

## vector calculus.

### co-ordinate Systems

1. Cartesian or Rectangular  $\rightarrow (x, y, z)$

$$\begin{array}{l} -\infty \leq x \leq \infty \\ -\infty \leq y \leq \infty \\ -\infty \leq z \leq \infty \end{array}$$

Any vector  $A$  in Cartesian co-ordinates can be written as  $\rightarrow A_x a_x + A_y a_y + A_z a_z$

② Cylindrical  $\rightarrow (p, \phi, z)$

$$\begin{array}{l} 0 \leq p < \infty \\ 0 \leq \phi < 2\pi \\ -\infty < z < \infty \end{array}$$

Any vector  $A$  in cylindrical coordinates can be written as  $A_p a_p + A_\phi a_\phi + A_z a_z$

③ Spherical  $\rightarrow (r, \theta, \phi)$

$$\begin{array}{l} 0 \leq r < \infty \\ 0 \leq \theta \leq \pi \\ 0 \leq \phi < 2\pi \end{array}$$

Any vector  $A$  in spherical CO. systems =  $A_r a_r + A_\theta a_\theta + A_\phi a_\phi$

### Conversions.

#### ① Cylindrical to Cartesian

$$\begin{aligned} x &= p \cos \phi \\ y &= p \sin \phi \\ z &= z. \end{aligned}$$

#### ② Cartesian to cylindrical

$$\begin{aligned} p &= \sqrt{x^2 + y^2} \\ \phi &= \tan^{-1}\left(\frac{y}{x}\right) \\ z &= z \end{aligned}$$

#### ③ Cartesian to spherical.

$$\begin{aligned} r &= \sqrt{x^2 + y^2 + z^2} = \sqrt{p^2 + z^2} \\ \theta &= \tan^{-1}\left(\frac{\sqrt{x^2 + y^2}}{z}\right) = \tan^{-1}\left(\frac{p}{z}\right) \\ \phi &= \tan^{-1}\left(\frac{y}{x}\right) \end{aligned}$$

#### ④ Spherical to Cartesian

$$\begin{aligned} x &= r \cos \phi = r \sin \theta \cos \phi \\ y &= r \sin \phi = r \sin \theta \sin \phi \\ z &= r \cos \theta \end{aligned}$$

## Transformation matrices

$$\begin{bmatrix} A_p \\ A_\phi \\ A_z \end{bmatrix} = \begin{bmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} \quad (\text{from Cartesian to cylindrical})$$

$$\begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} = \begin{bmatrix} \cos \phi & -\sin \phi & 0 \\ \sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} A_p \\ A_\phi \\ A_z \end{bmatrix} \quad (\text{from cylindrical to Cartesian})$$

$$\begin{bmatrix} A_r \\ A_\theta \\ A_\phi \end{bmatrix} = \begin{bmatrix} \sin \theta \cos \phi & \sin \theta \sin \phi & \cos \theta \\ \cos \theta \cos \phi & \cos \theta \sin \phi & -\sin \theta \\ -\sin \phi & \cos \phi & 0 \end{bmatrix} \begin{bmatrix} A_x \\ A_y \\ A_z \end{bmatrix} \quad \text{From Cartesian to spherical.}$$

## Elemental Differential Displacement (vector) - length

$$\begin{aligned} d\vec{l} &= dx \vec{a}_x + dy \vec{a}_y + dz \vec{a}_z \\ &= dp \vec{a}_p + (p d\phi) \vec{a}_\phi + dz \vec{a}_z \\ &= dr \vec{a}_r + (r d\theta) \vec{a}_\theta + (p d\phi) \vec{a}_\phi \end{aligned}$$

## Differential Elemental area

$$\begin{aligned} d\vec{S} &= dy dz \vec{a}_x = dx dy \vec{a}_y = dx dz \vec{a}_z \\ &= (p d\phi) dz \vec{a}_p = (dp dx) \vec{a}_\phi = (dp)(p d\phi) \vec{a}_z \\ &= (r d\theta)(p d\phi) \vec{a}_r = (dr)(r d\theta) \vec{a}_\phi = dr(p d\phi) \vec{a}_\theta \end{aligned}$$

## Differential volume

$$\begin{aligned} dv &= dx dy dz \\ &= dp dz (p d\phi) \\ &= dr (r d\theta) (p d\phi) \\ &= r^2 \sin \theta dr d\theta d\phi. \end{aligned}$$

