

## Design Calculation Sheet for me

Designer: er

Location: ion

City: ty

Country: ry

Date: 2020-06-20 10:06:55

# Table of Contents

## 1-Secondary Beams

- Design For Flexural and shear
- Design For serviceability
- Connections Design

## 2-Main Beams

- Design For Flexural and shear
- Design For serviceability
- Connections Design

## 3-Columns

- Design For Normal Stress

## Secondary Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
7	(20,0,6)	(20,4,6)	4	0.04	0.04

### Design Limit state:

Combo: D+L

Md: 0.04 t.m

Vd: 0.04 ton

### Service Limit State

Combo: LIVE

Span: 4 m

Load: 0 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 15.58 < 81.98 \Rightarrow$  Compact Web

$c/t_f = 3.06 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 59.39 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE270

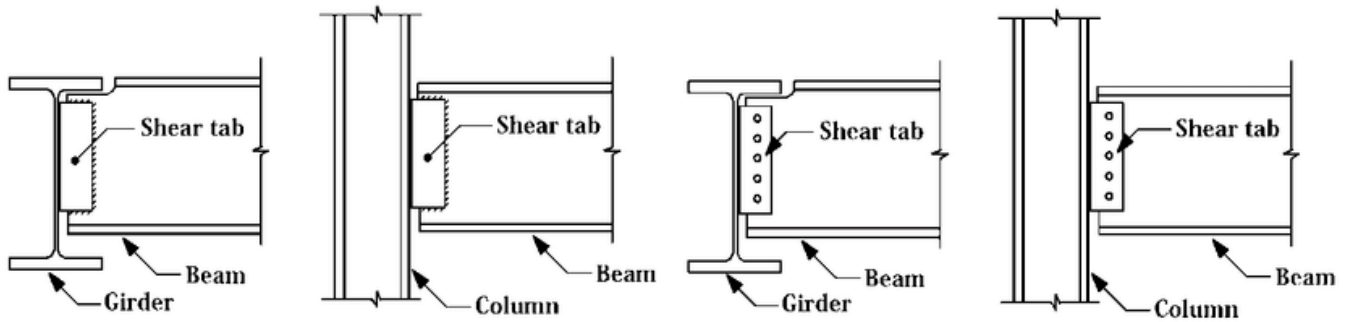
$f_{act} = 0.22 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$q_{act} = 0.01 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection

$d_{act} = 0 \text{ cm} < d_{all} = 1.33 \text{ cm}$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.04$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0$  t/cm<sup>2</sup> &  $q = 0$  t/cm<sup>2</sup>  $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0$  t/cm<sup>2</sup>  $< 1.1 * 0.2F_u = 0.79$  t/cm<sup>2</sup>  $\Rightarrow$  OK

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0$  t/cm<sup>2</sup> &  $q_{mt} = 0$  t/cm<sup>2</sup>  $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0$  t/cm<sup>2</sup>  $< 0.2F_u = 0.72$  t/cm<sup>2</sup>  $\Rightarrow$  OK

#### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0$  t/cm<sup>2</sup>  $< 0.72 * F_y = 1.73$  t/cm<sup>2</sup>  $\Rightarrow$  OK

Plate Layout  $\Rightarrow L = 189$  mm &  $t_p = 10$  mm &  $S_w = 6$  mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
8	(20,4,6)	(20,8,6)	4	1.54	1.54
1	(0,0,6)	(0,4,6)	4	1.54	1.54

#### Design Limit state:

Combo: D+L

$M_d = 1.54$  t.m

$V_d = 1.54$  ton

#### Service Limit State

Combo: LIVE

Span: 4 m

Load: -0.5 t/m'

## Design Checks

### 1-Check Local Buckling

$dw/tw = 26.08 < 81.98 \Rightarrow$  Compact Web

$c/tf = 4.21 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 105.86 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

