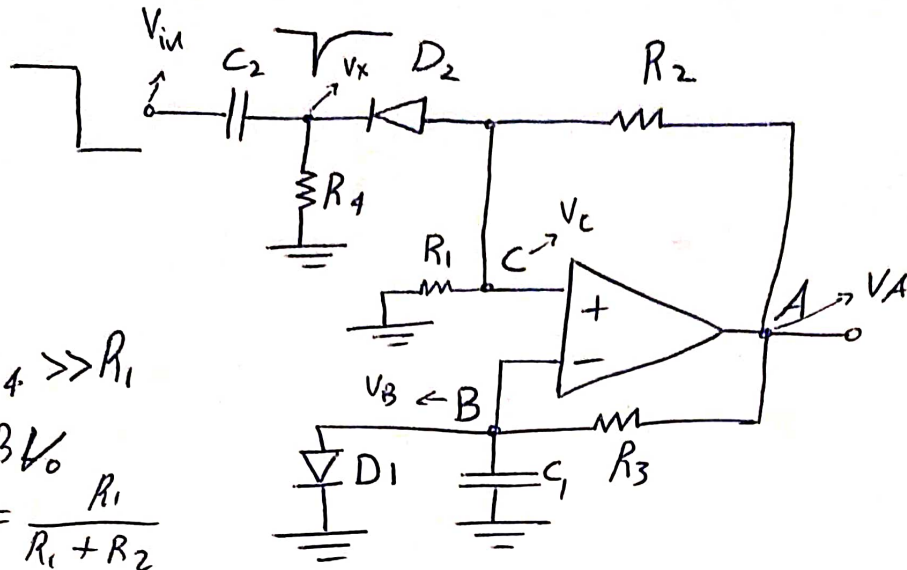


Monostable Multivibrator :



* Assume $R_4 \gg R_1$

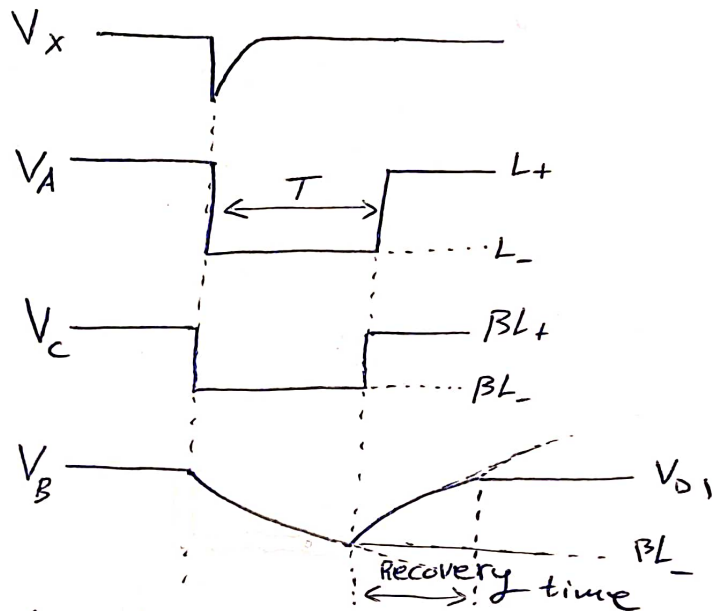
$$\begin{aligned} \rightarrow V_c &\approx \beta V_o \\ \rightarrow \beta &= \frac{R_1}{R_1 + R_2} \end{aligned}$$

* When -ve pulse is applied at $V_{in} \Rightarrow C_2$ discharges forcing V_x to drop.

\rightarrow this will force D_2 to conduct & forces V_c to drop.

When V_c reaches V_{D1} , V_A will switch to $L_- \Rightarrow D_2$ now will cutoff & C_1 will start to discharge through R_3 (note that its initial value is V_{D1} due to diode D_1).

$\rightarrow C_1$ will continue discharging until $V_B \leq \beta L_-$, at this Pt. the op-amp will switch V_A to L_+ & C_1 starts to charge again till it reaches V_{D1} .



To determine the width of pulse T :

T is the same time the capacitor C_1 takes to discharge from $+V_{D1}$ to βL_- .

