

# **Lecture (3)**

## **Feedback Amplifiers (II)**

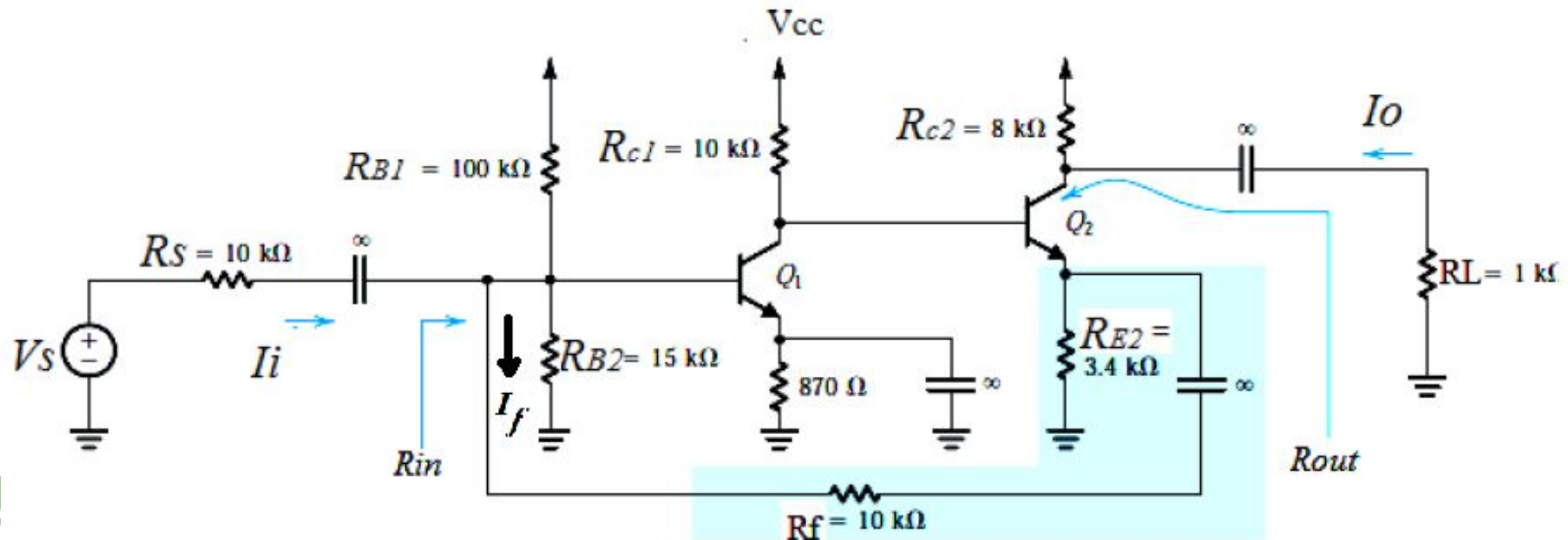
# Example (Shunt-series Feedback)

The circuit shown in Figure represents a Shunt-Series Feedback amplifier circuit.

Analyze the circuit and Calculate:

- (a) The feedback factor  $\beta$  and the open loop gain  $A$ .
- (b) The feedback gain  $A_f$ .
- (c) The feedback input and output resistances ( $R_{if}$  and  $R_{of}$ ).
- (d)  $R_{in}$  and  $R_{out}$ .

Given:  $\beta_1 = \beta_2 = 100$ ,  $r_{e1} = 30\Omega$ ,  $r_{e2} = 35\Omega$ , and  $V_A = \infty$ .



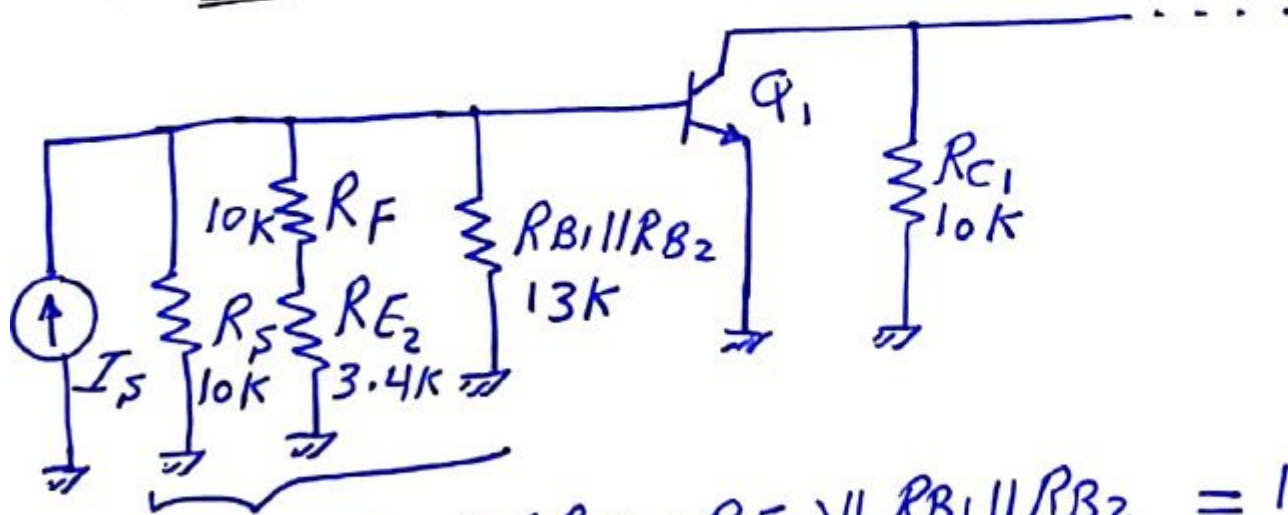
# Solution:

(a) The feedback factor  $\beta$  and the open loop gain  $A$ .

shunt-series F.B  
 $i_{ip} = I$     $o/p = I \rightarrow \therefore$  current amplifier is used.

