

## Design Calculation Sheet for ITIFinal02

Designer: abc

Location: mansoura

City: giza

Country: giza

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## Table of Contents

### 1-Secondary Beams

- Design For Flexural and shear
- Design For serviceability
- Connections Design

### 2-Main Beams

- Design For Flexural and shear
- Design For serviceability
- Connections Design

### 3-Columns

- Design For Normal Stress

## Secondary Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
9	(20,4,6)	(20,8,6)	4	0.04	0.04
8	(20,0,6)	(20,4,6)	4	0.04	0.04
5	(14,0,6)	(14,4,6)	4	0.04	0.04
4	(6,0,6)	(6,4,6)	4	0.04	0.04
1	(0,0,6)	(0,4,6)	4	0.04	0.04

### Design Limit state:

Combo: D+L

Md: 0.04 t.m

Vd: 0.04 ton

### Service Limit State

Combo: LIVE

Span: 4 m

Load: 0 t/m'

### Design Checks

#### 1-Check Local Buckling

$dw/tw = 15.58 < 81.98 \Rightarrow$  Compact Web

$c/tf = 3.06 < 10.91 \Rightarrow$  Compact Flange

#### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 59.39 \text{ m} \Rightarrow$  Supported (No LTB)

#### 3-Check Bending Stress

Section: IPE270

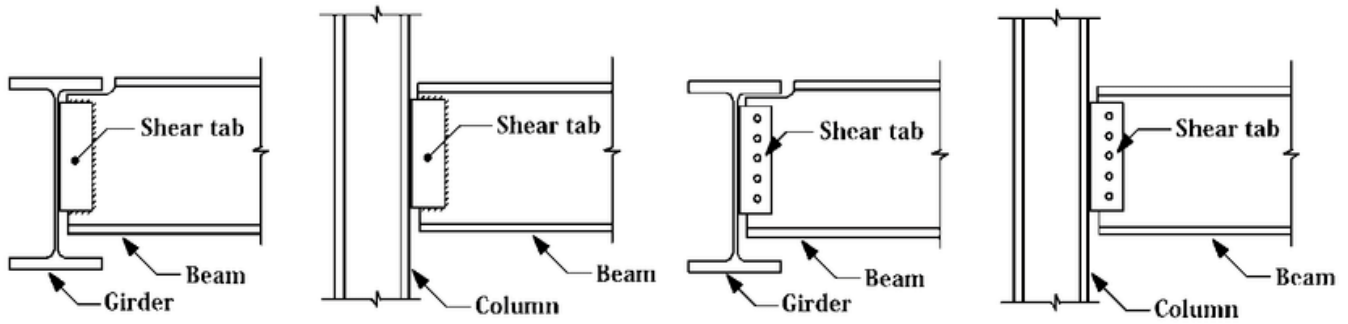
$f_{act} = 0.22 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

#### 4-Check Shear Stress

$q_{act} = 0.01 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

#### 5-Check Deflection

$d_{act} = 0 \text{ cm} < d_{all} = 1.33 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 0.04$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0$  t/cm<sup>2</sup> &  $q = 0$  t/cm<sup>2</sup>  $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0$  t/cm<sup>2</sup>  $< 1.1 * 0.2F_u = 0.79$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0$  t/cm<sup>2</sup> &  $q_{mt} = 0$  t/cm<sup>2</sup>  $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0$  t/cm<sup>2</sup>  $< 0.2F_u = 0.72$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0$  t/cm<sup>2</sup>  $< 0.72 * F_y = 1.73$  t/cm<sup>2</sup>  $\Rightarrow$  OK

Plate Layout  $\Rightarrow L = 189$  mm &  $t_p = 10$  mm &  $S_w = 6$  mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
15	(8,3,6)	(12,3,6)	4	2.04	2.04
14	(8,1,6)	(12,1,6)	4	2.04	2.04
13	(10,7,6)	(14,7,6)	4	2.04	2.04
12	(10,5,6)	(14,5,6)	4	2.04	2.04
11	(6,6,6)	(10,6,6)	4	2.04	2.04
7	(18,4,6)	(18,8,6)	4	2.04	2.04
6	(16,4,6)	(16,8,6)	4	2.04	2.04
3	(4,0,6)	(4,4,6)	4	2.04	2.04
2	(2,0,6)	(2,4,6)	4	2.04	2.04

