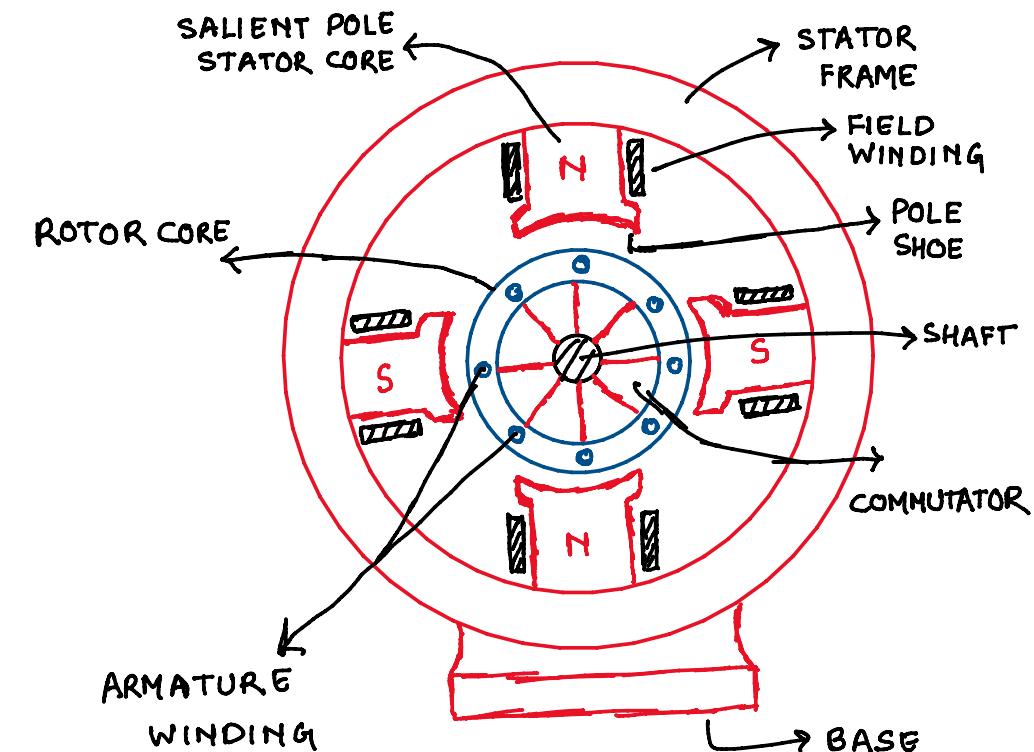


CONSTRUCTION OF DC MACHINES :

- ↳ It has mainly two parts
 - The stationary part is called STATOR.
 - The rotating part is called ROTOR.
 - Apart from these two there is end covers, base, bearing, shaft etc.



STATOR:

- It consists frame of unlaminated ferromagnetic material.
- It has salient pole.
- The pole shoe area of salient pole is larger to increase flux per pole.
- There is concentrated field winding on salient pole.
- Field winding is always DC (direct current) excited.

4-POLE DC MACHINE

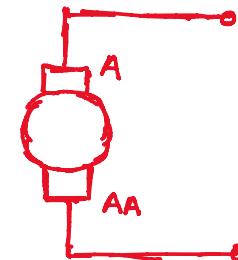
ROTOR:

- Rotor core is made of stacked laminated steel.

RUN.

