Engineerin g Physics

Second Edition

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Professor Malik is highly cited in India and abroad for his research work and books with h-index of 24 and i10-index of 70. Governments of India, Germany and France, through DST, CSIR, DRDO, AICTE, DAAD, CEFIPRA, etc., have provided him funding to accomplish 12 sponsored research projects. He is on the editorial board of 5 reputed research journals (including Springer). In recognition of his outstanding research and teaching contributions, he has been asked to deliver more than 50 keynote and invited talks in India, Japan, South Korea, USA, France, Germany, South Africa, and Turkey. Also, he has been chief guest in various universities, mentor of faculty colleagues of engineering institutions, and member of organizing and advisory committees of national and international conferences held in India and abroad.

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Apart from this book, he has also authored another textbook on Laser-Matter Interaction, CRC Press, 3 Chapters in the Books Wave Propagation, InTechOpen Science, Croatia (featured as highly downloaded chapter), Society, Sustainability and Environment, Shivalik Prakashan, New Delhi, and Plasma Science and Nanotechnology, Apple Academic Press, exclusive worldwide distribution by CRC Press, a Taylor & Francis Group.



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Dedicated to

OMENDRA Bhaiya and all those moments that remain with me as a source of inspiration and help me to move ahead with great success, satisfaction and optimistic approach

Brief Contents

Foreword xix Preface to the Second Edition xxii Preface to the First Edition xxiii

1. Interference 1 2. Diffraction 63 3. Polarisation 121 4. Lasers and Holography 155 5. Fibre Optics 186 6. Electron Optics 208 7. Waves and Oscillations 233 8. Simple Harmonic Motion and Sound Waves 259 9. Sound Waves and Acoustics of Buildings 284 10. Dielectrics 313 11. Electromagnetism 328 12. Theory of Relativity 395 13. Applied Nuclear Physics 451 14. Crystal Structure 517 15. Development of Quantum Mechanics 551 16. Quantum Mechanics 595 17. Free Electron Theory 634 18. Band Theory of Solids and Photoconductivity 654 19. Magnetic Properties of Solids 685 20. Superconductivity 716 21. X-Rays 735

viii Brief Contents

22. Nanoscience and Nanotechnology 751 Appendices

Appendix 1 Measurements and Errors 779 Appendix 2 Optics 790 Appendix 3 Mechanical Properties of Materials 794 Chapter-wise Answers to Objective Type Questions 805 Index 809

Contents

Foreword xix Preface to the Second Edition xxi Preface to the First Edition xxiii

- 1. Interference 1 Learning Objectives 1
- 1.1 Young's Double Slit Experiment 2
- 1.2 Concept of Waves and Huygens' Principle 2
- 1.3 Phase Difference and Path Difference 3
- 1.4 Coherence 4
- 1.5 Coherent Sources 5
- 1.6 Analytical Treatment of Interference 6
- 1.7 Conditions for Sustained Interference 8
- 1.8 Multiple Beam Superposition 9
- 1.9 Interference by Division of Wavefront 10
- 1.10 Interference by Division of Amplitude 16
- 1.11 Applications of Interference in the Field of Engineering 32
- 1.12 Scientific Applications of Interference 35
- 1.13 Homodyne and Heterodyne Detection 35

Summary 37

Solved Examples 38

Objective Type Questions 57

Short-Answer Questions 58

Practice Problems 58

Unsolved Questions 60

- 2. Diffraction 63 Learning Objectives 63
- 2.1 Young's Double Slit Experiment: Diffraction or Interference? 64 2.2

Difference between Diffraction and Interference 64

- 2.3 Types of Diffraction 64
- 2.4 Fresnel's Half-period Zones 66
- 2.5 Zone Plate 68
- 2.6 Fresnel's Diffraction by a Circular Aperture 72

x Contents

- 2.7 Fraunhofer Diffraction by a Single Slit 76
- 2.8 Fraunhofer Diffraction by Double Slits 80
- 2.9 Fraunhofer Diffraction by N Slits: Diffraction Grating 84
- 2.10 Application of Diffraction Grating 90
- 2.11 Resolving Power of an Optical Instrument 91

- 2.12 Resolving Power of a Telescope 93
- 2.13 Resolving Power of a Microscope 94
- 2.14 Resolving Power of a Plane Diffraction Grating 96
- 2.15 Dispersive Power of a Plane Diffraction Grating 97

Solved Examples 99

Objective Type Questions 116

Short-Answer Questions 118

Practice Problems 118

Unsolved Questions 119

- 3. Polarisation 121 Learning Objectives 121
- 3.1 Mechanical Experiment Showing Polarisation of Transverse Wave 122 3.2 Difference between Unpolarised Light and Polarised Light 123 3.3 Means of Production of Plane–Polarised Light 123
- 3.4 Theory of Production of Plane, Circularly and Elliptically Polarised Light 135 3.5 Optical Activity 138
- 3.6 Specific Rotation 138
- 3.7 Laurent's Half-shade Polarimeter 138
- 3.8 Biquartz Polarimeter 139
- 3.9 Saccharimeter 140
- 3.10 Photoelasticity 141

Summary 142

Solved Examples 143

Objective Type Questions 150

Short-Answer Questions 151

Practice Problems 152

Unsolved Questions 153

- 4. Lasers and Holography 155 Learning Objectives 155
- 4.1 Absorption and Emission of Radiation 156
- 4.2 Population Inversion 159
- 4.3 Characteristic of Laser Light 161
- 4.4 Main Components of Laser 163
- 4.5 Types of Laser 163
- 4.6 Applications of Lasers 169
- 4.7 Laser Cooling 170
- 4.8 Holography 170

Contents xi

- 4.9 Holography Versus Conventional Photography 171
- 4.10 Recording and Reconstruction of Image on Holograph 172
- 4.11 Types of Holograms 174
- 4.12 Applications of Holography 177

Summary 178

Solved Examples 179

Objective Type Questions 183

Practice Problems 184

5. Fibre Optics 186 Learning Objectives 186

- 5.1 Fundamental Ideas about Optical Fibre 187
- 5.2 Optical Fibres as a Dielectric Waveguide 188
- 5.3 Types of Optical Fibres 188
- 5.4 Acceptance Angle and Numerical Aperture 190
- 5.5 Fibre Optics Communication 193
- 5.6 Optical Fibre Sensors 196
- 5.7 Optical Fibre Connector 197
- 5.8 Optical Fibre Couplers 197
- 5.9 Applications of Optical Fibre Couplers 198

Solved Examples 200

Objective Type Questions 206

Short-Answer Questions 206

Practice Problems 207

- 6. Electron Optics 208 Learning Objectives 208
- 6.1 Specific Charge of an Electron 208
- 6.2 Determination of Specific Charge of an Electron: Thomson's Method 209 6.3

Motion of an Electron in Uniform Electric and Magnetic Fields 210 6.4

Electrostatic and Magnetostatic Focusing 219

- 6.5 Scanning Electron Microscope (SEM) 220
- 6.6 Scanning Tunneling Microscope (STM) 225

Summary 226

Solved Examples 227

Objective Type Questions 231

Practice Problems 232

- 7. Waves and Oscillations 233 Learning Objectives 233
- 7.1 Translational Motion 233
- 7.2 Vibrational or Oscillatory Motion 233
- 7.3 Simple Harmonic Motion (SHM) 234
- 7.4 Differential Equation of SHM and Its Solution 234
- 7.5 Simple Pendulum 239

xii Contents

- 7.6 Mass-string System 241
- 7.7 Damped Harmonic Oscillator 243
- 7.8 Attenuation Coefficients of a Vibrating System 245
- 7.9 Forced Vibrations 247
- 7.10 Resonance 250

Summary 251

Solved Examples 252

Objective Type Questions 257

Short-Answer Questions 257

- 8. Simple Harmonic Motion and Sound Waves 259 Learning Objectives 259
- 8.1 Superposition of Two SHMs 260
- 8.2 Sound Wave and its Velocity 260
- 8.3 Sound Displacement 261

- 8.4 Standing Waves 261
- 8.5 Standing Waves in Air Columns 262
- 8.6 Doppler Effect 264
- 8.7 Supersonic and Shock Waves 266
- 8.8 Derivation of Sound Speed 267
- 8.9 Intensity of Sound and Its Derivation 268
- 8.10 Sound-Intensity Level 269
- 8.11 Interference of Sound Waves in Time: Beats 270
- 8.12 Relation between Displacement and Pressure Amplitude 271
- 8.13 Lissajous Figures 272
- 8.14 Endoscopy 274

Solved Examples 276

Objective Type Questions 280

Practice Problems 282

Unsolved Questions 283

- 9. Sound Waves and Acoustics of Buildings 284 Learning Objectives 284
- 9.1 Audible, Ultrasonic and Infrasonic Waves 284
- 9.2 Production of Ultrasonic Waves 285
- 9.3 Absorption and Dispersion of Ultrasonic Waves 290
- 9.4 Detection of Ultrasonic Waves 291
- 9.5 Applications of Ultrasonic Waves 292
- 9.6 Types of Acoustics 295
- 9.7 Acoustics of Buildings 296
- 9.8 Factors Affecting the Architectural Acoustics 300

Summary 301

Solved Examples 302

Contents xiii

Objective Type Questions 308 True or False 311 Practice Problems 312

- 10. Dielectrics 313 Learning Objectives 313
- 10.1 Dielectric Constant 313
- 10.2 Types of Dielectrics 314
- 10.3 Polarisation of Dielectrics 315
- 10.4 Types of Polarisation 317
- 10.5 Gauss's Law in Dielectrics 318
- 10.6 Dielectric Loss 319
- 10.7 Clausius-Mosotti Equation 321

Summary 322

Solved Examples 323

Objective Type Questions 325

Short-Answer Questions 326

- Electromagnetism 328 Learning Objectives 328
- 11.1 Charge Density 329

- 11.2 Del Operator 330
- 11.3 Gradient 331
- 11.4 Divergence 331
- 11.5 Curl 332
- 11.6 Fundamental Theorem of Calculus 333
- 11.7 Fundamental Theorem for Gradient 333
- 11.8 Gauss's or Green's Theorem 334
- 11.9 Stokes' Theorem 335
- 11.10 Electric Field and Electric Potential 335
- 11.11 Poisson's and Laplace's Equations 336
- 11.12 Capacitor 337
- 11.13 Magnetic Flux Density (BE) 338
- 11.14 Magnetic Field Strength (H^Æ) 338
- 11.15 Ampere's Circuital Law 338
- 11.16 Electrostatic Boundary Conditions 339
- 11.17 Scalar and Vector Potentials 341
- 11.18 Continuity Equation 342
- 11.19 Maxwell's Equations: Differential Form 343
- 11.20 Maxwell's Equations: Integral Form 348
- 11.21 Significance of Maxwell's Equations 350
- 11.22 Maxwell's Displacement Current and Correction in Ampere's Law 351
- 11.23 Eletromagnetic (EM) Wave Propagation in Free Space 352
- 11.24 Transverse Nature of Electromagnetic Waves 355

xiv Contents

- 11.25 Maxwell's Equations in Isotropic Dielectric Medium: EM Wave Propogation 355
- 11.26 Maxwell's Equations in Conducting Medium: EM Wave Propagation and Skin Depth 357
- 11.27 Electromagnetic Energy Density 360
- 11.28 Poynting Vector and Poynting Theorem 361
- 11.29 Wave Propagation in Bounded System: Waveguide 363
- 11.30 Coaxial Cable 364

Summary 365

Solved Examples 369

Objective Type Questions 388

Short-Answer Questions 390

- 12. Theory of Relativity 395 Learning Objectives 395
- 12.1 Frame of Reference 395
- 12.2 Galilean Transformation 396
- 12.3 Michelson-Morley Experiment 398
- 12.4 Postulates of Special Theory of Relativity 401
- 12.5 Lorentz Transformation 401
- 12.6 Length Contraction 403
- 12.7 Time Dilation 405
- 12.8 Addition of Velocities 406
- 12.9 Variation of Mass with Velocity 407
- 12.10 Einstein's Mass Energy Relation 409

Solved Examples 413

Objective Type Questions 447

Short-Answer Questions 448

Practice Problems 449

Unsolved Questions 450

- 13. Applied Nuclear Physics 451 Learning Objectives 451
- 13.1 Basic Properties of Nucleus 452
- 13.2 Nuclear Forces 454
- 13.3 Binding Energy of Nucleus 455
- 13.4 Nuclear Stability 457
- 13.5 Nuclear Models 457
- 13.6 Nuclear Shell Model 457
- 13.7 Nuclear Liquid Drop Model 459
- 13.8 Radioactivity 460
- 13.9 Discovery of Neutron 469
- 13.10 Nuclear Reactions: Conservation Laws 471
- 13.11 Nuclear Fission 473

Contents XV

- 13.12 Nuclear Fusion 476
- 13.13 Controlled Fusion 477
- 13.14 Particle Accelerators 481

Summary 487

Solved Examples 492

Objective Type Questions 508

Short-Answer Questions 512

Practice Problems 513

Unsolved Questions 515

- 14. Crystal Structure 517 Learning Objectives 517
- 14.1 Types of Solids 518
- 14.2 Unit Cell 518
- 14.3 Types of Crystals 519
- 14.4 Translation Vectors 520
- 14.5 Lattice Planes 521
- 14.6 Miller Indices 521
- 14.7 Simple Crystal Structures 523
- 14.8 Coordination Number 523
- 14.9 Interplanar Spacing 524
- 14.10 Nearest Neighbour Distance and Atomic Radius 525
- 14.11 Packing Fraction 526
- 14.12 Potential Energy Curve and Nature of Interatomic Forces 528
- 14.13 Different Types of Bonding Forces 529
- 14.14 Crystal Structure Analysis 531
- 14.15 Point Defects in Solids 534

Summary 537

Solved Examples 539

Objective Type Questions 546

Short-Answer Questions 548 Practice Problems 549 Unsolved Questions 550

- 15. Development of Quantum Mechanics 551 Learning Objectives 551
- 15.1 Blackbody Radiation: Spectral Distribution 552
- 15.2 Planck's Quantum Hypothesis 554
- 15.3 Simple Concept of Quantum Theory 556
- 15.4 Wave Particle Duality 557
- 15.5 Photoelectric Effect 557
- 15.6 de Broglie Waves: Matter Waves 559
- 15.7 Compton Effect: Compton Scattering 561
- 15.8 Phase and Group Velocities: de Broglie Waves 565

Summary 569

xvi Contents

Solved Examples 570
Objective Type Questions 591
Short-Answer Questions 592
Practice Problems 593
Unsolved Questions 594

- 16. Quantum Mechanics 595 Learning Objectives 595
- 16.1 Heisenberg Uncertainty Principle 596
- 16.2 Wave Function and Its Physical Significance 601
- 16.3 Time Independent Schrödinger Equation 602
- 16.4 Time Dependent Schrödinger Equation 603
- 16.5 Operators 604
- 16.6 Applications of Schrödinger Equation 605
- 16.7 Quantum Statistics 614

Summary 617

Solved Examples 618

Objective Type Questions 630

Short-Answer Questions 632

Practice Problems 632

Unsolved Questions 633

- 17. Free Electron Theory 634 Learning Objectives 634
- 17.1 Lorentz–Drude Theory: Classical Free Electron Theory of Metals 635
- 17.2 Applications of Lorentz-Drude Theory 636
- 17.3 Limitations of Lorentz-Drude or Free Electron Theory 638
- 17.4 Quantum Theory of Free Electrons 638
- 17.5 Thermionic Emission 644

Summary 645

Solved Examples 646

Objective Type Questions 651

Short-Answer Questions 652

Practice Problems 653

18. Band Theory of Solids and Photoconductivity 654 Learning Objectives 654

- 18.1 Kronig-Penney Model 655
- 18.2 One- and Two-Dimensional Brillouin Zones 659
- 18.3 Effective Mass of an Electron 660
- 18.4 Distinction between Insulators, Semiconductors and Conductors (Metals) 661
- 18.5 Intrinsic Semiconductor 664
- 18.6 Extrinsic Semiconductor 667
- 18.7 Hall Effect 669
- 18.8 Photoconductivity 671
- 18.9 Simple Model of Photoconductor 671

Contents xvii

- 18.10 Effect of Traps 674
- 18.11 Applications of Photoconductivity 675

Summary 676

Solved Examples 678

Objective Type Questions 680

Practice Problems 683

- 19. Magnetic Properties of Solids 685 Learning Objectives 685
- 19.1 Magnetic Moment of an Electron 687
- 19.2 Classification of Magnetic Materials 688
- 19.3 Comparison of Properties of Paramagnetic, Diamagnetic and Ferromagnetic Materials 689
- 19.4 Classical Theory of Diamagnetism (Langevin's Theory) 689 19.5 Classical Theory of Paramagnetism (Langevin's Theory) 693
- 19.6 Classical Theory of Ferromagnetism 696
- 19.7 Hysteresis: Nonlinear Relationship between B^Æ and H^Æ 697
- 19.8 Energy Loss Due to Hysteresis 698
- 19.9 Importance of Hysteresis Curve 699
- 19.10 Magnetic Circuits 700
- 19.11 Forces on Magnetic Materials 700
- 19.12 Magnetic Materials and Their Applications 700

