

**ME3210**  
**Control Systems**

**ME21BTECH11001**  
**Abhishek Ghosh**

## Question 1

ME3120 Control Systems :-

ME21BTECH11001

Assignment -1

Abhichet Ghosh

Question 1

$$(a) \lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} s f(s)$$

Ans:  $\mathcal{L}[f(t)] = f(s)$

Also,  $\mathcal{L}[f'(t)] = s \mathcal{L}[f(t)] - f(0)$

$$\text{LHS} \rightarrow \mathcal{L}[f'(t)] = \mathcal{L}\left[\frac{d}{dt}f(t)\right] = \int_0^{\infty} e^{-st} \left(\frac{d}{dt}f(t)\right) dt$$

$$\Rightarrow \int_0^{\infty} e^{-st} \frac{d}{dt}f(t) dt = s f(s) - f(0)$$

$$\begin{aligned} \rightarrow \lim_{s \rightarrow 0} \mathcal{L}\left[\frac{d}{dt}f(t)\right] &= \lim_{s \rightarrow 0} \int_0^{\infty} \frac{1}{e^{st}} \frac{d}{dt}f(t) dt \\ &= \int_0^{\infty} 1 * \frac{d}{dt}f(t) dt \\ &= f(\infty) - f(0) = f(\infty) \end{aligned}$$

$$\text{RHS} \quad \lim_{s \rightarrow 0} [s f(s) - f(0)] = \lim_{s \rightarrow 0} s f(s)$$

$$\therefore \lim_{t \rightarrow \infty} f(t) = \lim_{s \rightarrow 0} s f(s) \longrightarrow \text{Proved}$$

$$(b) \mathcal{L}[t f(t)] = - \frac{d f(s)}{ds}$$

Ans:  $\mathcal{L}[f(t)] = f(s) = \int_0^{\infty} f(t) e^{-st} dt$

$$\frac{d}{ds} f(s) = \frac{d}{ds} \left( \int_0^{\infty} f(t) e^{-st} dt \right)$$

$$= \int_0^{\infty} \frac{d}{ds} (b(t) e^{-st}) dt$$

$$= - \int_0^{\infty} e^{-st} t b(t) dt$$

$$= - \mathcal{L}[t b(t)] \longrightarrow \text{Proved}$$

$$\textcircled{c} \quad \mathcal{L}\left[\int_0^t b(\tau) d\tau\right] = \frac{F(s)}{s}$$

$$\text{considering } g(t) = \int_0^t b(\tau) d\tau$$

$$g'(t) = b(t) \quad \& \quad g(0) = 0$$

$$\mathcal{L}[g'(t)] = s \mathcal{L}[g(t)] - g(0)$$

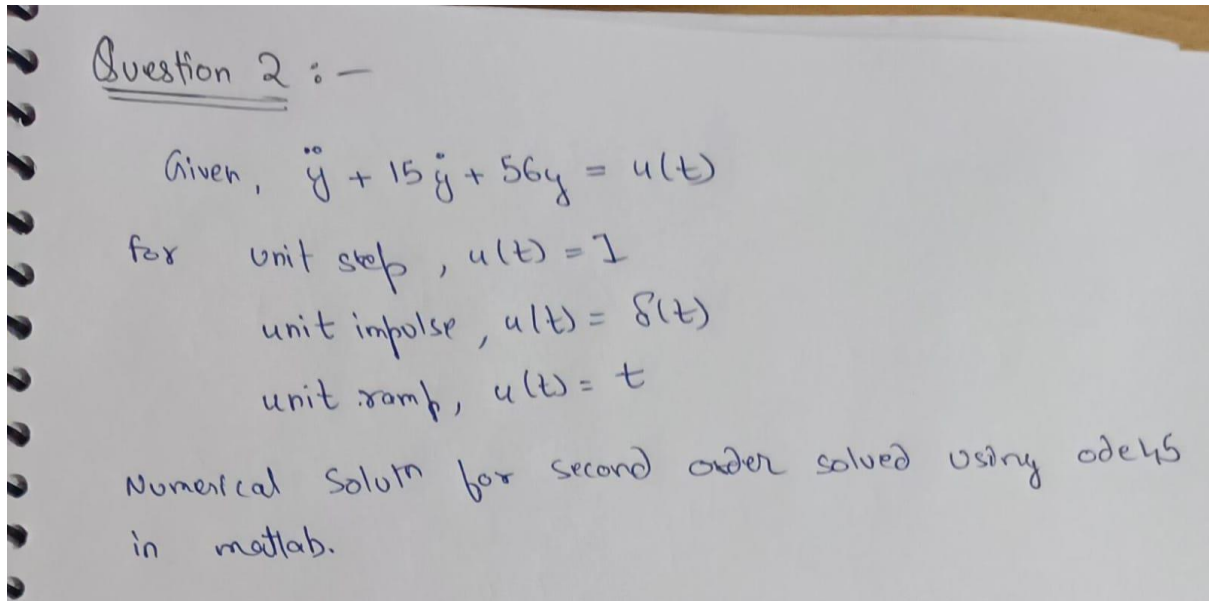
$$\Rightarrow \mathcal{L}[b(t)] = s \mathcal{L}[g(t)]$$

