| Company Name | LoremIpsum | Project Title | Fossee |
|-----------------|--------------|---------------|------------|
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| Designer | LoremIpsum | Job Number | 123 |
| Date | 18 /05 /2020 | Client | LoremIpsum |

1 Input Parameters

| Module MainModule | | | Fin Plate |
|-----------------------|------------|------------------------|--------------------------------|
| MainModule | | | |
| | | Shear Connection | |
| Connectivity | | Column flange-Beam web | |
| Shear(kN)* | Shear(kN)* | | 400.0 |
| | Suj | pporting Sect | ion |
| Supporting Se | ection | | UC $356 \times 406 \times 393$ |
| Material | * | | E 250 (Fe 410 W)A |
| Ultimate strength, | , fu (MPa) | | 410 |
| Yield Strength, f | fy (MPa) | | 250 |
| α Mass 393 | 3.0 | Iz(cm4) | 1466180000.0 |
| ZZ D Area(cm2) - 500 | 060.0 | Iy(cm4) | 553650000.0 |
| D(mm) 419 | 9.0 | rz(cm) | 171.0 |
| R_1 $B(mm)$ 407 | | ry(cm) | 105.0 |
| R_2 $t(mm)$ 30. | .6 | Zz(cm3) | 6998000.0 |
| T(mm) 49. | .2 | Zy(cm3) | 2721000.0 |
| FlangeSlope 90 | | Zpz(cm3) | 8222000.0 |
| R1(mm) 15. | .2 | Zpy(cm3) | 2721000.0 |
| R2(mm) 0.0 |) | | |
| | Su | pported Sect | ion |
| Supported Se | ection | | NPB 600x220x122.4 |
| Material | * | | E 250 (Fe 410 W)A |
| Ultimate strength, | , fu (MPa) | | 410 |
| Yield Strength , f | fy (MPa) | | 250 |
| (B-t) | | Iz(cm4) | 920834000.0 |
| ZZ D Area(cm2) - 156 | 600.0 | Iy(cm4) | 33828700.0 |
| D(mm) 600 | 0.0 | rz(cm) | 243.0 |
| R_1 $B(mm)$ 220 | 0.0 | ry(cm) | 46.6 |
| $rac{R_2}{t(mm)}$ 12. | | Zz(cm3) | 3069450.0 |
| T(mm) 19. | .0 | Zy(cm3) | 307530.0 |
| FlangeSlope 90 | | Zpz(cm3) | 3512400.0 |
| R1(mm) 2.4 | 4 | Zpy(cm3) | 307530.0 |

R2(mm)

Diameter (mm)*

Grade *

Type *

Bolt hole type

Slip factor (μ_f)

Type of edges

0.0

Bolt Details

| T . | 1 (| _ |
|------|-----|----|
| Page | Lot | .7 |

[12.0, 16.0, 20.0, 24.0, 30.0, 36.0]

 $[3.6,\,4.6,\,4.8,\,5.6,\,5.8,\,6.8,\,8.8,\,9.8,\,10.9,\,12.$

Friction Grip Bolt

Standard

 $\begin{array}{c} 0.3 \\ \text{a - Sheared or hand flame cut} \end{array}$

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| Gap between beam and support (mm) | 10.0 | |
|--|---|--|
| Are the members exposed to corrosive influences | False | |
| | Plate Details | |
| Thickness(mm)* | [3.0, 4.0, 5.0, 6.0, 8.0, 10.0, 12.0, 14.0, 16.0, 18.0, 20.0, 22.0, 24.0] | |
| Material * | E 250 (Fe 410 W)A | |
| Ultimate strength, fu (MPa) | 410 | |
| Yield Strength , fy (MPa) | 250 | |
| | Weld Details | |
| Weld Type | Fillet | |
| Type of weld fabrication | Shop Weld | |
| Material grade overwrite (MPa) Fu | 410.0 | |