$$A = \frac{I_o}{I_i}, \quad \beta = \frac{I_f}{I_o}$$

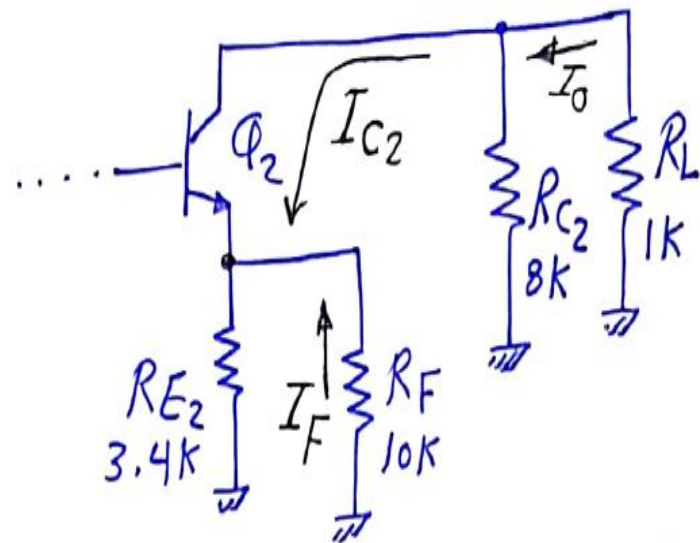
\* The input circuit without feedback (o/p open)



$$R_X = R_S \parallel (R_F + R_{E2}) \parallel R_{B1} \parallel R_{B2} = 10 \parallel 13.4 \parallel 13$$

$$R_X = 3.975 \text{ k}\Omega$$

\* output circuit without feedback (Input = 0)



$$R_Y = R_{E2} \parallel R_F = 3.4 \parallel 10 \approx 2.54 \text{ k}\Omega$$

$$* - I_O = - I_{C2} \frac{R_{C2}}{R_{C2} + R_L} \rightarrow I_O = I_{C2} \frac{R_{C2}}{R_{C2} + R_L}$$

$$\therefore I_O = \frac{8}{9} I_{C2} \rightarrow \boxed{I_{C2} = \frac{9}{8} I_O}$$

$$* - I_F = I_{C2} \frac{R_{E2}}{R_{E2} + R_F}$$

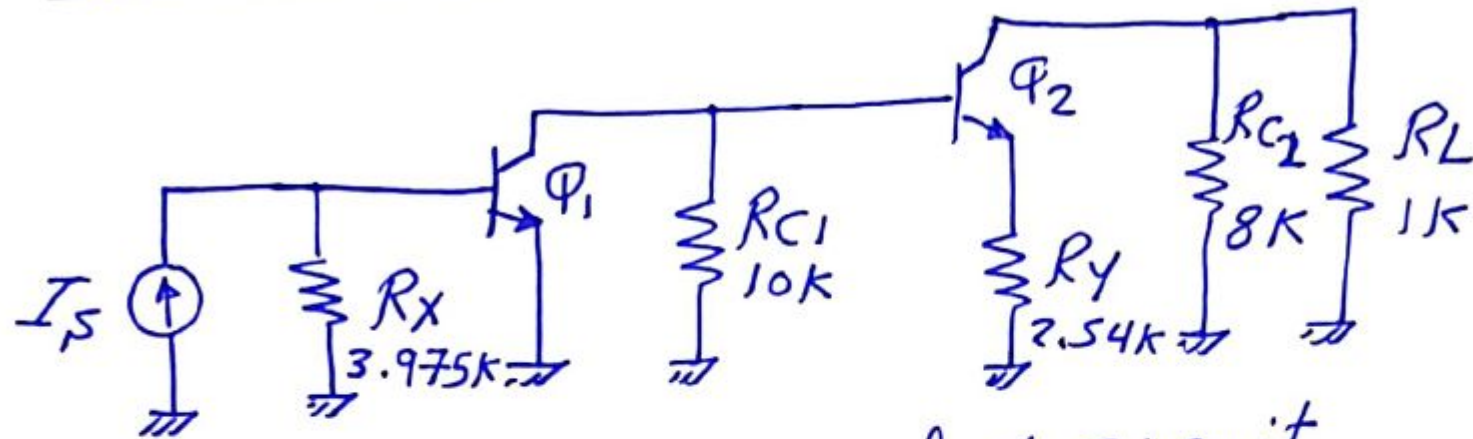
$$\therefore I_F = - \left( \frac{9}{8} I_O \right) \frac{R_{E2}}{R_{E2} + R_F} = - \frac{9}{8} I_O \frac{3.4}{13.4}$$

$$\therefore I_F = - 0.28545 I_O$$

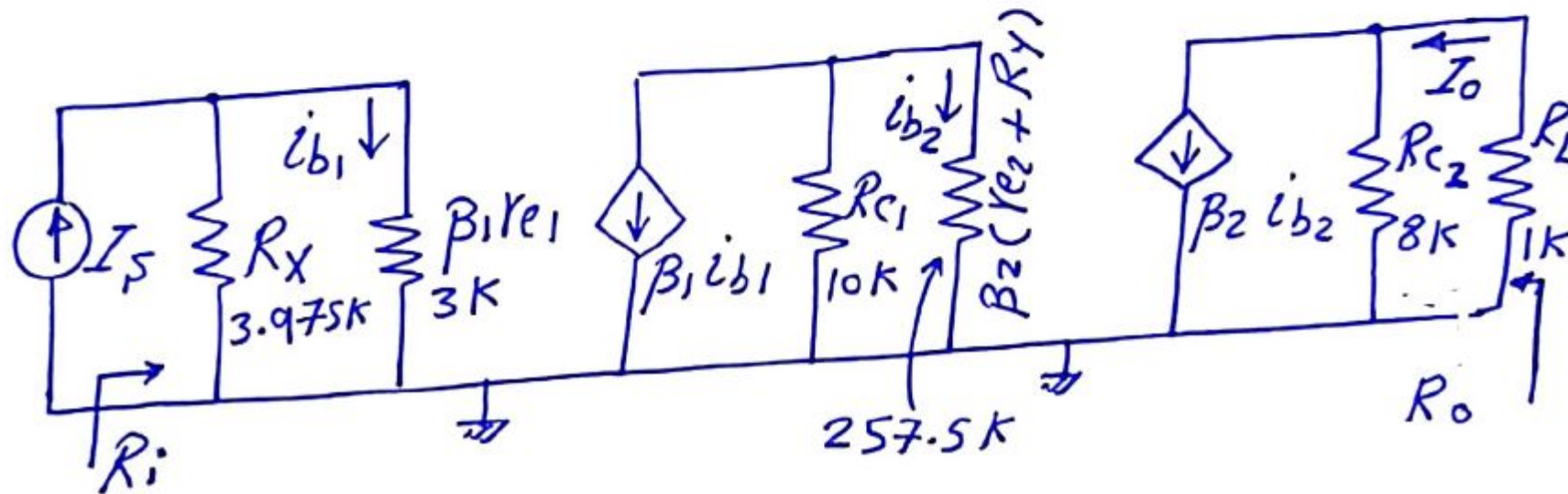
$$\therefore \boxed{\beta = \frac{I_F}{I_O} = - 0.28545} \quad \# \text{ Feedback Factor}$$



