



**POLITECNICO**  
MILANO 1863

# Study of a Hypersonic Scramjet under thermochemical equilibrium and non-equilibrium conditions

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Nil Couto

# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions



# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions

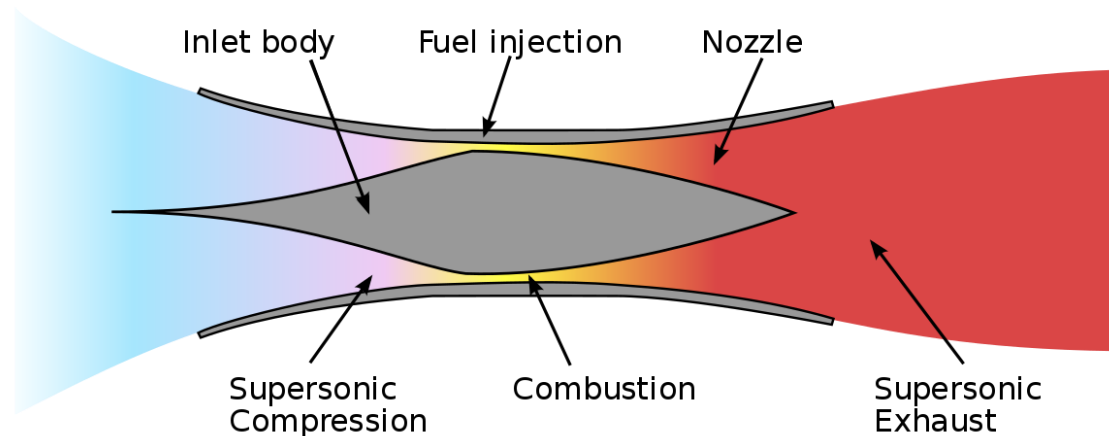


# BACKGROUND



Boeing X-51 A prototype

- Initial Project: Study of a waverider.
- Weak shocks didn't produce enough temperature jump to activate finite rate chemical reactions
- Diamond shape to further increase temperature



Scramjet's interior



# OPERATING CONDITIONS

	COLD	HOT
Inlet Mach	5, 10, 15	5, 10, 15
Inlet Tr [K]	386.8	800
Inlet Pressure [Pa]	1177	2553.14
Outlet Pressure [Pa]	1090.2	1090.2

Bibliographic reference for cold case. Hot case done to mimic combustion

Initial Composition : 77% N<sub>2</sub> , 23% O<sub>2</sub>, 0% NO, 0% N, 0% O

For thermochemical nonequilibrium:  $T_v = 1179.6$  K

Geometry : L = 9m ; H\_Inlet = 2 m ; H\_Outlet = 4 m ; L\_diamond = 4 ;  
H\_diamond = 0.5 m



# GOVERNING EQUATIONS

Field Variables:  $\rho, \mathbf{u}, T^{(rt)}, T^{(ev)}, Y_s$

Mass Balance: 
$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0$$
$$\frac{\partial \rho Y_s}{\partial t} + \nabla \cdot (\rho Y_s \mathbf{u}) = \dot{\omega}_s$$

Momentum Balance: 
$$\frac{\partial \rho \mathbf{u}}{\partial t} + \nabla \cdot (\rho \mathbf{u} \mathbf{u} + p \hat{\mathbf{I}}) = \mathbf{0}$$

Energy Balance: 
$$\frac{\partial}{\partial t} \left[ \rho \left( \frac{1}{2} \mathbf{u}^2 + e \right) \right] + \nabla \cdot \left\{ \rho \mathbf{u} \left( \frac{1}{2} \mathbf{u}^2 + e \right) + p \mathbf{u} \right\} = 0$$

Vibrational Energy Balance: 
$$\frac{dE^{(v)}}{dt} = \frac{E^*(T^{(rt)}) - E^{(v)}}{\tau_v(n, T^{(rt)})}$$



# SOLVER SETUP

- Software : SU2Nemo
- Solver : Nemo Euler
- Fluid Model : Mutation++
- Mixture : Air5 species
- Meshing software : Gmsh
- Convective Numerical Method : AUSM
- Slope Limiter : Venkatakrishnan Wang
- Time Discretization : Explicit
- CFL : 0.8
- Park's Two Temperature model

SU2  
code





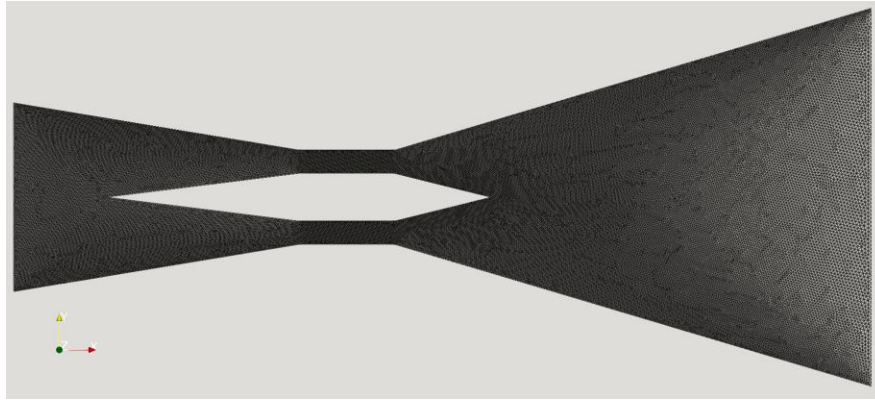
# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. **Mesh Independence Test**
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions

