### **EE-379 Linear Control Systems**

#### Week No. 6: Root Locus Analysis

- Background
- Pole Zero Plots
- General Method
- Construction Rules
- > Examples

#### **Background**

- Chapter 1: D.E can be written for various systems and can be solved, and the response could be divided into forced and natural components
- Chapter 2: Established definitions related to natural response and types of stability (stability is generally considered to be the property of the natural response)
- Chapter 3: The other response component (steady state) was considered that is the tendency of a device to follow (track) a command.
- Chapter 4: Return to stability and provide a very broad and useful measure as compared to the Routh Hurwitz criterion.

#### **Background**

- Logical approach to determine stability would be to
  - ✓ Extract roots of the characteristic polynomial as the adjustable gain varies (computational packages i.e., MATLAB can readily perform this task)
  - ✓ Walter Evans (1940) developed a set of rules by which the path traced by roots of a closed loop characteristic equation can be sketched this plot is the root locus.
  - ✓ There are two chapters devoted to root locus: in chapter 4 we will concentrate on the basic understanding of root locus principles

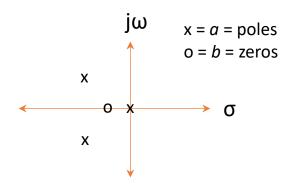
#### **Background**

- Zeros are the values at which the function is zero (numerator roots)
- Poles are the values at which the function is infinite (denominator roots)
- A rational function in the factored form is given by:
- The constant  $k = \frac{b_m}{a_m}$  is the multiplying constant
- When poles and zeros are plotted on the complex plain the result is a pole-zero plot

$$F(s) = \frac{b_m s^m + b_{m-1} s^{m-1} + \dots + b_0}{s^n + a_{n-1} s^{m-1} + \dots + a_0}$$

$$F(s) = \frac{K[(s - z_1)(s - z_2) \dots (s - z_m)]}{[(s - p_1)(s - p_2) \dots (s - p_n)]}$$

 $z_1, z_2, z_{3,...}z_m$  are the zeros of the function  $p_1, p_2, p_{3,...}p_n$  are the poles of the function



$$F(s) = \frac{4s+5}{s^3+4s^2+13s} = \frac{4(s+5/4)}{s(s+2+3j)(s+2-3j)}$$

#### **Pole-Zero Plot: Graphical Evaluation**

- The roots of the closed-loop characteristic equation define the system characteristic responses.
- Their location in the complex s-plane lead to the prediction of the characteristics of the time domain responses in terms of:
  - ✓ damping ratio,  $\zeta$ ✓ natural frequency,  $\omega_n$ ✓ damping constant, bSecond order modes
    first order modes
- Consider how these roots change as the loop gain is varied from 0 to ∞

#### **Example**

The closed-loop transfer function is

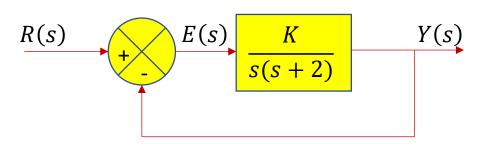
$$T(s) = \frac{Y(s)}{R(s)} = \frac{K}{s(s+2) + K}$$

The characteristic equation is

$$s^2 + 2s + K = 0$$

Consider the characteristic roots as:

$$K = 0 \rightarrow \infty$$

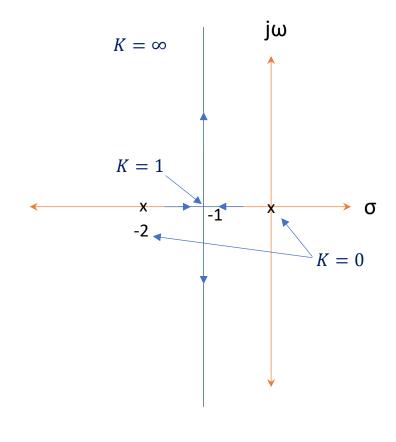


#### **Example**

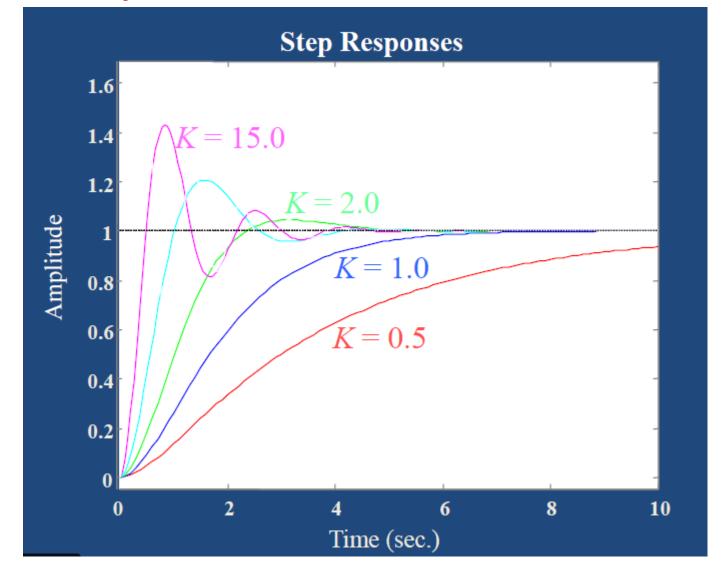
$$s = -1 \pm \sqrt{1 - K}$$

- For K = 0 the closed-loop poles are at the **open-loop poles**.
- For 0 < K < 1 the closed loop poles are on the **real axis**:
- For K > 1 the closed-loop poles are complex, with a real value of -1 and an imaginary value increasing with gain K.

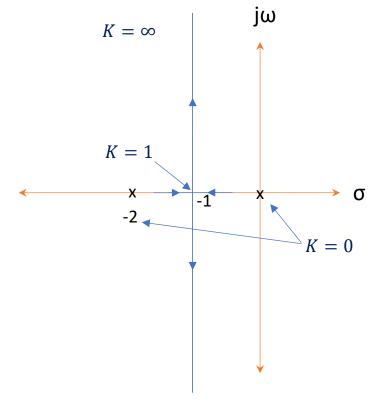
#### Loci of closed-loop roots



#### **Example**



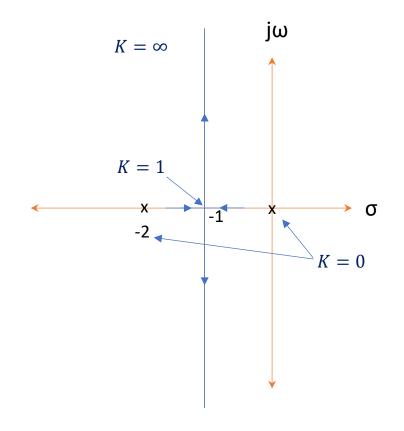
#### **Loci of closed-loop roots**



#### **Example-Observations**

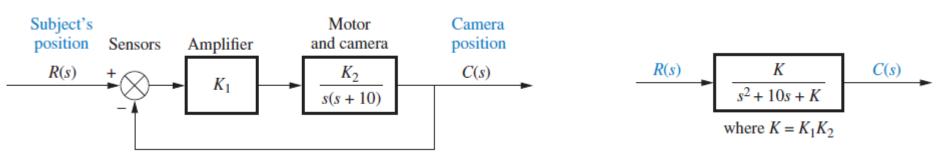
- This is a second-order system and there are two loci.
- The root loci start at the open loop poles
- The root loci tend towards the open loop zeros at infinity as  $K \to \infty$ . (Note: the **number of zeros** is equal to the **number of poles** when the zeros at infinity are included.)
- The relationship between the characteristic responses and the increasing gain is seen through the root loci.