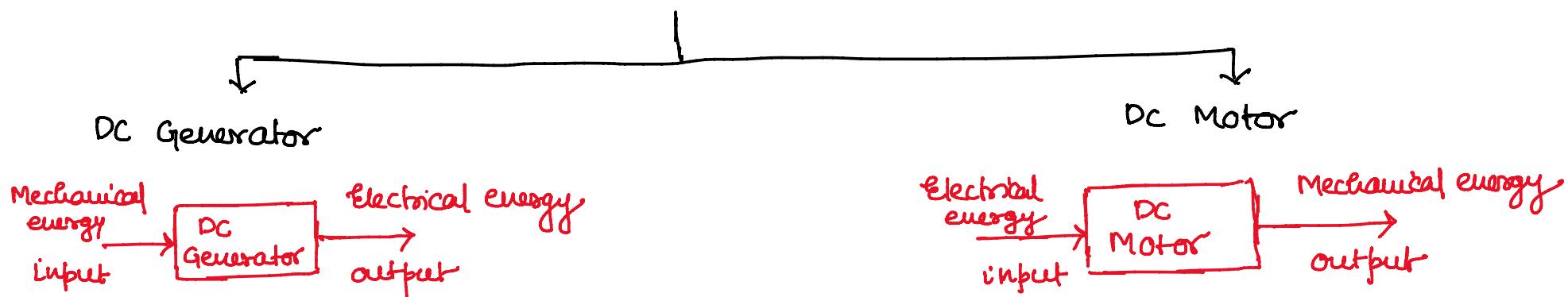
- Rotor core is made of stacked laminated steel.
- There is distributed winding in the rotor core.
- It also has a commutator which is basically a mechanical rectifier which converts AC to DC with help of carbon brushes & vice versa.
- The generated emf in armature winding is AC in nature which is converted to DC across brushes with the help of commutator.

