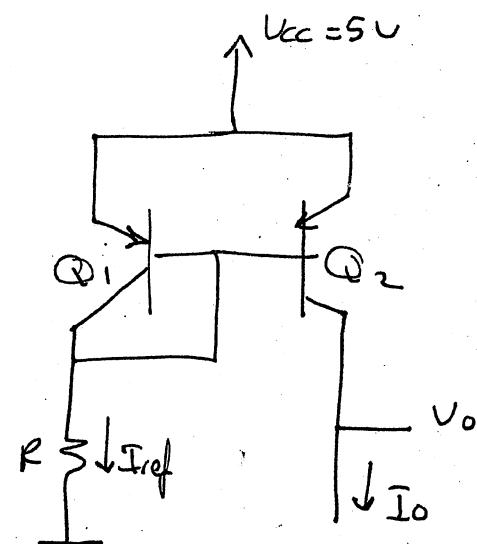


III

1 - The Current Source Shown, Transistors are matched having $I_S = 10^{-15} A$
 $B = 50$ and $|V_A| = 50 V$.

Design the circuit for $I_o = 1 mA$ at
 $V_o = 2 V$. what I_{ref} and R needed.
 what Change in I_o Corresponding to V_o
 Change from max +ve to -5V



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(2)

early voltage \rightarrow current mirror bias

Mirror CS $\sim V_{EB}$, \therefore

$$I_0 = \frac{I_{ref}}{1 + 2/\beta} \left(1 + \frac{V_0 - V_{EB}}{V_A} \right)$$

$$\begin{aligned} V_{EB_1} &= V_{EB_2} = V_T \ln \frac{\frac{I_C}{I_S}}{I_0} \\ &= V_T \ln \frac{I_0}{I_S} \end{aligned}$$

$$\therefore V_{EB_1} = 0.025 \ln \left(\frac{10^{-3}}{10^{-15}} \right) = 0.69 \text{ volt}$$

$$\therefore I_0 = \frac{I_{ref}}{1 + 2/\beta} \left(1 + \frac{V_0 - V_{EB}}{V_A} \right)$$

$$10^{-3} = \frac{I_{ref}}{1 + 2/50} \left(1 + \frac{2 - 0.69}{80} \right)$$

$$\boxed{I_{ref} = 1.013 \text{ mA}}, R = \frac{V_{CC} - V_{EB}}{I_{ref}}$$

$$R = \frac{5 - 0.69}{1.013} = 4.25 \text{ k}\Omega$$

$$\boxed{R = 4.25 \text{ k}\Omega}$$

[3]

for $V_o = -5 \text{ V}$

$$I_o = \frac{I_{ref}}{1 + 2/B} \left(1 + \frac{V_o - V_{EB}}{V_A} \right)$$
$$= \frac{1.013 \times 10^{-3}}{1 + 2/50} \left(1 + \frac{-5 - 0.69}{50} \right)$$

$$I_o = 0.86 \text{ mA}$$

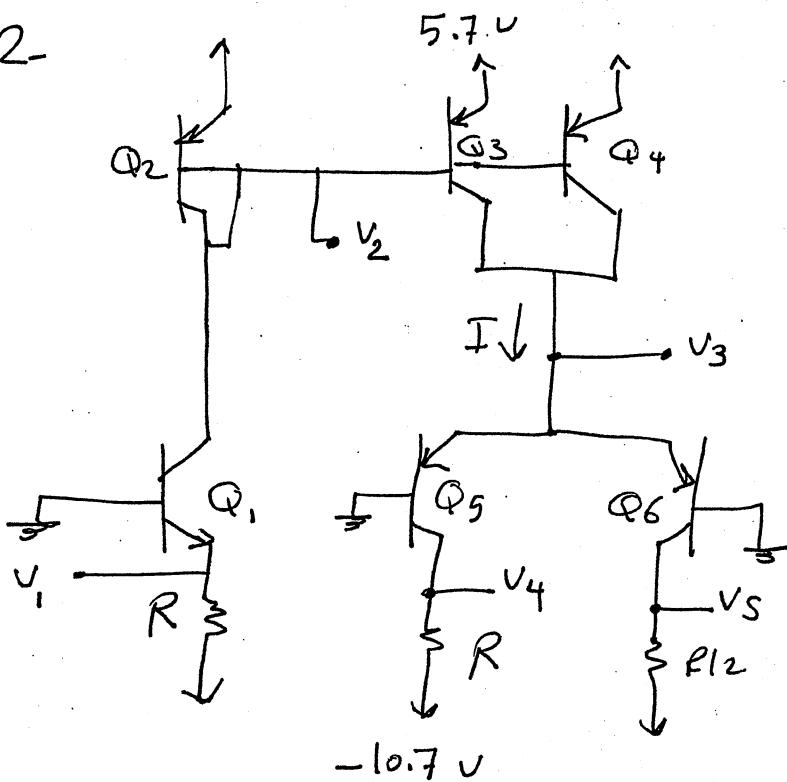
$\therefore I_o$ changes from 1 mA to 0.86 mA



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4

2



For the circuit shown $|V_{BE}| = 0.7$

$\beta = \infty$, find $I, V_1, V_2, V_3, V_4, V_5$

for $R = 10k\Omega$, $R = 100k\Omega$



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[5]