## Total Circuit without Feedback



Small-signal A.c equivalent circuit



\* open-Loop gain (A)

$$A = \frac{I_o}{I_s} = \frac{I_o}{i_{b2}} \times \frac{i_{b2}}{i_{b1}} \times \frac{i_{b1}}{I_s}$$

$$* - I_o = -\beta_2 i_{b2} \frac{R_{C2}}{R_{C2} + R_L}$$

$$\therefore \frac{I_o}{i_{b2}} = +\beta_2 \frac{R_{C2}}{R_{C2} + R_L} = \frac{100 \times 8}{8 + 1}$$

$$\boxed{\frac{I_o}{i_{b2}} = \frac{800}{9} = 88.89} \quad [1]$$

$$* i_{b2} = -\beta_1 i_{b1} \frac{R_{C1}}{R_{C1} + \beta_2 (R_{E2} + R_Y)}$$

$$\frac{i_{b2}}{i_{b1}} = \frac{-\beta_1 R_{C1}}{R_{C1} + \beta_2 (R_{E2} + R_Y)} = \frac{-100 \times 10}{10 + 257.5}$$

$$\boxed{\frac{i_{b2}}{i_{b1}} \approx -3.74} \quad [2]$$

$$* i_{b1} = I_s \frac{R_X}{R_X + \beta_1 R_{E1}}$$

$$\frac{i_{b1}}{I_s} = \frac{R_X}{R_X + \beta_1 R_{E1}} = \frac{3.975}{3.975 + 3}$$

$$\boxed{\frac{i_{b1}}{I_s} \approx 0.5699} \approx 0.57 \quad [3]$$

$$\therefore A = (88.89)(-3.74)(0.5699)$$

$$A = -189.46 \quad \# \text{ open-Loop gain}$$

$$\beta = -0.28545 \quad \# \text{ Feedback Factor.}$$



(b) The feedback gain  $A_f$ .

$$1 + A\beta = 1 + 189.46 \times 0.28545 = 55.1$$

$$* A_f = \frac{A}{1 + A\beta} = \frac{-189.46}{55.1} \rightarrow A_f \approx -3.44 \quad \#$$

(c) The feedback input and output resistances ( $R_{if}$  and  $R_{of}$ ).

$$* R_i = R_x \parallel \beta_1 r_{e1} = 1.71 \text{ k}\Omega$$

$$* R_{if} = \frac{R_i}{1 + A\beta} = \frac{1.71}{55.1}$$

$$R_{if} \approx 0.031 \text{ k}\Omega = 31 \Omega \quad \#$$

$$* R_o = R_{c2} \parallel R_L = \frac{8}{9} \text{ k}\Omega = 0.8889 \text{ k}\Omega$$

$$* R_{of} = R_o (1 + A\beta) = \frac{8}{9} \times 55.1$$

$$R_{of} \approx 48.98 \text{ k}\Omega \quad \#$$



(d)  $R_{in}$  and  $R_{out}$ .

$$* R_{in} = \frac{1}{\frac{1}{R_{if}} - \frac{1}{R_s}} = \frac{1}{\frac{1}{0.031} - \frac{1}{10}}$$

