

COMS 30115

Classic Radiosity

Carl Henrik Ek - carlhenrik.ek@bristol.ac.uk March 18th, 2018

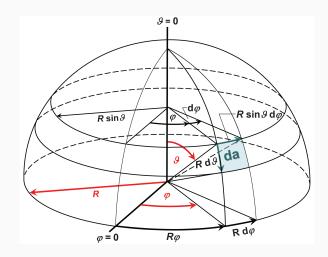
http://www.carlhenrik.com

Introduction

Last Time

- Hemisphere
- BRDFs
- Rendering Equation

Hemisphere



BRDFs

 The BRDF tells us how to represent reflected radiance in terms of incoming radiance

$$L_r(x \to \Theta) = \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

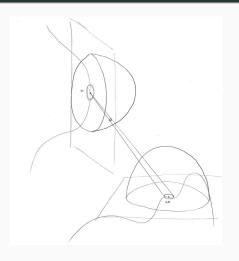
Putting these together gives the rendering equation,

$$L(x \to \Theta) = L_{e}(x \to \Theta) + \int_{\Omega_{x}} f_{r}(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_{x}, \Psi) d\omega_{\Psi}$$

• We want to solve for the radiance $L(\forall x \to \forall \theta)$ for the whole scene, why is this complicated?

3

Rendering Equation



$$L(x \to \Theta) = L_e(x \to \Theta) + \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

Today

- Area formulation of the rendering equation
- Classic Radiosity

Cornell Box



Material

- Comparing two Global Illumination Models
- Radiosity
- Equation Compendium

- Our eyes sensitive to radiance
- Want to compute radiance from all "surfaces" & solid angles
- Flux is emitted from light sources
- The rendering equation tells us how this flux is distributed in the scene

$$L(x \to \Theta) = L_e(x \to \Theta) + \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

$$L(x \to \Theta) = L_{e}(x \to \Theta)$$

$$+ \int_{\Omega_{x}} f_{r}(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_{x}, \Psi) d\omega_{\Psi}$$

$$= L_{e}(x \to \Theta) + \mathcal{T}(L(x \to \Theta))$$

$$L(x \to \Theta) = L_e(x \to \Theta)$$

$$+ \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

$$= L_e(x \to \Theta) + \mathcal{T}(L(x \to \Theta))$$

$$\mathcal{T}(L(x \to \Theta)) = \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

$$\mathbf{x}^{\mathrm{T}}\mathbf{a} = \sum_{i=1}^{D} x_i \cdot a_i, \quad \langle f, g \rangle = \int f(x)g(x) \mathrm{d}x$$

- Rendering Equation formulates recursive transport
- Transport is a <u>linear</u> operator in radiance

$$\langle F^{\rightarrow}, G^{\leftarrow} \rangle = \int_{A} \int_{\Omega} F(x \to \Theta) G(x \leftarrow \Theta) \cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA$$

Inner product formulation

 Transport problem can be written as the inner-product of two functions

$$L(x \to \Theta) = L = L_e + \langle T, L \rangle$$

$$L(x \to \Theta) = L = L_e + \langle T, L \rangle$$

= $L_e + \langle T, L_e \rangle + \langle T, TL \rangle$

$$L(x \to \Theta) = L = L_e + \langle T, L \rangle$$

$$= L_e + \langle T, L_e \rangle + \langle T, TL \rangle$$

$$= L_e + \langle T, L_e \rangle + \langle T, TL_e \rangle + \langle T, TTL_e \rangle + \dots$$

$$L(x \to \Theta) = L = L_e + \langle T, L \rangle$$

$$= L_e + \langle T, L_e \rangle + \langle T, TL \rangle$$

$$= L_e + \langle T, L_e \rangle + \langle T, TL_e \rangle + \langle T, TTL_e \rangle + \dots$$

• Adjoint operator:

$$\forall F, G \in V : \langle \mathcal{O}_1 F, G \rangle = \langle F, \mathcal{O}_2 G \rangle$$

$$\begin{split} L(x \to \Theta) &= L = L_e + \langle T, L \rangle \\ &= L_e + \langle T, L_e \rangle + \langle T, TL \rangle \\ &= L_e + \langle T, L_e \rangle + \langle T, TL_e \rangle + \langle T, TTL_e \rangle + \dots \end{split}$$

Adjoint operator:

$$\forall F, G \in V : \langle \mathcal{O}_1 F, G \rangle = \langle F, \mathcal{O}_2 G \rangle$$

- Think raytracer!
- Computing light transport back to light source or from light source are adjoint operators
- Remember dual formulation of raytracing

How to proceed

1. Input: geometry and emitted light

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- 3. What is the set of points & solid angles?

