/s^2 and density of water = $1000kg/m^3$.

57) The velocity of water at the tip of the nozzle (in m / s) is

a) 13.4	b) 18.0	c) 23.2	d) 27.1	
			(GATE CH	2009)
58) The gauge pres	sure (in kPa) at point B i	S		
a) 80.0	b) 100.0	c) 239.3	d) 367.6	
			(GATE CH	2009)
Statement for	Linked Answer Questio	ns 59 and 60	`	ŕ
The liquid-phas	se reaction $A \rightarrow B + C$ is	conducted isothermally a	t $50^{\circ}C$ in a continuous stirre	d tank
reactor (CSTR)). The inlet concentration	of A is 8.0 gmol/liter.	At a space time of 5 minute	es, the
concentration of	of A at the exit of CSTR is	s 4.0 gmol/liter. The kin	etics of the reaction is	
$-r_{1} - k^{0.5}C_{1} = \frac{g}{2}$	mol_			

 $-r_A = K^{OS} C_A \frac{S^{OS}}{liter.min}$ A plug flow reactor of the same volume is added in series after the existing CSTR.

59) The rate constant (k) for this reaction at $50^{\circ}C$ is

a)
$$0.2 \left(\frac{gmol}{liter}\right)^{0.5} min^{-1}$$
 c) $0.4 \left(\frac{gmol}{liter}\right)^{0.5} min^{-1}$ b) $0.2 \left(\frac{gmol}{liter}\right)^{0.5} min^{-1}$ d) $0.4 \left(\frac{gmol}{liter}\right)^{0.5} min^{-1}$

(GATE CH 2009)

60) The concentration of A (in gmol/liter) at the exit of the plug flow reactor is