Summary 702

Solved Examples 705

Objective Type Questions 712

Short-Answer Questions 714

- 20. Superconductivity 716 Learning Objectives 716
- 20.1 Electrical Resistivity of Solids and Phonons 717
- 20.2 Properties of Superconductors 717
- 20.3 Classification of Superconductors 719
- 20.4 Effect of Magnetic Field 719
- 20.5 Isotope Effect 720
- 20.6 London Equations 720
- 20.7 Penetration Depth 722
- 20.8 Cooper Pairs 723
- 20.9 Bose-Einstein Condensation 724
- 20.10 BCS Theory: Qualitative Explanation 724
- 20.11 Coherence Length 725

20.12 High Temperature (Hi-Tc) Superconductivity 726

20.13 Application of Superconductivity 726

Summary 727

Solved Examples 729

xviii Contents

Objective Type Questions 732 Short-Answer Questions 734 Practice Problems 734

- 21. X-Rays 735 Learning Objectives 735
- 21.1 Origin of X-rays 736
- 21.2 Properties of X-rays 736
- 21.3 X-ray Spectra 737
- 21.4 Moseley's Law 738
- 21.5 Practical Applications of X-rays 740

Summary 740

Solved Examples 741

Objective Type Questions 747

Short-Answer Questions 748

Practice Problems 749

Unsolved Questions 749

- 22. Nanoscience and Nanotechnology 751 Learning Objectives 751
- 22.1 How Nanomaterials are Differenet from Bulk Materials? 752
- 22.2 Difference between Nanoscience and Nanotechnology 752
- 22.3 Quantum Confinement and Classification of Nanostructures 752
- 22.4 Nanoscale in 1-D 753
- 22.5 Nanoscale in 2-D 760
- 22.6 Nanoscale in 3-D 760
- 22.7 Applications of Nanotechnology 768
- 22.8 Limitations of Nanotechnology 770
- 22.9 Disadvantages of Nanotechnology 770

Summary 771

Solved Examples 773

Objective Type Questions 774

Practice Problems 776

Appendices

Appendix 1 Measurements and Errors 779 Appendix 2 Optics 790 Appendix 3 Mechanical Properties of Materials 794 Chapter-wise Answers to Objective Type Questions 805 Index 809

Foreword



It gives me immense pleasure to see the present textbook on "Engineering Physics" which covers almost the entire syllabus taught at undergraduate level at different engineering colleges and institutions throughout India. I complement the authors and appreciate their efforts in bringing out this book written in a very simple language. The text is comprehensive and the explanation of topics is commendable. I understand that this book carries all the elements required for a good presentation.

I have been a student of IIT Kharagpur and later on taught at IIT Delhi. Being a part of the IIT system, I recognise that the rigorous and enriching teaching experience at IITs originating from the interaction with the best engineering students and their strong feedback results in continuous evolution and refinement of the teachers. This spirit is reflected in the comprehensive and in-depth handling of important topics in a very simple manner in this book. I am happy to note that this textbook has been penned down by IITian and hope that it would serve to be a good textbook on the subject. Since this book also covers advanced topics, it will be an important learning resource for the teachers, and those students who wish to develop research skills and pursue higher studies. I hope that the book is well received in the academic world.

Professor Prem Vrat
Vice-Chancellor, U.P. Technical University, Lucknow
Founder Director, IIT Roorkee
Preface to the Second Edition XXI

Preface to the Second Edition

The first edition of the textbook was appreciated by the teachers and students of many universities, engineering colleges and institutes, including IIT's throughout India. Words of appreciation were also received from faculty colleagues from Japan, China, Taiwan, Russia, Canada, South Korea, Pakistan, Bangladesh, Turkey, Iran, South Africa, Germany, France, United Kingdom, and United States of America. Students preparing for GATE/CSIR competitive examinations also suggested for more examples in the book and inclusion of topics of postgraduate level. The students very enthusiastically informed us about the utility of the book for the preparation of interviews for admission in PhD programmes at IITs and other universities (including foreign universities) or to get government jobs in India.

In view of all the above points, we have come up with the second edition of the book, where we have used simple language for explaining each and every topic. We have included more physical insight, wherever required. Some chapters are thoroughly revised in terms of new topics and solved problems. We have also updated advanced topics keeping in mind the research going on in these fields. The solutions to the Objective

Type Questions are also provided at the end of the book.

In particular, Chapter 4 includes details of the topic Population Inversion which covers various schemes for the same, i.e., two-level, three-level and four-level systems. In Chapter 5, a topic on Optical Fibres as a Dielectric Waveguide is included. After Chapter 7 on Waves and Oscillations, a new Chapter 8 on Simple Harmonic Motion and Sound Waves has been included that discusses standing waves, supersonic and shock waves, in addition to sound waves, Doppler effect and Lissajous figures. Chapter 9 on Sound Waves and Acoustics of Buildings has been thoroughly revised. In this chapter, Recording and Reproduction of Sound has been withdrawn and other topics are revisited. New topics on ultrasonics have been included which talk about production of ultrasonic waves and their absorption, dispersion, detection and applications. In Chapter 10 on Dielectrics, a topic Energy Stored in an Electrostatic Field is withdrawn as its concept is discussed in Chapter 11 on Electromagnetism. Moreover, details of Clausius-Mosotti equation are revised with the inclusion of physical insight of this equation. The chapter on Electromagnetism has been thoroughly revised. For example, Section 11.21 has been rewritten in order to make the readers understand which form of the Maxwell's equations is appropriate for free space, dielectric medium and conducting medium and how are these equations modified in these media. Bound charges and bound currents are also discussed. The solution to wave equation in conducting medium is included as Section 11.28.1, where dispersion relation, skin depth and phase relationship of the electric and magnetic field vectors are discussed. New solved problems, objective type questions and other practice problems are also included in order to provide an indepth knowledge on the electromagnetic fields and their propagation in different media.

In Chapter 12 on Theory of Relativity, physical insight to two interesting topics, viz. Length Contraction and Time Dilation is provided. Several new solved problems on various topics are also provided for the readers. Chapter 13 on Applied Nuclear Physics has been thoroughly revised and new topics are included on

XXII Preface to the Second Edition

basic properties of nucleus, nuclear forces, binding energy of nucleus, nuclear stability and various nuclear models, in addition to more equations and problems, both solved and unsolved. Introduction part of Chapter 16 on Quantum Mechanics has been revised. The topic on

Thermionic Emission (Section 17.7) has been shortened but significance of Richardson's equation is included. The earlier Chapter 21 on Photoconductivity and Photovoltaics has been withdrawn but its important topics, viz. photoconductivity, simple model of photoconductor and effect of traps, are included in Chapter 18 on Bond Theory of Solids and Photoconductivity.

The much important Chapter 22 on Nanophysics has been rewritten in view of recent advances in the field. Now, it is renamed as Nanoscience and Nanotechnology. Certain new topics are included to clarify how nanomaterials are different from bulk materials and to know the differences between nanoscience and nanotechnology. The chapter very systematically discusses the nanoscales in 1D, 2D, 3D and OD. Particu

larly, nanowires, carbon nanotubes, inorganic nanotubes, biopolymers, nanoparticles, buckyballs/fullerenes and quantum dots are discussed in detail along with the methods of their synthesis, properties and their applications. Finally, the applications, limitations and disadvantages of nanotechnology are also discussed.

The exhaustive OLC supplements of the book can be accessed at http://www.mhhe.com/malik/ep and contain the following:

For Instructors

- Solution Manual
- Chapter-wise Power Point slides with diagrams and notes for effective lecture presentations

For Students

- A sample chapter
- A Solved Question Paper
- · An e-guide to aid last minute revision need

We believe the readers shall find the second edition of the book more beneficial in terms of syllabus covered, quality of topics, large number of solved problems aimed at providing physical insight to various topics, and teaching various methods of solving difficult problems. The systematic approach adopted in the present book shall certainly help the teachers and students providing for crystal clear understanding of the topics and carrying out research in the related fields. This edition will be vital in enhancing the self confidence of our UG and PG students which will help them in advancing their careers.

Finally, we look forward to receive feedback from the teachers and students on the recent edition of the

H K Malik Ajay K Singh

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Piracy-related issues may also be reported.

Preface to the First Edition

Physics is a mandatory subject for all engineering students, where almost all the important elements of the subject are covered. Finally, these evolve as different branches of the engineering course. The book entitled Engineering Physics has been written keeping in mind the need of undergraduate students from various engineering and science colleges of all Indian universities. It caters to the complete syllabus for both—Physics-I and Physics-II papers in the first year Engineering Physics course.

The aim of writing this book has been to present the material in a concise and very simple way so that even weak students can grasp the fundamentals. In view of this, every chapter starts with a simple introduction and then related topics are covered with a detailed description along with the help of figures. Particularly the solved problems (compiled from University Question Papers) are at the end of each chapter. These problems are not merely numerical; many of them focus on reasoning and require thoughtful analysis. Finally, the chap

ters carry unsolved questions based on which the students would be able to test their knowledge as to what they have acquired after going through various chapters. A chapter-end summary and list of important formu lae will be helpful to students for a quick review during examinations. The rich pedagogy consists of solved examples (450), objective-type questions (230), short-answer questions (224) and practice problems (617). The manuscript has been formulated in such a way that students shall grasp the subject easily and save their time as well. Since the complete syllabus is covered in a single book, it would be highly convenient to both.

The manuscript contains 22 chapters which have been prepared as per the syllabus taught in various colleges and institutions. In particular, the manuscript discusses optics, lasers, holography, fibre optics, waves, acoustics of buildings, electromagnetism, theory of relativity, nuclear physics, solid state physics, quantum physics, magnetic properties of solids, superconductivity, photoconductivity and photovoltaic, X-rays and nanophysics in a systematic manner. We have discussed advanced topics such as laser cooling, Bose-Einstein condensation, scanning electron microscope (SEM), scanning tunnelling microscope (STM), controlled fusion including plasma, Lawson criterion, inertial confinement fusion (ICF), plasma based accelerators, namely, plasma wake field accelerator, plasma beat wave accelerator, laser wake field accelerator and self modulated laser wake field accelerator, and nanophysics with special emphasis on properties of nanoparticles, carbon nanotubes, synthesis of nanoparticles and applications of nanotechnology. These will be of interest to the teachers who are involved in teaching postgraduate courses at the universities and the students who opt for higher studies and research as their career. Moreover, a series of review questions and problems at the end of each chapter together with the solved questions would serve as a question bank for the students preparing for various competitive examinations. They will get an opportunity to learn the subject and test their knowledge on the same platform.

The structuring of the book provides in-depth coverage of all topics. Chapter 1 discusses Interference. Chapter 2 is on Diffraction. Chapter 3 is devoted to Polarization. Coherence and Lasers are described in

XXIV Preface to the First Edition

Chapter 4. Chapter 5 discusses Fibre Optics and its Applications, while Electron Optics is dealt with in Chapter 6. Chapter 7 describes Waves and Oscillations. Chapter 8 is on Sound Waves and Acoustics. Chapter 9 is on Dielectrics. Electromagnetic Wave Propagation is described in Chapter 10. Chapter 11 discusses the Theory of Relativity.

Chapter 12 is devoted to Nuclear Physics. Crystal Structure is described in Chapter 13. Chapter 14 deals with the Development of Quantum Physics, while Chapter 15 is on Quantum Mechanics. Chapter 16 discusses Free Electron Theory. Band Theory of Solids is explained in Chapter 17. Chapter 18 describes the Magnetic Properties of Solids. Chapter 19 is on Superconductivity. Chapter 20 explains X-rays in detail while Chapter 21 is on Photoconductivity and Photovoltaics. Finally, Chapter 22 discusses Nanophysics in great detail. The manuscript has been organised such that it provides a link between different topics of a chapter. In order to make it simpler, all the necessary mathematical steps have been given and the physical feature of the mathematical expressions is discussed as and when required.

The exhaustive OLC supplements of the book can be accessed at http://www.mhhe.com/malik/ep and contain the following:

For Instructors

- Solution Manual
- Chapter-wise Power Point slides with diagrams and notes for effective lecture presentations

For Students

- A sample chapter
- · Link to reference material
- Solved Model Question Paper
- Answers to objective type questions given in the book.

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Interference

After reading this chapter you will be able to

LO1 Explain interference through Young's double slit experiment

LO2 Describe the concept of wave and Huygen's principle

LO3 Illustrate phase and path difference LO4 Explain coherence, its various types and coherent sources

LO5 Discuss analytical treatment of interference and conditions for sustained interference

LO6 Examine multiple beam superposition and interference by division of wavefront and amplitude

LO7 Review engineering/scientific applications of interferences including homodyne and heterodyne detection

Introduction

You would have seen beautiful colours in soap films or patch of oil floating on the surface of water. Moreover, the colour gets changed when you watch it from different angles. Did you ever try to find out the reason? In scientific language, this takes place due to the phenomenon of interference. The phenomenon of interference of light tells us about the wave nature of the light. In optics, the interference means the superposition of two or more waves which results in a new wave pattern. Here, we are talking about the interaction of waves emerging from the same source or when the frequencies of these waves are the same. In the context of light, which is an electromagnetic wave, we say that when the light from two different sources moves in the same direction, then these light wave trains superimpose upon each other. This results in the modification of distribution of intensity of light. According to the principle of superposition, this is called the interference of light. More precisely the interference can be defined as the interaction between two or more waves of the same or very close frequencies emitted from coherent sources (defined later), where the wavefronts are combined according to the principle of superposition. The resulting variation in the disturbances produced by the waves is called the interference pattern. Thomas Young, in 1802, explained the interference successfully in his double slit experiment.

2 Engineering Physics

YOung's DOubLe sLit experiment



The phenomenon of interference may be better understood by taking two point light sources S_1 and S_2 which produce similar waves (Fig. 1.1). Let the sources S_1 and S_2 be at equal distances from the main source S while being close to each other. Since the sources emit waves in all the directions, the spherical waves first pass through S and then S_1 and S_2 . Finally these waves

expand into the space.

by dotted arcs. It is seen that constructive interference takes place at the points where the crests due to one source meet the crests due to another source or where their troughs meet each other. In this case. the resultant amplitude will be minimum. Therefore, due to the Sa the sum of the amplitudes of the intersection of these lines, an separate waves and hence the alternate bright and dark fringes intensity of the light will be maximum at these points. Similarly, at those points where sources S_1 and S_2 . These crests due to one source meet the troughs due to another source or vice-versa, the liaht. resultant amplitude will be the difference of the amplitudes of the separate waves. At these

The crests of the waves are represented by complete arcs and the troughs

points the intensity of the waves (or light) will be S are observed on the screen placed at the right side of the Figure 1.1 fringes are obtained due to the Screen phenomenon of interference of

COnCept Of Waves anD HuYgens' prinCipLe

A wave is a disturbance that propagates through space and time, usually with the transference of one point to another without any particle of the medium being permanently displaced. Under this situation, the particles only oscillate about their equilibrium positions. If the oscillations of the particles are in the direction of wave propagation, then the wave is called longitudinal wave. However, if these oscillations take place in perpendicular direction with the direction of wave propagation, the wave is said to be transverse in nature. In electromagnetic waves, such as light waves, it is the changes in electric and magnetic fields which represent the wave disturbance. The progress of the wave propagation is described by the passage of a waveform through the medium with a certain velocity called the phase velocity or wave velocity. However, the energy is transferred at the group velocity of the waves making the waveform.

The wave theory of the light was proposed in 1678 by Huygens, a Dutch scientist. On the basis of his wave theory, he explained satisfactorily the phenomena of reflections, refraction etc. In the beginning, Huygens' supposed that these waves are longitudinal waves but later he came to know that these waves are transverse in nature. Huygens' gave a hypothesis for geometrical construction of the position of a common wavefront at any instant when the propagation of waves takes place in a medium. The wavefront is an imaginary surface joining the points of constant phase in a wave propagated through the medium. The way in which the wavefront is propagated further in the medium is given by Huygens' principle. This principle is based on the following assumptions:

- (i) Each point on the given wavefront acts as a source of secondary wavelets.
- (ii) The secondary wavelets from each point travel through space in all the directions with velocity of light.
 - (iii) A surface touching the secondary wavelets tangentially in the forward direction at any given time constructs the new wavefront at that instant. This is known as secondary wavefront.