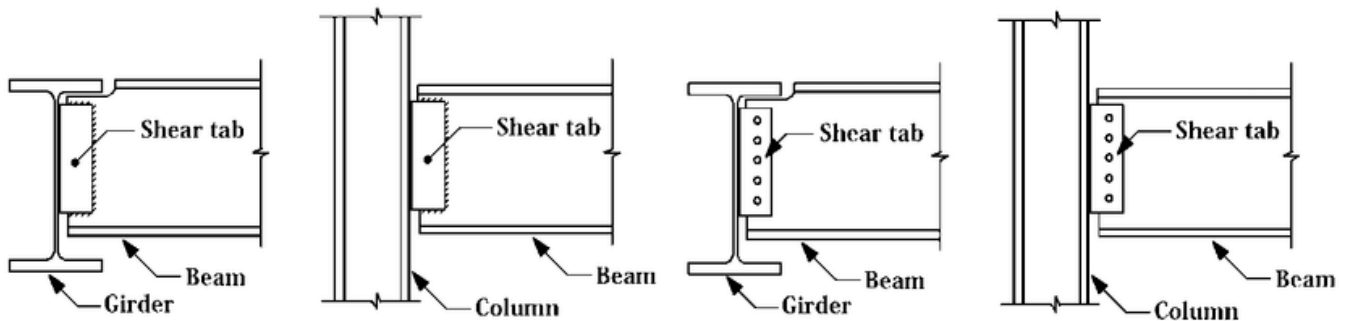
$f_{act} = 1.42 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.19 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$d_{act} = 0.91 \text{ cm} < d_{all} = 1.33 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 1.54 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.11 \text{ t/cm}^2$  &  $q = 0.07 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.16 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.07 \text{ t/cm}^2$  &  $q_{mt} = 0.11 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.13 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.13 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
14	(10,3,6)	(14,3,6)	4	3.04	3.04
12	(6,2,6)	(10,2,6)	4	3.04	3.04
11	(8,7,6)	(12,7,6)	4	3.04	3.04
10	(8,5,6)	(12,5,6)	4	3.04	3.04
6	(18,4,6)	(18,8,6)	4	3.04	3.04
5	(16,4,6)	(16,8,6)	4	3.04	3.04
4	(14,4,6)	(14,8,6)	4	3.04	3.04
3	(4,0,6)	(4,4,6)	4	3.04	3.04
2	(2,0,6)	(2,4,6)	4	3.04	3.04
13	(10,1,6)	(14,1,6)	4	3.18	3.18

### Design Limit state:

Combo: D+L

Md: 3.18 t.m

Vd: 3.18 ton

### Service Limit State

Combo: LIVE

Span: 4 m

Load: -1 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 31.06 < 81.98 \Rightarrow \text{Compact Web}$

$c/t_f = 4.66 < 10.91 \Rightarrow \text{Compact Flange}$

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 142.01 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

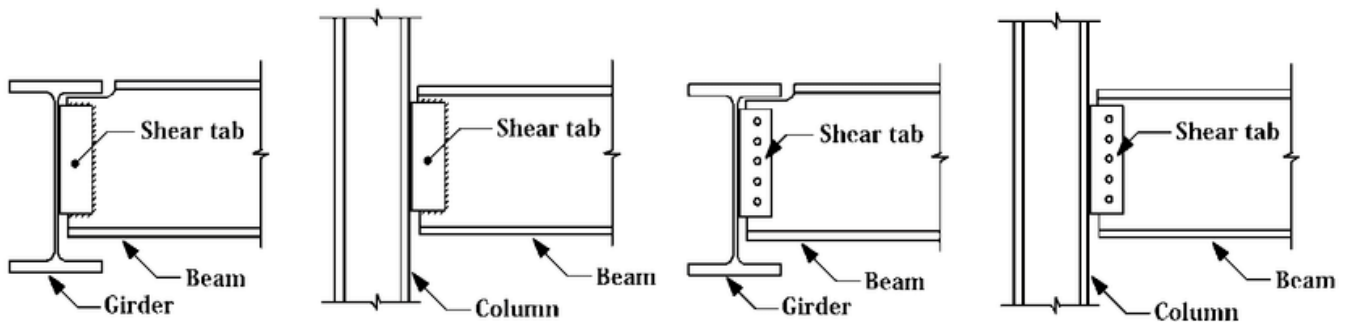
$f_{act} = 1.26 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.25 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$\delta_{act} = 0.57 \text{ cm} < \delta_{all} = 1.33 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 3.18 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.22 \text{ t/cm}^2$  &  $q = 0.14 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.34 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.14 \text{ t/cm}^2$  &  $q_{mt} = 0.22 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.27 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.27 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
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9	(0,6,6)	(6,6,6)	6	6.91	4.61
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### Design Limit state:

Combo: D+L

Md: 6.91 t.m

Vd: 4.61 ton

### Service Limit State

Combo: LIVE

Span: 6 m

Load: -1 t/m'

### Design Checks

#### 1-Check Local Buckling

$dw/tw = 36.23 < 81.98 \Rightarrow$  Compact Web

$c/tf = 5.68 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 193.65 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE300

$f_{act} = 1.24 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

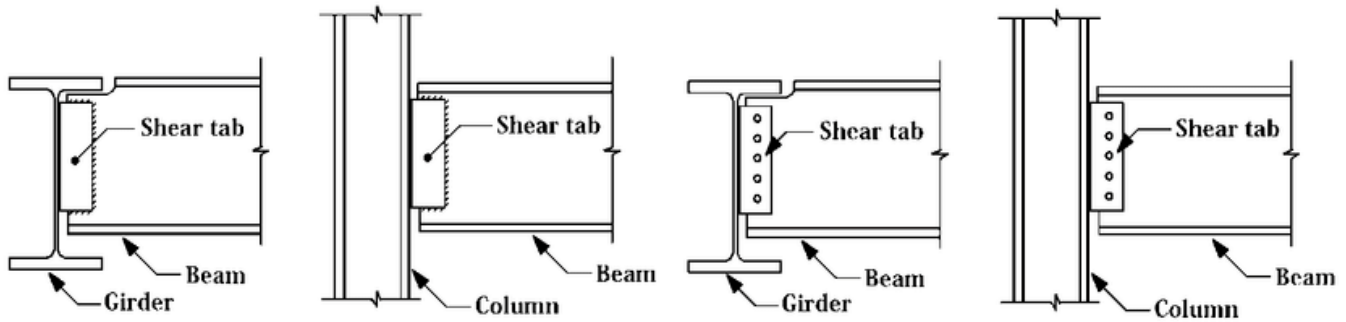
#### 4-Check Shear Stress

$q_{act} = 0.22 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection

$d_{act} = 0.96 \text{ cm} < d_{all} = 2 \text{ cm}$





### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 4.61$  ton

$R_{least} = 3.07$  ton

$N = 3$  with Pitch = 70 mm & Full Layout: (35;70 70 35)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.26$  t/cm<sup>2</sup> &  $q = 0.18$  t/cm<sup>2</sup>  $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.41$  t/cm<sup>2</sup>  $< 1.1 * 0.2F_u = 0.79$  t/cm<sup>2</sup>  $\Rightarrow$  OK

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.18$  t/cm<sup>2</sup> &  $q_{mt} = 0.26$  t/cm<sup>2</sup>  $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.32$  t/cm<sup>2</sup>  $< 0.2F_u = 0.72$  t/cm<sup>2</sup>  $\Rightarrow$  OK

#### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.31$  t/cm<sup>2</sup>  $< 0.72 * F_y = 1.73$  t/cm<sup>2</sup>  $\Rightarrow$  OK