$$\rightarrow \mathcal{L}[g(t)] = \frac{\mathcal{L}[b(t)]}{s}$$

$$= \frac{F(s)}{s}$$

$$\Rightarrow \mathcal{L}\left[\int_0^t b(\tau) d\tau\right] = \frac{F(s)}{s} \longrightarrow \text{Proved}$$

## Question 2



## Code:

```
%Abhishek Ghosh
%ME21BTECH11001
%Question 2

% Parameters
tspan = [0 2.5]; % Time interval
y0 = [0; 0]; % Initial conditions: y(0) = 0, dy(0) = 0

% Case 1: u(t) = 1
u1 = @(t) 1; % Define the function u(t) = 1
[t1, y1] = ode45(@(t, y) odefunc(t, y, u1), tspan, y0);

% Case 2: u(t) = t
u2 = @(t) t; % Define the function u(t) = t
[t2, y2] = ode45(@(t, y) odefunc(t, y, u2), tspan, y0);

% Case 3: u(t) = Dirac Delta approximation
impulse_magnitude = 100000; % Large magnitude to approximate Dirac delta
impulse_duration = 0.00001; % Very short duration for impulse
u_dirac = @(t) (t >= 0 & t <= impulse_duration) * impulse_magnitude;

[t_dirac, y_dirac] = ode45(@(t, y) odefunc(t, y, u_dirac), tspan, y0);

% Plotting the results
figure;

% Plot for u(t) = 1
subplot(3, 1, 1);
plot(t1, y1(:, 1), 'b', 'LineWidth', 2);
title('Solution y(t) for Unit Step Response u(t) = 1');
xlabel('t');
ylabel('y(t)');
grid on;

% Plot for u(t) = Dirac Delta approximation
subplot(3, 1, 2);
plot(t_dirac, y_dirac(:, 1), 'g', 'LineWidth', 2);
title('Solution y(t) for Unit Impulse Response u(t) = Dirac Delta (Approximated)');
```

```

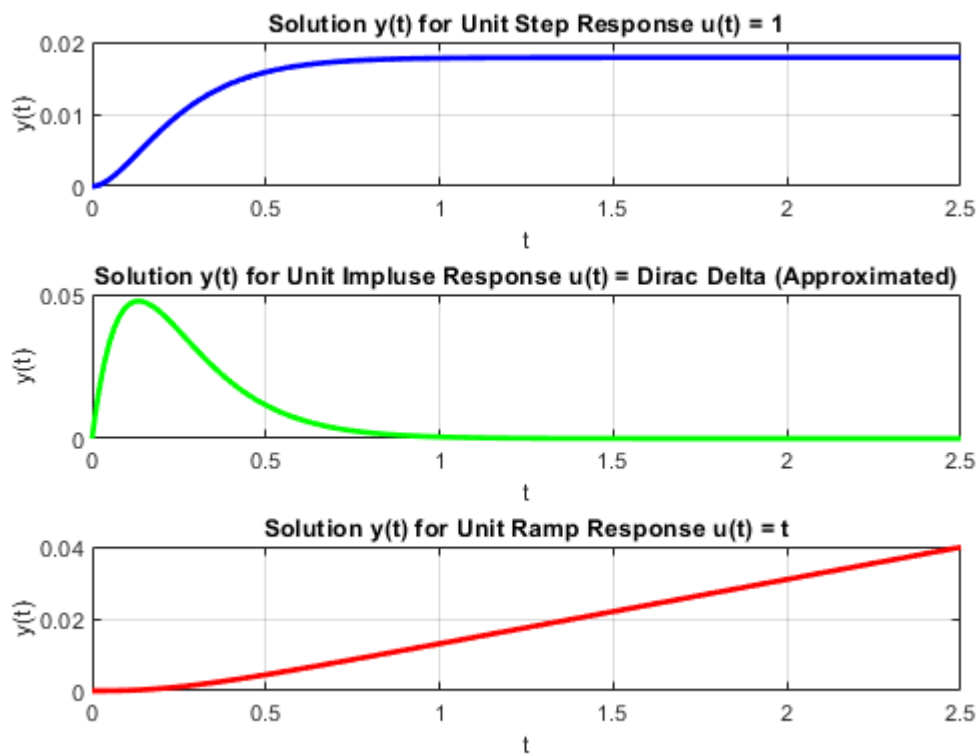
xlabel('t');
ylabel('y(t)');
grid on;

% Plot for u(t) = t
subplot(3, 1, 3);
plot(t2, y2(:, 1), 'r', 'LineWidth', 2);
title('Solution y(t) for Unit Ramp Response u(t) = t');
xlabel('t');
ylabel('y(t)');
grid on;

% Function to define the system of first-order ODEs
function dydt = odefunc(t, y, u)
    dydt = zeros(2, 1);
    dydt(1) = y(2); % dy1/dt = y2
    dydt(2) = u(t) - 15 * y(2) - 56 * y(1); % dy2/dt = u(t) - 15*y2 - 56*y1
end