Interference 3

In order to demonstrate (Fig. 1.2a) or plane P_2 the Huygens' principle, we consider the

propagation of a spherical wavefront wavefront (Fig. 1.2b) in PP1 an isotropic (uniform)

medium (for example, ether) emerging from a source of light S. At

any time, suppose PQ is a section of the primary wavefront			2
drawn from the source S. To find the position of the wavefront		2	•
after an interval t, we take points 1, 2, 3, on the primary		0	3
wavefront PQ. As per Huygens' principle, these points act		3	
		4	4
as the source of secondary wavelets. Taking each point as		·	5
the centre, we draw spheres of radii ct, where c is the speed		-	3
of light. These spherical surfaces represent the position of		5	
		6	6
secondary wavelets at time t. Further, we draw a surface P_1Q_1 that touches tangentially all these secondary wavelets			
	Q_2		
in the forward direction. This surface P ₁ Q ₁ is the waves.			

secondary Q

pHase DifferenCe anD patH DifferenCe

 $\mathsf{Q_1}\mathsf{Q}\;\mathsf{Q_1}\;\mathsf{Q_2}$

wavefront. Another surface P₂Q₂ in the backward direction is not called the secondary wavefront as there is no backward flow of the energy during the propagation of the light





As mentioned, the interference pattern is obtained when the two or more waves superimpose each other. In order to understand this pattern it is very important to know about the path and phase differences between the interfering waves.

1.3.1 phase Difference

Two waves that have the same frequencies and different phases are known to have a phase difference and are said to be out of phase, with each other. If the phase difference is 180°, then the two waves are said to be in antiphase and if it is 0°, then they are in phase as shown in Fig. 1.3(a and b). If the two interfering waves meet at a point where they are in antiphase, then the destructive interference occurs. However, if these two waves meet at a point where they are in the same phase, then the constructive interference takes place.

1.3.2 path Difference

In Fig. 1.4, while the two wave crests are traveling a different distance from their sources, they meet at a point P in such a way that a crest meets a crest. For this particular location on the pattern, the difference in distance traveled is known as path difference.

4 Engineering Physics 1.3.3 Relation between Path	Suppose for a path difference of d the corresponding phase difference is f. Then it is S ₂ clear that	r ₁
Difference and	0.61	r_2
phase Difference	2p f d	d P
It is clear from the positions of crests or troughs of the waves that if the path difference between the two waves is equal to the wavelength I, the corresponding phase difference is 2p (360°).	S_1 = r_2 - r_1 (Path difference) $F_{igure} 1.4$	

Phase difference =
$${}^{2p}_{I}$$
 ¥ Path difference (i)

This can be made clearer with the help of Fig. 1.4, where two sources of waves S_1 and S_2 are shown. The wavelength of these sources is I and the sources are in phase at S_1 and S_2 . The frequencies of both the waves are taken to be the same as f. Therefore, the angular frequency w

= 2pf. They travel at the same speed and the propagation constant for them is $k = \frac{2p}{l}$. We can write the wave equations for both the waves at point P as

 $y_1 = a \cos(wt - kr_1)$ for the wave emerging from source S_1 and $y_2 = a \cos(wt - kr_2)$ for the wave emerging from source S_2

Here $(wt - kr_1)$ is the phase f_1 and $(wt - kr_2)$ is the phase f_2 . Therefore, the phase difference between them is $f_1 - f_2$, given by $f_1 - f_2 = wt - kr_1 - wt + kr_2 = k(r_2 - r_1)$.

Using Eq. (i) and k = $^{2p}_{I}$, the path difference is obtained as Path difference d = $r_2 - r_1$.

COHerenCe

Coherence is a property of waves that helps in getting stationary interference, i.e., the interference which is temporally and spatially constant. During interference the waves add constructively or subtract destructively, depending on their relative phases. Two waves are said to be coherent if they have a constant relative phase. This also means that they have the same frequency. Actually the coherence is a measure of the correlation that exists between the phases of the

wave measured at different points. The coherence of a wave depends on the characteristics of its source.

1.4.1 Temporal Coherence

Temporal coherence is a measure of the correlation between the phases of a wave (light) at different points along the direction of wave propagation. If the phase difference of the wave crossing the two points lying along the direction of wave propagation is independent of time, then the wave is said to have temporal coherence. Temporal coherence is also known as longitudinal coherence. This tells us how monochromatic a source is. In Fig. 1.5A, a wave traveling along the positive x-direction is shown, where two points A and B

are lying on the x-axis. Let the phases of the wave at these points at any instant t be f_A and f_{B_1} respectively, and at a later time $t\phi$ they be $f_A\phi$ and $f_B\phi$. Under this situation, if the phase difference $f_B - f_A = f f_{BA} \phi \phi$, then the wave is said to have temporal coherence.

Interference 5

x axis A B

Figure 1.5A

1.4.2 Spatial Coherence

Spatial coherence is a measure of the correlation between the phases of a wave (light) at different points transverse to the direction of propagation. If the phase difference of the waves crossing the two points lying on a plane perpendicular to the direction of wave propagation is independent of time, then the wave is said to have spatial coherence. This tells us how uniform the phase of the wavefront is. In Fig. 1.5B, a wave traveling along the positive x-direction is shown, where PQRS is a transverse plane and A and B are the two points situated on this plane within the waveforms. Let the waves crossing these points at any time t have the same phase f and at a later time $t\phi$ the phases of the waves are again the same but equal to $t\phi$. Under this situation, the waves are said to have spatial coherence.

Q
PS
AB
x axis x axis
R
Figure 1.5B

1.4.3 Coherence Time and Coherence Length

A monochromatic source of light emits radiation of a single frequency (or wavelength). In practice, however, even the best source of light emits radiations with a finite range of wavelengths. For a single frequency wave, the time interval over which the phase remains constant is called the coherence time. The coherence time is generally represented by Dt. In a monochromatic sinusoidal wave the coherence time is infinity because the phase remains constant throughout. However, practically the coherence time exists and the distance traveled by the light pulses during this coherence time is known as coherence length DL. The coherence length is also called

the spatial interval, which is the length over which the phase of the wave remains constant. The coherence length and coherence time are related to each other according to the following formula

DL = cDt



Two sources of light are said to be coherent, if they emit waves of the same frequency (or wavelength), nearly the same amplitude and maintain a constant phase difference between them. Laser is a good example of coherent source. In actual practice, it is not possible to have two independent sources which are coherent. This can be explained as follows. A source of light consists of large number of atoms. According to the atomic

6 Engineering Physics

theory, each atom consists of a central nucleus and the electrons revolve around the nucleus in different orbits. When an atom gets sufficient energy by any means, its electrons jump from lower energy level to higher energy level. This state of an atom is called an excited state. The electron lives in this state only for about 10⁻⁸ seconds. After this interval of time the electrons fall back to the inner orbits. During this process, the atoms radiate energy in the form of light. Out of the large number of atoms some of them emit light at any instant of time and at the next instant other atoms do so and so on. This results in the emission of light waves with different phases.

So, it is obvious that it is difficult to get sources. coherent light from different parts of the same Many Source Points Many Wavelengths Figure 1.6

1.5.1 Production of Coherent Light from Incoherent Sources

sources of light can never act as coherent

An ordinary light bulb is an example of an incoherent source. We can produce coherent light from such an incoherent source, though we will have to a lot of the light. If we use spatially filter the light coming from such source, we can increase the spatial coherence (Fig. 1.7). Further, spectrally filtering of the light increases the temporal coherence. This way we can produce the coherent light from the incoherent source.

Spatial Filter Spectral Filter

Coherent Light

Incoherent Source

Wavelength Filter

Pinhole

anaLYtiCaL treatment Of interferenCe

Let us consider the superposition of two waves of same frequency w and a constant phase difference f traveling in the same direction. Their amplitudes are taken as a_1 and a_2 , respectively. The displacement due to one wave at any instant is given by

 y_1 = a_1 sin wt (i) and the displacement due to another wave at the same instant is given by

$$y_2 = a_2 \sin (wt + f) (ii)$$

Interference 7

According to the principle of superposition, the resultant displacement (y_R) is given by $y_R = y_1 + y_2$ (iii) = $a_1 \sin wt + a_2 \sin (wt + f)$

= $a_1 \sin wt + a_2 \sin wt \cos f + a_2 \cos wt \sin f$

= $(a_1 + a_2 \cos f) \sin wt + a_2 \sin f \cos wt$ (iv) Assuming $a_1 + a_2 \cos f = A \cos q$ (v) $a_2 \sin f = A \sin q$ (vi) We obtain using Eq. (iv) – (vi)

 $y_R = A \sin (wt + q)$ (vii) On squaring and adding Eqs. (v) and (vi), we have $A^2 (\sin^2 q + \cos^2 q) = {}^2_2 a \sin^2 f + {}^2_1 a + 2a_1 a_2 \cos f + {}^2_2 a \cos^2 f$ $A^2 = {}^2^2$

a a $_{12}$ + (sin²f + cos²f) + 2a₁a₂ cos f (viii) The resultant intensity is therefore

given by

$$I = A^2 = 22$$

 $_{12}$ a a + + $_{2a_{1}a_{2}}$ cos f (ix)

The angle q can be calculated from Eqs. (v) and (vi) as

aa

1.6.1 Condition for Constructive Interference

It is clear from Eq. (ix) that the intensity, I will be maximum at points where the values of cos f are +1, i.e, phase difference f be 2np, with n = 0, 1, 2, 3, Then the maximum intensity is obtained from Eq. (ix) as $I_{max} = (a_1 + a_2)^2$ (xi) In other words, the intensity will be maximum when the phase difference is an integral multiple of 2p. In this case,

Thus, the resultant intensity will be greater than the sum of the individual intensities of the waves.

If
$$a_1 = a_2 = a$$
, then
$$I_{max} = 4a^2$$

1.6.2 Condition for Destructive Interference

It is clear from Eq. (ix) that the intensity I will be minimum at points where $\cos f = -1$. i.e., where

phase difference f = (2n + 1)p, with n = 0, 1, 2, 3,... Then Eq. (ix) gives

 $I_{min} = (a_1 - a_2)^2$ (xii) Therefore, it is clear that in destructive interference the intensity will be minimum when the phase difference f is an odd multiple of p.

If
$$a_1 = a_2$$
, then $I_{min} = 0$
8 Engineering Physics

If
$$a_1 \pi a_2$$
, then $I_{min} \pi 0$

$$22$$

$$min 1 2 I a a < +$$

Thus, in the case of destructive interference the resultant intensity will be less than the sum of the individual intensities of the waves.

Figure 1.8 represents the intensity variation with phase differences f graphically (for $a_1 = a_2 = a$).

1.6.3 Conservation of Energy

The resultant intensity due to the interference of two waves $a_1 \sin wt$ and $a_2 \sin (wt + f)$ is given by Eq. (ix), reproduced below

$$I = {}^{22}$$

$${}_{12}aa + 2a_{1}a_{2}\cos f$$

$${}_{12}aa + 2a_{1}a_{2} = (a_{1} + a_{2})^{2}$$
and $I_{min} = {}^{22}$

$${}_{12}aa + 2a_{1}a_{2} = (a_{1} + a_{2})^{2}$$

$${}_{12}aa + 2a_{1}a_{2} = (a_{1} - a_{2})^{2}$$

If
$$a_1 = a_2 = a$$
 then

Therefore, average intensity (Iav) will be obtained as

$$I_{av} = 2a^2$$

For unequal amplitudes a_1 and a_2 the average intensity would be 22

 $_{1\,2}$ () a a + . Thus, in interference only some part of energy is transferred from the position of minima to the position of maxima, and the average intensity or energy remains constant. This shows that the phenomenon of interference is in accordance with the law of conservation of energy.

interferenCe

COnDitiOns fOr sustaineD



interference, the following conditions must be satisfied

(i) The two sources should emit waves of the same frequency (wavelength). If it is not so, then the positions of maxima and minima will change with time.

Interference 9

- (ii) The waves from the two sources should propagate along the same direction with equal speeds.
 - (iii) The phase difference between the two interfering waves should be zero or it should remain constant. It means the sources emitting these waves must be coherent.
 - (iv) The two coherent sources should be very close to each other, otherwise the interference fringes will be very close to each other due to the large path difference between the interfering waves. For the large separation of the sources, the fringes may even overlap and the maxima and minima will not appear distinctly.
 - (v) A reasonable distance between the sources and screen should be kept, as the maxima and minima appear quite close if this distance is smaller. On the other hand, the large distance of the screen reduces the intensity.
 - (vi) In order to obtain distinct and clear maxima and minima, the amplitudes of the two interfering waves must be equal or nearly equal.
 - (vii) If the source is not narrow, it may act as a multi source. This will lead to a number of interference patterns. Therefore, the coherent sources must be narrow.
 - (viii) In order to obtain the pattern with constant fringe width and good intensity fringes, the sources should be monochromatic and the background should be dark.

1.7.1 Condition of Relative Phase Shift

This is regarding the introduction of additional phase change between the interfering waves when they emerge after reflecting from two different surfaces. In most of the situations, the reflection takes place when the beam propagates from the medium of lower refractive index to the medium of higher refractive index or vice-versa. When the reflection occurs with light going from a lower index toward a higher index, the condition is called internal reflection. However, when the reflection occurs for light going from a higher index toward a lower index, the condition is referred to as external reflection. A relative phase shift of p takes place between the externally and internally reflected beams so that an additional path difference of I/2 is introduced between the two beams. If both the interfering beams get either internally or externally reflected, no phase shift takes place between them.

muLtipLe beam superpOsitiOn

In Section 1.6, we have given theoretical analysis of the interference due to the superposition of two waves of the same frequency and the constant phase difference. The intensity of the interference pattern showed its dependence on the amplitudes of the interfering waves. However, now we consider a large number of waves of the same frequency and amplitude, which propagate in the same direction. The amount by which each wave train is ahead or lags behind the other is a matter of chance. Based on the amplitude and intensity of the resultant wave, we can examine the interference. We assume n number of wave trains whose individual amplitudes are equal (= a, say). The amplitude of the resultant wave can be understood as the amplitude of motion of a particle undergoing n simple harmonic motions (each of amplitude a) at once. In this case, if all these motions are in the same phase, the resultant wave will have an amplitude equal to na and the intensity would be n^2a^2 , i.e., n^2 times that of one wave. However, in our case, the phases are distributed purely at random, as shown in Fig. 1.9 as per graphical method of

compounding amplitudes. Here, the phases f_1 , f_2 , f_3 , ... take arbitrary values between 0 and 2p. The intensity due to the superposition of such waves can be calculated by the square of the resultant amplitude A. In order to find A^2 , we should square the sum of the

10 Engineering Physics

projections of all vectors a along the x-direction and add it to the square of the corresponding sum along the y-direction. The summation of projections along x-direction are given by the following expression

$$a(\cos f_1 + \cos f_2 + \cos f_3 + ... + \cos f_n)$$

$$y$$

$$f_3$$

$$A = 0$$

$$f_1$$

$$f_2$$

$$a$$

$$a$$

$$X$$

Figure 1.9

The square of quantity in the parentheses gives the terms of the form $\cos^2 f_1$, $2\cos f_1\cos f_2$, etc. It is seen that the sum of these cross product terms increases approximately in proportion to number n. So we do not obtain a definite result with one given array of arbitrarily distributed waves. For a large number of such arrays, we find their average effect in computing the intensity in any physical problem. Under this situation, it is safe to conclude that these cross product terms will average to zero. So we consider only the $\cos^2 f$ terms. Similarly, for the y projections of the vectors we obtain $\sin^2 f$ terms. With this we have

 $I^a A^2 = a^2(\cos^2 f_1 + \cos^2 f_2 + \cos^2 f_3 + ... + \cos^2 f_n) + a^2(\sin^2 f_1 + \sin^2 f_2 + \sin^2 f_3 + ... + \sin^2 f_n)$. Using the identity $\sin^2 f_p + \cos^2 f_p = 1$, the above expression reduces to $I^a a^2 Y^a = 1$. Since $A^a Y^a = 1$ is the intensity due to a single wave, the above relation shows that the average intensity resulting from the superposition of n waves with arbitrary phases is n times of a single wave. It means the resultant amplitude A increases in proportion with in length as n gets increased.