* Schematic diagram of armature is

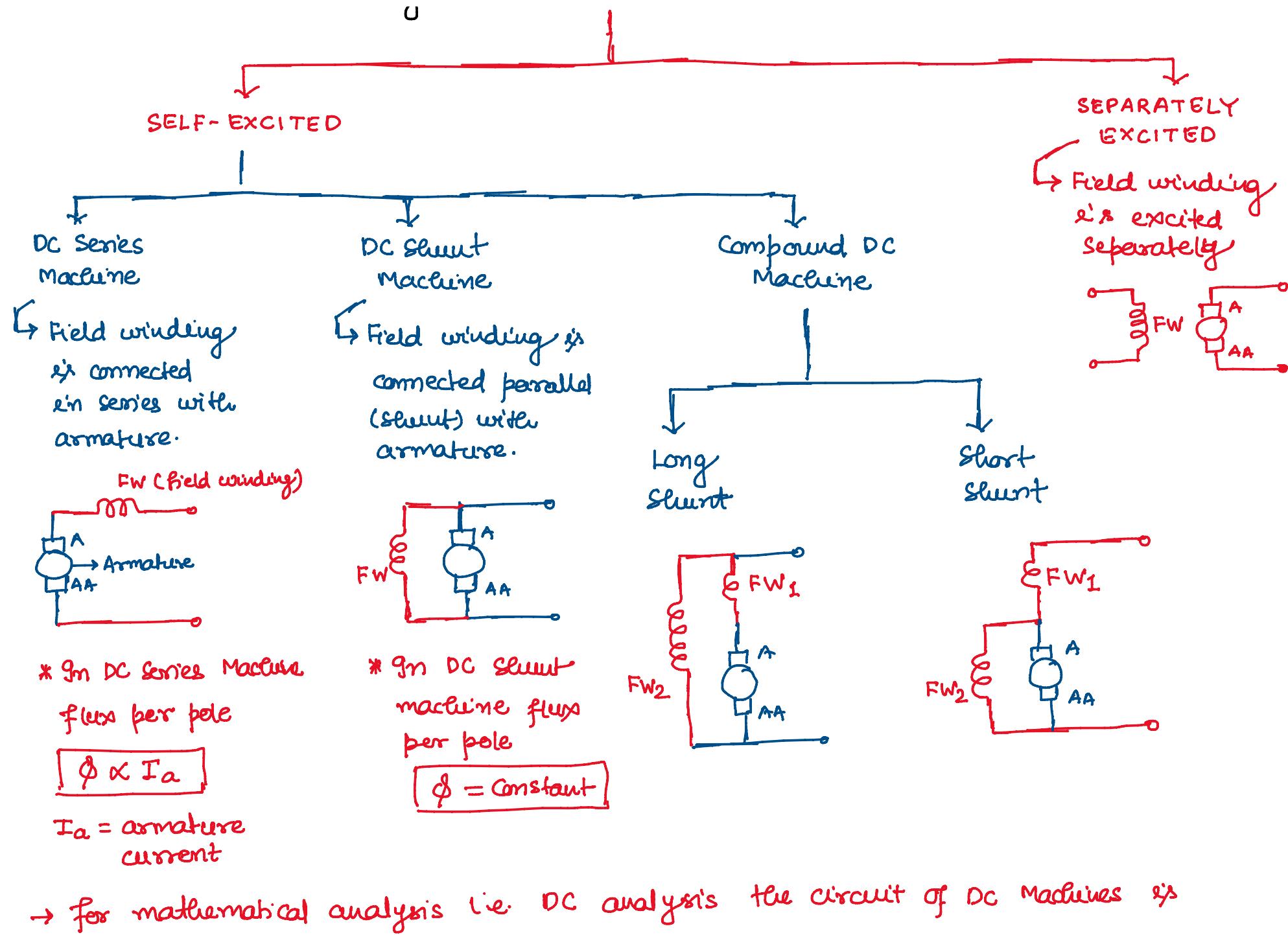


TYPES OF DC MACHINES:

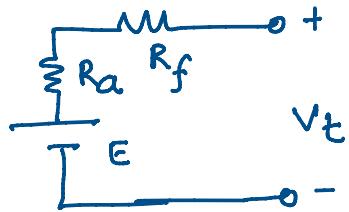
→ Based on Electro mechanical conversion



→ Based on Field winding construction



* DC Series Machine



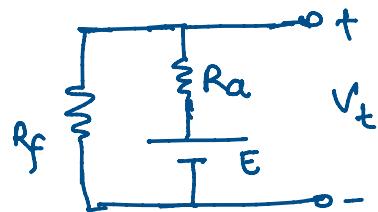
R_f = field winding resistance

R_a = armature winding resistance

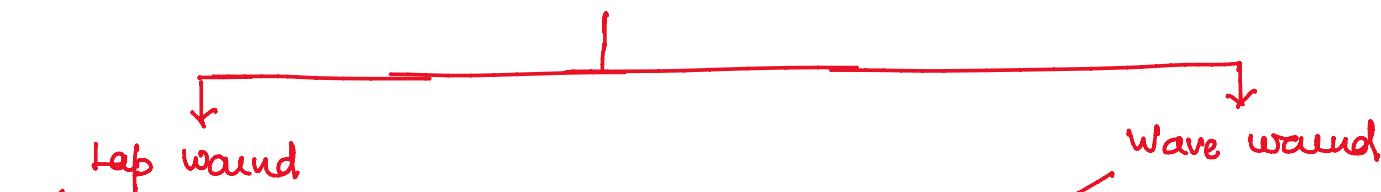
E = emf

V_t = terminal voltage

* DC Shunt Machine



→ Based on Armature winding,



↳ In lap wound, the number of parallel paths (A) = No. of Poles (P)

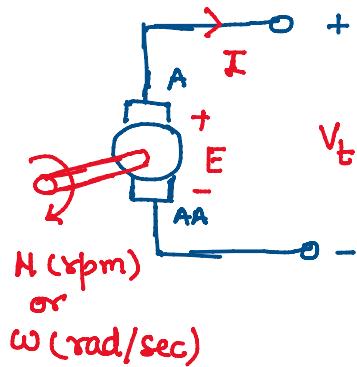
$$\text{i.e. } A = P$$

↳ irrespective of no. of poles, number of parallel paths $\boxed{A = 2}$

* DC Generator :

Working Principle :

Mechanical energy or
a input is provided to
Rotor by using prime mover



Since the field
winding is DC excited
there is relative
motion between
flux and Rotor

flux cuts the
Rotor Radially

i.e. it converted
into electrical
energy as a
output.