$$R_{in} \approx 0.0311 \text{ k}\Omega = 31.1 \Omega \quad \#$$

$$* R_{out} = R_{of} - R_L$$

$$R_{out} = 48.98 - 1$$

$$R_{out} = 47.98 \text{ k}\Omega \quad \#$$

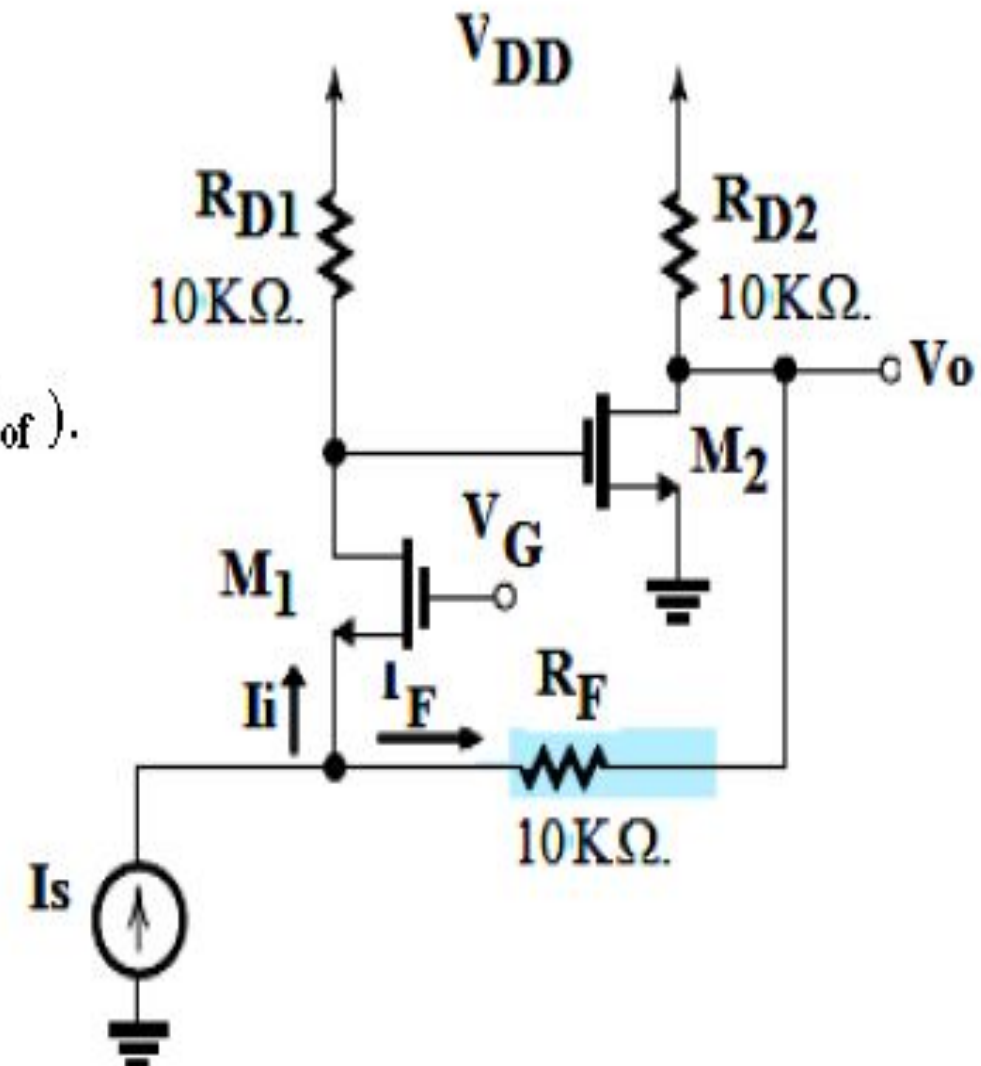


## Example (Shunt-Shunt Feedback)

The circuit shown in Figure represents a **Shunt-Shunt** Feedback amplifier circuit. Analyze the circuit and Calculate:

- (a) The feedback factor ( $\beta$ ) and the open loop gain ( $A$ ).
- (b) The feedback gain  $A_f$ .
- (c) The feedback input and output resistances ( $R_{if}$  and  $R_{of}$ ).

Given:  $g_{m1} = g_{m2} = 2 \text{ mA/V}$  and  $V_A = \infty$ .

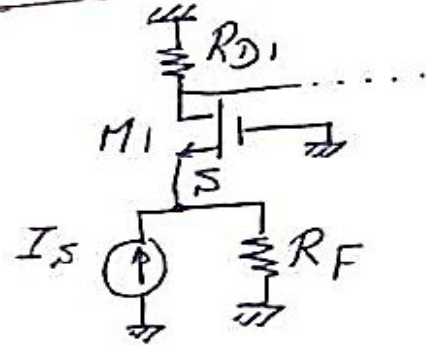


# Solution:

\* Topology      shunt-shunt  
                        I/P        O/P  
                        I        V

$$\therefore A = \frac{V_o}{I_i}, \quad \beta = \frac{I_f}{V_o}$$

\* The input circuit without F.B ( $V_o = 0$ )

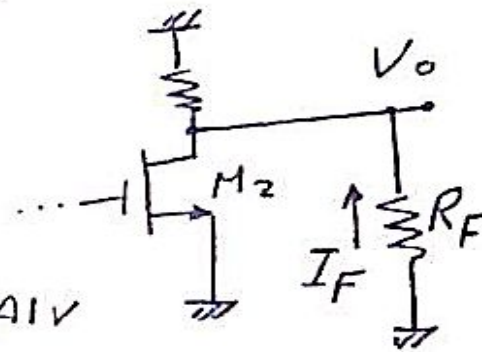


\* The output circuit without F.B ( $I_s = 0$ )