For $R = 10k\Omega$

$$V_1 = -0.7 \text{ V}$$

$$I_{C_1} = \frac{-0.7 - (-10.7)}{10k\Omega} = 1 \text{ mA}$$

$$V_2 = 5.7 - 0.7 = 5 \text{ V}$$

$$I = I_{C_3} + I_{C_4}, \quad I_{C_3} = I_{C_4} = I_C,$$

$$I = 2 \times 1 = 2 \text{ mA}$$

$$V_3 = V_{EB_S} = V_{EB_6} = 0.7 \text{ V}$$

$$V_4 = -10.7 + 1 \times 10 = -0.7 \text{ V}$$

$$V_5 = -10.7 + 1 \times \frac{10}{2} = -5.7 \text{ V}$$



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[6]

for $R = 100k\Omega$

$$V_1 = -0.7 \text{ V}$$

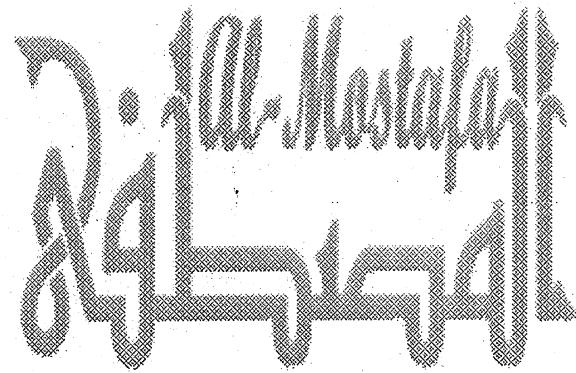
$$I_C = \frac{-0.7 + 10.7}{100k} = 0.1 \text{ mA}$$

$$I = 2 I_C = 0.2 \text{ mA}$$

$$V_3 = 0.7 \text{ V} , V_2 = 5.7 - 0.7 = 5 \text{ V}$$

$$V_4 = -10.7 + \frac{1 \times 100}{10} = -0.7 \text{ V}$$

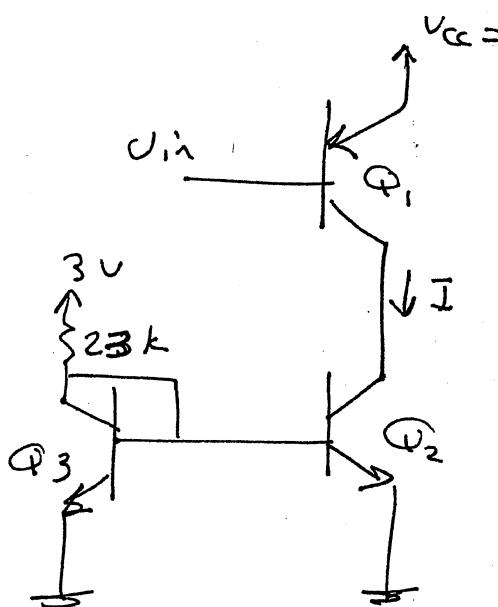
$$V_5 = -10.7 + 0.1 \times \frac{100}{2} = -5.7 \text{ V}$$



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(7)

3 -



a] Neglect I_B of Q_1, Q_2
and let $V_{BE} = 0.7\text{ V}$

Q_2 has 5-area
times area of Q_3 .

- find I

b] If Q_1, Q_2 have $V_A = 50\text{ V}$, find r_o ,
and r_{o2} and total r_o at Collector of Q_1

c) find $\pi_i \rightarrow g_m$, assuming $B = 50$.



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(8)

a) \therefore Neglect I_B

$$\therefore I_{ref} \approx I_{E_3} = I_{C_3}$$

$$I_{ref} = \frac{3 - 0.7}{23} = 0.1 \text{ mA}$$

$$\therefore \boxed{I_{C_3} = 0.1 \text{ mA}}$$

$$\frac{I_{C_2}}{I_{C_3}} = \frac{\text{Area of } Q_2}{\text{Area of } Q_3} = 5$$

$$\therefore I_{C_2} = I = 5 I_{C_3} = 0.5 \text{ mA}$$

$$\therefore \boxed{I_{C_2} = 0.5 \text{ mA}}$$



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[9]

b) $|V_A| = 50$

$$r_{o_1} = \frac{|V_A|}{I_{C_1}} = \frac{|V_A|}{I} = \frac{50}{0.5 \text{ mA}}$$

$$\boxed{r_{o_1} = 100 \text{ k}\Omega}$$

$$r_{o_2} = \frac{|V_A|}{I_{C_2}} = \frac{|V_A|}{I} = \frac{50}{0.5 \text{ mA}}$$

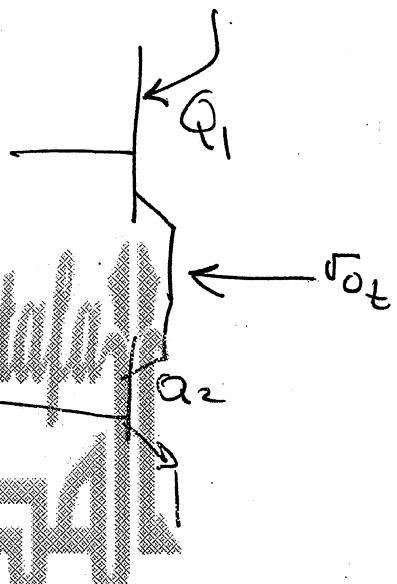
$$\therefore \boxed{r_{o_2} = 100 \text{ k}\Omega}$$

~~at~~ at Collector of Q_1

$$r_{ot} = r_{o_1} \parallel r_{o_2}$$

$$\therefore r_{ototal} = \frac{100 \text{ k}\Omega}{2}$$

$$\boxed{r_{ototal} = 50 \text{ k}\Omega}$$



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(10)

