

Solution

The 8Ω and 7Ω resistors are in series:

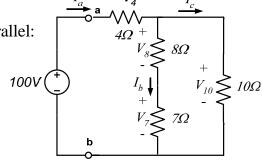
$$R1 = 8 + 7 = 15\Omega$$

R1 and 10Ω are in parallel:

$$R2 = \frac{1}{\frac{1}{10} + \frac{1}{R1}}$$

$$=\frac{10(R1)}{10+R1}=6\Omega$$

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Solution

 4Ω and R2 are in series:

$$R_{ab} = 4 + R2 = 10\Omega$$

 ΩL :

$$I_a = \frac{V_{ab}}{R_{ab}} = \frac{100}{10} = 10A$$
 100V(

$$V_4 = 4 \cdot I_a = 40V \quad (\Omega L)$$

$$V_{10} = 100 - 40 = 60V$$
 (KVL)

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 8Ω

 7Ω

Solution

$$I_{c} = \frac{V_{10}}{10} = \frac{60}{10} = 6A \quad (\Omega L)$$

$$KCL:$$

$$I_{b} = I_{a} - I_{c} = 10 - 6 = 4A$$

$$V_{8} = 8 \cdot I_{b} = 32V \quad (\Omega L)$$

$$V_{7} = 7 \cdot I_{b} = 28V \quad (\Omega L)$$

$$V_{7} = 1000 \quad (\Omega L)$$

$$V_{8} = 8 \cdot I_{0} = 28V \quad (\Omega L)$$

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$$V_{7} = 7 \cdot I_{0} = 28V \quad (\Omega L)$$

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Absorbed Powers...

$$R_4 \cdot I_a^2 = 4(10)^2 = 400W$$

In General:

$$R_{10} \cdot I_c^2 = 10(6)^2 = 360W$$

 $P_{ABS} = P_{DEV}$

$$\boldsymbol{R}_7 \cdot \boldsymbol{I}_b^2 = 7(4)^2 = 112W$$

(Tellegen's

$$R_8 \cdot I_b^2 = 8(4)^2 = 128W$$

Theorem)

Total Absorbed Power = 1000W

Power Delivered by Source = $V_s \cdot I_a = 100(10) = 1000W$

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2. Complex Numbers

Consider
$$x^2 - 2x + 5 = 0$$

$$x = \frac{2 \pm \sqrt{(-2)^2 - 4(1)(5)}}{2 \cdot 1} = \frac{2 \pm \sqrt{-16}}{2}$$

$$=1\pm\frac{4\sqrt{-1}}{2}=1\pm2\sqrt{-1}$$

The numbers " $1\pm 2\sqrt{-1}$ " are called **complex numbers**

Summer 2008

The "I" (j) operator

Math Department....

Define i =
$$\sqrt{-1}$$

Define
$$j = \sqrt{-1}$$

$$x = 1 \pm 2i$$

$$x = 1 \pm j2$$

We choose ECE notation! Terminology...

Rectangular Form.....

$$\overline{Z} = X + jY =$$
a complex number

$$X = \Re e(\bar{Z}) = \text{real part of } \bar{Z}$$

$$Y = \operatorname{Im}(\overline{Z}) = \operatorname{imaginary part of } \overline{Z}$$

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Polar Form

Math Department.....

 $\overline{Z} = R \cdot e^{\theta i} = \text{a complex number}$

 $R = |\bar{Z}| = \text{modulus of } \bar{Z}$

 $\theta = \arg(\bar{Z}) = \text{argument of } \bar{Z} \text{ (radians)}$

ECE Department.....

 $\overline{Z} = Z \angle \theta =$ a complex number

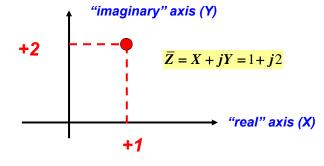
 $Z = |\bar{Z}| = \text{magnitude of } \bar{Z}$

 $\theta = \operatorname{ang}(\overline{Z}) = \operatorname{angle of} \overline{Z}(\operatorname{degrees})$

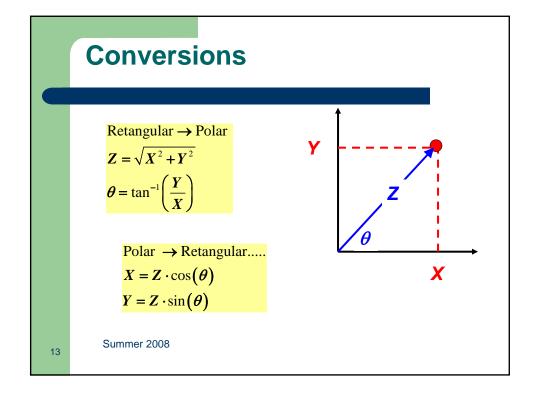
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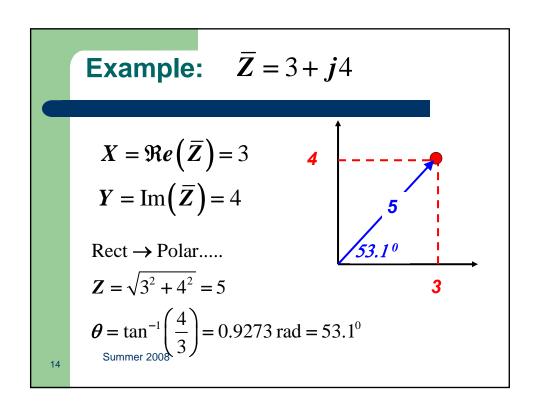
The Argand Diagram

It is useful to plot complex numbers in a 2-D cartesian space, creating the so-called Argand Diagram (Jean Argand (1768-1822)).