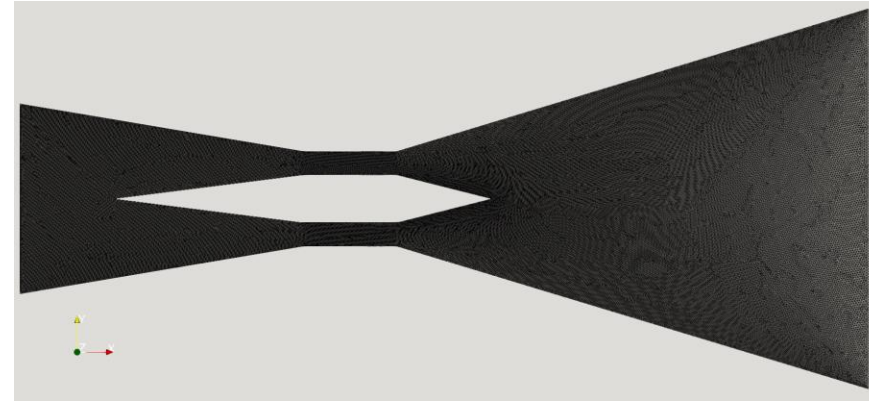




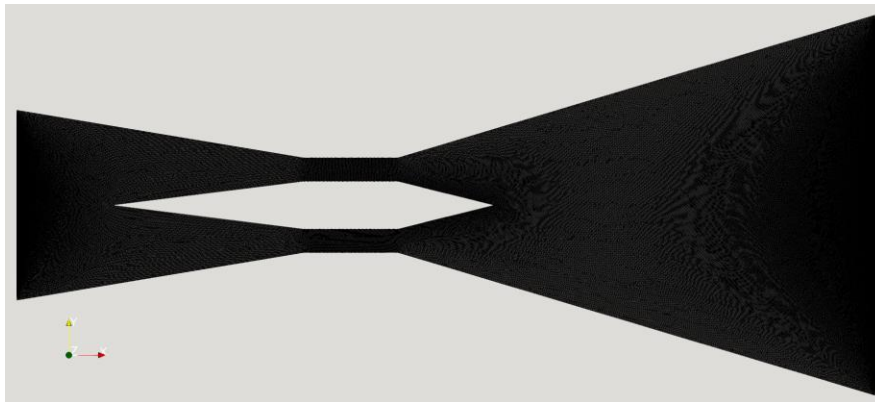
# MESH INDEPENDENCE TEST



Coarse



Medium



Fine

Mesh type	Relative error
Coarse	2.007%
Medium	0.382%

Performed for  $Ma = 15$  and  $Tr = Tv = 800$  K

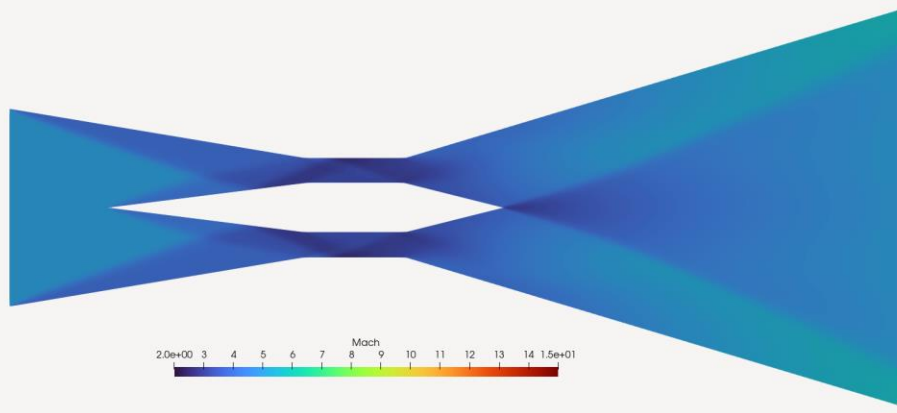


# LIST OF CONTENTS

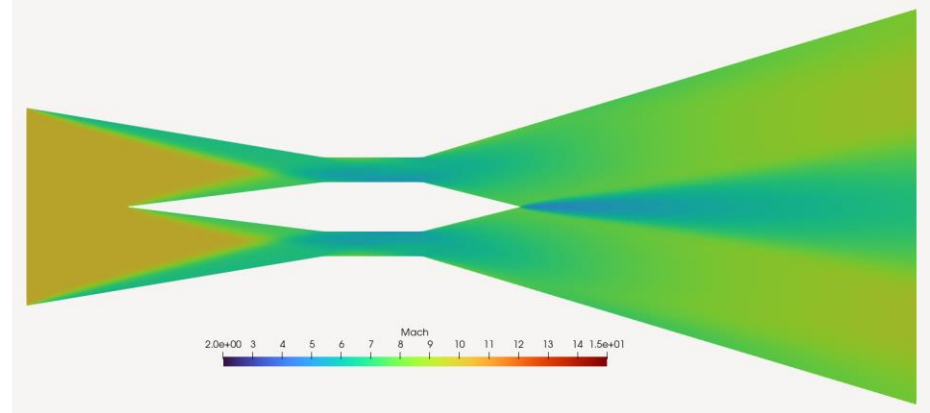
1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions



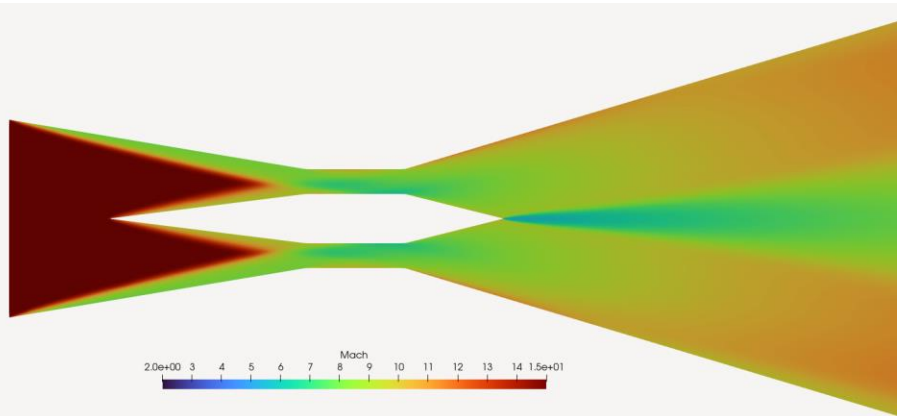
# THERMOCHEMICAL EQUILIBRIUM



Ma = 5    Tr = Tv = 386.8K



Ma = 10    Tr = Tv = 386.8 K

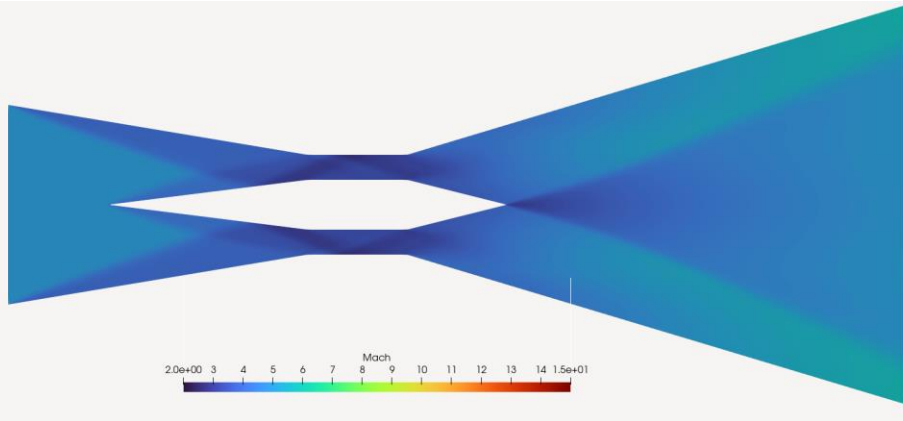


Ma = 15    Tr = Tv = 386.8K

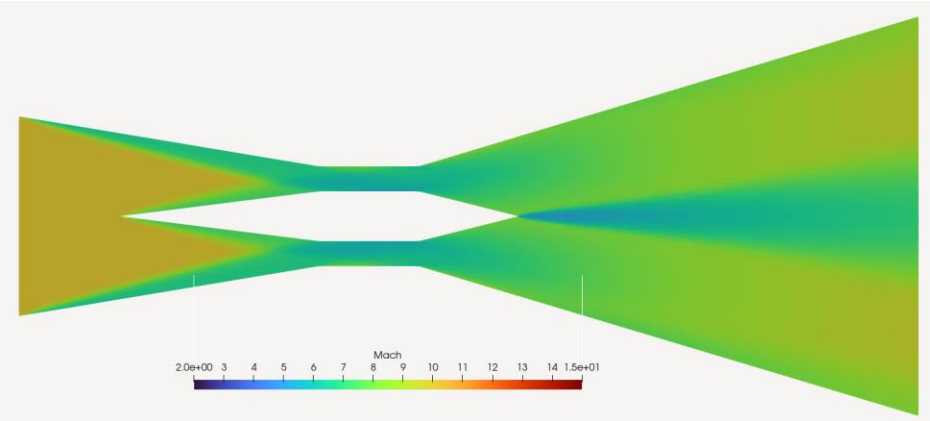
- Shock angle decreases as Ma increases
- Shock intensity after the diamond is larger as freestream Ma increases
- Lower Ma always after diamond