C] $\beta = 50$

$$g_{m1} = \frac{I_{C1}}{V_T} = \frac{0.5}{0.025}$$

$$g_{m1} = 20 \text{ mA/V}$$

$$r_{T1} = \frac{\beta}{g_m} = \frac{50}{20} = 2.5 \text{ k}\Omega$$

$$r_{T1} = 2.5 \text{ k}\Omega \equiv R_{in}$$



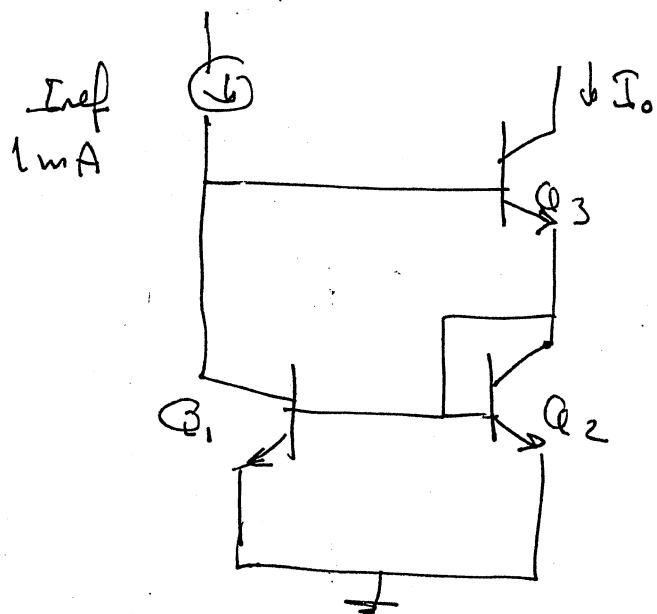
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III

4- For Wilson C.S shown $I_{ref} = 1 \text{ mA}$

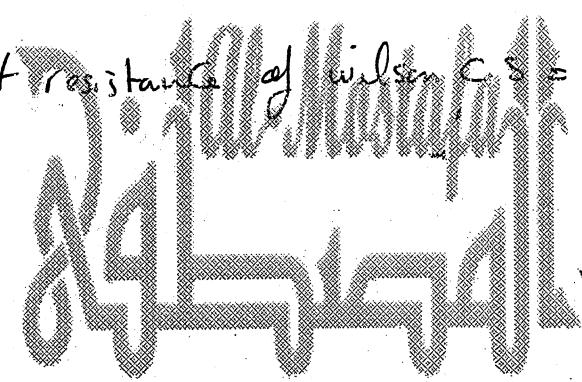
what change in I_o due to change
of +10V at collector of Q_3 . Let

$$\beta = 100, V_A = 100 \text{ V}$$



Hint:

output resistance of wilson C.S is $\frac{\beta r_o}{2}$



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[12]

for wilson Current source

$$I_o \approx \frac{1}{1 + \frac{2}{\beta^2 + 2\beta}} I_{ref}$$

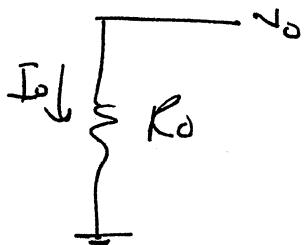
for $\beta = 100$

$$\therefore I_o = 0.999 \text{ mA}$$

for wilson current source $R_o = \frac{\beta r_o}{2}$

$$\therefore \Delta I_o = \frac{\Delta V_o}{R_o} \rightarrow \text{voltage}$$

$$\Delta V_o = 10 \text{ volt}$$



$$R_o = \frac{\beta r_o}{2} = \frac{\beta}{2} \left(\frac{V_A}{I_C} \right) = \frac{100}{2} \times \frac{100}{0.999} = 5.005 \mu\Omega$$

$$\therefore R_o = 5.005 \mu\Omega$$

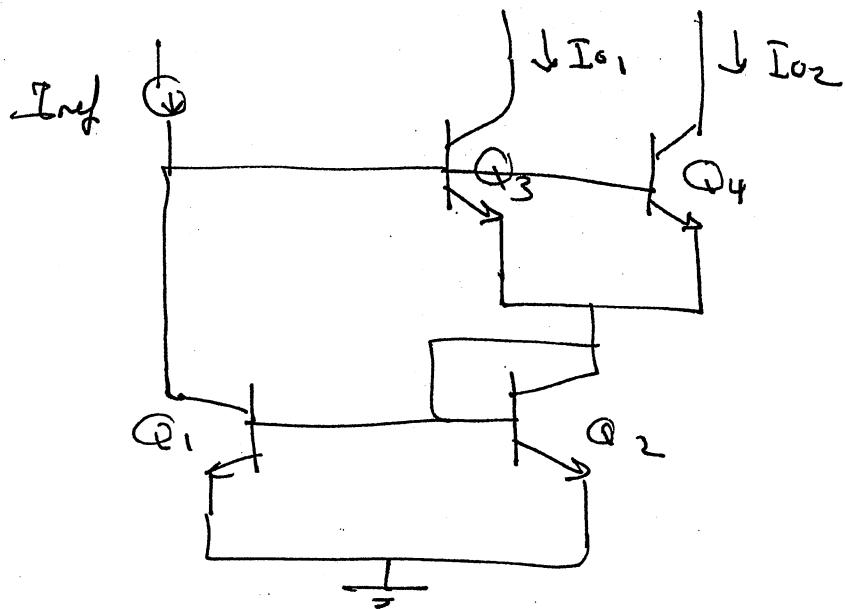
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$$\therefore \Delta I_o = \frac{10}{5.005 \mu\Omega} = 1.998 \times 10^{-6}$$

$$\approx 2 \mu\text{A}$$

[13]