Plate Layout  $\Rightarrow L = 210$  mm &  $t_p = 10$  mm &  $S_w = 6$  mm

## Main Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
10	(14,0,6)	(20,0,6)	6	0.16	0.11

#### Design Limit state:

Combo: D+L

$M_d = 0.16$  t.m

$V_d = 0.11$  ton

#### Service Limit State

Combo: LIVE

Span: 6 m

Load: 0 t/m'

## Design Checks

### 1-Check Local Buckling

$dw/tw = 15.58 < 81.98 \Rightarrow$  Compact Web

$c/tf = 3.06 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 59.39 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

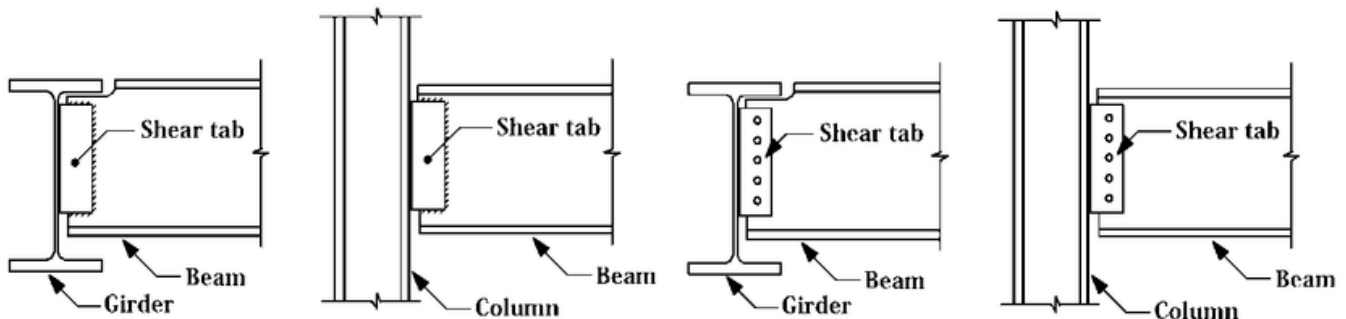
$f_{act} = 0.81 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.04 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$\delta_{act} = 0 \text{ cm} < \delta_{all} = 2 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.11 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.01 \text{ t/cm}^2$  &  $q = 0 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.01 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0 \text{ t/cm}^2$  &  $q_{mt} = 0.01 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.01 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.01 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

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Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
3	(6,0,6)	(6,4,6)	4	3.09	1.57
1	(14,0,6)	(14,4,6)	4	3.18	3.19
14	(0,8,6)	(6,8,6)	6	3.54	2.36
5	(8,4,6)	(8,8,6)	4	4.59	4.59
4	(12,4,6)	(12,8,6)	4	4.59	4.59

### Design Limit state:

Combo: D+L

Md: 4.59 t.m

Vd: 4.59 ton

### Service Limit State

Combo: LIVE

Span: 6 m

Load: -0.5 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 32.39 < 81.98 \Rightarrow \text{Compact Web}$

$c/t_f = 4.81 < 10.91 \Rightarrow \text{Compact Flange}$

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 154.92 \text{ m} \Rightarrow \text{Supported (No LTB)}$

