

# Formulas

Wednesday, April 14, 2021 12:15 PM

## Chapter 13:

$$\cos \theta_m = \frac{\omega_{cm}}{\omega} = \frac{f_{cm}}{f} = \frac{\lambda}{\lambda_{cm}} \rightarrow f, \lambda = \text{operating}$$

$$V_{gm} = \frac{2\omega}{\beta} = \frac{a}{n} \sin \theta_m, \quad V_{pm} = \frac{\omega}{\beta} = \frac{c}{n} \sin \theta_m$$

$$f_{cm} = \frac{m \cdot c}{2nd}$$

$$f = \frac{c}{\lambda}$$

$$d = \frac{n \cdot \lambda}{2}$$

$$f_c \rightarrow d = \frac{\lambda_c}{2}$$

$$\rightarrow \text{lowest freq}$$

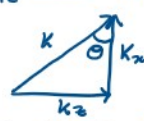
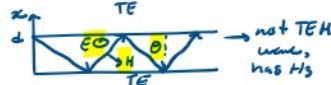
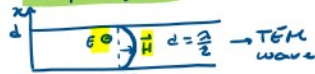
$$@ f = f_c, v_g = 0$$

$$v_{max} = \frac{c}{n}$$

$$\rightarrow TE_1 \text{ mode (1 half cycle)}$$

$$\rightarrow TM_2 \text{ mode (2 half cycles)}$$

TE-polarized:



$$k = k_x = k_z = \frac{2\pi}{\lambda}$$

$$k_z = \frac{2\pi}{\lambda_c} \quad k_x = \beta = \frac{2\pi}{\lambda_g}$$

$\rightarrow TM \text{ polarized} = TM_0 \text{ mode}$   
 $\rightarrow \text{no } TE_0 \text{ mode}$



Rectangular waveguides:



Brewster's Angle

Angle of Incidence  $\rightarrow$  no reflection of p-polarized light, only s-polarized reflected



$$\theta_B = \tan^{-1} \left( \frac{n_2}{n_1} \right) = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$$

$$\rightarrow n = \sqrt{\epsilon_r}$$

## Chapter 10

2 wire Transmission line (High freq)

$$\lambda = \frac{v}{f} \xrightarrow{\text{air}} = \frac{c}{f}$$



If account for losses in conductor & dielectric

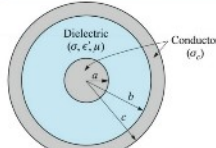
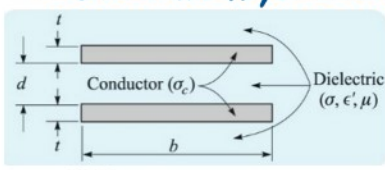
$$\rightarrow \gamma = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$\rightarrow Z_0 = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

TEM = Uniform plane wave

$\rightarrow$  characteristic impedance  $Z_0 = \frac{E}{H} \rightarrow$  depends only on x-sectional, not resistive

$$Z_0 = \sqrt{\frac{\mu}{\epsilon}} \frac{d}{b} = \sqrt{\frac{L}{C}}$$



$$Z_0 = \frac{1}{2\pi\epsilon} \ln \left( \frac{b}{a} \right) = \sqrt{\frac{L}{C}}$$

$$\beta = \frac{V_{max}}{V_{min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$V_L(z) = V_{L0} e^{-j\beta z}$$

$$V_R(z) = V_{R0} e^{j\beta z}$$

$$\beta = \frac{2\pi}{\lambda}$$

Smith Chart

Mapping of Z (impedance) plane onto T (reflection coeff) plane

$$\Gamma_0 = \frac{V_R}{V_L} = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{V_0 - V_L}{V_L + V_0} \rightarrow \text{bilinear transformation}$$