WavefrOnt

interferenCe bY DivisiOn Of

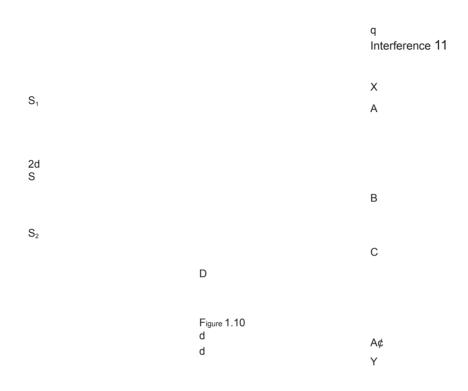


This method uses multiple slits, lenses, prisms or mirrors for dividing a single wavefront laterally to form two smaller segments that can interfere with each other. In the division of a wavefront, the interfering beams of radiation that left the source in different directions and some optical means is used to bring the beams back together. This method is useful with small sources. Double slit experiment is an excellent example of interference by division of wavefront. Fresnel's biprism is also used for getting interference pattern based on this method.

1.9.1 Fresnel's Biprism

Fresnel's Biprism is a device by which we can obtain two virtual coherent sources of light to produce sustained interference. It is the combination of two acute angled prisms which are joined

with their bases in such a way that one angle becomes obtuse angle q_c of about 179° and remaining two angles are acute angles each of about 1/2°, as shown in Fig. 1.10.



q¢

Let monochromatic light from slit S fall on the biprism, placed at a small distance from S. When the light falls on upper part of the biprism, it bends downward and appears to come from source S_1 . Similarly, the other part of the light when falls on the lower part of the biprism, bends upward and appears to come from source S_2 . Here, the images S_1 and S_2 act as two virtual coherent sources of light (Fig. 1.10). Coherent sources are the one that have a constant or zero phase difference throughout. In the situation, on placing the screen XY on right side of the biprism, we obtain an alternate bright and dark fringes in the overlapping region BC.

1.9.1.1 Theory of Fringes Let A and B be two virtual coherent sources of light separated by a distance 2d.

The screen XY, on which the

fringes are obtained, is

separated by a distance D from point C is zero. Thus the point the two coherent sources, as C will be the centre of a bright shown in Fig. 1.11. The point C fringe. On both sides on the screen is equidistant from A and B. Therefore, the path difference between the two waves from sources A and B at

A of C, alternately bright and dark of C, alternately bright and dark fringes are produced. S the screen from the Draw perpendiculars central bright fringe at C
$$\frac{NP = x_n - d}{In \text{ right angled DANP}}$$
, $\frac{AN}{A}$ and BM from A and be $\frac{A}{A}$. B on the screen. Let the From geometry, we distance of a point P on have $\frac{A}{A}$ $\frac{AN}{A}$ $\frac{AN}{A$

$$AP^2 = AN^2 + NP^2 (i) = D^2 + (x_n - d)^2$$

12 Engineering Physics

$$\dot{E} = \int_{1}^{\infty} \cdot \dot{P} + \dot{P} = \int_{1}^{2} \cdot \dot{P} = \int_{1}^{2} \cdot \dot{P} + \dot{P} = \int_{1}^{2} \cdot \dot{P} = \int_{1}$$

Similarly, in DBMP,

$$x d BP D$$

$$D^+$$

$$= + (iii) 2$$

Hence, the path difference between the waves reaching via AP and BP paths at the point P

on the screen
2
 2 1 1 () ()
$$\dot{E} \ddot{E} + D = - = - \int_{\dot{I} \cdot \dot{I}} + \dot{I} \cdot \dot$$

Condition for Bright Fringes: In order to interfere constructively and produce bright fringes, the two rays should arrive at points P in phase. This is possible if the path difference is an integral multiple of I. Therefore,

D

D = nI
$$2 \\ d_x$$

$$D = nI \text{ where } n = 0, 1, 2 \dots$$

$$x |_{d} = (v)$$

$$x |_{d} = (v)$$

$$2^n$$

Here it may be recalled that x_n is the distance of the n^{th} order bright fringe from the central maxima. The distance of the next $(n + 1)^{th}$ maximum from the point C can be calculated by replacing n by n + 1 in equation (v). Therefore,

$$(1)_{2}^{n}_{D}$$
 $x n_{d}$

The separation between two consecutive maxima gives the fringe width b,

as follows b =
$$x_{n+1} - x_n$$

or fringe width

$$b = (vi)D$$

Condition for Dark Fringes: In order to interfere destructively and produce dark fringe at point P, the two rays should arrive at this point in out of phase (phase difference of p). This is possible, if the path difference is an odd multiple of $\frac{1}{2}$. Therefore,

$$D = {1 \over n_1} \hat{E}_{\hat{A}}^{\hat{A}} + \dot{E}_{\hat{A}}^{\hat{A}}, \text{ where } n = 0, 1, 2, ...$$

From Eq. (iv)

$$D = x + (vii)^{2(21)} 2^{n}$$

$$d_{xn}$$

$$D$$

$$(21)$$

$$n D$$

$$x_{d}$$

Equation (viii) gives the distance of n^{th} order dark fringe from the point C. The distance of the next $(n+1)^{th}$ minimum from the point C will be

Hence, the fringe width between two consecutive minima

2 d

It is clear from Eqs. (vi) and (x) that the bright and dark fringes are of equal width. 1.9.1.2 Experimental Method for Determination of Wavelength of Light

The experimental setup used for the determination of wavelength of light consists of a good quality heavy optical bench of about 1.5 meter length fitted with scale. It has four uprights that carry an adjustable slit S, a biprism, a convex lens and a micrometer eyepiece, respectively. These components are shown in Fig. 1.12. Each upright can be moved along the length of the optical bench and screws are provided to rotate the slit and biprism in their own planes and the eyepiece can also move at right angle to the length of the optical bench.

To obtain well defined and sharp interference fringes, the following adjustments are necessary: (i) Labeled optical bench by using spirit level and leveling screws.

- (ii) Adjust all uprights to the same height.
- (iii) Illuminate the vertical slit by monochromatic source of light. Make the slit narrow.
- (iv) Now place the biprism on the second upright and try to adjust its edge parallel to the slit until two equally bright virtual sources A and B are observed.
- (v) Shift the micrometer eyepiece on the bench away from the slit and also move it at right angle to the length of optical bench until the fringes are observed in the field of view.
- 14 Engineering Physics
- (vi) In order to get fine fringes, change the position of the biprism slowly in its own plane such that its edge remains parallel to the slit.



Figure 1.12

Lateral shift and its removal: On moving the micrometer eye piece on the bench towards the biprism, if the fringes appear to shift at right angle to the optical bench then it is known as lateral shift (Fig. 1.13(a)). However, if the principle axis and axis of optical bench become parallel, then no lateral shift remains, as shown in Fig. 1.13(b).

Axis of Optical Bench

1.9.1.3 Determination of Distance between Two Virtual Coherent Sources

For measuring 2d, a convex lens of short focal length is placed between the biprism and the micrometer eye piece. This distance between the biprism and the micrometer eye piece is more than 4 times of the focal length of the convex lens. By moving the lens we obtain two positions L_1 and L_2 of the convex lens such that two separated images d_1 and d_2 of the two coherent sources respectively can be observed, as shown in Fig. 1.14.

For the first position of lens, L₁, the magnification is given as

$$v d$$

$$1$$

$$u d = (i)$$

and for second position of the lens, the magnification is

$$u d$$
 $v d = (ii)2$

Interference 15

Then from Eqs. (i) and (ii), we get

Therefore, the measurement of positions of images d_1 and d_2 will determine the distance 2d between the sources. The wavelength I of monochromatic light can be calculated when we substitute the values of b, D and 2d in the formula I = b(2d/D), derived in the previous section.

1.9.1.4 Determination of Thickness of Thin Transparent Sheet (Displacement of Fringes)

and partly was originally at Co shifts to Let A and B be two virtual another position P, as shown in coherent sources of light. The Fig. 1.15. point Co on the screen is t equidistant from both the sources (Fig. 1.15). When a X_n transparent material plate G of thickness t and having refractive G index m, it is placed in the path A of one of the light wave, we The time taken by the light wave observe that the fringe which from A to P partly through air

through the plate is the same as the time taken by the other light wave from B to P in air. If c and v be the velocity of light in air and in the plate, B respectively, then

$$\begin{array}{ccc} & & & & & & \\ & -m & & & & \\ \text{or} & = + & & & & \\ \text{BP AP t t} & & & m & & \\ \end{array} \begin{array}{c} \text{C C C} \\ \text{or BP = (AP - t) + mt} \\ \text{E} \ \tilde{} = \text{I} \ \tilde{} \cdot \text{Q V} \end{array}$$

or BP - AP = (m - 1)t (i) Here BP - AP is the path difference between the two interfering waves.

С

 C_0

Figure 1.15

If the point P is originally occupied by the n^{th} order bright fringe, then the path difference between the two interfering waves will be

$$BP - AP = nI,$$

$$(m-1) t = nI (ii)$$

16 Engineering Physics

The distance x_n through which the fringe is shifted to point P from the central maximum C_0 is

given by
$${}_{d}^{X}I = (iii)$$

n D

 2^{n} where,

$$_{2}^{D}d$$
 $_{3}^{I}=b=fringe width.$

From Eq. (iii), we get

$$2 {\atop 0}^{x} {\atop 0}^{x}$$
n

DI ${\atop 0}^{0}$ = (iv) From Eqs. (ii) and (iv), we get

Therefore, by knowing x_n , 2d, D and m, we can calculate thickness t of the glass plate by using Eq. (v).

ampLituDe

interferenCe bY DivisiOn Of

The method, which is used to produce two coherent sources from a common source, is called division of amplitude that maintains the same width but reduced amplitude. After following different paths the two waves of reduced amplitudes are combined to produce an interference pattern. In this method, the interfering beams consist of radiation that has left the source in the same direction. This radiation is divided after leaving the source and later combined to produce interference. This method can be used with extended sources. Michelson interferometer is an example of interference by division of amplitude. Thin films are also used for getting interference pattern based on this method.

1.10.1 Interference Due to Thin Films

This is clear that the interference takes place when the two waves superimpose each other after traveling some distance, i.e., when there is a path difference between them. Since the thin film has its two surfaces, the

waves reflected from these surfaces can attain a path difference and can interfere. The same may be applied on the waves that transmit through the film.

$$A_{M}^{C}$$
 E Air

thickness r along BF at t and a refractive index r r 1.10.1.1 Thin Film of m. A ray of light AB t (90 - i) H Uniform Thickness incident t _r r at an angle i on the Film upper surface of the film $(\mu > 1)$ is partly reflected along r r Consider a uniform BC and partly refracted _D transparent film having

an angle r. At point F the wave BF is again partly

G F

Air

reflected from the second surface along FD and partly

Interference 17

```
The path difference between the reflected rays
```

$$D = (BF + FD)_{in film} - (BM)_{in air}$$

$$D = m (BF + FD) - BM$$

$$Q BF = FD$$

$$D = 2 mBF - BM (i) In the right angled DBFH,$$

$$cos or = tt r BF$$

$$BF r (ii) and tan or = tan = BH r BH tr$$

$$t$$

$$BD = 2 ¥ BH$$

$$BD = 2t tan r (iii) In the DBMD,$$

$$sin or = sin BM i BM BD i$$

$$BD = 1$$

\BM = 2t tan r sin i (iv) From Eqs. (i), (ii) and (iv), we get

22 tan sin

cos
or sin = sin

$$iir_{r} m m = (vi)$$

sin

$$\sqrt{2} \sin 2^{2} 2 \sin [1 \sin]$$

$$\begin{array}{c} m m \\ D = - = -m \\ trt \\ trr \\ rrr \\ cos cos cos \\ \end{array}$$

 $D = 2mt \cos r \text{ (vii)}$

Equation (vii) represents only the apparent path difference and does not represent the effective total path difference. When the light is reflected from the surface of an optically denser medium in case of rad BC, a phase change of pa equivalent to path difference of I/2 is introduced. Therefore, the total path difference between BC and DE will be

$$D = 2mt \cos r + I/2 \text{ (viii)}$$

Condition for Maxima: To have a maximum at a particular point, the two rays should arrive there in phase. So the path difference must contain a whole number of wavelength, i.e.,

$$D = nI$$
, $n = 0, 1, 2...$, (ix) From Eq. (viii) and (ix), we get

$$2mt \cos r + I/2 = nI$$
$$2mt \cos r = nI - I/2$$

 $2mt \cos r = (2n - 1)I/2 (x)$

18 Engineering Physics

Condition for Minima: To have a minimum at a particular point, the two rays should arrive there in out of phase (odd multiple of p) for which the path difference must contain a half odd integral number of wavelength, i.e,

$$\begin{array}{ccc}
 & 1 & \\
 & \hat{E}_{-} \hat{D} = & + \\
 & \hat{A}_{-} & \stackrel{.}{E}_{-} (xi) 2
\end{array}$$

Using Eq. (viii), we obtain

It should be noted that the interference pattern will not be perfect because the intensities of the rays BC and DE are not the same and their amplitudes are different.

In order to obtain the interference between the transmitted waves, we calculate the path difference between the waves, FK and GL as under

$$D = (FD + DG)_{in film} - (FJ)_{in air}$$
$$D = m[FD + DG] - FJ$$

QFD = DG

$$\D = 2mFD - FJ (xiii)$$
 DItt

In DFDI, cos or cos

$$FD FD r = = = (xiv) FI FI r FI t r$$

and tan or tan

FG = 2t tan r (xv) In right angled DFJG,

\FJ = 2t tan r sin i (xvi) From Eq. (xiii), (xiv) and (xvi), we get

tri 2 sin ^{sin} 2 sin

 $^{\rm m}$ $_{\rm m}$ $_{\rm m}$

cos cos sin

Since these two waves are emerging from the same medium, the additional phase difference (or path_difference) will not be introduced. Therefore, the total path difference

D = 2mt cos r (xvii) Condition for Maxima: As discussed, it is possible when

D = nl (xviii) Interference 19

From Eqs. (xvii) and (xviii), we get

2mt cos r = nl where, n = 0, 1, 2, 3, ... (xix) Condition for Minima: For obtaining minimum intensity, we should have

which gives $2mt \cos r = \frac{1}{2}$

$$n_{\parallel} \hat{E}_{-} \hat{A}^{-} + \ddot{E}_{-} = 0, 1, 2, 3, ...(xx)$$

Thus, the conditions for interference with transmitted light are obviously opposite to those obtained with reflected light. Hence, if the film appears dark in the reflected light, it will appear bright in the transmitted light and vice-versa. This shows that the interference pattern in the reflected and transmitted lights are complimentary to each other.

(i) Necessity of an Extended Source of Light for Interference in Thin Films

When a thin transparent film is exposed to white light and seen in the reflected light, different colours are seen in the film. These colours arise due to the interference of the light waves reflected from the top and bottom surfaces of the film. The path difference between the reflected rays depends upon the thickness t, refractive index m of the film and the angle q of inclination of the incident rays. The light which comes from any point from the surface of the film will include the colour whose wavelength satisfies the equation $2mt \cos r = (2n - 1) \frac{1}{2}$ and only this colour will be present with the maximum intensity in the reflected light.

When the transparent film of a large thickness as compared to the wavelength of the light, is illuminated by white light, the path difference at any point of the film will be zero. In the case of such a thick film, at a given point, the condition of constructive interference is satisfied by a large number of wavelengths, as << t. The condition of destructive interference is also satisfied at the same point for the large number of wavelengths. Therefore, consequently that point receives an average intensity due to the light of all wavelengths and no colours are observed.

In the context of realization of above phenomena it is always needed to use a broad power of light that will enable the eye to see whole of the film simultaneously.

If we use a point source, then we observe that different parts of reflected light cannot reach the eye due to small size of the pupil, as shown in Fig. 1.17(a). The reflected rays only from a small portion of the film can enter the eye. Hence, the whole of the film cannot be seen by the eye placed in a fixed position. However, if a

Extended Source Eye Eye

Point Source

0

(a) (b)

Figure 1.17

20 Engineering Physics

broad source of light is used to illuminate a thin film, the light reflected from each part of the film reaches the eye placed in a fixed position, as shown in Fig. 1.17(b). Hence, one can seen the entire film simultaneously by employing an extended source of light.