**Design Limit state:**

Combo: D+L

Md: 2.04 t.m

Vd: 2.04 ton

**Service Limit State**

Combo: LIVE

Span: 4 m

Load: -1 t/m'

**Design Checks****1-Check Local Buckling**

$dw/tw = 27.93 < 81.98 \Rightarrow$  Compact Web

$c/tf = 4.36 < 10.91 \Rightarrow$  Compact Flange

**2-Check Lateral Torsional Buckling**

$Lu_{act} = 0 \text{ m} < Lu_{max} = 117.48 \text{ m} \Rightarrow$  Supported (No LTB)

**3-Check Bending Stress**

Section: IPE270

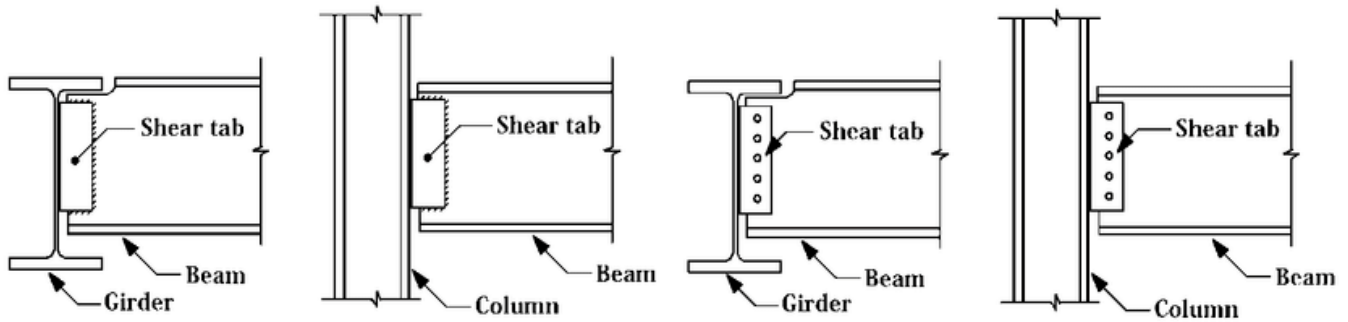
$f_{act} = 1.4 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

**4-Check Shear Stress**

$q_{act} = 0.21 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

**5-Check Deflection**

$d_{act} = 1.2 \text{ cm} < d_{all} = 1.33 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 2.04$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.14$  t/cm<sup>2</sup> &  $q = 0.09$  t/cm<sup>2</sup>  $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.22$  t/cm<sup>2</sup>  $< 1.1 * 0.2F_u = 0.79$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.09$  t/cm<sup>2</sup> &  $q_{mt} = 0.14$  t/cm<sup>2</sup>  $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.17$  t/cm<sup>2</sup>  $< 0.2F_u = 0.72$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.17$  t/cm<sup>2</sup>  $< 0.72 * F_y = 1.73$  t/cm<sup>2</sup>  $\Rightarrow$  OK

Plate Layout  $\Rightarrow L = 189$  mm &  $t_p = 10$  mm &  $S_w = 6$  mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
10	(0,6,6)	(6,6,6)	6	4.66	3.11

### Design Limit state:

Combo: D+L

Md: 4.66 t.m

Vd: 3.11 ton

### Service Limit State

Combo: LIVE

Span: 6 m

Load: -1 t/m'

## Design Checks

### 1-Check Local Buckling

$d_w/t_w = 34.73 < 81.98 \Rightarrow$  Compact Web

$c/t_f = 5.3 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 174.28 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

