Frame {B} is rotated relative to frame {A} about z-axis by 30 degree and translated 4 units in x-axis and 3 units in y axis. Frame {C} is rotated relative to frame {B} about x-axis by 60 degrees and translated 6 units in x-axis and 5 units in z-axis. Find the position of P relative to frame $\{A\}$ if ${}^{c}P = [8\ 7\ 9]^{T}$

$${}_{B}^{A}T = \begin{bmatrix} 0.866 & -0.5 & 0 & 4 \\ 0.5 & 0.866 & 0 & 3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \qquad {}_{C}^{B}T = \begin{bmatrix} 1 & 0 & 0 & 6 \\ 0 & 0.5 & -0.866 & 0 \\ 0 & 0.866 & 0.5 & 5 \\ 0 & 0 & 0 & 1 \end{bmatrix} \qquad {}_{C}P = \begin{bmatrix} 8 \\ 7 \\ 9 \\ 1 \end{bmatrix}$$

$$E_C^BT = \begin{bmatrix} 1 & 0 & 0 & 6 \\ 0 & 0.5 & -0.866 & 0 \\ 0 & 0.866 & 0.5 & 5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$P = \begin{bmatrix} 8 \\ 7 \\ 9 \\ 1 \end{bmatrix}$$

$${}^{A}_{C}T = \begin{bmatrix} 0.866 & -0.25 & 0.433 & 9.196 \\ 0.5 & 0.433 & -0.75 & 6 \\ 0 & 0.866 & 0.5 & 5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^{A}P = {}^{A}_{B}T_{C}^{B}T^{C}P$$

$${}^{A}_{C}T = {}^{A}_{B}T_{C}^{B}T$$

$${}_C^A T = {}_B^A T_C^B T$$

8
7
9
1)
$$\frac{1}{\sqrt{3}}$$
 $\frac{1}{\sqrt{3}}$ $\frac{1}$

$$^{\mathsf{A}P} = \begin{bmatrix} 18.24 \\ 6.28 \\ 15.56 \\ 1 \end{bmatrix}$$

Transformation Arithmetic

$${}_{A}^{B}T = \begin{bmatrix} {}_{B}^{A}R^{T} & {}_{-B}^{A}R^{TA}P_{BORG} \\ \hline 0 & 0 & 0 & 1 \end{bmatrix}$$

according to this theorem to invert the transformation matrix from aRb to bRa we need to take transpose of the orientation part and for the translation - (aRb ^T aPb_org)

Inverting Transform (Proof)

To find ${}^B_A T$, we must compute ${}^B_A R$ and ${}^B_A P_{AORG}$ from ${}^A_B R$ and ${}^A_B P_{BORG}$. First, recall from our discussion of rotation matrices that

$${}_A^B R = {}_A^A R^T. (2.42)$$

Next, we change the description of ${}^AP_{BORG}$ into $\{B\}$ by using (2.13):

$${}^{B}({}^{A}P_{BORG}) = {}^{B}_{A}R {}^{A}P_{BORG} + {}^{B}P_{AORG}.$$
 (2.43)

The left-hand side of (2.43) must be zero, so we have

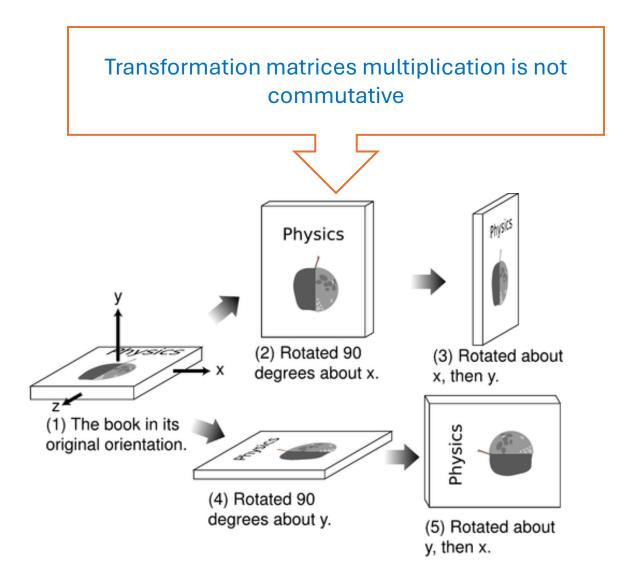
$${}^{B}P_{AORG} = -{}^{B}_{A}R {}^{A}P_{BORG} = -{}^{A}_{R}R^{TA}P_{BORG}.$$
 (2.44)