```

## Plots:



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### Question 3

Ques<sup>n</sup> 3 :-

$$\text{Given, } \ddot{y} + 15\dot{y} + 56y = u(t)$$

Taking Laplace,

$$s^2 Y(s) - sY(0) - \dot{y}(0) + 15(sY(s) - y(0)) + 56Y(s) = U(s)$$

$$\rightarrow \text{Initial condition } y(0) = 0 \text{ \& } \dot{y}(0) = 0$$

$$\rightarrow s^2 Y(s) + 15sY(s) + 56Y(s) = U(s)$$

$$Y(s) = \frac{U(s)}{(s^2 + 15s + 56)}$$

Transfer funct<sup>n</sup>,

$$P(s) = \frac{Y(s)}{U(s)} = \frac{1}{s^2 + 15s + 56}$$

(i) for unit step response,

$$u(t) = 1, \quad u(s) = 1/s$$

$$Y(s) = P(s) U(s)$$

$$= \frac{1}{(s^2 + 15s + 56)} \times \frac{1}{s}$$

$$= \frac{1}{s(s+8)(s+7)} = \frac{A}{s} + \frac{B}{s+8} + \frac{C}{s+7}$$

$$\text{Solving } A = 1/56 \quad B = 1/8 \quad C = -1/7$$

$$Y(s) = \frac{1}{56s} + \frac{1}{8(s+8)} - \frac{1}{7(s+7)}$$

Taking Inverse Laplace

$$Y(t) = \frac{1}{56} + \frac{1}{8} e^{-8t} - \frac{1}{7} e^{-7t} \quad \underline{\underline{\text{Ans}}}$$