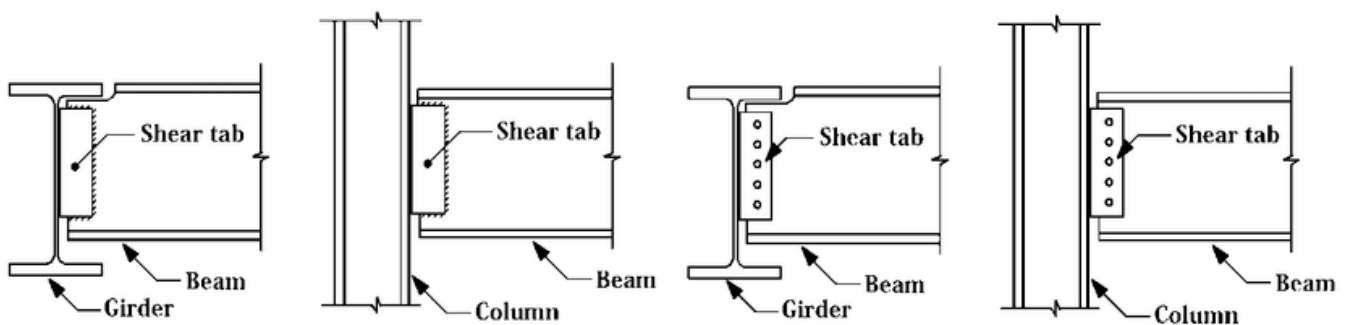
$f_{act} = 1.09 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.17 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$d_{act} = 1.39 \text{ cm} < d_{all} = 2 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 3.11 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.22 \text{ t/cm}^2$  &  $q = 0.14 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.33 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.14 \text{ t/cm}^2$  &  $q_{mt} = 0.22 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.26 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.26 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

## Main Beams

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
13	(0,8,6)	(6,8,6)	6	0.16	0.11
9	(14,0,6)	(20,0,6)	6	0.16	0.11

#### Design Limit state:

Combo: D+L

Md: 0.16 t.m

Vd: 0.11 ton

#### Service Limit State

Combo: LIVE

Span: 6 m

Load: 0 t/m'

#### Design Checks

##### 1-Check Local Buckling

$d_w/t_w = 15.58 < 81.98 \Rightarrow \text{Compact Web}$

$c/t_f = 3.06 < 10.91 \Rightarrow \text{Compact Flange}$

##### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 59.39 \text{ m} \Rightarrow \text{Supported (No LTB)}$

##### 3-Check Bending Stress

Section: IPE270

$f_{act} = 0.81 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

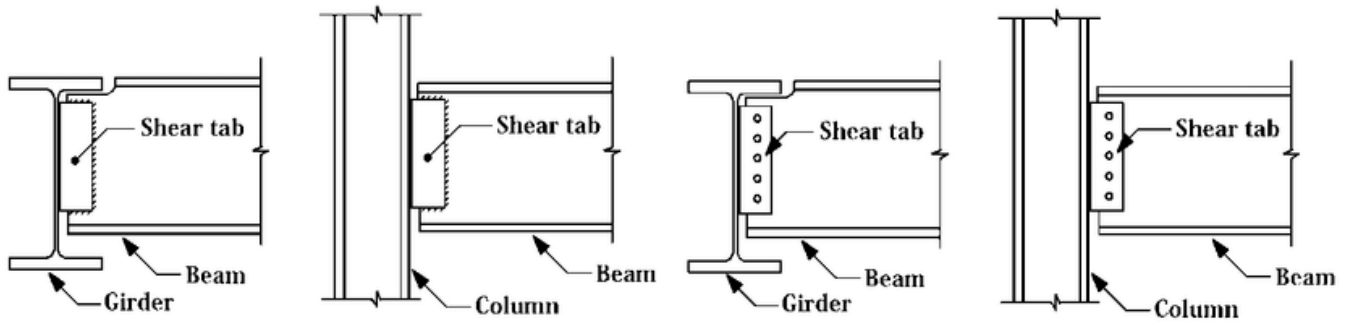
##### 4-Check Shear Stress

$q_{act} = 0.04 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

##### 5-Check Deflection



dact= 0 cm < dall= 2 cm



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

Vd= 0.11 ton

Rleast= 2.85 ton

N= 3 with Pitch= 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.01 \text{ t/cm}^2$  &  $q = 0 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.01 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0 \text{ t/cm}^2$  &  $q_{mt} = 0.01 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.01 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.01 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
3	(14,4,6)	(14,8,6)	4	2.09	2.09
2	(8,0,6)	(8,4,6)	4	2.09	2.09
1	(12,0,6)	(12,4,6)	4	2.09	2.09