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Conjugate

$$\overline{Z} = X + jY = Z \angle \theta$$

$$\overline{Z}^*$$
 = conjugate of $\overline{Z} = X - jY = Z \angle - \theta$

Example...

$$(3+j4)$$
* = $3-j4$ = $5\angle -53.1^0$

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Addition (think rectangular)

$$\overline{A} = a + jb = A \angle \alpha = 3 + j4 = 5 \angle 53.1^{\circ}$$

 $\overline{B} = c + jd = B \angle \beta = 5 - j12 = 13 \angle -67.4^{\circ}$

$$\overline{A} + \overline{B} = (a + jb) + (c + jd)$$
$$= (a + c) + j(b + d)$$

$$\overline{A} + \overline{B} = (3 + j4) + (5 - j12)$$

= $(3 + 5) + j(4 - 12) = 8 - j8$

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Multiplication (think polar)

$$\overline{A} = a + jb = A \angle \alpha = 3 + j4 = 5 \angle 53.1^{\circ}$$

$$\overline{B} = c + jd = B \angle \beta = 5 - j12 = 13 \angle - 67.4^{\circ}$$

$$\overline{A} \cdot \overline{B} = (A \angle \alpha) \cdot (B \angle \beta)$$

$$= A \cdot B \angle (\alpha + \beta)$$

$$\overline{A} \cdot \overline{B} = (5 \angle 53.1^{\circ}) \cdot (13 \angle - 67.4^{\circ})$$

 $= (5) \cdot (13) \angle (53.1^{\circ} - 67.4^{\circ}) = 65 \angle -14.3^{\circ}$

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Division (think polar)

$$\overline{A} = a + jb = A\angle\alpha = 3 + j4 = 5\angle 53.1^{0}$$

$$\overline{B} = c + jd = B\angle\beta = 5 - j12 = 13\angle - 67.4^{0}$$

$$\frac{\overline{A}}{\overline{B}} = \frac{A\angle\alpha}{B\angle\beta} = \left(\frac{A}{B}\right)\angle(\alpha - \beta)$$

$$\frac{\overline{A}}{\overline{B}} = \left(\frac{5\angle 53.1^{0}}{13\angle - 63.4^{0}}\right) = \left(\frac{5}{13}\right)\angle\left(53.1^{0} - \left(-67.4^{0}\right)\right)$$

$$= 0.3846\angle 120.5^{0}$$
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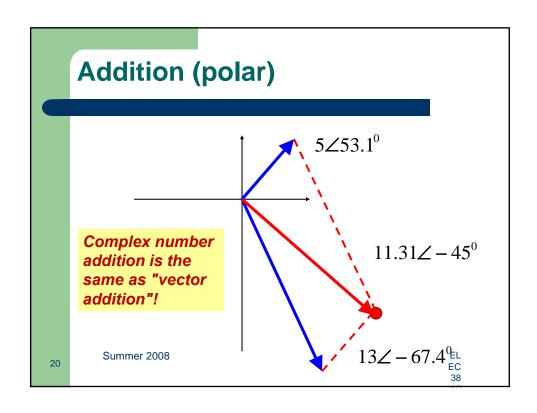
Multiplication (rectangular)

$$\overline{A} \cdot \overline{B} = (a + jb) \cdot (c + jd)$$

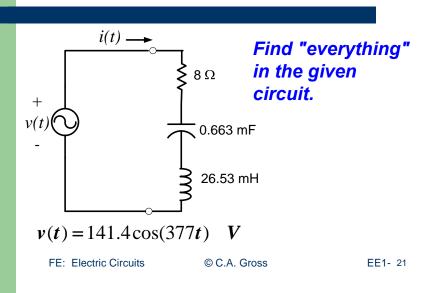
= $(ac - bd) + j(ad + bc)$
 $\overline{A} \cdot \overline{B} = (3 + j4) \cdot (5 - j12)$
= $(15 + 48) + j(-36 + 20)$
= $63 - j16 = 65 \angle -14.3^{\circ}$

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EL EC 38



3. ac Circuits



Frequency, period

$$v(t) = 141.4\cos(377t)$$
 V

(radian) frequency =
$$\omega = 377 \, rad / s$$

(cyclic) frequency =
$$f = \frac{\omega}{2\pi} = 60 \text{ Hz}$$

$$Period = \frac{1}{f} = \frac{1}{60} = 16.67 \ ms$$

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The ac Circuit

To solve the problem, we convert the circuit into an "ac circuit":

$$R, L, C$$
 elements $\rightarrow \overline{Z}$ (impedance)

$$v, i \text{ sources } \rightarrow \overline{V}, \overline{I} \text{ (phasors)}$$

$$R: \ \overline{Z}_R = R + j0 = 8 + j0$$

$$L: \ \overline{Z}_L = 0 + j\omega L = 0 + j(0.377)(26.53) = 0 + j10$$

$$C: \ \overline{Z}_C = 0 + \frac{1}{j\omega C} = 0 - j\frac{1}{0.377(0.663)} = 0 - j4$$

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The Phasor

$$v(t) = V_{MAX} \cos(\omega t + \alpha)$$

To convert to a phasor...
$$\overline{V} = \frac{V_{MAX}}{\sqrt{2}} \angle \alpha$$

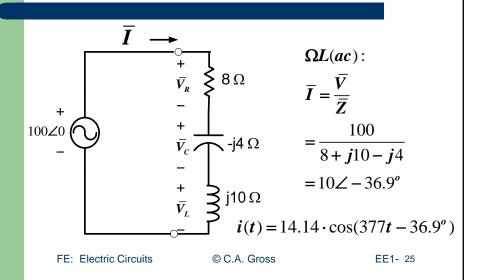
For example..
$$v(t) = 141.4\cos(377t)$$

$$\overline{V} = \frac{V_{MAX}}{\sqrt{2}} \angle \alpha = 100 \angle 0^{\circ}$$

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The "ac circuit"



Solving for voltages

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$$\begin{split} \overline{V}_R &= \overline{Z}_R \cdot \overline{I} = (8)(10 \angle - 36.9^{\circ}) = 80 \angle - 36.9^{\circ} V \\ v_R(t) &= 113.1 \cdot \cos(377t - 36.9^{\circ}) \\ \overline{V}_C &= \overline{Z}_C \cdot \overline{I} = (-j4)(10 \angle - 36.9^{\circ}) = 40 \angle - 126.9^{\circ} V \\ v_C(t) &= 56.57 \cdot \cos(377t - 126.9^{\circ}) \\ \overline{V}_L &= \overline{Z}_L \cdot \overline{I} = (j10)(10 \angle - 36.9^{\circ}) = 100 \angle 53.1^{\circ} V \\ v_L(t) &= 141.4 \cdot \cos(377t + 53.1^{\circ}) \end{split}$$