$$T(\Gamma) = T_0 e^{j2\beta z}$$

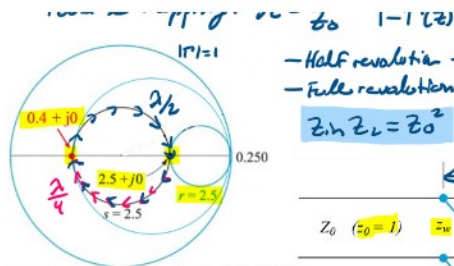
$$T(L) = T_0 e^{-j2\beta L}$$

$$\text{reverse mapping: } Z_L = \frac{Z_0}{1 - \Gamma(L)}$$

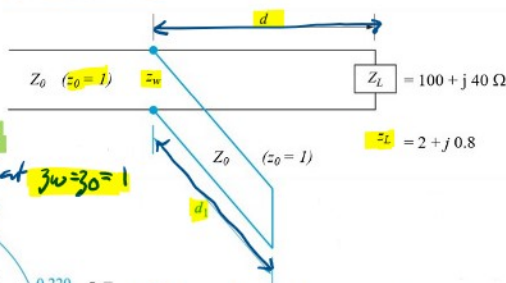


Half revolution  $\rightarrow \lambda/4 \text{ travel (transformer)} \rightarrow Z_{in} = Z_0^2 / Z_L$

Full revolution  $\rightarrow \lambda/2 \text{ travel (transformer)} \rightarrow Z_{in} = Z_L$

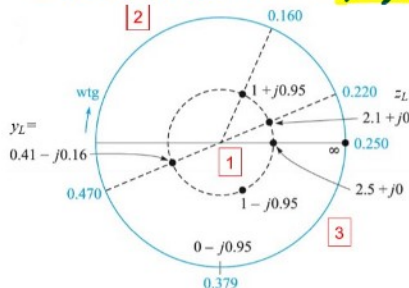


Half revolution  $\rightarrow \lambda/2$  travel (transformer)  $\rightarrow Z_{in} = Z_0^2/Z_L$   
 Full revolution  $\rightarrow \lambda$  travel (transformer)  $\rightarrow Z_{in} = Z_L$   
 $Z_{in} Z_L = Z_0^2$



### Single Shunt Stub Match

Select  $d$  &  $d_1$  such that  $Y_{in} = Y_0 = 1$



1 Convert values  $\rightarrow$  Admittance

$\hookrightarrow$  convert  $Z = r + jx \rightarrow y = g + jb$

2 Find  $d$ : (shortest stub dist. from load)

$\hookrightarrow$  towards generator until  $g = 1 \pm jb$

(2 solutions!)

3 Find  $d_1$ : (stub length)

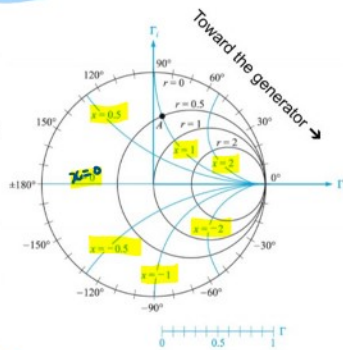
$\hookrightarrow$  find stub length for  $y = 0 \mp jb$

$\hookrightarrow$  cancel  $b$

4 If stub // line  $d, y_{in} = 1$

$\rightarrow$  Finding  $\Gamma_L$ : use  $\lambda$  in bottom scale (RFL coeff,  $\Gamma_L$ )  
 - Read (RFL coeff,  $\Gamma_L$ )

$\rightarrow$  Finding  $\Gamma_L$ : Plot  $Z_L$  from center to normalized  $Z_L \rightarrow Z_L/Z_0$   
 - Read (Angle of RFL coeff in deg)



ladder-line  $Z_0 = \frac{120\pi}{\ln} a \cosh \frac{z}{d} \rightarrow$  separation between wires

### Chapter 12 Plane wave Reflection & Dispersion

#### Boundary Conditions for E-Fields

charge-free:  $D_{n1} = D_{n2}$ ,  $\tan \theta_1 = \frac{E_{t1}}{E_{r1}}$

surface charge:  $(D_{n1} - D_{n2}) \cdot \hat{n} = \rho_s$

$E_{t1} = E_{t2}$

$E_{n1} - E_{n2} = \frac{\rho_s}{\epsilon_0}$

$H_{t1} - H_{t2} = H_0$

$H_{n1} = H_{n2}$

#### Boundary Conditions for H-Fields

current-free:  $H_{t1} = H_{t2}$ ,  $\tan \theta_1 = \frac{H_{r1}}{H_{t1}}$

current sheet:  $(H_{t1} - H_{t2}) \cdot \hat{n} = K$

$B_{n1} = B_{n2}$

$H_{n1} - H_{n2} = K$

$H_{t1} = H_{t2}$

$H_{n1} = H_{n2}$

$\epsilon_1 = \epsilon_2$

$\mu_1 = \mu_2$

$\sigma_1 = \sigma_2$

$\rho_1 = \rho_2$

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Any medium  $\frac{Z''}{Z} = \frac{\sigma}{\omega \epsilon}$

free space

$Z_0 = \sqrt{\frac{\mu_0}{\epsilon_0}}$

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Perfect dielectric (lossless)