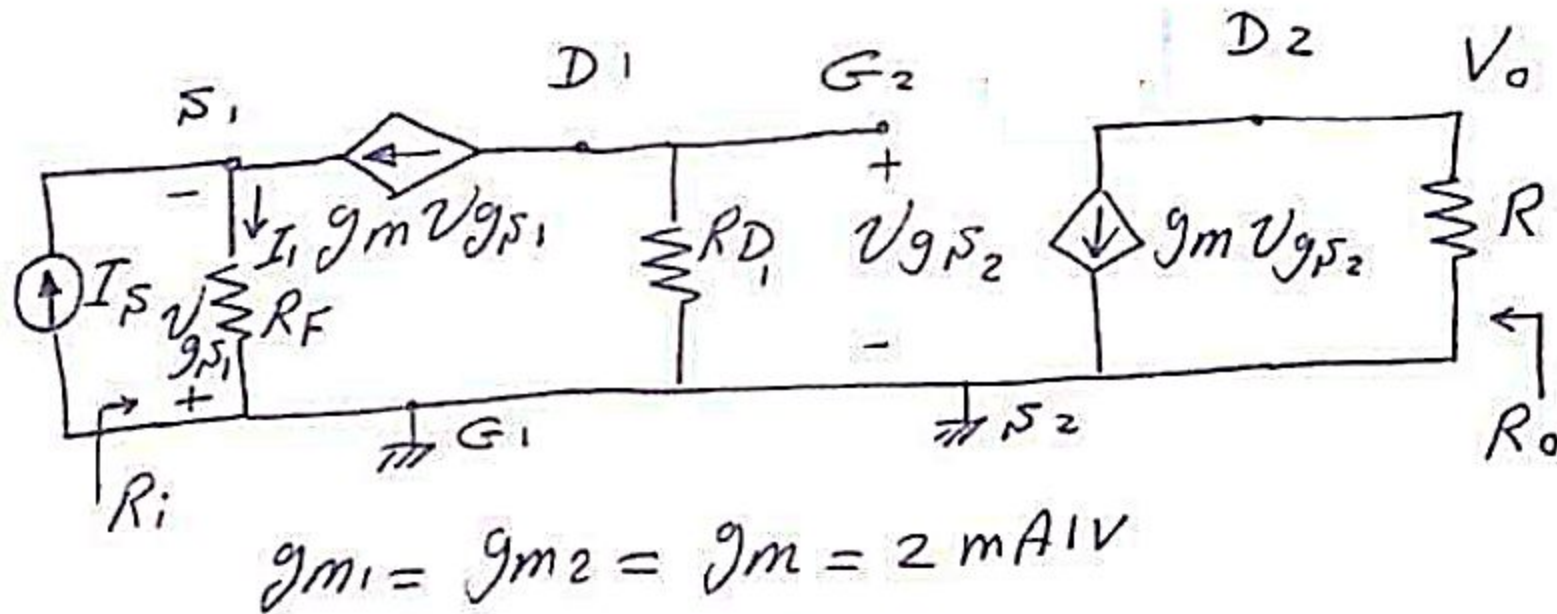
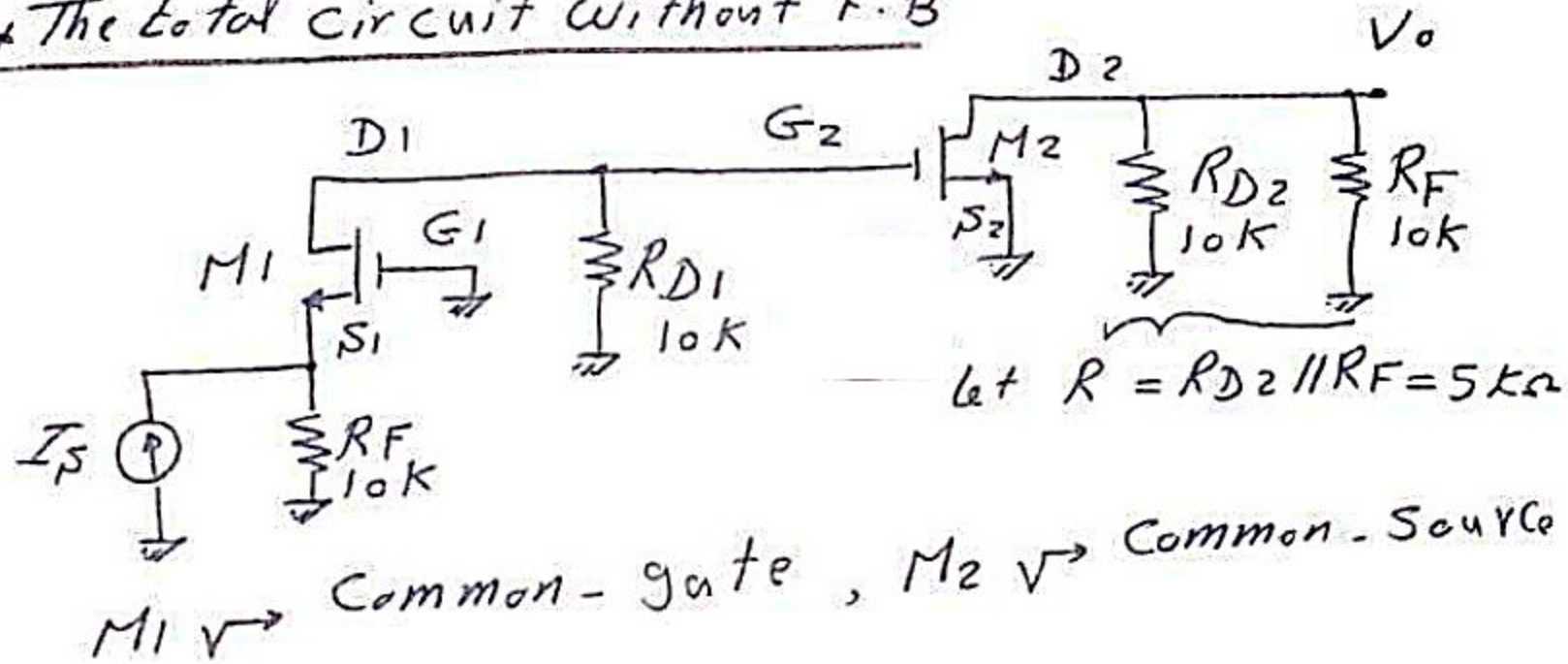
$$I_f = \frac{0 - V_o}{R_F} \Rightarrow V_o = -I_f R_F$$

$$\therefore \boxed{\beta = \frac{I_f}{V_o} = -\frac{1}{R_F} = -0.1} \text{ mA/V}$$

↳ Feedback Factor



\* The total circuit without F.B



\* open-Loop gain (A)

$$A = \frac{V_o}{I_s} = \frac{V_o}{v_{gs2}} \times \frac{v_{gs2}}{v_{gs1}} \times \frac{v_{gs1}}{I_s} \rightarrow \boxed{1}$$

$$* V_o = -g_m v_{gs2} R$$

$$\therefore \boxed{\frac{V_o}{v_{gs2}} = -g_m R = -2 \times 5 = -10} \quad (2)$$

$$* v_{gs2} = -g_m v_{gs1} R_{D1}$$

$$\therefore \boxed{\frac{v_{gs2}}{v_{gs1}} = -g_m R_{D1} = -2 \times 10 = -20} \quad (3)$$



\* K.C.L  $I_S + g_m V_{gs1} = I_1$

$$I_S + g_m V_{gs1} = - \frac{V_{gs1}}{R_F}$$

$$I_S = - V_{gs1} \left[ g_m + \frac{1}{R_F} \right] \quad (4)$$

$$\therefore \boxed{\frac{V_{gs1}}{I_S} = \frac{-1}{g_m + \frac{1}{R_F}} = \frac{-1}{2 + 0.1} = -\frac{10}{21}} = -0.4762$$

Sub. from (2), (3) and (4) into (1)

$$\therefore A = (-g_m R)(-g_m R_{D1}) \left( \frac{-1}{g_m + \frac{1}{R_F}} \right)$$

$$A = (-10)(-20) \left( -\frac{10}{21} \right)$$

$$\boxed{A = -95.2381} \text{ open-Loop gain}$$

(b) The feedback gain  $A_f$ .

$$A_f = \frac{A}{1 + A\beta} = \frac{-95.2381}{1 + (-95.2381)(-0.1)}$$

$$\boxed{A_f \approx -9.05}$$

(c) The feedback input and output resistances ( $R_{if}$  and  $R_{of}$ ).