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Absorbed powers $\overline{S} = \overline{V} \cdot \overline{I}^* = P + jQ$

$$\begin{split} \overline{S}_R &= \overline{V}_R \cdot \overline{I}^* = 80 \angle -36.9^o (10 \angle -36.9^o)^* = 800 + j0 \\ \overline{S}_C &= \overline{V}_C \cdot \overline{I}^* = 40 \angle -126.9^o (10 \angle -36.9^o)^* = 0 - j400 \\ \overline{S}_L &= \overline{V}_L \cdot \overline{I}^* = 100 \angle 53.1^o (10 \angle -36.9^o)^* = 0 + j1000 \\ \overline{S}_{TOT} &= \overline{S}_R + \overline{S}_C + \overline{S}_L = 800 + j600 \\ P_{TOT} &= 800 \text{ watts;} \qquad Q_{TOT} = 600 \text{ var s;} \\ S_{TOT} &= |\overline{S}_{TOT}| = 1000 \text{ VA} \end{split}$$

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Delivered power

$$\overline{S}_{S} = \overline{V}_{S} \cdot \overline{I}^{*} = 100 \angle 0^{\circ} (10 \angle -36.9^{\circ})^{*} = 800 + \mathbf{j}600$$

$$\overline{S}_{S} = \overline{S}_{TOT} = 800 + \mathbf{j}600$$

$$P_{S} = P_{TOT} = 800 \text{ watts}$$

$$Q_{S} = Q_{TOT} = 600 \text{ var s}$$

In General:
$$P_{ABS} = P_{DEV}$$
 $Q_{ABS} = Q_{DEV}$ (Tellegen's Theorem)

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The Power Triangle
$$\overline{S} = 800 + j600$$

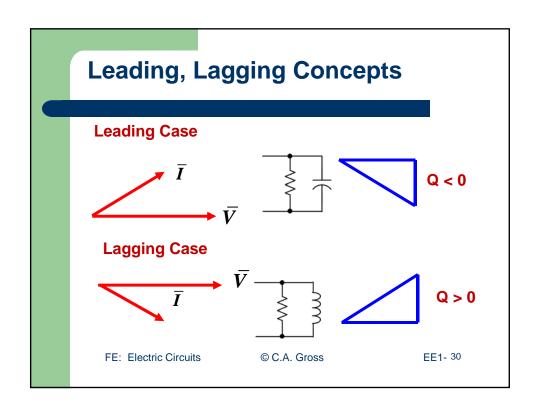
$$S = 1000 \text{ VA}$$

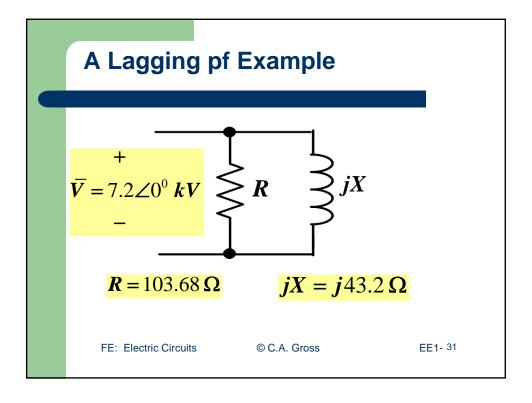
$$Q = 600 \text{ var}$$

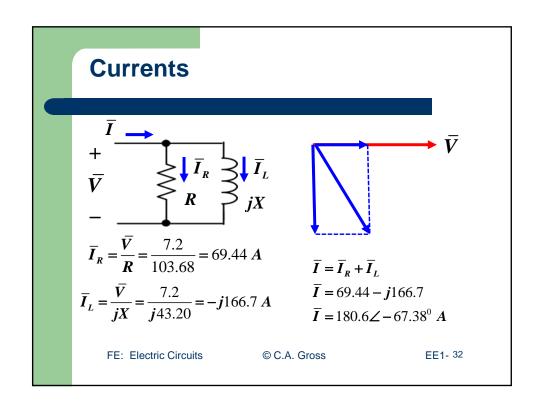
$$\overline{V} = 100 \angle 0^{\circ}$$

$$\overline{I} = 10 \angle -36.9^{\circ}$$

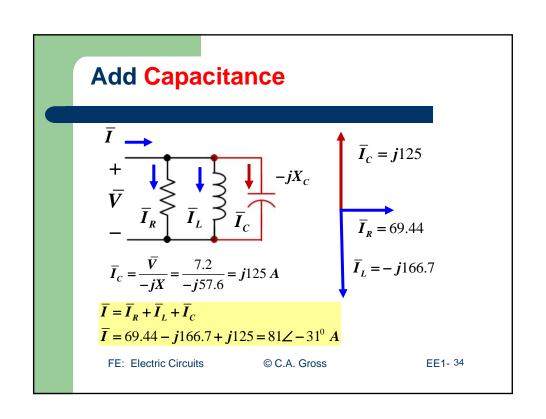
$$\overline{I}$$

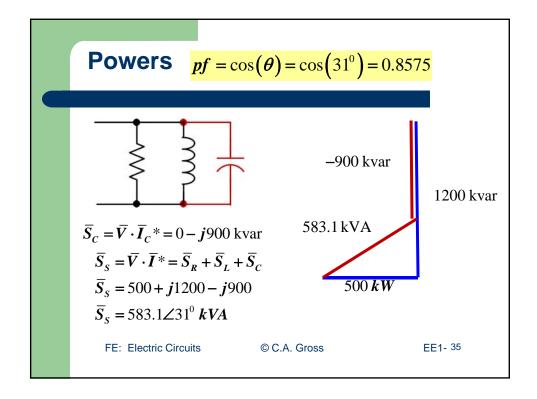






Powers
$$pf = \cos(\theta) = \cos(67.36^{\circ}) = 0.3845$$
 $\downarrow I$
 $\downarrow I$





Observations

By adding capacitance to a lagging pf (inductive) load, we have significantly reduced the source current., without changing P!

Before I = 180.6 A; pf = 0.3845

After I = 81 A; pf = 0.8575

Note that: low pf, high current; high pf, low current;

If we consider the "source" in the example to represent an Electric Utility, this reduction in current is of major practical importance, since the utility losses are proportional to the square of the current.

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Observations

That is, by adding capacitance the utility losses have been reduced by almost *a factor of 5!* Since this results in significant savings to the utility, it has an incentive to induce its customers to operate at high pf.

This leads to the "Power Factor Correction" problem, which is a classic in electric power engineering and is extremely likely to be on the FE exam.

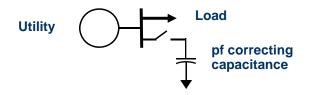
We will be using the same numerical data as we did in the previous example. Pretty clever, eh' what?