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- 3. What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- 3. What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?
- 4. How do we perform series expansion?

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- 3. What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?
- 4. How do we perform series expansion?
 - How does normal raytracing do this?

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- 3. What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?
- 4. How do we perform series expansion?
 - How does normal raytracing do this?
 - Perceptual importance?

- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?
- 4. How do we perform series expansion?
 - How does normal raytracing do this?
 - Perceptual importance?
- 5. Different algorithms approach this in different way

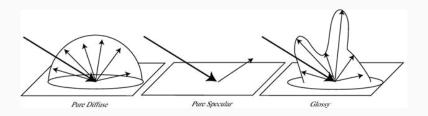
- 1. Input: geometry and emitted light
- 2. Output: radiance for position & solid angle
- What is the set of points & solid angles?
 - what is the perceptual importance of each part of the geometry?
- 4. How do we perform series expansion?
 - How does normal raytracing do this?
 - Perceptual importance?
- 5. Different algorithms approach this in different way
- 6. We know that energy is balanced in the scene



- Initially developed for solving heat transfer
- Formulation for Computer Graphics¹
- Game engine Geomerics²

¹Goral, C. M., Torrance, K. E., Greenberg, D. P., & Battaile, B. (1984).

²http://www.geomerics.com/



- Diffuse reflections means that reflection is the same in all directions
- This means radiance is the same in each direction
- This simplifies the problem rendering problem hugely
- Classic Radiosity assumes all surfaces are perfectly diffuse

Radiosity the exitant radiant power on a surface per unit surface area

Radiance the radiant power per unit projected area per unit solid angle

•
$$L(x)$$
 - $[Watt/steradian \cdot m^2]$

If we are assuming each surface to be diffuse we do not need the angle

$$B_{i} = \frac{1}{A_{i}} \int_{S_{i}} \int_{\Omega_{x}} L(x \to \Theta) cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$L(x \to \Theta) = L_e(x \to \Theta)$$

$$+ \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

- Angles does not matter if we have perfectly diffuse surfaces
- Write the rendering equation in terms of surfaces instead

$$L(x \to \Theta) = L_e(x \to \Theta)$$

$$+ \int_{\Omega_x} f_r(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

$$= L_e(x) + \int_{\Omega_x} f_r(x) L(x \leftarrow \Psi) cos(\mathbf{n}_x, \Psi) d\omega_{\Psi}$$

- Angles does not matter if we have perfectly diffuse surfaces
- Write the rendering equation in terms of surfaces instead

$$L(x \to \Theta) = L_{e}(x \to \Theta)$$

$$+ \int_{\Omega_{x}} f_{r}(x, \Psi \to \Theta) L(x \leftarrow \Psi) cos(\mathbf{n}_{x}, \Psi) d\omega_{\Psi}$$

$$= L_{e}(x) + \int_{\Omega_{x}} f_{r}(x) L(x \leftarrow \Psi) cos(\mathbf{n}_{x}, \Psi) d\omega_{\Psi}$$

$$= L_{e}(x) + \rho(x) \int_{S} K(x, y) L(y) dA_{y}$$

- Angles does not matter if we have perfectly diffuse surfaces
- Write the rendering equation in terms of surfaces instead

$$B_i = \frac{1}{A_i} \int_{S_i} \int_{\Omega_x} L(x \to \Theta) cos(\mathbf{n}_x, \Theta) \mathrm{d}\omega_{\Theta} \mathrm{d}A_x$$

$$B_{i} = \frac{1}{A_{i}} \int_{S_{i}} \int_{\Omega_{x}} L(x \to \Theta) cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$
$$= \frac{1}{A_{i}} \int_{S_{i}} L(x) \int_{\Omega_{x}} cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$B_{i} = \frac{1}{A_{i}} \int_{S_{i}} \int_{\Omega_{x}} L(x \to \Theta) cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$= \frac{1}{A_{i}} \int_{S_{i}} L(x) \int_{\Omega_{x}} cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$= \frac{1}{A_{i}} \int_{S_{i}} L(x) \pi dA_{x}$$

$$B_{i} = \frac{1}{A_{i}} \int_{S_{i}} \int_{\Omega_{x}} L(x \to \Theta) cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$= \frac{1}{A_{i}} \int_{S_{i}} L(x) \int_{\Omega_{x}} cos(\mathbf{n}_{x}, \Theta) d\omega_{\Theta} dA_{x}$$

$$= \frac{1}{A_{i}} \int_{S_{i}} L(x) \pi dA_{x}$$

$$= \frac{1}{A_{i}} \int_{S_{i}} B(x) dA_{x}$$

Reflectivity

 If we have only perfectly diffuse surfaces we don't need full BRDF

$$\rho(x)$$
 - reflectivity at point x

 The light that arrives at point x from surface y only depends on visibility

K(x,y) — how much of light leaving point y arrives at x

$$\frac{1}{A_i} \int_{S_i} B(x) \mathrm{d}A_x = \frac{1}{A_i} \int_{S_i} B_e(x) \mathrm{d}A_x + \frac{1}{A_i} \int_{S_i} \rho(x) \int_{S} K(x,y) B(y) \mathrm{d}A_y \mathrm{d}A_x$$