#### Loci of closed-loop roots



**Pole-Zero Plot** 





**Root Locus Plot** 

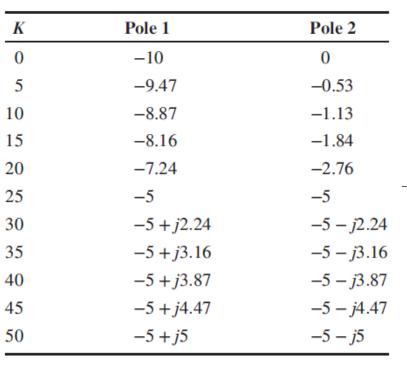
20 15 10 5

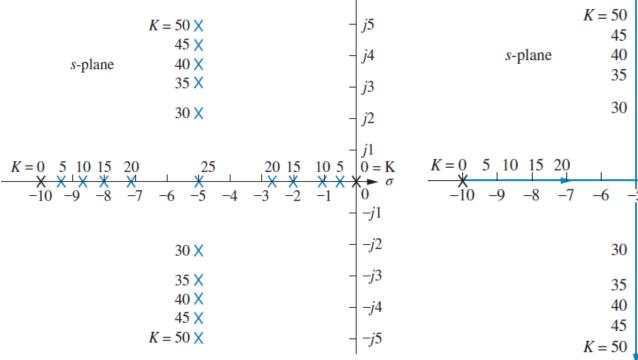
−*j*2

−*j*3

-j4

*−j*5

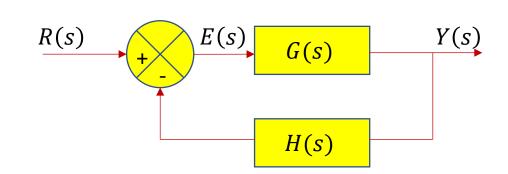




#### The General Root Locus Method

Consider the general system

$$T(s) = \frac{Y(s)}{R(s)} = \frac{G(s)}{1 + GH(s)}$$



The characteristic equation is

$$1 + GH(s) = 0$$
  $\Rightarrow$   $GH(s) = -1$   $\rightarrow$  Complex quantity

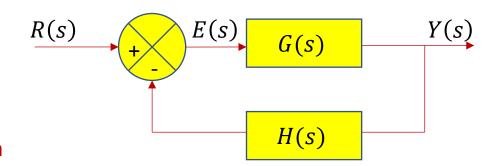
Therefore, GH(s) = -1, can be split into two equations

- 1. |GH(s)| = 1  $\rightarrow$  represents magnitude
- 2.  $\angle GH(s) = (2k+1)180^{\circ} \rightarrow represents \ angle$

$$k = 0, \pm 1, \pm 2 \dots$$

#### The General Root Locus Method

- All values of 's' which satisfy
- $\circ |GH(s)| = 1$  Magnitude criterion
- $\bigcirc \angle GH(s) = (2k+1)180^{\circ} \text{ Angle criterion}$   $k = 0, \pm 1, \pm 2 \dots$



are roots of the closed-loop characteristic equation.

Consider the following general form

$$GH(s) = \frac{K[(s+z_1)(s+z_2)...(s+z_m)]}{[(s+p_1)(s+p_2)...(s+p_n)]}$$

#### The General Root Locus Method

• Then,

1. 
$$|GH(s)| = \frac{|K| \prod_{i=1}^{m} |s+z_i|}{\prod_{i=1}^{n} |s+p_i|} = 1$$
  $\longrightarrow$   $|F(s_0)| = \frac{|K| \binom{product \ of \ lengths \ of \ dir}{segment \ from \ poles \ to \ s_0}}{\binom{product \ of \ lengths \ of \ dir}{segment \ from \ poles \ to \ s_0}}$ 

The **magnitude condition** is that the **point** (which satisfied the angle condition) at which the **magnitude of the open loop transfer function is one**.

2. 
$$\angle GH(s) = \sum_{i=1}^{m} \angle(s + z_i) - \sum_{i=1}^{m} \angle(s + p_i) = (2k + 1)180^{\circ}$$
  $k = 0, \pm 1, \pm 2 \dots$   $\angle F(s_0) = (sum \ of \ angles \ of \ dir \ segments)$   $\angle F(s_0) = (from \ zeros \ to \ s_0) - (sum \ of \ poles \ angles) + 180^{\circ} \ (if \ K < 0)$ 

The angle condition is the point at which the angle of the open loop transfer function is an odd multiple of 180°.

#### **Pole-Zero Plot: Graphical Evaluation**

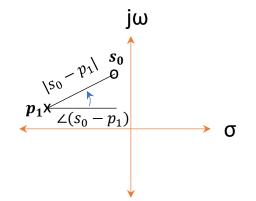
- On a **pole-zero** plot suppose a line is drawn from  $p_1$  to  $s_0$  where the function is being evaluated.
- This segment has length  $|s_0 p_1|$  and angle  $\angle (s_0 p_1)$  with real axis

$$F(s) = \frac{K[(s - z_1)(s - z_2) \dots (s - z_m)]}{[(s - p_1)(s - p_2) \dots (s - p_n)]}$$

$$F(s_0) = \frac{K[(s_0 - z_1)(s_0 - z_2) \dots (s_0 - z_m)]}{[(s_0 - p_1)(s_0 - p_2) \dots (s_0 - p_n)]}$$

$$F(s_0) = \frac{K(|s_0 - z_1|e^{j\angle(s_0 - z_1)})(|s_0 - z_2|e^{j\angle(s_0 - z_2)})}{(|s_0 - p_1|e^{j\angle(s_0 - p_1)})(|s_0 - p_2|e^{j\angle(s_0 - p_2)})}$$

$$|F(s_0)| = \frac{|K| \binom{product \ of \ lengths \ of \ dir}{segment \ from \ zeros \ to \ s_0}}{\binom{product \ of \ lengths \ of \ dir}{segment \ from \ poles \ to \ s_0}}$$



