

Secondary Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
1	(0,0,6)	(4,0,6)	4	0.05	0.05

Design Limit state:

Combo: 1.2D+1.4L

Md: 0.05 t.m

Vd: 0.05 ton

Service Limit State

Combo: LIVE

Span: 4 m

Load: 0 t/m'

Design Checks

1-Check Local Buckling

$d_w/t_w = 29.65 < 81.98 \Rightarrow$ Compact Web

$c/t_f = 4.56 < 10.91 \Rightarrow$ Compact Flange

2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 129.1 \text{ m} \Rightarrow$ Supported (No LTB)

3-Check Bending Stress

Section: IPE270

$f_{act} = 0.03 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

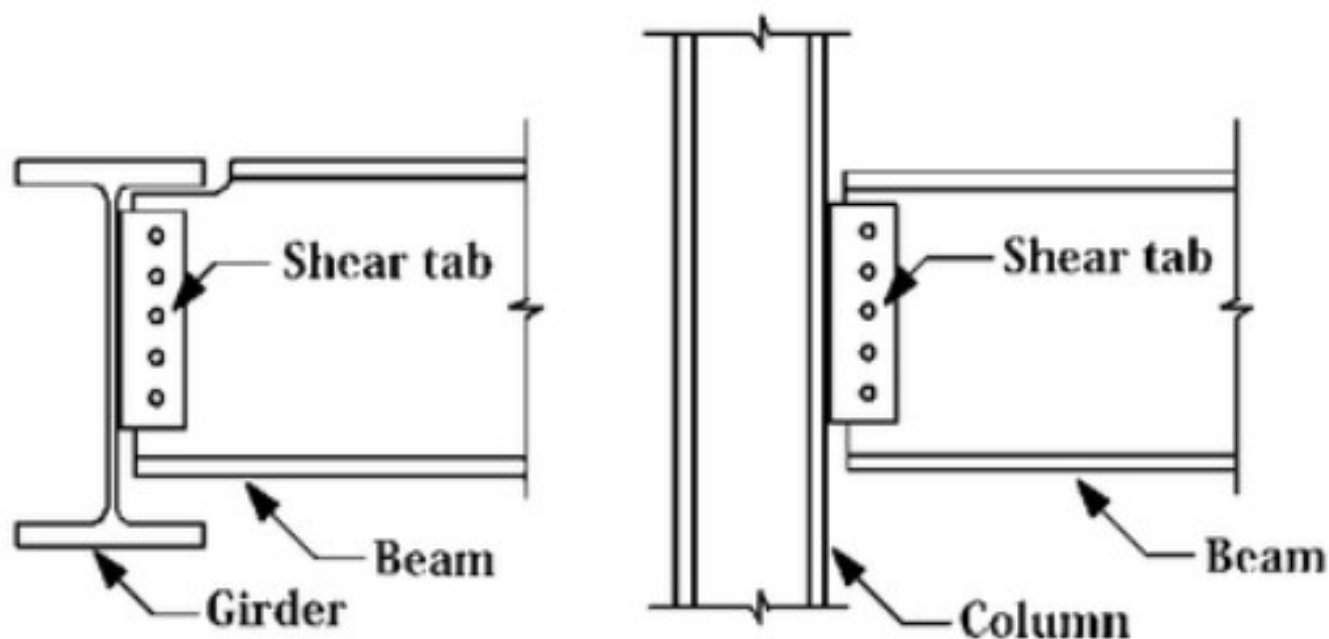
4-Check Shear Stress

$q_{act} = 0 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

5-Check Deflection

$d_{act} = 0 \text{ cm} < d_{all} = 1.33 \text{ cm}$

Group Connection Design (Simple Shear Plate Connection)



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.05$ ton

$R_{least} = 2.85$ ton

$N = 3$ with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0$ t/cm² & $q = 0$ t/cm² $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.01$ t/cm² $< 1.1 * 0.2F_u = 0.79$ t/cm²
 \Rightarrow OK

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0$ t/cm² & $q_{mt} = 0$ t/cm² $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0$ t/cm² $< 0.2F_u = 0.72$ t/cm² \Rightarrow OK

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0$ t/cm² $< 0.72 * F_y = 1.73$ t/cm² \Rightarrow OK IPE270

Plate Layout $\Rightarrow L = 189$ mm & $t_p = 10$ mm & $S_w = 6$ mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
13	(0,20,6)	(4,20,6)	4	2.05	2.05

2	(4,0,6)	(8,0,6)	4	2.05	2.05
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Design Limit state:

Combo: 1.2D+1.4L

Md: 2.05 t.m

Vd: 2.05 ton

Service Limit State

Combo: LIVE

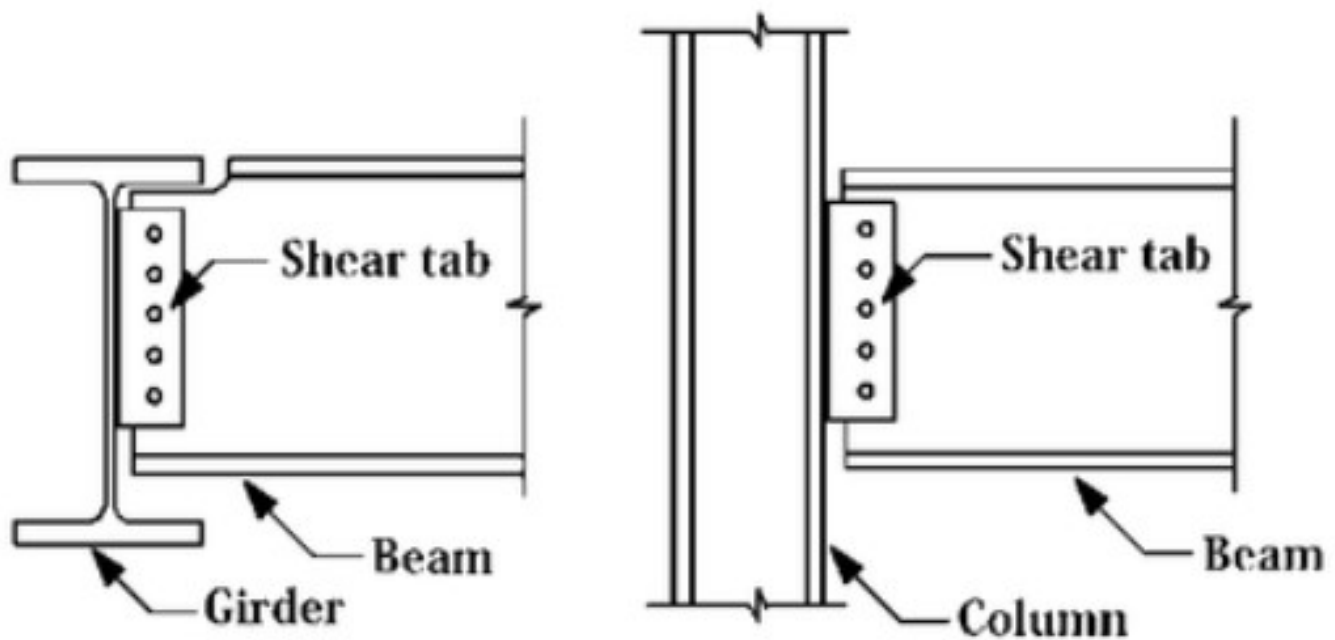
Span: 4 m

Load: -0.5 t/m'

Design Checks**1-Check Local Buckling** $dw/tw = 29.65 < 81.98 \Rightarrow$ Compact Web $c/tf = 4.56 < 10.91 \Rightarrow$ Compact Flange**2-Check Lateral Torsional Buckling** $Lu_{act} = 0 \text{ m} < Lu_{max} = 129.1 \text{ m} \Rightarrow$ Supported (No LTB)**3-Check Bending Stress**

Section: IPE270

 $f_{act} = 1.06 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$ **4-Check Shear Stress** $q_{act} = 0.18 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$ **5-Check Deflection** $d_{act} = 0.41 \text{ cm} < d_{all} = 1.33 \text{ cm}$ **Group Connection Design (Simple Shear Plate Connection)**



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 2.05$ ton

$R_{least} = 2.85$ ton

$N = 3$ with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.14$ t/cm² & $q = 0.09$ t/cm² $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.22$ t/cm² < $1.1 * 0.2F_u = 0.79$ t/cm² \Rightarrow OK

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.09$ t/cm² & $q_{mt} = 0.14$ t/cm² $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.17$ t/cm² < $0.2F_u = 0.72$ t/cm² \Rightarrow OK

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.17$ t/cm² < $0.72 * F_y = 1.73$ t/cm² \Rightarrow OK IPE270

Plate Layout $\Rightarrow L = 189$ mm & $t_p = 10$ mm & $S_w = 6$ mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
15	(6,8,6)	(6,12,6)	4	4.05	4.05

12	(0,18,6)	(4,18,6)	4	4.05	4.05
11	(0,16,6)	(4,16,6)	4	4.05	4.05
10	(0,14,6)	(4,14,6)	4	4.05	4.05
9	(0,12,6)	(4,12,6)	4	4.05	4.05
8	(0,10,6)	(4,10,6)	4	4.05	4.05
7	(0,8,6)	(4,8,6)	4	4.05	4.05
6	(4,6,6)	(8,6,6)	4	4.05	4.05
5	(0,6,6)	(4,6,6)	4	4.05	4.05
4	(4,4,6)	(8,4,6)	4	4.05	4.05
3	(4,2,6)	(8,2,6)	4	4.05	4.05

Design Limit state:

Combo: 1.2D+1.4L

Md: 4.05 t.m

Vd: 4.05 ton

Service Limit State

Combo: LIVE

Span: 4 m

Load: -1 t/m'

Design Checks**1-Check Local Buckling**

$d_w/t_w = 32.39 < 81.98 \Rightarrow$ Compact Web

$c/t_f = 4.81 < 10.91 \Rightarrow$ Compact Flange

2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 154.92 \text{ m} \Rightarrow$ Supported (No LTB)