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2 Design Checks

2.1 Bolt Design Checks

| Check | Required | Provided | Remarks |
|-------------------------|--|---|---------|
| Diameter (mm)* | | 30.0 | |
| Grade * | | 10.9 | |
| Slip Resistance | | $V_{dsf} = \frac{\mu_f \ n_e \ K_h \ F_o}{\gamma_{mf}}$ $Where, F_o = 0.7 * f_{ub} A_{nb}$ $V_{dsf} = \frac{0.3 * 1 * 1.0 * 0.7 * 1000.0 * 56}{1.25}$ $= 94.25$ | 1 |
| No of Bolts | $R_{u} = \sqrt{V_{u}^{2} + A_{u}^{2}}$ $n_{trial} = R_{u}/V_{bolt}$ $R_{u} = \frac{\sqrt{400.0^{2} + 300.0^{2}}}{94.25}$ $= 6$ | 8 | |
| No of Columns | | 2 | |
| No of Rows | | 4 | |
| Min. Pitch (mm) | $p/g_{min} = 2.5 d$ $= 2.5 * 30.0 = 75.0$ | 75 | Pass |
| Max. Pitch (mm) | $p/g_{max} = \min(32 \ t, \ 300 \ mm)$ = $\min(32 * 12.0, \ 300 \ mm)$ = 384.0 |) 75 | Pass |
| Min. Gauge (mm) | $= 384.0$ $p/g_{min} = 2.5 d$ $= 2.5 * 30.0 = 75.0$ | 105 | Pass |
| Max. Gauge (mm) | $p/g_{max} = \min(32 \ t, \ 300 \ mm)$ = $\min(32 * 12.0, \ 300 \ mm)$ = 384.0 |) 105 | Pass |
| Min. End Distance (mm) | $e/e'_{min} = [1.5 \text{ or } 1.7] * d_0$ = 1.7 * 33.0 = 56.1 $e/e'_{max} = 12 t \varepsilon$ | 60 | Pass |
| Max. End Distance (mm) | $\varepsilon = \sqrt{\frac{250}{f_y}}$ $e/e'_{max} = 12 * 12.0 * \sqrt{\frac{250}{250}}$ | 60 | Pass |
| Min. Edge Distance (mm) | $= 144.0$ $e/e'_{min} = [1.5 \text{ or } 1.7] * d_0$ $= 1.7 * 33.0 = 56.1$ | 60 | Pass |

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| Check | Required | Provided | Remarks |
|-------------------------|---|----------|---------|
| Max. Edge Distance (mm) | $e/e'_{max} = 12 \ t \ \varepsilon$ $\varepsilon = \sqrt{\frac{250}{f_y}}$ $e/e'_{max} = 12 \ *12.0 * \sqrt{\frac{250}{250}}$ $= 144.0$ | 60 | Pass |
| Capacity (kN) | 112.68 | 113.1 | Pass |

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2.2 Plate Design Checks

| Check | Required | Provided | Remarks |
|---|------------------------------------|---|---------|
| Min. Plate Height (mm) | $0.6 * d_b = 0.6 * 600.0 = 360.0$ | 435 | Pass |
| | $d_b - 2(t_{bf} + r_{b1} + gap)$ | | |
| Max. Plate Height (mm) | = 600.0 - 2 * (19.0 + 2.4 + 10) | 435 | Pass |
| | = 557.2 | | |
| | $2*e_{min} + (n \ c - 1)*p_{min})$ | | |
| Min. Plate Length (mm) | = 2 * 56.1 + (2 - 1) * 75.0 | 205.0 | Pass |
| 16 Di | = 197.2 | 10.0 | D |
| Min.Plate Thickness (mm) | $t_w = 12.0$ | 12.0 | Pass |
| | | $V_{dg} = \frac{A_v * f_y}{\sqrt{3} * \gamma_{mo}}$ | |
| | | $\sqrt{3} * \gamma_{mo}$ | |
| Shear yielding Capacity (V_dy) (kN) | | $= \frac{435 * 12.0 * 250}{\sqrt{3} * 1.1}$ | |
| (v_dy) (kiv) | | 004.05 | |
| | | $V_{dn} = \frac{0.75 * A_{vn} * f_u}{\sqrt{3} * \gamma_{mo}}$ | |
| | | $V_{dn} \equiv \frac{1}{\sqrt{3} * \gamma_{mo}}$ | |
| Shear Rupture Capacity (V_dn) (kN) | | = 1 * (435 - (4 * 33.0)) * 12.0 * 43.0 | 10 |
| (v_dii) (kiv) | | = 1118.07 | |
| Block Shear Capacity in Shear (V_db) (kN) | | 893.35 | |
| | | $V_d = Min(V_{dy}, V_{dn}, V_{db})$ | |
| Shear Capacity (V_d) | 400.0 | = Min(684.95, 1118.07, 893.35) | Pass |
| (kN) | | =684.95 | |
| | | $T_{dg} = \frac{l * t_p * f_y}{\gamma_{mo}}$ | |
| Tangian Violding Consoits | | γ_{mo} 435 ± 12.0 ± 250 | |
| Tension Yielding Capacity (kN) | | $=\frac{435*12.0*250}{1.1}$ | |
| (') | | = 1186.36 | |
| | | $T_{dn} = \frac{0.9 * A_n * f_u}{\gamma_{m1}}$ | |
| | | | |
| Tension Rupture Capacity | | $= \frac{0.9 * (435 - 4 * 33.0) * 12.0 * 4}{1.25}$ | 10 |
| (kN) | | = 1307.15 | |
| Block Shear Capacity in | | = 1307.13 1101.75 | |
| Tension (T_db) (kN) | | | |
| , , , , , | | $T_d = Min(T_{dg}, T_{dn}, T_{db})$ | |
| Tension Capacity (kN) | 300.0 | = Min(1186.36, 1307.15, 1101.75) | Pass |
| | | =1101.75 | |
| Moment Capacity (kN-m) | 43.0 | 129.02 | Pass |
| Interaction Ratio | ≤ 1 | $\frac{43.0}{129.02} + \frac{300.0}{1101.75} = 0.61$ | Pass |
| | | $\frac{1}{129.02} + \frac{1}{1101.75} = 0.01$ | |

