# USSR: An UltraSound Sparse Regularization Framework

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## Introduction and objectives

1. Ultrafast ultrasound (US) imaging uses unfocused waves to insonify the whole field-of-view at once
2. We present USSR: An UltraSound Sparse Regularization framework which provides:
   - Matrix-free and highly parallel formulations of the measurement and its adjoint in the context of plane-wave (PW) imaging
   - Sparse regularization algorithm with two sparsity priors: $\ell_p$-norm to the power of $p$ ($p \geq q$), $\ell_1$-norm in a sparsity averaging (SA) model
3. USSR provides a fast, high-quality and low memory-footprint image reconstruction method

## Notations and model

- Notations:
  - 1D probe composed of $N_{el}$ transducer elements located at $\boldsymbol{p}^i \in \Pi$ recording samples at time instants $t^l = t^0 + l\Delta t$, with $l \in \{1, \dots, N_t\}$
  - $m\left(\boldsymbol{p}^i, t^l\right)$ signal received at time instant $t^l$ by element located at $\boldsymbol{p}^i$
  - $v_{pe}(t)$ pulse-shape of the experiment
  - Medium $\Omega$ composed of points located at $\boldsymbol{r}^n = \left[x^k, z^l\right]^T$, $(k, l) \in \{1, .., N_x\} \times \{1, .., N_z\}$ and $n = (k-1)N_z + l$
  - Each point characterized by its tissue-reflectivity function $\gamma\left(\boldsymbol{r}^n\right)$

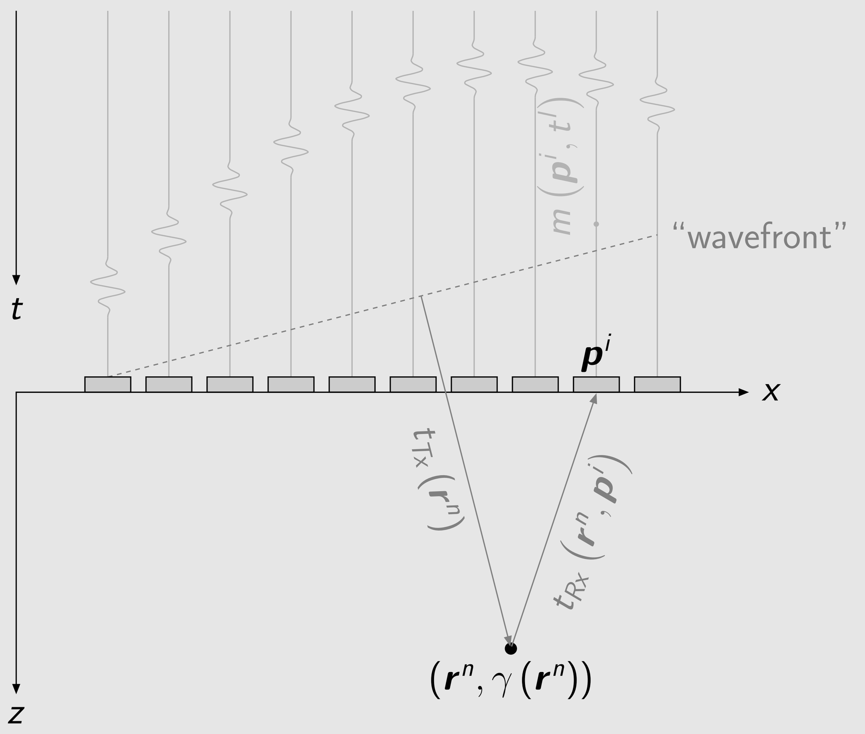


**Figure** Standard setting for US imaging

- Pulse-echo spatial impulse response model [1]

$$m\left(\boldsymbol{p}^i, t^l\right) = \int_{\boldsymbol{r}\in\Omega} o_d\left(\boldsymbol{r}, \boldsymbol{p}^i\right) \gamma\left(\boldsymbol{r}\right) v_{pe}\left(t^l - t_{Tx}\left(\boldsymbol{r}\right) - t_{Rx}\left(\boldsymbol{r}, \boldsymbol{p}^i\right)\right) d\boldsymbol{r},$$