Using (2.42) and (2.44), we can write the form of ${}_{A}^{B}T$ as

$${}_{A}^{B}T = \left[\begin{array}{c|c} {}_{B}^{A}R^{T} & -{}_{B}^{A}R^{TA}P_{BORG} \\ \hline 0 & 0 & 1 \end{array} \right]. \tag{2.45}$$

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Transformation Arithmetic



EXAMPLE 2.7

Consider two rotations, one about \hat{Z} by 30 degrees and one about \hat{X} by 30 degrees:

$$R_{z}(30) = \begin{bmatrix} 0.866 & -0.500 & 0.000 \\ 0.500 & 0.866 & 0.000 \\ 0.000 & 0.000 & 1.000 \end{bmatrix}$$

$$R_{x}(30) = \begin{bmatrix} 1.000 & 0.000 & 0.000 \\ 0.000 & 0.866 & -0.500 \\ 0.000 & 0.500 & 0.866 \end{bmatrix}$$

$$R_{z}(30)R_{x}(30) = \begin{bmatrix} 0.87 & -0.43 & 0.25 \\ 0.50 & 0.75 & -0.43 \\ 0.00 & 0.50 & 0.87 \end{bmatrix}$$

$$\neq R_{x}(30)R_{z}(30) = \begin{bmatrix} 0.87 & -0.50 & 0.00 \\ 0.43 & 0.75 & -0.50 \\ 0.25 & 0.43 & 0.87 \end{bmatrix}$$

$$(2.61)$$

Transform Equations

$$_{D}^{U}T={}_{A}^{U}T{}_{D}^{A}T;$$

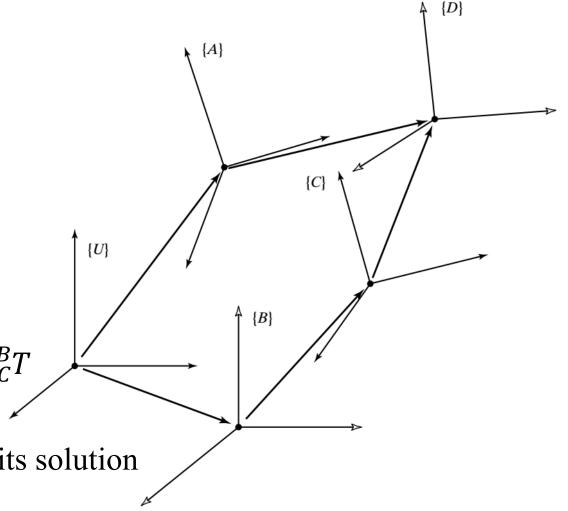
$$_{D}^{U}T = _{B}^{U}T _{C}^{B}T _{D}^{C}T.$$

$${}_A^U T {}_D^A T = {}_B^U T {}_C^B T {}_D^C T.$$

Consider that all transforms are known except B_CT Here, we have one transform equation and one unknown transform; hence, we easily find its solution to be

$$_{C}^{B}T = _{B}^{U}T^{-1} _{A}^{U}T _{D}^{A}T _{D}^{C}T^{-1}$$

inverting theorem would be used to find these inverses



Transform Equations

if we want to calculate UT_A we choose 2 paths to an unknown point (like UT_C preferably, as we