#### 3-Check Bending Stress

Section: IPE270

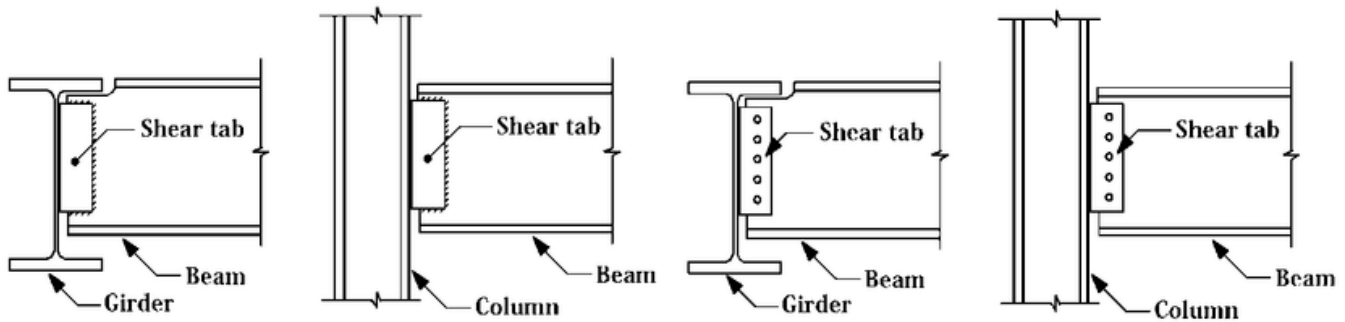
$f_{act} = 1.42 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$$q_{act} = 0.31 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$$

#### 5-Check Deflection

$$\delta_{act} = 1.03 \text{ cm} < \delta_{all} = 2 \text{ cm}$$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$$V_d = 4.59 \text{ ton}$$

$$R_{least} = 2.85 \text{ ton}$$

$$N = 3 \text{ with Pitch} = 63 \text{ mm \& Full Layout: (31;63 63 31.5)}$$

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$$f = 0.32 \text{ t/cm}^2 \text{ \& } q = 0.21 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.48 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$$q = 0.21 \text{ t/cm}^2 \text{ \& } q_{mt} = 0.32 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.38 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 4-Check Thickness of Plate

$$f = (6 * V_d * e) / (t_p * L^2) = 0.39 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$$

$$\text{Plate Layout} \Rightarrow L = 189 \text{ mm \& } t_p = 10 \text{ mm \& } S_w = 6 \text{ mm}$$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
7	(0,4,6)	(0,8,6)	4	4.65	2.35
6	(6,4,6)	(6,8,6)	4	6.15	3.85
2	(10,0,6)	(10,4,6)	4	6.2	4.71
16	(14,8,6)	(20,8,6)	6	6.25	3.15
13	(14,4,6)	(20,4,6)	6	6.25	3.15
8	(0,0,6)	(6,0,6)	6	6.25	3.15

**Design Limit state:**

Combo: D+L

Md: 6.25 t.m

Vd: 3.15 ton

**Service Limit State**

Combo: LIVE

Span: 6 m

Load: -0.67 t/m'

**Design Checks****1-Check Local Buckling**

$dw/tw = 34.73 < 81.98 \Rightarrow$  Compact Web

$c/tf = 5.3 < 10.91 \Rightarrow$  Compact Flange

**2-Check Lateral Torsional Buckling**

$Lu_{act} = 0 \text{ m} < Lu_{max} = 174.28 \text{ m} \Rightarrow$  Supported (No LTB)

**3-Check Bending Stress**

Section: IPE270

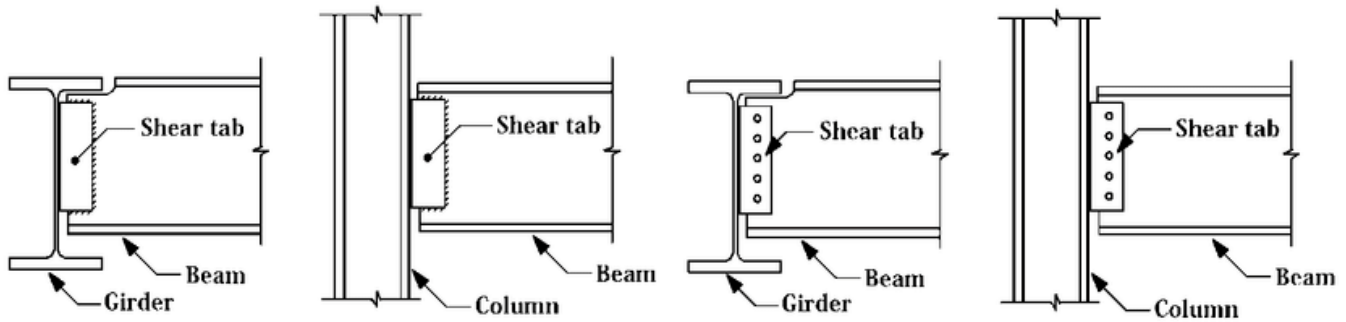
$f_{act} = 1.46 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

