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1 Input Parameters

Modu	ıle		Beam	Coverplate Weld Connection
MainMo	odule			Moment Connection
Moment(l	kNm)*			10.0
Shear(k	(N)*			10.0
Axial (k	:N) *			10.0
		Section	•	
	Beam S	ection *		NPB 750x270x146.9
	Mate	rial *		E 250 (Fe 410 W)A
т Ү	Ultimate stren	ngth, fu (MPa)		410
	Yield Strength , fy (MPa)		250	
α	Mass	146.87	Iz(mm4)	1645354000.0
4	Area(mm2) -	18710.0	Iy(mm4)	52878600.0
ZZ D	A			
	D(mm)	750.0	rz(mm)	296.6
R ₁	B(mm)	265.0	ry(mm)	53.2
В	t(mm)	13.2	Zz(mm3)	4387610.0
Y	T(mm)	17.0	Zy(mm3)	399080.0
•	FlangeSlope	90	Zpz(mm3)	5081800.0
	R1(mm)	1.7	Zpy(mm3)	399080.0
	R2(mm)	0.0		
		Weld Details		
Weld T	ype			Fillet
Type of weld	fabrication			Shop Weld
Material grade over	rwrite (MPa) Fu			410.0

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2 Design Checks

2.1 Member Capacity

Check	Required	Provided	Remarks
Axial Capacity Ac (kN)		$Ac = \frac{A * f_y}{\gamma_{m0} * 1000}$ $= \frac{18710.0 * 250}{1.1 * 1000}$ $= 4252.27$	
Shear Capacity Sc (kN)		$S_c = \frac{A_v * f_y}{\sqrt{3} * \gamma_{mo} * 1000}$ $= \frac{716.0 * 13.2 * 250}{\sqrt{3} * 1.1 * 1000}$ $= 1240.14837999999999999999999999999999999999999$	
Plastic Moment Capacity Pmc (kNm)		$Pmc = \frac{\beta_b * Z_p * fy}{\gamma_{mo} * 1000000}$ $= \frac{1 * 1691765 * 250}{1.1 * 1000000}$ $= 384.49$	
Moment Deformation Criteria Mdc (kNm)		$Mdc = \frac{1.5 * Z_e * fy}{1.1}$ $= \frac{1.5 * 4387610.0 * 250}{1.1}$ $= 1495.78$	
Moment Capacity Mc (kNm)		$M_c = min(Pmc, Mdc)$ = $min(384.49, 1495.78)$ = 384.49	

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2.2 Load Consideration

Check	Required	Provided	Remarks
	$Ac_{min} = 0.3 * A_c$	$Au = max(A, Ac_{min})$	
Axial Load Au (kN)	=0.3*4252.27	= max(10.0, 1275.68)	Pass
	= 1275.68	= 1275.68	
	$Sc_{min} = 0.6 * A_c$	$Vu = max(V, Vc_{min})$	
Shear Load Vu (kN)	= 0.6 * 1240.15	= max(10.0, 744.09)	Pass
	=744.09	=744.09	
	$Mc_{min} = 0.5 * M_c$	$Mu = max(M, Mc_{min})$	
Moment Load Mu (kNm)	= 0.5 * 384.49	= max(10.0, 192.25)	Pass
	= 192.25	= 192.25	
		$A_w = Axial \ force \ in \ web$	
		$=\frac{(D-2*T)*t*Au}{A}$	
		$= \frac{(750.0 - 2 * 17.0) * 13.2 * 1}{(750.0 - 2 * 17.0) * 13.2 * 1}$	1275.68
		18710.0	
Forces Carried by Web		= 644.4	
		$M_w = Moment \ in \ web$	
		$=\frac{Z_w*Mu}{Z}$	
		$= \frac{1691765 * 192.25}{5001000.0}$	
		$=\frac{1001100 * 102.20}{5081800.0}$	
		= 64.0	
		$A_f = Axial \ force \ in \ flange$	
		$=\frac{Au*B*T}{A}$	
		$=\frac{1275.68 * 265.0 * 17.0}{2000}$	
		18710.0	
		= 307.16	
		$M_f = Moment \ in \ flange$	
Forces Carried by Flange		$=Mu-M_w$	
		= 192.25 - 64.0	
		= 128.25	
		$F_f = flange \ force$	
		$=\frac{M_f*1000}{D-T}+A_f$	
		D 1	
		$= \frac{128.25}{750.0 - 17.0} + 307.16$	
		$\begin{vmatrix} 750.0 - 17.0 \\ = 482.12 \end{vmatrix}$	
		=482.12	

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2.3 Weld Design Checks

Check	Required	Provided	Remarks
	Thickness of Thicker part		
	= max(17.0, 14.0)		
Min Weld Size (mm)	= 17.0	12	Pass
	$IS800:2007\ cl.10.5.2.3\ Table 21,$		
	$t_{w_{min}} = 5$		
	Thickness of Thinner part		
Max Weld Size (mm)	=Min(17.0, 14.0) = 14.0	12	Pass
	$t_{w_{max}} = 14.0$		
	$Stress = \frac{F_f * 1000}{F_{rl}}$		
Flange Weld Strength	$-\frac{482.12*1000}{}$	1590.72	Pass
(N/mm)	760		
	= 634.3678780249971		

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2.4 Flange Plate Check-Outside/Inside

Check	Required	Provided	Remarks
Min. Plate Height (mm)	50	$b_{fp} = B - 2 * sp$ = 265.0 - 2 * 17 = 230	Pass
Min. Plate Length (mm)	230	$l_{fp} = [2 * (l_w + 2 * s) + g]$ $= [2 * (2752 * 12) + 10.0]$ $= 610$	Pass
Min. Inner Plate Height (mm)	50	$b_{ifp} = \frac{B - 4 * sp - t_w - 2 * r_1}{2}$ $= \frac{265.0 - 4 * 17 - 13.2 - 2 * 1.7}{2}$ $= 90$	Pass
Max. Inner Plate Height (mm)	$b_{ifp} = \frac{B - 4 * sp - t_w - 2 * r_1}{2}$ $= \frac{265.0 - 4 * 17 - 13.2 - 2 * 1.7}{2}$ $= 90$	90	Pass
Min. Inner Plate Length (mm)	230	$l_{fp} = [2 * (l_w + 2 * s) + g]$ $= [2 * (2752 * 12) + 10.0]$ $= 610$	Pass

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3 3D View



Figure 1: 3D View