

## MSD Walls Technical Appendix v2.0.0

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Released: January 2026

This online supplement details the equations used in the python code available at:  
[https://github.com/AbiBateman/MSD\\_Walls](https://github.com/AbiBateman/MSD_Walls).

This code (v2.0.0) has been used in the publication:

Hua, Y., Struzik, Z., Bateman, A.H., Crispin, J.J., Huang, H., Zhang, D., Mylonakis, G.E. & Vardanega, P.J. (2026). Assessing the effectiveness of the mobilizable strength design method for prediction of retaining wall movements using a database. *Submitted*.

v1.0.0 of this code has been used in the publication:

Crispin, J.J., Bateman, A.H., Voyagaki, E., Campbell, A., Mylonakis, G., Bolton, M.D. & Vardanega, P.J. (2024). MSD applied to the construction of the British Library basement: a multistage excavation in London Clay. *Canadian Geotechnical Journal*, 61(3):596-603. <https://doi.org/10.1139/cgj-2023-0238>

Section 1 of this supplement details the displacements from Stage 1 (pure rotation). Section 2 of this supplement details the displacements from the bulging stages (stages 2 onwards).

## NOTATION

### Latin

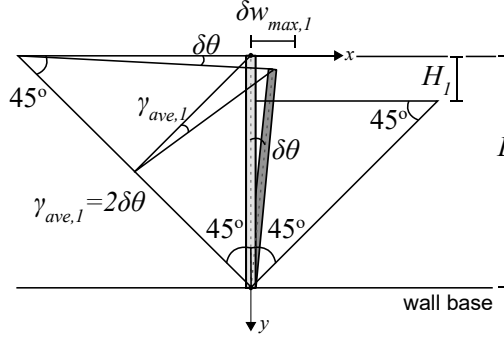
$A$  = Normalised (dimensional) parameter accounting for the potential energy loss at each stage (Eq. A6)  
 $a$  = Normalised (dimensionless) parameter accounting for the potential energy loss at each stage (Eq. A6)  
 $B$  = Normalised (dimensional) parameter accounting for the change in internal elastoplastic work (Eq. A7)  
 $B_{max}$  =  $B$  normalised by the mobilisation factor (Eq. A14)  
 $b$  = Soil non-linearity exponent  
 $b_0$  = Normalised (dimensionless) contribution to  $B$  of the constant component of  $s_u$  (Eq. A7)  
 $b_{var}$  = Normalised (dimensionless) contribution to  $B$  of the depth varying component of  $s_u$  (Eq. A7)  
 $C_1, C_2$  = Normalised (dimensional) parameters used to describe the strain energy stored in the wall (Eq. A9)  
 $EI$  = Plane-strain bending stiffness per meter length of the wall  
 $H_m$  = Excavated depth at stage  $m$   
 $H_{p,m}$  = Depth to the prop installed prior to the excavation stage  $m$   
 $h_{p,m}$  = Distance between the excavated depth and the last installed prop [ $h_{p,m} = H_m - H_{p,m}$ ]  
 $L$  = Length of the wall  
 $M_c$  = Similarity factor  
 $m$  = Excavation stage index  
 $r$  = Radial distance from the zone centre of rotation in zones CDE and EFH (Eq. A8)  
 $r_0$  = Radial distance of the centre of rotation of zones CDE and EFH from point D (Eq. A8)  
 $r_{1,m} \approx 0.371\lambda_m$  = Radial distance from point D where the sign of  $\delta\gamma$  changes in zone CDE  
 $r_{2,m}, r_{3,m}$  = Two radial distances from point F where the sign of  $\delta\gamma$  changes in zone EFH  
 $r_p$  = Radial distance from point F of peak value of  $\delta\gamma$  in zone EFH  
 $s_m$  = Distance between the last installed prop and the base of the wall [ $s_m = L - H_{p,m}$ ]  
 $s_u$  = Soil undrained shear strength  
 $s_{u,0}$  = Soil undrained shear strength at the top of the wall  
 $s_{u,var}$  = Change of the soil undrained shear strength per meter depth  
 $w_m$  = Wall displacement at excavation stage  $m$   
 $y$  = Depth below the top of the wall

