INSTITUTO TECNOLÓGICO DE AERONÁUTICA



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ANALYSIS METHOD OF TEMPERATURES AND HEAT FLOWS FOR ORTHOGONAL CUTTING 1045 STEEL BY THERMAL IMAGING

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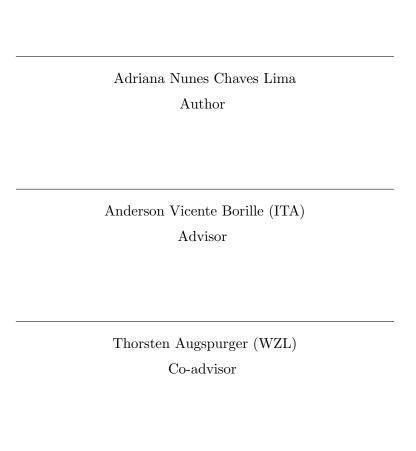
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São José dos Campos: November 22, 2017.

Prof. Dr. Jesuíno Takashi Tomita Course Coordinator of Mechanical Engineering

I dedicate this work to my family, which have always supported me in my decisions and are the most happy ones with this academic achievement.

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Resumo

A manipulação de arquivos de geometria é usualmente associada ao uso de programas de CAD, que costumam ter licenças caras devido à quantidade de recursos sofisticados oferecidos por eles. Esse gasto é facilmente justificável quando o trabalho envolve a aplicação de um número grande dessas funções, por exemplo, no desenvolvimento de uma nova geometria para um projeto. No entanto, para muitos usuários, a tarefa pode ser simples e requerer poucas funções, por exemplo, para gerar um padrão regular de projeções ao longo de uma superfície de modo a obter um conjunto de pontos para guiar a trajetória de uma ferramenta de usinagem durante o processo. Esses clientes teriam que gastar uma quantia elevada em licenças, para então usar apenas uma pequena porção do que o programa tem a oferecer. Esse trabalho apresenta uma solução que permite a leitura direta de um arquivo IGES e a geração de um conjunto específico de pontos usando funções de código aberto. Embora seja programado em $MATLAB^{TM}$, ele é compilado em um arquivo executável, de forma que seja possível seu uso sem a necessidade de licença.

Abstract

The handling of geometry files is usually associated with the usage of CAD software, which commonly have costly licenses due to the amount of sophisticated features that they offer. This expense is easily justifiable when the work involves thorough application of a number of these functions, for example, when developing a new geometry for a given project. However, for many users, the task is simple and only requires a small amount of features, for example, when generating a regular pattern of projections along a surface to obtain a set of points to guide the path of a turning or milling tool throughout a machining process. These clients usually have to spend a lot of money on licenses, only to use a small portion of what the program has to offer. This paper presents a solution which can directly read an IGES geometry file and generate a specific set of points using simple open source functions. Although it is programmed using $MATLAB^{TM}$, it is compiled to an independent executable file, thus being capable of running without any license at all.

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List of Abbreviations and Acronyms

ANSI American National Standards Institute
ASME American Society of Mechanical Engineers

MATLAB Numerical computation software from MathWorks

GUI graphic user interface

GUIDE graphic user interface development environment

AISI American iron and steel institute

WZL Werkzeugmaschinenlabor (Laboratory of Machine Tools and Production Engineering)

FOV Field of view

List of Symbols

- F_c Cutting force on the power direction [N]
- F_p Passive force [N]
- v_c Cutting velocity [m/min]
- P Power developed along cutting process [W]
- w Width of tool [mm]
- t_{uc} Uncut chip thickness $[\mu m]$
- T_e Environment temperature $[{}^oC]$
- λ_{Tool} Heat conductivity of tool material
- t Time [s]

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1 Introduction

In many machining cases, orthogonal cutting may be considered a good approximation to performance on the major cutting edge, that is why it has been extensively studied (SHAW; COOKSON, 2005). For instance, planing and facing processes are some examples that orthogonal cutting conditions can be observed.

Also, it is know that thermal behavior during the cutting process, as temperature fields and heat flows, has a important influence on tool life, surface finish and mattalurgical structure of workpiece and machinability. Then, the study of thermal analysis on orthogonal cutting case shall be able to provide a better comprehension of many studies concerning thermal modeling of metal cuting processes (KOMANDURI; HOU, 2000), (KOMANDURI; HOU, 2001).

The aim of this paper is to develop a method to analyze thermal images generated during the orthogonal cutting of AISI 1045 metal, focusing on the trasient state due to the short time of cutting. It will be analyzed temperature distribution along the cutting tool, heat flows through tool, chip and workpiece.