**4-Check Shear Stress**

$q_{act} = 0.18 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

**5-Check Deflection**

$d_{act} = 0.93 \text{ cm} < d_{all} = 2 \text{ cm}$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 3.15$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.22 \text{ t/cm}^2$  &  $q = 0.14 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.33 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.14 \text{ t/cm}^2$  &  $q_{mt} = 0.22 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.26 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.26 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
15	(6,8,6)	(14,8,6)	8	9.47	4.73
11	(0,4,6)	(6,4,6)	6	9.63	5.4
9	(6,0,6)	(14,0,6)	8	9.72	2.5

### Design Limit state:

Combo: D+L

$M_d = 9.72 \text{ t.m}$

$V_d = 2.5$  ton

### Service Limit State

Combo: LIVE

Span: 8 m

Load: -0.75 t/m'

### Design Checks

#### 1-Check Local Buckling

$dw/tw = 37.87 < 81.98 \Rightarrow$  Compact Web

$c/tf = 5.64 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 206.56 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE330

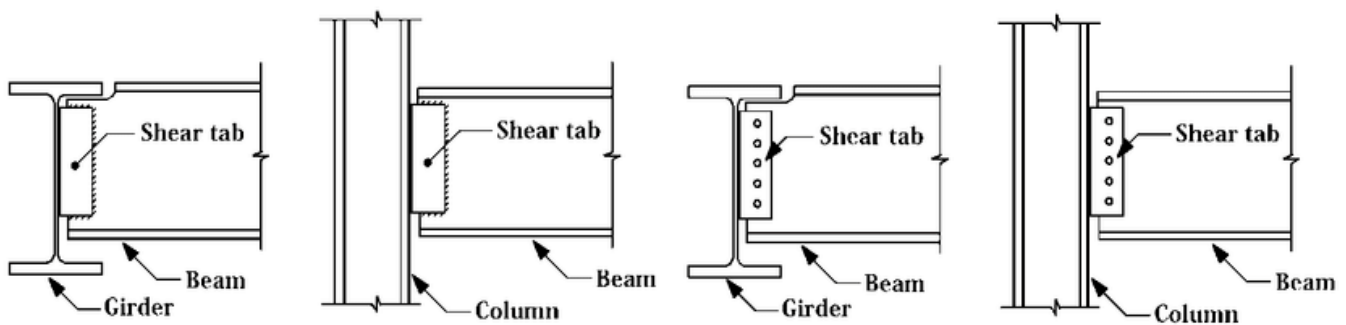
$f_{act} = 1.36 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$q_{act} = 0.1 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection

$d_{act} = 1.62 \text{ cm} < d_{all} = 2.67 \text{ cm}$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 2.5 \text{ ton}$

$R_{least} = 3.24 \text{ ton}$

$N = 3$  with Pitch = 77 mm & Full Layout: (38;77 77 38.5)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.12 \text{ t/cm}^2$  &  $q = 0.09 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.2 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79$

$t/cm^2 \Rightarrow OK$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.09 \text{ t/cm}^2$  &  $q_{mt} = 0.12 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.15 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow OK$

### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.14 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow OK$

Plate Layout  $\Rightarrow L = 231 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

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Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
12	(6,4,6)	(14,4,6)	8	18.76	7.06

