### Politecnico di Torino Bachelor degree in Computer Engineering

AUTOMATIC CONTROL - (06LSL<sub>LM</sub> - 06LSL<sub>OA</sub>)

Surname id PC

### **Exam simulation**

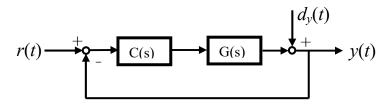
### Part I (6 points)

Solve the proposed exercises and write the answers in the table below. For every correct answer, 3 points are added. For every wrong answer, a penalty corresponding to 1 point is subtracted. Every omitted answer leads to a null score. Please provide the correct numerical computations and/or reasoning needed for the answer (otherwise a null score is given).

Exercise	1	2
Answer		

#### Exercise 1

Consider the feedback control system below:



Where: 
$$G(s) = \frac{1}{s^2 + 9s - 10}$$
,  $d_y(t) = \delta \varepsilon(t)$ ,  $|\delta| \le 0.2$ .

Design a steady state controller C<sub>SS</sub>(s) in order to meet the following requirements:

- 
$$|e_r^{\infty}| \le 0.5$$
 for  $r(t) = 0.2 t$   
-  $|y_{d_y}^{\infty}| \le 0.25$ .

A) 
$$C_{SS}(s) = \frac{4}{s}$$

B) 
$$C_{SS}(s) = -\frac{4}{s}$$

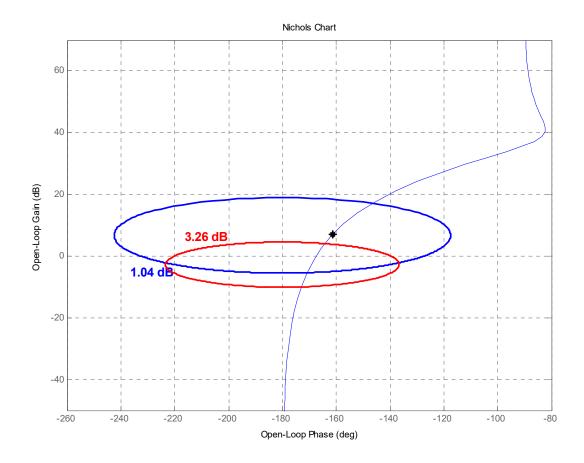
C) It is not possible to design C<sub>SS</sub>(s) since after the steady state step the closed loop system is not stable.

$$D) C_{SS}(s) = \frac{2}{s}$$

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### Exercise 2

After the steady state design step, the Nichols plot of the loop function L(s) of a unitary feedback system shows the course reported in the Figure below. (The asterisk indicates the point corresponding to the desired crossover frequency  $\omega_{c,des}$ )



Which of the following controller function can be reasonably employed in order to satisfy the frequency domain requirements described by the reported constant magnitude loci and the desired crossover frequency.

- A) A lead-lag network
- B) A lag network only
- C) A PI controller only
- D) More than one among the other reported answers is correct.

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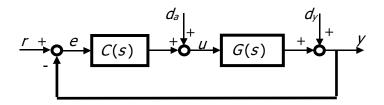
### Part II (10 points)

Choose and develop one (only) of the following subjects. (The second subject is on the next page)..

1 - Show that an LTI dynamical system is internally asymptotically stable iff all its natural modes are convergent.

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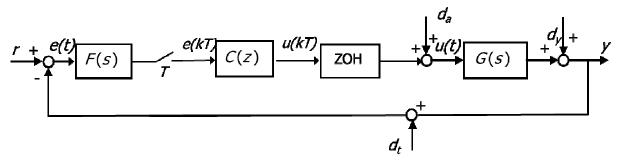
**2** – Show that, in the feedback control system structure below (supposed stable), the condition  $\left|\mathcal{Y}_{d_a}^{\infty}\right| = 0$  when  $d_a(t)$  is constant, is achieved either when C(s) contains a pole at the origin or when G(s) contains a zero at the origin.



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### Part III (17 points)

Consider the feedback control structure below.



Where

$$G(s) = \frac{3.3 \cdot 10^4}{s^2} \quad d_a(t) = \delta_a \varepsilon(t), |\delta_a| \le 0.2 \quad d_y(t) = \delta_y(1 + \sin(\omega_y t)), |\delta_y| \le 0.5, \ \omega_y \le 240 \,\text{rad/s}$$

Assume a sampling time  $T_s = 4.5 \cdot 10^{-5} s$ , design a digital controller C(z) in order to meet the following requirements:

- $|y_{d_a}^{\infty}| \le 0.0125$
- $\left| y_{d_v}^{\infty} \right| \le 0.5 \cdot 10^{-2}$
- $\hat{S} \leq 16\%$ ;
- $t_{s,2\%} \le 0.002 \text{ s}$
- $\max_{t} |u(t)| \le 6$  in the presence of a step reference signal with amplitude 0.001

At the end of the design evaluate, through simulation, the maximum value of the controlled output y(t) when both a step reference signal with amplitude 0.001 and the input disturbance  $d_a(t)$  are acting on the system.

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Set MatLab path >> cd D:\

Steady state requirements analysis and design (4 points, <u>quit</u> the exercise evaluation in the presence of either a "destabilizing" steady state controller or the wrong type of the control system)

# $\label{eq:control} Politecnico \ di \ Torino \\ Bachelor \ degree \ in \ Computer \ Engineering \\ \textit{AUTOMATIC CONTROL} - (06LSL_{LM} \ - \ 06LSL_{OA})$

Report the expression	of the steady state controller in the form	$_{1}C_{SS}(s) = \frac{K_{c}}{s^{h}}, K_{c} =, h =$

$$C_{SS}(s) =$$

**Transient and other requirements analysis** (2 points)

### **Design procedure description** (5 points)

Please resume and deeply motivate all the design steps performed to obtain the final controller.

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Report the expression of the final analog controller in the dc-gain form

(e.g. 
$$C_0(s) = \frac{K_c}{s^r} \frac{1 + s / \omega_D}{1 + s / (m_D \omega_D)}, K_c = ..., r = ..., \omega_D = ..., m_D = ..., this is only an example!!!!)$$

(If the expression of  $C_0(s)$  is missing: quit the exercise evaluation. -1 point if provided in the wrong form

$$C_0(s) =$$

Report the expression of the final digital controller in the polynomial form

$$C_d(z) =$$
 discretization method

Details on the Butterworth anti-aliasing filter (if designed and not needed: -2 points)

$$\omega_h$$
 =  $\gamma$  =  $\omega_f$  =  $\eta$  =

#### **Performance evaluation** (5 points)

Use simulation in order to evaluate the achieved performance.

(0,5 each correct evaluation, 0 if the evaluation is wrong or missing

0,5 if the requirement has been satisfied (within 5%),

0 for each unsatisfied requirement with an error > 5%

-0,5 for each unsatisfied requirement with an error > 15%

-1 for each unsatisfied requirement with an error > 30%)

- 
$$\left| y_{d_a}^{\infty} \right| =$$

- 
$$\left|y_{d_{y}}^{\infty}\right| =$$

$$\hat{S} =$$

$$- t_{s,2\%} =$$

- 
$$\max_{t} |\mathbf{u}(t)| =$$

in the presence of a step reference signal with amplitude 0.001

#### Final evaluation after design

(1 point if the evaluation is correct within 10%, 0 point if it is wrong or missing)

$$\max_{t} |y(t)| =$$

Save results >> save Results\_AC\_s123456 G CO Ts Cd F (-3 if not done)