1.1 Structure

This work is divided into 6 Chapters, including this **Introduction**, plus one Appendix.

The second chapter, **State of the Art**, describes the existing technology which is relevant for the scope of this paper and upon which the work was built.

The third chapter, **Experimental Setup**, describes the methodology and materials that conducted the experiments.

The fourth, **Code Implementation**, describes the logical implementation of the final analysis code.

The fifth, **Results**, presents the results and dicussions about the outputs of the final code.

The sixth and final chapter, Conclusion, sums up what was accomplished in this

work and sugests how it may be expanded for new processes.

The Appendix Source Code contains all the code written for the program.

2 State of the Art

2.1 Infrared Termography

Infrared termography is a contactless way to measure infrared eletromagnetic energy. It makes possible to observe contours of different bodies due to their temperature distribution, since every body is able to emit eletromagnetic radiation when its temperature is above absolute zero. For this reason, it is a very important tecnology in military use, because it allows objects be seen even without propoer illumination or in total lack of light situations.

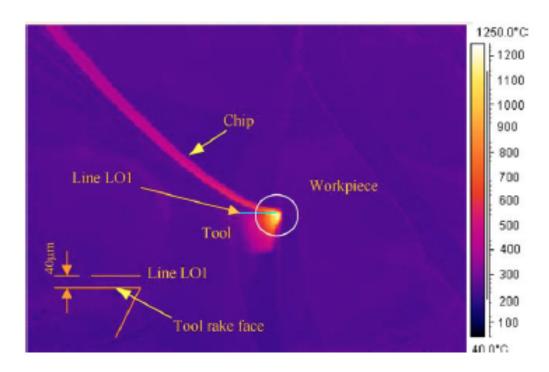


FIGURE 2.1 – Infrared photography of a cutting process (ABUKHSHIM et al., 2006)

The thermography tool is able to work in two dfferent ways: passive and active. The passive way occurs when the subject matter has its temperature different from the environment (often higher). On the other hand, the active way needs an external heat source to induce a reasonable contrast between the object and the background (MALDAGUE,

2000). For the case under study, high speed thermography has its positive and negative points. On the positive side, it may be mentioned:

- Fast inspection rate (reasonable number of images of high speed cutting)
- Contactless (no interference during the cutting process)
- Easy interpretation of the results (indexed image with temperatures in each pixel)

But it is also important to mention the difficulties that in this method still prevail:

- Only a limited thickness can be measured (under the main surface)
- Determine a suitable emissivity is a chalenge (it changes with temperature variation)

2.2 Temperature Modelling

write

2.3 Image Processing

Infrared termography is a contactless way to measure infrared eletromagnetic energy. It makes possible to observe contours of different bodies due to their temperature distribution, since every body is able to emit eletromagnetic radiation when its temperature is above absolute zero. For this reason, it is a very important tecnology in military use, because it allows objects be seen even without propoer illumination or in total lack of light situations. The thermography tool is able to work in two dfferent ways: passive and active. The passive way occurs when the subject matter has its temperature different from the environment (often higher). On the other hand, the active way needs an external heat source to induce a reasonable contrast between the object and the background (MALDAGUE, 2000). For the case under study, high speed thermography has its positive and negative points. On the positive side, it may be mentioned:

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But it is also important to mention the difficulties that this method still have:

- Only a limited thickness can be measured (under the main surface)
- Determine a suitable emissivity is a chalenge (it changes with temperature variation)

3 Experimental Setup

The experiments were carried out on WZL shop floor, located in Aachen in Germany, acquiring thermal images by means of high speed infrared camera FLIR SC7600 (with framerate of 328 fps and a resoloution of 640 x 512 pixels), it was equipped with a macro lens 1:1 and FOV 9.6 x 7.7 mm. The test bench works in a way that the tool stays in a fixed position in relation to the camera, keeping the relative distance between tool and camera constant, then the scale factor provided by this setting was 15 μ m/pixel. It allows the metric conversion for future post processing of images.