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The Power Factor Correction problem



An Electric Utility supplies 7.2 kV to a customer whose load is 7.2 kV 1300 kVA @ pf = 0.3845 lagging. The utility offers the customer a reduced rate if he will "correct" ("improve" or "raise") his pf to 0.8575. Determine the requisite capacitance.

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PF Correction: the solution

1. Draw the load power triangle. 1300 kVA @ pf = 0.3845 lagging.

$$pf = 0.3845 = \cos(\theta)$$

$$\theta = 67.38^{\circ}$$

1200 kvar

$$\bar{S}_{LOAD} = S \angle \theta = 1300 \angle 67.38^{\circ}$$

$$\overline{S}_{LOAD} = 500 + j1200$$

Because the pf is lagging, the load is inductive, and Q is positive. Therefore we must add negative Q to reduce the total, which means we must add capacitance.



500 kW

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PF Correction: the solution

2. We need to modify the source complex power so that the pf rises to 0.8575 lagging.

$$pf = 0.8575 = \cos(\theta)$$

Closing the switch (inserting the capacitors)

$$\overline{S}_S = 500 + j1200 - jQ_C = 500 + j(1200 - Q_C)$$

Let
$$Q_X = 1200 - Q_C$$

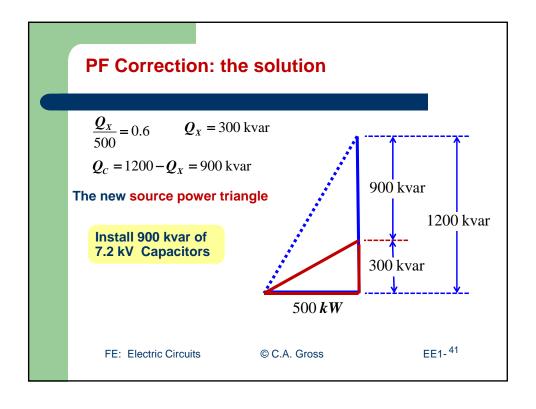
Therefore
$$\overline{S}_s = 500 + jQ_x = S_s \angle 31^0 \text{ kVA}$$

Then
$$Tan(\theta) = \frac{Q_x}{500} = Tan(31^0) = 0.6$$

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 $\theta = 31^{\circ}$

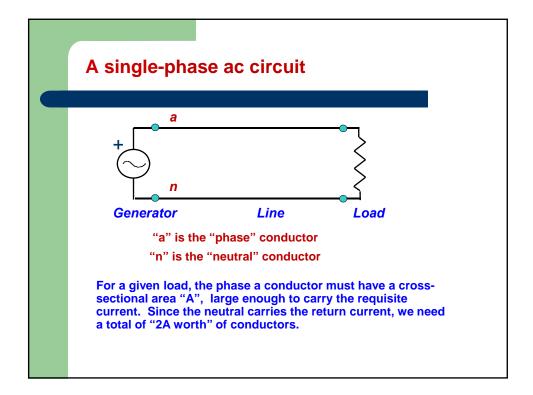


4. Three-phase ac Circuits

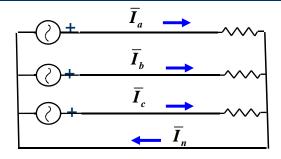
Although essentially all types of EE's use ac circuit analysis to some degree, the overwhelming majority of applications are in the high energy ("power") field.

It happens that if power levels are above about 10 kW, it is more practical and efficient to arrange ac circuits in a "polyphase" configuration. Although any number of "phases" are possible, "3-phase" is almost exclusively used in high power applications, since it is the simplest case that achieves most of the advantage of polyphase.

It is virtually certain that some 3-phase problems will appear on the FE and PE examinations, which is why 3-phase merits our attention.



Tripling the capacity



If
$$\overline{I}_a = \overline{I}_b = \overline{I}_c = I \angle \theta$$
 then $\overline{I}_n = 3I \angle \theta$

We need a total of A + A + A + 3A = 6A conductors.

But what if the currents are not in phase?

Suppose
$$\overline{I}_a = I \angle 0^0$$
 $\overline{I}_b = I \angle -120^0$ $\overline{I}_c = I \angle +120^0$

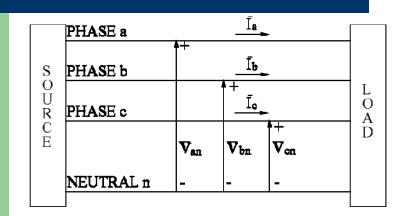
Then

$$\begin{split} \overline{I}_n &= \overline{I}_a + \overline{I}_b + \overline{I}_c = I \angle 0^0 + I \angle -120^0 + I \angle +120^0 \\ \overline{I}_n &= I \Big[\Big(1 + j0 \Big) + \Big(-0.5 - j0.866 \Big) + \Big(-0.5 + j0.866 \Big) \Big] \\ \overline{I}_n &= I \Big[\Big(1.0 - 0.5 - 0.5 \Big) + j(0.0 - 0.866 + 0.866 \Big) \Big] = I(0 + j0) = 0 \end{split}$$

Now we only need a total of A + A + A + 0 = 3A conductors!

A 50% savings!

The 3-Phase Situation



"PHASE" CONDUCTORS ARE ALSO CALLED "LINES"

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"Balanced" voltage means equal in magnitude, 120° separated in phase

$$v_{an}(t) = V_{\text{max}} \cos(\omega t) = \sqrt{2} \cdot V \cdot \cos(\omega t)$$

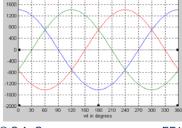
$$v_{bn}(t) = V_{\text{max}} \cos(\omega t - 120^{\circ}) = \sqrt{2} \cdot V \cdot \cos(\omega t - 120^{\circ})$$

$$v_{cn}(t) = V_{\text{max}} \cos(\omega t + 120^{\circ}) = \sqrt{2} \cdot V \cdot \cos(\omega t + 120^{\circ})$$

$$\overline{V}_{an} = V \angle 0^0$$

$$\overline{V}_{bn} = V \angle -120^{\circ}$$

$$\overline{V}_{cn} = V \angle + 120^{\circ}$$



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The "Line" Voltages

By KVL
$$\bar{V}_{ab} = \bar{V}_{an} - \bar{V}_{bn}$$

$$\overline{V}_{ab} = V \angle 0^0 - V \angle -120^0 = V \left[1 + j0 - \left(-\frac{1}{2} - j\frac{\sqrt{3}}{2} \right) \right] = V \sqrt{3} \angle 30^0$$

$$\overline{V}_{bc} = V \sqrt{3} \angle - 90^{\circ}$$

$$\overline{V}_{ca} = V \sqrt{3} \angle 150^{\circ}$$

$$V_{ab} = V_{bc} = V_{ca} = V_L = V\sqrt{3}$$

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An Example

When a power engineer says "the primary distribution voltage is 12 kV" he/she means...

