13/9/23

Laplace Transform

S(t) = 1

u(t)= 1/5

t= 1/82

12= 3/83

t 3= 6/84

in = n!

snt!

ext = 1/s+02

e = 1/s-x

text = 1 (S+x)2

te* = (5-x)2

tre = n:/(8+x) n+1 trext = n!/(8-x)n+1

leswt = 8/82+w2

Sinct = W/g2+w2

e Shut = w/(8+x)2+w2

e lowt = 8/(5+x)2+w2

Sinhat = 2/82-22

Coshat = 8/32-24

Proposities of LT?

1. Linearity property: Let C, C2 be constants

f(t) & g(t) are functions wish time t

then L { C, f(1) + (2 g(1)) = L { (, f(1)) + L { (2 g (1))}

a. First shifting theorems ES LLf(f)) = F(8) then

 $L\left\langle e^{tat}f(t)\right\rangle = F(s-a)$

Definition: F(8) = 5.14) e d.

3 - 0 -1 /45

For
$$n=1$$

$$L \frac{d}{dt} f(t) = \frac{3}{4} L \{f(t)\} - f(0)\}$$

$$L \frac{d^2 f(t)}{dt^2} = \frac{3^2 L}{4} \{f(t)\} - \frac{3}{4} \{f(t)\} - \frac{3}{4}$$

For n=3
$$\frac{d^{3}f(t)}{dt^{3}} = S^{3}L \left\{ f(t) - S^{2}f(0) - Sf(0) - f(0) \right\}$$

$$L\left[\iint \cdot \cdot \int f(t) dt\right] = F(s) \text{ then.}$$

$$L\left[\iint \cdot \cdot \int f(t) dt\right] = \frac{1}{s} L f(t) + \frac{s^{n-1}f(0)}{s} + \cdots + \frac{f(0)}{s}$$

5. Integralion:

6. Time shifting :
$$L\left\{f(t-T)u(t-T)\right\} = e^{-st}F(8) \quad \text{when} \quad U(t-T) \text{ is unit step.}$$

$$= L f''(f) + 3 L f'(f) + 2 L f(f),$$

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$$= L f''(f) + 2 L f(f) + 2 L f(f) + 2 L f(f),$$

$$= L f''(f) + 2 L f(f) + 2 L f(f) + 2 L f(f),$$

$$= L f''(f) + 2 L f(f) + 2$$

$$= \frac{3^{2} F(3) - 3 + 38[F(3) - 1] + 2F(3) = 0}{F(3) E 8^{2} + 38 + 27 - 3 - 38 = 0}.$$

$$F(3) = \frac{S+3}{8^{2}+38+2} = \frac{8+3}{8+1} = \frac{-3\pm\sqrt{9-8}}{8} = \frac{-3$$

11 = 3 & m 2 t

b. 28+1 =

C. 28+2 1496+5

Solve the different Paleq to dx + 9x = 12 where x(0+) = 1

A system as suffresented by the relation $t(B) = R(S) = \frac{120}{S^2 + 5s + 10}$ where R(S) is the L7 of unit step fn. Find the value of $\chi(H)$ out $H \to \infty$

→ X(3) 2 1 120 Hint; Use inetial value theorem.

Fourier transformer

Enveux Fourier tuans fours:

$$f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} F(\omega) e^{\int_{-\infty}^{\infty} d\omega}$$

Laplace transform Fourier transform.