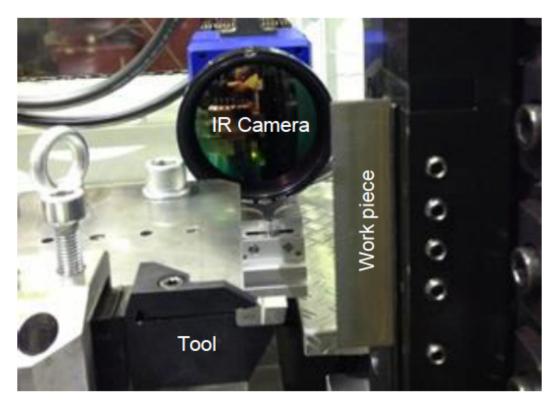


FIGURE 3.1 – Experimental setup (AUGSPURGER et al., 2016)

An important factor for a reliable temperature measurement is the correct choice of the components emissivity. To make it easier, the tool was coated with a black ink, allowing the emissivity valuation for this case, which provided a value of $\epsilon = 0.85$. For the chip case, it was evaluated in its temperature range $\epsilon = 0.4$. It is also important to highlight the

camera settings, factors as integration time and filters are essential to determine a reliable measurements due to the amount of eletromagnetic radiation received on camera's sensors. The higher are the temperatures higher is the energy produced, then smaller should be the integration time, which is the time that sensor of energy receives radiation and converts into temperature afterwards. These configurations allowed measurements in a range from 200 °C until 900 °C.

The tool material was uncoated carbide insert (Sandvik H13A), with rake angle 6° , clearance angle 3° , cutting radius $r_{\beta} < 5\mu m$ and width 4.4 mm. The workpiece material was AISI 1045 normalized and its dimensions were 3.5 x 200 x 80 mm (width, lengh, heigh respectively).

For force acquisition during the process, it was used a three-component piezoelectric force platform, determining the cutting force and passive force. Since the cutting process is carried out in a linear and constant motion, it is possible to determine the overall power P with velocity and cutting force.

All the experiments were were held without coolant, with velocities of $100 \ m/min$ and $150 \ m/min$ and $a_p = [0.2, 0.3, 0.4, 0.5]$ mm. The analysis method was built on MATLAB platform with the support of its image processing toolbox. This was the chosen software due the easy connection between FLIR software and MATLAB, since FLIR software can export its images to .mat format, which are indexed matrices prejected to MATLAB environment. Each pixel from the exported images contains information about position and its temperature.

The design of the experiments are listed on the table bellow:

Experiments	Cutting Velocity [m/min]	Uncut chip thickness [µm]	Integration time [µs]	Cutting Force [N]	Passive Force [N]	Heat treatment
VP41_1_H200_V100_C45_MF_425	100	200	425	1500	1000	Normalized
VP41_2_H200_V100_C45_MF_425	100	200	425	1565	1005	Normalized
VP42_1_H300_V100_C45_MF_425	100	300	425	2250	1159	Normalized
VP42_2_H300_V100_C45_MF_285	100	300	285	2136	1079	Normalized
VP43_1_H400_V100_C45_MF_285	100	400	285	2716	1118	Normalized
VP45_2_H200_V150_C45_MF_425	150	200	425	1448	688	Normalized
VP46_1_H300_V150_C45_MF_285	150	300	285	2006	801	Normalized
VP46_2_H300_V150_C45_MF_285	150	300	285	2004	875	Normalized
VP49_1_H400_V150_C45_MF_285	150	400	285	2675	1046	Normalized
VP49_2_H400_V150_C45_MF_285	150	400	285	2590	1000	Normalized
VP50_1_H500_V150_C45_MF_285	150	500	285	3220	1120	Normalized
VP50_2_H500_V150_C45_MF_285	150	500	285	3178	1162	Normalized

TABLE 3.1 – Design of experiments (AUGSPURGER et al., 2016)

4 Code Implementation

4.1 MATLAB environment

As mentioned on chapter 3, FLIR software provides as output variables indexed matrices in .mat format, which is MATLAB variable format. Each pixel contains temperature information about itself, it is possible to visualize an example on a scaled image on the following figure:

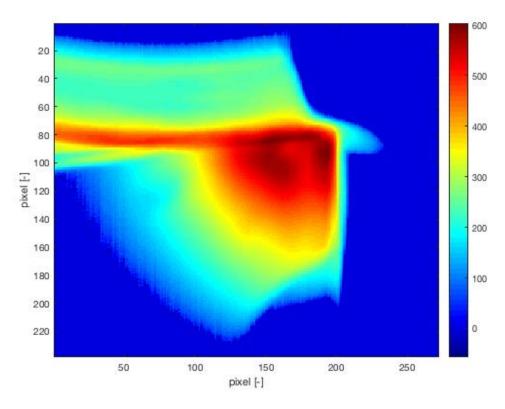


FIGURE 4.1 – Scaled image showing temperature distribution

From figure **4.1** with MATLAB Image Processing Toolbox support it possible to extract many informations about the image, such as:

• Edges recognition

- Image segmentation for tool, chip and workpiece
- Detection of tool tip
- Determine isotherms along tool

4.2 Auxiliar functions

4.2.1 Contour plot

This is an important tool for this paper, contour plot is able to provide same level curves. Since the variable used on the process is a temperature matrix, this tool will calculate continuous lines, whose each pixel has a very close temperature measurements. Doing it with a determined and small tolerance, the lines calculated are isotherms of the image. Then, with these lines it is also possible to get its coordinates, which it will be essential to calculate heat carried away from volume control by means of tool.