$\eta = \sqrt{\frac{\mu}{\epsilon}}$

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Good Dielectric (low loss)

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Good conductor

skin effect

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Partially conducting:  $\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$ ,  $\vec{E} = E_0 e^{-\gamma z} \hat{x}$ ,  $\nabla \times \vec{E} = -j\omega\mu \vec{H}$

$\vec{E}(z,t) = E_0 e^{-\gamma z} e^{j(\omega t - \beta z)} \hat{x}$

$\vec{H}(z,t) = \frac{E_0}{\eta} e^{-\gamma z} e^{j(\omega t - \beta z - \theta)} \hat{y}$

conducting:  $\eta = \sqrt{\frac{j\omega\mu}{\sigma + j\omega\epsilon}}$

Skin Effect

- Conducting medium  $\rightarrow$  good conductor if  $\sigma \gg \omega\epsilon$

Propagation const:  $\gamma = \alpha + j\beta = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$

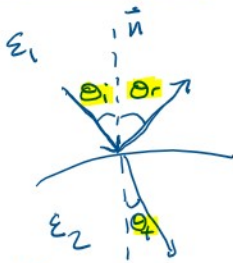
$\alpha = \beta = \sqrt{\frac{\omega\mu\sigma}{2}} = \sqrt{\frac{\pi f \mu \sigma}{2}}$

$\delta = \frac{1}{\alpha} = \sqrt{\frac{2}{\omega\mu\sigma}} = \sqrt{\frac{2}{\pi f \mu \sigma}}$

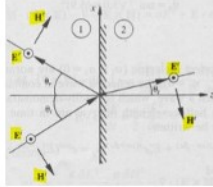


Propagation const:  $\gamma = \alpha + j\beta = \sqrt{j\omega\mu(\sigma + j\omega\epsilon)}$   
 $\alpha = \beta = \frac{\sqrt{\mu\sigma\omega}}{2} = \sqrt{\frac{\mu\sigma\omega}{2}}$   
 $\gamma = \sqrt{\frac{j\omega\mu}{2}} \angle 45^\circ$   
 $\delta = \frac{1}{\sqrt{j\omega\mu}} = \frac{1}{\alpha} = \frac{1}{\beta}$

## Snell's law



Or law of Reflection:  $\theta_i = \theta_r$   
 Or law of Refraction:  $\frac{\sin \theta_i}{\sin \theta_t} = \sqrt{\frac{\mu_2 \epsilon_2}{\mu_1 \epsilon_1}} = \frac{v_1}{v_2}$



Boundary b/w regions

$$\frac{E_{0i}}{E_{0t}} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

$$\frac{E_{0i}}{E_{0r}} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

for normal incidence:  $\theta_i = \theta_t = 0^\circ$

- If  $\mu_1 = \mu_2 \rightarrow$  No Reflected wave @ Brewster Angle

Brewster's Angle  $\theta_B = \tan^{-1} \sqrt{\frac{\epsilon_2}{\epsilon_1}}$

Standing Wave: combination of incident & reflected waves

$$E(z,t) = [E_0 e^{j(\omega t - \beta z)} + E_0' e^{j(\omega t + \beta z)}] \hat{z}$$

## Chapter 11 Plane Waves

### Maxwell's Equations

- w/ time function  $e^{j\omega t}$  & source-free

$$\begin{aligned} \nabla \cdot \vec{E} &= 0 \\ \nabla \cdot \vec{H} &= 0 \\ \nabla \times \vec{E} &= -j\omega \vec{B} = -j\omega \mu \vec{H} \\ \nabla \times \vec{H} &= j\omega \vec{D} = j\omega \epsilon \vec{E} \end{aligned}$$