Assumption the radiosity is constant across a patch

$$\forall x \in S_i : B(x) = B_i$$

Assumption the reflectivity is constant across $\forall x \in S_i : \rho(x) = \rho_i$

$$\frac{1}{A_i} \int_{S_i} B(x) dA_x = \frac{1}{A_i} \int_{S_i} B_e(x) dA_x + \frac{1}{A_i} \int_{S_i} \rho(x) \int_{S} K(x, y) B(y) dA_y dA_x$$

$$B_i = B_{ei} + \rho_i \sum_j \frac{1}{A_i} \int_{S_i} \int_{S_j} K(x, y) B(y) dA_y dA_x$$

Assumption the radiosity is constant across a patch

$$\forall x \in S_i : B(x) = B_i$$

Assumption the reflectivity is constant across $\forall x \in S_i : \rho(x) = \rho_i$

$$\frac{1}{A_i} \int_{S_i} B(x) dA_x = \frac{1}{A_i} \int_{S_i} B_e(x) dA_x + \frac{1}{A_i} \int_{S_i} \rho(x) \int_{S} K(x, y) B(y) dA_y dA_x$$

$$B_i = B_{ei} + \rho_i \sum_j \frac{1}{A_i} \int_{S_i} \int_{S_j} K(x, y) B(y) dA_y dA_x$$

$$B_i = \frac{1}{A_i} \int_{S_i} B(x) dA_x$$

$$\rho_i = \rho(x)$$

Assumption the radiosity is constant across a patch

$$\forall x \in S_i : B(x) = B_i$$

Assumption the reflectivity is constant across $\forall x \in S_i : \rho(x) = \rho_i$

$$B_i = B_{ei} + \rho_i \sum_j \frac{1}{A_i} \int_{S_i} \int_{S_j} K(x, y) B(y) dA_y dA_x$$

- Discretise the scene into patches
- K(x,y) constant over patch
- \bullet F_{ij} is depends only on the geometry
- referred to as a form factor

$$B_{i} = B_{ei} + \rho_{i} \sum_{j} \frac{1}{A_{i}} \int_{S_{i}} \int_{S_{j}} K(x, y) B(y) dA_{y} dA_{x}$$
$$= B_{ei} + \rho_{i} \sum_{j} F_{ij} B_{j}$$

- Discretise the scene into patches
- K(x,y) constant over patch
- \bullet F_{ij} is depends only on the geometry
- referred to as a form factor

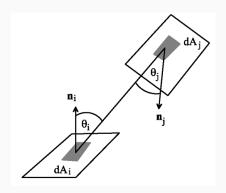
$$B_{i} = B_{ei} + \rho_{i} \sum_{j} \frac{1}{A_{i}} \int_{S_{i}} \int_{S_{j}} K(x, y) B(y) dA_{y} dA_{x}$$

$$= B_{ei} + \rho_{i} \sum_{j} F_{ij} B_{j}$$

$$F_{ij} = \frac{1}{A_{i}} \int_{S_{i}} \int_{S_{i}} K(x, y) dA_{y} dA_{x}$$

- Discretise the scene into patches
- K(x,y) constant over patch
- \bullet F_{ij} is depends only on the geometry
- referred to as a form factor

Form Factor



ullet "How large portion of the view from i is blocked by j"

$$B_i = B_{ei} + \rho_i \sum_j F_{ij} B_j$$

 $B_{ei} = B_i - \rho_i \sum_j F_{ij} B_j$

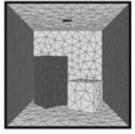
- The radiosity of patch B_i is a linear combination of radiosities of all other patches B_j
- Importantly the coefficients of this system depends only on geometry which is known and self emitted radiosity which is known