The LT of fr x(t) can be represented as a continuous sum of refronential damped wave of form est

- . The FT of An A(E) can be suffree entered by a continuous sur of exp fins of the form, of effect
- · LT is applied for solving DES that Suchate 1/P & 0/P of the system
- . LT can be used to analyze unitable system
- . Does not suquem ef a for oblined for a set of regative numbers
- Li easts for every for with a FT
- LT is widely used for solving DE. sink It exists even for signaly for which FT does not exist

- · FT is applied for solving Dts that elace Elo & old of the sys
- . FT cannot be used to analyze unitable systems.
- · Only defined for In that are defined for all sual numbers.
- · It is not always true that every for with a LT has a FT.
- · at is really used for solving DE since FT does not exest for many signor En x(E) as it is not absolutely integray

Purporties of FT &

· Lineaui ty:

Time scalingin

Time differentiation:

If
$$F(w) = F[f(t)]$$
 then $F[f'(t)] = fwF(w)$
In general, $F[f'(t)] = (fw)^n F(w)$

Time sheftengs

Time Integrations

F. Reversal

If
$$f(\omega) = f(JA)$$

Fiffett = $f(\omega)$

Fifett = $f(\omega)$

Fifett

1.
$$f''(t)$$
; $g(t+1) - 2g(t) + g(t-1)$
 $\Rightarrow (fw)^2 F(w) = e^{fw} - 2 + e^{fw}$
 $\Rightarrow (gw)^2 - 2$
 $(fw)^2$
 $\Rightarrow 2(1 - (gw))$
 $= 2(1 - (gw))$
 $=$

$$S = -2 \Rightarrow -16 = 4A \Rightarrow A = -8$$

 $S = -4 \Rightarrow -36 = -2B \Rightarrow B = 18$

$$S = -4 \Rightarrow -36 = -28 \Rightarrow B = 18$$

$$\frac{106 + 1}{1200} = \frac{-8}{642} + \frac{18}{18}$$

$$\frac{106H_{4}}{2} = \frac{-8}{(10)} + \frac{18}{(10)}$$

$$\frac{106H_{1}}{6211018} = \frac{-8}{642} + \frac{18}{642}$$

$$\frac{108 + 4}{5^2 + 68 + 8} = \frac{-8}{(5 + 2)} + \frac{18}{(5 + 4)} = \left[-8e + 18e^{-4 + 1} \right] u(1)$$

$$\frac{108 + 14}{5^2 + 68 + 8} = \frac{-8}{(5+2)} + \frac{1}{(5+2)}$$

$$5 - 6(w) = w^{2} + 21 = x$$

25 9123

}k ⇒ł

B - 300

Im -> Mar

3.
$$G(w) = \frac{w^2+2i}{w^2+9} = \frac{x^2}{w^2}$$

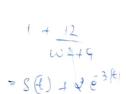
= 108+4

8288+8

(5+2) (5+4)

= 105+4





b) July b, No falution

 $K_{1} = -\frac{k_{1}}{k_{2}} = -\frac{k_{1}}{k_{1}} - \frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{2} = -\frac{k_{1}}{k_{2}} - \frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{1} = -\frac{k_{1}}{k_{1}} - \frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{2} = -\frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{3} = -\frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{1} = -\frac{k_{1}}{k_{1}} - \frac{k_{2}}{k_{2}} \left(\frac{1}{2} - \frac{1}{2} \right) - \frac{1}{2} \cdot \frac{1}{2}$ $K_{1} = -\frac{k_{1}}{k_{1}} - \frac{1}{2} \cdot \frac{1}$

C) J. KI M. M. F. K. M. F. M.

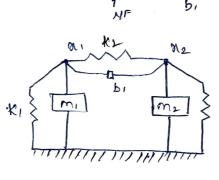
 $m_{1}\frac{d^{2}x_{1}}{olt^{2}} = -k_{1}x_{1} - k_{2}(x_{1} - t_{2}) - b_{1}\left(\frac{dx_{1}}{olt} - \frac{dx_{2}}{olt}\right)$ $m_{2}\frac{d^{2}x_{2}}{olt^{2}} = F - k_{2}(x_{2} - x_{1}) - b_{1}\left(\frac{dx_{2}}{olt} - \frac{dx_{2}}{olt}\right)$

I write the DF for the mechanical sys shown below. Given that there

are no initial conditions for both masses.