 $\angle F(s_0) = (sum\ of\ anglesof\ dir\ segments\ from\ zeros\ to\ s_0) - (sum\ of\ anglesof\ dir\ segments\ from\ poles\ to\ s_0) + 180^\circ\ (if\ k<0)$ 

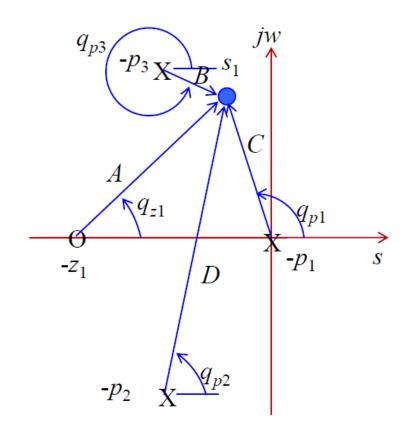
#### **General Method – Geometric Interpretation**

Consider the example,

$$GH(s) = \frac{K(s+z_1)}{s(s+p_2)(s+p_3)}$$

• Then the values of  $s = s_1$  which satisfy

1. 
$$\frac{K|s+z_1|}{|s||s+p_2||s+p_3|} = 1$$



2. 
$$\angle(s+z_1) - (\angle s + \angle(s+p_2) + \angle(s+p_3)) = (2k+1)180^{\circ}$$

are on the loci and are roots of the characteristic equation.

#### **General Method – Geometric Interpretation**

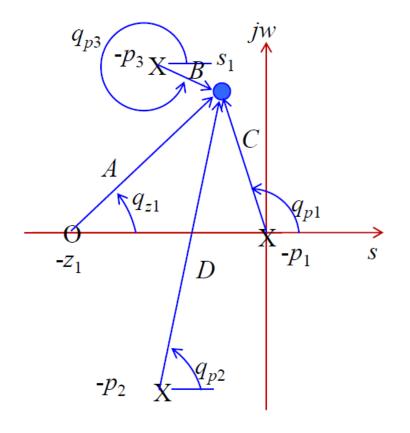
• In terms of vectors, the condition for  $s = s_1$  to be on the root loci:

$$\frac{|K|A}{BCD} = 1$$
 or  $\frac{A}{BCD} = \frac{1}{|K|}$ 

and,

$$\theta_{z1} - (\theta_{p1} + \theta_{p2} + \theta_{p3}) = (2k+1)180^{\circ}$$

$$k = 0. +1. +2 \dots$$



are roots of the characteristic equation.

#### **Analysis**

- When plotting the loci of the roots as  $K=0\to\infty$ , the magnitude condition is always satisfied. Along the root locus, the magnitude condition can always be satisfied by adjusting K
- Therefore, a value of  $s=s_1$  that satisfies the angle condition, is a point of the root loci
- The magnitude condition may then be used to determine the gain K corresponding to that value  $S_1$ .

#### **Analysis – Construction Rules**

1. The loci start (K = 0) at the poles of the open-loop system. There are n -loci.

2. The loci **terminate**  $(K \rightarrow \infty)$  at the zeroes of the open-loop system (include zeroes at infinity).

For our example system

$$|GH(s)| = \frac{K|s + z_1|}{|s||s + p_2||s + p_3|} = \frac{1}{K}$$

- Therefore, as  $K \to 0$   $GH(s) \to \infty$ , the poles of the loop  $transfer\ function$
- As,  $K \to \infty$   $GH(s) \to 0$ , the zeros of the loop transfer function

#### **Analysis – Construction Rules**

- 3. The root loci are **symmetrical** about the real axis.
- The roots with imaginary parts always occur in conjugate complex pairs

4. As  $K \to \infty$  the loci approach asymptotes. There are q = n - m asymptotes and they intersect the real axis at angles defined by

$$\frac{(2k+1)180^{\circ}}{q}$$
,  $k=0,\pm 1,\pm 2...(q-1)$ 

#### **Analysis – Construction Rules**

5. The asymptotes intersection point on the real axis is defined by.

$$\sigma_a = \frac{\sum poles \ of \ GH(s) - \sum zeroes \ of \ GH(s)}{q}$$

 Real axis sections of the root loci exist only where there is an odd number of poles and zeroes to the right.

