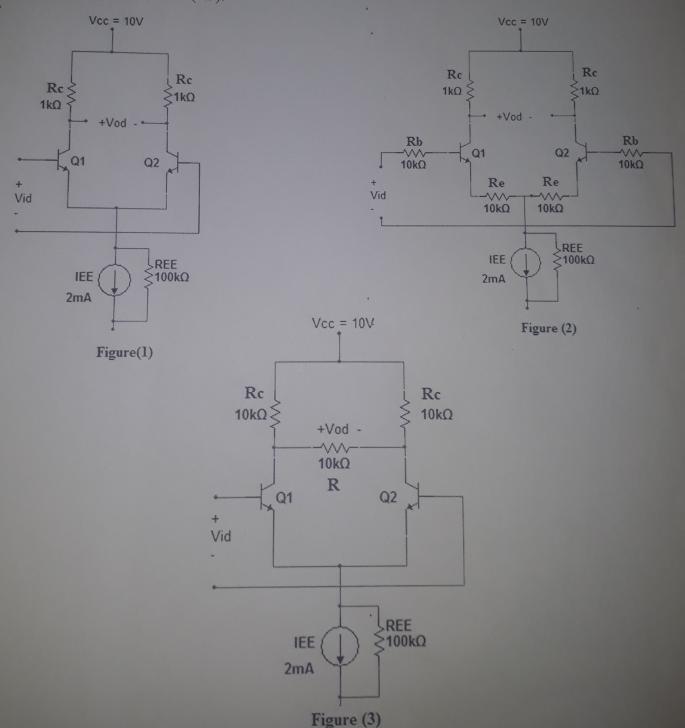
Problem (1)

The differential amplifier shown in Figures (1,2,3) are use two matched BJT's Q_1 and Q_2 with $\beta = 100$ and $V_A = \infty$.

Calculate:

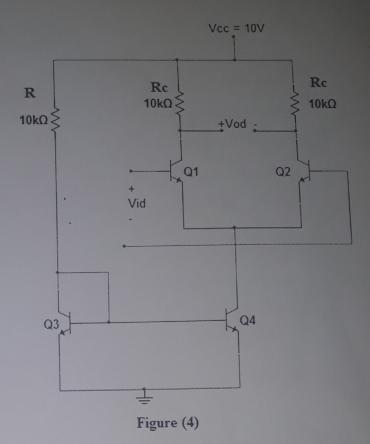
- 1. The Value of collector current for Q_1 and Q_2 .
- 2. The differential mode gain A_{dm} .
- 3. The common mode gain A_{cm}.
- 4. The CMRR in decibel (dB).



Problem (2)

The differential amplifier shown in Figure (4) uses the current mirror current source Q3 and Q4 with $\beta = 200$ and $V_{A3} = V_{A4} = 120V$. If $V_{A1} = V_{A2} = \infty$, Calculate:

- 1. The Value of collector current for Q_1 and Q_2 .
- 2. The differential mode gain A_{dm} .
- 3. The common mode gain A_{cm}.
- 4. The CMRR in decibel (dB).



Problem (3)

For the differential amplifier shown in Figure (5), calculate the voltage gain, input and output resistances. $(\beta=100, V_{A1}=V_{A2}=\infty)$.

Problem (4)

The MOS-differential amplifier shown in Figure (6,) uses two matched MOSFET's M_1 and M_2 with $K=2mA/V^2$ and $V_A=\infty$.

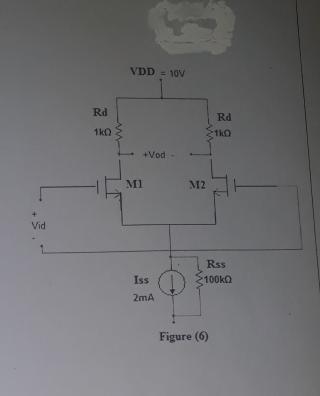
Calculate:

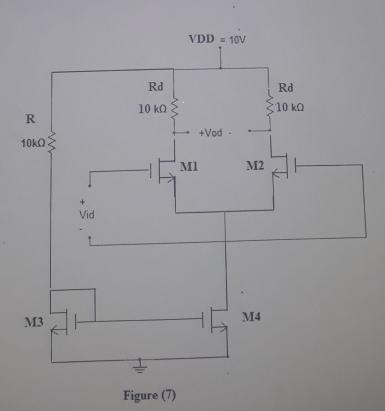
- 1. The Value of the drain current for M_1 and M_2 .
- 2. The differential mode gain A_{dm} .
- 3. The common mode gain A_{cm} .
- 4. The CMRR in decibel (dB).

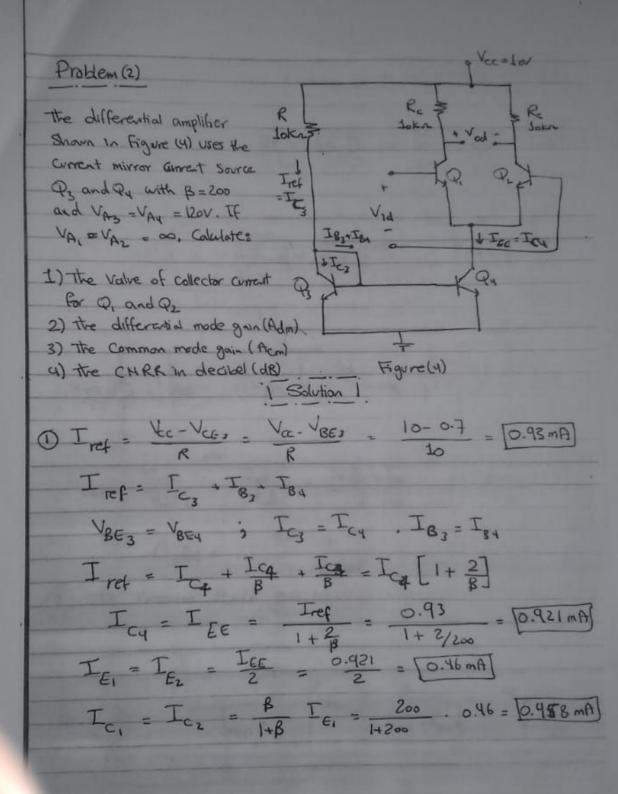
Problem (5)

