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import Figure from "@site/src/components/Figure"; import FigRefer-
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zontal from "@site/src/components/TableHorizontal"; import TableRef-
erence from "@site/src/components/TableReference"; import Citation
from "@site/src/components/Citation"; import CitationFootnote from
"@site/src/components/CitationFootnote"; import NavAndPrint from
"@site/src/components/NavAndPrint"; import Link from "@docusaurus/Link";
import { addBaseUrl } from "@docusaurus/useBaseUrl";
```

## Constricted Exit

Constricted, or non-erodible, exits consist of open joints, defects, or cracks in conduits, drains, walls, or rock. For erosion to continue, the opening size must be sufficient for the adjacent base soil particles to pass through it. This worksheet assesses the joint/defect opening size that allows erosion to continue.

### Base Soil Characterization

Step 1 characterizes the base material. The range of  $D_{95B}$  of the base soil adjacent to the open joint, defect, or crack is obtained from the Base Gradation worksheet, where the finest and coarsest  $D_{95B}$  of the adjacent base soil after regrading (if applicable) are interpolated using a logarithmic scale for particle size and linear scale for percent passing. is an example of step 1.

### Open Joint, Defect, or Crack Characterization

Step 2 characterizes the open joint, defect, or crack, and the joint/defect opening size ( $JOS$ ) is input. The user-specified  $JOS$  and range of  $D_{95B}$  of the adjacent base soil are portrayed on a cumulative particle-size plot to visually compare their relative sizes, as shown in . The y-axis (percent passing by weight) is truncated at 90 percent passing since only the particle-size diameter corresponding to 95 percent passing is used in the evaluation. The size of the open joint, defect, or crack is depicted with a vertical back line at the  $JOS$  and horizontal lines that extend infinitely smaller since a logarithmic scale is used. The range of  $D_{95B}$  displays as a red horizontal line.

The plot options for this chart are illustrated in . The minimum and maximum values for the x-axis (particle size) are user-specified.

### Likelihood of Continuation

Step 3 estimates the probability of continuing erosion ( $PCE$ ) using the procedure of Fell and Foster . The  $JOS$  that allows continuing erosion of the adjacent

base soil (*JOSCE*) is between *D95B* and *3D95B*. Sherard et al. concluded that uniform filters act similar to laboratory sieves with an opening sieve size approximately equal to  $\frac{D_{15}F}{9}$ . The *D95B* criterion assumes the Foster and Fell continuing erosion criterion (see section 8.4) applies to erosion into an open joint, defect, or crack, and the crack width is equivalent to the filter opening size of the voids between the particles in a filter. The *3D95B* criterion is based on the *JOS* for cement grout to penetrate and flow along the opening of joints in rock.

The probabilities shown in considered these limits. In the table, *PCE* is a function the ratio of the *JOS* to the finest *D95B* of the adjacent base soil after regrading (if applicable). If  $\frac{JOS}{D_{95}B}$  is less than 0.4, zero is displayed. If  $\frac{JOS}{D_{95}B}$  is greater than or equal to 0.4 and less than 0.5, {“<0.0001”} is displayed. Intermediate values between 0.5 and 3.0 are interpolated using a z-variate scale for probability and a linear scale for the ratio  $\frac{JOS}{D_{95}B}$ .

```
<TableHorizontal parentDocId="107" tableKey="constricted-exit-probabilities"
headers={["JOS / D95B", "PCE"]} rows={["< 0.4", "0.5", "0.75", "1.0",
"2.0", " 3.0"], // Row 1 ["0", "0.0001", "0.001", "0.1", "0.5", "0.9"] //
Row 2]} alt="Probability of continuing erosion for joint/defect opening size."
caption="Probability of continuing erosion for joint/defect opening size." />
```

According to Fell and Foster , these probabilities apply to erosion into open defects in the foundation and conduits or walls with steady flow conditions. Use higher probabilities for erosion into open defects in conduits or walls with dynamic flow conditions.

If the coarsest *D95B* of the adjacent base soil after regrading is less than or equal to the *JOS* (*coarsest D95B* = *JOS*), the proportion of the *D95B* finer than the *JOS* is 100 percent. If the finest *D95B* of the adjacent base soil after regrading is greater than or equal to the *JOS* (*finest D95B* = *JOS*), the proportion of the *D95B* finer than the *JOS* is 0 percent. If the coarsest *D95B* of the adjacent base soil after regrading (if applicable) is greater than the *JOS* and the finest *D95B* after regrading (if applicable) is less than the *JOS*, the proportion of the *D95B* finer than the *JOS* is calculated as in the following equation. is an example of step 3.

$$P_{CE} = \frac{\log_{10}(JOS) - \log_{10}(finest D_{95}B)}{\log_{10}(coarsest D_{95}B) - \log_{10}(finest D_{95}B)}$$