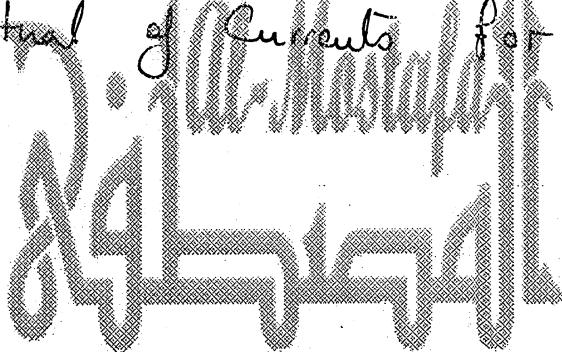
5- For circuit shown



Q_3, Q_4 Matched Find I_{o1}, I_{o2}

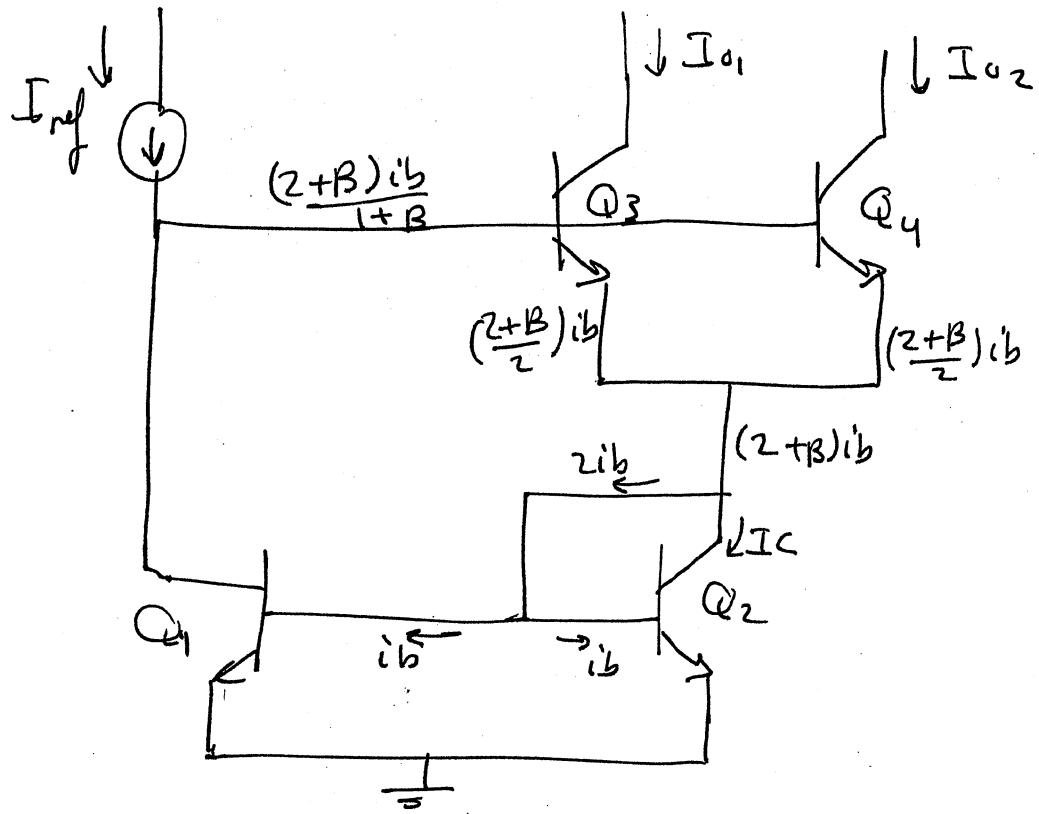
in terms of I_{ref} assume all Tr are matched

- use above idea to design a circuit to generate 1mA, 2mA and 4mA using $I_{ref} = \cancel{7}\text{mA}$
- What actual currents for $B = 50$.



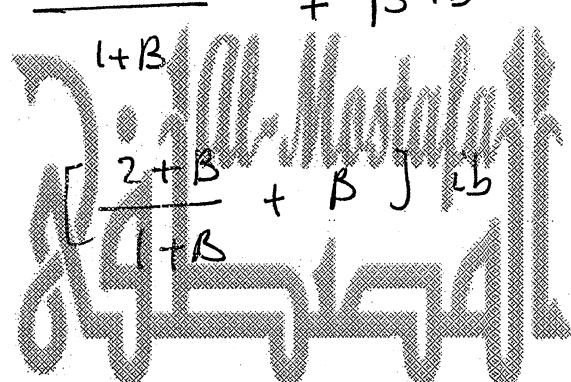
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$$I_{o_1} = \beta \left[\frac{(2+B)iB}{2(1+B)} \right] = I_{o_2} \rightarrow ①$$

$$I_{ref} = \frac{(2+B)iB}{1+B} + \beta iB$$

$$I_{ref} = \left[\frac{2+B}{1+B} + \beta \right] iB \rightarrow ②$$


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JS

From ①, ②

$$\therefore I_{o_1} = \frac{B(2+B)}{2(1+B)} \cdot \frac{1}{\frac{2+B}{1+B} + B} I_{ref}$$

$$= \frac{B(2+B)}{2[2+B + B(1+B)]} I_{ref}$$

$$I_{o_1} = \frac{B(2+B)}{2[B^2 + 2B + 2]} I_{ref}$$

$$= \frac{1}{2} \cdot \frac{B^2 + 2B}{B^2 + 2B + 2} I_{ref}$$

$$B^2 \gg 2B$$

$$= \frac{1}{2} \cdot \frac{B^2}{B^2 + 2B + 2} I_{ref}$$

$$= \frac{1}{2} \cdot \frac{1}{1 + 2/B + 2/B^2} I_{ref}$$

~~ملاحظة~~

$$I_{o_1} \approx \frac{0.10011000000000001}{2} \left(\frac{1}{1 + 2/B^2} \right) I_{ref}$$

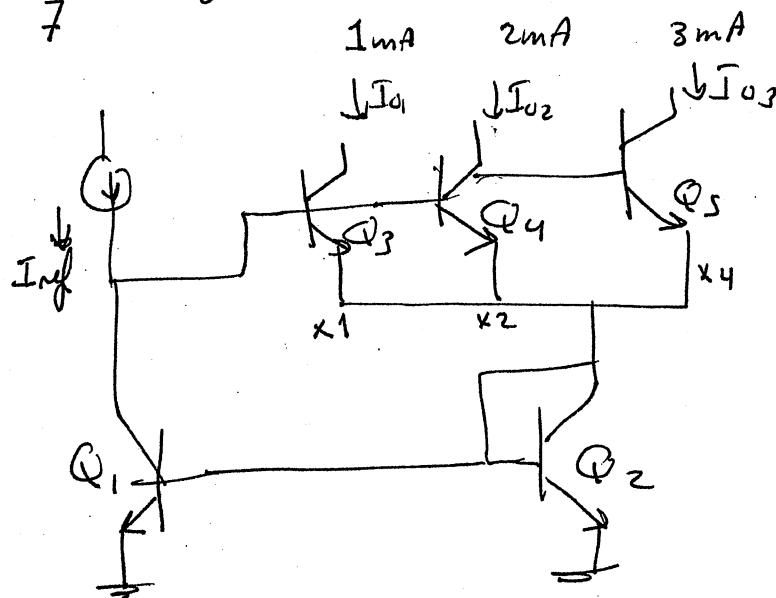
$$I_{o_1} = I_{o_2} = \text{نسبة الماء}$$