# THERMOCHEMICAL EQUILIBRIUM

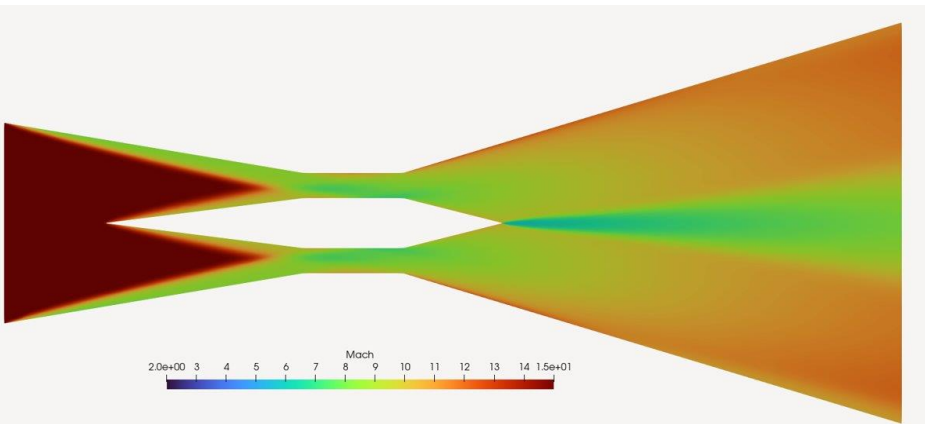


$Ma = 5$   $Tr = Tv = 800K$



$Ma = 10$   $Tr = Tv = 800K$

- Almost no difference between cold and hot for  $Ma = 5$ .
- Large freestream  $T$  produces larger  $Ma$  at the divergent section for the same freestream  $Ma$

