

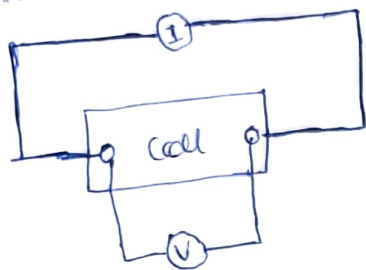
BMS2: ECM Simulation

* Week 2: Parameterization of Static Model

#1 Lab equipment for cell characterization

A cell's OCV is a static function of SOC and temperature. Separate cell tests are performed to collect data for the OCV versus SOC relationship in the lab.

- Physical test setup: 4-wire connection



It is critical to use 4-wire or Kelvin connection in test setup. When the battery is connected using 4-wires, the active sensing the cell voltage through the thin wire draws essentially zero current, hence zero voltage drop.

- Equipment:

Lab equipment known as ~~battery cell cycler~~ or ~~battery cell test setup~~ is used. An example, the one Chroma Spring manufactured by Arbin Instruments.

- Controlling Ambient Temperature

In addition to controlling the input current or power to a battery cell, the ambient temperature also should be controlled.

Example of an environmental chamber is that, manufactured by Cincinnati Sub-zero that can maintain constant temperatures between -45°C & 190°C .

#2 Cell test to determine OCV

The cell should be slowly discharged, then slowly charged between specified cut-off voltage by manufacturer. The test equipment will continuously measure voltage, accumulated ampere-hours discharged, and accumulated ampere-hours charged per second (1s).

Since OCV is a function of temperature, the test is done at the number of temperature spread over cell's operational range. Also, used very low current for negligible heat generation.

* Discharge portion of test

Assuming you want to carry out OCV test @ 35°C test temperature, follow this steps:

- Soak fully charged cell at ~~room~~ ^{test} temperature (35°C) for at least 2 hrs to ensure uniform temperature
- discharge cell at a constant-current C/30 rate until terminal voltage equal V_{\min}

→ Test @ 25°C ; follow same step

* Charge portion of test

- Soak cell at test temperature (35°C) for at least two hours to ensure uniform temperature throughout
- charge the cell at constant-current rate C/30 until cell terminal voltage equal V_{\max}

Test 1 @ 35°C
100% SOC → V_{\min}

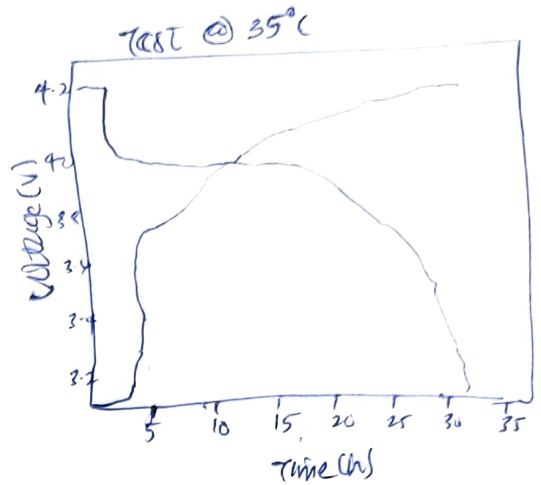
Test 3 @ 35°C
0% SOC → V_{\max}

Test 2 @ 25°C
 V_{\min} → 0% SOC

Test 4 @ 25°C
 V_{\max} → 100% SOC

} Calibration

N.B: OCV is different from equilibrium terminal voltage due to hysteresis, so set point SOC is not truly achieved.



Summary

- To determine OCV relationship, we generally want to average discharge and charge curves
- Calibrate tests by starting with fully charged cell and ensuring that SOC is OK after discharge and 100% after charge.
- Record of accumulated sample hours discharged will be used to determine total capacity, coulombic efficiency, and discharge voltage at every point in the test
- The voltages will be processed to compute OCV

#3 Determining cell's Coulombic Efficiency

* How to process the OCV test data to compute Coulombic efficiency and total capacity