3-Check Bending Stress

Section: IPE270

$f_{act} = 1.25 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

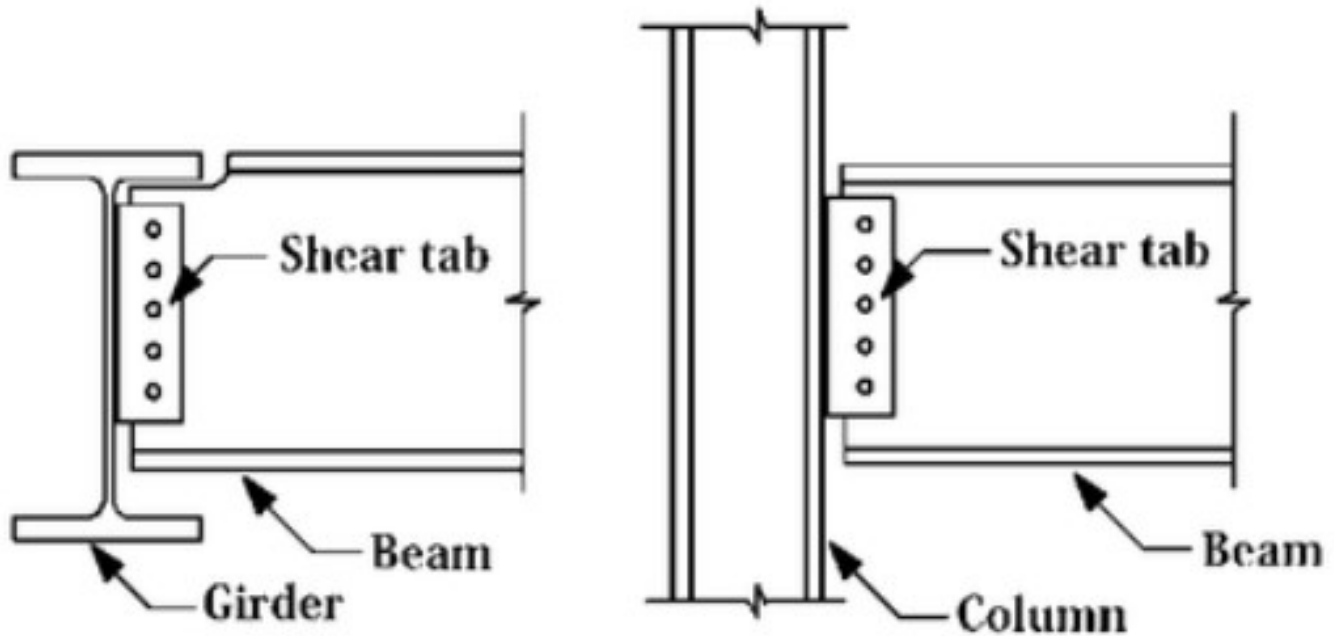
4-Check Shear Stress

$q_{act} = 0.27 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

5-Check Deflection

$$d_{act} = 0.41 \text{ cm} < d_{all} = 1.33 \text{ cm}$$

Group Connection Design (Simple Shear Plate Connection)



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 4.05 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$ with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$$f = 0.28 \text{ t/cm}^2 \text{ \& } q = 0.18 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.43 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$$

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$$q = 0.18 \text{ t/cm}^2 \text{ \& } q_{mt} = 0.28 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.34 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$$

4-Check Thickness of Plate

$$f = (6 * V_d * e) / (t_p * L^2) = 0.34 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK IPE270}$$

Plate Layout $\Rightarrow L = 189 \text{ mm}$ & $t_p = 10 \text{ mm}$ & $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
14	(6,14,6)	(6,20,6)	6	9.19	6.13

Design Limit state:

Combo: 1.2D+1.4L

Md: 9.19 t.m

Vd: 6.13 ton

Service Limit State

Combo: LIVE

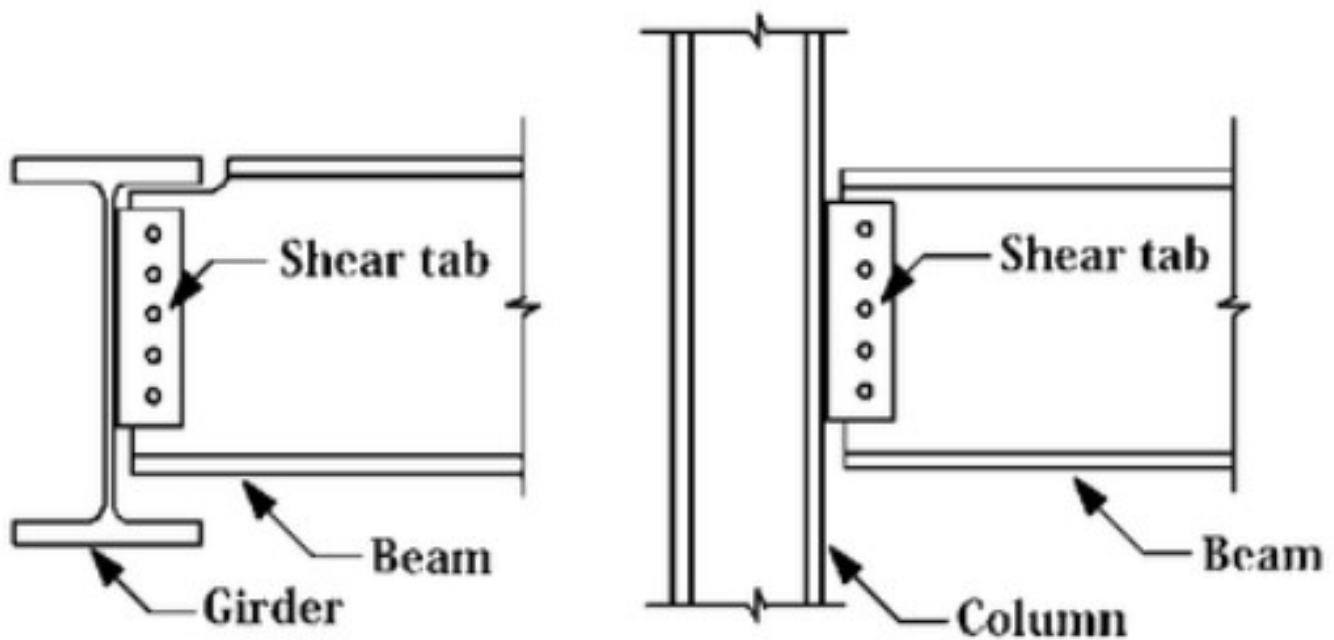
Span: 6 m

Load: -1 t/m'

Design Checks**1-Check Local Buckling** $dw/tw = 37.87 < 81.98 \Rightarrow$ Compact Web $c/tf = 5.64 < 10.91 \Rightarrow$ Compact Flange**2-Check Lateral Torsional Buckling** $Lu_{act} = 0 \text{ m} < Lu_{max} = 206.56 \text{ m} \Rightarrow$ Supported (No LTB)**3-Check Bending Stress**

Section: IPE330

 $f_{act} = 1.29 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$ **4-Check Shear Stress** $q_{act} = 0.25 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$ **5-Check Deflection** $d_{act} = 0.68 \text{ cm} < d_{all} = 2 \text{ cm}$ **Group Connection Design (Simple Shear Plate Connection)**



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 6.13$ ton

$R_{least} = 3.24$ ton

$N = 3$ with Pitch = 77 mm & Full Layout: (38;77 77 38.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.29 \text{ t/cm}^2$ & $q = 0.23 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.49 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.23 \text{ t/cm}^2$ & $q_{mt} = 0.29 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.37 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.35 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK IPE330}$

Plate Layout $\Rightarrow L = 231 \text{ mm}$ & $t_p = 10 \text{ mm}$ & $S_w = 6 \text{ mm}$

Main Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
5	(0,0,6)	(0,6,6)	6	0.19	0.13

Design Limit state:

Combo: 1.2D+1.4L

Md: 0.19 t.m

Vd: 0.13 ton

Service Limit State

Combo: LIVE

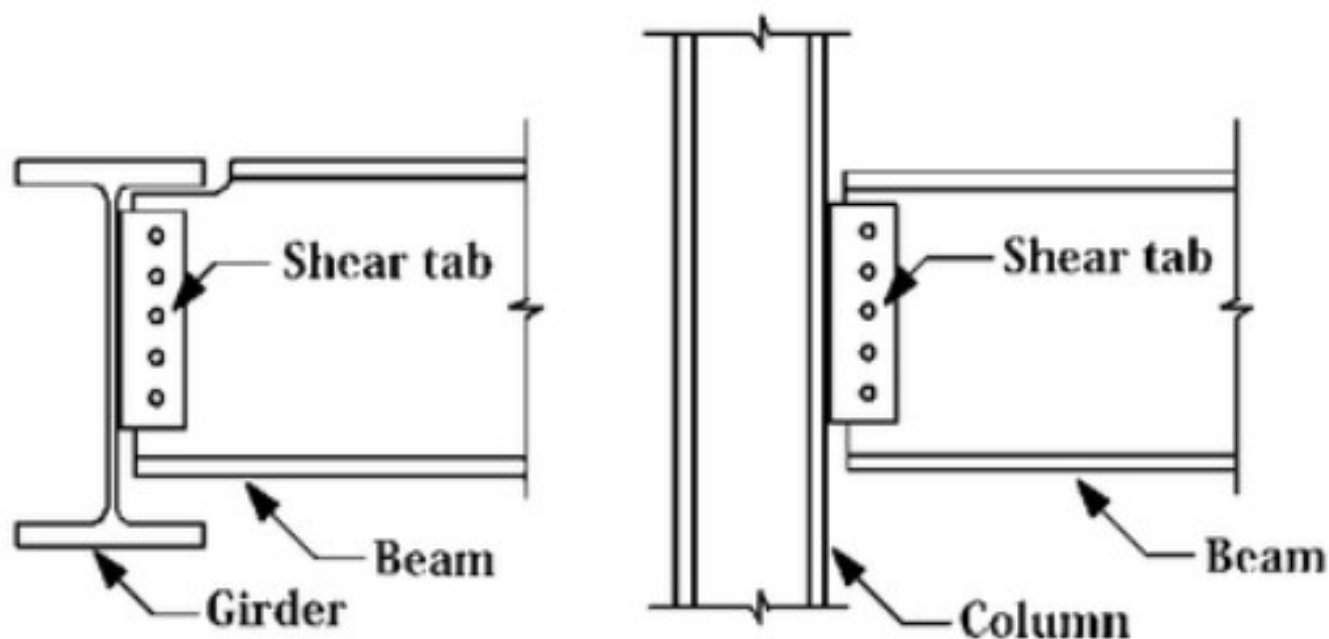
Span: 6 m

Load: 0 t/m'