#### **Analysis – Construction Rules: Example**

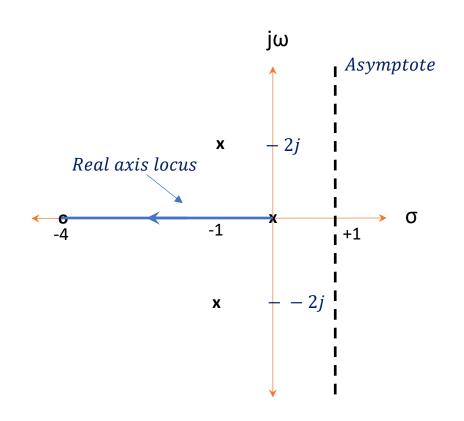
• Consider our example with  $z_1 = 4$ ,  $p_{12} = 1 \pm 2j$ 

$$GH(s) = \frac{K(s+4)}{s(s+1+2j)(s+1-2j)}$$

Asymptotes:

$$Angle = \frac{(2k+1)180^{\circ}}{3-1} = \pm 90^{\circ}$$

$$\sigma_a = \frac{[-0 - (1+2j) - (1-2j)] - [(-4)]}{3-1} = +1$$



#### **Analysis – Construction Rules**

- 7. The angles of departure,  $q_d$  from poles and arrival,  $q_a$  to zeroes may be found by applying the angle condition to a point very near the pole or zero.
- The angle of arrival at the zero,  $-t_1$  is obtained from

$$\theta_{az1} + \sum_{i=2}^{m} \angle(-z_1 + z_i) - \sum_{i=1}^{n} \angle(-t_1 + p_i) = (2k+1)180^{\circ}$$

This rule is applicable to "imaginary poles/zeros"

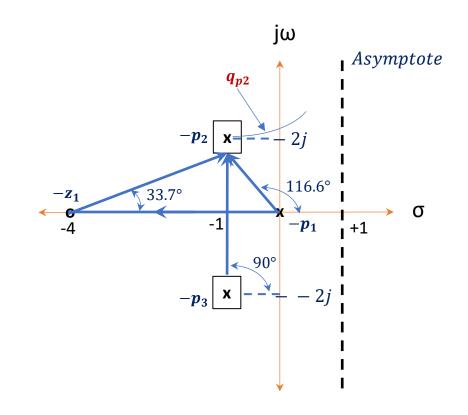
#### **Analysis – Construction Rules**

• Departure angle from,  $p_2$ .

$$q_{z1} = \tan^{-1}(2/3) = 33.7^{\circ}$$
  
 $q_{p1} = \tan^{-1}(-2/1) = 116.6^{\circ}$   
 $q_{p3} = 90^{\circ}$ 

Then,

$$33.7^{\circ} - (90^{\circ} + 116.6^{\circ} + q_{p2}) = 180^{\circ}$$
  
 $q_{p2} = -352.9^{\circ} = +7.1^{\circ}$ 



#### **Analysis – Construction Rules**

- 8. The imaginary axis crossing is obtained by applying the Routh-Hurwitz criterion and checking for the gain that results in marginal stability. The imaginary components are found from the solution of the resulting auxiliary equation
- Marginal stability refers to the point where the roots of the closedloop system are on the stability boundary, i.e. the imaginary axis.

#### **Analysis – Construction Rules**

Imaginary axis crossing: Characteristic equation

$$s(s+1+2j)(s+1-2j) + K(s+4) = 0$$
  
$$s^3 + 2s^2 + (5+K)s + 4K = 0$$

| $s^3$ | 1            | 5 + K      | 0 |
|-------|--------------|------------|---|
| $s^2$ | 2            | 4 <i>K</i> | 0 |
| $s^1$ | 5 <i>- K</i> | 0          |   |
| $s^0$ | 4 <i>K</i>   |            |   |

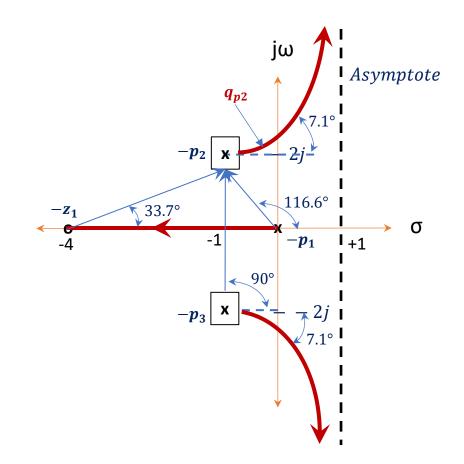
For marginal stability, K = 5 and the auxiliary equation is.

$$2s^{2} + 20 = 0$$
$$s = \pm \sqrt{10j} = \pm 3.16j$$

• Therefore, the imaginary axis intersection is  $= \pm 3.16j$ .