- Processing data for 25°C

• Discrete time equation of SOC

$$z[k] = z[0] - \frac{1}{Q} \sum_{j=0}^{k-1} \eta[j] i[j]$$

time step
 $k = \text{final data point}$
 ① time $k = 1056 \text{ SOC}$
 $k=0 = 1056 \text{ SOC}$

$$z[k] = z[0] = 1 \text{ (cancels out)}$$

• Multiply by -Q, split summation

$$z[k] - z[0] = -\frac{1}{Q} \sum_{j=0}^{k-1} \eta[j] i[j]$$

$$0 = -\frac{1}{Q} \sum_{j=0}^{k-1} \eta[j] i[j]$$

$$0 = \sum_{j=0}^{k-1} \eta[j] i[j]$$

Split summation into discharging & charging sets

$$0 = \sum_{\text{discharge}} i[j] + \sum_{\text{charge}} \eta[k] i[j]$$

• Since temperature is constant; $\eta[k] = \eta(25^\circ\text{C})$ in all steps, the Coulombic efficiency at 25°C =

$$\eta(25^\circ\text{C}) = \frac{\text{total absolute ampere-hours discharge in all steps at } 25^\circ\text{C}}{\text{total absolute ampere-hour charged in all steps @ } 25^\circ\text{C}}$$

- Processing data for other temperatures

Once efficiency in 25°C is known, η at other temperature can be calculated.

• $z[k] = z[0] = 1$, but now

$$\begin{aligned} 0 &= \sum_{\text{discharge}} i[j] + \sum_{\text{charge at } T} \eta[k] i[j] + \sum_{\text{charge @ } 25^\circ\text{C}} \eta[k] i[j] \\ &= \sum_{\text{discharge}} i[j] + \eta(T) \sum_{\text{charge at } T} i[j] + \eta(25^\circ\text{C}) \sum_{\text{charge at } 25^\circ\text{C}} i[j] \end{aligned}$$

- Compute Coulombic efficiency at test temperature T :

$$\eta(T) = \frac{\text{total absolute ampere-hours discharged}}{\text{total absolute ~~temperature~~ ampere-hours charged at temperature } T}$$

$$= -\eta(25^\circ\text{C}) \frac{\text{total absolute ampere-hours charged at } 25^\circ\text{C}}{\text{total absolute ampere-hours charged at temperature } T}$$

* Capacity estimation for 25°C

Theoretically, total capacity Q is not a function of temperature, but it can be verified experimentally as well.

SOC is 100% at start of test and 0% at the end of step 4. Use SOC relationship

$$z[k] = 0 \text{ and } z[0] = 1$$

$$z[k] = z[0] - \sum_{j=0}^{k-1} \frac{\eta[j] i[j]}{Q}$$

- Summing over all data in step 1-4 gives Q in ampere-seconds

$$Q(25^\circ\text{C}) = \sum_{j=0}^{k-1} \eta[j] i[j]$$

* Capacity estimation for ~~other~~ temperature

- SOC is still 100% at start of test and 0% at the end of step 4

- Again, use SOC relationship where $z[k] = 0$ and $z[0] = 1$

$$z[k] = z[0] - \sum_{j=0}^{k-1} \frac{\eta[j] i[j]}{Q}$$

- Summing over all data in step 1-4 gives Q in ampere-seconds

$$1 = \sum_{\text{data @ } 25^\circ\text{C}} \frac{\eta(25^\circ\text{C}) i[j]}{Q(25^\circ\text{C})} + \sum_{\text{data } T} \frac{\eta(T) i[j]}{Q(T)}$$

N.B.: Assumed $Q(25^\circ\text{C}) = Q(T)$ when computing $\eta(T)$, but can solve simultaneously for $Q(T)$ and $\eta(T)$ if not convinced this is true.

* Summary

To determine a cell's Coulombic efficiency and total capacity:

- calculate absolute sum of ampere-hours discharged
- calculate absolute sum of ampere-hours charged @ 25°C
- calculate absolute sum of ampere-hours charged at all other temperatures
- compute $\eta(25^\circ\text{C})$, $\eta(T)$ for other temperature of interest
- compute $Q(25^\circ\text{C})$, $Q(T)$ for other temperature of interest

NB: While total capacity is not a function of temperature, there is a strong temperature dependence on discharge capacity & charge capacity.

→ Total capacity is the maximum number of ampere-hours that can be removed from a fully charged cell before fully discharged.

- discharge capacity: no. of ampere-hours that can be extracted from a fully charged cell at some constant current rate before encountering minimum voltage limit.