### Design Limit state:

Combo: D+L

Md: 18.76 t.m

Vd: 7.06 ton

### Service Limit State

Combo: LIVE

Span: 8 m

Load: -1.12 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 41.66 < 81.98 \Rightarrow$  Compact Web

$c/t_f = 5.19 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 245.29 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE450

$f_{act} = 1.25 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

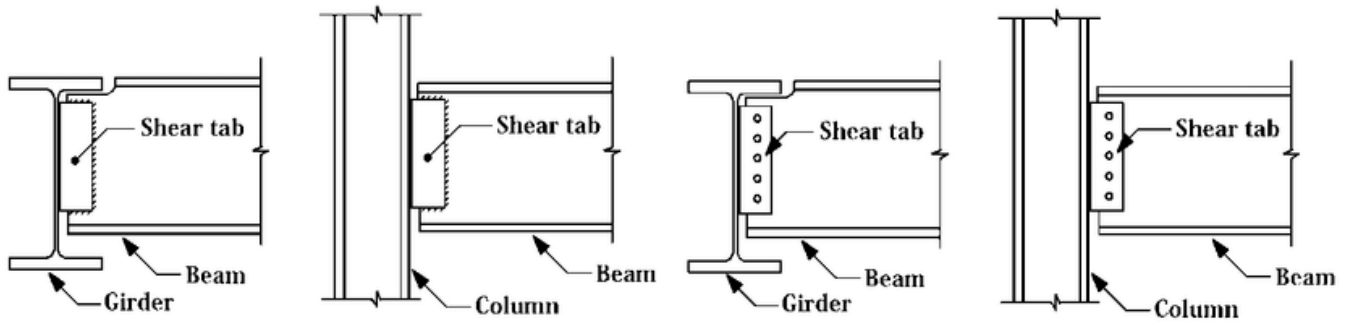
#### 4-Check Shear Stress

$q_{act} = 0.17 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection



$$d_{act} = 0.85 \text{ cm} < d_{all} = 2.67 \text{ cm}$$



### Group Connection Design (Simple Shear Plate Connection)

#### 1-Bolts Design

Bolts: M20 of Grade 8.8

$$V_d = 7.06 \text{ ton}$$

$$R_{least} = 4.06 \text{ ton}$$

N = 3 with Pitch = 105 mm & Full Layout: (52;105 105 52.5)

#### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$$f = 0.18 \text{ t/cm}^2 \text{ \& } q = 0.19 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.38 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$$q = 0.19 \text{ t/cm}^2 \text{ \& } q_{mt} = 0.18 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.26 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$$

#### 4-Check Thickness of Plate

$$f = (6 * V_d * e) / (t_p * L^2) = 0.21 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$$

Plate Layout  $\Rightarrow L = 315 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

## Columns

Column ID	Start Point	End Point	Height (m)	Nmax (ton)
6	(6,4,0)	(6,4,6)	6	-18.13
7	(14,4,0)	(14,4,6)	6	-16.63
10	(6,8,0)	(6,8,6)	6	-11.19
11	(14,8,0)	(14,8,6)	6	-11.19
5	(0,4,0)	(0,4,6)	6	-9.55
2	(6,0,0)	(6,0,6)	6	-7.48

3	(14,0,0)	(14,0,6)	6	-6.06
8	(20,4,0)	(20,4,6)	6	-5
9	(0,8,0)	(0,8,6)	6	-4.96
12	(20,8,0)	(20,8,6)	6	-4.95
1	(0,0,0)	(0,0,6)	6	-4.95
4	(20,0,0)	(20,0,6)	6	-0.41

### Design Limit state:

Combo: D+L

Nd: -18.13 ton

### 1-Check Local Buckling

$dw/tw = 36.23 < 37.44 \Rightarrow$  Compact Web

$c/tf = 5.68 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Normal Stress

Section: IPE300

$\lambda = 179.1 > 100$

$f_c = 0.34 \text{ t/cm}^2 < F_c = 0.23 \text{ t/cm}^2$

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