Design Checks**1-Check Local Buckling** $dw/tw = 34.73 < 81.98 \Rightarrow$ Compact Web $c/tf = 5.3 < 10.91 \Rightarrow$ Compact Flange**2-Check Lateral Torsional Buckling** $Lu_{act} = 0 \text{ m} < Lu_{max} = 174.28 \text{ m} \Rightarrow$ Supported (No LTB)**3-Check Bending Stress**

Section: IPE270

 $f_{act} = 0.05 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$ **4-Check Shear Stress** $q_{act} = 0.01 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$ **5-Check Deflection** $d_{act} = 0 \text{ cm} < d_{all} = 2 \text{ cm}$ **Group Connection Design (Simple Shear Plate Connection)**



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.13$ ton

$R_{least} = 2.85$ ton

$N = 3$ with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.01$ t/cm² & $q = 0.01$ t/cm² $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.01$ t/cm² < $1.1 * 0.2F_u = 0.79$ t/cm² \Rightarrow OK

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.01$ t/cm² & $q_{mt} = 0.01$ t/cm² $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.01$ t/cm² < $0.2F_u = 0.72$ t/cm² \Rightarrow OK

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.01$ t/cm² < $0.72 * F_y = 1.73$ t/cm² \Rightarrow OK IPE270

Plate Layout $\Rightarrow L = 189$ mm & $t_p = 10$ mm & $S_w = 6$ mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
13	(8,14,6)	(8,20,6)	6	4.69	3.13

2	(4,8,6)	(8,8,6)	4	6.11	4.08
1	(4,12,6)	(8,12,6)	4	6.11	4.08
3	(4,20,6)	(8,20,6)	4	6.18	3.12

Design Limit state:

Combo: 1.2D+1.4L

Md: 6.18 t.m

Vd: 3.12 ton

Service Limit State

Combo: LIVE

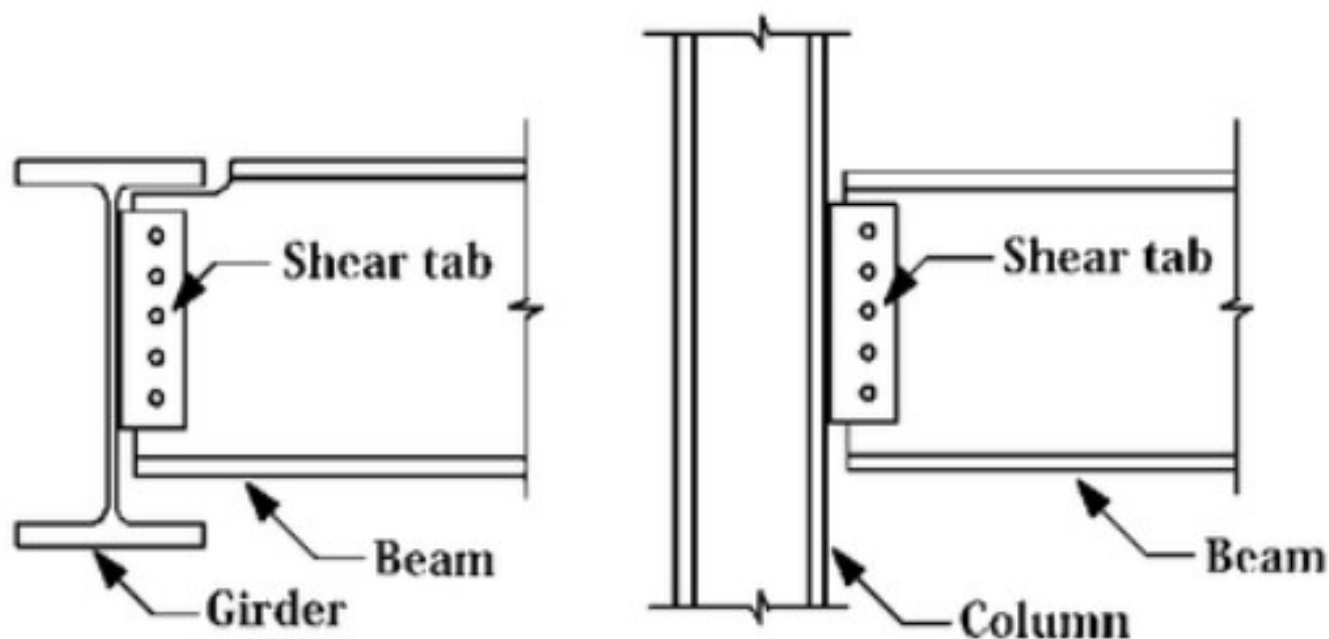
Span: 6 m

Load: -0.5 t/m'