$$V_{ab} = V_{bc} = V_{ca} = V_L = 12.47 \ kV$$

$$\overline{V}_{ab} = 12.47 \angle 30^{\circ} \, kV$$

$$\overline{V}_{bc} = 12.47 \angle -90^{\circ} \, kV$$

$$\overline{V}_{ca} = 12.47 \angle +150^{\circ} \, kV$$

$$V_{an} = V_{bn} = V_{cn} = \frac{V_L}{\sqrt{3}} = 7.2 \, kV$$

$$\overline{V}_{an} = V_{bn} = V_{cn} = \frac{V_L}{\sqrt{3}} = 7.2 \, kV$$

$$\overline{V}_{an} = 7.2 \angle 0^0 \, kV$$

$$\overline{V}_{bn} = 7.2 \angle -120^0 \, kV$$

$$\overline{V}_{cn} = 7.2 \angle +120^0 \, kV$$

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An Important Insight....

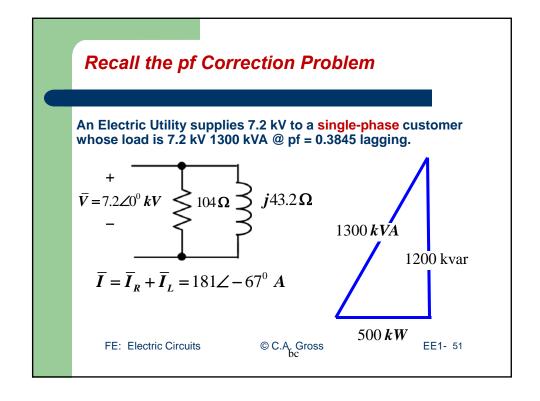
All balanced three-phase problems can be solved by focusing on a-phase, solving the single-phase (a-n) problem, and using 3-phase symmetry to deal with b-n and c-n values!

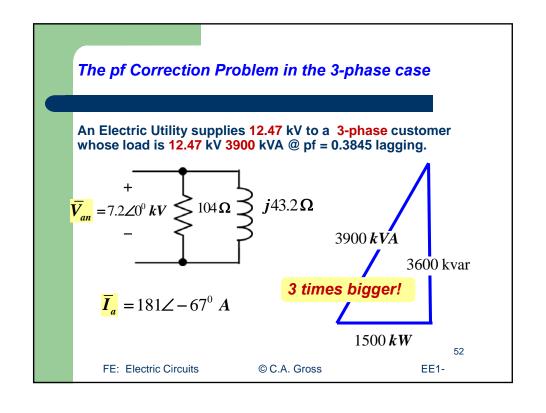
> This involves judicious use of the factors 3, $\sqrt{3}$, and 120°!

To demonstrate...

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If we want all the V's, I's, and S's

$$\overline{V}_{an} = 7.2 \angle 0^0 \ kV$$

 $\bar{V}_{ab} = 12.47 \angle 30^0 \ kV$

$$\overline{V}_{bn} = 7.2 \angle -120^0 \ kV$$

 $\overline{V}_{bc} = 12.47 \angle -90^{\circ} kV$

$$\overline{V}_{cn} = 7.2 \angle + 120^0 \ kV$$

 $\overline{V}_{ca} = 12.47 \angle + 150^{\circ} \, kV$

$$\bar{I}_{a} = 181 \angle -67^{0} A$$

 $\bar{I}_a = 181 \angle -67^0 A$ $\bar{S}_a = 500 + j1200 kVA$

$$\bar{I}_{L} = 181 \angle -187^{0} A$$

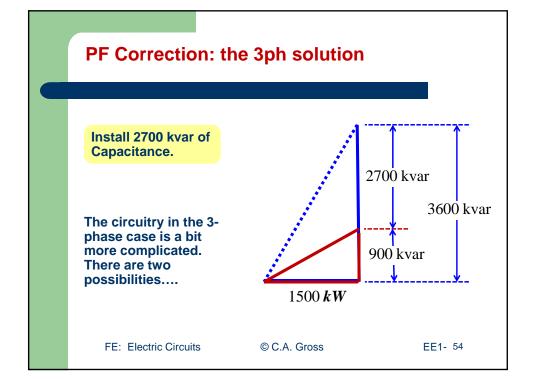
 $\bar{I}_b = 181 \angle -187^0 A$ $\bar{S}_b = 500 + j1200 \, kVA$

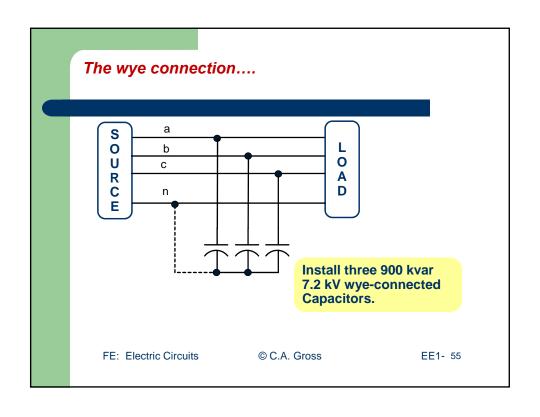
$$\bar{I} = 181 \angle + 53^{\circ} \angle$$

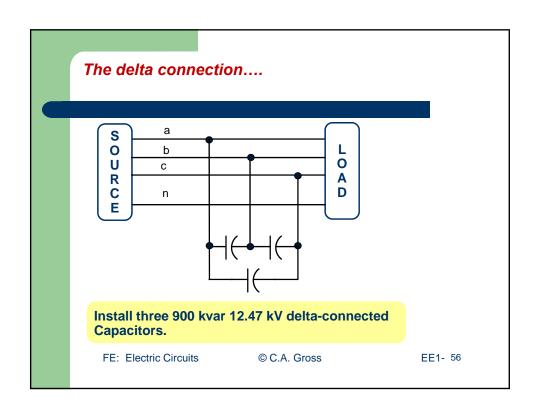
 $\bar{I}_c = 181 \angle + 53^0 A$ $\bar{S}_c = 500 + j1200 \, kVA$