### Helmholtz Equations

- in lossless medium (perfect dielectric)

$$\vec{E}_z = A e^{-jkz} + B e^{jkz} \quad \text{V/m} \rightarrow k = \omega \sqrt{\mu \epsilon} = \frac{\omega}{v} = \frac{2\pi}{\lambda} = \beta$$

$$\vec{H}_y = \frac{1}{\eta_0} (A e^{-jkz} - B e^{jkz}) \quad \text{A/m}$$

$$\left| \frac{E_0}{H_0} \right| = \eta_0$$

### Poynting Vector

- Power flux Density:  $\vec{S} = \frac{1}{2} \text{Re} \{ \vec{E} \times \vec{H}^* \}$  W/m<sup>2</sup>

$$\rightarrow \text{for } e^{-jkz}: \vec{S} = \frac{A^2}{2\eta_0} \hat{z}$$

$$\rightarrow \text{for } e^{jkz}: \vec{S} = \frac{B^2}{2\eta_0} \hat{z}$$

$$P(t) = \oint_V (\vec{E} \times \vec{H}) \cdot d\vec{s} = \oint_V \vec{S} \cdot d\vec{s}$$

$$\vec{S}_{avg} = \frac{1}{2} \text{Re} (\vec{E} \times \vec{H}^*) \quad \text{avg. (1+1) if } 1-j0$$

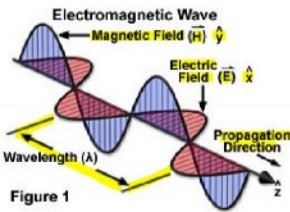


Figure 1

Loss Tangent  $\tan \delta = \frac{\epsilon''}{\epsilon'} = \frac{\sigma}{\omega \epsilon'}$

good conductor:

$$\begin{aligned} \langle S_z \rangle &= \frac{1}{2} \frac{E_{x0}^2}{\eta_1} e^{-2\gamma z} \cos \theta_1 \\ &= \frac{1}{4} \sigma \delta E_{x0}^2 e^{-2\gamma z} \end{aligned}$$

$$P_0 = P_i e^{-2\alpha z}$$

## Chapter 9 Time-varying Fields & Maxwell's Equations

$$\vec{D} = \epsilon_0 \epsilon_r \vec{E}$$

$$\vec{B} = \mu_0 \mu_r \vec{H} = \nabla \times \vec{A} \rightarrow \vec{A} = \oint \frac{\vec{r} \times d\vec{l}}{4\pi r^2}$$

$$\vec{J} = \sigma \vec{E}$$

$$\vec{E} = -\nabla V$$

### Maxwell's Equations

- point-form

$$\nabla \cdot \vec{D} = \rho$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

- Integral form

$$\oint_V \vec{D} \cdot d\vec{s} = \int_V \rho dv$$

$$\oint_V \vec{B} \cdot d\vec{s} = 0$$

$$\oint_V \vec{H} \cdot d\vec{l} = \int_V (\vec{J} + \frac{\partial \vec{D}}{\partial t}) \cdot d\vec{s}$$

$$\oint_V \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \int_V \vec{B} \cdot d\vec{s}$$

- Free Space

$$\nabla \cdot \vec{D} = 0 \rightarrow \nabla \cdot \vec{E} = 0$$

$$\nabla \cdot \vec{B} = 0 \rightarrow \nabla \cdot \vec{H} = 0$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t}$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

- Integral

$$\oint_V \vec{D} \cdot d\vec{s} = 0$$

$$\oint_V \vec{B} \cdot d\vec{s} = 0$$

$$\oint_V \vec{H} \cdot d\vec{l} = \frac{\partial}{\partial t} \int_V \vec{D} \cdot d\vec{s}$$

$$\oint_V \vec{E} \cdot d\vec{l} = -\frac{\partial}{\partial t} \int_V \vec{B} \cdot d\vec{s}$$

### Divergence Theorem

$$\oint_V \vec{D} \cdot d\vec{s} = \int_V (\nabla \cdot \vec{D}) dv = Q_{enc.}$$



### Stokes' Theorem

$$\oint_C \vec{A} \cdot d\vec{l} = \int_S (\nabla \times \vec{A}) \cdot \vec{n} \cdot d\vec{s} = \oint_S \vec{B} \cdot d\vec{s} = \phi$$



### Displacement Current

$$\text{Static fields: } \nabla \times \vec{H} = \vec{J}_c$$

$$\text{time varying fields: } \nabla \cdot \vec{J}_c = -\frac{\partial \rho}{\partial t}$$

$$\nabla \times \vec{H} = \vec{J}_c + \vec{J}_d \rightarrow \vec{J}_d = \frac{\partial \vec{D}}{\partial t}$$

$$\vec{J} = \vec{J}_c + \vec{J}_d = \sigma \vec{E} + j\omega \epsilon \vec{E}$$

$$\left| \frac{\vec{J}_d}{\vec{J}_c} \right| = \frac{\sigma}{\omega \epsilon}$$