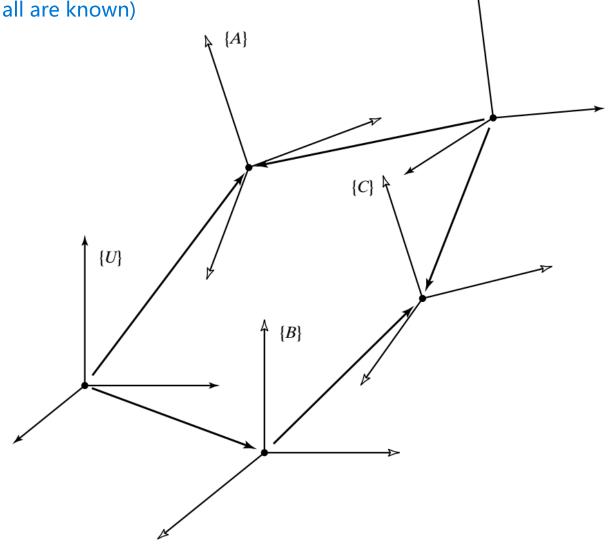
don't know its position so it could be cancelled out or known if all are known)

and apply equations of the path

$$_{C}^{U}T = _{A}^{U}T \,_{A}^{D}T^{-1} \,_{C}^{D}T$$

$$_{C}^{U}T = _{B}^{U}T _{C}^{B}T.$$

$${}_A^U T = {}_B^U T {}_C^B T {}_C^D T^{-1} {}_A^D T.$$



 $\{D\}$

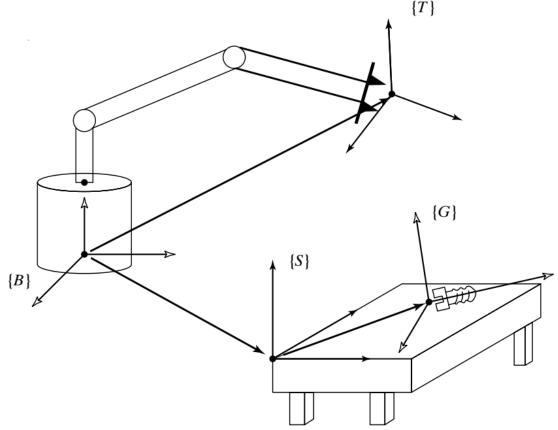
Example

Assume that we know the transform $_T^BT$ in Fig. 2.16, which describes the frame at the manipulator's fingertips $\{T\}$ relative to the base of the manipulator, $\{B\}$, that we know where the tabletop is located in space relative to the manipulator's base (because we have a description of the frame $\{S\}$ that is attached to the table as shown, $_S^BT$), and that we know the location of the frame attached to the bolt lying on the table relative to the table frame—that is, $_G^ST$. Calculate the position and orientation of the bolt relative to the manipulator's hand, $_G^TT$.

$${}_{G}^{B}T = {}_{S}^{B}T {}_{G}^{S}T \qquad {}_{G}^{B}T = {}_{T}^{B}T {}_{G}^{T}T$$

Equating above two to get the bolt frame Relative to the tool frame

$$_{G}^{T}T = _{T}^{B}T^{-1} _{S}^{B}T _{G}^{S}T.$$



More on Representation of Orientation

- Orientation is by giving a 3 × 3 rotation matrix.
- Rotation matrices are special in that all columns are mutually orthogonal and have unit magnitude
- Determinant of Rotation matrices is always equal to +1 (Proper Orthonormal)

Cayley's formula for orthonormal matrices

For any proper orthonormal matrix R, there exists a skew-symmetric matrix S such that

$$R = (I_3 - S)^{-1}(I_3 + S) \qquad S = \begin{bmatrix} 0 & -s_z & s_y \\ s_z & 0 & -s_x \\ -s_y & s_x & 0 \end{bmatrix}.$$