$$\times R_i = \frac{V_{in}}{I_{in}} = -\frac{V_{gs}}{I_s} \rightarrow \text{from (4)}$$

$$\boxed{R_i = -\frac{V_{gs}}{I_s} = \frac{1}{g_m + \frac{1}{R_F}} = \frac{1}{g_m} \parallel R_F = \frac{10}{21} \text{ k}\Omega}$$

$$\times R_{if} = \frac{R_i}{1 + A\beta} = \frac{10/21}{10.52381}$$

$$\boxed{R_{if} = 0.04525 \text{ k}\Omega = 45.25 \Omega}$$

$$\times R_o = \left. \frac{V_x}{I_x} \right|_{I_s=0} \rightarrow A_s \quad I_s=0 \rightarrow V_{gs1}=0 \\ \therefore g_m V_{gs1}=0 \rightarrow V_{gs2}=0 \therefore g_m V_{gs2}=0$$

$$\boxed{R_o = R = 5 \text{ k}\Omega}$$

$$\times R_{of} = \frac{R_o}{1 + A\beta} = \frac{5}{10.52381}$$

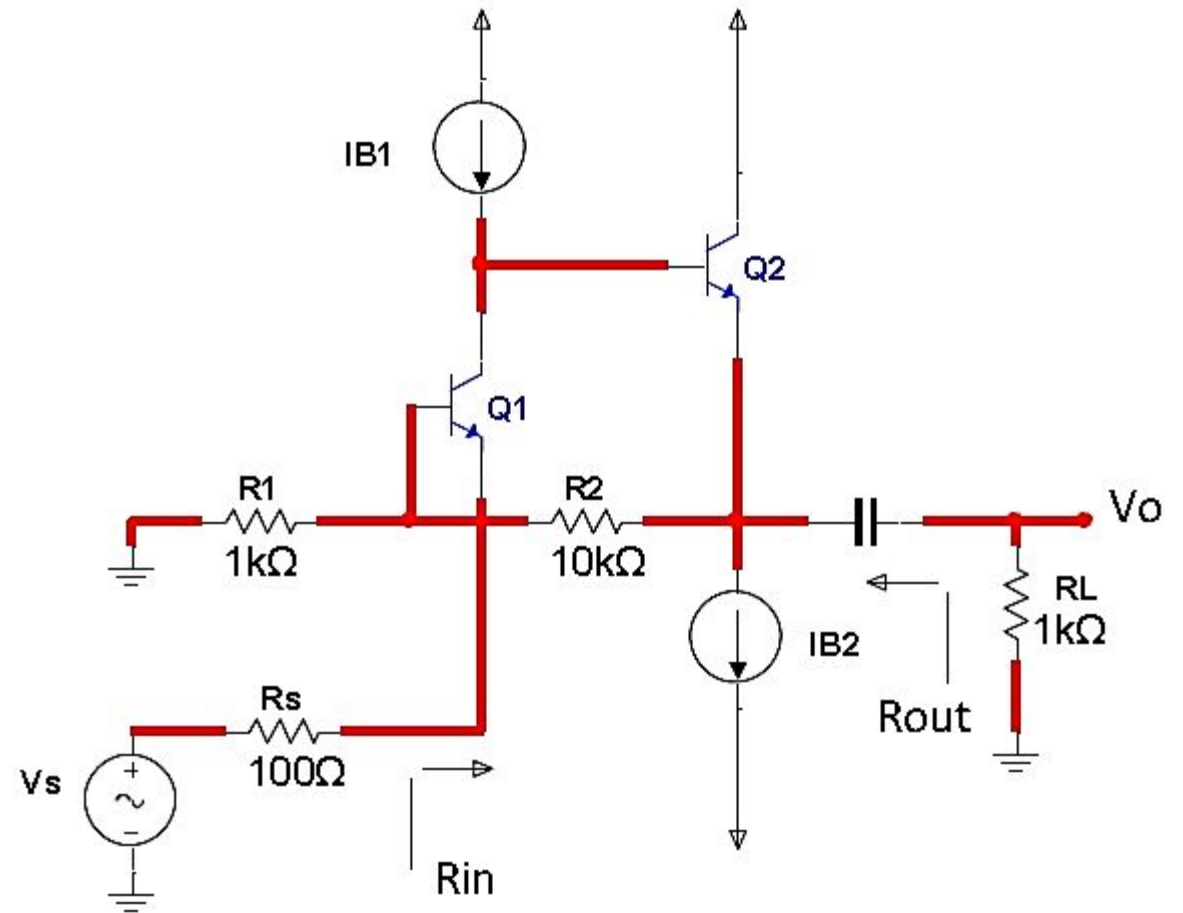
$$\boxed{R_{of} = 0.475 \text{ k}\Omega = 475 \Omega \#}$$

# Example (Series-Shunt Feedback)

Analyze the Series-Shunt feedback amplifier circuit shown in Figure .

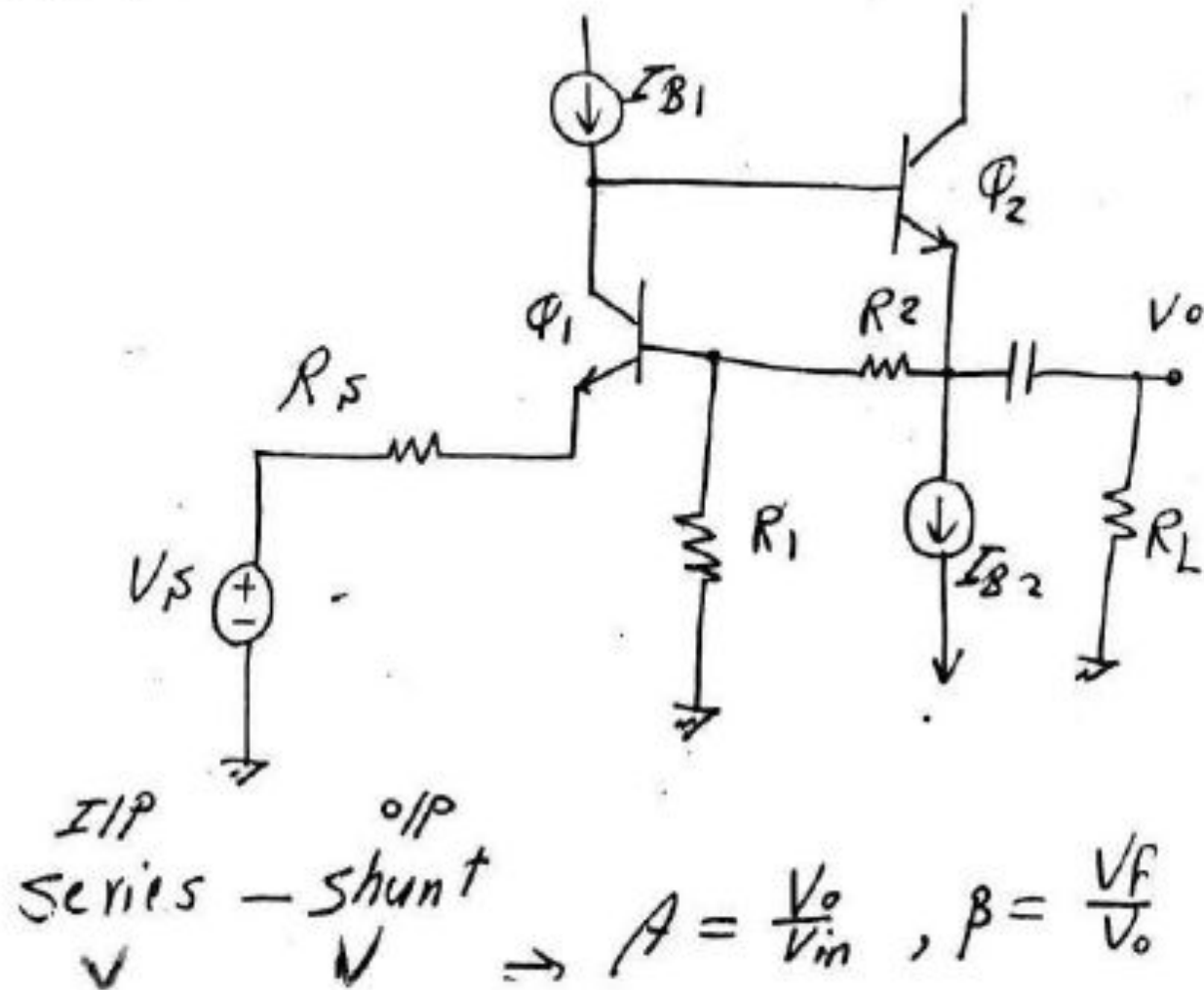
Assuming  $\beta_1 = \beta_2 = 100$ ,  $r_{e1} = 260 \Omega$ ,  $r_{e2} = 26 \Omega$  and  $r_o$  is neglected.