#### **Analysis – Construction Rules**

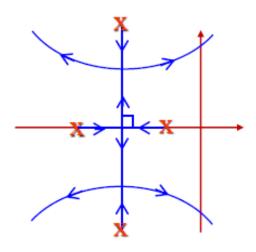
- Summary:
  - 1. There are three root loci.
    - I. One on the real axis from  $-p_1$  to  $-z_1$
    - II. A pair of loci from  $-p_2$  and  $-p_3$  to zeroes at infinity along the asymptotes.
  - 2. The departure angle from these poles is  $\pm 7.1^{\circ}$  and an imaginary axis crossing at  $s = \pm 3.16j$

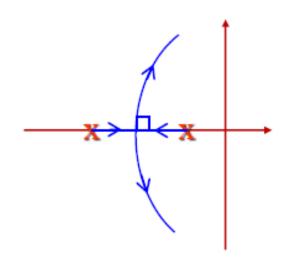


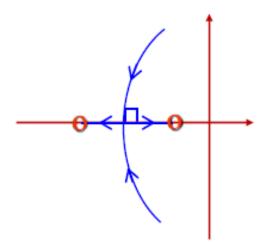
#### **Analysis – Construction Rules**

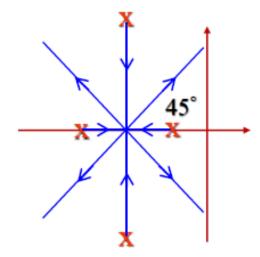
#### Breakaway Points

When two or more loci meet, they will break away from this point at particular angles. The point is known as a **breakaway point**. It corresponds to multiple roots.









#### **Analysis – Construction Rules**

- 9. The **angle** of breakaway is  $180^{\circ}/k$  where k is the number of closed-loop poles, departing from the breakaway point on the real axis.
- ✓ The **location** of the breakaway point is found from.

$$\frac{dK}{ds} = 0 \qquad or \quad \frac{d[GH(s)]}{ds} = 0$$

Note:

$$K = -[GH(s)]^{-1}$$

$$\frac{dK}{ds} = [GH(s)]^{-2} \frac{d[GH(s)]}{ds} = 0$$

• Also:

$$\frac{d[GH(s)]}{ds} = \frac{d[N(s)/D(s)]}{ds}$$
$$\frac{N'(s)}{D(s)} - \frac{N(s)D'(s)}{D(s)^2} = 0$$

$$D(s)N'(s) - N(s)D'(s) = 0$$

### **Analysis – Construction Rules**

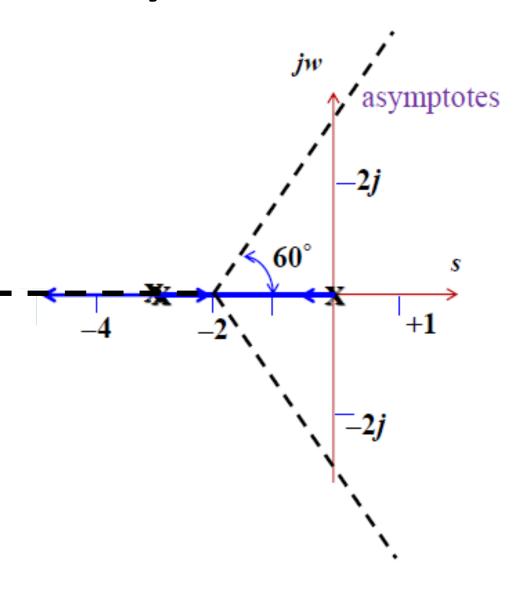
Consider the following loop

$$GH(s) = \frac{K}{s(s+3)^2}$$

- Real axis loci exist for the full negative axis. the following loop.
- Asymptotes:

$$=\frac{(2k+1)180^{\circ}}{3}=60^{\circ}, 180^{\circ}, 300^{\circ}$$

$$\sigma_a = \frac{(-3-3-0)-(0)}{3} = -2$$



### **Analysis – Construction Rules**

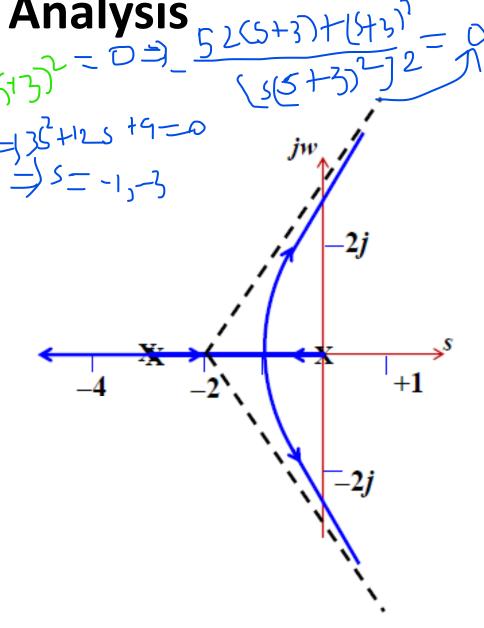
Determine the breakaway points from

$$\frac{d}{ds} \left[ \frac{K}{s(s+3)^2} \right] = \frac{d}{ds} \left[ \frac{K}{s^3 + 6s^2 + 9s} \right]$$