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wye-delta connections

$$\bar{\mathbf{Z}}_{\Delta} = 3 \cdot \bar{\mathbf{Z}}_{Y}$$

wye case

 $Q_{an} = \frac{2700}{3} = 900 \text{ kvar}$ $Q_{an} = \frac{2700}{3} = 900 \text{ kvar}$

delta case

 $I_a = \frac{Q_{an}}{V_{an}} = \frac{900}{7.2} = 125 A$ $I_{ab} = \frac{Q_{ab}}{V_{ab}} = \frac{900}{12.47} = 72.17 A$

 $Z_{an} = Z_{Y} = \frac{V_{an}}{I_{a}} = 57.6 \Omega$ $Z_{ab} = Z_{\Delta} = \frac{12.47}{72.17} = 172.8 \Omega$ $C_{Y} = \frac{1}{\omega Z_{Y}} = 46.05 \,\mu\text{F}$ $C_{\Delta} = \frac{1}{\omega Z_{\Delta}} = 15.35 \,\mu\text{F}$

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1st Order Transients.....

Network B Network A contains contains v(t)one energy dc sources, storage resistors, element one switch (L or C)

The problem...(1) solve for v and/or i @ t < 0; (2) switch is switched @ t = 0; (3) solve for v and/or i for t > 0

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The inductive case

$$\begin{array}{c|c} \vdots & & \\ & \downarrow \\ & \downarrow \\ & \downarrow \\ & - \end{array} \right\} \quad L \qquad v_L = L \cdot \frac{di_L}{dt}$$

L's are SHORTS to dc $i_L(t)$ cannot change in zero time

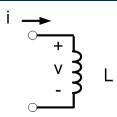
$$i_L(0^-) = i_L(0) = i_L(0^+)$$

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An Example...



$$v_{L} = L \cdot \frac{di_{L}}{dt}$$
 $i_{L}(0^{-}) = i_{L}(0) = i_{L}(0^{+})$

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$$t \le 0$$
: $v_C(t) = v_C(0)$ (constant)

$$t \to \infty$$
: $v_C(t) = v_C(\infty)$ (constant)

$$\begin{aligned} 0 &< t < \infty: & v_C(t) = v_C(\infty) + \left[v_C(0) - v_C(\infty)\right] \cdot e^{-t/\tau} \\ \tau &= R_{ab} \cdot C \end{aligned}$$

Our job is to determine

$$\mathbf{v}_{C}(0); \quad \mathbf{v}_{C}(\infty); \quad \text{and } \mathbf{\tau} = \mathbf{R}_{ab} \cdot \mathbf{C}$$

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EE1- 61

Solution....

For a

capacitor:
$$i_C = C \cdot \frac{dv_C}{dt}$$

C's are OPENS to dc

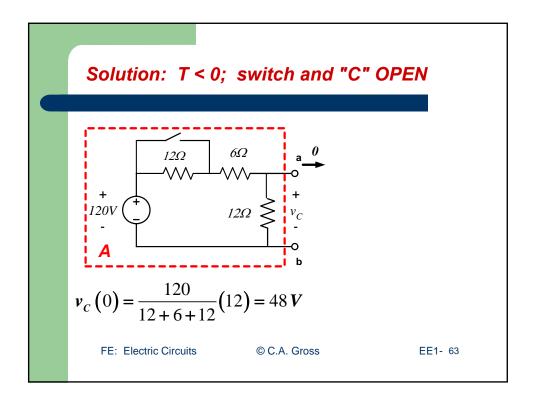
 $v_c(t)$ cannot change in zero time

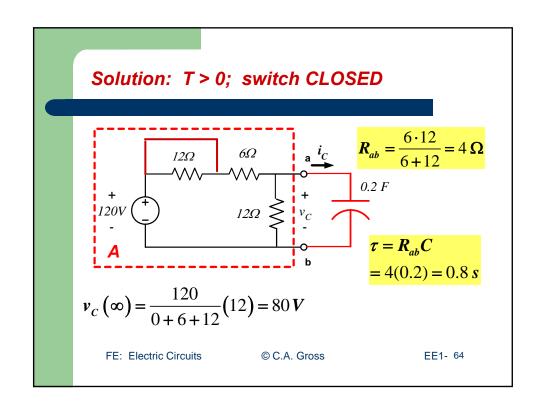
Therefore, if the circuit is switched at t = 0:

$$\mathbf{v}_C(0^-) = \mathbf{v}_C(0) = \mathbf{v}_C(0^+)$$

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$$v_C(0) = 48 \quad v_C(\infty) = 80$$

$$t > 0$$
: $v_C(t) = 80 + (48 - 80) \cdot e^{-1.25t}$

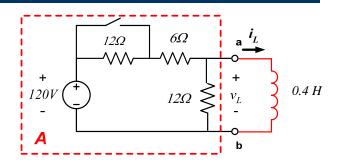
$$v_C(t) = 80 - 32 \cdot e^{-1.25t}$$

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3. 1st Order Transients: RL



b. The switch is closed at t = 0. Find and plot $i_L(t)$.

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$$t \le 0$$
: $i_L(t) = i_L(0)$

$$t>0: \qquad i_L(t)=i_L(\infty)+\left[i_L(0)-i_L(\infty)\right]\cdot e^{-t/\tau}$$

$$\tau = \frac{L}{R_{ab}}$$

Our job is to determine

$$i_L(0); \quad i_L(\infty); \quad \text{and } \tau = L / R_{ab}$$

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Solution....