(ii) Unit Impulse Response

$$u(t) = \delta(t) \quad u(s) = 1$$

Dirac delta

$$\begin{aligned} Y(s) &= P(s) \cdot u(s) \\ &= \frac{1}{s^2 + 15s + 56} \times 1 \\ &= \frac{1}{(s+8)(s+7)} \end{aligned}$$

$$Y(s) = \frac{1}{s+7} - \frac{1}{s+8}$$

Inverse Laplace

$$y(t) = e^{-7t} - e^{-8t} \quad \text{--- Ans ---}$$

(iii) Unit Ramp Response

$$u(t) = t \quad u(s) = 1/s^2$$

$$\begin{aligned} Y(s) &= P(s) u(s) \\ &= \frac{1}{s^2 + 15s + 56} \times \frac{1}{s^2} \\ &= \frac{1}{s^2(s+8)(s+7)} \\ &= \frac{1}{56s^2} + \frac{1}{49(s+7)} - \frac{1}{64(s+8)} - \frac{15}{3136s} \end{aligned}$$

Inverse Laplace

$$y(t) = \frac{1}{56}t + \frac{1}{49}e^{-7t} - \frac{1}{64}e^{-8t} - \frac{15}{3136} \quad \text{--- Ans ---}$$

## Code:

```
%Abhishek Ghosh
%ME21BTECH11001
%Question 3

% Parameters for the ODE
tspan = [0 2.5]; % Time interval
y0 = [0; 0]; % Initial conditions: y(0) = 0, dy(0) = 0
impulse_magnitude = 100000; % Large magnitude to approximate Dirac delta
impulse_duration = 0.00001; % Very short duration for impulse

% Numerical Solutions Using ode45

% Case 1: u(t) = 1
u1 = @(t) 1; % Define the function u(t) = 1
[t1_num, y1_num] = ode45(@(t, y) odefunc(t, y, u1), tspan, y0);

% Case 2: u(t) = t
u2 = @(t) t; % Define the function u(t) = t
[t2_num, y2_num] = ode45(@(t, y) odefunc(t, y, u2), tspan, y0);

% Case 3: u(t) = Dirac Delta approximation
u_dirac = @(t) (t >= 0 & t <= impulse_duration) * impulse_magnitude;
[t_dirac_num, y_dirac_num] = ode45(@(t, y) odefunc(t, y, u_dirac), tspan, y0);

% Analytical Solutions Using Laplace Transforms
% Analytical solution for u(t) = 1
y1_analytical = @(t) ((1/56) + (1/8) * (exp(-8*t)) - (1/7) * exp(-7*t));

% Analytical solution for u(t) = t
y2_analytical = @(t) ((1/56) * t + (1/49) * (exp(-7*t)) - (1/64) * exp(-8*t) - 15/3136);

% Analytical solution for u(t) = Dirac Delta
y_dirac_analytical = @(t) (exp(-7*t) - exp(-8*t));

% Time vector for plotting analytical solutions
t_analytical = linspace(0, 2.5, 1000);

% Plotting the comparison between numerical and analytical solutions
figure;

% Case 1: u(t) = 1
subplot(3, 1, 1);
plot(t1_num, y1_num(:, 1), 'b', 'LineWidth', 2); hold on;
plot(t_analytical, y1_analytical(t_analytical), 'r--', 'LineWidth', 2);
title('Solution y(t) Unit Step Response for u(t) = 1');
xlabel('t');
ylabel('y(t)');
legend('Numerical Solution', 'Analytical Solution');
grid on;

% Case 3: u(t) = Dirac Delta approximation
subplot(3, 1, 2);
plot(t_dirac_num, y_dirac_num(:, 1), 'b', 'LineWidth', 2); hold on;
plot(t_analytical, y_dirac_analytical(t_analytical), 'r--', 'LineWidth', 2);
title('Solution y(t) for Unit Impulse Response u(t) = Dirac Delta (Approximated)');
xlabel('t');
ylabel('y(t)');
legend('Numerical Solution', 'Analytical Solution');
grid on;

% Case 2: u(t) = t
subplot(3, 1, 3);
```