Design Checks**1-Check Local Buckling** $dw/tw = 34.73 < 81.98 \Rightarrow$ Compact Web $c/tf = 5.3 < 10.91 \Rightarrow$ Compact Flange**2-Check Lateral Torsional Buckling** $Lu_{act} = 0 \text{ m} < Lu_{max} = 174.28 \text{ m} \Rightarrow$ Supported (No LTB)**3-Check Bending Stress**

Section: IPE270

 $f_{act} = 1.44 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$ **4-Check Shear Stress** $q_{act} = 0.18 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$ **5-Check Deflection** $d_{act} = 0.69 \text{ cm} < d_{all} = 2 \text{ cm}$ **Group Connection Design (Simple Shear Plate Connection)**



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 3.12$ ton

$R_{least} = 2.85$ ton

$N = 3$ with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.22 \text{ t/cm}^2$ & $q = 0.14 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.33 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.14 \text{ t/cm}^2$ & $q_{mt} = 0.22 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.26 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.26 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK IPE270}$

Plate Layout $\Rightarrow L = 189 \text{ mm}$ & $t_p = 10 \text{ mm}$ & $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
11	(8,0,6)	(8,6,6)	6	8.3	4.18

8	(4,0,6)	(4,6,6)	6	8.3	4.18
7	(0,14,6)	(0,20,6)	6	8.3	4.18
4	(4,14,6)	(8,14,6)	4	10.18	7.12

Design Limit state:

Combo: 1.2D+1.4L

Md: 10.18 t.m

Vd: 7.12 ton

Service Limit State

Combo: LIVE

Span: 6 m

Load: -0.67 t/m'

Design Checks**1-Check Local Buckling**

$dw/tw = 37.87 < 81.98 \Rightarrow$ Compact Web

$c/tf = 5.64 < 10.91 \Rightarrow$ Compact Flange

2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 206.56 \text{ m} \Rightarrow$ Supported (No LTB)

3-Check Bending Stress

Section: IPE330

$f_{act} = 1.43 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

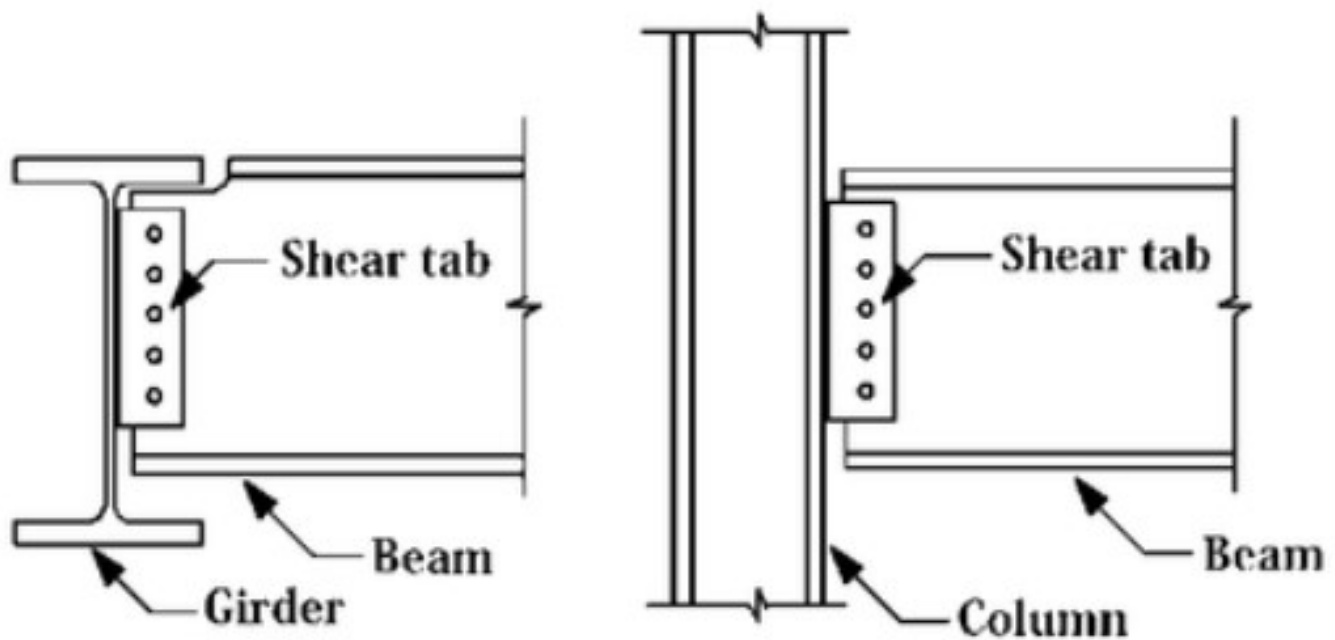
4-Check Shear Stress

$q_{act} = 0.29 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

5-Check Deflection

$d_{act} = 0.46 \text{ cm} < d_{all} = 2 \text{ cm}$

Group Connection Design (Simple Shear Plate Connection)



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 7.12$ ton

$R_{least} = 3.24$ ton

$N = 3$ with Pitch = 77 mm & Full Layout: (38;77 77 38.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.33 \text{ t/cm}^2$ & $q = 0.26 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.57 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.26 \text{ t/cm}^2$ & $q_{mt} = 0.33 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.43 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.4 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK IPE330}$