Due to the relative
motion an emf is
induced or generated
in armature winding
of Rotor

Generated EMF in Generator:

Let's assume

P = No. of poles

ϕ = flux per pole

N = rotor speed in rpm (rev/min)

Z = total No. of conductors

A = No. of parallel paths

According to Faraday's law of electromagnetic induction emf in a single conductor is

$$e = \frac{d\phi}{dt} = \frac{\text{Total flux}}{\text{Total time per revolution.}}$$

①

$$e = \frac{d\phi}{dt} = \frac{\text{Total flux}}{\text{Total time per revolution}} \quad \text{--- } ①$$

$$\begin{aligned}\therefore \text{Total flux} &= \text{flux per pole} \times \text{No. of Poles} \\ &= \phi \times P \quad \text{--- } ②\end{aligned}$$

$$\begin{aligned}\therefore \text{rotor speed} &= N \text{ revpm (rev/min)} \\ &= N \frac{\text{rev}}{60 \text{ sec}} = \frac{N}{60} \text{ rev/sec}\end{aligned}$$

$$\therefore \text{time for } \frac{N}{60} \text{ revolution} = 1 \text{ sec}$$

$$\therefore \text{time for 1 (ONE) revolution} = \frac{1}{N/60} = \frac{60}{N} \text{ sec} \quad \text{--- } ③$$

$$\therefore \text{emf in single conductor } e = \frac{P\phi}{60/N} = \frac{NP\phi}{60} = \frac{P}{60} \times N\phi \quad \text{--- } ④$$

\therefore no. of conductors is Z & no. of parallel paths is A

$$\text{then No. of series connected conductor} = \frac{Z}{A}$$

\therefore Total Generated emf in armature winding,

$$E = \frac{Z}{A} \times e = \frac{Z}{A} \times \frac{P}{60} \times N\phi$$

$$E = \frac{ZP}{60A} \times N\phi \Rightarrow E \propto N\phi$$

* If speed in rpm is N then speed in rad/sec is $\therefore 1 \text{ rev} = 2\pi \text{ rad}$
 $1 \text{ min} = 60 \text{ sec}$

$$\omega = N \times \frac{2\pi \text{ rad}}{60 \text{ sec}} = \frac{2\pi}{60} \times N \text{ rad/sec}$$

i.e.

$$\boxed{\omega = \frac{2\pi}{60} \times N}$$

$$\therefore E = \frac{ZP}{60A} \times N\phi = \frac{ZP}{60A} \times \frac{60}{2\pi} \omega \phi \quad \therefore N = \frac{60}{2\pi} \omega$$

$$E = \frac{ZP}{2\pi A} \phi \omega = k \phi \omega \quad \text{where } k = \frac{ZP}{2\pi A}$$

$$\therefore \boxed{E = k \phi \omega}$$

* Circuits for DC Generator for analysis :

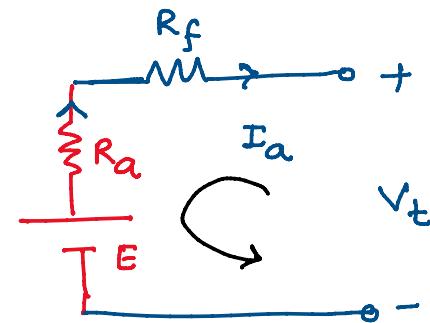
→ DC Series Generator

As shown in the circuit

R_f = field winding Resistance

R_a = Armature winding Resistance

E = Generated emf



r_a = armature winding resistance

E = Generated emf

V_t = terminal voltage

I_a = armature current

Apply KVL in the circuit

$$V_t + I_a R_f + I_a r_a - E = 0$$

$$E = V_t + I_a (R_a + R_f)$$

→ DC Shunt Generator:

As shown in the circuit

r_f = field winding resistance

r_a = Armature winding Resistance

E = Generated emf

V_t = terminal voltage

I = line current

I_a = armature current

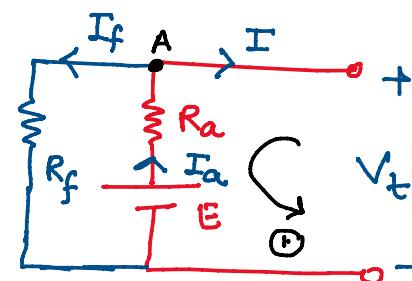
I_f = field current

Applying KVL in loop ①



* NOTE: If the brush drop V_{BD} given in the numerical then

$$E = V_t + I_a (R_a + R_f) + V_{BD}$$



* NOTE: If the brush drop V_{BD} given in the numerical then

$$E = V_t + I_a R_a + V_{BD}$$

$$V_t + I_a R_a - E = 0 \Rightarrow E = V_t + I_a R_a \quad \text{--- (1)}$$

\therefore voltage across field winding is V_t

$$\therefore V_t = I_f R_f \Rightarrow I_f = \frac{V_t}{R_f} \quad \text{--- (2)}$$

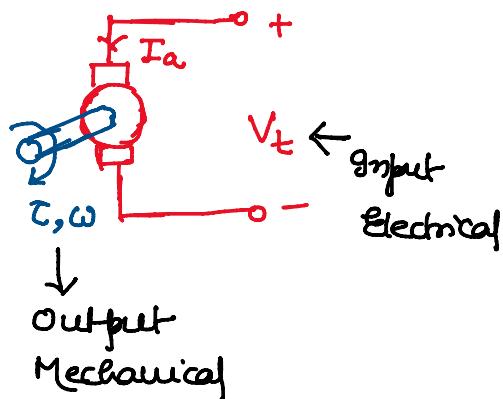
Applying KCL at Node A

$$I_a = I + I_f \quad \text{--- (3)}$$

DC Motor :

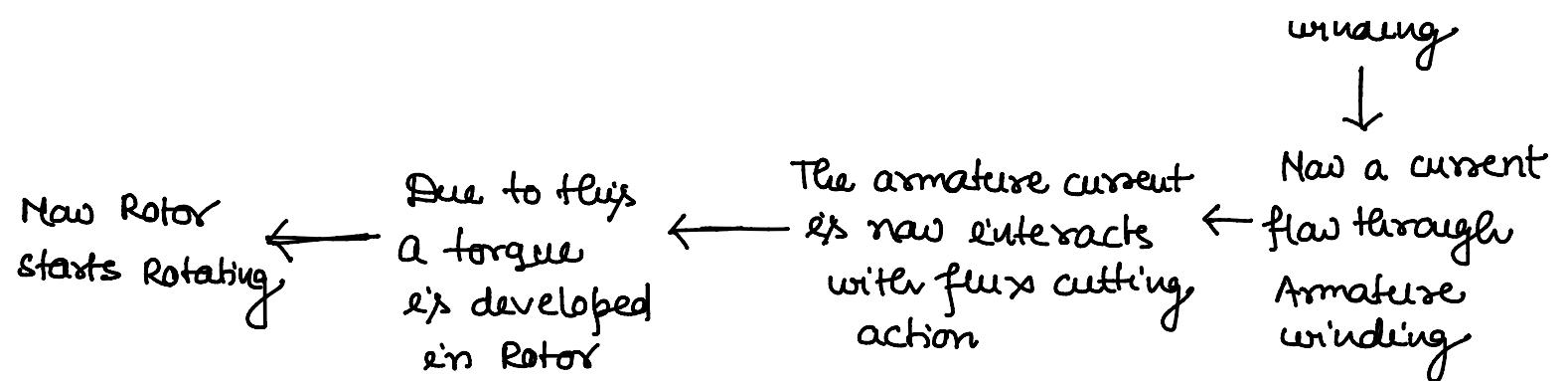
* Working Principle :

A DC supply is \longrightarrow Since field winding \longrightarrow A flux is produced \longrightarrow This flux cuts the armature winding of Rotor radially,



\downarrow
Due to this
an emf is
induced in
armature
winding.