$\therefore V_A = L_-$ during the discharge

$$\Rightarrow V_B = V_{src} + (V_{initial} - V_{src}) e^{-\frac{t}{\tau}}, \quad \tau = R_3 C_1$$

$$= L_- + (V_{D1} - L_-) e^{-\frac{t}{R_3 C_1}}$$

at $t = T \Rightarrow V_B = \beta L_-$

$$\Rightarrow \beta L_- = L_- + (V_{D1} - L_-) e^{-\frac{T}{R_3 C_1}}$$

$$\Rightarrow \beta L_- - L_- = (V_{D1} - L_-) e^{-\frac{T}{R_3 C_1}}$$

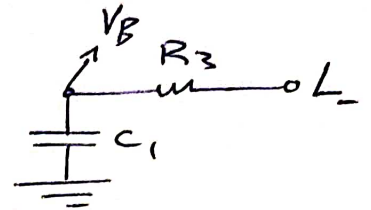
$$\Rightarrow e^{\frac{T}{R_3 C_1}} = \frac{V_{D1} - L_-}{\beta L_- - L_-}$$

$$\Rightarrow \frac{T}{R_3 C_1} = \ln \left(\frac{V_{D1} - L_-}{\beta L_- - L_-} \right)$$

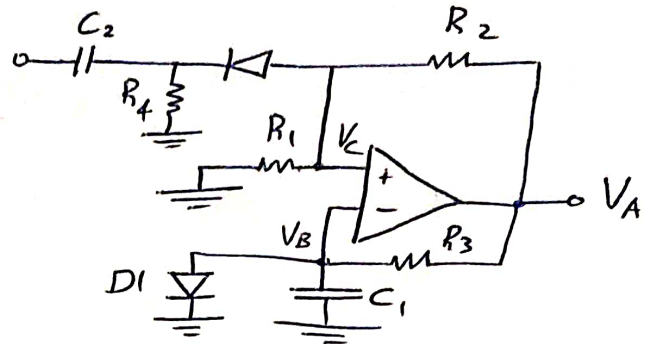
$$\Rightarrow \boxed{T = R_3 C_1 \ln \left(\frac{V_{D1} - L_-}{\beta L_- - L_-} \right)}$$

if $|L_-| \gg V_{D1}$:

$$\Rightarrow T \approx R_3 C_1 \ln \left(\frac{1}{1 - \beta} \right)$$



- Q. For a monostable circuit find the value of R_3 that will result in a 100- μ s o/p pulse for $C_1 = 0.1 \mu$ F, $\beta = 0.1$, $V_D = 0.7$ V, & $L_+ = -L_- = 12$ V.
- 2) Calculate the recovery time.



Sol:

$$1) \quad T = R_3 C_1 \ln \left(\frac{V_{D1} - L_-}{\beta L_- - L_-} \right)$$

$$\Rightarrow R_3 = \frac{100 \times 10^{-6}}{0.1 \times 10^{-6} \times \ln \left(\frac{0.7 + 12}{-(0.1)(12) + 12} \right)} = 6.17 \text{ K}\Omega$$

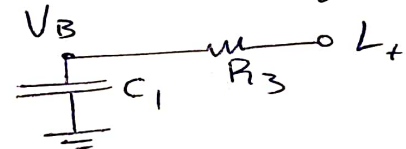
- 2) during the recovery of C_1 voltage, C_1 will charge through R_3 until it reaches V_{D1} .

From ($V_A = L_+$)

$D1$ will clamp the voltage at V_{D1}

$$\Rightarrow V_B(t) = V_{SRC} + (V - V_{SRC}) e^{-t/\tau}, \quad \tau = R_3 C_1$$

\downarrow \downarrow
 L_+ V_D



$$\Rightarrow V_B(t) = L_+ + (\beta L_- - L_+) e^{-t/R_3 C_1}$$

at $t = T_{\text{recovery}} \Rightarrow V_B = V_{D1}$

$$\Rightarrow V_{D1} = L_+ + (\beta L_- - L_+) e^{-\frac{T_{\text{recovery}}}{R_3 C_1}}$$