### Greek

$\alpha_\lambda$  = Modification factor to scale the displacement mechanism for different wall base conditions  
 $\beta_m$  = Soil strength mobilisation factor ( $\tau/s_u$ ) (Eq. A11)  
 $\gamma$  = Soil engineering shear strain  
 $\gamma_{50}$  = Soil shear strain when 50% of the soil shear strength is mobilised  
 $\gamma_{ave,m}$  = Average mobilised shear strain in the mechanism for each stage  $m$  (Eq. A11)  
 $\gamma_{sat}$  = Soil saturated unit weight  
 $\Delta U_m$  = Elastic strain energy stored in the wall at stage  $m$   
 $\Delta P_m$  = Potential energy loss at each stage  $m$   
 $\Delta W_m$  = Internal elastoplastic work at stage  $m$   
 $\delta u_{y,m}$  = Incremental vertical soil displacement at stage  $m$   
 $\delta w_m$  = Incremental wall displacement at stage  $m$   
 $\delta w_{max,m}$  = Maximum incremental wall displacement at stage  $m$  (Eq. A1 & A10)  
 $\delta\gamma$  = Incremental shear strain  
 $\delta\theta$  = Angle of wall rotation during stage 1  
 $\lambda_m$  = Wavelength of the deformation mechanism  
 $\tau$  = Soil engineering shear stress  
 $\chi_1$  = Contribution of the previous stages to  $\beta_m$  when  $b = 0.5$  (Eq. A13b)  
 $\chi_2$  = Contribution of the current stage to  $\beta_m$  when  $b = 0.5$  (Eq. A13c)

## 1. RIGID WALL ROTATION

Stage 1 of the excavation is modelled as pure rotation around the base of the wall (see Fig. A1). Triangular displacement mechanisms are modelled on both sides of the wall (Fig. A1). These deform in uniform shear (Osman and Bolton 2004) and energy equilibrium is considered (potential energy loss equals internal plastic work) to determine the wall rotation.



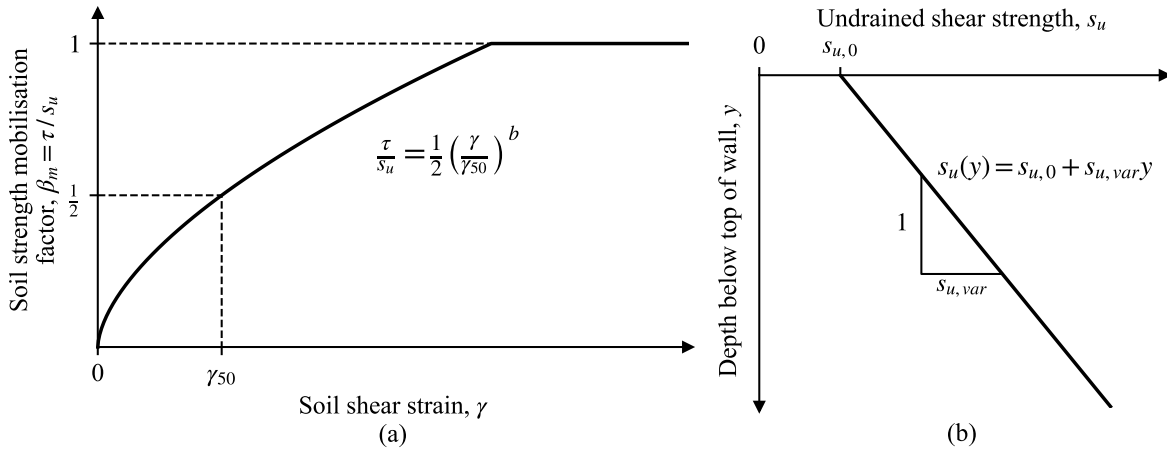
**Figure A1.** Illustration of the wall rotation around the base of the wall during stage 1 (modified from Osman and Bolton 2006).