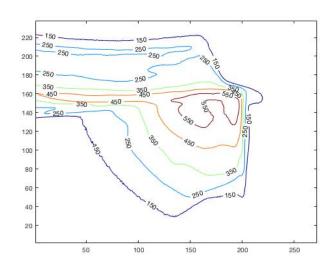


FIGURE 4.2 – Contour plot

4.2.2 Hough lines transformation

Hough transform is a extensively method used in computer vision. It is a extraction feature for complex geometries, using normal parametrization for straight lines (DUDA; HART, 1972). Concerning about the images, the rake and clearance face can be mapped by means of hough lines transformation in MATLAB. It is necessary to provide a probable angle range in what the angular coefficient of seeked lines are defined. More precise is this angle range, more reliable and faster will be the output.

The test bench, where the experiments were held, allows a fixed placement of tool.

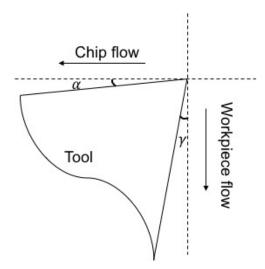


FIGURE 4.3 – Placement of tool

It means the angle between the rake face and horizontal line and the angle between clearance face and vertical line are always the designed rake and clearance angles, respectively. In other words, the tool does not rotate in relation to the reference axes. Because of this, it is possible to perform hough transformation on the image, being very accurate. As the rake and clearance angle are always 6° and 3° , respectively, the hough transform processing will last a shoter time with predetermined angles than otherwise.

4.3 Implementation steps

4.3.1 Overview

The final aim of the program was be able to identify the tool and chip shapes, then the analysis could extract and provide features that were essential for the results of this paper. By means of image processing and some input data, features like maximum cutting zone temperature, maximum chip temperature, heat flows through chip and tool are some examples of what the code is able to provide.

FAZER tabela COM INPUT/OUTPUT

4.3.2 Finding tool edges

As mentioned in the subsection Hough lines transformation, the method to find tool edges has to provide an accurate range of angles that the rake and clearence angles are inserted. The process is simple and it is demonstrated as follow:

```
function obj = calculateCoordinates(obj)
2
               obj.BW = edge(obj.frame,'sobel');
                      -----Finding the clearance face--
3
4
                [H, THETA, RHO] = hough(obj.BW,'Theta',2:5); %Hough transformation
5
               P = houghpeaks(H, 10);
               obj.lines = houghlines(obj.BW, THETA, RHO, P, 'FillGap', 15,'MinLength'
       ,10); Here we can find the lines of cutting edge and afterwards find the
       coordinate of the tool tip
               1 = length(obj.lines);
7
8
               obj.coordCF = [];
                for i=1:1
9
                    Theta = obj.lines(i).theta;
10
                    t1 = obj.lines(i).point1;
11
12
                    t2 = obj.lines(i).point2;
                    rho = obj.lines(i).rho;
13
                    if rho < 204 && rho > 198
14
                        obj.coordCF = [t1;t2];
15
                        obj.ClearanceAngle = Theta;
16
                    end
17
               end
18
                           ----Finding the rake face-----
19
                [H, THETA, RHO] = hough(obj.BW,'Theta',81:85); %Hough transformation
20
^{21}
               P = houghpeaks(H, 10);
               obj.lines = houghlines(obj.BW, THETA, RHO, P, 'FillGap', 15,'MinLength'
22
       ,10); Here we can find the lines of cutting edge and afterwards find the
       coordinate of the tool tip
23
                1 = length(obj.lines);
               obj.coordRF = [];
24
                for i=1:1
25
                    Theta=obj.lines(i).theta;
26
                    t1 = obj.lines(i).point1;
27
                    t2 = obj.lines(i).point2;
28
                    rho = obj.lines(i).rho;
29
                    if rho < 103 && rho > 98
30
31
                        obj.coordRF = [t1;t2];
                        obj.RakeAngle = 90 - Theta;
32
                    end
33
34
               end
35
```

Since the rake angle is 6° and the clearance is 3° ranges of [81:85] and [2:5] were given to each respectively. Concerning about the rake angle, the range of angles is given by the complementar(?) angles due to its reference in hough method.