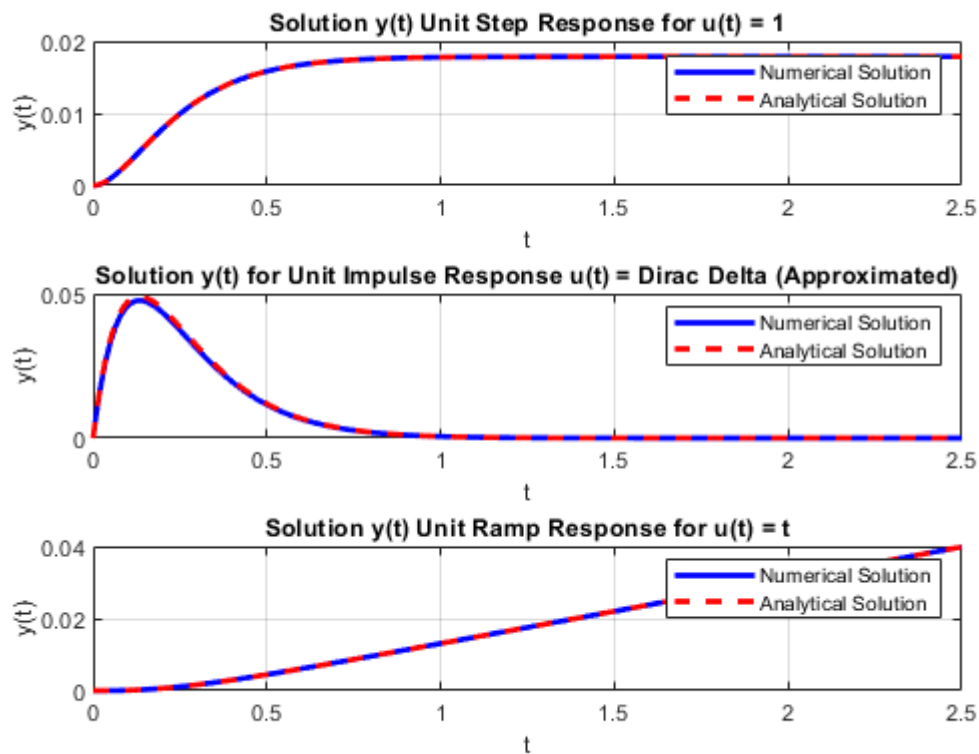
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plot(t2_num, y2_num(:, 1), 'b', 'LineWidth', 2); hold on;
plot(t_analytical, y2_analytical(t_analytical), 'r--', 'LineWidth', 2);
title('Solution y(t) Unit Ramp Response for u(t) = t');
xlabel('t');
ylabel('y(t)');
legend('Numerical Solution', 'Analytical Solution');
grid on;