For an inductor:

$$v_L = L \cdot \frac{di_L}{dt}$$

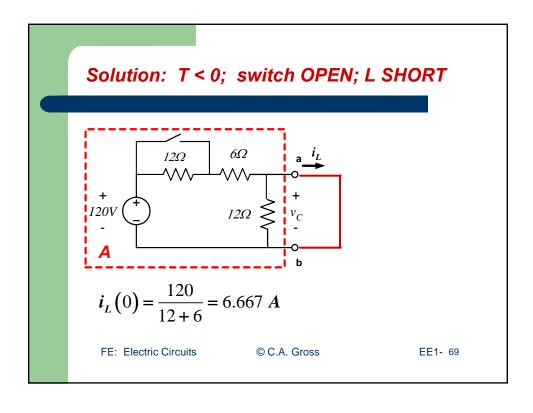
L's are SHORTS to dc

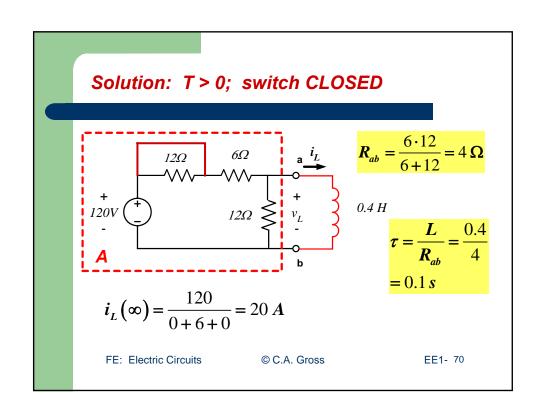
 $i_L(t)$ cannot change in zero time

$$i_L(0^-) = i_L(0) = i_L(0^+)$$

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 $t \le 0$: $i_L(t) = 6.667$

t > 0: $i_L(t) = 20 + (6.667 - 20) \cdot e^{-t/\tau}$

 $i_L(t) = 20 - 13.33 \cdot e^{-10t}$

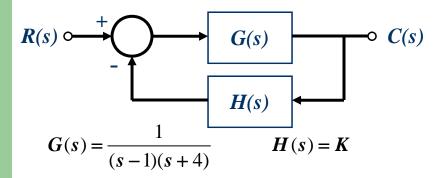
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5. Control

Given the following feedback control system:



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a. Write the closed loop transfer function in rational form

$$\frac{C}{R} = \frac{G}{1 + GH} = \frac{\frac{1}{(s-1)(s+4)}}{1 + \frac{K}{(s-1)(s+4)}}$$

$$\frac{C}{R} = \frac{1}{(s-1)(s+4) + K} = \frac{1}{s^2 + 3s + (K-4)}$$

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b. Write the characteristic equation

$$s^2 + 3s + (K - 4) = 0$$

- c. What is the system order? 2
- d. For K = 0, where are the poles located?

$$s^{2} + 3s - 4 = (s - 1) \cdot (s + 4) = 0$$

$$s = +1$$
; $s = -4$

e. For K = 0, is the system stable?

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f. Complete the table $s^2 + 3s + (K - 4) = 0$

Roots of the CE are poles of the CLTF

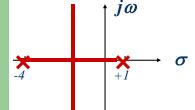
K	poles	damping
0	- 4.00, +1.00	unstable
4	-3.00, 0.00	over
5	-2.62, -0.382	over
6.25	-1.50, -1.50	critical
10.25	-1.5 - j2, -1.5 + j2	under

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f. Sketch the root locus



g. Find the range on K for system stability.

If K = 4:

$$s^2 + 3s + 0 = (s) \cdot (s+3) = 0$$

Poles at s = 0; s = -3

Therefore for K>4, poles are in LH s-plane and system is stable.

K ≥ 4

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h. Find K for critical damping

$$CE:$$
 $s^2 + 3s + (K - 4) = 0$

Solving the CE:
$$s = \frac{-3 \pm \sqrt{9 - 4(K - 4)}}{2}$$

Critical damping occurs when the poles are real and equal

$$\sqrt{9-4(K-4)}=0$$

$$K - 4 = 9/4$$
;

$$K = 4 + 2.25 = 6.25$$

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6. Signal Processing

- a. periodic time-domain functions have continuous discrete frequency spectra.

 (circle the correct adjective)
- b. aperiodic time-domain functions have continuous discrete frequency spectra.

 (circle the correct adjective)

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c. Matching

Laplace Transform

Fourier Transform

Fourier Series Inverse FT

Convolution integral **b**

a.
$$x(t) = \sum_{n=-N}^{N} \overline{D}_n \exp(jn\omega_0 t)$$

b.
$$y(t) = \int_{0}^{t} x(\tau) \cdot h(t - \tau) \cdot d\tau$$

b.
$$y(t) = \int_{-\infty}^{t} x(\tau) \cdot h(t-\tau) \cdot d\tau$$
 c. $\overline{X}(j\omega) = \int_{-\infty}^{\infty} x(t) \cdot e^{-j\omega t} \cdot dt$

d.
$$X(s) = \int_{0}^{\infty} x(t) \cdot e^{-st} \cdot dt$$

d.
$$X(s) = \int_{0}^{\infty} x(t) \cdot e^{-st} \cdot dt$$
 e. $x(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \overline{X}(j\omega) \cdot e^{+j\omega t} \cdot d\omega$

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c. Matching

Z-Transform



Inverse ZT

Discrete Convolution **b**

Inverse DFT

a.
$$\overline{X}(j\Omega) = \sum_{n=-\infty}^{\infty} x[n] \cdot e^{-jn\Omega}$$

b.
$$y[k] = \sum_{n=-\infty}^{k} x[n] \cdot h[n-k]$$

b.
$$y[k] = \sum_{n=-\infty}^{k} x[n] \cdot h[n-k]$$
 c. $\overline{X}_k = \sum_{n=0}^{N-1} x[n] \cdot e^{-j2\pi kn/N}$

d.
$$X(z) = \sum_{n=0}^{\infty} x[n] \cdot z^{-n}$$

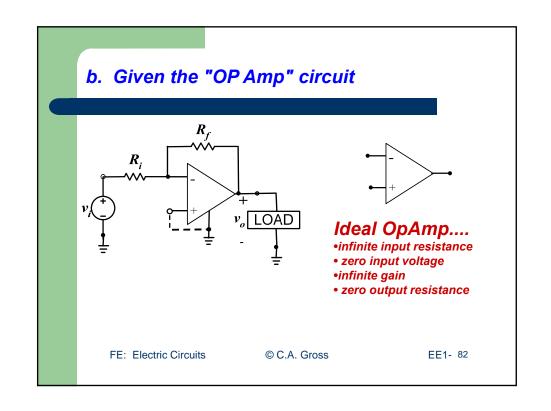
d.
$$X(z) = \sum_{n=0}^{\infty} x[n] \cdot z^{-n}$$
 e. $x[n] = \frac{1}{N} \sum_{k=0}^{N-1} \overline{X}_k \cdot e^{+j2\pi kn/N}$

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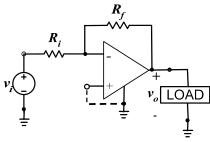
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7. Electronics
$$e(t) = 169.7 \cdot \sin(\omega t)$$
a. Darken the conducting diodes at time T