$$= -\frac{K(3s^2 + 12s + 9)}{(s^3 + 6s^2 + 9s)^2} = 0$$

Then,

$$(s^2 + 4s + 3) = (s + 1)(s + 3) = 0$$
  
 $s = -1, \qquad s = -3$ 



#### **Analysis – Construction Rules: Summary**

- 1. Plot the poles and zeros of the open-loop system.
- 2. Find the section of the loci on the real axis (odd number of poles and zeroes to the right).
- 3. Determine the asymptote angles and intercepts.

$$angles = \frac{(2k+1)180^{\circ}}{q}$$
  $where, q = n - m, and, k = 0, \pm 1, \pm 2, \pm 3 \dots (q-1)$ 

$$\sigma_a = \frac{\sum Poles - \sum zeros}{q}$$

# Analysis – Construction Rules: Summary 150 - ≤L

4. Determine departure angles in case of **imaginary poles**. For a pole  $-p_1$ .

$$\angle(-p_1+z_1)+\angle(-p_1+z_2)+\cdots-\theta_{p_1}-\angle(-p_1+p_2)-\angle(-p_1+p_3)=(2k+1)180^\circ$$

- 5. Check for imaginary axis crossings using the Routh-Hurwitz criterion.
- 6. Determine breakaway points in case of loci originates from two poles together.

$$angle = \frac{180^{\circ}}{k}$$
, where  $k = No \ of \ converging \ loci$ 

**location from** 
$$\frac{d[GH(s)]}{ds} = 0$$

7. Complete the plot

### **Analysis – Construction Rules: Example**

Loop Transfer function:

$$SH(s) = \frac{K}{s(s+4)(s^2+4s+20)}$$

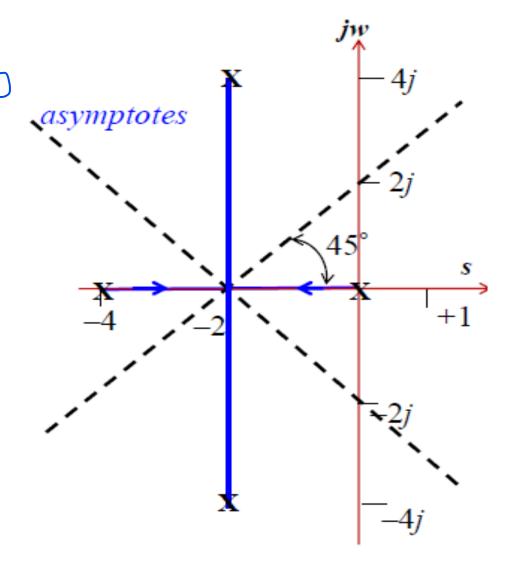
Roots:

$$s = 0, s = -4, s = -2 \pm 4j$$

- Real axis segments between 0 and -4
- Asymptotes:

$$angles = \frac{(2k+1)180^{\circ}}{4-0} = 45^{\circ}, 135^{\circ}, 225^{\circ}, 315^{\circ}$$

$$\sigma_a = \frac{(-4-2-2-0)}{4} = -2$$



#### **Analysis – Construction Rules: Example**

• Breakaway points:

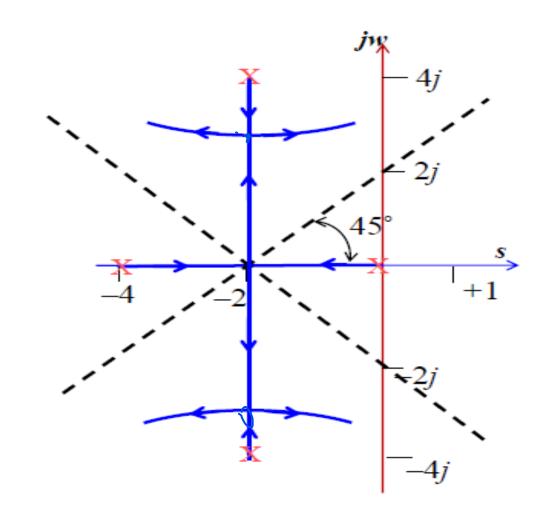
$$\frac{d}{ds} \left[ \frac{K}{s^4 + 8s^3 + 36s^2 + 80s} \right]$$