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b) using 3 transistors in parallel having relative area ratios of 1, 2, 4 as shown below

$$I_{O_1} = \frac{1}{7} I_{ref}$$

$$\therefore \text{Area of } Q_3 = \frac{1}{7} \text{ Area of } Q_1$$



$$\therefore I_{O_2} = \frac{2}{7} I_{O_1} \quad \text{Area of } O_4 = 2 [\text{Area of } O_3]$$

$$I_{O_3} = \frac{4}{7} [\text{Area of } Q_3]$$

$$\text{Area of } Q_5 = 2 \left[\text{Area of } Q_4 \right] = 4 \left[\text{Area of } Q_3 \right]$$

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for $\beta = 50$

Actual value of I_{o1} , I_{o2} , I_{o3}

$$I_{o1} = \frac{1}{7} \left(\frac{I_{ref}}{1 + \frac{2}{\beta^2}} \right)$$

$$= \frac{1}{7} \left(\frac{1}{1 + \frac{2}{50^2}} \right) = \frac{1}{7} \left(\frac{1}{1 + \frac{2}{2500}} \right)$$

$I_{o1} = 0.998 \text{ mA}$

(1mA ideally)

$$I_{o2} = \frac{2}{7} I_{ref}$$

$I_{o2} = 1.996 \text{ mA}$

(2mA ideally)

$$I_{o3} = \frac{4}{7} I_{ref}$$
(4mA ideally)

$I_{o3} = 3.992 \text{ mA}$

Note:

$$I_o = \frac{1}{1 + \frac{2}{\beta^2} + 2\beta}$$

~~101005704545 is not a Wilson C.S~~

مقدار إسقاط التيار الموصول إلى العاكس بالنسبة لـ β

$$I_o = \frac{1}{1 + \frac{2}{\beta^2}}$$

C

~~Rev~~

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Sheet # 1

Electronics (3)

Electronics & comm. dept

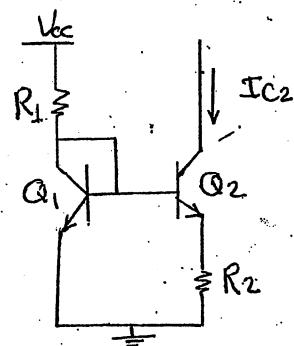
electronics (3)

Sheet#1

Current Source , Active loads , Output stages:

1-For the shown Widler current source :

- Derive an expression for the output current .
- compare this circuit with the mirror current source.
- find the output impedance of the shown widler current source.



Neglecting base currents we can write

$$I_{E_2} \approx I_{C_2} \approx I_o$$

$$I_{ref} \approx I_{C_1} \approx I_{E_1}$$

From KV

$$V_{BE_1} = V_{BE_2} + I_{C_2} R_E$$

(1)

$$\therefore I_C = I_S (e^{\frac{V_{BE_1}}{V_T}} - 1)$$

where $I_S \rightarrow$ Reverse saturation current

(2)

$$I_{C_1} \approx I_{ref} = I_{S_1} \left(e^{\frac{V_{BE_1}}{V_T}} \right) \rightarrow ①$$

$$I_{C_2} \approx I_0 = I_{S_2} \left(e^{\frac{V_{BE_2}}{V_T}} \right) \rightarrow ②$$

for identical transistors $\therefore I_{S_1} = I_{S_2}$

From ①

$$V_{BE_1} = V_T \ln \left(\frac{I_{ref}}{I_{S_1}} \right)$$

From ②

$$V_{BE_2} = V_T \ln \left(\frac{I_0}{I_{S_2}} \right)$$

$$V_{BE_1} - V_{BE_2} = V_T \ln \left(\frac{I_{ref}}{I_0} \right)$$

from Eq ①"

$$V_{BE_1} - V_{BE_2} = I_{S_1} R_B$$

$$0.10052014 \ln \left(\frac{I_{ref}}{I_0} \right)$$

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[3]

Q6,

$$I_O R_E = V_T \ln \left(\frac{I_{ref}}{I_O} \right)$$

Note

use Try and Error To Solve this
Equation.

- Compare This Circuit with Mirror CS

Widlar differs from the basic Current Mirror

Circuit in The Resistor (R_E) in the

Emitter of Q_2 .

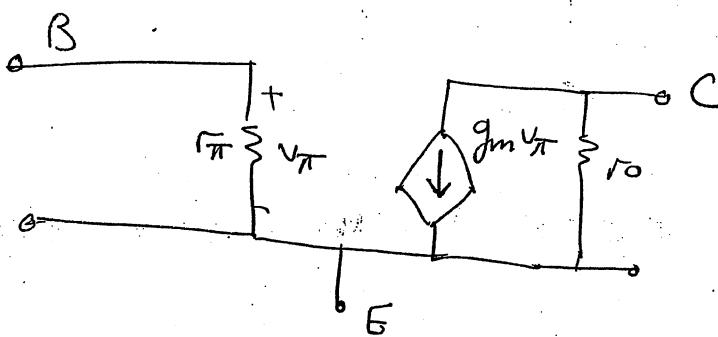
- And Widlar Current source has an output resistance higher than Mirror.
- Widlar Circuit avoids the generation of a small Constant Current using relatively Small Resistors. (Saving in Chip Area).