### Design Limit state:

Combo: D+L

Md: 2.09 t.m

Vd: 2.09 ton

## Service Limit State

Combo: LIVE

Span: 4 m

Load: -1 t/m'

## Design Checks

### 1-Check Local Buckling

$d_w/t_w = 29.65 < 81.98 \Rightarrow$  Compact Web

$c/t_f = 4.56 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 129.1 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE270

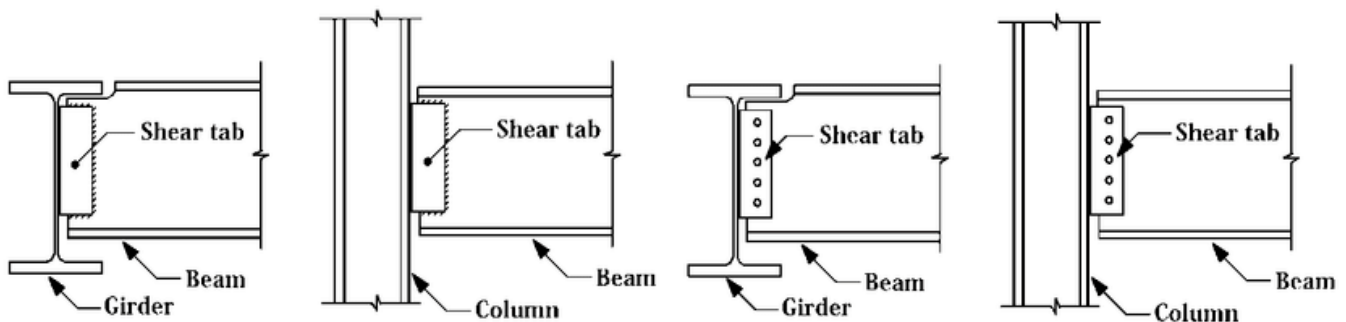
$f_{act} = 1.08 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.19 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$\delta_{act} = 0.82 \text{ cm} < \delta_{all} = 1.33 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 2.09 \text{ ton}$

$R_{least} = 2.85 \text{ ton}$

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.15 \text{ t/cm}^2$  &  $q = 0.09 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.22 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.09 \text{ t/cm}^2$  &  $q_{mt} = 0.15 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.17 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.18 \text{ t/cm}^2 < 0.72 * F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 189 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
6	(0,4,6)	(0,8,6)	4	3.15	1.6
4	(10,4,6)	(10,8,6)	4	4.13	3.11
15	(14,8,6)	(20,8,6)	6	4.25	2.15
12	(14,4,6)	(20,4,6)	6	4.25	2.15
10	(0,4,6)	(6,4,6)	6	4.25	2.15
7	(0,0,6)	(6,0,6)	6	4.25	2.15
8	(6,0,6)	(14,0,6)	8	4.47	2.23

### Design Limit state:

Combo: D+L

Md: 4.47 t.m

Vd: 2.23 ton

### Service Limit State

Combo: LIVE

Span: 8 m

Load: -0.5 t/m'

### Design Checks

#### 1-Check Local Buckling

$d_w/t_w = 34.73 < 81.98 \Rightarrow \text{Compact Web}$

$c/t_f = 5.3 < 10.91 \Rightarrow \text{Compact Flange}$

#### 2-Check Lateral Torsional Buckling

$L_{uact} = 0 \text{ m} < L_{umax} = 174.28 \text{ m} \Rightarrow \text{Supported (No LTB)}$