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2.3 Weld Checks

| Check | Required | Provided | Remarks |
|-----------------------|--|---|---------|
| Min Weld Size (mm) | | 10 | Pass |
| Max Weld Size (mm) | $Thickness of Thinner part$ $= Min(49.2, 12.0) = 12.0$ $t_{w_{max}} = 12.0$ | 10 | Pass |
| Weld Strength (kN/mm) | $R_w = \sqrt{(T_{wh} + A_{wh})^2 + (T_{wv} + V_{wv})^2}$ $T_{wh} = \frac{M * y_{max}}{Ipw} = \frac{43000000.0 * 207.5}{11912229.17}$ $T_{wv} = \frac{M * x_{max}}{Ipw} = \frac{43000000.0 * 0.0}{11912229.17}$ $V_{wv} = \frac{V}{l_w} = \frac{400000.0}{830}$ $A_{wh} = \frac{A}{l_w} = \frac{300000.0}{830}$ $R_w = \sqrt{(749.02 + 361.45)^2 + (0.0 + 481.93)^2}$ $= 1282.92$ | $f_w = \frac{t_t * f_u}{\sqrt{3} * \gamma_{mw}}$ $= \frac{7.0 * 410}{\sqrt{3} * 1.25}$ $= 1325.6$ | Pass |

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3 3D View

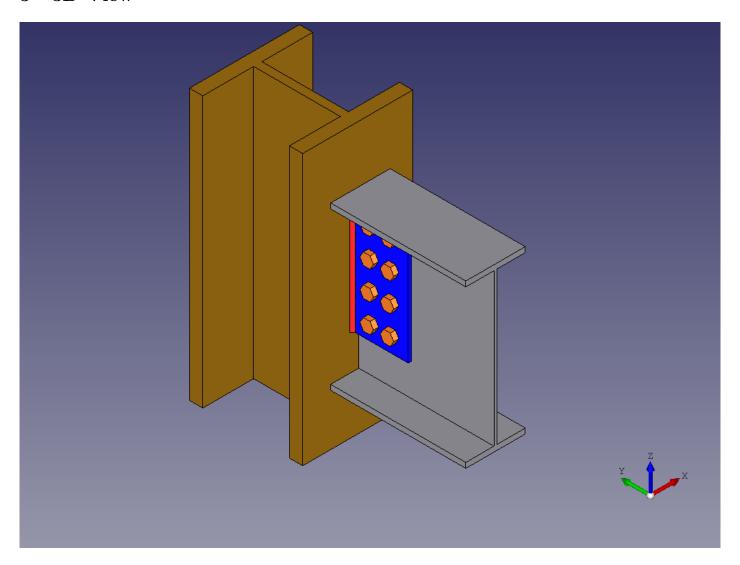


Figure 1: 3D View