By assuming a power-law soil constitutive model (Fig. A2a) and a linear variation of the shear strength,  $s_u$ , with depth below the top of the wall,  $y$ , ( $s_u = s_{u,0} + s_{u,var}y$ , see Fig. A2b), the following solution is obtained for the wall displacement at stage 1,  $\delta w_1$  (modified from Osman and Bolton 2006).

$$\delta w_1 = \delta w_{max,1} \left(1 - \frac{y}{L}\right) \quad (A1a)$$

$$\delta w_{max,1} = \frac{L\gamma_{50}}{2} \left[ \frac{\gamma_{sat}H_1 \left[ 3 - 3\left(\frac{H_1}{L}\right) + \left(\frac{H_1}{L}\right)^2 \right]}{3s_{u,0} \left[ 2 - 2\left(\frac{H_1}{L}\right) + \left(\frac{H_1}{L}\right)^2 \right] + s_{u,var}L \left[ 2 - 3\left(\frac{H_1}{L}\right)^2 + 2\left(\frac{H_1}{L}\right)^3 \right]} \right]^{\frac{1}{b}} \quad (A1b)$$

where  $\delta w_{max,1}$  is the maximum wall displacement at stage 1,  $L$  denotes the length of the wall,  $H_1$  is the excavated depth at stage 1,  $\gamma_{sat}$  is the saturated unit weight of the soil,  $\gamma_{50}$  is the shear strain when 50% of the soil shear strength is mobilised,  $b$  is a soil non-linearity exponent,  $s_{u,0}$  is the undrained shear strength at the surface of the soil and  $s_{u,var}$  is the variation of the undrained shear strength with depth. The average mobilised shear strain in the mechanism  $\gamma_{ave,1}$  is approximately twice the angle of rotation of the wall  $\delta\theta$  [ $\delta\theta = \delta w_{max,1}/L = \gamma_{ave,1}/2$ ].



**Figure A2.** (a) Soil constitutive behaviour modelled using a power-law function, and (b) variation of soil undrained shear strength with depth

## 2. BULGING OF A BRACED EXCAVATION

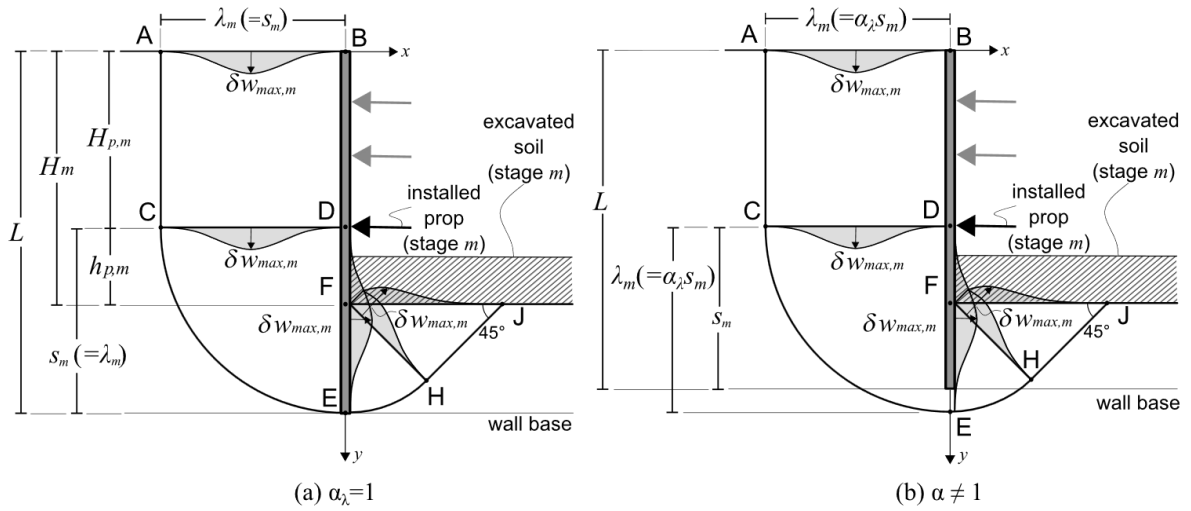
An elastoplastic deformation mechanism, used by Osman and Bolton (2006), is assumed (depicted in Fig. A3). The wall, of length  $L$ , has a plane-strain bending stiffness per meter length of the wall  $EI$ . The wall has an assumed incremental displacement for each stage (for  $m \geq 2$ ) according to the shape function (O'Rourke 1993):

$$\delta w_m(y) = \frac{1}{2} \left[ 1 - \cos \left( \frac{2\pi(y-H_{p,m})}{\lambda_m} \right) \right] \delta w_{max,m} \quad (A2)$$

where  $\delta w_m(y)$  is the wall displacement as a function of the depth measured from the top of the wall  $y$  and  $\delta w_{max,m}$  is the maximum wall displacement. Stage  $m$  refers to the current excavation stage, where  $H_m$  is the excavated depth,  $H_{p,m}$  is the depth to the prop installed prior to this excavation stage.  $\lambda_m$  refers to the size of the deformation mechanism and is dependent on wall fixity at the base  $\alpha_\lambda$  (shown in Fig. A3), given by:

$$\lambda_m = s_m \alpha_\lambda \quad (A3)$$

where  $s_m$  is the distance between the previously installed prop and the base of the wall [ $s_m = L - H_{p,m}$ ] and  $\alpha_\lambda$  is parameter used to model the boundary condition at the base of the wall (suggested by Osman and Bolton 2006; values of this parameter are discussed in the main text).