% Function to define the system of first-order ODEs
function dydt = odefunc(t, y, u)
    dydt = zeros(2, 1);
    dydt(1) = y(2); % dy1/dt = y2
    dydt(2) = u(t) - 15 * y(2) - 56 * y(1); % dy2/dt = u(t) - 15*y2 - 56*y1
end

```

## Plots:



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Advantages of Laplace Transform :-

- i) Time domain eq<sup>n</sup> can be converted into simple algebraic form
- ii) for a known transfer funct<sup>n</sup>, o/p response is easy to determine for any i/p.
- iii) Helps to determine important parameter like poles/zeros.
- iv) Stability of system can be analysed.

#### Question 4

Ques<sup>n</sup> 4 :-

$$\mathcal{L}[P(t)] = P(s) \longrightarrow \text{Transfer funct<sup>n</sup>}$$

$$|P(t)| \rightarrow 0 \quad \text{as } t \rightarrow \infty$$

$$Y(s) = P(s) \cdot u(s) \quad y(t) = P(t) * u(t)$$

$$y(t) = \int_0^t P(t-\tau) u(\tau) d\tau \quad \text{convolut<sup>n</sup>}$$

for BIBO stability  $u(t) \rightarrow \text{bounded}$

$$|u(t)| \leq m < \infty \quad \forall \quad t > 0$$

$$y(t) = \left| \int_0^t P(t-\tau) u(\tau) d\tau \right|$$

$$\leq \int_0^t |P(t-\tau)| |u(\tau)| d\tau$$

$$\leq m \int_0^t |P(t-\tau)| d\tau$$

BIBO  $\rightarrow y(t)$  should be bounded when  $t \rightarrow \infty$

$\Rightarrow \int_0^t |p(t-\tau)| d\tau$  should be bounded @  $t \rightarrow \infty$

Area of curve  $|p(t)|$  should be constant in  $t \in [0, \infty)$

$\Rightarrow \lim_{t \rightarrow \infty} |p(t)| = 0$

since  $|y(t)| \leq m \int_0^t |p(t-\tau)| d\tau$

if  $\lim_{t \rightarrow \infty} |p(t)| \neq 0$

$\lim_{t \rightarrow \infty} \int_0^t |p(t-\tau)| d\tau \rightarrow \infty$

$y(t) \rightarrow \text{unbounded}$

$\therefore \lim_{t \rightarrow \infty} |p(t)| = 0 \rightarrow \text{necessary condition for BIBO stability}$

$\therefore$  If  $\lim_{t \rightarrow \infty} |p(t)| = 0$  is given  
then  $|y(t)| \leq m \int_0^t |p(t-\tau)| d\tau$  is bounded

$\Rightarrow \lim_{t \rightarrow \infty} |p(t)| = 0$  is necessary & sufficient condition for BIBO stability

if  $|p(t)| \rightarrow \infty$   
then  $|y(t)| \leq m \int_0^t |p(t-\tau)| d\tau \rightarrow \infty$

$\Rightarrow |y(t)|$  is unbounded

$\therefore$  This system is not BIBO stable since for bounded  $p \rightarrow$  unbounded  $y$

$p(t) \rightarrow \infty$

for a finite value of  $t \rightarrow$  no system

$p(s) = \frac{1}{s-a}$   $p(t) = e^{at} \rightarrow \infty$  when  $t \rightarrow \infty$

## Question 5

Question 5 :-

System :- An automatic fan control system.

This system manages the operation of an electric fan based on temperature readings. This system can be used in computer cooling systems or industrial processes where we need to maintain stable temp.

Necessity :-

- To prevent overheating
- To reduce energy consumption
- To extend lifespan of fan/device.

### Constraints :-

- The system must maintain temp within a predefined range.
- Response Time: System should respond quick enough to change temp.
- Power Consump<sup>n</sup>: The system should minimize power usage and be cost effective

### Assumpt<sup>n</sup>s :-

- Assuming fan's speed is linear to its speed.
- Temp sensors and fan respond instantaneously to changes.
- External factors are constant or slow changing

### Mathematical Model :-

$T(t)$ : Temp of system at time  $t$

$T_{set}$ : Desired setpoint Temp.

$T_{env}$ : Ambient Temp.

$u(t)$ : Control i/p | fan speed

$K_f$ : fan constant.

Heat Balance Eq<sup>n</sup>:  $C \frac{dT(t)}{dt} = -K_f u(t) + \dot{Q}_{env}$

where  $C$ : Thermal capacity of system

Control eq<sup>n</sup>:  $\frac{dT(t)}{dt} = -\frac{K_f}{C} u(t) + \frac{K_f}{C} T_{set} + \frac{\dot{Q}_{env}}{C}$

Taking Laplace Transform

$$sT(s) = -\frac{K_b}{c}U(s) + \frac{K_b}{c}\frac{T_{set}}{s} + \frac{den}{c}\frac{1}{s}$$

Isolating I/p & o/p relation

$$T(s) = -\frac{K_b}{c}\frac{U(s)}{s}$$

Transfer function:  $\frac{T(s)}{U(s)} = \frac{-K_b}{cs}$

$$\Rightarrow H(s) = \frac{T(s)}{U(s)} = \frac{-K_b}{cs}$$