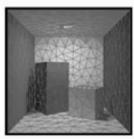
$$B_{ei} = B_{i} - \rho_{i} \sum_{j} F_{ij} B_{j}$$

$$\begin{bmatrix} B_{e1} \\ B_{e2} \\ \vdots \\ B_{en} \end{bmatrix} = \begin{bmatrix} 1 - \rho_{1} F_{11} & -\rho_{1} F_{12} & \dots & \rho_{1} F_{1n} \\ -\rho_{2} F_{21} & 1 - \rho_{2} F_{22} & \dots & \rho_{2} F_{2n} \\ \vdots & \vdots & \vdots & \vdots \\ -\rho_{n} F_{n1} & -\rho_{n} F_{n2} & \dots & 1 - \rho_{n} F_{nn} \end{bmatrix} \begin{bmatrix} B_{1} \\ B_{2} \\ \vdots \\ B_{n} \end{bmatrix}$$

- We know B_{ei} and we can comput F_{ij}
- Solve for Bi







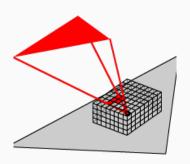
- Compute form factors
- Solve system of equations
- Render image (Raycaster)



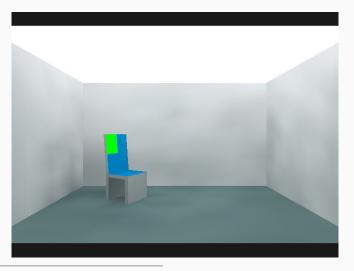
Discretisation Computational and storage cost
Form Factor Computations 1 Cubic storage in number of
patches

Form Factor Computations 2 Complicated integral Nummerical Solution Structure in coefficent to exploit

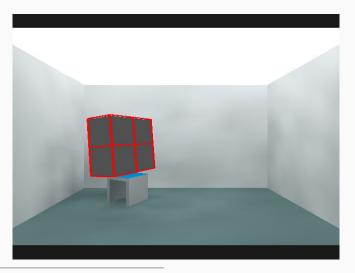
Hemicube approximation



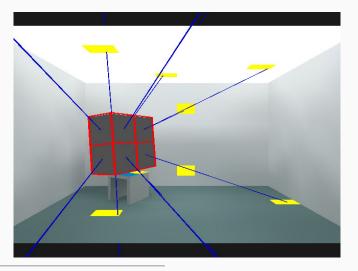
- Form factor computations are expensive
- Approximate with projections onto sphere



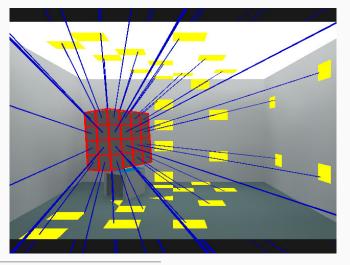
 $^{^{3}} http://www.deluxerender.com/2014/11/hemicube-form-factors/\\$



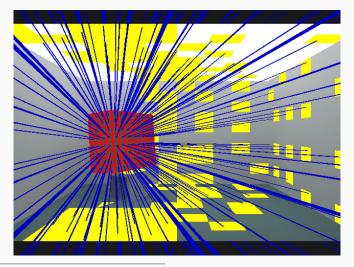
 $^{^{3}} http://www.deluxerender.com/2014/11/hemicube-form-factors/\\$



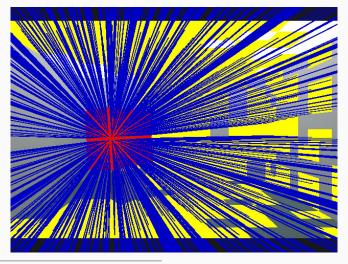
³http://www.deluxerender.com/2014/11/hemicube-form-factors/



³http://www.deluxerender.com/2014/11/hemicube-form-factors/

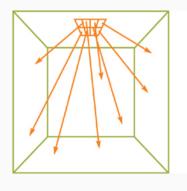


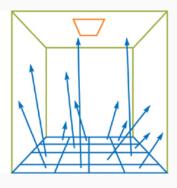
³http://www.deluxerender.com/2014/11/hemicube-form-factors/



³http://www.deluxerender.com/2014/11/hemicube-form-factors/

Progressive Radiosity⁴





- Solve equation iteratively
- Each patch stores, accumulated and residual energy
- Iterate until residual energy low

//http.developer.nvidia.com/GPUGems2/gpugems2_chapter39.html

⁴http:

Summary

Summary

- Intuition into rendering equation
- Cast raytracing as a solution to the rendering equation
- Classic Radiosity
 - very clear what assumptions are
 - images look very "radiosity" ;-)

Next Time

Lecture Monday 23rd of March

• Path Tracing (Stochastic Methods)

Lecture Thursday 16th of April

Photon Mapping (Caustics)

Lecture Monday 27th of April

- Last lecture
- Unit Summary

eof