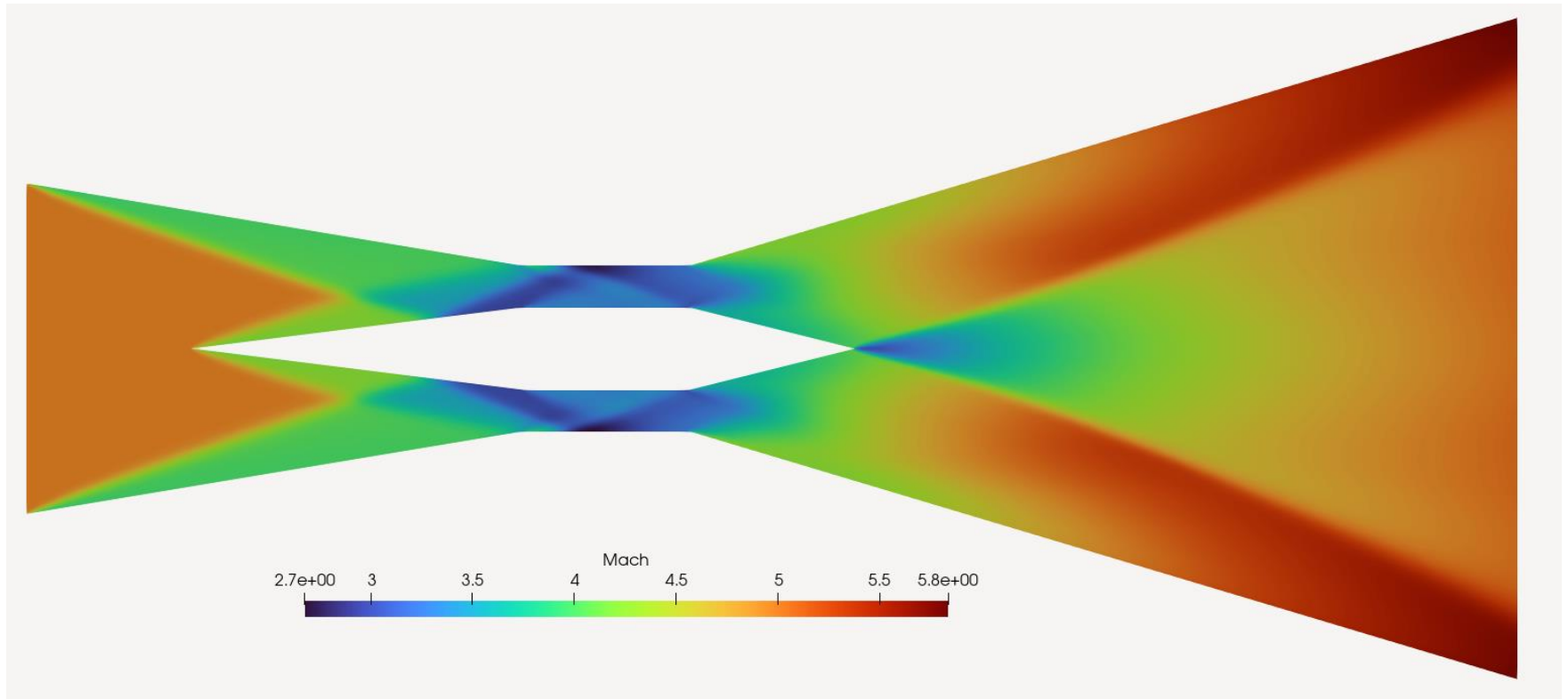


$Ma = 15$   $Tr = Tv = 800K$



# THERMOCHEMICAL EQUILIBRIUM

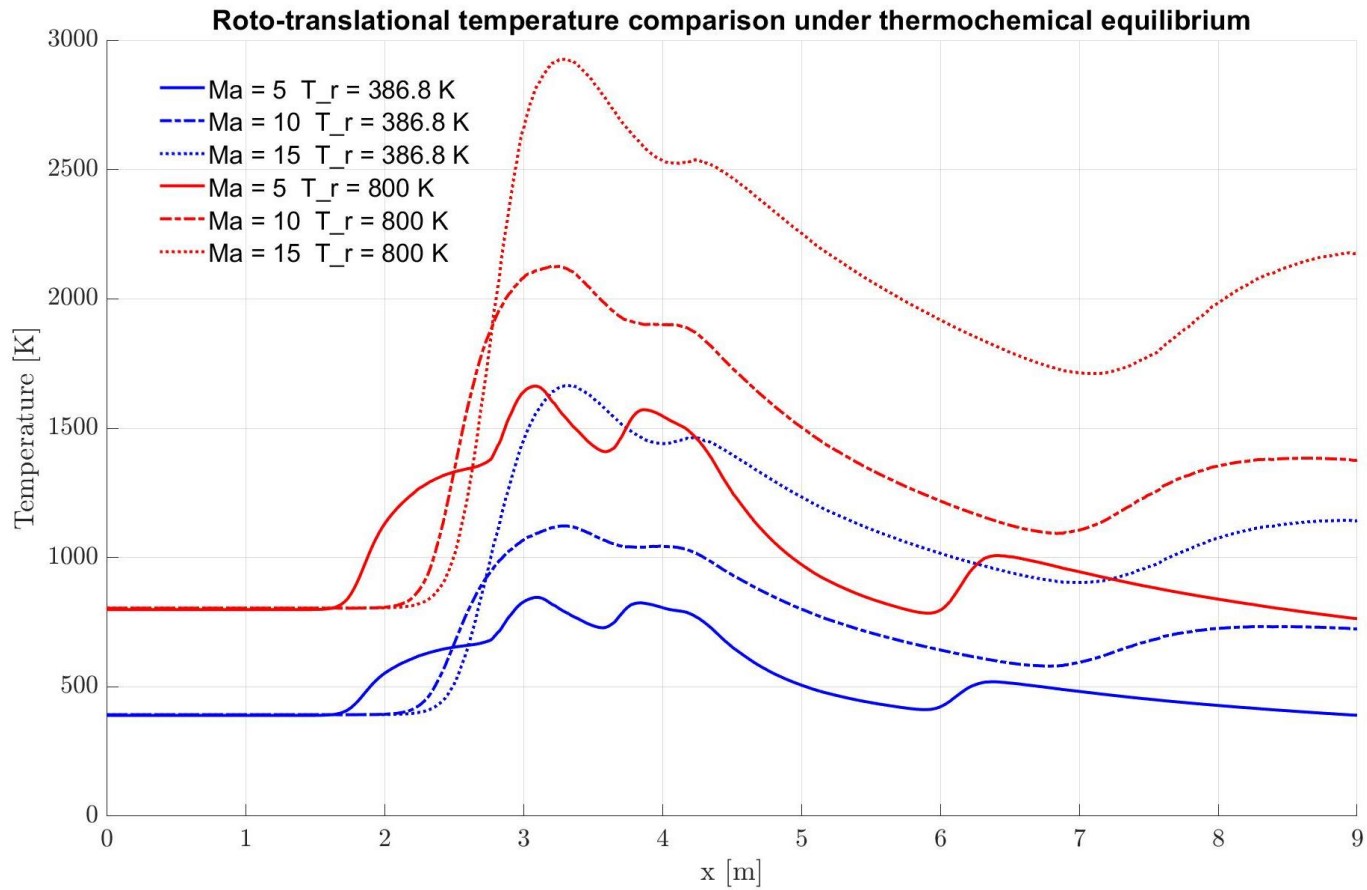
Reflections in central region are better captured as Ma reduces