More on Representation of Orientation

- Therefore any 3 × 3 rotation matrix can be specified by just three parameters
- This means there are six constraints on the nine elements of a rotation matrix
- A human operator at a computer terminal who wishes to type in the specification of the desired orientation of a robot's hand would have a hard time inputting a nine-element matrix with orthonormal columns
- A representation that requires only three numbers would be simpler

$$|\hat{X}| = 1,$$

$$|\hat{Y}| = 1$$
,

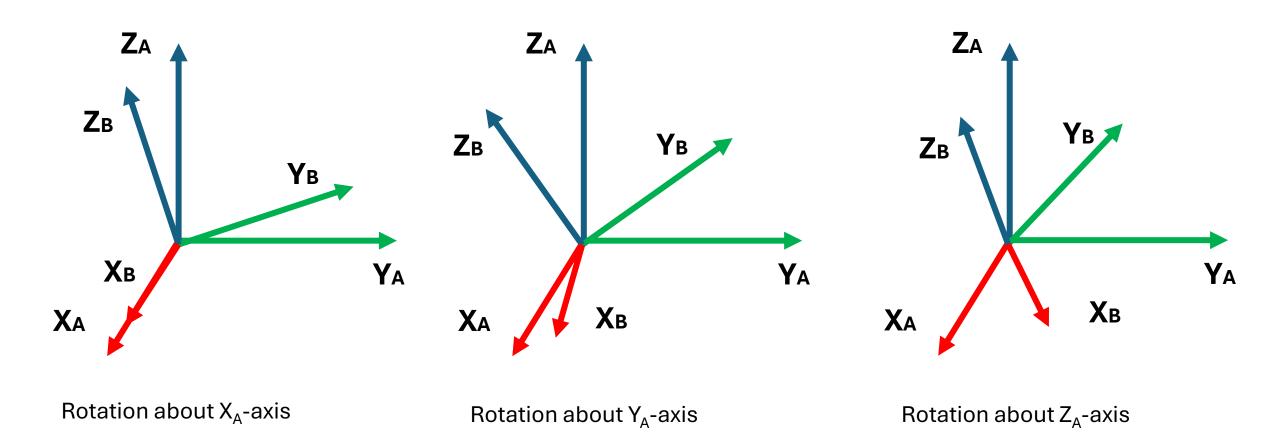
$$|\hat{Z}| = 1$$
,

$$\hat{X} \cdot \hat{Y} = 0,$$

$$\hat{X} \cdot \hat{Z} = 0,$$

$$\hat{Y} \cdot \hat{Z} = 0.$$

Start with the frame coincident with a known reference frame $\{A\}$. Rotate $\{B\}$ first about \hat{X}_A by an angle γ , then about \hat{Y}_A by an angle β , and, finally, about \hat{Z}_A by an angle α .



Start with the frame coincident with a known reference frame $\{A\}$. Rotate $\{B\}$ first about \hat{X}_A by an angle γ , then about \hat{Y}_A by an angle β , and, finally, about \hat{Z}_A by an angle α .

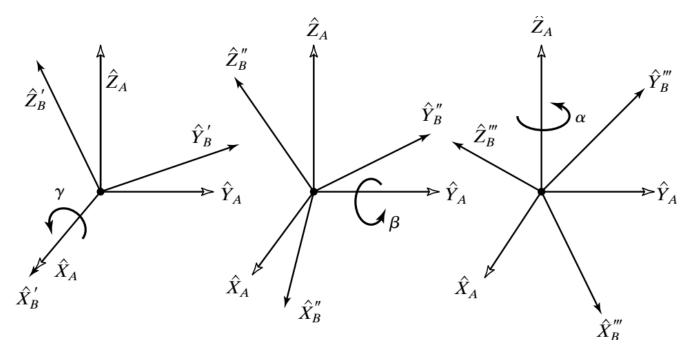


FIGURE 2.17: X-Y-Z fixed angles. Rotations are performed in the order $R_X(\gamma)$, $R_Y(\beta)$, $R_Z(\alpha)$.

X-Y-Z Fixed Angles
$${}_{2^{\text{nd}}}^{A} R_{XYZ}(\gamma, \beta, \alpha) = R_{Z}(\alpha) R_{Y}(\beta) R_{X}(\gamma)$$

$$= \begin{bmatrix} c\alpha & -s\alpha & 0 \\ s\alpha & c\alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c\beta & 0 & s\beta \\ 0 & 1 & 0 \\ -s\beta & 0 & c\beta \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\gamma & -s\gamma \\ 0 & s\gamma & c\gamma \end{bmatrix}$$

$${}_{B}^{A}R_{XYZ}(\gamma,\beta,\alpha) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