**Figure A3.** Incremental wall bulging at excavation stage  $m$ , plus plastic deformation mechanism considered for propped wall, for (a)  $\alpha_\lambda = 1$ , and (b)  $\alpha_\lambda \approx 1.1$  (modified from Osman and Bolton 2006).

### 2.1 General Solution

Considering the above elastoplastic mechanism for each stage, the potential energy loss  $\Delta P_m$  equals the sum of the internal elastoplastic work  $\Delta W_m$  and the elastic strain energy stored in the wall  $\Delta U_m$  (Lam and Bolton 2011):

$$\Delta P_m = \Delta W_m + \Delta U_m \quad (A4)$$

each term of which can be expressed as (modified from Lam and Bolton 2011):

$$\Delta P_m = \int_{area} \gamma_{sat} \delta u_{y,m} dArea \quad (A5a)$$

$$\Delta W_m = \int_{area} |\beta_m (s_{u,0} + s_{u,var} y) \delta \gamma| dArea \quad (A5b)$$

$$\Delta U_m = \frac{1}{2} EI \int_{H_{p,m}}^L \left[ (\delta w_m'')^2 + 2 \delta w_m'' \sum_{i=2}^{m-1} \delta w_i'' \right] dy \quad (A5c)$$

where  $\delta u_{y,m}$  is the incremental vertical soil displacement within the mechanism at each specific stage,  $\delta\gamma$  is the corresponding incremental shear strain,  $\beta_m$  is the average mobilised stress within the mechanism ( $\tau/s_u$ ) defined by Vardanega and Bolton (2011), and  $y$  is the depth measured from the top of the wall. These equations are simplified from those provided in Lam and Bolton (2011) by removing the discretisation of the mechanism. Note these equations are for the bulging stages only (the sum in Eq. A5c starts at stage 2). Calculations for stage 1 (the rotation stage) are discussed in Section 1.

The potential energy loss  $\Delta P_m$  (Eq. A5a) within the mechanism is given by:

$$\Delta P_m = A\delta w_{max,m} = [a \gamma_{sat} \lambda_m^2] \delta w_{max,m} \quad (A6)$$

where  $A$  and  $a$  are a normalised parameters (dimensional and dimensionless, respectively) used to describe the change in potential energy. The contribution to  $a$  for each zone within the mechanism is given in Table A1, where  $h_{p,m}$  is the distance between the excavated depth and the last installed prop ( $H_m - H_{p,m}$ ).

**Table A1:** Potential energy loss calculated for each zone within the mechanism

Zone	$a$ (Eq. A6)
ABCD (rectangular)	$\overline{H_p}/2$
CDE (circular segment)	$1/4$
EFH (circular segment)	$-\left(\frac{2-\sqrt{2}}{8\pi^2}\right) \left[\pi^2(1-\overline{h_p})^2 - \sin^2(\pi \overline{h_p})\right]$
FHJ (triangular)	$-\frac{\sqrt{2}}{8\pi^2} \left[\pi^2(1-\overline{h_p})^2 - \sin^2(\pi \overline{h_p})\right]$
<b>Total</b>	$\frac{1}{4} \left[1 + 2\overline{H_p} - (1-\overline{h_p})^2 + \frac{1}{\pi^2} \sin^2(\pi \overline{h_p})\right]$
$\overline{H_p} = H_{p,m}/\lambda_m$ ; $\overline{h_p} = h_{p,m}/\lambda_m$	

Similarly, the internal elastoplastic work  $\Delta W_m$  (Eq. A5b) within the mechanism is given by:

$$\Delta W_m = B\delta w_{max,m} = \beta_m B_{max} \delta w_{max,m} = [\beta_m \lambda_m (b_0 s_{u,0} + b_{var} \lambda_m s_{u,var})] \delta w_{max,m} \quad (A7)$$

where  $b_0$  and  $b_{var}$  are the (dimensionless) contributions due to the constant and depth varying components of  $s_u$ , respectively.  $B$  is a normalised (dimensional) parameter used to describe the change in internal elastoplastic work and  $B_{max}$  is  $B$  normalised by the mobilisation factor,  $\beta_m = \tau/s_u$  (Eq. A11a). The contribution to  $B$  for each zone within the mechanism is split into  $b_0$  and  $b_{var}$  as given in Table A2 and A3, respectively.