### 3-Check Bending Stress

Section: IPE270

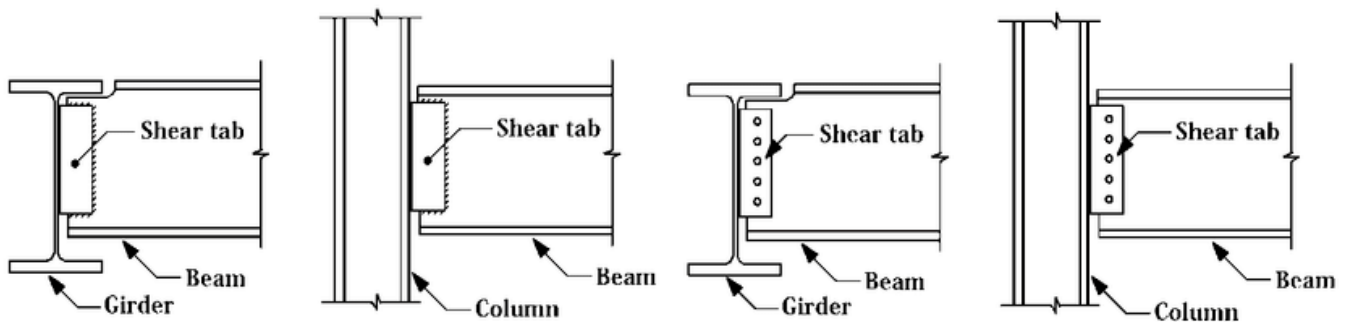
$$fact = 1.04 \text{ t/cm}^2 < Fb = 1.54 \text{ t/cm}^2$$

### 4-Check Shear Stress

$$qact = 0.13 \text{ t/cm}^2 < qall = 0.84 \text{ t/cm}^2$$

### 5-Check Deflection

$$dact = 2.19 \text{ cm} < dall = 2.67 \text{ cm}$$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$$Vd = 2.23 \text{ ton}$$

$$Rleast = 2.85 \text{ ton}$$

$$N = 3 \text{ with Pitch} = 63 \text{ mm \& Full Layout: (31;63 63 31.5)}$$

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$$f = 0.16 \text{ t/cm}^2 \& q = 0.1 \text{ t/cm}^2 \Rightarrow feq = (f^2 + 3q^2)^{0.5} = 0.24 \text{ t/cm}^2 < 1.1 * 0.2Fu = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$$q = 0.1 \text{ t/cm}^2 \& qmt = 0.16 \text{ t/cm}^2 \Rightarrow qres = (q^2 + qmt^2)^{0.5} = 0.19 \text{ t/cm}^2 < 0.2Fu = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$$

### 4-Check Thickness of Plate

$$f = (6 * Vd * e) / (tp * L^2) = 0.19 \text{ t/cm}^2 < 0.72 * Fy = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$$

$$\text{Plate Layout} \Rightarrow L = 189 \text{ mm \& tp} = 10 \text{ mm \& Sw} = 6 \text{ mm}$$

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
5	(6,4,6)	(6,8,6)	4	5.2	2.62
14	(6,8,6)	(14,8,6)	8	6.51	1.7

**Design Limit state:**

Combo: D+L

Md: 6.51 t.m

Vd: 1.7 ton

**Service Limit State**

Combo: LIVE

Span: 8 m

Load: -0.38 t/m'

**Design Checks****1-Check Local Buckling**

$dw/tw = 34.73 < 81.98 \Rightarrow$  Compact Web

$c/tf = 5.3 < 10.91 \Rightarrow$  Compact Flange

**2-Check Lateral Torsional Buckling**

$Lu_{act} = 0 \text{ m} < Lu_{max} = 174.28 \text{ m} \Rightarrow$  Supported (No LTB)