The inverse problem, that of extracting equivalent X–Y–Z fixed angles from a rotation matrix, is often of interest

$${}_{B}^{A}R_{XYZ}(\gamma,\beta,\alpha) = \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ r_{31} & r_{32} & r_{33} \end{bmatrix}$$

$${}^{A}_{B}R_{XYZ}(\gamma,\beta,\alpha) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

$$\beta = \text{Atan2}(-r_{31}, \sqrt{r_{11}^2 + r_{21}^2}),$$

$$\alpha = \text{Atan2}(r_{21}/c\beta, r_{11}/c\beta),$$

$$\gamma = \text{Atan2}(r_{32}/c\beta, r_{33}/c\beta),$$

Although a second solution exists, by using the positive square root in the formula for β , we always compute the single solution for which $-90.0^{\circ} \le \beta \le 90.0^{\circ}$.

If $\beta = 90.0^{\circ}$, then a solution can be calculated to be

$$\beta = 90.0^{\circ},$$
 $\alpha = 0.0,$
 $\gamma = \text{Atan2}(r_{12}, r_{22}).$

If $\beta = -90.0^{\circ}$, then a solution can be calculated to be

$$\beta = -90.0^{\circ},$$
 $\alpha = 0.0,$
 $\gamma = -\text{Atan2}(r_{12}, r_{22}).$

 3 Atan2(y, x) computes tan⁻¹($\frac{y}{x}$) but uses the signs of both x and y to identify the quadrant in which the resulting angle lies. For example, Atan 2(-2.0, -2.0) = -135°, whereas Atan 2(2.0, 2.0) = 45°, a distinction which would be lost with a single-argument arc tangent function. We are frequently computing angles that can range over a full 360°, so we will make use of the Atan2 function regularly. Note that Atan2 becomes undefined when both arguments are zero. It is sometimes called a "4-quadrant arc tangent," and some programming-language libraries have it predefined.

Frame {B} was initially coincident with {A}. We then rotated {B} about Z_A -axis by 60. Then we rotated about Y_A -axis by 45 and finally we rotated it about X_A -axis by 30. Calculate the resultant rotation matrix.

$$R_{X}(30) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & C30 & -S30 \\ 0 & S30 & C30 \end{bmatrix}$$

$$\begin{bmatrix} C45 & 0 & S45 \end{bmatrix}$$

$$\begin{bmatrix} C45 & 0 & S45 \end{bmatrix}$$

$$\begin{bmatrix} 0.35 & -0.61 & 0.71 \end{bmatrix}$$

$$R_{Y}(45) = \begin{bmatrix} C45 & 0 & S45 \\ 0 & 1 & 0 \\ -S45 & 0 & C45 \end{bmatrix}$$

$$R_{Z}(60) = \begin{bmatrix} C60 & -S60 & 0\\ S60 & C60 & 0\\ 0 & 0 & 1 \end{bmatrix}$$

$$R_{B}^{A}R_{ZYX}(60,45,30) = R_{X}(30).R_{Y}(45).R_{Z}(60) =$$

$$R_{Y}(45) = \begin{bmatrix} C45 & 0 & S45 \\ 0 & 1 & 0 \\ -S45 & 0 & C45 \end{bmatrix} \begin{bmatrix} 0.35 & -0.61 & 0.71 \\ 0.93 & 0.13 & -0.35 \\ 0.13 & 0.78 & 0.61 \end{bmatrix}$$

Find the Fixed angles of rotation (γ , β , α) for the following XYZ rotation matrix.

$${}_{B}^{A}R = \begin{bmatrix} 0.9077 & -0.2946 & 0.2989 \\ 0.3304 & 0.9408 & -0.0760 \\ -0.2588 & 0.1677 & 0.9513 \end{bmatrix}$$

$$\beta = \text{Atan2}(-r_{31}, \sqrt{r_{11}^2 + r_{21}^2}),$$
 $\alpha = \text{Atan2}(r_{21}/c\beta, r_{11}/c\beta),$
 $\gamma = \text{Atan2}(r_{32}/c\beta, r_{33}/c\beta),$
 $\beta = 15^{\circ}$
 $\gamma = 20^{\circ}$
 $\gamma = 10^{\circ}$

Z-Y-X Euler Angles

Start with the frame coincident with a known frame $\{A\}$. Rotate $\{B\}$ first about \hat{Z}_B by an angle α , then about \hat{Y}_B by an angle β , and, finally, about \hat{X}_B by an angle γ .