Note that Eq. A5b requires the absolute value of the virtual strain,  $\delta\gamma$ . Therefore, for zones CDE and EFH, where  $\delta\gamma$  can change sign, the integrated function is no-longer continuous and the integration must be split into sub-zones. Changes in sign can be found from the roots of  $\delta\gamma(r)$ , where  $r$  is the radial distance from the zone centre of rotation. For zone CDE, this occurs at  $r = r_{1,m} \approx 0.371\lambda_m$ , where  $r$  is the distance from point D. For EFH, a sign change only occurs when  $h_{p,m}$  is below approximately  $0.091\lambda_m$ , or, more accurately, when the peak value of  $\delta\gamma$  (at radius  $r_p$  from point F) is positive.  $r_p$  is in turn found from the root of  $d\delta\gamma(r)/dr$ , the derivative of  $\delta\gamma$

with respect to  $r$ . If  $\delta\gamma(r_p) > 0$ , there are two sign changes, at  $r = r_{2,m}$  and  $r = r_{3,m}$ . Values for  $r_p$ ,  $r_{1,m}$ ,  $r_{2,m}$  and  $r_{3,m}$  can be obtained through numerical root finding methods, such as bisection, using the following equations:

$$\delta\gamma(r) = \frac{\pi}{\lambda_m} \sin\left(2\pi \frac{r+r_0}{\lambda_m}\right) - \frac{1}{2r} \left(1 - \cos\left(2\pi \frac{r+r_0}{\lambda_m}\right)\right) \quad (\text{A8a})$$

$$\frac{d\delta\gamma(r)}{dr} = \frac{1}{2r^2} \left[1 - \left(1 - 4\pi^2 \frac{r^2}{\lambda_m^2}\right) \cos\left(2\pi \frac{r+h_{p,m}}{\lambda_m}\right) - 2\pi \frac{r}{\lambda_m} \sin\left(2\pi \frac{r+h_{p,m}}{\lambda_m}\right)\right] \quad (\text{A8b})$$

where  $r_0$  is the distance of the centre of rotation from point D.  $r_0 = 0$  for zone CDE, and  $r_0 = h_{p,m}$  for zone EFH.

**Table A2:** Internal elastoplastic work calculated for each zone within the mechanism

Zone	$b_0$ (Eq. A7)
ABCD (rectangular)	$2 \overline{H_p}$
CDE (circular segment)	$\frac{1}{2} [\sin(2\pi \overline{r_1}) - 2\pi \overline{r_1} \cos^2(\pi \overline{r_1}) + \pi]$ where $\overline{r_1} \approx 0.371$ (see above Eq. A8)
EFH (circular segment)	if $\gamma_r(r_p) \leq 0$ : (approximately $\overline{h_p} > 0.091$ ) $\frac{1}{8} [\sin(2\pi \overline{h_p}) - 2\pi(\overline{h_p} - 1)]$ else: $\frac{1}{8} [2\pi(1 - \overline{h_p}) + \sin(2\pi \overline{h_p})$ $+ 2 \sin(2\pi(\overline{h_p} + \overline{r_3})) - 2 \sin(2\pi(\overline{h_p} + \overline{r_2}))$ $+ 2\pi \overline{r_2} (\cos(2\pi(\overline{h_p} + \overline{r_2})) + 1) - 2\pi \overline{r_3} (\cos(2\pi(\overline{h_p} + \overline{r_3})) + 1)]$ where $r_p$ , $\overline{r_2}$ and $\overline{r_3}$ can be obtained from the method described above Eq. A8
FHJ (triangular)	$\frac{1}{4\pi} [4\pi - \sin(2\pi \overline{h_p}) - 6\pi \overline{h_p}]$

where  $\overline{H_p} = H_{p,m}/\lambda_m$ ;  $\overline{h_p} = h_{p,m}/\lambda_m$ ;  $\overline{r_1} = r_{1,m}/\lambda_m$ ;  $\overline{r_2} = r_{2,m}/\lambda_m$ ;  $\overline{r_3} = r_{3,m}/\lambda_m$

