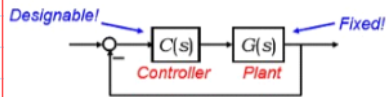


L14 Lead-lag Compensator Design

Saturday, June 19, 2021 4:29 PM

Controller Design

- Place closed-loop poles at desired locations by tuning $C(s) = K$



- If RL does not pass through desired location, reshape RL

→ Add poles/zeros to $C(s)$

- Adding Poles

→ pulls RL Right

→ ↓ Stable

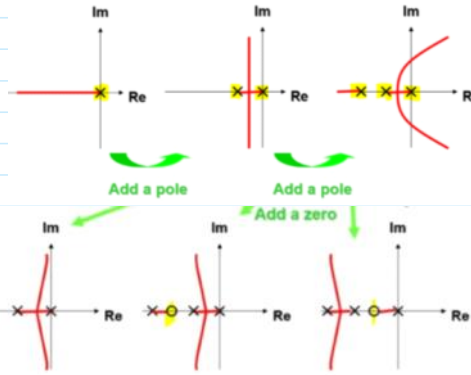
→ slower settle time T_s

- Adding Zeros

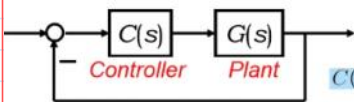
→ pulls RL Left

→ ↑ Stable

→ faster settle time T_s

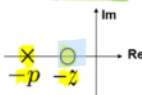


Lead Lag Compensators

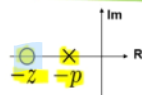


$$C(s) = K \frac{s+z}{s+p}, \quad (z > 0, p > 0)$$

• Lead compensator



• Lag compensator

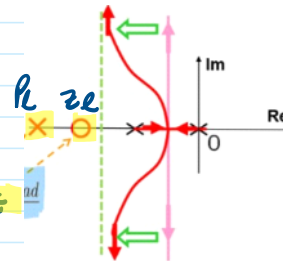


Reshaping RL of Lead Compensator

- Move centroid/Asymptote Intersection left

→ Plant: $\sum \text{pole} - \sum \text{zero}$

→ Plant & lead: $\sum \text{pole} - \sum \text{zero} + \text{pole lead} - \text{zero lead}$



- Improves transient response

- Improves stability

$$C_{\text{lead}}(s) = K \frac{s + z_{\text{lead}}}{s + p_{\text{lead}}}$$

Design

- 1 Select pole in allowable region (s_d)

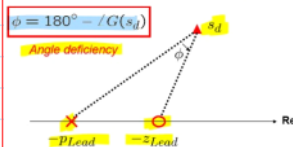
Reshape RL to pass through s_d

- 2 Select pole/zero in $C_{\text{lead}}(s) \rightarrow \phi = 180^\circ - \angle G(s_d)$

For OLTF:

- Angle condition: $\angle L(s) = 180^\circ (2k+1), k=0, \pm 1, \pm 2, \dots$

- Magnitude condition: $K = \frac{1}{|L(s)|}$



- Find ϕ

- 1 $s_d = -\zeta \omega_n + j \omega_n \sqrt{1 - \zeta^2}$

- 2 $G(s_d)$

- 3 $\angle G^*(s_d)$

- 4 $\angle G^*(s_d)$ convert to +Re-axis angle $\angle G(s_d) \rightarrow \angle G(s_d) = 360^\circ - \angle G^*(s_d)$

- 5 $\phi = 180^\circ - \angle G(s_d) \rightarrow$ can get $\angle G(s_d)$ directly if use angle on HP

ex. $s_d = -2 + 2\sqrt{3}j, G(s) = \frac{4}{(-2 + 2\sqrt{3}j)2\sqrt{3}j}$

$$\angle G^*(s_d) = \angle 4 - \angle(-2 + 2\sqrt{3}j) - \angle 2\sqrt{3}j = 0 - (\tan^{-1}(\frac{2\sqrt{3}}{-2})) - 90^\circ = -240^\circ$$

$$\angle G(s_d) = 360^\circ - 240^\circ = 120^\circ$$

$$\phi = 180^\circ - \angle G(s_d) = 60^\circ$$

- Find K

- 1 $\beta_{\text{lead}} = |Re\{s_d\}|$

- 2 Find p_{lead} using $\phi = \angle \frac{s_d + \beta_{\text{lead}}}{s_d + p_{\text{lead}}}$

Evaluate $G(s)$ at the desired pole.

$$s_d = -\zeta \omega_n + j \omega_n \sqrt{1 - \zeta^2}$$

$$s_d = -2 + 2\sqrt{3}j$$

$$G(s_d) = \frac{4}{(-2 + 2\sqrt{3}j)2\sqrt{3}j}$$

$$\angle G^*(s_d) = \angle 4 - \angle(-2 + 2\sqrt{3}j) - \angle 2\sqrt{3}j$$

Desired pole

Im

★ Use Rad Mode!
to solve Angles!!