1.10.1.2 Non-uniform Thickness Film (Wedge Shaped Film)

Consider two plane surfaces OM and OM¢ inclined at an angle q enclosing a wedge shaped air film of increasing thickness, as shown in Fig 1.18. A beam of monochromatic light is incident on the upper surface of the film and the interference occurs between the rays reflected at its upper and lower surfaces. The interference occurs between the reflected rays BK and DL, both of which are obtained from the same incident ray of light AB.

i t
r
A r+q (r+q) M¢
B
ii
E
D
N
qr
(r+q) C H M

The path difference between the two reflected rays

$$D = [BC + CD]_{in film} - [BE]_{in air}$$
$$D = m(BC + CD) - BE$$

QCD = CI

$$D = m(BC + CI) - BE$$

= mBI - BE

= m(BN + NI) – BE (i) In right angled DBED,

sin BE i BD = (ii) Interference 21

In right angled DBND,

or BE = mBN (iv) From Eqs. (i) and (iv), we get

$$D = m(BN + NI) - mBN$$

or D = mNI (v) In right angled DDNI,

$$cos()$$
 $+ = q$

$$cos() or 2 cos() r NI r NI t r$$

+ = = + q q (vi) DI

From Eqs. (v) and (vi), we get

 $D = 2mt \cos(r + q)$ (vii)

Equation (vii), in the case of reflected light, does not represent the effective total path difference, as a phase difference of p (Stokes phase change) has been introduced through the reflection of wave BK. Therefore, the total path difference between the reflected rays,

$$D = 2mt cos(r + q) + I/2 (viii)$$

Equation (viii) shows that the path difference D depends on the thickness t. However, t is not uniform and it is different at different positions.

$$D = 1/2$$

which is the condition for darkness. Therefore, the edge of the film appears to be dark. This is called zero order band.

For normal incidence, i = 0 and r = 0. Then, the path difference

D = 2mt cos q + 1/2 (ix) Condition for Maxima: As explained earlier, the constructive interference takes place when D = nl where, n = 0, 1, 2, 3, (x) From Eqs. (ix) and (x), we get

 $2mt \cos q + I/2 = nI$

$$2mt \cos q = (2n - 1) \frac{1}{2} (xi)$$

22 Engineering Physics

Condition for Minima: In order to get destructive interference, the path

difference 1

$$n_{i} = \hat{A}^{-} + = (xii)$$

For normal incidence of the light waves or a parallel incident beam, the incident angle remains constant and hence the angle of refraction. If the light is monochromatic, then I is also fixed. Therefore, the change in path difference will take place due to mt or thickness t of the film only. As we move outwards from the point of contact O, the thickness of the film increases. However, at a particular place along a line parallel to the edge, t has only one value. Since the locii of the points of constant thickness of the film are straight lines parallel to the edge, straight bright and dark fringes parallel to the edge will be formed in the reflected light. If we use the white light in place of monochromatic light, coloured fringes will be observed.

(ii) Derivation for Fringe Width

For a wedge shaped film the conditions of maxima and minima are reproduced below. 2mt cos (r + q) = (2n - 1)I/2

$$2mt \cos(r + q) = nI$$

For normal incidence and small values of q the above conditions read as

2mt = (2n - 1)I/2 (xiv) and 2mt = nI (xv) If points A and C (Fig. 1.19) represent positions of two consecutive dark

fringes corresponding to film thicknesses AB = t_1 and CD = t_2 respectively,

then the fringe width (w) will be equal to BE. Now from Eq. (xv), we get

q Ε

В

D

the following condition corresponding to the points A and C.

$$2mt_1 = nI$$
 and $2mt_2 = (n + 1)I$ or $2m(t_2 - t_1) = or 2(CD - AB) = I$

A C Figure 1.19

or 2(DE) = I(xvi) But tan q = DE/BE or DE = BE tan q(xvii) From Eqs. (xvi) and (xvii), we get $2m(BE \tan q) = I$

or 2 tan

For smaller values of q, tan q; q and we get

$$\frac{I}{w \, mq} = (xviii) 2$$

Interference 23

It is clear from (xviii) that the fringe width w is independent of thickness t for smaller angle q. Therefore the fringes are equally spaced and of same width for fixed I, m and q.

1.10.2 Newton's Rings

If a plano-convex lens is placed such that its curved surface lies on a glass plate, then an air film of gradually increasing thickness is formed between the two surfaces. When a beam of monochromatic (single wavelength) light is allowed to fall normally on this film and viewed as shown in Fig. 1.20, an alternating dark and bright circular fringes are observed. These circular fringes are formed because of the interference between the reflected waves from the top and the bottom surfaces of the air film. These fringes are circular since the air film has a circular symmetry and the thickness of the film corresponding to each fringe is same throughout the circle. The interference fringes so formed were first investigated by Newton and hence known as Newton's rings.

The path difference between the two reflected rays, can be obtained as done in the case of wedge shaped film. It is reproduced below as

D = 2mt cos (r + q) + 1/2 (i) Where (1/2) is due to Stokes phase change.

Μ

45°

S

Plano-Convex Lens

O Figure 1.20
Glass Plate P Air Film

For normal incidence and an air film, i = 0, r = 0, m = 1. In addition, if q is also very small, then cos q = 1. Under this situation, the path differences becomes

$$_{t}^{I}D = + (ii)^{2}2$$

Here t is the thickness of the air film at a particular point.

At the point of contact, t = 0

which is the condition of minimum intensity and hence, the central spot of the ring will be dark. 24 Engineering Physics

Condition for Maxima: For constructive interference

1

or $2t = (2n - 1) {1 \choose 2}$ where n = 0, 1, 2, 3... (iv) Condition for Minima: For destructive interference

or 22

or
$$2t = nl$$
 where $n = 0, 1, 2, 3... (v)$

Diameter of Dark and Bright Rings: Let us consider the thickness of the air film at point Q as t and r, as the radius of the fringe at that point together with R as the radius of curvature of the lens (Fig. 1.21).

Hence, OC = CQ = R, HQ =
$$r_n$$
 HC = R - t

In right angled DCHQ

 $CQ^2 = CH^2 + HQ^2$
 $R^2 = (R - t)^2 + \frac{2}{n}r$

or $\frac{2}{n}r = 2Rt - t^2$

Figure 1.21

In actual practice, R is quite large and t is very small. Therefore, t^2 may be neglected in comparison with $2Rt \setminus_n^2 r = 2Rt$

or $^{2}_{n}$ r = R \forall 2t (vi) For Bright Rings: From Eq. (iii), we get

When we put this value of 2t in Eq. (vi), we get

or

١

The above equation gives the diameter D_n of n^{th} order bright



μ (viii)

Interference 25

Thus the diameter of the bright circular fringe(s) is proportional to the square root(s) of the odd natural numbers.

For Dark Rings: Applying the condition 2t = nI for the dark rings, Eq. (vi)

$$_{n}r = nIR.$$

or
$$^2D_n = 4nIR$$

 $\ \ D_n \mu$ (ix) Thus the diameter D_n of dark circular fringe(s) is proportional to the square root(s) of the natural numbers. 1.10.2.1 Determination of Wavelength of Light

We have seen that the diameter of nth order dark fringe in Newton's rings method is 2 4 D n R $_n$ = I (x) From the above relation, the diameter of (n + p)th order dark fringe can be written as 2

() 4() D n p R
$$_{n p +}$$
 = + I (xi) Subtracting Eq. (x) from equation (xi), we get D D p R () $_{-}$ = 4 I

Therefore, the measurement of diameters of the n^{th} and $(n + p)^{th}$ dark fringes together with the radius of curvature of the lens gives us the wavelength of sodium light with the help of above formula.

1.10.2.2 Determination of Radius of Curvature of Plano Convex Lens

This is clear from the theory of Newton's rings that the measurement of diameters of n^{th} order and $(n + p)^{th}$ order dark fringes play an important role in the determination of wavelength of monochromatic light. For this purpose, the following relation is used

Therefore, if we use the monochromatic source of light of known wavelength, it would be possible to determine the radius of curvature of the plano convex lens with the help of following formula 22

1.10.2.3 Determination of Refractive Index of a Liquid

The liquid whose refractive index is to be determined is placed between the lens and the glass plate and then we evaluate the diameters of the dark fringes.

The diameter of nth order dark fringe in air film is given by

2
4 D n R $_{n}$ = I

26 Engineering Physics

Similarly, the diameter of nth order dark fringe in liquid film

would be
4
 [] n R n D m =

where m is the refractive index of the liquid and $D_{liquid} < D_{air}$

Therefore, the refractive index of the liquid can be calculated from the following formula once we are able to determine the diameters of dark fringes.

n liquid becomes

1.10.2.4 Newton's Rings in Transmitted Light

D = 2t (ii)

Newton's rings can be observed in reflected as well as in transmitted light. Figure 1.22 shows that the rays QA and HRB are the transmitted rays, which interfere. From the figure it is also clear that the ray QA suffers no reflection at a medium of higher index, so its phase does not change. However, the ray HRB encounters two reflections at the denser medium at Q and H. OQ Since a phase change of p occurs at each reflection, the total phase change due to both R reflections would be 2p. Therefore, there will not Transmitted be any phase shift. In view of this, the path difference between the two transmitted rays QA and HRB would be

D = 2mt cos(r + q)(i)

ВА

Figure 1.22

For air (m = 1), normal incidence (r = 0) and smaller angle $q(\cos q = 1)$, the path difference

The above equations shows that at t = 0, the path difference between the two transmitted rays D = 0. Therefore, at the centre, the bright fringe will appear.

From Eq. (ii), the conditions for maxima and minima can respectively be obtained as below 2t = nl, n = 0, 1, 2, ... (iii) 2t = (n + 1/2)l, n = 0, 1, 2, ... (iv)

Because of the same reason as discussed earlier, the fringes in the transmitted light will also be circular. The diameter of bright circular fringes can be obtained as

Thus the diameter of the bright fringes is proportional to the square root of natural numbers. When we calculate the diameter of dark circular fringes, it comes out to be



This relation shows that the diameter of the dark fringes is proportional to the square root of odd natural numbers.

Interference 27

From the above relation, it is clear that the fringes observed in the transmitted light are exactly complementary to that of the reflected light. These fringes are much poorer in contrast as the transmitted rays emerge with lower intensity in comparison with the reflected rays. The Newton's rings obtained in the reflected as well as in the transmitted light are shown in Fig. 1.23a and b, respectively.

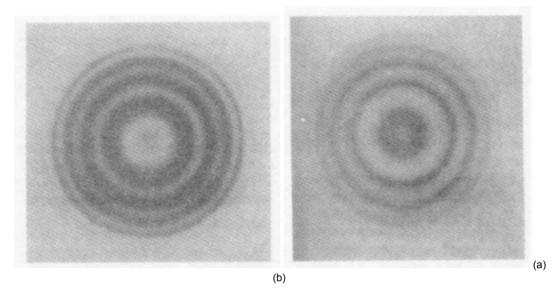


Figure 1.23

```
1.10.2.5 Newton's Rings formed between Two Curved Surfaces
```

enclosed between the formed and can be Let us consider two curved surfaces of radii two curved surfaces seen with a Air film (Fig. 1.24). In this of curvature R₁ and R₂ arrangement also, dark in contact at the point and bright rings are Q O. A thin air film is geometry, 22 traveling microscope. rrPT QT RR The thickness of the air film at P is $\frac{O T}{r_n}$ Figure 1.24 PQ = PT - QT

If the radius of n^{th} dark ring be r_n , then from

and 22 1222 = \ rrPQ RR 22 12

If we assume the thickness of the film as t, then

Now, this is clear from Fig. 1.24 that this type of film is similar to the wedge shaped film. Therefore, the path difference between the wave reflected from the upper and lower surfaces of the film would be

28 Engineering Physics

For air (m = 1), normal incidence (r = 0) and the smaller angle q, the path difference

takes the form tl

Therefore, in case of reflected light, for nth dark fringes

or 2t = nI

or ¹²2

or Î

1 1

r n n $_{n}$ where = 0, 1, 2, 3... R RI $\stackrel{\dot{E}}{=}$ = $\stackrel{\dot{I}}{\hat{I}}$ $\stackrel{\circ}{\circ}$ (i)

Similarly, for nth bright fringe the path difference should satisfy the following

condition I

$$t n_{\parallel} \hat{E}^{\hat{}} = A^{-\hat{}} \dot{E}^{-\hat{}}$$

$$11 (21)$$

$$n_{\parallel} R_{\parallel}$$

$$\dot{E}^{-1} = \hat{I}^{\hat{}} \text{ where } n = 0, 1, 2, 3... (ii) 2$$

2 ⁿ

Thus, bright and dark fringes are obtained according to Eqs. (i) and (ii). The diameter of the fringes can also be calculated.

```
Now we invert the lower surface PQ = PT + QT
                                                                             Air film
of the film. Under this
                                                                             Р
R₁
situation, the film would appear
                                                                             Т
thicker than the previous case
                                                                             m = 1
(Fig. 1.25). The film thickness
PQ in this case would be
                                      rrt<sub>RR</sub>
= +
                                                        2t = nI (for air)
1222
                                                       11
For the reasons explained in wedge-shaped
                                                       R<sub>2</sub>Q r<sub>2</sub>
film, the following condition should be
                                                       Figure 1.25
satisfied in order to obtain nth order dark
fringe of radius r<sub>n</sub>
                       R RI + = Í · ĵ ·
                  or 2
                       2 n r n 12
                      R RI \dot{E}_{+}^{-} = \dot{I}_{-}^{+} where n = 0, 1, 2, 3... (iii) 2
                         <sub>n</sub>r n 12
```

Interference 29

For nth bright fringe

A comparison of Eq. (i) with Eq. (iii) reveals that the diameter of dark fringes in the second case, where below curved surface looks like convex when viewed from above, would be smaller than

the one in first case. This effect is similar to the situation as if we increase the width or thickness of the film. The same is the case for bright fringes.

1.10.3 Michelson's Interferometer

It consists of two highly polished mirrors M_1 and M_2 and two plane glass plates P and Q parallel to each other, as shown in Fig. 1.26. The glass plate P is half-silvered on L

glass plate Q is such that S P and Q are of equal thickness and of the same material.

 $M_1 M \phi_2 45^{\circ}$

its back surface and inclined at an angle of 45° to the beam of incident light. Another

Two plane mirrors M₁ and M₂ are silvered on their front

Q

0

 M_2

surfaces and mounted on two arms at right angle to each

other. The position of the mirror M_1 can be changed with the help of a fine screw.

Т

Light from a monochromatic source S, rendered parallel by a lens L, falls on the glass plate P. incident light beam into two parts of The semi-silvered plate P divides the Figure 1.26

nearly equal intensities, namely reflected and transmitted beams. The reflected beam moves towards mirror M_1 and falls normally on it and hence it is reflected back to P and enters the telescope T. The transmitted beam moves towards mirror M_2 and falls normally on it after passing through the plate Q. Therefore, it is reflected by the mirror M_2 and follows the same path. At P it is reflected to enter the telescope T. Since the beams entering the telescope have been derived from the same incident beam, these two rays are capable of giving the phenomenon of interference; thereby producing interference fringes.

Function of Plate Q: The beam going towards the mirror M_1 and reflected back, crosses the plate P twice, while the other beam in the absence of Q would travel wholly in air. Therefore, to compensate the additional path, the plate Q is used between the mirror M_2 and plate P. The light beam going towards the mirror M_2 and reflected back towards P also passes twice through the compensation plate Q. Therefore, the optical paths of the two rays in glass are the same.

Types of Fringes: The fringes in Michelson interferometer depend upon the inclination of M_1 and M_2 . Let $M_2\phi$ be the image of M_2 formed by the reflection at the half-silvered surface of the plate P so that $OM_2 = OM_2\phi$. The interference fringes may be regarded as formed by the light reflected from the surfaces of M_1 and $M_2\phi$. Thus, the arrangement is equivalent to an air-film enclosed between the reflecting surfaces M_1

and M2¢.

30 Engineering Physics

It is obvious that the path difference between the two beams produced by the reflecting surfaces M_1 and $M_2\phi$ is equal to the twice of the thickness of the film $M_1\,M_2\phi$. This path difference can be varied by moving M_1 backwards or forward parallel to itself. If we use monochromatic light, the pattern of bright and dark fringes

will be formed. Here the shape of the fringes will depend upon the inclination of M_1 and M_2 . If M_1 and M_2 are exactly at right angles to each other, the reflecting surfaces M_1 and $M_2 \phi$ are parallel and hence air film between M_1 and $M_2 \phi$ is of constant thickness t so that we get circular fringes of equal inclination. These fringes are called as Haidinger's fringes that can be seen in the field view of a telescope. When the distance between the mirrors M_1 and M_2 or between M_1 and $M_2 \phi$ is decreased, the circular fringes shrink and vanish at the centre. A ring disappears each time when the path 2t decreases by I.

Since the vertical ray first gets reflected from the inner surface of P (internal reflection), and then from the front surface of the mirror M_1 (external reflection) a phase change of p takes place. The horizontal ray first gets reflected from the front surfaces of M_2 (external reflection) and then from the inner surface of glass plate P (external reflection), so there is no phase change. Therefore, the total path difference for normal incidence would be

$$\begin{array}{c}
1 \\
t D = + q \\
2 \cos_2
\end{array}$$

For bright fringes, the following condition should be satisfied

1 2
$$\cos_2$$

 $t \neq 0$ $\int_0^2 f^2 = \int_0^2 f^2$

$$2t\cos q = nI^{1}2$$

$$n_{\dot{I}} \dot{E}_{\dot{A}} \dot{E}_{\dot{A}} D = \dot{A}_{\dot{A}} + \dot{I} \dot{E}_{\dot{A}} \dot{E}_{\dot{$$

When t is further decreased, a limit is attained where M_1 and $M_2\phi$ coincide and the path difference between the two rays becomes zero. Now the field of view is perfectly dark. When M_1 is further moved, the fringes appear again.