Plate Layout $\Rightarrow L = 231 \text{ mm}$ & $t_p = 10 \text{ mm}$ & $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
12	(8,6,6)	(8,14,6)	8	12.51	6.25

10	(4,14,6)	(4,20,6)	6	12.8	7.18
6	(0,6,6)	(0,14,6)	8	16.56	6.25

Design Limit state:

Combo: 1.2D+1.4L

Md: 16.56 t.m

Vd: 6.25 ton

Service Limit State

Combo: LIVE

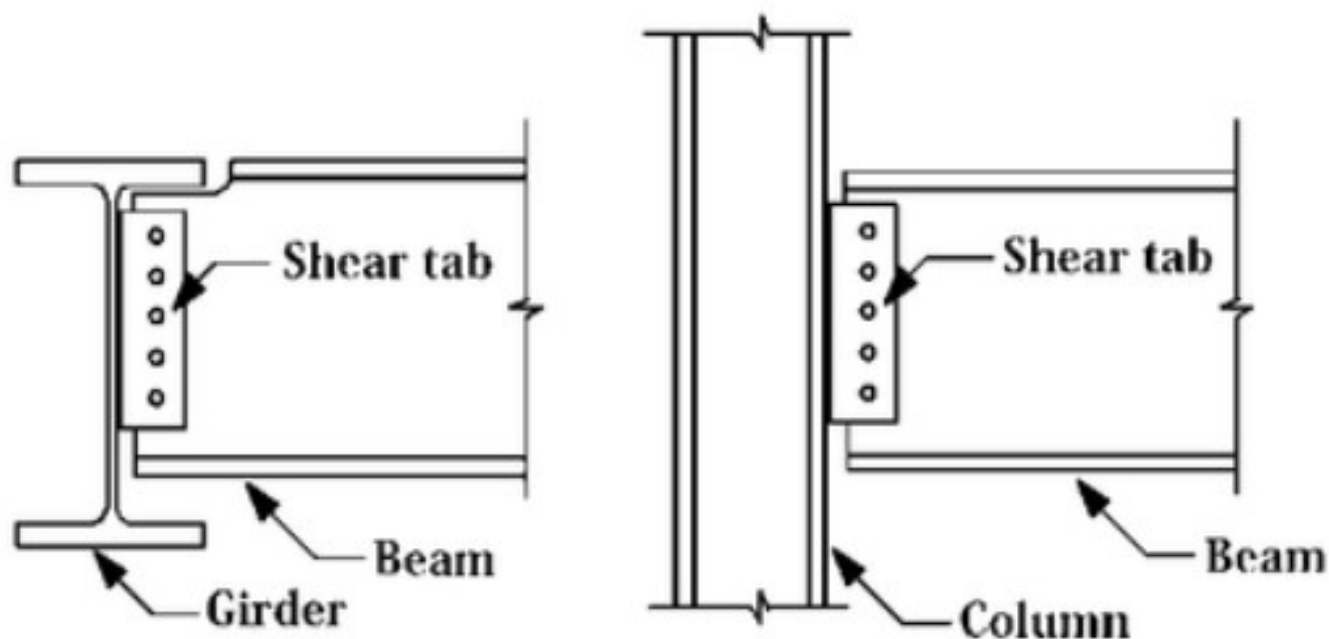
Span: 8 m

Load: -0.75 t/m'

Design Checks**1-Check Local Buckling** $dw/tw = 40.24 < 81.98 \Rightarrow$ Compact Web $c/tf = 5.35 < 10.91 \Rightarrow$ Compact Flange**2-Check Lateral Torsional Buckling** $Lu_{act} = 0 \text{ m} < Lu_{max} = 232.38 \text{ m} \Rightarrow$ Supported (No LTB)**3-Check Bending Stress**

Section: IPE400

 $f_{act} = 1.43 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$ **4-Check Shear Stress** $q_{act} = 0.18 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$ **5-Check Deflection** $d_{act} = 0.82 \text{ cm} < d_{all} = 2.67 \text{ cm}$ **Group Connection Design (Simple Shear Plate Connection)**



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 6.25$ ton

$R_{least} = 3.72$ ton

$N = 3$ with Pitch = 93 mm & Full Layout: (46;93 93 47.5)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.2$ t/cm² & $q = 0.19$ t/cm² $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.38$ t/cm² < $1.1 \cdot 0.2F_u = 0.79$ t/cm² \Rightarrow OK

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.19$ t/cm² & $q_{mt} = 0.2$ t/cm² $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.28$ t/cm² < $0.2F_u = 0.72$ t/cm² \Rightarrow OK

4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.24$ t/cm² < $0.72 \cdot F_y = 1.73$ t/cm² \Rightarrow OK IPE400

Plate Layout $\Rightarrow L = 280$ mm & $t_p = 10$ mm & $S_w = 6$ mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
9	(4,6,6)	(4,14,6)	8	28.72	12.33

Design Limit state:

Combo: 1.2D+1.4L

Md: 28.72 t.m

Vd: 12.33 ton

Service Limit State

Combo: LIVE

Span: 8 m

Load: -1.5 t/m'