- Find K

- ① $\bar{z}_{lead} = |Re\{s_d\}|$
- ② Find P_{lead} using $\phi = \angle \frac{s_d + \bar{z}_{lead}}{s_d + P_{lead}}$
- ③ $C_{lead} = K \frac{s + P_{lead}}{s + \bar{z}_{lead}}$
- ④ $K = |L(s_d)| \rightarrow L(s) = C(s)G(s)$

- Error Const

Step Error: $K_p = \lim_{s \rightarrow 0} G(s)C(s)$
 Ramp Error: $K_v = \lim_{s \rightarrow 0} sG(s)C(s)$

Reshaping RL w/ lag compensator

- Move centroid / Asymptote intersection right

→ Plant: $\frac{\sum pole - \sum zero}{s}$

→ Plant & Lag: $\frac{\sum pole - \sum zero + pole_{lag} - zero_{lag}}{s}$

- Reduce Steady state Error

$C_{lag}(s) = \frac{s + \bar{z}_{lag}}{s + P_{lag}}$

Design

→ Select pole in allowable region (s_d)

→ Reshape RL to pass through s_d

- want small $\phi_{lag} \rightarrow$ given

$$K_v = \lim_{s \rightarrow 0} sG(s)C_{lead}(s)C_{lag}(s) = 2.89 \times \frac{z_{Lag}}{P_{Lag}} \xrightarrow{K_v > 20} 2.89 \times \frac{z_{Lag}}{P_{Lag}} > 20 \Rightarrow \frac{z_{Lag}}{P_{Lag}} > 6.92$$

→ $z_{Lag} > 6.92 P_{Lag}$

→ $C_{lag}(s_d) \approx 1$

→ $\angle G(s_d)C_{lead}(s_d)C_{lag}(s_d) \approx 180^\circ$

Lag-Lag compensator

- Takes into account transient & Steady state

$C_{ll}(s) = K \frac{s + \bar{z}_{lead}}{s + P_{lead}} \cdot \frac{s + \bar{z}_{lag}}{s + P_{lag}}$

Steady State Error

- Step $r(t)$: $K_p = \lim_{s \rightarrow 0} L(s) = \infty \rightarrow e_{ss} = \frac{R}{1 + K_p} = 0$
- Ramp $r(t)$: $K_v = \lim_{s \rightarrow 0} sL(s) = \frac{3.15K}{0.75} = 4.2K \rightarrow e_{ss} = \frac{R}{K_v} = \frac{R}{4.2K}$
- Parabolic $r(t)$: $K_a = \lim_{s \rightarrow 0} s^2 L(s) = 0 \rightarrow e_{ss} = \frac{R}{K_a} = \infty$

$$G(-2 + 2\sqrt{3}j) = \frac{(-2 + 2\sqrt{3}j)2\sqrt{3}j}{s_d}$$

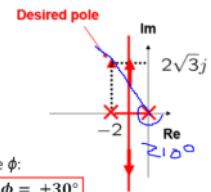
$$\begin{aligned} \angle G^*(s_d) &= \angle 4 - \angle(-2 + 2\sqrt{3}j) - \angle 2\sqrt{3}j \\ &= 0^\circ - \left(\tan^{-1} \left(\frac{2\sqrt{3}}{-2} \right) \right) - 90^\circ \\ &= 0^\circ - (+120^\circ) - 90^\circ = -210^\circ \rightarrow \end{aligned}$$

$$\angle G^*(s_d) = -210^\circ$$

Convert -210° to an angle from +Re-axis:
 $360^\circ - 210^\circ = +150^\circ \rightarrow \angle G(s_d) = +150^\circ$

Now, use the angle deficiency formula to calculate ϕ :

$$\phi = 180^\circ - \angle G(s_d) \rightarrow \phi = 180^\circ - 150^\circ \rightarrow \phi = +30^\circ$$



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