$Ma = 5$   $T_r = T_v = 800K$



# THERMOCHEMICAL EQUILIBRIUM



# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions





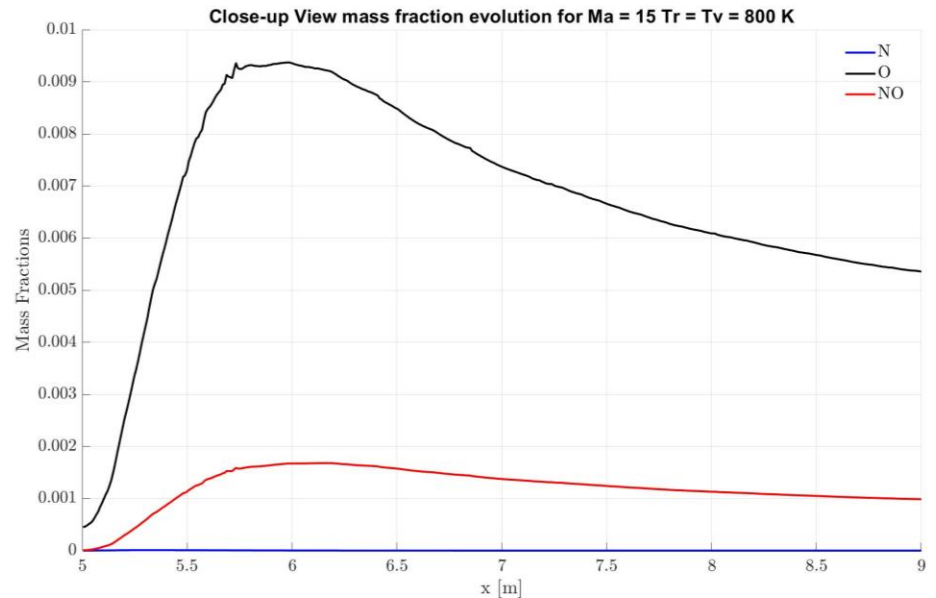
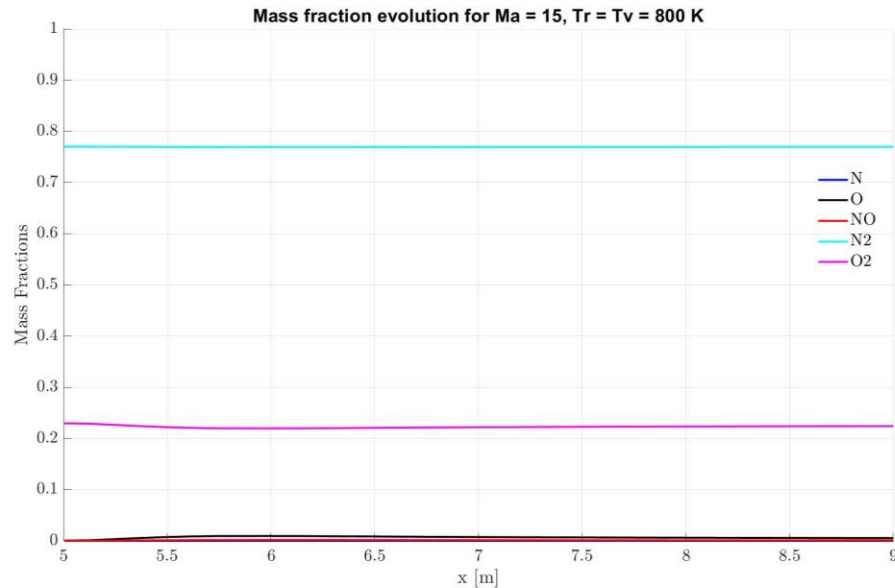
# CHEMICAL NON-EQUILIBRIUM

	Ma=5 (C)	Ma=10 (C)	Ma=15 (C)	Ma=5 (H)	Ma=10 (H)	Ma=15 (H)
N <sub>2</sub>	0.77	0.77	0.77	0.77	0.77	0,7699
O <sub>2</sub>	0.23	0.23	0.23	0.23	0.23	0.2280
NO	0	2.8e-31	1.91e-14	9.45e-17	1.06e-10	3.03 e-4
N	0	1.91e-42	5.28e-24	4.66e-33	1.30e-18	6.06e-10
O	1.64e-34	1.14e-21	3.22e-10	4.05e-12	3.20e-7	0.0019

- For all Ma in cold condition, mass fractions of NO, N, O are extremely low
- Mass fractions of O, N, NO increase with Ma
- For the hot condition, at Ma=15 we can see the effect of diatomic oxygen dissociation in the resulting mass fraction of O<sub>2</sub>