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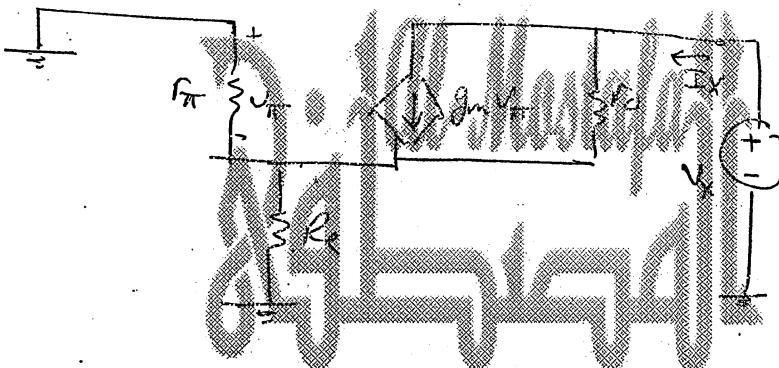
- To find The output impedance of Widlar Current source.

use The π -Model of \underline{Q}_2

Replace the BJT with its low-frequency hybrid π Model.



To find r_o , apply a Test voltage v_x to the Collector



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(5)

Note R_E parallel with r_{π}

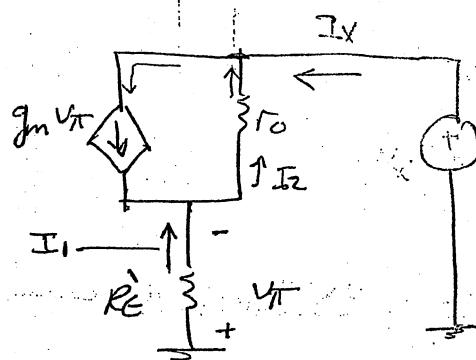
$$R_E' = R_E \parallel r_{\pi} = \frac{R_E * r_{\pi}}{R_E + r_{\pi}}$$

From The Model

$$I_1 = \frac{V_T}{R_E'}$$

$$I_1 = -I_X$$

$$\therefore I_X = -\frac{V_T}{R_E'}$$

Note

$$I_X = g_m V_{\pi} + I_2$$

$$\text{So, } I_2 = g_m V_{\pi} - I_X$$

$$I_2 = g_m V_{\pi} + \frac{V_T}{R_E'} = V_T \left(g_m + \frac{1}{R_E'} \right)$$

$$R_O = \frac{V_X}{I_X} = -\left[r_o \left(1 + \left(g_m + \frac{1}{R_E'} \right) \right) + V_T \right] - V_T / R_E'$$

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(G)

$$R_o = \frac{r_o \left(g_m + \frac{1}{R_E'} \right) + 1}{1/R_E'}$$

$$R_o = \frac{r_o (g_m R_E' + 1) + R_E' }{1}$$

- The output Resistance = $r_o (g_m R_E' + 1) + R_E'$

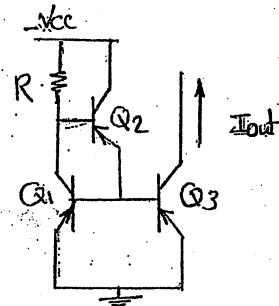


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[7]

2-Determine the value of the output current
if β of the PNP transistor is in the range of 2-10.

Compare this circuit with the simple (mirror) current source.



Note All Transistor PnP

for matching between (Q_1, Q_3)

$$\therefore I_{b1} = I_{b3}$$

And The two operate in Active Mode

$$\therefore V_{BE1} = V_{BE3} = 0.7 \text{ V}$$

From (KCL)

$$I_{ref} = \frac{-1.4 + V_{CC}}{R}$$

$$I_{E2} = I_{b1} + I_{b3}$$

$$= 2 I_b$$

$$I_{ref} = I_{b1} + I_C$$

$$= \frac{I_C}{(1+\beta)} + \beta I_b$$

$$= \frac{0.1005704545}{(1+\beta)} + \beta \frac{I_b}{(1+\beta)} \left(\beta + \frac{2}{1+\beta} \right)$$

(8)

$$I_{ref} = I_b \left(\beta + \frac{2}{1+\beta} \right) \rightarrow ①$$

$$I_o \approx I_{CQ}$$

$$= \beta I_b$$

$$= \beta \frac{I_{ref}}{\left(\beta + \frac{2}{1+\beta} \right)}$$

$$I_o = \frac{I_{ref}}{\left(1 + \frac{2}{(1+\beta)\beta} \right)}$$

#

for β in range 2-10 (small)

The greater value (β^2)

$$\text{So } I_o \approx I_{ref}$$

* This Circuit giving I_o approximately equal I_{ref} for small values of β

which that not satisfied in Mirror Current source.

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Current Source Examples

Example:

For The Current Source Shown
in Fig(1).

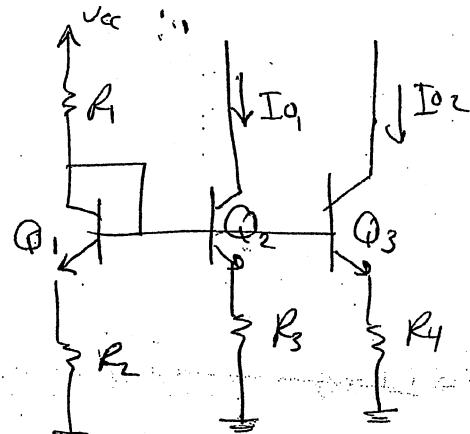
- a) Derive an approximate expression
for I_{Q1} , I_{Q2} as a function of V_{CC}

[assume identical transistors]

- b) Find I_{Q1} , I_{Q2}

If $V_{CC} = 10V$; $R_1 = 1k\Omega$

$$R_2 = R_3 = 50\Omega \quad R_4 = 100\Omega$$



Fig(1)

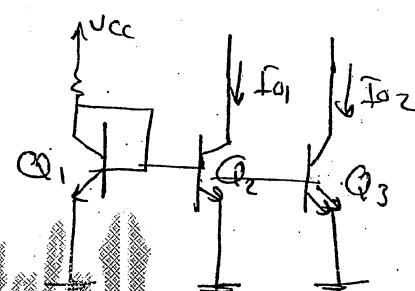
- c) If The Circuit of Fig(1)

IS Replaced by the Current Source

Shown in Fig(2), Find The

new values of I_{Q1} , I_{Q2} .