- 4.3.2.1 Rake and clearance face
- 4.3.2.2 Tool tip coordinates
- 4.3.3 Maximum temperatures
- 4.3.4 Temperature fields
- 4.3.5 Heat flows Chip and Tool
- 4.3.5.1 Heat partitions

5 Results

write

6 Conclusion

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Appendix A - Source Code

A.1 Temperature Analysis

```
classdef TemperatureAnalyze
       % This class was built to analyze the temperature inside the tool
2
3
       % shape, the temperature gradient, the isotherms...
4
       properties(GetAccess = 'public', SetAccess = 'private')
           CoordinateToolTip;
6
            TemperatureToolTip;
           RakeAngle; %Rake face slope
8
           ClearanceAngle; %Clearance face slope
10
           ShearAngle;
           FrictionAngle;
11
           MeanTemperatureTool;
12
13
           MaximumTemperatureTool;
14
           MaximumTemperatureChip;
           MaximumTemperatureCuttingZone;
15
16
           HeatCarriedAwayByChip;
           HeatFluxAwayFromToolTip;
17
18
           HeatFluxThroughWorkpiece;
           TotalPowerBalance;
19
20
           InternalEnergyTool;
           CuttingForcePowerDirection;
^{21}
22
           CuttingForceUncutChipThicknessDirection;
           CuttingForceParallelToolFace;
23
24
            CuttingForceParallelShearPlane;
           CuttingForcePerpendicularShearPlane;
25
           CuttingForcePerpendicularToolFace;
           CoefficientFriction;
27
            ShearStress;
           NormalStress;
29
           PecletNumber;
30
31
           RatioR;
            ShearEnergyVolume;
32
33
           FrictionEnergyVolume;
           Cutting Velocity;
34
35
           UnCutChipThickness;
           ContactLength;
36
37
38
       properties(GetAccess = 'private', SetAccess = 'private')
39
40
           coordRF;
41
           coordCF;
           BW;
42
43
           lines;
           frame:
44
45
           pointCF; %auxiliar to plot the cutting edge
           pointRF;
46
           pointM;
47
           Tx; %auxiliar to plot the gradients of the frame
48
49
            Ту;
           biImageTool; %Binary image of the tool shape
50
           biImageChip;
```

```
biShearLine;
52
            xyMaxTemp; %coordinates of the point inside the chip with maximum Temperature
53
            lineChip;
54
            lineTool:
55
            validTemperature;
56
57
            heatCapacity;
            nExcPoints;
58
            heatAccumulatedPerLine;
59
60
            ptosLines;
            extPtosLineChip;
61
62
            line200;
        end
63
64
65
        methods
            % methods, including the constructor are defined in this block
66
67
            function obj = TemperatureAnalyze2(Frame, index)%constructor
68
69
                 %Inputs
                 Fp = 3220; %Cutting force in the power direction (Newtons)
70
                 Fq = 1120;%Passive force (Newtons)
71
                 widthTool = 4.4*10^{-3}; %meters
72
                 Vp = 150/60;%meters/second
73
                 tuc = 500*10^{-6}; %meters
74
                 clength = 0.00251; % Define as an empty vector if we do not have
75
                 %the mean value
76
                 tt = [197 78];
77
                 obj.validTemperature = 200;% For any experiment
78
                 A = 0.1; *percentage of the deformation energy that is converted in heat
79
80
81
                 obj.CuttingVelocity = Vp * 60; %m/minute
                 obj.UnCutChipThickness = tuc;
82
                 obj.frame = Frame(index).f;
83
                 if isequal(clength,[])
84
85
                     clength = obj.contactLength();
86
                 end
                 obj.ContactLength = clength;
87
88
                   obj = obj.calculateCoordinates();
                   if isempty(obj.coordRF) == 0 && isempty(obj.coordCF) == 0
89
    9
90
                         obj = obj.coordinateToolTip();
                   else %Default conditions
91
92
    응
                       if isempty(obj.coordRF)
    응
                           obj.RakeAngle = 6;
93
94
    응
                       if isempty(obj.coordCF)
95
    응
                           obj.ClearanceAngle = 3;
96
    응
                       end
97
98
                   end
                 obj.CoordinateToolTip = tt;
99
                 obj.ClearanceAngle = 3;
100
101
                 obj.RakeAngle = 6;
                 obj.frame = Frame(index).f;