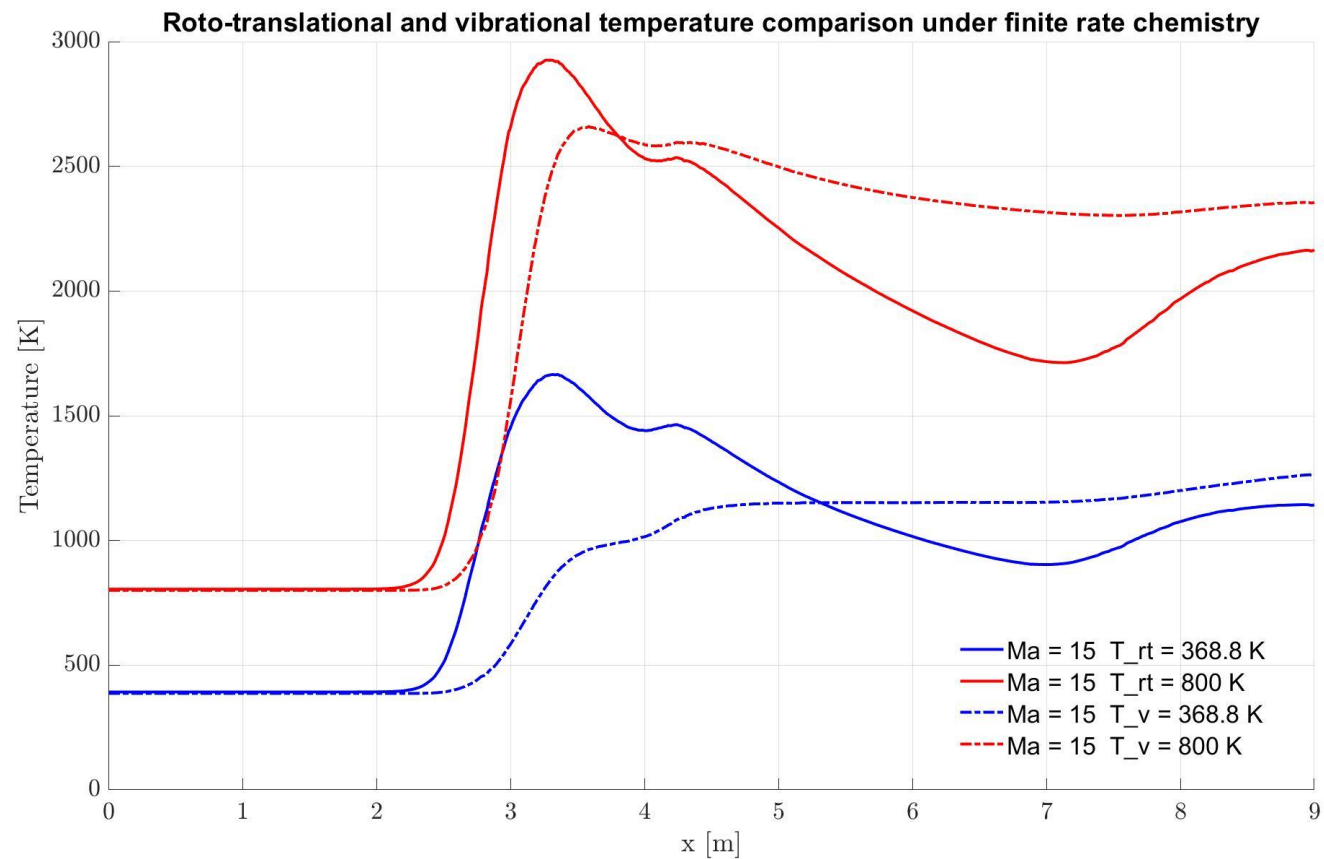
# CHEMICAL NON-EQUILIBRIUM



- Finite rate chemical reaction concentrated in the post-diamond region
- Increase of O close to the diamond edge because of  $O_2$  dissociation
- Formation of O reduced after  $x = 6$  m due to recombination (NO formation)
- Very low N mass fraction. Higher temperature required to dissociate  $N_2$