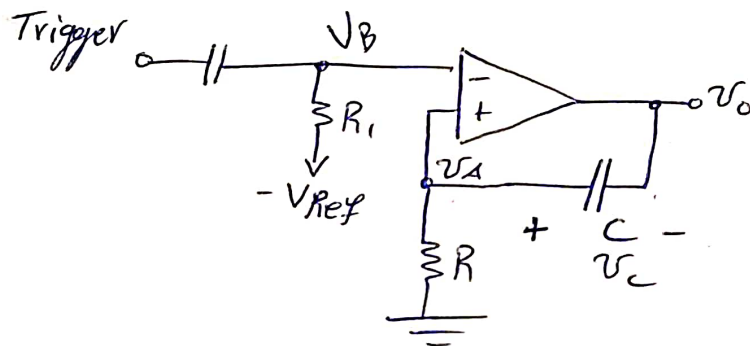
$$\Rightarrow e^{\frac{T_{\text{recovery}}}{R_3 C_1}} = \frac{\beta L_- - L_+}{V_{D1} - L_+}$$

$$\Rightarrow T_{\text{recovery}} = R_3 C_1 \ln \left(\frac{\beta L_- - L_+}{V_{D1} - L_+} \right) = (6.17 \times 10^3 \times 0.1 \times 10^{-6}) \ln \left(\frac{-13.2}{0.7 - 12} \right) = 95.89 \mu\text{s}$$

$$\beta L_- = (0.1)(-12) = -1.2$$

Q2: The given ct. shows a monostable multivibrator
 ct. given that in its stable state, $V_o = L_+$, $V_A = 0$, &
 $V_B = -V_{Ref}$. The ct. can be Triggered by applying
 a +ve input pulse of height greater than V_{Ref}
 For normal operation, $R_1 C_1 \ll RC$. Show the
 resulting waveforms of V_o & V_A . Also show
 that the pulse generated at the output will have
 a width T given by:

$$T = RC \ln \left(\frac{L_+ - L_-}{V_{Ref}} \right)$$



Sol:

Voltage across C

$$V_C = V_{final} + (V_{initial} - V_{final}) e^{-\frac{t}{\tau}}$$

Trigger:

$$\tau = RC$$

$$\Rightarrow V_C = -L_- + (L_- - L_+) e^{-\frac{t}{\tau}}$$

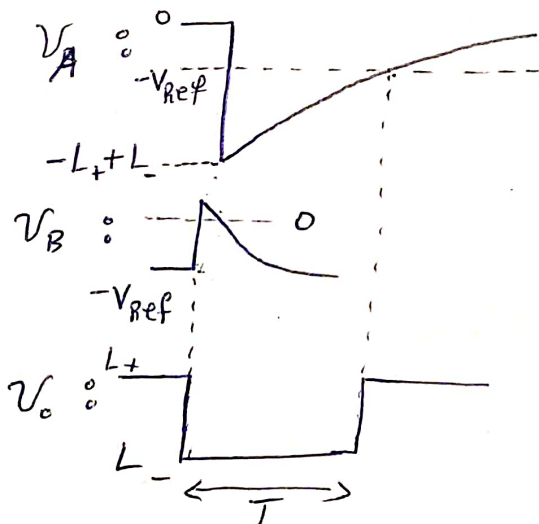
$$V_A = V_C + V_o$$

$$\Rightarrow V_A = V_C + L_-$$

$$V_A = (L_- - L_+) e^{-\frac{t}{\tau}}$$

at $t = T \Rightarrow V_A = -V_{Ref}$

$$-V_{Ref} = (L_- - L_+) e^{-\frac{T}{\tau}}$$



$$\Rightarrow e^{+T/\tau} = \frac{L_- - L_+}{-V_{REF}} = \frac{L_+ - L_-}{V_{REF}}$$

$$\Rightarrow T = \tau \ln \left(\frac{L_+ - L_-}{V_{REF}} \right)$$

$$\Rightarrow \boxed{T = RC \ln \left(\frac{L_+ - L_-}{V_{REF}} \right)}$$

↳ in this case the time of the pulse can be adjusted by changing V_{REF} .