$$= \frac{K(4s^3 + 24s^2 + 72s + 80)}{s^4 + 8s^3 + 36s^2 + 80s} = 0$$

$$or \quad s^3 + 6s^2 + 18s + 20 = 0$$

$$solving \quad s_b = -2, -2 \pm 2.45j$$

Three points that breakaway at 90°



### **Analysis – Construction Rules: Example**



**Characteristics equation** 

$$s^4 + 8s^3 + 36s^2 + 80s + K = 0$$

| $s^4$ | 1                    | 36 | K |
|-------|----------------------|----|---|
| $s^3$ | 8                    | 80 | 0 |
| $s^2$ | 26                   | K  | 0 |
| $s^1$ | $80 - \frac{8K}{26}$ | 0  |   |
| $s^0$ | K                    |    |   |

Condition for critical stability

$$80 - \frac{8K}{26} > 0$$

The auxiliary equation

$$26s^2 + 260 = 0$$

Solving,

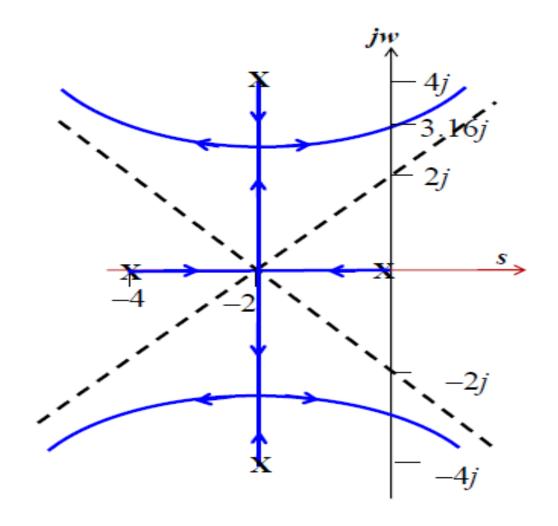
$$s = \pm \sqrt{10}j = \pm 3.16j$$

#### **Analysis – Construction Rules: Example**

The final plot is shown on the right.

What is the value of the gain K corresponding to the breakaway point at.

$$s_b = -2 \pm 2.45j$$
?



#### **Analysis – Construction Rules: Example**

• From the general magnitude condition the gain corresponding to the point  $s_1$  on the loci is.

$$K = \frac{\prod_{i=1}^{n} (s + p_i)}{\prod_{i=1}^{m} (s + z_i)}$$

• For the point  $s_1 = -2 \pm 2.45j$ 

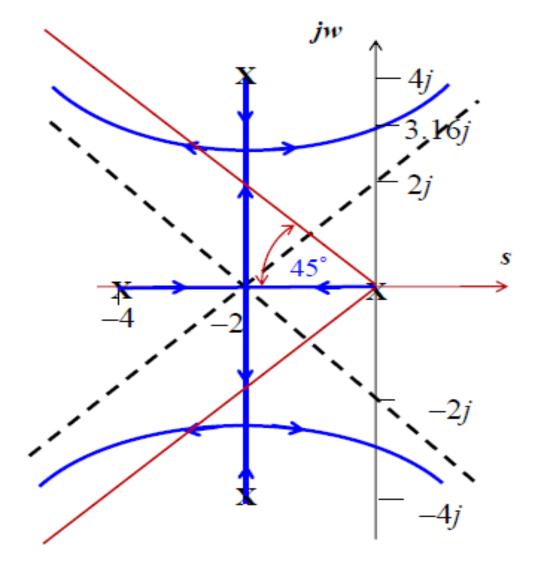
$$K = \frac{|-2 + 2.45j + 4||-2 - 2.45j + 4||-2 + 2.45j + 2 + 4j||-2 - 2.45j + 2 - 4j|}{1}$$

$$K = 3.163 \cdot 3.163 \cdot 6.45 \cdot 1.55 = 100$$

#### **Analysis – Construction Rules: Example**

• Is there a gain corresponding to a damping ratio of **0.707** or more for all system modes?

$$\zeta = 0.707 = \cos(q)$$
$$q = 45^{\circ}$$



- Examine the responses for the various gains and relate them to the location of the closed loop roots.
  - K = 64, roots are -2, -2,  $-2 \pm 3.46$ j
  - K = 100, roots are -2 + 2.45j, -2 2.45j
  - K = 260, roots are $\pm 3.16j, -4 \pm 3.16j$