The differential amplifier shown in Figure (7) uses the current mirror current source M3 and M4 with $K = 0.5 \text{mA/V}^2$ and $V_{A3} = V_{A4} = 120 \text{V}$. If $V_{A1} = V_{A2} = \infty$, Calculate:

- 1. The differential mode gain A_{dm}.
- 2. The common mode gain A_{cm}.
- 3. The CMRR in decibel (dB).







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The differential mode gain:

$$R_{EE} = r_{O4} = \frac{V_{Au}}{I_{C4}} = \frac{120}{0.921} = \frac{130.29km}{30.29km} R_{E} = \frac{120}{100} R_{E}$$

$$= \frac{V_{Au}}{I_{C4}} = \frac{120}{0.921} = \frac{130.29km}{10.92km} R_{E} = \frac{120}{100} R_{E}$$

$$= \frac{200 \times 0.025}{0.458} = \frac{10.92km}{10.92km} R_{E} = \frac{120}{100} R_{E}$$

$$= \frac{10.92km}{100} R_{E} = \frac{10.92km}{100} R_{E}$$

$$= \frac{10.92km}{100} R_{E} = \frac{183.15}{100} R_{E}$$

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$$A_{CM} = \frac{V_{0c}}{V_{1c}} = \frac{-\beta i k}{k^{2}} R_{c}$$

$$A_{CM} = \frac{-\beta R_{c}}{r_{TT}} + 2 R_{ec} (1+\beta) = \frac{-200 \times 10}{10.42 + 2(130.24)} (1+00)$$

$$A_{CM} = -0.038$$

$$A_{CM} = -0.038$$

$$A_{CM} = \frac{A_{dM}}{A_{cM}} = \frac{183.15}{0.038} = 4797.39$$

$$CMRR(dB) = 20 \log 4797.39 = [73.62 dB]$$

 $x IE_1 = 1mA$ Note: D.c Analysis vei Jez Ve1 = -0.7V Ver = -0.7V i I=0 " IE = 1 mA = Ici : IEz=IMA = ICZ PAI = YX2 = B TE = 100X (52) = 2.5 KM Part Common-Base Win & En RE EZ

RE Common-Base

Common-Base

Common-Base

Common-Base

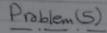
Common-Base

Common-Base

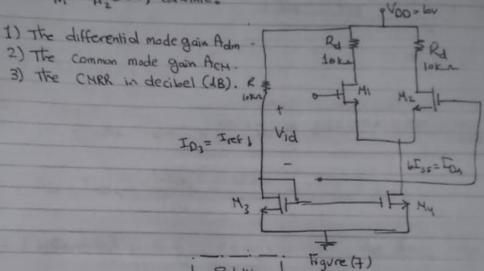
Common-Base Dry Common-Base Vin Bibi | RE | E2 | Bibi | Bi ≥ Rc Rout (1+B)(b2 = - (1+B) (b) : 262 = - 661

Av=Vo Vo=-Bibz Rc = +Bibi Rc [Vo= Bibi Rc] 0 * Vin = 16, 1/x + (1+B) (b) RE-162 1/x Un=[YX+G+B]RE+YX] Cbi Win = (2 Yx + CI+B) RESib, (2) 0+6 Av= Vo = BRC
21/17 + 4+B)RE AV= 100×7.5 = 750 2×2.5+101×0.2 = 5+101×1.12= * Rin = Vin = From @ $R_{in} = 2 \int_{X} + (1+\beta) R E = 2 \times 2.5 + \log x \cdot .2$ * Row = Rc = 7.5 km

As Un = (- ib) = (open)



The differential amplifier shown in figure 7) uses the current mirror current source H3 and H4 with $K=0.5\,\text{mA}\,\text{lV}^2$ and $V_{A_3}=V_{A_3}=120\text{V}$. IF $V_{A_1}=V_{A_2}=\infty$, Calulate:



1 DC Analysis - Condition For Saturation Vos > VGS- 4

[Known]
$$T_{O_3} = \frac{K}{2} (V_{GS_3} - V_T)^2$$

 $1 - 0.1 V_{GS_3} = \frac{0.5}{2} (V_{GS_2} - 1)^2$
 $4 - 0.4 V_{GS_3} = V_{GS_3}^2 - 2 V_{GS_3} + 1$

$$V_{GS_3}^2 = 1.6 V_{GS_3} = V_{GS_3}^2 = 2.71 \times 10^{-1.11} \times 10^{-1.$$

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2) Common mode gain (Acm)
$$V_{i_1} = V_{i_2} = V_{i_2} = V_{i_2} = V_{i_2} = V_{i_3} = V_{i_4} = V_{i_5} = V_{i_5}$$

3) CMRR =
$$\left| \frac{A_{dM}}{A_{CM}} \right| = \frac{6.041}{0.0302} = 199.88$$

CMRR(dB) = 20 log 199.88 = $\frac{46.02 \text{ dB}}{20.02 \text{ dB}}$