**Table A3:** Internal elastoplastic work calculated for each zone within the mechanism

Zone	$b_{var}$ (Eq. A7)
ABCD (rectangular)	$\overline{H}_p^2$
CDE (circular segment)	$\frac{1}{4\pi^2} [6\pi \overline{r}_1 \sin(2\pi \overline{r}_1) - 3(1 - \cos(2\pi \overline{r}_1)) + \pi^2(3 - 4\overline{r}_1^2 \cos(2\pi \overline{r}_1) - 2\overline{r}_1^2) + 2\pi^2 \overline{H}_p (\pi - \pi \overline{r}_1 (1 + \cos(2\pi \overline{r}_1)) + \sin(2\pi \overline{r}_1))]$ <p>where <math>\overline{r}_1 \approx 0.371</math> (see above Eq. A8)</p>
EFH (circular segment)	<p>if <math>\gamma_r(r_p) \leq 0</math>: (approximately <math>\overline{h}_p &gt; 0.091</math>)</p> $\frac{1}{16\pi^2} [3\sqrt{2}(\cos(2\pi \overline{h}_p) - 1) + 4\pi^3 \overline{H}(1 - \overline{h}_p) + 2\pi^2 (\overline{H} \sin(2\pi \overline{h}_p) + 3\sqrt{2} (1 - \overline{h}_p)^2)]$ <p>else:</p> $\frac{1}{16\pi^2} [2\sqrt{2}\pi^2 (2\overline{r}_2^2 - 2\overline{r}_3^2 + 3(1 - \overline{h}_p)^2) + 4\pi^3 \overline{H}(1 - \overline{h}_p + \overline{r}_2 - \overline{r}_3) - 3\sqrt{2} + 3\sqrt{2} (\cos(2\pi \overline{h}_p) - 2(c_{r2} - c_{r3})) + 2\pi^2 \overline{H} (\sin(2\pi \overline{h}_p) - 2(s_{r2} - s_{r3})) + 4\pi^3 \overline{H} (\overline{r}_2 c_{r2} - \overline{r}_3 c_{r3}) - 12\sqrt{2}\pi (\overline{r}_2 s_{r2} - \overline{r}_3 s_{r3}) + 8\sqrt{2}\pi^2 (\overline{r}_2^2 c_{r2} - \overline{r}_3^2 c_{r3})]$ <p>where <math>c_{r2}</math>, <math>c_{r3}</math>, <math>s_{r2}</math> and <math>s_{r3}</math> are given by:</p> $c_{r2} = \cos(2\pi(\overline{h}_p + \overline{r}_2)); c_{r3} = \cos(2\pi(\overline{h}_p + \overline{r}_3))$ $s_{r2} = \sin(2\pi(\overline{h}_p + \overline{r}_2)); s_{r3} = \sin(2\pi(\overline{h}_p + \overline{r}_3))$ <p>and <math>r_p</math>, <math>\overline{r}_2</math> and <math>\overline{r}_3</math> can be obtained from the method described above Eq. A8</p>
FHJ (triangular)	$\frac{1}{16\pi^2} [\pi^2 (3\sqrt{2} + 16\overline{H} - 24\overline{h}_p \overline{H} + 6\sqrt{2} \overline{h}_p^2 - 8\sqrt{2} \overline{h}_p) - 4\pi \overline{H} \sin(2\pi \overline{h}_p) - 2\sqrt{2}(\cos^2(\pi \overline{h}_p) + 1)]$

where  $\overline{H}_p = H_{p,m}/\lambda_m$ ;  $\overline{H} = H_m/\lambda_m$ ;  $\overline{h}_p = h_{p,m}/\lambda_m$ ;  $\overline{r}_1 = r_{1,m}/\lambda_m$ ;  $\overline{r}_2 = r_{2,m}/\lambda_m$ ;  $\overline{r}_3 = r_{3,m}/\lambda_m$