$t_{Tx}\left(\boldsymbol{r}\right)$ propagation delay on transmit, $t_{Rx}\left(\boldsymbol{r}, \boldsymbol{p}^i\right) = \left\|\boldsymbol{r} - \boldsymbol{p}^i\right\|_2 / c$ propagation delay on receive and $o_d\left(\boldsymbol{r}, \boldsymbol{p}^i\right) = o\left(\boldsymbol{r}, \boldsymbol{p}^i\right) / 2\pi \left\|\boldsymbol{r} - \boldsymbol{p}^i\right\|_2$ where $o\left(\boldsymbol{r}, \boldsymbol{p}^i\right)$ accounts for the element directivity [2]

## Parametric formulation of the model

- Equation (1) can be written as:

$$\begin{aligned} m\left(\boldsymbol{p}^i, t^l\right) &= \iint_{\tau\in\mathbb{R}, \boldsymbol{r}\in\Gamma\left(\boldsymbol{p}^i, \tau\right)} \frac{o_d\left(\boldsymbol{r}, \boldsymbol{p}^i\right)\gamma\left(\boldsymbol{r}\right)}{\mid \nabla_{\boldsymbol{r}} g \mid} d\sigma\left(\boldsymbol{r}\right) v_{pe}\left(t^l - \tau\right) d\tau \\ &= \mathcal{H}\left\{\gamma\right\}\left(\boldsymbol{p}^i, t^l\right) \end{aligned} \quad (1)$$

$g\left(\boldsymbol{r}, \boldsymbol{p}^i, t\right) = t - t_{Tx}\left(\boldsymbol{r}\right) - t_{Rx}\left(\boldsymbol{r}, \boldsymbol{p}^i\right)$, $\Gamma\left(\boldsymbol{p}^i, t\right) = \left\{\boldsymbol{r} \in \Omega \mid g\left(\boldsymbol{r}, \boldsymbol{p}^i, t\right) = 0\right\}$, $\nabla_{\boldsymbol{r}} g$ denotes the gradient of $g$ w.r.t $\boldsymbol{r}$, $d\sigma\left(\boldsymbol{r}\right)$ is the measure over the 1D-curve $\Gamma\left(\boldsymbol{p}^i, t\right)$

- To have an efficient way of calculating the integral defined in Equation (1), we derive a parameterization of $\Gamma\left(\boldsymbol{p}^i, t\right)$ as follows:

$$\boldsymbol{r} = [x, z]^T \in \Gamma\left(\boldsymbol{p}^i, t\right) \Leftrightarrow \boldsymbol{r}\left(\alpha, \boldsymbol{p}^i, t\right) = \left[\alpha, f\left(\alpha, \boldsymbol{p}^i, t\right)\right]^T, \ \alpha \in \mathbb{R} \quad (2)$$

- This leads us to the parametric formulation of the model

$$m\left(\boldsymbol{p}^i, t^l\right) = \iint_{\tau\in\mathbb{R}, \alpha\in\mathbb{R}} o_d\left(\boldsymbol{r}\left(\alpha, \boldsymbol{p}^i, t^l\right), \boldsymbol{p}^i\right) \gamma\left(\boldsymbol{r}\left(\alpha, \boldsymbol{p}^i, t^l\right)\right) \frac{\mid J_\alpha \mid}{\mid \nabla_{\boldsymbol{r}} g \mid} d\alpha v_{pe}\left(t^l - \tau\right) d\tau, \quad (3)$$

$|J_\alpha|$ Jacobian associated with the change of variable

## Parametric equations for plane wave imaging

- Parametric equations obtained by finding the roots of the following function:

$$f\left(z\right) = \sqrt{\left(x - p_x^i\right)^2 + \left(z - p_z^i\right)^2} + z\cos\left(\theta\right) + x\sin\left(\theta\right) - ct, \quad (4)$$

which gives the following solution:

$$z = \frac{1}{\sin\left(\theta\right)^2}\left(p_z^i - ct\cos\left(\theta\right) + x\sin\left(\theta\right)\cos\left(\theta\right) \pm \sqrt{\Delta}\right), \quad (5)$$

$$\Delta = \left(ct - p_z^i\cos\left(\theta\right) - p_x^i\sin\left(\theta\right)\right)\left(ct - p_z^i\cos\left(\theta\right) + \left(p_x^i - 2x\right)\sin\left(\theta\right)\right).$$