K, 1-1/2, K2 1-1/2 k,

m, 1/2 m2 1/2 k,



 $m_1 \frac{d^2 x_1}{o t^2} = -k_1 x_1 - k_2 \left(x_1 - x_2 \right) - b_1 \left(\frac{d x_1}{o t} - \frac{d x_2}{o t} \right)$ $m_2 \frac{d^2 x_2}{o t^2} = K_2 \left(x_1 - x_2 \right) - b_1 \left(\frac{d x_1}{o t} - \frac{d x_2}{o t} \right) - k_1 x_2$

In me any mechanical sys, there is flexibility blue one partiand another fig. 3 deficts such a situation, where a force v is applied to the mass m and another mass m is connected to it. The coupling blue the effects is often modellinged by spring const- k with a damping couple be although the actival situation is resually much mode complicated than this

b Find the to for bus the control Elp v & olf y.

Y= (m82+68+K)u

012 M 023 + K (3-2) + P (34 - 92) k(2-y) + b d(2-y) = md2x

Taking Laplace Triansform: U(3) = M32 y(3) + K(y(8) - x(3)) + 62(y-x)

K(x(3)-7(3)) + b,8(x-y) = m8+x(3) (-K-bs)x(3) + (Ms2+K+bs)y(3)2 U(s)

(m82-K-65) x(8) + (K+65) y(8) = 0,00 (raner's rule:

(m 52+b3+kx (k+b3)) -(E 3+K) xx (k+b3) -(E 3+K)U (m 52+b3+K) (m 82+h8+k) 1 (b8+k) = mMS + Mb83+ M82k + bms 3+6283+b8k+ mk82

(m 82+68+K) (M82+68+K) -(K+6812 η ε (m 82+68+k) (W87+ P8+K) (W8+4P8+K) - (K+P8)3

6K8+K2 - (682+K2+268K)

4. White the eggs of a motion of a fundalum consisting of a try stick of length L suspended from pivot. How long should the tool be in order for the period to be exactly essess HINT: NOTE: The intented I of a thin stick about an end pointies 1 M12. Assume o is small enough that sino x o

$$F = 200$$

$$M = -mg \sin \theta \frac{1}{2} = \frac{1}{3} ml^{2} \frac{d^{2}\theta}{dt^{2}} = \frac{1}{3} ml^{2} \frac{d^{2}\theta}{dt^{2}}$$

$$-mg \frac{1}{3} \sin \theta = \frac{1}{3} ml^{2} \frac{d^{2}\theta}{dt^{2}}$$

$$\frac{d^{2}\theta}{dt^{2}} + \frac{3}{2} \frac{g}{l} \sin \theta = 0$$

$$\Rightarrow \frac{d^{2}\theta}{dt^{2}} + \frac{3}{2} \frac{g}{l} \theta = 0$$

$$\omega^{2} = \frac{3}{2} \frac{9}{4}. \qquad \lambda = \frac{3}{2} \frac{9}{\omega}, = 1.5 \times \frac{9.8}{n^{2}} = \frac{1.5m}{n^{2}}$$

$$\omega = \sqrt{\frac{3}{2}} \frac{9}{4}.$$

or write the eq ns of motion for double perdulum system shown in tig Assume that displacement angles of the perdulum are small enough to ensure that spin is always horizontal. The perdulum socks are taken to be mossless of the length le Ee the spring attached 3/2 th of the way down

K K M

6. From write the eq of motion for a body of muss in suspended from a fined point with by a point with a condail callefully define where the body displacement is zuro second Ouder Bystemse-

V:(3) RC3 +32/C+1 82+28 wn 8 + wp2 > wn = 1 $2\&w_n = \frac{R}{L}$

 $\xi_1 = \frac{R}{2Lw_0} = \frac{R}{2}\sqrt{\frac{C}{L}}$

16 MIP = - TE X100

Tp: To = To &.