**3-Check Bending Stress**

Section: IPE270

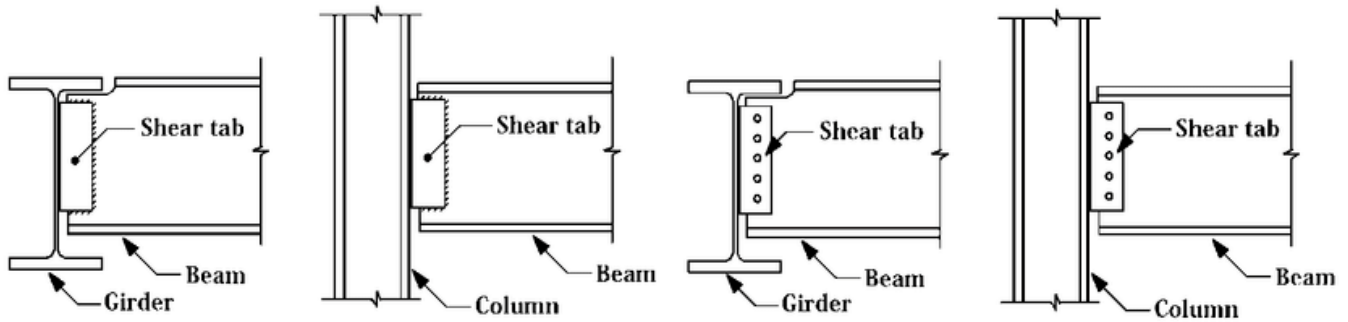
$f_{act} = 1.52 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

**4-Check Shear Stress**

$q_{act} = 0.1 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

**5-Check Deflection**

$d_{act} = 1.64 \text{ cm} < d_{all} = 2.67 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 1.7$  ton

$R_{least} = 2.85$  ton

$N = 3$  with Pitch = 63 mm & Full Layout: (31;63 63 31.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.12$  t/cm<sup>2</sup> &  $q = 0.08$  t/cm<sup>2</sup>  $\Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.18$  t/cm<sup>2</sup>  $< 1.1 * 0.2F_u = 0.79$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.08$  t/cm<sup>2</sup> &  $q_{mt} = 0.12$  t/cm<sup>2</sup>  $\Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.14$  t/cm<sup>2</sup>  $< 0.2F_u = 0.72$  t/cm<sup>2</sup>  $\Rightarrow$  OK

### 4-Check Thickness of Plate

$f = (6 * V_d * e) / (t_p * L^2) = 0.14$  t/cm<sup>2</sup>  $< 0.72 * F_y = 1.73$  t/cm<sup>2</sup>  $\Rightarrow$  OK

Plate Layout  $\Rightarrow L = 189$  mm &  $t_p = 10$  mm &  $S_w = 6$  mm

Beam ID	Start Point	End Point	Span (m)	Mmax (t.m)	Vmax (ton)
11	(6,4,6)	(14,4,6)	8	10.69	3.79

### Design Limit state:

Combo: D+L

Md: 10.69 t.m

Vd: 3.79 ton

### Service Limit State

Combo: LIVE

Span: 8 m

Load: -0.88 t/m'

## Design Checks

### 1-Check Local Buckling

$dw/tw = 37.87 < 81.98 \Rightarrow$  Compact Web

$c/tf = 5.64 < 10.91 \Rightarrow$  Compact Flange

### 2-Check Lateral Torsional Buckling

$Lu_{act} = 0 \text{ m} < Lu_{max} = 206.56 \text{ m} \Rightarrow$  Supported (No LTB)

### 3-Check Bending Stress

Section: IPE330

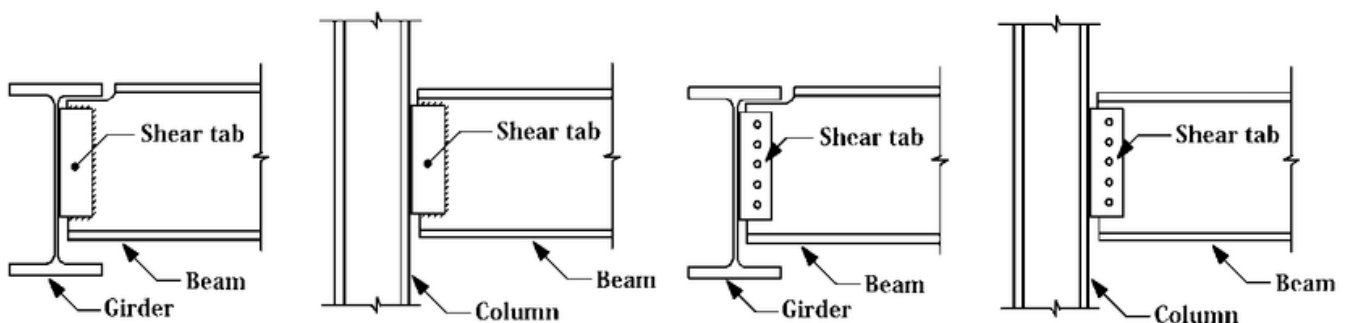
$f_{act} = 1.5 \text{ t/cm}^2 < F_b = 1.54 \text{ t/cm}^2$