# CHEMICAL NON-EQUILIBRIUM

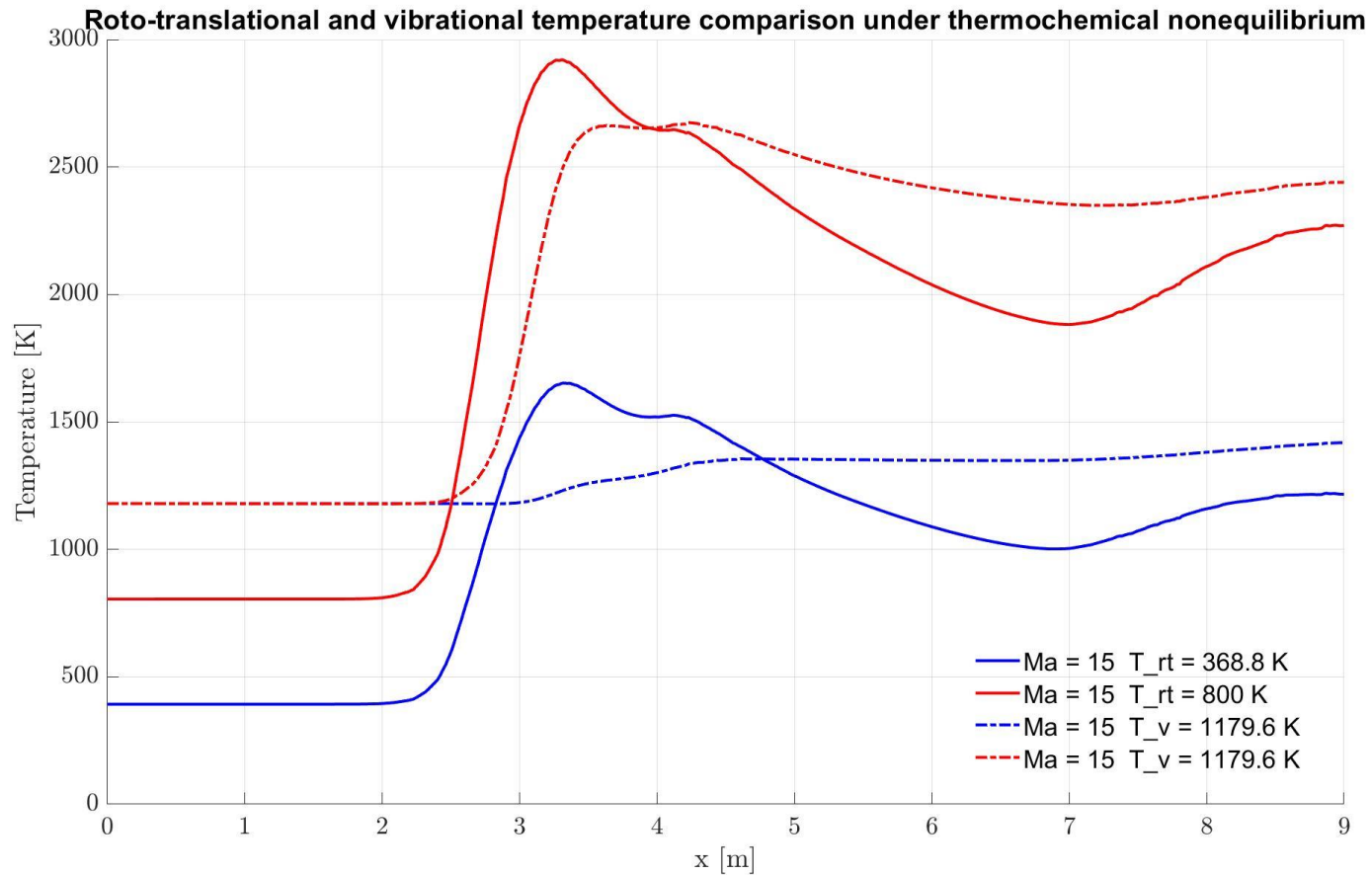


# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
6. Conclusions

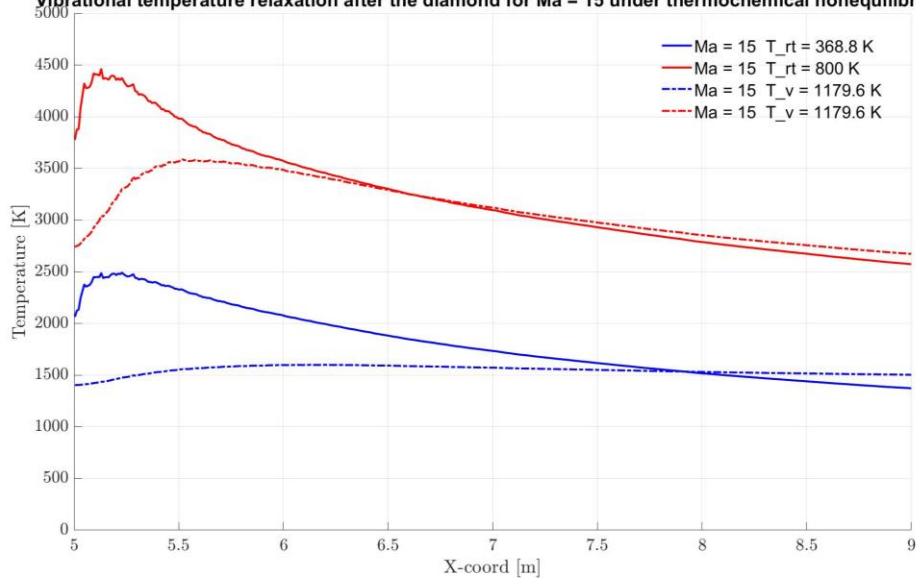


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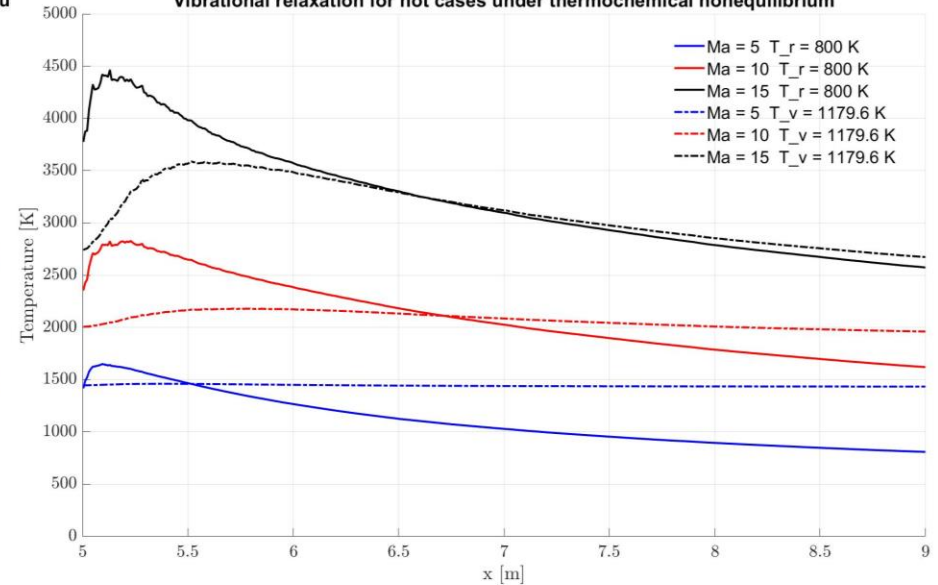


# THERMOCHEMICAL NON-EQUILIBRIUM

Vibrational temperature relaxation after the diamond for Ma = 15 under thermochemical nonequilibrium



Vibrational relaxation for hot cases under thermochemical nonequilibrium



Larger vibrational excitation with hot gas

Shorter relaxation time as Ma increases

At the scramjet's outlet, there's still thermal nonequilibrium



# LIST OF CONTENTS

1. Background
  - 1.1 Operating conditions
  - 1.2 Governing equations
  - 1.3 Solver Setup
2. Mesh Independence Test
3. Thermochemical equilibrium
  - 3.1 Flowfield visualization
  - 3.2 Roto-translational temperature comparison
4. Chemical nonequilibrium
  - 4.1 Mass fractions
  - 4.2 Roto-translational and Vibrational temperatures
5. Thermochemical nonequilibrium
  - 5.1 Roto-translational and Vibrational temperatures
  - 5.2 Vibrational temperature relaxation
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# CONCLUSIONS

- Similar shock patterns for the same  $Ma$  under different thermal conditions
- Stronger shock localized at the post-diamond region
- Temperature reached across the domain should be larger to better appreciate finite rate chemical reactions
- Chemical reactions observed are in accordance with the theory
- Relaxation time higher for higher Mach number
- Thermochemical non equilibrium persists throughout the geometry





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