## Dicretization of the model

- Equation (3) is discretized as

$$m\left(\boldsymbol{p}^i, t^l\right) = \mathcal{H}_d\left\{\gamma\right\}\left(\boldsymbol{p}^i, t^l\right) = \left(\tilde{\boldsymbol{m}}\left(\boldsymbol{p}^i\right) *_t \boldsymbol{v_{pe}}\right)\left(t^l\right), \quad (6)$$

where $*_t$ is the 1D-convolution and $\tilde{\boldsymbol{m}}\left(\boldsymbol{p}^i\right) = \left(\tilde{m}\left(\boldsymbol{p}^i, t^l\right)\right)_{t^l\in T_d}$ defined by:

$$\tilde{m}\left(\boldsymbol{p}^i, t^l\right) = \sum_{k=1}^{N_x} w^k o_d\left(\boldsymbol{r}\left(\alpha^k, \boldsymbol{p}^i, t^l\right), \boldsymbol{p}^i\right) \varphi\left(\boldsymbol{r}\left(\alpha^k, \boldsymbol{p}^i, t^l\right)\right)\gamma, \quad (7)$$

where $w^k$ is the integration weight and $\varphi$ is a 1D-interpolation kernel

## Parametric formulation of the adjoint operator of the model

- Adjoint operator of the linear operator $\mathcal{H}\left\{\gamma\right\}$ described in (1) is defined as:

$$\mathcal{H}^\dagger\left\{m\right\}\left(\boldsymbol{r}^n\right) = \sum_{\boldsymbol{p}^i\in\Pi} o_d\left(\boldsymbol{r}^n, \boldsymbol{p}^i\right) \int_{\tau\in\mathbb{R}} m\left(\boldsymbol{p}^i, \tau\right) u\left(t_{Tx}\left(\boldsymbol{r}^n\right) + t_{Rx}\left(\boldsymbol{r}^n, \boldsymbol{p}^i\right) - \tau\right) d\tau, \quad (8)$$

where $u\left(t\right) = v_{pe}\left(-t\right)$ is the matched filter of the pulse shape

- Discretization of the adjoint operator expressed as:

$$\mathcal{H}_d^\dagger\left\{\boldsymbol{m}\right\}\left(\boldsymbol{r}^n\right) = \sum_{\boldsymbol{p}^i\in\Pi} \omega^n o_d\left(\boldsymbol{r}^n, \boldsymbol{p}^i\right) \psi\left(t_{Tx}\left(\boldsymbol{r}^n\right) + t_{Rx}\left(\boldsymbol{r}^n, \boldsymbol{p}^i\right)\right) \hat{\boldsymbol{m}}, \quad (9)$$

where $\hat{\boldsymbol{m}} = \boldsymbol{m} *_t \boldsymbol{u}$, $\psi$ is a 1D-interpolation kernel and $\omega^n$ accounts for the integration weight.