102
                 obj = obj.toolContour();
103
                 obj = obj.findLineTool();
104
                 obj = obj.chipContour();
105
                 obj = obj.findLineChip();
106
                 obj = obj.pointsRFandCF();
107
                 obj = obj.TempTT();
108
109
                 obj = obj.meanTemperatureTool();
                 obj = obj.maxTemperatureTool();
110
111
                 obj = obj.maximumTemperature();
                 obj = obj.maxTemperatureChip();
112
113
                 obj = obj.calculateGradient();
                 obj = extremePointsChip(obj);
114
                 obj = obj.heatBalance(tuc, Vp, widthTool);
115
                 obj = obj.internalEnergyTool(widthTool);
116
117
                 obj = obj.shearLine();
                 obj = obj.calculatePecletNumber();
118
                 obj = obj.forcesValues(Fp,Fq,widthTool,tuc);
119
                 obj.TotalPowerBalance = 0.97*(obj.CuttingVelocity*(obj.
120
        CuttingForcePowerDirection*(1-A) + obj.CuttingForceParallelToolFace*A*obj.RatioR
```

```
)/60);
                 obj.HeatFluxThroughWorkpiece = obj.TotalPowerBalance - obj.
121
        HeatCarriedAwayByChip - obj.HeatFluxAwayFromToolTip;
122
123
            function obj = framesOverlap(obj,Frame,index)
124
                 cTT = obj.CoordinateToolTip;
125
                 alpha = (90 - obj.ClearanceAngle) *pi/180;
126
                 gamma = obj.RakeAngle*pi/180;
127
                 p1 = cTT + 67*[-cos(gamma) sin(gamma)];
128
                 p2 = cTT + 33*[-cos(alpha) sin(alpha)];
129
                 c = [cTT(1) p1(1) p2(1)];
130
131
                 r = [cTT(2) p1(2) p2(2)];
132
                 biTool70 = roipoly(Frame(index).e70,c,r);
                 aux = biTool70 == 1 & obj.biImageChip == 1;
133
134
                 biTool70 = biTool70 - aux;
                 biTool70andChip = biTool70 == 1 | obj.biImageChip == 1;
135
                 biFrame85 = ones(size(Frame(index).e85)) - biTool70andChip;
136
                 obj.frame = biTool70andChip.*Frame(index).e70 + biFrame85.*Frame(index).
137
        e85;
            end
138
139
            function obj = toolContour(obj)
140
                 A = round(obj.CoordinateToolTip);
141
                 m = size(obj.frame,1);
142
                 xt = A(1);
143
                 yt = A(2);
144
                 y1 = round(yt + (xt - 1)*tan(obj.RakeAngle*pi/180));
145
                 x2 = round(xt - (m - yt)*tan(pi/2 - (90 - obj.ClearanceAngle)*pi/180));
146
147
                 c = [xt 0 0 x2];
                 r = [yt y1 m m];
148
                 B = roipoly(obj.frame,c,r);
149
150
                 obj.biImageTool = B;
151
152
             function obj = chipContour(obj)
153
154
                 c = obj.line200(1,:);
                 r = obj.line200(2,:);
155
                 B = roipoly(obj.frame,c,r);
156
                 obj.biImageChip = B;
157
                 B2 = obj.biImageTool ==1 & B == 1;
158
                 B = B - B2;
159
                 obj.biImageChip = B;
160
            end
161
162
            function obj = maximumTemperature(obj)
163
164
                 obj.MaximumTemperatureCuttingZone = max(max(obj.frame));
                 [\sim, lin] = max(obj.frame);
165
                 [\sim, col] = max(max(obj.frame));
166
                 lin = lin(col);
167
                 obj.xyMaxTemp = [col lin];
168
            end
169
170
            function 1 = contactLength(obj)
171
172
                 imagesc(obj.frame)
                 imdistline \verb§{Help} to measure the amount of pixels on the contact length
173
                 v = input('What is the value of the contact length for this frame?');
174
175
                 close all
                 1 = 15*10^{-6}v;
176
177
            end
178
            function obj = maxTemperatureTool(obj)
179
                 C = obj.biImageTool;
180
                 Frame = C.*obj.frame;
181
                 T = max(max(Frame));
182
183
                 obj.MaximumTemperatureTool = T;
184
185
            function obj = maxTemperatureChip(obj)
186
                 Frame = obj.biImageChip.*obj.frame;
187
```

```
obj.MaximumTemperatureChip = max(max(Frame));
188
            end
189
190
            function obj = meanTemperatureTool(obj)
191
                B = obj.biImageTool;
192
                Frame = B.*obj.frame;
193
