

## Design Calculation Sheet for Path

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Location:

City:

Country: Iwelw

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## Secondary Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
6	(6,0,3)	(6,5,3)	5	1.11	0.89
3	(0,0,3)	(0,5,3)	5	1.11	0.89

### Design Limit state:

Combo: 1\*Dead + 1\*Live

Md: 1.11 t.m

Vd: 0.89 ton

### Service Limit State

Combo: LIVE

Span: 5 m

Load: -0.2 t/m'

### Design Checks

#### 1-Check Local Buckling

$dw/tw = 23.92 < 81.98 \Rightarrow$  Compact Web

$c/tf = 3.95 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 94.24 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE270

$fact = 1.44 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$q_{act} = 0.14 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection

$d_{act} = 1.43 \text{ cm} < d_{all} = 1.67 \text{ cm}$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.89$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.06 \text{ t/cm}^2$  &  $q = 0.04 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.09 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.04 \text{ t/cm}^2$  &  $q_{mt} = 0.06 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.07 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.07 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
5	(4,0,3)	(4,5,3)	5	2.21	1.76
4	(2,0,3)	(2,5,3)	5	2.21	1.76

### Design Limit state:

Combo: 1\*Dead + 1\*Live

$M_d = 2.21 \text{ t.m}$

$V_d = 1.76$  ton

### Service Limit State

Combo: LIVE

Span: 5 m

Load: -0.4 t/m'

## Design Checks

### 1-Check Local Buckling

$d_w/t_w = 27.93 < 81.98 \Rightarrow$  Compact Web

$c/t_f = 4.36 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 117.48 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

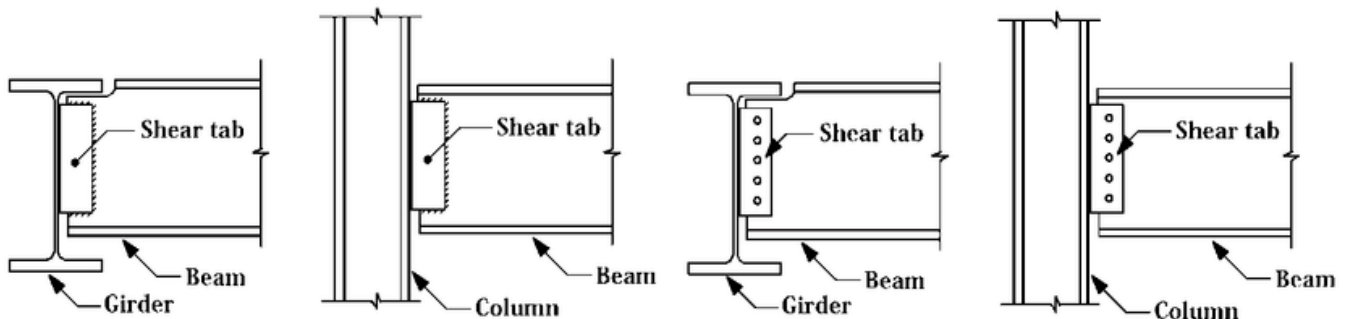
$f_{act} = 1.51 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.19 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$\delta_{act} = 1.17 \text{ cm} < \delta_{all} = 1.67 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 1.76 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.12 \text{ t/cm}^2$  &  $q = 0.08 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.19 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.08 \text{ t/cm}^2$  &  $q_{mt} = 0.12 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.15 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.15 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

## Main Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
2	(0,5,3)	(6,5,3)	6	3.56	1.78
1	(0,0,3)	(6,0,3)	6	3.56	1.78

### Design Limit state:

Combo: 1\*Dead + 1\*Live

Md: 3.56 t.m

Vd: 1.78 ton

### Service Limit State

Combo: LIVE

Span: 6 m

Load: -0.33 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 31.06 < 81.98 \Rightarrow \text{Compact Web}$

$c/t_f = 4.66 < 10.91 \Rightarrow \text{Compact Flange}$

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 142.01 \text{ m} \Rightarrow \text{Supported (No LTB)}$

#### 3-Check Bending Stress

Section: IPE270

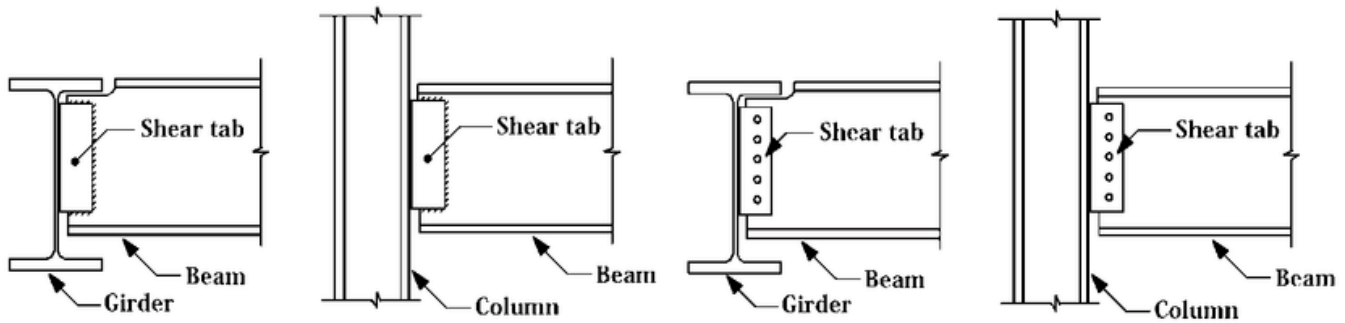
$f_{act} = 1.41 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$q_{act} = 0.14 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$$d_{act} = 0.97 \text{ cm} < d_{all} = 2 \text{ cm}$$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$$V_d = 1.78 \text{ ton}$$

$$R_{least} = 2.85 \text{ ton}$$

$$N = 3 \text{ with Pitch} = 63 \text{ mm \& Full Layout: (31;63 63 31.5)}$$

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$$f = 0.12 \text{ t/cm}^2 \text{ \& } q = 0.08 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.19 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$$q = 0.08 \text{ t/cm}^2 \text{ \& } q_{mt} = 0.12 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.15 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 4-Check Thickness of Plate

$$f = (6 * V_d * e) / (t_p * L^2) = 0.15 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$$

$$\text{Plate Layout} \Rightarrow L = 189 \text{ mm \& } t_p = 10 \text{ mm \& } S_w = 6 \text{ mm}$$

## Columns

Column ID	Start Point	End Point	Height (m)	Nmax (ton)
7	(0,0,0)	(0,0,3)	3	-2.69
8	(6,0,0)	(6,0,3)	3	-2.69
9	(0,5,0)	(0,5,3)	3	-2.69
10	(6,5,0)	(6,5,3)	3	-2.69

#### Design Limit state:

Combo: 1\*Dead + 1\*Live

Nd: -2.69 ton

**1-Check Local Buckling**

$d_w/t_w = 26.08 < 37.44 \Rightarrow$  Compact Web

$c/t_f = 4.21 < 10.91 \Rightarrow$  Compact Flange

**2-Check Normal Stress**

Section: IPE160

$\lambda = 163.04 > 100$

$f_c = 0.13 \text{ t/cm}^2 < F_c = 0.28 \text{ t/cm}^2$

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