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Find the output voltage.



$$v_i = 5V$$

$$R_i = 10 k\Omega$$

$$R_f = 50 k\Omega$$

$$\mathbf{v}_0 = -\left(\frac{50}{10}\right) \cdot 5 = -25 \,\mathbf{V}$$

$$KCL: \frac{\mathbf{v}_{i}}{\mathbf{R}_{i}} + \frac{\mathbf{v}_{0}}{\mathbf{R}_{f}} = 0$$

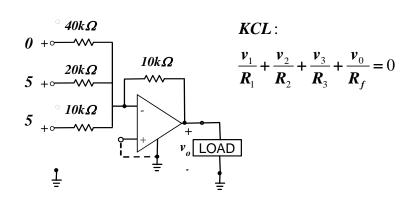
$$\mathbf{v}_{0} = -\left(\frac{\mathbf{R}_{f}}{\mathbf{R}_{i}}\right) \cdot \mathbf{v}_{i}$$

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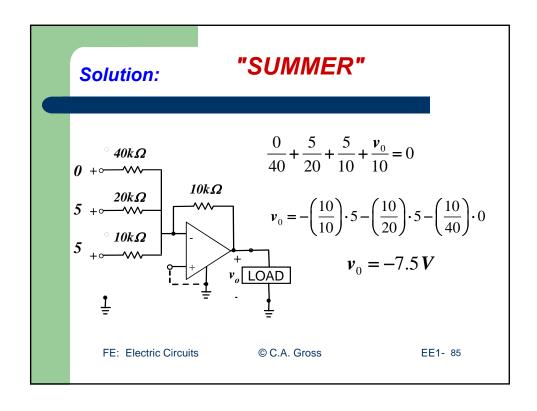
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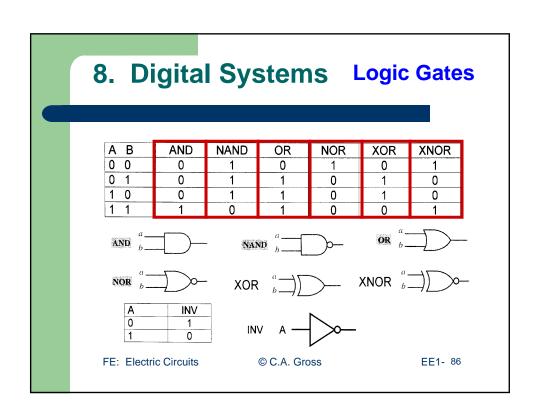
c. Find the output voltage.

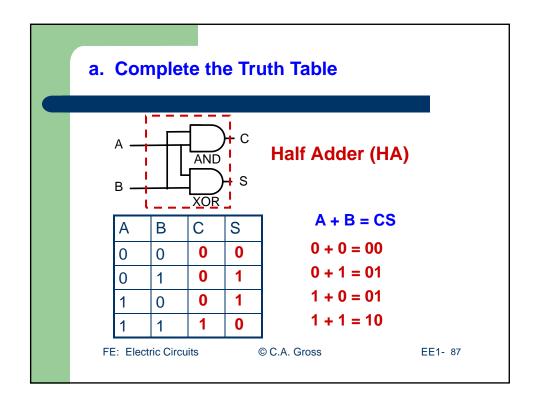


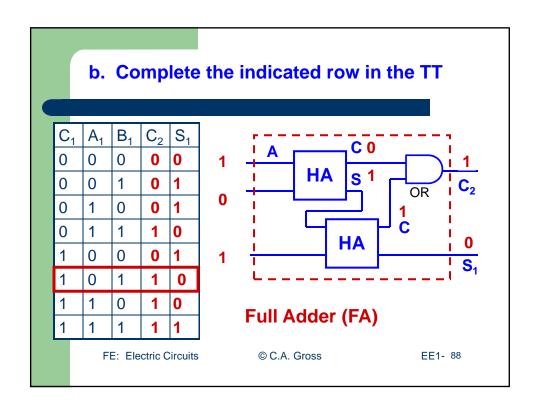
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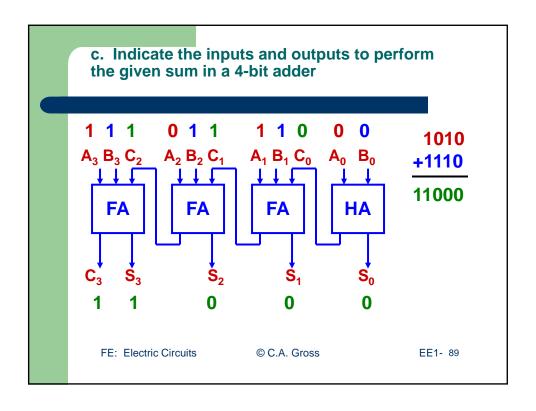
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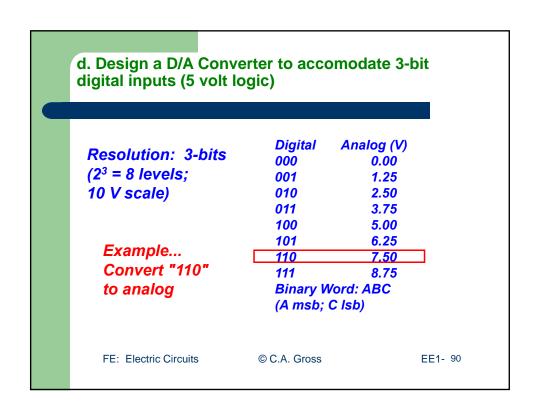


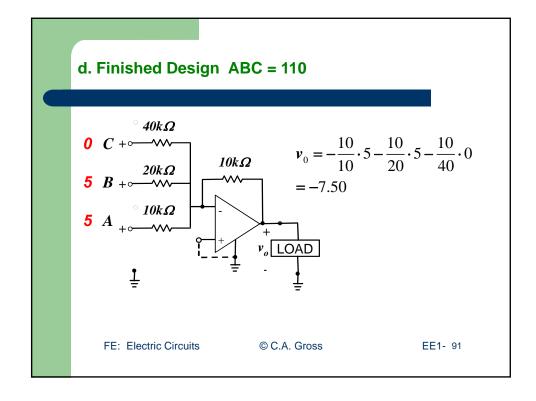












Good Luck on the Exam!

If I can help with any ECE material, come see me (7:30 - 11:00; 1:15 - 2:30)

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Good Evening...

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