If M_1 and M_2 are not perfectly perpendicular, a wedge shaped film will be formed between M_1 and M_2 ¢ then we get almost straight line fringes of equal thickness in the field of view of telescope, as the radius of fringes is very large.

All the above discussed films are shown in Fig. 1.27.

(a) (b) (c) (d)

Figure 1.27

Interference 31

1.10.3.1 Applications

Michelson's interferometer uses the concept of interference that takes place with the help of two mirrors. The distance between one mirror and the image of another plays an important role in the formation of fringes. Michelson's interferometer has diverse applications, some of which are listed

below.

(i) Determination of Wavelength of Light

First of all the Michelson's interferometer is set for circular fringes with central bright spot, which is possible when both the mirrors are parallel (q = 0). If t be the thickness of air film enclosed between the two mirrors (M_1 and $M_2\phi$) and n be the order of the spot obtained, then for normal

incidence $\cos r = 1$, we have $\frac{1}{r}$

t n
+ =

$$2^{2}$$

 1^{2}
 $\hat{E}^{\hat{A}} = \hat{A}^{-\hat{C}} = \hat{B}$
or t n I

If M_1 is moved $\frac{1}{2}$ away from $M_2 \not c$, then an additional path difference of I will be introduced and hence $(n+1)^{th}$ bright spot appears at the centre of the field. Thus each time M_1 moves through a distance $\frac{1}{2}$, a new bright fringe appears. Therefore, if M_1 moves by a distance x (x_1 to x_2) and x0 new fringes appear at the centre of the field, then we have

The difference $(x_2 - x_1)$ is measured with the help of micrometer screw and N is actually counted. The experiment is repeated for number of times and the mean value of I is obtained.

(ii) Determination of Difference in Wavelengths

Michelson's interferometer is adjusted in order to obtain the circular fringes. Let the source be not monochromatic and have two wavelengths I_1 and I_2 ($I_1 > I_2$) which are very close to each other (as Sodium D lines). The two wavelengths form their separate fringe patterns but as I_1 and I_2 are very close to each other and thickness of air film is small, the two patterns practically coincide with each other. As the mirror M_1 is moved slowly, the two patterns separate slowly and when the thickness of air film is such that the dark fringe of I_1 falls on bright fringe of I_2 , the result is maximum indistinctness. Now the mirror M_1 is further moved, say through a distance x, so that the next indistinct position is reached. In this position, if n fringes of I_1 appear at the centre, then (n +1) fringes of I_2 should appear at the centre of the field of view. Hence

$$\begin{array}{ccc} & & & & & \\ & & & & \\ & & & 12 \\ & & x & n & x & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & \\ & & & \\ & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & &$$

(i)

$$\begin{array}{c} & & & \\ & & & \\ 2 \\ & & \\ \end{array} \\ \text{and} \\ & & \\ 32 \text{ Engineering Physics} \end{array}$$

On subtracting Eq. (i) from Eq. (ii), we

or

Thus measuring the distance x moved by mirror M_1 between the two consecutive positions of maximum indistinctness, the difference between two wavelengths of the source can be determined, if I_{av} is known.

(iii) Determination of Thickness and Refractive Index of a Thin Transparent Sheet The Michelson's interferometer is adjusted for producing straight white light fringes and cross-wire is set up on the central bright fringe. Now insert thin transparent plate in the path of one of the interfering waves. On the inclusion of a plate of thickness t and refractive index m, the path difference is increased

by a factor of 2(m-1)t. The fringes are therefore shifted. The mirror M_1 is now moved till the central fringe is again brought back to its initial position. The distance x traveled by the mirror M_1 is measured by micrometer. Therefore x

$$22(1) \text{ or } (1)$$
 $x \text{ tt m} = -= m - (iii)$

From Eq. (iii), we can write

$$1 x m = + (iv)$$

Thus, by knowing the thickness of the transparent sheet and the distance x, we can calculate the refractive index of the sheet with the help of a Michelson's interferometer.

fieLD Of engineering

appLiCatiOns Of interferenCe in tHe



The phenomenon of interference arises in many situations and the scientists and engineers have taken advantage of interference in designing and developing various instruments.

1.11.1 Testing of Optical Flatness of Surfaces

An example of the application of interference method is the testing of optical components for surface quality. The most important example is that of optical flats. However, the methods used for fl at surfaces can be adapted simply to test spherical surfaces.

1.11.1.1 Flatness Interferometers

With these interferometers we can compare the flatness of two surfaces by placing them in contact with slight wedge of air between them. This gives a tilt and thus the fringes start originating like that of Newton's ring between the two surfaces. To get half wavelength contours of the space between the surfaces, they should be viewed from infiity. Further, to avoid the risk of scratching, a desirable distance should be there between the two surfaces. Most common examples of flatness interferometers are Fizeau and Twyman interferometers.

Interference 33

(i) Fizeau Interferometer

In this type of interferometer, the sources and viewing point are kept at infinity (Fig. 1.28). This interferometer generates interference between the surface of a test sample and a reference surface that is brought close to the test sample. The interference images are recorded and analysed by an imaging optic system. However, the contrast and the shape of the interference signals depend on the reflectivity of the test samples.

(ii) Twyman-Green Interferometer

This is an important instrument used to measure defects in optical components such as lenses, prisms, plane parallel windows, laser rods and plane mirrors. Twyman-Green interferometer, shown in Fig. 1.29 resembles Michelson interferometer in the beam splitter and mirror arrangement. However, the difference lies in the way of their illumination. In the case of Twyman-Green interferometer, we use a Figure 1.28 monochromatic point source

which is located at the principal focus of a well-corrected lens whereas in Michelson interferometer an extended source is used. If the mirrors M_1 and M_2 are perpendicular to each other and the beam-splitter BS makes an angle of 45° with the normal of each mirror, then the interference is exactly analogous to thin film interference at normal incidence. Therefore, completely constructive interference is obtained when d = ml/2, where d is the path difference between the two arms adjusted by translating the mirror M_1 . The complete destructive interference is obtained when d = (m + 1/2)l/2. With the help of rotation of mirror M_2 we can see fringes of equal thickness on the screen, as the angle of incidence is constant. This situation is analogous to interference pattern observed with collimated light and a thin film with varying thickness. In order to test the optical components, one of the mirrors is intentionally tilted to create fringes. Then the quality of the component can be determined from the change in the fringe pattern when the component is placed in the interferometer. Lens testing is specifically important for quantifying aberrations and measuring the focal length.

S

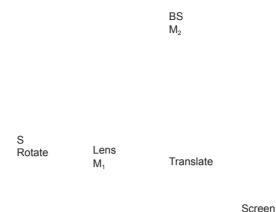


Figure 1.29

34 Engineering Physics

1.11.2 Nonreflecting or Antireflecting (AR) Coatings

Interference-based coatings were invented in November 1935 by Alexander Smakula, who was working for the Carl Zeiss optics company. Antireflecting coatings are a type of optical coatings. These are applied to the surface of lenses and other optical devices for reducing reflection. This way the efficiency of the system gets improved since less light is lost. For example, in a telescope the reduction in reflections improves the contrast of the image by elimination of stray light. In another applications a coating on eyeglass lenses makes the eyes of the wearer more visible. The anti-reflecting coatings can be mainly divided into three groups.

1.11.2.1 Single-layer Interference Coatings

The simplest interference non-reflecting coating consists of a single quarter-wave layer of transparent material. The refractive index of this material is taken to be equal to the square root of the substrate's refractive index. This theoretically gives zero reflectance at the center wavelength and decreased reflectance for wavelengths in a broad band around the center. The use of an intermediate layer to form an antireflection coating can be thought of as analogous to the technique of impedance matching of electrical signals. A similar method is used in fibre optic research where an index matching oil is sometimes used to temporarily defeat total internal reflection so that light may be coupled into or out of a fiber.

The antireflection coatings rely on an intermediate layer not only for its direct reduction of reflection coefficient, but also use the interference effect of a thin layer. If the layer thickness is controlled precisely and it is made exactly one quarter of the light's wavelength (I/4), then it is called a quarter-wave coating (Fig. 1.30). In this case, the incident beam I, when reflected from the second interface, will travel exactly half its own wavelength further than the beam reflected from the first surface. The two reflected beams R_1 and R_2

will destructively interfere as they are exactly out of phase and cancel each other if their intensities are equal. Therefore, the reflection from the surface is suppressed and all the energy of the beam is propagated through the transmitted beam T. In the calculation of the reflection from a stack of layers, the transfer-matrix method can be used.

I

n_s n₁ n₀

 R_{1T}

 R_2

Figure 1.30

Interference 35

1.11.2.2 Multilayer Coatings or Multicoating

Multiple coating layers can also be used for reflection reduction. It is possible if we design them such that the reflections from the surfaces undergo maximum destructive interference. This can be done if we add a second quarter-wave thick higher-index layer between the low-index layer (for example, silica) and the substrate. Under this situation, the reflection from all three interfaces produces destructive interference and antireflection. Optical coatings can also be made with near-zero reflectance at multiple wavelengths or optimum performance at angles of incidence other than 0°.

1.11.2.3 Absorbing Antireflecting Coatings

Absorbing antireflecting coatings are an additional category of antireflection coatings. These coatings are useful in situations where low reflectance is required and high transmission through a surface is unimportant or undesirable. They can produce very low reflectance with few layers. They can often be produced more cheaply or at greater scale than standard non-absorbing anti-reflecting coatings. In sputter deposition system for such films, titanium nitride and niobium nitride are frequently used.

1.11.2.4 Practical Problems with AR Coatings

Real coatings do not reach perfect performance, though they are capable of reducing a surface's reflection coefficient to less than 0.1%. Practical details include correct calculation of the layer thickness. This is because the wavelength of the light is reduced inside a medium and this thickness will be $l_0/4n_1$, where l_0 is the vacuum wavelength and n_1 is the refractive index of the film. Finding suitable materials for use on ordinary glass is also another difficulty, since few useful substances have the required refractive index (n a 1.23) which will make both reflected rays exactly equal in intensity. Since magnesium fluoride (MgF $_2$) is hard-wearing and can be easily applied to substrates using physical vapour deposition, it is often used for this purpose even though its index is higher than desirable (n = 1.38).

interferenCe





In interferometry, we use the principle of superposition to combine different waves in a way that will cause the result of their combination to have some meaningful property, that is indicative of

the original state of the waves. The phenomenon of interference is employed under various situations for its scientific applications. For a better understanding of the applications, we first need to know about the homodyne and heterodyne detections.

DeteCtiOn

HOmODYne anD HeterODYne



In standard interferometry, the interference occurs between the two beams at the same wavelength (or carrier frequency). The phase difference between the two beams results in a change in the intensity of the light on the detector. Measuring the resulting intensity of the light after the mixing of these two light beams is known as homodyne detection. In heterodyne detection, we modulate one of the two beams prior to detection, usually by a frequency shift. A special case of heterodyne detection is optical heterodyne detection, which detects the interference at the beat frequency.

1.13.1 Imaging Interferometry

In this interferometry, the pattern of radiation across a region can be represented as a function of position i(x, y), i.e., an image and the pattern of incoming radiation i(x, y) can be transformed into the Fourier domain

36 Engineering Physics

f(u, v). A single detector measures information from a single point in (x, y) space. An interferometer measures the difference in phase between two points in the (x, y) domain. This corresponds to a single point in the (u, v) domain. An interferometer builds up a full picture by measuring multiple points in (u, v) space. The image i(x, y) can then be restored by performing an inverse Fourier transform on the measured f(u, v) data.

1.13.2 Holographic Interferometry (HI)

Holographic interferometry (HI) is a technique that enables static and dynamic displacements of objects with optically rough surfaces to be measured to optical interferometric precision, i.e., to fractions of a wavelength of light. These measurements can be applied to stress, strain and vibration analysis, as well as to nondestructive testing. It can also be used to detect optical path length variations in transparent media, which enables, for example, fluid flow to be visualised and analysed. It can also be used to generate contours representing the form of the surface. Holography interferometry is of two types.

(i) Live Holography Interferometry

Holography enables the light field scattered from an object to be recorded and replayed. If this recorded field is superimposed on the "live field" scattered from the object, then the two fields will be identical. However, if a small deformation is applied to the object, the relative phases of the two light fields will alter and it is possible to observe interference. This technique is known as live holographic interferometry.

(ii) Frozen-Fringe Holography

In this holography, it is also possible to obtain fringes by making two recordings of the light field scattered from the object on the same recording medium. The reconstructed light fields may then interfere to give fringes, which map out the displacement of the surface.

1.13.3 Electronic Speckle Pattern Interferometry

Electronic Speckle Pattern Interferometry (ESPI), also known as TV Holography, is a technique that uses laser light together with video detection, recording and processing to visualize static and dynamic displacements of components with optically rough surfaces. The visualisation is in

the form of fringes on the image where each fringe normally represents a displacement of half a wavelength of the light used, i.e., quarter of a micrometre or so.

1.13.4 Angle Resolved Low Coherence Interferometry

Angle resolved low coherence interferometry is an emerging biomedical imaging technology that uses the properties of scattered light to measure the average size of cell structures, including the cell nuclei. The technology shows promise as a clinical tool for in situ detection of dysplatic or precancerous tissue.

1.13.5 Optical Coherence Tomography

This is a medical imaging technique based on low-coherence interferometry, where subsurface light reflections are resolved to give tomographic visualisation. Recent advances have struggled to combine the nanometre phase retrieval with the ranging capability of low-coherence interferometry.

1.13.6 Geodetic Standard Baseline Measurements

A famous use of white light interferometry is the precise measurement of geodetic standard baselines. Here the light path is split in two, and one leg is folded between a mirror pair 1 m apart. The other leg bounces once off a mirror 6 m away. The fringes will be seen only if the second path is precisely 6 times the first. Starting

Interference 37

from a standard quartz gauge of 1 m length, it is possible to measure distances up to 864 m by repeated multiplication. Baselines thus established are used to calibrate geodetic distance measurement equipments. This leads to a metrologically traceable scale for geodetic networks measured by these instruments. More modern geodetic applications of laser interferometry are in calibrating the divisions on levelling staffs and in monitoring the free fall of a reflective prism within a ballistic or absolute gravimeter. This allows determination of gravity, i.e., the acceleration of free fall, directly from the physical definition at a few parts in a billion accuracy.

1.13.7 Interference Lithography

This is a technique for patterning regular arrays of fine features, without the use of complex optical systems or photo marks. The basic principle of this is the same as interferometry. An interference pattern between two or more coherent light waves is set up and recorded in a recording layer. This interference pattern consists of a periodic series of fringes of representing intensity maxima and minima. The benefit of using interference lithography is the quick generation of dense features over a wide area without loss of focus.



We summarise the main outcome of the chapter as follows:

- ◆ We fi rst discussed the phenomenon of interference and then explained it based on Young's double slits experiment.
- ◆ Concepts of wavefront and secondary wavelets were discussed based on Huygens' principle. Then secondary wavefront was introduced as the surface touching the secondary wavelets tangentially in the forward direction at any given time.
- ◆ Phase difference and path difference between the two waves play a key role for obtaining constructive or destructive interference. Therefore, phase and path differences were

- explained in detail together with their relation.
- ◆ For obtaining sustained interference pattern, the two sources should be coherent. So the concept of coherence, both temporal and spatial, was introduced and coherence time and coherence length were talked about.
- ◆ A short description of a technique for producing coherent light from incoherent sources was given.
 - ◆ Analytical treatment of the interference was discussed where conditions were obtained for the constructive and destructive interferences.
 - ◆ When a light wave gets refl ected from a surface, a phase change may take place. Therefore, condition of relative phase shift was explained.
 - ◆ Superposition was extended for n number of waves and it was observed that the resultant amplitude increases in proportion with in length as n gets increased.
 - ◆ Interfering waves can be produced either by division of wavefront or by division of amplitude. Therefore, the details of interference were discussed based on these two methods.
 - ◆ Fresnel's biprism, which is used to create two virtual coherent sources, was discussed in detail for obtaining interference pattern and the related conditions for dark and bright fringes

 Application of biprism for the determination of wavelength of liaht. distance between two virtual coherent sources and thickness of transparent sheet were discussed. The displacement of fringes by the introduction thin of transparent sheet in the path of one liaht wave was also explored.

→ Thin fi Ims are used for the division of amplitude of light waves which superimpose each other. The interference pattern obtained by thin fi lms of uniform and non-uniform thicknesses was investigated.

