With the switch open, each pair of  $3.00 \,\mu\text{F}$  and  $6.00 \,\mu\text{F}$  capacitors are in series with each other and each pair is in parallel with the other pair. When the switch is closed, each pair of  $3.00 \,\mu\text{F}$  and  $6.00 \,\mu\text{F}$  capacitors are in parallel with each other and the two pairs are in series.

(a) With the switch open 
$$C_{\text{eq}} = \left( \left( \frac{1}{3 \,\mu\text{F}} + \frac{1}{6 \,\mu\text{F}} \right)^{-1} + \left( \frac{1}{3 \,\mu\text{F}} + \frac{1}{6 \,\mu\text{F}} \right)^{-1} \right) = 4.00 \,\mu\text{F}.$$

 $Q_{\rm total} = C_{\rm eq}V = (4.00~\mu{\rm F})(210~{\rm V}) = 8.40\times10^{-4}~{\rm C}$ . By symmetry, each capacitor carries  $4.20\times10^{-4}~{\rm C}$ . The voltages are then calculated via V = Q/C. This gives  $V_{ad} = Q/C_3 = 140~{\rm V}$  and  $V_{ac} = Q/C_6 = 70~{\rm V}$ .  $V_{cd} = V_{ad} - V_{ac} = 70~{\rm V}$ .

(b) When the switch is closed, the points c and d must be at the same potential, so the equivalent

capacitance is 
$$C_{\text{eq}} = \left(\frac{1}{(3.00 + 6.00) \,\mu\text{F}} + \frac{1}{(3.00 + 6.00) \,\mu\text{F}}\right)^{-1} = 4.5 \,\mu\text{F}.$$

 $Q_{\text{total}} = C_{\text{eq}}V = (4.50 \ \mu\text{F})(210 \ \text{V}) = 9.5 \times 10^{-4} \ \text{C}$ , and each capacitor has the same potential difference of 105 V (again, by symmetry).

(c) The only way for the sum of the positive charge on one plate of  $C_2$  and the negative charge on one plate of  $C_1$  to change is for charge to flow through the switch. That is, the quantity of charge that flows through the switch is equal to the change in  $Q_2 - Q_1$ . With the switch open,  $Q_1 = Q_2$  and  $Q_2 - Q_1 = 0$ . After the switch is closed,  $Q_2 - Q_1 = 315 \,\mu\text{C}$ , so  $315 \,\mu\text{C}$  of charge flowed through the switch.

24.66.

(a) 
$$C = \left(\frac{1}{C_1} + \frac{1}{C_1}\right)^{-1} = \frac{1}{2}C_1 = \frac{1}{2}\frac{e_0 A}{(d-a)/2} = \frac{e_0 A}{d-a}$$

**(b)** 
$$C = \frac{e_0 A}{d - a} = \frac{e_0 A}{d} \frac{d}{d - a} = C_0 \frac{d}{d - a}$$

(c) As  $a \to 0$ ,  $C \to C_0$ . The metal slab has no effect if it is very thin. And as  $a \to d$ ,  $C \to \infty$ . V = Q/C. V = Ey is the potential difference between two points separated by a distance y parallel to a uniform electric field. When the distance is very small, it takes a very large field and hence a large Q on the plates for a given potential difference. Since Q = CV this corresponds to a very large C.

a) The electric field must be in the outward (+r) direction. To find it, integrate over a Gaussian cylinder of radius r and length L:

$$\begin{split} & \iint \vec{E} \cdot d\vec{A} = 2 \pi r L E_r = \frac{\lambda L}{\epsilon_0}; \\ & E_r = \frac{\lambda}{2 \pi \epsilon_0 r} = \left| \vec{E} \right|. \end{split}$$

The energy density is

$$u = \frac{\epsilon_0}{2} |\vec{E}|^2 = \frac{\epsilon_0}{2} \left(\frac{\lambda}{2 \pi \epsilon_0 r}\right)^2 = \frac{\lambda^2}{8 \pi^2 \epsilon_0 r^2}.$$

b)

$$\frac{U}{L} = \frac{\lambda^2}{4\pi\epsilon_0} \ln \frac{r_b}{r_a}.$$

c) From Example 24.4,

$$\frac{C}{L} = \frac{2\pi\epsilon_0}{\ln(r_b/r_a)}$$
 (for a cylindrical capacitor).

From Eq. 24.9,

$$U = \frac{Q^2}{2C} = \frac{(\lambda L)^2}{2C},$$

 $\mathbf{SC}$ 

$$\frac{U}{L} = \frac{\lambda^2 L}{2 C} = \frac{\lambda^2}{2 C/L} = \frac{\lambda^2}{2 \left[2 \pi \epsilon_0 / \ln \left(r_b / r_a\right)\right]} = \frac{\lambda^2}{4 \pi \epsilon_0} \ln \frac{r_b}{r_a},$$

which agrees with part (b).

74.

a) We can view this as two capacitors connected in parallel, the first with dielectric K and plate height h, and the second with dielectric 1 and plate height L-h. Both have the same plate width w and separation between plates, which I'm calling d. Then  $C_1 = K \epsilon_0 \frac{wh}{d}$ ,  $C_2 = \epsilon_0 \frac{w(L-h)}{d}$ , and the total capacitance is

$$C = C_1 + C_2 = (Kh + L - h) \epsilon_0 \frac{w}{d} = \left[ (K - 1) \frac{h}{L} + 1 \right] \epsilon_0 \frac{wL}{d}.$$

If there were a single uniform dielectric constant K' in this capacitor, the capacitance would be  $C' = K' \epsilon_0 \frac{w^L}{d}$ . Therefore it makes sense to say the effective dielectric constant is  $K_{\text{eff}} = (K-1)\frac{h}{L} + 1$  so that  $C = K_{\text{eff}} \epsilon_0 \frac{w^L}{d}$ . (This is the same result you get by assuming  $K_{\text{eff}}$  is a weighted average of K and 1, weighted by the fraction of the plates touching fuel and air, respectively.)

b) 
$$^{1}\!/_{4}$$
 full:  $K_{\text{eff}} = (1.95 - 1) \frac{1}{4} + 1 = 1.24$ 

$$\frac{1}{2}$$
 full:  $K_{\text{eff}} = (1.95 - 1) \frac{1}{2} + 1 = 1.48$ 

$$^{3}/_{4}$$
 full:  $K_{\text{eff}} = (1.95 - 1) \frac{3}{4} + 1 = 1.71$ 

c) 
$$^{1}\!/_{4}$$
 full:  $K_{\text{eff}} = (33.0 - 1) \frac{1}{4} + 1 = 9.00$ 

$$\frac{1}{2}$$
 full:  $K_{\text{eff}} = (33.0 - 1)\frac{1}{2} + 1 = 17.0$ 

$$^{3}/_{4}$$
 full:  $K_{\text{eff}} = (33.0 - 1)\frac{3}{4} + 1 = 25.0$ 

d) It is more practical using methanol because there will be a greater (and easier to detect) change in capacitance as the tank is emptied.