Finally, the elastic strain energy stored in the wall  $\Delta U_m$  (Eq. A5c) can be calculated as:

$$\Delta U_m = C_1 \delta w_{max,m}^2 + C_2 \delta w_{max,m} \quad (A9a)$$

$$C_1 = \pi^4 \frac{EI}{\lambda_m^3} \left[ \frac{1}{\alpha_\lambda} + \frac{1}{4\pi} \sin\left(\frac{4\pi}{\alpha_\lambda}\right) \right] \quad (A9b)$$

$$C_2 = \pi^3 EI \sum_{i=2}^{m-1} \frac{\delta w_{max,i}}{\lambda_i^3 \left(1 + \frac{\lambda_m}{\lambda_i}\right)} \left[ \frac{2}{\frac{\lambda_m}{\lambda_i} - 1} \sin\left(\frac{2\pi}{\alpha_\lambda} \left(\frac{\lambda_m}{\lambda_i} - 1\right)\right) + \frac{\lambda_i}{\lambda_m} \sin\left(\frac{4\pi}{\alpha_\lambda}\right) \right] \quad (A9c)$$

where  $C_1$  and  $C_2$  are normalised (dimensional) parameters used to describe the strain energy stored in the wall.

Substituting Eqs. A6, A7 and A9 into Eq. A4 yields:

$$\delta w_{max,m} = \frac{A-B-C_2}{C_1} \quad (A10)$$

The above solution requires assuming a value for the mobilisation factor  $\beta_m$  contributing to coefficient  $B$ . The soil shear stress mobilisation factor  $\beta_m$  can be found using the assumed soil constitutive model (Fig A2(a)) and setting the shear strain to average shear strain in the mechanism for each stage,  $\gamma_{ave,m}$ :

$$\beta_m = \frac{\tau}{s_u} = \frac{1}{2} \left( \frac{\gamma_{ave,m}}{\gamma_{50}} \right)^b \quad (A11a)$$

The average shear strain in the mechanism can be calculated as (Lam and Bolton 2011):

$$\gamma_{ave,m} = M_c \sum_{i=2}^m \frac{\delta w_{max,i}}{\lambda_i} \quad (A11b)$$

where  $M_c$  is a similarity factor suggested by Osman and Bolton (2006) to be 2.0 ( $\pm 10\%$ ).

Eq. A10 is a polynomial of  $\delta w_{max,m}$ . When  $b = 0.58$  (as per the example in the main text) an iterative approach is suggested to find a solution. In the supplied spreadsheet, a “guess” can be changed manually until it matches the predicted (“result”) incremental maximum displacement within a tolerable error. This is automated in the provided python script.

The overall displacements (for  $m \geq 2$ ) can then be found by superimposing the displacements along the wall for each stage, including the rotation stage, Eq. A1a (Clough *et al.* 1989):

$$w_m = \delta w_{max,1} \left(1 - \frac{y}{L}\right) + \sum_{i=2}^m \frac{1}{2} \left[1 - \cos\left(\frac{2\pi(y-H_{p,m})}{\lambda_m}\right)\right] \delta w_{max,m} \quad (A12)$$

## 2.2 Closed Form Solution ( $b = 0.5$ )

For the special case where  $b = 0.5$ , a closed-form solution can be derived that allows solving directly for  $\delta w_{max,m}$  without iteration (as is required for the above general solution). Using this assumption,  $\beta_m$  can be written as:

$$\beta_m = \frac{1}{2} \sqrt{\chi_1 + \chi_2 \delta w_{max,m}} \quad (A13a)$$

$$\chi_1 = \frac{M_c}{4\gamma_{50}} \sum_{i=1}^{m-1} \frac{\delta w_{max,i}}{\lambda_i} \quad (A13b)$$

$$\chi_2 = \frac{M_c}{4\lambda_m \gamma_{50}} \quad (A13c)$$

where  $\chi_1$  and  $\chi_2$  are the contributions of the previous and current stages, respectively, to  $\beta_m$ .

Then, substituting Eqs. A6, A7, A9 and A13 into Eq. A4 yields:

$$\delta w_{max,m} = \frac{1}{2C_2^2} \left[ B_{max}^2 \chi_2 + 2C_1(A - C_2) - B_{max} \sqrt{B_{max}^2 \chi_2^2 + 4\chi_2 C_1 A + 4\chi_1 C_1^2 - 4\chi_2 C_1 C_2} \right] \quad (A14)$$

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