- ◆ When the air fi Im is created between the curved surface of a plano-convex lens and the fl at surface of a mirror, the interference takes place between the refl ected as well as the transmitted light. Here the fringes are obtained in the form of rings known as Newton's rings.
- ◆ Newton's rings method was used for determination of the wavelength of light, radius of curvature of a plano-convex lens and the refractive index of liquid.
- ◆ The theory was extended to Newton's rings formed between two curved surfaces.
- ◆ Theory and practical applications of Michelson's interferometer were discussed. Clarifi cation of path difference and the details of formation of fringes were given.
- ◆ Engineering applications of interference were included, particularly related to the testing of optical fl atness of surfaces and nonrefl ecting or antirefl ecting coatings.
- ◆ Finally the scientific applications of interference were discussed related to various interferometry, tomography and lithography.

Example 1 If light of wavelength 660 nm has wave trains 13.2×10^{-6} m long, what would be the coherence time.

Solution Given I = 6.6 ± 10^{-7} m, coherence length (DL) = 1.32 ± 10^{-5} m and coherence time (Dt) = ?

Formula used is DL = c ◊ Dt

Example 2 Coherence length of a light is $2.945 \ \mbox{$\stackrel{>}{=}$} \ 10^{-2} \ \mbox{m}$ and its wavelength is 5896 Å. Calculate the coherence time and number of oscillations corresponding to the coherence length. Solution Given DL = $2.945 \ \mbox{$\stackrel{>}{=}$} \ 10^{-2} \mbox{m}$ and I = $5.896 \ \mbox{$\stackrel{>}{=}$} \ 10^{-7} \mbox{$\stackrel{>}{=}$} \ Dt$ = ?

Formula used is DL = cDt $\begin{array}{c} -D \ ^{2} D = = \ ^{2} \\ L \ ^{2} - \\ 2.945 \ 10 \\ \\ \text{or} \ ^{11} \ 9.816 \ 10 \\ \\ \text{t} \ ^{2} \ ^{2} \\ \text{sec} \ ^{8} \\ D \ ^{2} \\ \text{and number of} \\ \text{oscillations in a length L}, \\ ^{2} \ ^{2} \ ^{4} \ ^{4}.99 \ 10 \\ = \ ^{2} = \ ^{4} \end{array}$

Example 3 A coherent beam has band width of 1200 Hz. Obtain the coherence length. Solution Given Dn = 1200 Hz and C = 3 ± 10^8 m/s

Interference 39

Example 4 Calculate the line-width, coherence time and frequency stability for a line of Krypton having a wavelength of 6.058 ¥ 10^{-7} m and coherence length as 0.2 m.

where x is the distance between two mirrors. The above expression can be written as

where I_{av} is the mean wavelength of I_1 and I_2 . Here DI is called line width.

In view of the fact that the fringes are not observed if the path difference exceeds the coherence length DL, we can assume the beam to contain all wavelengths lying between I and (I + dI).

Therefore,
$$^{2av}_{2x} \stackrel{|}{L} = \stackrel{|}{D} = \stackrel{|}{D}$$

or $^{2}_{1} \stackrel{|}{a} \stackrel{|}{V} \stackrel{|}{D} = \stackrel{|}{D} \stackrel{|}{L}$

Q frequency, $^{cn}_{1} = ^{nc}_{\dot{c}} \stackrel{|}{C} \stackrel{|}{C} \stackrel{|}{D} = \stackrel{|}{1} \stackrel{|}{C} \stackrel{|}{D} = \stackrel{|}{1} \stackrel{|}{C} \stackrel{|}{D} = \stackrel{|}{D} = \stackrel{|}{D}$

or $^{2}_{2}$
 $^{cc}_{\dot{c}} \stackrel{|}{D} = \stackrel{|}{D} = \stackrel{|}{D}$

or $^{2}_{2}$

Here, Dv is called frequency spread of the line, which can be written in terms of Dt as follows. 1 1

In addition, frequency stability is defined as the ratio of frequency spread and frequency of any

D 0.2

spectral line, i.e., frequency stability =
$$^{V}v^{D}$$
 272
 $^{I}\Gamma Y ^{-}D = = Y$

Line width
 $^{12}1.83410 \text{ m}$
 $^{av}(6.05810)$
 DL
 DL
 $^{0.2}$
 $^{8}310^{9}1.5$

Frequency spread $^{C}V Y ^{Y}D = = Y$

Frequency 3 10

$$c \ V \ I^{-} = Y$$
 6.058 10

$$= 4.952 \times 10^{14} \text{ Hz}$$

and Frequency stability
$${9\atop 6}$$
 D ${4\atop V}$ ${0\atop 1.5}$ 10 ${0\atop 1.5}$ 10 ${0\atop 1.5}$ 10 ${0\atop 1.5}$ 4.952 10 ${0\atop 1.4}$

40 Engineering Physics

Formula used is

Example 5 The Doppler width for an orange line of Krypton is 550×10^{-15} m. If the wavelength of light is 605.8 nm, calculate the coherent length.

13

Solution Given Doppler line width (DI) = 5.5×10^{-13} m.

$$I = I_{av} = 6.058 \times 10^{-7} \,\text{m}, \, DL = ?$$

$$272 \qquad \qquad I \qquad -$$

$$Y = D = 0$$

$$0.6673 \, \text{m}$$

$$D \times 0.6673 \, \text{m}$$

Å with a band width of 6 ¥ 10⁸ nce length of a He–Ne laser

```
The coherence length is given by ^{272} L ^{1} L ^{1} D = = = ^{(5.641\ 10\ )} 0.534 m ^{av\ 1} ^{13} D ^{4} 5.964 10 For He – Ne laser, Given I_{av} = 6.328 ^{4} 10^{-7} m, Dv = 10^{6} Hz ^{272\ 6}
```

5.964 10 m

Example 7 Find the coherence length of a laser beam for which the band width is 3000 Hz. Solution Given Dv = 3000 Hz.

Coherence length (DL) = cDt and coherence time (Dt) =
1
Dv 4 So 1 3 3.333 10 sec 1 D = = 4 3000 2 L = c 4 t = 3 4 108 4 3.333 4 10 $^{-4}$ = 1.0 4 105m

Example 8 Calculate the resultant line-width, band width and coherence length assuming that we chop a continuous perfectly monochromatic beam of wavelength 6328 Å in 10^{-10} seconds using some sort of shutter. Solution Given $I_{av} = 6.328 \pm 10^{-7}$ m and $t = 10^{-10}$ sec Coherence length, DL = cDt = $3 \pm 10^8 \pm 10^{-10} = 3 \pm 10^{-2}$ m

Interference 41

$$\begin{array}{c} 1\ 1 \\ 10\ \text{Hz} \\ \text{Bandwidth, Dg} = ^{10} \\ 10^{-} = = \\ 10 \\ &$$

deduce the

√ √

_{1 2} a a: = 16 : 1 or a_1 : a_2 = 4 : 1

or $a_1 = 4a_2$

22
Iaaaa
++===
()(4)25
max1222
22
min1222

Example 10 The ratio of intensities of two waves that produce interference pattern is 16:1. Deduce the ratio of maximum to minimum intensities in fringe system.

Solution Given $I_1: I_2 = 16: 1$ The intensity, $I \mu a^2$

i.e.,
$$I_{max}$$
: I_{min} = 25:9

Example 11 Two waves of same frequency with amplitudes 1.0 and 2.0 units, interfere at a point, where the phase difference is 60°. What is the resultant amplitude?

Solution Given a_1 = 1.0 unit, a_2 = 2.0 unit and f = 60° the resultant amplitude

R a a a a = + + f
$${}_{1212}2 \cos$$
= + + =
$${}_{1427}$$
= 2.65 units

Example 12 Distance between two slits is 0.1 mm and the width of the fringes formed on the screen is 5 mm. If the distance between the screen and the slit is one meter, what would be the wavelength of light used?

42 Engineering Physics

Solution Given b = 5.0 ± 10^{-3} m, 2d = 1.0 ± 10^{-4} m and D =

Example 13 A biprism of angle 1° and



refractive index 1.5 is at a distance of 40 cm from the slit. Find the fringe width at 60 cm from the biprism for sodium light of wavelength 5893 Å.

Solution Given a = .4 m, m = 1.5, I = 5.893 ± 10^{-7} m and D = 1.0 m

From the Fig. 1.31 d =
$$\frac{d}{a}$$
 or d = ad or 2d = 2ad

The deviation produced in the incident light is given by

$$d = (m - 1) a$$

2d = 2a (m - 1)a

where a = angle of prism

Example 14 Interference fringes are produced by Fresnel's bi-prism on the focal plane of a reading microscope which is 1.0 m far from the slit. A lens interposed between the biprism and the microscope gives two images of the slit in two positions. If the images of the slits are 4.05 mm apart in one position and 2.90 mm apart in the other position and the wavelength of the sodium light is 5893 Å, find the distance between the consecutive interference bands?

Solution Given I =
$$5.893 \pm 10^{-7}$$
 m, D = 1.0 m, $d_1 = 4.05 \pm 10^{-3}$ m and $d_2 = 2.90 \pm 10^{-3}$ m Formula used is $2d = 6$

or 2d = 3.427×10^{-3} m

Interference 43

$$b^{-1}$$

D 5.893 10 1.0

Now

3

2 3.427 10 d

b = 0.172 mm

Example 15 In a biprism experiment fringes were first obtained with the sodium light of wavelength 5890 Å and fringe width was measured to be 0.342 mm. Sodium light was then replaced with white light and central fringe was located. On introducing a thin glass sheet in half of the beam, the central fringe was shifted by 2.143 mm. Calculate the thickness of the glass sheet if the refractive index of glass is 1.542.

Solution Given I = 5890 \(\pm\$ 10⁻¹⁰ m, = 1.542, x_n = 2.143 \(\pm\$ 10⁻³ m\) $b = 3.42 \(\pm$ 10⁻⁴ m\)$

nt of I = 5896 he biprism is

or 2d = 6.55 ¥ 10⁻⁴m

Example 17
The distance between the slit and biprism and between biprism and

screen are 50 cm each, Angle of biprism and refractive index are 179° and 1.5, respectively. Calculate the wavelength of light used if the distance between two successive fringes is 0.0135 m.

Example 18 The distance between the slit and biprism and between biprism and eyepiece are 45 cm each. The obtuse angle of biprism is 178° and its refractive index is 1.5. If the fringe width is

Solution ₂D d | b | = d D Given a = 45cm. D = 90cm, m = 1.5,a = 1° = p/180 rad b = 15.6 Y $10^{-3} \, \text{cm}$ 2d can be calculated by the relation 2d = 2a (m -1) a = 2 ¥ 45 ¥ $0.5 \pm (22/7) \pm$ (1/180) =0.786 $b_{\Gamma} = d$ 3 (2) 15.6 10 0.789 = 0.90= 13676 Å Example

19 In a biprism experiment, the eye piece was placed at a distance of 120 cm from the source. Calculate the wavelength of light, if the eye is required to move through a distance of 1.9 cm for 20 fringes and distance between two slits is 0.06 cm.

Solution Given $x_n = 1.9 \text{ cm}$, n = 20, D = 120 cm and 2d = 0.06 cm.

or 2 0.095 0.06

$$b_{\parallel}^{4} = = 0$$
 $D \quad A$
 $A = 4750$

Example 20 In a biprism experiment using light of wavelength 5890 Å, 40 fringes are observed in the field of view. If this light is replaced by light of wavelength 4358 Å. Calculate how many fringes are observed in the field of view.

Solution Given I_1 = 5890 Å, N_1 = 40 and I_2 = 4358 Å, N_2 = ? II = = b $DD \times NNN$ 12111222

$$N_1I_1 = N_2I_2$$

 $40 \pm 5890 \pm 10^{-10} = N_2 \pm 4358 \pm 10^{-10}$
 $N_2 = 54$

Example 21 Light of wavelength 5893 Å is reflected at normal incidence from a soap film of refractive index 1.42. What is the least thickness of the film that will appear (a) bright and (b) dark? Solution Given I = 5.893 ± 10^{-7} m, i = r = 0, = 1.42 and for smallest thickness n = 1

Condition for thin film to appear bright in reflected light is

m

Similarly condition for thin film to appear to dark in reflected light is $2mt \cos r = nl$

Interference 45

 $= Y^{-4} = 2.075 = 10 \text{ mm}$

floating on a surface of water (m ith dark fringe is seen. Find the



2 1.4 0.934 $= Y^{-3} = 1.351 = 10 \text{ mm}$

Example 23 Calculate the thickness of a soap film (m = 1.463) that will result in constructive interference in the reflected light, if the film is illuminated normally with light whose wavelength in free space is 6000 Å. Solution Given I = 6.0 ¥ 10^{-7} m, m = 1.463, for normal incidence $i = r = 0^{\circ}$ and for smallest thickness n = 1.

For constructive interference 2 mt $\cos r = (2n - 1) \frac{1}{2}$ $n_{t^{-}} - - * * = * * * * *$ ⁷ (2 1) (2 1) 6.0 10 2 2 1.463 1 4 1.463 $= Y^{-4} 1.025 10 \text{ mm}$

Example 24 A parallel beam of sodium light (I = 5890 Å) strikes a film of oil floating on water.

When viewed at an angle of 30° from the normal, q^{th} dark band is seen. Determine the thickness of the film. (Refractive index of oil = 1.46).

Solution Given I = 5.89×10^{-7} m, i = 30° , m = 1.46 and n = 8

Condition for obtaining dark band is $2mt \cos r = nl$ (i) I

or 2 cos

As we know, sin i

 $_{r}$ m = (ii)

or 2 cos 1 sin

r r = -

Example 25 White light is



reflected from an oil film of thickness 0.01 mm and refractive index 1.4 at an angle of 45° to the vertical. If the reflected light falls on the slit of a spectrometer, calculate the number of dark bands seen between wavelengths 4000 and 5000 Å.

Solution Given t = 1.0 ± 10^{-5} m, m = 1.4, i = 45° , I₁ = 4.0 ± 10^{-7} m and I₂ = 5.0 ± 10^{-7} m Condition of dark bands in reflected light is

2mt cos r = nl (i)
$$iirm_{rm} = 1$$

 $sin sin_{or sin}$
 $sin_{or sin} = 1$
 sin_{or

For wavelength I_1 , i.e, 4.0×10^{-7} m

4.0 10

For wavelength I₂, i.e, 5.0 ± 10^{-7} m t r m_{1 5}

$$YYYY = Y$$

$$2 \cos 2 1.4 1.0 10 0.86^{27} 2$$

$$5.0 10$$

=
$$48.16 \text{ or } n_2^a 48 \quad n_1 - n_2 = 60 - 48 = 12$$

i.e, 12 dark bands are seen between wavelengths 4000 and 5000 Å.

Example 26 A parallel beam of light of wavelength 5890 Å is incident on a glass plate having refractive index m = 1.5 such that the angle of refraction in the plate is 60° . Calculate the smallest thickness of glass plate which will appear dark by reflected light.