## Reconstructed B-mode images

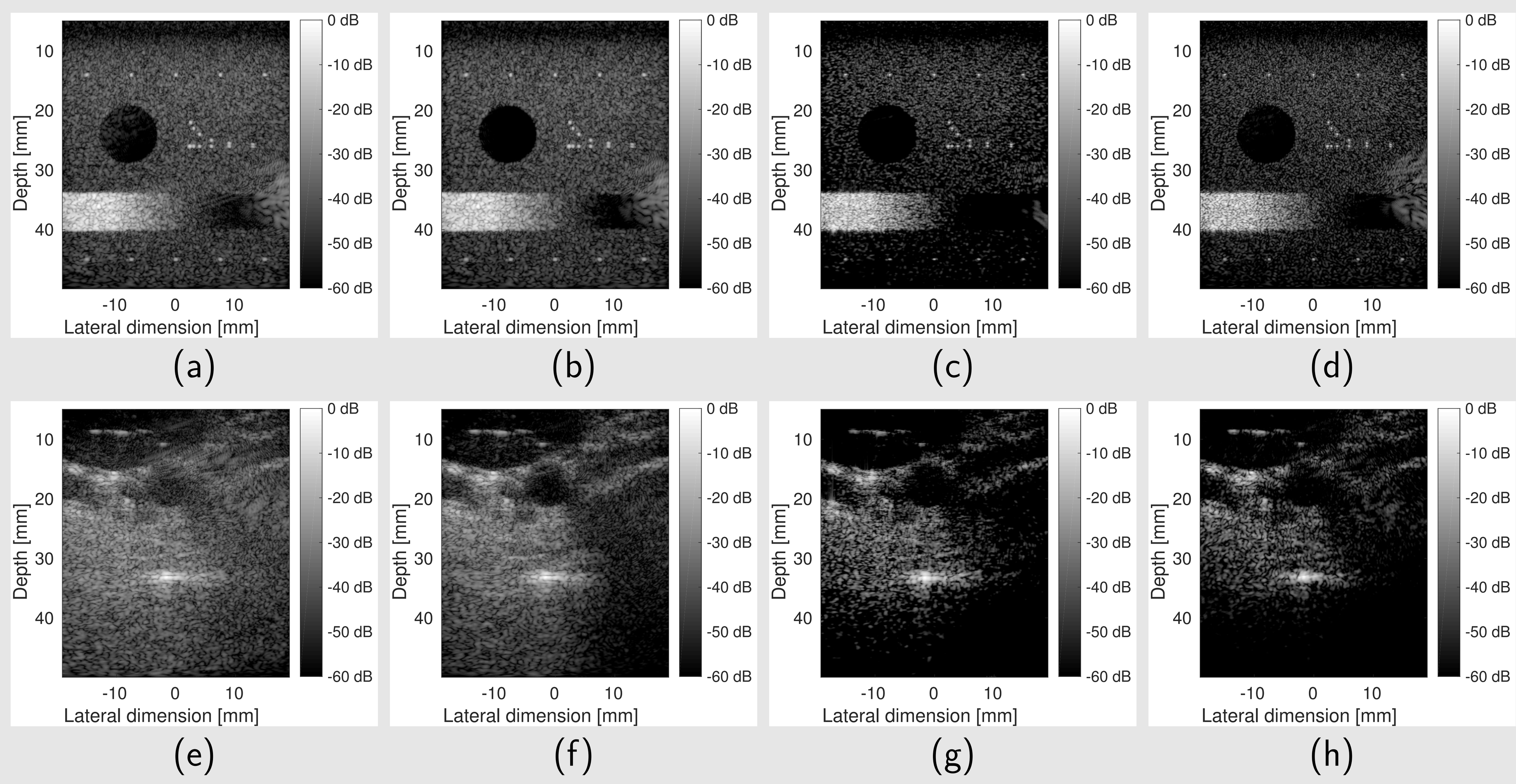


**Figure** Image of the numerical phantom reconstructed with (a) DAS - 1 PW insonification, (b) DAS - 5 PW insonifications, (c) USSR-SA - 1 PW insonification, (c) USSR - $\ell_p$ - 1 PW insonification; Image of the *in-vivo* carotid reconstructed with (e) DAS - 1 PW insonification, (f) DAS - 5 PW insonifications, (g) USSR-SA - 1 PW insonification, (h) USSR-$\ell_p$ - 1 PW insonification.

## Conclusion and perspectives

1. We propose a compressed sensing approach for US image recovery
   - Exploits a stream of pulses model for sparsity of US images
   - Uses multiple CMUX for analog compression of the data
   - Applies a $\ell_{11}$-minimization algorithm for image reconstruction
2. The proposed approach leads to high-quality reconstruction with far fewer data than standard approaches
3. Study of the hardware implementation will be achieved in future work

## References

[1] P. R. Stepanishen, "The time–dependent force and radiation impedance on a piston in a rigid infinite planar baffle", *J. Acoust. Soc. Am.*, vol. 49, no. 3B, pp. 841–849, 1971.

[2] A. R. Selfridge, G. S. Kino, and B. T. Khuri-Yakub, "A theory for the radiation pattern of a narrow-strip acoustic transducer", *Appl. Phys. Lett.*, vol. 37, no. 1, p. 35, 1980.

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