1.



Torque Developed in Motor:

Let's assume there is no mechanical losses

\therefore Electrical input to the rotor which converts into mechanical output power is

$$P_{e,i/p} = EI_a \quad \text{--- (1)}$$

where E = Back emf & I_a = armature current

Now the developed mechanical output power is

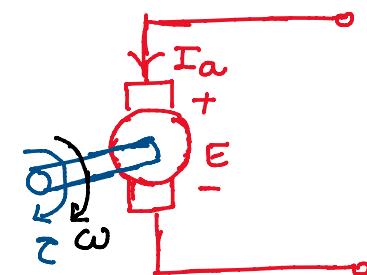
$$P_{m o/p} = \tau \omega \quad \text{--- (2)}$$

where τ = developed torque & ω = speed of rotor in rad/sec

\therefore there is no losses (mechanical)

$$\therefore P_{e,i/p} = P_{m o/p} \Rightarrow EI_a = \tau \omega$$

$$\Rightarrow \tau \omega = EI_a \quad \text{--- (3)}$$



$$\text{IP} \quad \text{IT}$$

$$\Rightarrow \tau \omega = EI_a \quad \text{--- } ③$$

\therefore Back emf $E = k\phi\omega$ where $k = \frac{ZP}{2\pi A}$

Now put the value of E in equation ③

$$\tau \omega = k\phi I_a$$

$$\Rightarrow \boxed{\tau = k\phi I_a} \quad \text{where } k = \frac{ZP}{2\pi A}$$

Z = No. of Conductors
 P = No. of Poles
 A = No. of parallel paths

* Circuits for DC Motor for analysis :

→ DC Series Motor

As shown in the circuit

R_f = field winding Resistance

R_a = Armature winding Resistance

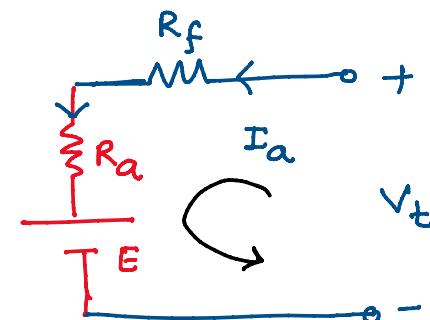
E = Generated emf

V_t = terminal voltage

I_a = armature current

Apply KVL in the circuit

$$V_t - I_a R_f - I_a R_a - E = 0$$



* NOTE: If the brush drop V_{BD} given in the numerical then

$$E = V_t - I_a (R_a + R_f) - V_{BD}$$

$$E = V_t - I_a (R_a + R_f)$$

→ DC Shunt Motor :

As shown in the circuit

R_f = field winding Resistance

R_a = Armature winding Resistance

E = Generated emf

V_t = terminal voltage

I = line current

I_a = armature current

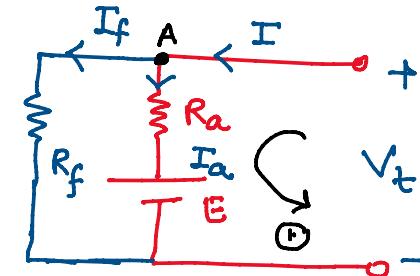
I_f = field current

Applying KVL in loop ①

$$V_t - I_a R_a - E = 0 \Rightarrow E = V_t - I_a R_a$$

∴ voltage across field winding is V_t

$$\therefore V_t = I_f R_f \Rightarrow I_f = \frac{V_t}{R_f}$$



* NOTE : If the brush drop V_{BD} given in the numerical then

$$E = V_t - I_a R_a - V_{BD}$$

Applying KCL at Node A

$$I = I_a + I_f$$

— ③