1. Calculate the open loop gain  $A$ , the feedback factor  $\beta$  and the feedback gain  $A_f$ .
2. Calculate  $R_{if}$ ,  $R_{in}$ ,  $R_{of}$  and  $R_{out}$ .



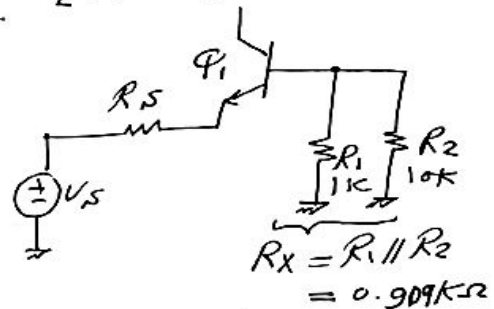
## Solution:

We can Redraw the circuit as follow

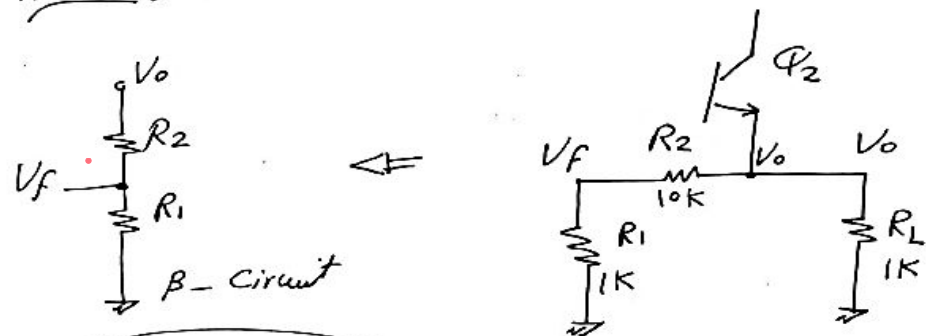




I/P Circuit without F.B [V<sub>o</sub> = 0]

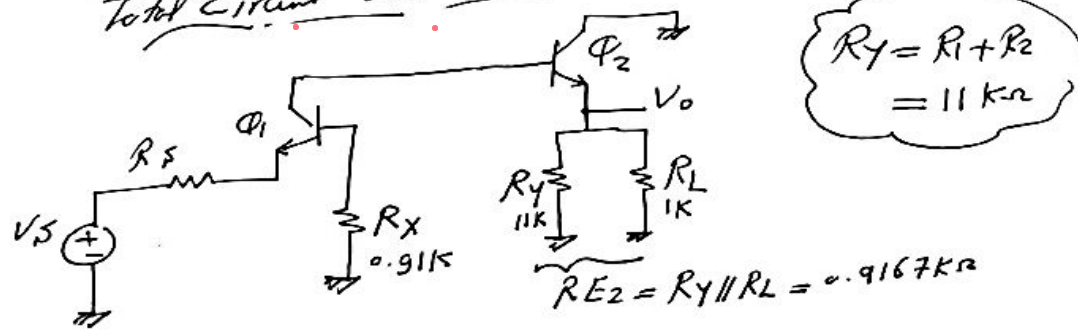


O/P Circuit without F.B [I/P open]