                B = Frame > obj.validTemperature;
194
                Frame = B.*Frame;
195
                s = sum(sum(Frame));
196
                n = sum(sum(B));
197
                meanT = s/n;
198
                obj.MeanTemperatureTool = meanT;
199
200
            end
201
            function obj = displayBinary(obj)
202
203
                imshow(obj.BW);
                hold on
204
205
                plot (obj.coordRF(:,1),obj.coordRF(:,2),'bx')
                plot (obj.coordCF(:,1),obj.coordCF(:,2),'yx')
206
207
                plot (obj.CoordinateToolTip(1), obj.CoordinateToolTip(2), 'xm')
                hold off
208
209
            end
210
            function obj = TempTT(obj)
211
                p1 = round(obj.CoordinateToolTip + 5*[-cos(obj.RakeAngle*pi/180) sin(obj
212
        .RakeAngle*pi/180)]);
                p2 = round(obj.CoordinateToolTip + 5*[-cos((90 - obj.ClearanceAngle)*pi]
213
        /180) sin((90 - obj.ClearanceAngle)*pi/180)]);
                p3 = round(obj.CoordinateToolTip + 5*[-(cos(obj.RakeAngle*pi/180)+cos]]
214
        ((90 - obj.ClearanceAngle)*pi/180)) (sin(obj.RakeAngle*pi/180)+sin((90 - obj.
        ClearanceAngle) *pi/180))]);
                T1 = obj.frame(p1(2),p1(1));
215
216
                T2 = obj.frame(p2(2), p2(1));
217
                T3 = obj.frame(p3(2),p3(1));
                TT = obj.frame(round(obj.CoordinateToolTip(2)),round(obj.
218
        CoordinateToolTip(1)));
219
                T = [T1 \ T2 \ T3 \ TT];
                obj.TemperatureToolTip = mean(T);
220
            end
221
222
223
            function obj = calculateCoordinates(obj)
                obj.BW = edge(obj.frame,'sobel');
224
                                -Finding the clearance face----
225
                [H, THETA, RHO] = hough(obj.BW,'Theta',2:5); %Hough transformation
226
                P = houghpeaks(H, 10);
227
                obj.lines = houghlines(obj.BW, THETA, RHO, P, 'FillGap', 15, 'MinLength'
228
        ,10); %Here we can find the lines of cutting edge and afterwards find the
        coordinate of the tool tip
                1 = length(obj.lines);
230
                obj.coordCF = [];
                 for i=1:1
231
                     Theta = obj.lines(i).theta;
232
                     t1 = obj.lines(i).point1;
233
                     t2 = obj.lines(i).point2;
234
235
                     rho = obj.lines(i).rho;
                     if rho < 204 && rho > 198
236
                         obj.coordCF = [t1;t2];
237
238
                         obj.ClearanceAngle = Theta;
                     end
239
                end
240
                             ---Finding the rake face----
241
                 [H, THETA, RHO] = hough (obj.BW, 'Theta', 81:85); %Hough transformation
242
                P = houghpeaks(H, 10);
243
                obj.lines = houghlines(obj.BW, THETA, RHO, P, 'FillGap', 15,'MinLength'
244
        ,10); Here we can find the lines of cutting edge and afterwards find the
        coordinate of the tool tip
                1 = length(obj.lines);
245
                obj.coordRF = [];
246
                for i=1:1
247
                     Theta=obj.lines(i).theta;
```

```
t1 = obj.lines(i).point1;
249
                     t2 = obj.lines(i).point2;
250
                     rho = obj.lines(i).rho;
251
                     if rho < 103 && rho > 98
252
                         obj.coordRF = [t1;t2];
253
                         obj.RakeAngle = 90 - Theta;
254
                     end
255
                end
256
257
            end
258
            function obj = coordinateToolTip(obj)
259
                \texttt{a = (obj.coordRF\,(1,2)-obj.coordRF\,(2,2))/(obj.coordRF\,(1,1)-obj.coordRF}
260
        (2,1)); The slope of the rake face hardly will be Inf(Infinite) or NaN(Not-a-
        number),
                 %because we took for this face a slope smaller than 45
261
262
                b = obj.coordRF(1,2) - a*obj.coordRF(1,1);
                m = (obj.coordCF(1,2)-obj.coordCF(2,2))/(obj.coordCF(1,1)-obj.coordCF
263
        (2,1)); % Slope of the cf, in some cases may be Inf(inclination of 90?, for
        example)
264
                h = Q(x)(a*x+b); %line of the clearance face represented by f
                 if m == Inf | |m == -Inf \% if the slope of the cf is 90? or -90?(Inf or -Inf
265