[assume identical transistors]



Fig(2)

- d) Which of The Two Circuits
do you prefer from the point of view

i) I-C fabrication

ii) Current Source performance.

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(2)

Solution

④ $R_2 = R_3$ for (Q_1, Q_2)

So Q_1, Q_2 matched (Mirror CS)

$I_{O_1} \approx I_{ref}$

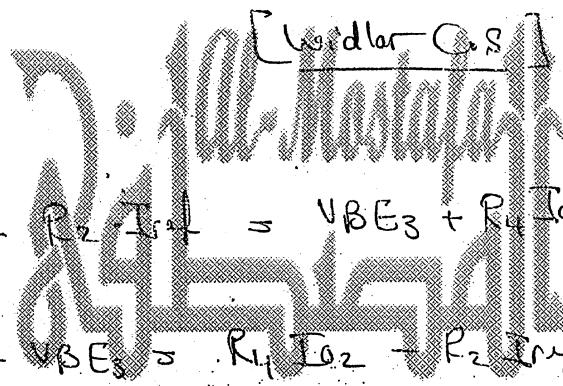
$$I_{ref} = \frac{V_{cc} - V_{BE_1}}{R_1 + R_2} = I_{O_1}$$

$$I_{ref} = \frac{10 - 0.7}{1k + 50\Omega} = 9.25 \text{ mA}$$

⑤ for Q_1, Q_3

$R_2 \neq R_4$ ∵ not matched
(Not Mirror CS)

from tvt



$$V_{BE_1} + R_2 I_{O_2} = V_{BE_3} + R_4 I_{O_2}$$

$$V_{BE_1} - V_{BE_3} = R_4 I_{O_2} - R_2 I_{ref}$$

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(3)

$$\therefore V_{BE_1} - V_{BE_2} = V_T \ln \frac{I_{ref}}{I_{O2}}$$

So

$$V_T \ln \frac{I_{ref}}{I_{O2}} = R_4 I_{O2} - R_2 I_{ref}$$

$$I_{ref} = 9 \text{ mA} \quad R_2 = 50 \Omega$$

$$V_T \approx 25 \text{ mV} \quad R_4 = 100 \Omega$$

So, we use try and error to find I_{O2}

using calculator in this equation

$$\text{So, } I_{O2} = 18 \text{ mA}$$

c) for Circuit in fig(2)

Q_1, Q_2 matched

$$\therefore I_{O1} = I_{ref} = \frac{V_{BE}}{R_2} = \frac{25}{50} = 0.5 \text{ mA}$$

Q_1, Q_3

$$I_{O2} = 2 I_{ref} = 2(0.5) = 1.0 \text{ mA}$$

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multi-Emitter
(P3)

d) For I.C fabrication

(4)

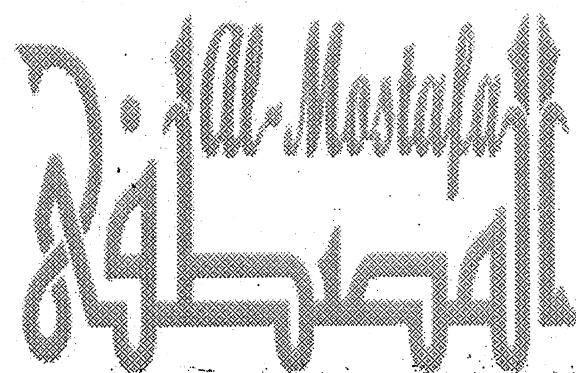
Circuit in fig(2) Contain less Resistors

So, it prefer for IC fabrication
 (less Area Needed)

For performance in Current Source

→ Circuit in fig(1) Widlar Current Source

for Q_3 which derive Small Current.



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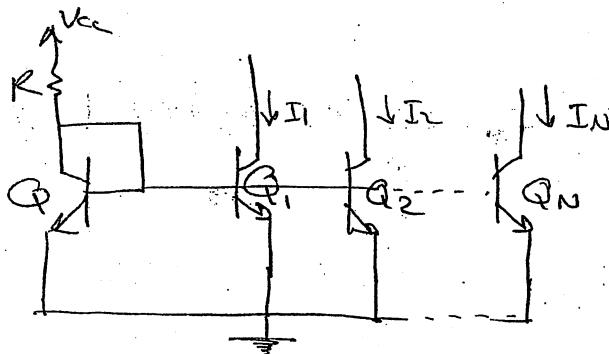
Example:

For shown figure

a) Prove that $I_1 = I_2 = \dots = I_N = \frac{I_{ref}}{1 + (N+1)/\beta}$

Assuming that all transistors are matched and have finite β

- b) For $\beta = 100$, find the maximum number of outputs for an error not exceeding 10%.