### 4-Check Shear Stress

$q_{act} = 0.15 \text{ t/cm}^2 < q_{all} = 0.84 \text{ t/cm}^2$

### 5-Check Deflection

$d_{act} = 1.89 \text{ cm} < d_{all} = 2.67 \text{ cm}$



## Group Connection Design (Simple Shear Plate Connection)

### 1-Bolts Design

Bolts: M20 of Grade 8.8

$V_d = 3.79 \text{ ton}$

$R_{least} = 3.24 \text{ ton}$

$N = 3$  with Pitch = 77 mm & Full Layout: (38;77 77 38.5)

### 2-Stresses Induced in Fillet Weld Lines at Plane(1-1)

$f = 0.18 \text{ t/cm}^2$  &  $q = 0.14 \text{ t/cm}^2 \Rightarrow f_{eq} = (f^2 + 3q^2)^{0.5} = 0.3 \text{ t/cm}^2 < 1.1 * 0.2F_u = 0.79 \text{ t/cm}^2 \Rightarrow \text{OK}$

### 3-Stresses Induced in Fillet Weld Lines at Plane(2-2)

$q = 0.14 \text{ t/cm}^2$  &  $q_{mt} = 0.18 \text{ t/cm}^2 \Rightarrow q_{res} = (q^2 + q_{mt}^2)^{0.5} = 0.23 \text{ t/cm}^2 < 0.2F_u = 0.72 \text{ t/cm}^2 \Rightarrow \text{OK}$

#### 4-Check Thickness of Plate

$f = (6 \cdot V_d \cdot e) / (t_p \cdot L^2) = 0.21 \text{ t/cm}^2 < 0.72 \cdot F_y = 1.73 \text{ t/cm}^2 \Rightarrow \text{OK}$

Plate Layout  $\Rightarrow L = 231 \text{ mm}$  &  $t_p = 10 \text{ mm}$  &  $S_w = 6 \text{ mm}$

## Columns

Column ID	Start Point	End Point	Height (m)	Nmax (ton)
6	(6,4,0)	(6,4,6)	6	-8.86
7	(14,4,0)	(14,4,6)	6	-8.33
11	(14,8,0)	(14,8,6)	6	-6.2
2	(6,0,0)	(6,0,6)	6	-4.69
10	(6,8,0)	(6,8,6)	6	-4.68
5	(0,4,0)	(0,4,6)	6	-4.05
1	(0,0,0)	(0,0,6)	6	-3.45
3	(14,0,0)	(14,0,6)	6	-2.64
8	(20,4,0)	(20,4,6)	6	-2.5
12	(20,8,0)	(20,8,6)	6	-2.45
9	(0,8,0)	(0,8,6)	6	-1.96
4	(20,0,0)	(20,0,6)	6	-0.41

#### Design Limit state:

Combo: D+L

Nd: -8.86 ton

#### 1-Check Local Buckling

$d_w/t_w = 36.23 < 37.44 \Rightarrow \text{Compact Web}$

$c/t_f = 5.68 < 10.91 \Rightarrow \text{Compact Flange}$

#### 2-Check Normal Stress

Section: IPE300

$\lambda = 179.1 > 100$

$f_c = 0.16 \text{ t/cm}^2 < F_c = 0.23 \text{ t/cm}^2$