Tx = x-0 wd

1. For the electrical ext shown in fig 92 find the following a Time domain equilibration ((t) & v.(t) 'b) Time domain equilibration equating the Not of c) Assuming all EC alle zuro, At In 12(8) & damping rated & and undamped natural friquency we of the system d) The values of p that well evenelt in v2 (1) having an overeshed

Types of inputs

ues, ses of

1/8 t 1/82

not mole than 25%, assuming Viti) is a unit step L=10mt & C= HUF.

NPPLY KVL.

V.(E) (1(4)) | Te vo(1) a) V.(I) = R(A) + Ld (A) + Vo(1) | [16] d b). V2(4) = 1 [(4).04 Cd v.(1) = i(1). Apply LT, V, (t) = RCd V, (t) + OLd2 V, (t) + V, (t), > V1(8)= RCSV2(8) + RL32V2(8) + V2(8) $\frac{V_{2}(8)}{V_{3}(8)} = \frac{1}{\frac{1}{8^{1}+R(8+1)}} = \frac{1}{\frac{1}{8^{1}+R(8+\frac{1}{10})}}$ WAR JEC Ez RVC of MP = e -TE In Mpz - x & 1- \(\frac{1}{2} \) 1.38/1-8'2 = 78 1.904 (1-8) = = 282 1.904 -1,904812 - X282 1,904 2 &12 A2+1.9047 £ = 0.4 & z R C R_2 $2 & \int_{C}^{L}$

= 2x0.4x \ 10x103 R= 402

For the unity flb sys shown in rig. 9.2. The gath. k

of the proportional controller so that the clp y (t.) has an overshoot of

the proportional controller so that the clp y (t.) has an overshoot of

not more that 10% in suspense to a unit step.

$$F(3) = \frac{K}{3(3+2)} = \frac{K}{3(3+2)} = \frac{K}{3(3+2)} = \frac{K}{3(3+2)} = \frac{K}{8^{2}+2^{2}+4}$$

$$S(S+2)$$

$$S$$

$$\frac{3}{\sqrt{1-\xi^{2}}} = \frac{-\pi \xi^{2}}{\sqrt{1-\xi^{2}}}$$

$$\frac{2.302(1-\xi^{2})}{2.302} = \frac{\pi^{2}\xi^{2}}{\xi^{2}}$$

$$\frac{2.302}{\xi^{2}} = \frac{2.302}{\pi^{2}+1302}$$

$$= \frac{1}{2000} = \frac$$

0 K K L 2.86

3. The open loop transfer in of a unity 11b sys as $G(S) = \frac{K}{S(S+2)}$. The destruct system suspense to a unit step i/p is specified as TP = 1540 and overshoot MP = 5%. a. Determine whether both specification can be met simultaneously in selecting the right value K. b. Select the region in S where both specifications are med. Indicate what root positions are possible for some likely values of K.

C Relax the specification in a by the space factor & pick a suitable value of K.

78)- K MIP = 0,11 Mp= e - 7 6 1 Tp = 2.215. $(\ln(0.5))^{\frac{1}{2}} = \frac{\pi^2 \xi^{\frac{1}{2}}}{F_{1-c^{\frac{1}{2}}}}$ 8.990 = (7+8.990) &2 & = 0.69. = K= 2.1 4 miles 1 = 1 = 1.338 man = 1 - 0.692 = 41.338 o- relaxation factor MP = 80.05 tp = 7 T wn /1-82 = 1 / (4)2 \$ wn/1-22 = 8 T ~ = 4.338×VI-0.692 Mp = e -x 1/h TX0.05 = 0 T A For the writy flb sys shown in fig; specify the goin & the pol location in the compensator so that overall closed loop susponse to a unit styp ilp has an overshoot of no more than 25% & 1% settling time of no move than 0.1 see. 760H.O & 3 War 114.07 rodels K ~ 113.34 Q= 67.10 Y(S) 2 100K S2+(25+Q)S+25Q+100K 2 & wn = 25+Q. WA = 10 JE 1250 + 100K 48 - 4 & g 3,. Sz. - Ewn + jwn /1-82 S, 2 -46.05 +104,36j az 80-25 Sz = -46.05 - 104.36