Sol:

a) for matched transistors

$$\therefore V_{BE1} = V_{BE2} = V_{BE3} = \dots = V_{BEU} = V_{BE}$$

for (active) $V_{BE} = 0.7 \text{ Volts}$

This is Minor C.S

$$Q100570454S - 01100338494 \\ \therefore I_1 = I_2 = \dots = I_N = I_{ref}$$

3

$$\frac{1}{1 + \frac{(N+1)}{B}} \geq 0.9$$

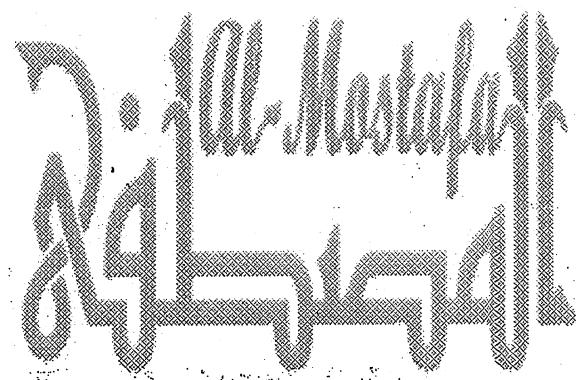
$$\frac{1 + \frac{(N+1)}{B}}{0.9} \quad \text{critical yield}$$

$$\frac{1}{0.9} \geq 1 + \frac{(N+1)}{B} \quad \downarrow 100$$

$$2 < 10.11$$

$$\therefore N = 10 \\ \max$$

#



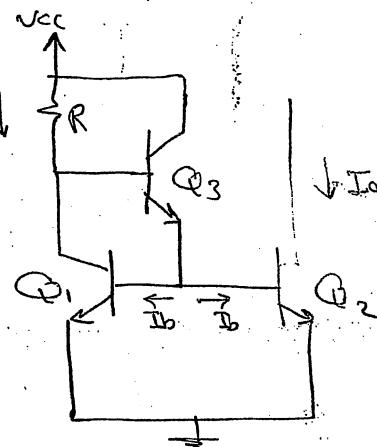
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Example:

For The shown Circui- find The smallest value of β so that $I_o \geq 0.99 I_{ref}$

Assume identical transistors.

This is improved
Mirror Current Source.



$$I_o = \frac{1}{1 + \frac{2}{\beta^2 + \beta}} I_{ref}$$

$$\frac{1}{1 + \frac{2}{\beta^2 + \beta}} \geq 0.99$$

$$1 + \frac{2}{\beta^2 + \beta} \leq \frac{1}{0.99}$$

$$\beta^2 + \beta + 2 \geq \frac{1}{0.99} (\beta + 1)$$

$$\beta^2 + \beta + 2 \leq 1.01\beta^2 + 1.01\beta$$

$$(0.01\beta^2 + 0.01\beta - 2) \geq 0$$

$$\beta = 13.6$$

$$\therefore \beta \geq 13.6$$

So the smallest value of $\boxed{\beta = 13.6}$

If you use approximation

$$\beta^2 \gg \beta$$

$$I_0 \approx \frac{1}{1 + \frac{2}{\beta^2}} I_{ref}$$

$$1 + \frac{2}{\beta^2} \leq \frac{1}{0.99}$$

$$\frac{2}{\beta^2} \leq 0.01$$

$$\boxed{\beta_{min} = 13.6}$$

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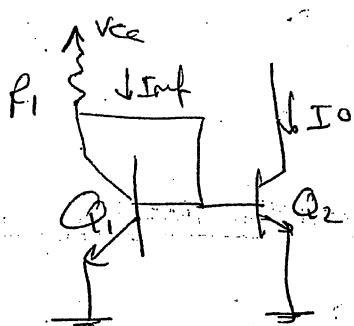
Example:

The two circuits for generating a constant current

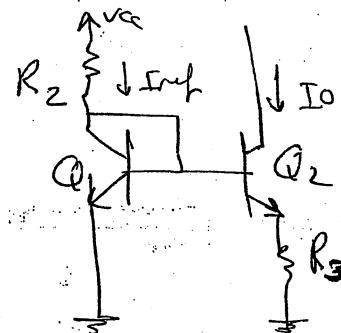
$I_o = 10\text{mA}$. operate from a 10 volt supply.

Determine the required resistors, Assuming

$V_{BE} = 0.7\text{ V}$ at a Current of 1mA



(a)



(b)

Solution

for circuit in fig(a)

we choose the value of $I_{inf} = 10\text{mA}$

at this current, the voltage drop across Q_1 ,
will be.

$V_{BE} = 0.7\text{ V}$ at 1mA

$V_{BE} = ??$ at 10mA

we know

$$\therefore V_{BE} = V_T \ln \left(\frac{I_c}{I_S} \right)$$

$$\therefore V_{BE} - V_{BE_2} = V_T \ln \left(\frac{I_1}{I_2} \right)$$

$$0.7 - V_{BE_2} = V_T \ln \left(\frac{1 \text{ mA}}{10 \mu\text{A}} \right)$$

0.025 ↙

$$\boxed{V_{BE_2} = 0.584 \text{ volt}}$$

So,

$$I_{ref} = \frac{V_{cc} - V_{BE}}{R_1} = 10 \mu\text{A}$$

10 volt $\rightarrow 0.584$

$$\therefore R_1 = 942 \text{ k}\Omega$$

which is large
(for IC fabrication)

for the circuit in Fig (b)

$$I_o = 10 \mu\text{A}$$

For the wider circuit, we must first decide

on the suitable value of I_{ref} (0.033819A)

$I_{ref} > I_o$
and $I_{ref} \approx I_o$
 $I_{ref} = 1 \text{ mA}$

If we select

$I_{ref} = 1\text{mA}$ then $V_{BE1} = 0.7$

$$\therefore R_2 = \frac{V_{CC} - 0.7}{I_{ref}}$$

$$\therefore \frac{10 - 0.7}{1\text{mA}} = 9.3\text{k}\Omega$$

The value of R_3 can be determined

from this Equation

$$I_0 R_3 = V_T \ln \left(\frac{I_{ref}}{I_0} \right)$$

$$I_0 = 10\mu\text{A} \quad I_{ref} = 1\text{mA}$$

$$V_T = 25\text{mV}$$

$$R_3 = \frac{0.025 \times \ln \left(\frac{1\text{mA}}{10\mu\text{A}} \right)}{10\mu\text{A}}$$

$$R_3 = 115\text{k}\Omega$$

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