• In this representation, each rotation performed about an axis of the moving system {B} rather than one of the fixed reference {A}

 \hat{Z}_{A} \hat{Z}_{B} \hat{Z}_{B} \hat{Z}_{B} \hat{Z}_{B} \hat{Y}_{B} \hat{Y}_{B} \hat{Y}_{B} \hat{Y}_{B} \hat{Y}_{B} \hat{Y}_{B} \hat{X}_{B} \hat{X}_{B} \hat{X}_{B} \hat{X}_{B} \hat{X}_{B} \hat{X}_{B}

Such sets of three rotations are calle
 Euler Angles

Z-Y-X Euler Angles

$$\begin{array}{l}
{}^{A}_{B}R_{Z'Y'X'} = R_{Z}(\alpha)R_{Y}(\beta)R_{X}(\gamma) \\
= \begin{bmatrix}
c\alpha & -s\alpha & 0 \\
s\alpha & c\alpha & 0 \\
0 & 0 & 1
\end{bmatrix}
\begin{bmatrix}
c\beta & 0 & s\beta \\
0 & 1 & 0 \\
-s\beta & 0 & c\beta
\end{bmatrix}
\begin{bmatrix}
1 & 0 & 0 \\
0 & c\gamma & -s\gamma \\
0 & s\gamma & c\gamma
\end{bmatrix}$$

$${}^{A}_{B}R_{Z'Y'X'}(\alpha,\beta,\gamma) = \begin{bmatrix} c\alpha c\beta & c\alpha s\beta s\gamma - s\alpha c\gamma & c\alpha s\beta c\gamma + s\alpha s\gamma \\ s\alpha c\beta & s\alpha s\beta s\gamma + c\alpha c\gamma & s\alpha s\beta c\gamma - c\alpha s\gamma \\ -s\beta & c\beta s\gamma & c\beta c\gamma \end{bmatrix}$$

Relations for finding Z-Y-X Euler angles from a given rotation matrix are exactly same as the X-Y-Z Fixed Angles (as the rotation matrix is same)

Z–Y–Z Euler angles

Start with the frame coincident with a known frame $\{A\}$. Rotate $\{B\}$ first about \hat{Z}_B by an angle α , then about \hat{Y}_B by an angle β , and, finally, about Z_b by an angle γ .

$${}^{A}_{B}R_{Z'Y'Z'}(\alpha,\beta,\gamma) = \begin{bmatrix} c\alpha c\beta c\gamma - s\alpha s\gamma & -c\alpha c\beta s\gamma - s\alpha c\gamma & c\alpha s\beta \\ s\alpha c\beta c\gamma + c\alpha s\gamma & -s\alpha c\beta s\gamma + c\alpha c\gamma & s\alpha s\beta \\ -s\beta c\gamma & s\beta s\gamma & c\beta \end{bmatrix}$$

if $\sin \beta \neq 0$, it follows that

$$\beta = \text{Atan2}(\sqrt{r_{31}^2 + r_{32}^2}, r_{33}),$$

$$\alpha = \text{Atan2}(r_{23}/s\beta, r_{13}/s\beta),$$

$$\gamma = \text{Atan2}(r_{32}/s\beta, -r_{31}/s\beta).$$

Z-Y-Z Euler angles

If $\beta = 0.0$, then a solution can be calculated to be

$$\beta = 0.0,$$
 $\alpha = 0.0,$
 $\gamma = \text{Atan2}(-r_{12}, r_{11}).$

If $\beta = 180.0^{\circ}$, then a solution can be calculated to be

$$\beta = 180.0^{\circ},$$
 $\alpha = 0.0,$
 $\gamma = \text{Atan2}(r_{12}, -r_{11}).$