- Total capacity: 100 → 0% SOC

- Discharge capacity: 100 → V_{\min}

Total capacity needed for SOC estimation

#4 Determine a cell's temperature-dependent OCV

To compute OCV vs SOC, you need to compute state of charge SOC for every single data point. Instead of computing SOC ^{directly}, you can compute DOD

- DOD (or Ah) at any point in time is calculated as:

depth of discharge (Ct) = total Ah discharge until t

- $-\eta(25^\circ\text{C}) \times \text{total Ah charged at } 25^\circ\text{C until } t$
- $-\eta(T) \times \text{total Ah charged at temperature } T \text{ until } t$

- likewise, SOC corresponding to every data sample is then:

$$\text{SOC}(t) = 1 - \frac{\text{DOD}(t)}{Q}$$

- Check: SOC at end of step 4 must be 0%, and SOC at the end of step 8 must be 100%

* Modeling temperature dependence

At any given ~~SDC~~ SDC, OCV remains \sim nearly linear in T - (assuming individual approximate single-temperature OCV results to make a final model of the form:

$$OCV(z(t), T(t)) = OCV_0(z(t)) + T(t) \times OCV_{rel}(z(t))$$

- $OCV_0(z(t))$ is the OCV relationship at 0_C and OCV_{rel} is the linear temperature correction factor at each SDC

- Once $OCV_0(z(t))$ and $OCV_{rel}(z(t))$ are determined, $OCV(z(t), T(t))$ can be computed via two computationally efficient 1D table lookups.

• To make $OCV_0(z(t))$ and $OCV_{rel}(z(t))$, note we can write:

$$\begin{bmatrix} \text{Approx. OCV at SDC } z, \text{ temp. } T_1 \\ \text{Approx. OCV at SDC } z, \text{ temp. } T_2 \\ \vdots \\ \text{Approx. OCV at SDC } z, \text{ temp. } T_n \end{bmatrix} = \begin{bmatrix} 1 & T_1 \\ 1 & T_2 \\ \vdots & \vdots \\ 1 & T_n \end{bmatrix} \begin{bmatrix} OCV_0(z) \\ OCV_{rel}(z) \end{bmatrix}$$

$\underbrace{\hspace{10em}}_A \quad \underbrace{\hspace{5em}}_X$

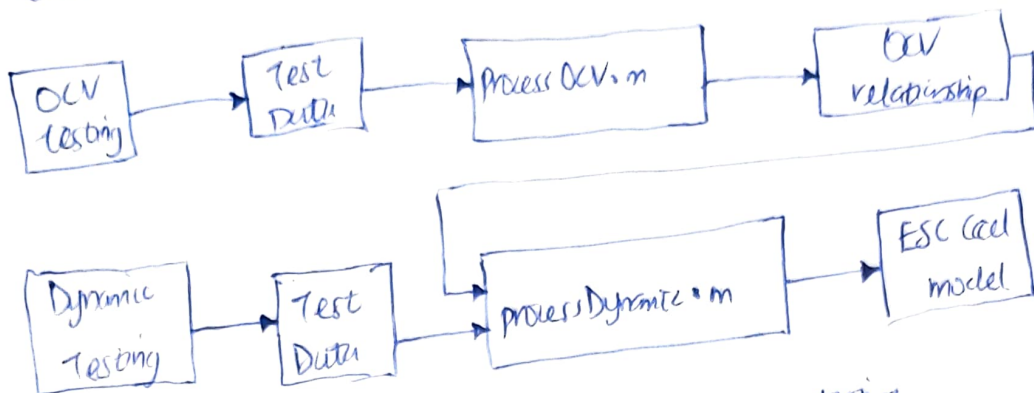
at m SDC value z for each g.n temperatures (γ is $n \times m$; A is $n \times 2$; X is $2 \times m$)

- one way to solve (find X from A and γ) is to use the least-squares solution, which is computed in Octave/MATLAB as $X = A \backslash \gamma$

- Two 1D table lookups used to compute OCV at any given SDC and temperature as:

$$OCV(z(t), T(t)) = OCV_0(z(t)) + T(t) \times OCV_{rel}(z(t))$$

#5: Octave code to determine static part of an ECM



- Laboratory processes: OCV testing, Dynamic testing
 - Data files: Test data, OCV relationship, ESC cell model
 - Octave/MATLAB function: processOCV.m, processDynamic.m
- ESC - Enhanced self-correcting

The processOCV.m computes OCV relationship from lab-test data

- the code first computes $\eta(25^\circ\text{C})$ and $Q(25^\circ\text{C})$
- then adjust discharge curve to compensate for estimated R_o
- computes approximate OCV vs SOC, compensating for steady-state resistance
- Repeat for all other test temperature
- Finally, computes OCV_o and OCV_{rel} , combining data from all temperature
- Results saved to a model file

* Summary

this week, how to determine a cell's static OCV relationship as a function of SOC, and temperature

- Lab-test equipment
- Test required to collect the necessary data
- how to process the data to determine Coulombic efficiency, total capacity, OCV

Octave/MATLAB code to produce the static model.