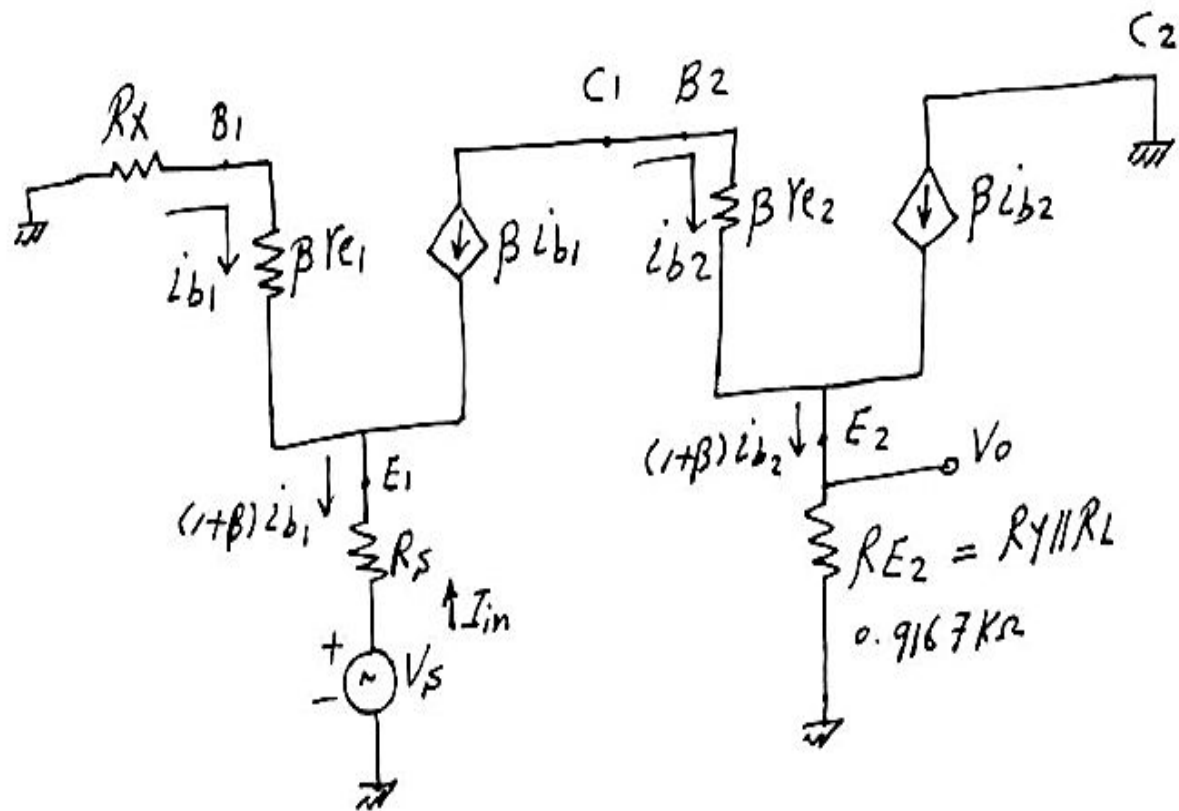
$$\beta = \frac{V_f}{V_o} = \frac{R_1}{R_1 + R_2} \Rightarrow \beta = \frac{1}{11} = 0.0909$$

Total Circuit without F.B



$$* r_{e1} \approx \frac{0.026}{I_{C1}} = \frac{0.026 \text{ V}}{0.1 \text{ mA}} = 0.26 \text{ k}\Omega = 260 \Omega$$

$$* r_{e2} \approx \frac{0.026}{I_{C2}} = \frac{0.026 \text{ V}}{1 \text{ mA}} = 0.026 \text{ k}\Omega = 26 \Omega$$



$$* \beta = \frac{V_f}{V_o} = \frac{1}{11} = 0.0909$$

$$* A = \frac{V_o}{V_s} = \frac{V_o}{i_{b2}} \times \frac{i_{b2}}{i_{b1}} \times \frac{i_{b1}}{V_s}$$

$$* V_o = (1 + \beta) i_{b2} \cdot R_{E2}$$

$$\therefore \boxed{\frac{V_o}{i_{b2}} = (1 + \beta) R_{E2}} = 101 \times 0.9167 = 92.583 \text{ K}$$

$$* i_{b2} = -\beta i_{b1}$$

$$\therefore \left\{ \frac{i_{b2}}{i_{b1}} = -\beta = -100 \right.$$

K.V.L at input Loop :-

$$0 = i_{b1}(R_X + \beta r_{e1}) + (1 + \beta)i_{b1}R_S + V_S$$

$$\therefore V_S = -i_{b1}[R_X + \beta r_{e1} + (1 + \beta)R_S]$$

$$\therefore \boxed{\frac{i_{b1}}{V_S} = \frac{-1}{R_X + \beta r_{e1} + (1 + \beta)R_S}} \quad \text{--- (I)}$$

$$\frac{i_{b1}}{V_S} = \frac{-1}{0.909 + 100 \times 0.26 + 101 \times 0.1} = -0.02702$$

$$\therefore A = \frac{V_o}{V_S} = 92.583 \times -100 \times -0.02702$$

$$A = \frac{V_o}{V_S} = 250.16, \quad \beta = 0.0909$$

$$* A_f = \frac{A}{1 + A\beta} = \frac{250.16}{1 + 250.16 \times 0.0909} = 10.5377$$

$$* R_i = \frac{V_S}{I_{in}} = \frac{V_S}{-(1 + \beta)i_{b1}} = -\frac{1}{1 + \beta} \left( \frac{V_S}{i_{b1}} \right)$$

$$\text{From (I)} \quad V_S = -i_{b1}[R_X + \beta r_{e1} + (1 + \beta)R_S]$$

$$\frac{V_S}{i_{b1}} = -[R_X + \beta r_{e1} + (1 + \beta)R_S]$$

$$\therefore \boxed{R_i = \frac{R_X + \beta r_{e1} + (1 + \beta)R_S}{1 + \beta}}$$

$$R_i = \frac{0.909 + 100 \times 0.26 + 101 \times 0.1}{101}$$

$$\boxed{R_i = 0.36643 \text{ K}\Omega} = 366.43 \Omega$$

$$* R_{if} = R_i(1 + A\beta) = 366.43 \Omega (1 + 250.16 \times 0.0909)$$

$$R_{if} = 8.699 \text{ K}\Omega \cong 8.7 \text{ K}\Omega$$

$$* R_{in} = R_{if} - R_S = 8.599 \text{ K}\Omega \quad \text{Series}$$

$$* R_o = \frac{V_X}{I_X} \big|_{V_S=0}, \text{ As } V_S=0 \rightarrow i_{b1}=0 \rightarrow i_{b2}=0$$

$$R_o = R_{E2} = R_Y \parallel R_L = 0.9167 \text{ K}\Omega$$

$$* R_{of} = \frac{R_o}{1 + A\beta} = \frac{0.9167}{1 + 250.16 \times 0.0909} = 0.0386 \text{ K}\Omega$$

$$R_{of} = 38.6 \Omega$$

$$* R_{out} = \frac{1}{\frac{1}{R_{of}} - \frac{1}{R_L}} = \frac{1}{\frac{1}{38.6} - \frac{1}{100}}$$

$$R_{out} = 62.866 \Omega$$