Solution Given I = 5.89×10^{-7} m, = 1.5 and r = 60°

Condition for the film to appear dark in reflected light is 2mt cos r = nl



```
2 cos 2 1.5 0.5
m
-6 0.3927 10 m
= ¥
```

Example 27 A soap film of refractive index 1.333 is illuminated by white light incident at an angle of 45°. The light refracted by it is examined by a spectroscope and two consecutive bright bands are focused corresponding to the wavelength 6.1 ¥ 10⁻⁵ cm and 6.0 ± 10^{-5} cm. Find the thickness of the film. Solution Given m = 1.333, i = 45° , $I_1 = 6.1 \text{ }$ 10^{-7} m and $I_2 = 6.0 \times 10^{-7}$ m ir ∞ rm ==== sin sin 45 1/ 2 0.707 or sin sin 1.333 1.333 1.333 $\sin r = 0.53$ $^{22}\cos 1 \sin 1 (0.53) 0.848 \text{ r r} = -= -$ Condition of bright film to observe in transmitted case is $2mt \cos r = nl_1 = (n + 1)l_2$ or $n \neq 6.1 \neq 10^{-7} = (n + 1) \neq 6.0 \neq$ 10⁷ n = 60

```
and \begin{array}{c} \text{n t} \\ \text{r} \\ \text{1} \\ \text{1} \\ \text{1} \\ \text{2 cos 2 1.333 0.848} \\ \text{= } \\ \text{1} \\ \text{1} \\ \text{2 cos 2 1.333 0.848} \\ \text{3} \\ \text{3} \\ \text{4} \\ \text{5} \\ \text{1} \\ \text{6} \\ \text{6} \\ \text{1} \\ \text{6} \\ \text{7} \\ \text{8} \\ \text{1} \\ \text{8} \\ \text{8} \\ \text{1} \\ \text{8} \\ \text{8} \\ \text{8} \\ \text{1} \\ \text{8} \\ \text
```

Example 28 A soap film suspended in air has thickness 5×10^{-5} cm viewed at an angle 35° to the normal. Find the wavelength of light in visible spectrum, which will be absent for a reflected light. The m for the soap film is 1.33 and visible spectrum is in the range of 4000 to 7800 Å

Solution Given $t = 5.0 \pm 10^{-7} \, \text{m}$, $i = 35^{\circ}$ and m = 1.33

By using the relation

```
2mt \cos r = nl \text{ and } m = \sin r
                                                           i
                                                       sin
                                     n
                                         m and \cos r = 21 \sin - r
     si
                                         <sup>22</sup> sin <sup>35</sup> 1 1 1.33
                                       i
Ê^Ê^-=-Á~Á~Ë-
     si
     n
                                            Ë<sup>-</sup>m
      = 0.902 for first order (n = 1)
      1 \lozenge I_1 = 2m + \cos r
                               I_1 = 2 \pm 1.33 \pm 5.0 \pm 10^{-7} \pm 0.902
      = 1.19 \times 10^{-6} = 1200 \text{ Å}
     In second order (n = 2)
      2 + I_2 = 2mt + cos r
48 Engineering Physics
or I_2 = m + \cos r = 1.33 \pm 5 \pm 10^{-7} \pm 0.902 = 6.0 \pm 10^{-7} m
(approx) In second order (n = 3)
2 ¥ 1 = 2mt + coe r
```

result in constructive
h light whose wavelength in
for normal incidence i = 0 and r



4 cos 4 1.463 1 = ¥ ⁷ 1.025 10 m. Example 30 A thin film is illuminated by white light at an angle of incidence (i = $\sin^{-1}(4/5)$). In reflected light, two dark consecutive overlapping fringes are observed corresponding to wavelengths 6.1 ± 10^{-7} m and 6.0 ± 1 0^{-7} m. The refractive index of the film is 4/3. Calculate the thickness of the film. Solution Given I₁ = 6.1 ± 10^{-7} m, I₂ = 6.0 ± 10^{-7} m and m = 4/3

```
sin sin 4/5 3 or sin
                           sin 4/3 5
                      9 4 cos 1 sin 1 0.8
and ^{\rm 2}
                                                    25 5
Condition for dark fringes is
2mt \cos r = nl_1 = (n + 1)l_2
or nI_1 = (n + 1)I_2
n \neq 6.1 \neq 10^{-7} = (n + 1) \cdot 6.0 \neq 10^{-7}
n(6.1 - 6.0) \times 10^{-7} = 6.0 \times 10^{-7}
or n = 60
and 2mt cos r = nl<sub>1</sub>
or
                     3
60 6.1 10
                        mmt
```

Interference 49

Example 31 Two plane glass surfaces in contact along one edge are separated at the opposite edge by a thin wire. If 20 interference fringes are observed between these edges in sodium light at normal incidence. What is the thickness of wire?

$$= 5.893 \times 10^{3} \, \text{mm}.$$

$$t$$
O 20 w
A
Figure 1.32

Example 32 A wedge air film is enclosed between two glass plates touching at one edge and separated by a wire of 0.06 ± 10^{-3} m diameter at a distance of 0.15 m from the edge. Calculate the fringe width. The light of wavelength 6.0 ± 10^{-7} m from the broad source is allowed to fall normally on the film.

Solution Given I =
$$6.0 \pm 10^{-7}$$
 m and m = $1_{2 \text{ w}}$ mq = $\frac{1}{100}$ M = $\frac{1}{100}$ M

Example 33 A wedge shaped film is illuminated by light of wavelength 4650 Å. The angle of wedge is 40≤. Calculate the fringe separation between two consecutive fringes.

Solution Given I =
$$4.56 \times 10^{-7}$$
 m and m = 1

$$p = 40$$
 40 rad
 $= = 4 e^{\phi \phi} \approx 3600 180$
 $= 1.9 10 \text{ rad } = \frac{4}{7}$
 $= 1.9 10 \text{ rad } = \frac{4}{7}$
 $= 1.9 10 \text{ rad } = \frac{4}{7}$
 $= 1.2 \text{ rad } = \frac{4}{7}$
 $= 1.2 \text{ rad } = \frac{4}{7}$
 $= 1.2 \text{ rad } = \frac{4}{7}$

Example 34 Two glass plates enclose a wedge-shaped air film touching at one edge are separated by a wire of 0.03 mm diameter at distance 15 cm from the edge. Monochromatic light (I = 6000 Å) from a broad source falls normally on the film. Calculate the fringe-width.

50 Engineering Physics

A

Example 35 A glass wedge having angle 0.01 radian is

illuminated normally by light of wavelength 5890 Å. At what distance from the edge of the wedge, will the 12^{th} dark fringe be observed by reflected light? Solution Given I = 5.89×10^{-7} m, n = 12, q = 0.01 rad and m = 1

Condition for obtaining dark fringe is

2mt $\cos (r + q) = nl (i)$ For normal incidence i = r = 0 and when q is very small $\cos q$ ^a 1

Eq. (i) reads 2t = nl (ii) Now the angle q can be written as $x \neq q = nl$

where t is the thickness and x is the distance from the edge (Fig. 1.34) then we have t = $q \lozenge x$ (iii)

Example 36 A glass wedge of angle 0.01 radian of illuminated by monochromatic light of wavelength 6000 Å falling normally on it. At what distance from the edge of the wedge will the 10th fringe be observed by reflected light?

Solution Given a = 0.01 radian, $I = 10 \times I = 6.0 \times 10^{-7}$ m the condition for dark fringe

= 2t = nl (i) The angle of wedge a = $\frac{t}{x}$ or t = ax (ii) Put the value of t from Eq. (ii) in Eq (i), we get 2ax = nl

$$_{2}^{2}$$
 $_{2}$ $_{3}$ $_{4}$ $_{5}$ $_{10}^{-4}$ $_{10}$

Interference 51

Example 37 Interference fringes are produced when monochromatic light is incident normally on a thin wedge-shaped film of refractive index 1.5. If the distance between two consecutive fringes is 0.02 mm. Find the angle of the film, the wavelength of light being 5.5 ± 10^{-5} cm.

Solution Given m = 1.5, w = 0.02 ± 10^{-3} m and I = 5.5 ± 10^{7} m.

 $= 0.009166 \text{ rad} = 0.525^{\circ}$

Example 38 In Newton's rings experiment, the diameter of the 15^{th} ring was found to be 0.59 cm and that of the 5^{th} ring was 0.336 cm. If the radius of the plano convex lens is 100 cm, compute

rings are 0.2 and 0.3 cm, Calculate the wavelength of $D_{20} = 0.3$ cm. p = 10



I = 277.8 nm

Example 40 In a Newton's rings arrangement a thin convex lens of focal length 1.0 m. (m = 1.5) remains in contact with an optical flat and light of wavelength 5896 \pm 10⁻¹⁰ m is used. Newton's rings are observed normally by reflected light. What is the diameter of 7th bright ring?

Solution Given m = 1.5, f = 1.0 m and I = 5.896×10^{-7} m

$$R_1 = R$$
 and $R_2 = R$
1 1 1

Formula used is $-\acute{A}^{"} \ddot{E}^{-}_{12}$ (1) $f_{RRm}^{\acute{E}^{"}} = -$ or $1^{11} (1.51) 1.0 RR$ $\grave{E}^{"} = - + \acute{1}^{"} \mathring{1}^{"}$

```
_{Of} 2 1

_{R \ 0.5} = or R = 1.0 m

_{now} ^{2} 4 D n R _{n} = I

for n = 7

_{7} D 4 7 5.896 10 1.0 ^{-} = _{7} _{7} _{7} _{7} = 4.063 _{7} _{7} _{7} _{7} = 4.063 _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7} _{7}
```

Example 41 Light source emitting the light of wavelengths $I_1 = 6.0 \pm 10^{-7}$ m and $I_2 = 4.8 \pm 10^{-7}$ m is used to obtain Newton's rings in reflected light. It is found that the nth dark ring of I_1 coincides with $(n + 1)^{th}$ dark ring of I_2 . If the radius of curvature of the curved surface of the lens is 0.96 m. Calculate the diameter of $(n + 1)^{th}$ dark ring of I_2 .

Solution Given $I_1 = 6.0 \pm 10^{-7} \text{ m}$, $I_2 = 4.8 \pm 10^{-7} \text{ m}$ and R = 0.96 n

The diameter of nth order dark ring of I₁ is

Similarly, the diameter of $(n + 1)^{th}$ order dark ring of I_2



```
0.96 D_{(n+1)} = 3.0358 \times 10^{-3} or D_{(n+1)} = 3.04 \times 10^{-3} m.
```

Example 42 In Newton's ring arrangement a source is emitting two wavelengths $I_1 = 6.0 \pm 10^{-7} \, \text{m}$ and $I_2 = 5.9 \pm 10^{-7} \, \text{m}$. It is found that n^{th} dark ring due to one wavelength coincides with $(n + 1)^{th}$ dark ring due to the other. Find the diameter of the n^{th} dark ring if radius of curvature of the lens is 0.9 m. Solution Given $I_1 = 6.0 \pm 10^{-7} \, \text{m}$, $I_2 = 5.9 \pm 10^{-7} \, \text{m}$ and $R = 0.9 \, \text{m}$.

The diameter of the nth order dark ring of I₁ is

$$_{11}^{2}()4DnR_{n}II=$$

The diameter of the $(n + 1)^{th}$ order dark ring of I_2 is

-11

$$^{2}_{(1)2(1)2}()4DR_{nn++}II=$$

Since two rings coincide

$$4nI_1R = 4(n + 1)I_2R$$

= = \pm \pm \pm \pm 1

n R

4 4 59 6.0 10 0.9 _n

Now

= 0.01128 m D_n = 0.0113 m

terference 53

Example 43 Newton's rings are formed using light of wavelength 5896 Å in reflected light with a liquid placed between plane and curved surfaces.

The diameter of 7th bright fringe is 0.4 cm and the radius of curvature is 1.0 m. Evaluate the refractive index of liquid.

Solution Given
$$D_7 = 4.0 \ \pm \ 10^{-3} \ m$$
, $I = 5.896 \ \pm \ 10^{-7} \ m$, $R = 1.0 \ m$ and $n = 7$. II
$$n R n D_D \\ -- e = e \\ 2(2 \ 1) \ 2(2 \ 1) \\ or = 2$$

$$R_n \\ m \\ 13 \ 5.896 \ 10 \\ m \\ \pm \ \pm \ \pm \ 2 \\ 1.0$$

$$R_1 \\ m \\ 0.96$$

Example 44 If the diameter of n^{th} dark ring in an arrangement giving Newton's ring changes from 0.3 cm and 0.25 cm as liquid is introduced between the lens and the plate, calculate the value of the refractive index of the liquid and also calculate the velocity of light in the liquid. Velocity of light in vacuum is 3 ± 10^8 m/sec. Solution Given $D_n = 3.0 \pm 10^{-3}$ m, $D_n = 2.5 \pm 10^{-3}$ m Formula used is $^2 4$ D n R $_n = 1$

Example 45 The Newton's rings are seen in reflected light of wavelength 5896Å. The radius of curvature of plano-convex lens is 1.0 meter. An air film is replaced by a liquid whose refractive index is to be calculated under the conditions if 16th ring is dark and its diameter is 5.1 mm.

Solution Given
$$D_{16}$$
 = 5.1 \(\neq 10^{-3}\) m, I = 5.896 \(\neq 10^{-7}\) m and R = 1.0 m n R n R D

Example 46 The Newton's rings are observed in reflected light of wavelength 6300 Å. A thin layer of liquid of refractive index 1.63 is formed between curved surface of plano-convex lens (m = 1.69) and plane glass plate (m = 1.03) and the radius of curvature of the curvex lens is 0.9 m. Find the radius of smallest dark ring. Solution Given I = 6.3 ± 10^{-7} m, m = 1.63 and R = 0.9 m

54 Engineering Physics

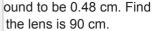
Example 47 Newton's rings are observed with two different media between the glass surfaces. The n^{th} rings have diameters as 10 : 7. Find the ratio of the refractive indices of the two media.

Solution Given Dn¢ : Dn≤ = 10 : 7

or m_1 : m_2 = 49 : 100

Example 48 A combination of convex lens plane glass plate is illuminated by monochromatic light.

n 7 49 10 100





I = 6400 Å

Example 49 In Newton's rings experiment the diameter of 5th dark ring is reduced to half of its value after placing a liquid between plane glass plate and convex surface. Calculate the refractive index of liquid.

Solution Given $D \phi s = {}^{5}2^{D} \Diamond m = ?$ Formula used is ${}^{2}D_{n} = 4nIR = {}^{2}D_{5} = 4 ¥ 5 ¥ IR or <math>D_{5} = 20IR$

Example 50 Newton's rings by reflection are formed between two bi-convex lenses having equal radii of curvatures as 100 cm each. Calculate the distance between the 5th and 15th dark rings, using monochromatic light of wavelength 5400 Å.

Solution Given I =
$$5.4 \ \mbox{$\stackrel{?}{=}$ 1.0 m}$$
 $^{7}_{24}$ $^{-}$ = = = $\mbox{$\stackrel{?}{=}$}$ $^{7}_{1}$ $^{7}_{1}$ Formula used is $^{1}_{1}$ $^{7}_{1}$ $^{7}_{1}$ $^{7}_{1}$ Formula used is $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{1}$ $^{1}_{2}$ $^{1}_{12}$ $^{1}_{22}$ $^{1}_{22}$

a sheet of ploured the



Example 52
If a movable mirror of Michelson's

interferometer is moved through a distance 0.06 mm, 200 fringes crossed the field of view. Find the wavelength of light.

Solution Given $x = 6.0 \pm 10^{-5}$ m and N = 200 fringes

Formula used is x = NI/2

where x is the separation of movable mirror from the fixed mirror, then $6.0 \pm 10^{-5} = 200 \pm 1/2$ or = 6000 Å

Example 53 In Michelson's interferometer a thin plate is introduced in the path of one of the beams and it is found that 50 band crosses the line of observation. If the wavelength of light used is 5896 Å and m = 1.4, determine the thickness of the plate.

Solution Given n = 50, I = 5896×10^{-10} m and m = 1.4

Example 54 Calculate the distance between successive positions of the movable mirror of Michelson's interferometer giving best fringes in case of a sodium source having wavelengths 5896 Å and 5890 Å. What will be the change in path difference between two successive reappearances of the interference pattern? Solution Given $I_1 = 5.896$ m and $10^{-7}I_2 = 5.89 \times 10^{-7}$ m

56 Engineering Physics

14

2()_{2610x}II

Example 55 In

Michelson's interferometer 100 fringes cross the field of view when the movable mirror is displaced through 0.02948 mm. Calculate the wavelength of monochromatic light used. Solution Given $x = 0.02948 \pm 10^{-3}$ m and n = 100

Formula used is ⁵ ² ² ² ² ² ² ⁹ ⁴⁸ ¹⁰ m ² or ¹⁰⁰

$$x \times n_{n \mid \Gamma}^{+} = = =$$

or I =
$$5.896 \times 10^{-7} \, \text{m} = 5896 \, \text{Å}$$

Example 56 The wavelength of two components of D-lines of sodium are 5890 Å and 5896 Å. By how much distance one of the mirror of Michelson's interferometer be moved so as to obtain consecutive position of maximum distinctness.

Solution Given $I_1 = 5.896 \text{ ¥ } 10^{-7} \text{ m}$ and $I_2 = 5.89 \text{ ¥ } 10^{-7} \text{ m}$

Formula used 12122x

where x is distance through which the movable mirror is moved from one position of maxima to the next, then we have

$$2()_{2610x}^{210}_{12}^{210}_{12}^{210}_{12}^{210}_{18965.8910}$$

x = 0.289 mm

Example 57 In an experiment with Michelson's interferometer, the distance traveled by the mirror for two successive position of maximum distinctness was 0.2945 mm. If the mean wavelength for the two component of sodium D–line is 5893 Å, calculate the difference between the two wavelengths. Solution Given $x = 0.2945 \pm 10^{-3}$ m and $I_{av} = 5.893 \pm 10^{-7}$ m

Example 58 In an experiment for determining the refractive index of a gas using Michelson's interferometer a shift of 140 fringes is observed when all the gas is removed from the tube. If the wavelength of light used is 5460 Å and the length of the tube is 20 cm, calculate the refractive index of the gas. Solution Given, $I = 5.46 \pm 10^{-7}$ m, t = 0.2 m and n = 140