## Del operator

is by Acz

$$\nabla = \frac{\partial}{\partial x} \bar{a}_x + \frac{\partial}{\partial y} \bar{a}_y + \frac{\partial}{\partial z} \bar{a}_z \quad (\text{Cartesian})$$

is by

$$= \frac{\partial}{\partial \rho} \bar{a}_\rho + \frac{1}{\rho} \frac{\partial}{\partial \phi} \bar{a}_\phi + \frac{\partial}{\partial z} \bar{a}_z \quad (\text{cylindrical})$$

$$= \frac{\partial}{\partial r} \bar{a}_r + \frac{1}{r} \frac{\partial}{\partial \theta} \bar{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial}{\partial \phi} \bar{a}_\phi \quad (\text{spherical})$$

$\hookrightarrow \rho = r \sin \theta$

Gradient of a scalar field  $\rightarrow$  vector quantity

It is a vector. maximum space rate of increase of  $V$ .

$$\begin{aligned} \nabla V &= \frac{\partial V}{\partial x} \bar{a}_x + \frac{\partial V}{\partial y} \bar{a}_y + \frac{\partial V}{\partial z} \bar{a}_z \\ &= \frac{\partial V}{\partial \rho} \bar{a}_\rho + \frac{1}{\rho} \frac{\partial V}{\partial \phi} \bar{a}_\phi + \frac{\partial V}{\partial z} \bar{a}_z \\ &= \frac{\partial V}{\partial r} \bar{a}_r + \frac{1}{r} \frac{\partial V}{\partial \theta} \bar{a}_\theta + \frac{1}{r \sin \theta} \frac{\partial V}{\partial \phi} \bar{a}_\phi \end{aligned}$$

Divergence of a vector field  $\rightarrow$  Scalar quantity

outward flux per unit volume

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$$\begin{aligned} \nabla \cdot \mathbf{A} &= \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} \\ &= \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho A_\rho) + \frac{1}{\rho} \frac{\partial A_\phi}{\partial \phi} + \frac{\partial A_z}{\partial z} \\ &= \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (A_\theta \sin \theta) + \frac{1}{r \sin \theta} \frac{\partial A_\phi}{\partial \phi} \end{aligned}$$

Curl of vector  $\rightarrow$  vector quantity (definition on next sheet)

$$\nabla \times \mathbf{A} = \begin{bmatrix} \bar{a}_x & \bar{a}_y & \bar{a}_z \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{bmatrix} \cdot \frac{1}{\rho} \begin{bmatrix} \bar{a}_\rho & \rho \bar{a}_\phi & \bar{a}_z \\ \frac{\partial}{\partial \rho} & \frac{\partial}{\partial \phi} & \frac{\partial}{\partial z} \\ A_\rho & \rho A_\phi & A_z \end{bmatrix}, \frac{1}{r^2 \sin \theta} \begin{bmatrix} \bar{a}_r & r \bar{a}_\theta & r \sin \theta \bar{a}_\phi \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial \phi} \\ A_r & r A_\theta & r \sin \theta A_\phi \end{bmatrix}$$



## Divergence Theorem or Gauss's Theorem

The Divergence Theorem states that the total outward flux of vector field  $A$  through the closed surface  $S$  is the same as the volume integral of the divergence of  $A$ .

$$\oint_S A \cdot d\mathbf{s} = \int_V \nabla \cdot A \, dV$$

## Stoke's Theorem

Stoke's Theorem states that the circulation of a vector field  $A$  around a closed path  $L$  is equal to the surface integral of the curl of  $A$  over the open surface  $S$  bounded by  $L$ , provided  $A$  and  $\nabla \times A$  are continuous on  $S$ .

$$\oint_L A \cdot d\mathbf{l} = \int_S (\nabla \times A) \cdot d\mathbf{s}$$

Curl of a vector  $\rightarrow$  A curl of  $A$  is an axial vector whose magnitude is the maximum circulation of  $A$  per unit area tends to zero and whose direction is the normal direction of area, when the area is oriented to make the circulation maximum.

$$\text{Curl } A = \nabla \times A = \left[ \lim_{\Delta S \rightarrow 0} \frac{\oint_L A \cdot d\mathbf{l}}{\Delta S} \right] \mathbf{a}_n$$

line integral  $\rightarrow \oint A \cdot d\mathbf{l}$

Surface integral  $\rightarrow \oint_S A \cdot d\mathbf{s}$

volume integral  $\rightarrow \int_V A \cdot d\mathbf{v}$

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For solenoidal  $\nabla \cdot \vec{A} = 0$

For irrotational  $\nabla \times \vec{A} = 0$

If  $\nabla \times \vec{E} = 0$   $\vec{E}$  field is conservative