Design Checks**1-Check Local Buckling**

$d_w/t_w = 42.75 < 81.98 \Rightarrow$ Compact Web

$c/t_f = 4.94 < 10.91 \Rightarrow$ Compact Flange

2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 258.2 \text{ m} \Rightarrow$ Supported (No LTB)

3-Check Bending Stress

Section: IPE500

$f_{act} = 1.49 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

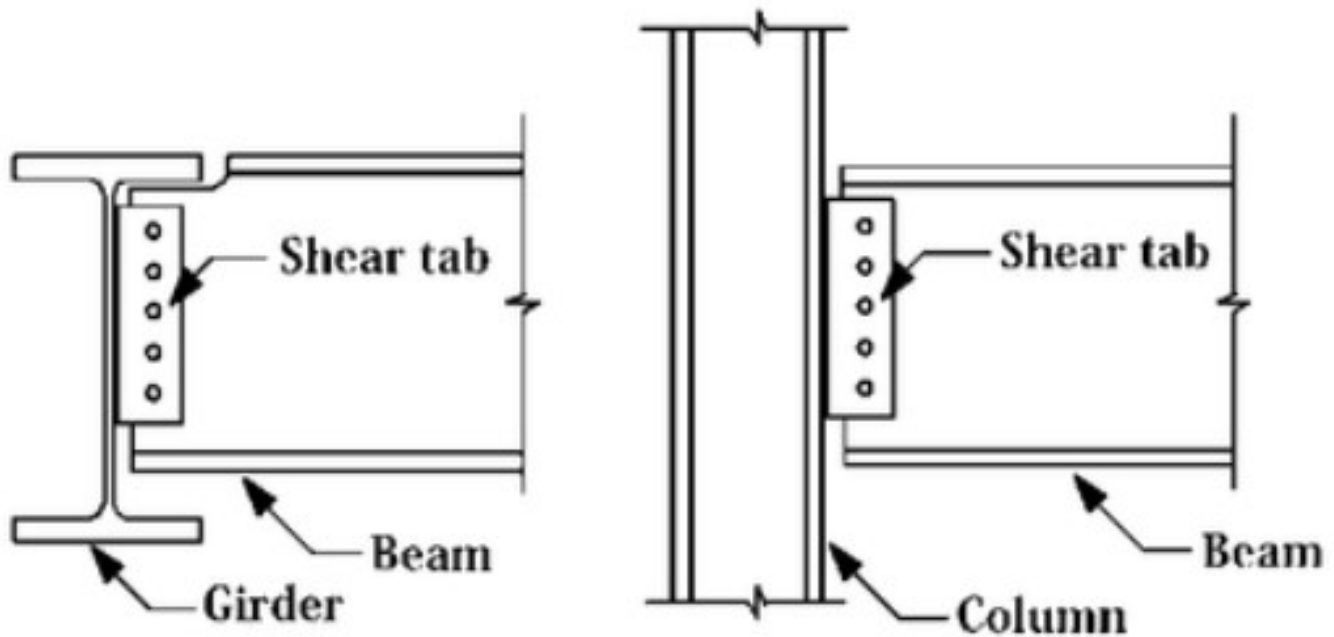
4-Check Shear Stress

$q_{act} = 0.24 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

5-Check Deflection

$d_{act} = 0.79 \text{ cm} < d_{all} = 2.67 \text{ cm}$

Group Connection Design (Simple Shear Plate Connection)



1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 12.33$ ton

$R_{least} = 4.41$ ton

$N = 3$ with Pitch = 116 mm & Full Layout: (58;116 116 60)

2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.25 \text{ t/cm}^2$ & $q = 0.29 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.57 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.29 \text{ t/cm}^2$ & $q_{mt} = 0.25 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.39 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.3 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK IPE500}$

Plate Layout $\Rightarrow L = 350 \text{ mm}$ & $t_p = 10 \text{ mm}$ & $S_w = 6 \text{ mm}$

Columns

Column ID	Start Point	End Point	Height (m)	Nmax (ton)
7	(4,14,0)	(4,14,6)	6	-30.99
6	(4,6,0)	(4,6,6)	6	-24.93
11	(8,14,0)	(8,14,6)	6	-16.81
3	(0,14,0)	(0,14,6)	6	-14.8
10	(8,6,0)	(8,6,6)	6	-14.8
8	(4,20,0)	(4,20,6)	6	-12.66
2	(0,6,0)	(0,6,6)	6	-10.74
5	(4,0,0)	(4,0,6)	6	-6.6
12	(8,20,0)	(8,20,6)	6	-6.55
4	(0,20,0)	(0,20,6)	6	-6.54
9	(8,0,0)	(8,0,6)	6	-6.54
1	(0,0,0)	(0,0,6)	6	-0.49

Design Limit state:

Combo: 1.2D+1.4L

Nd: -30.99 ton

1-Check Local Buckling

$dw/tw = 36.23 < 37.44 \Rightarrow$ Compact Web

$c/tf = 5.68 < 10.91 \Rightarrow$ Compact Flange

2-Check Normal Stress

Section: IPE300

$\lambda = 179.1 > 100$

$f_c = 0.58 \text{ t/cm}^2 < F_c = 0.23 \text{ t/cm}^2$