                     xi = obj.coordCF(1,1);%xi represents the coordinate x of the
266
        intersection(tool tip)
267
                else
                     n = obj.coordCF(1,2) - m * obj.coordCF(1,1);
268
                     xi = (n-b)/(a-m);
269
                end
270
                yi = h(xi);
271
272
                 obj.CoordinateToolTip = [xi yi];
            end
273
274
275
            function obj = displayImageAndToolTip(obj)
276
                 figure
                 imagesc(obj.frame);
277
278
                hold on
279
                plot (obj.CoordinateToolTip(1), obj.CoordinateToolTip(2), 'xm')
                hold off
280
281
            end
282
283
            function obj = pointsRFandCF(obj)
                 alpha = (90 - obj.ClearanceAngle)*pi/180;
284
                 gamma = obj.RakeAngle*pi/180;
285
                obj.pointRF = obj.CoordinateToolTip + 90*[-cos(gamma) sin(gamma)];
286
                 obj.pointCF = obj.CoordinateToolTip + 90*[-cos(alpha) sin(alpha)];
287
                obj.pointM = obj.CoordinateToolTip + 40*[-2*cos(alpha)-cos(gamma) 2*sin(
288
        alpha) +sin(gamma)];
289
            end
290
            function vT = temperatureRFandCF(obj)
291
                 pixelpitch = 15*10^-3; % mm/pixel
292
                extCF = obj.pointCF;% final point on the clearance face
293
                extRF = obj.pointRF; % final point on the rake face
294
                extM = obj.pointM;
295
296
                11 = round(abs(obj.CoordinateToolTip(1)-extRF(1)));%length in pixels
        rake line
                12 = round(abs(obj.CoordinateToolTip(2)-extCF(2)));%length in pixels
297
        clearance line
                13 = max(round(abs(obj.CoordinateToolTip-extM)));
298
                vRFx = round(linspace(obj.CoordinateToolTip(1),extRF(1),11));%
299
        coordinates x of the rake line
300
                vRFy = round(linspace(obj.CoordinateToolTip(2),extRF(2),11));%
        coordinates y of the rake line
                vCFx = round(linspace(obj.CoordinateToolTip(1),extCF(1),12));%
301
        coordinates x of the clearance line
302
                vCFy = round(linspace(obj.CoordinateToolTip(2),extCF(2),12));%
        coordinates y of the clearance line
                vMx = round(linspace(obj.CoordinateToolTip(1),extM(1),13));
303
                vMy = round(linspace(obj.CoordinateToolTip(2),extM(2),13));
304
```

```
305
                 T_RF = zeros(1,11); *temperature for each pixel (each coordinate pair) -
        rake line
                 T_CF = zeros(1,12); *temperature for each pixel (each coordinate pair) -
306
        clearance line
                 T_M = zeros(1,13);
307
                  for t=1:11
308
                      T_RF(t) = obj.frame(vRFy(t), vRFx(t)); %Building the temperature
309
        vector - rake line
310
                  for t=1:12
311
                      T_CF(t) = obj.frame(vCFy(t), vCFx(t)); *Building the temperature
312
        vector - clearance line
313
                 end
314
                  for t=1:13
315
                      T_M(t) = obj.frame(vMy(t), vMx(t)); Building the temperature vector -
         clearance line
316
                 end
                 d1 = zeros(1,11);%distance for each pixel along the line
317
                 d2 = zeros(1,12);
318
319
                 d3 = zeros(1,13);
                  for t=1:11 - 1
320
321
                      d1(t+1) = (((vRFx(t+1) - vRFx(1))^2) + ((vRFy(t+1) - vRFy(1))^2))^((1/2);
                 end
322
                  for t=1:12 - 1
323
                      d2(t+1) = (((vCFx(t+1) - vCFx(1))^2) + ((vCFy(t+1) - vCFy(1))^2))^((1/2);
324
                  end
325
                  for t=1:13 - 1
326
                      d3(t+1) = (((vMx(t+1) - vMx(1))^2) + ((vMy(t+1) - vMy(1))^2))^(1/2);
327
                 end
328
329
                 d1 = d1*pixelpitch;
                 d2 = d2*pixelpitch;
330
                 d3 = d3*pixelpitch;
331
332
                 figure
333
                 hold on
                 plot (d1, T_RF)
334
335
                 plot (d2, T_CF)
336
                 plot(d3, T_M)
                 xlabel('Distance from the tool tip (mm)')
337
                 ylabel('Temperature (?C)')
338
                 legend('Rake face','Clearance face','Middle vector')
339
340
                 hold off
                 figure
341
                 imagesc(obj.frame)
342
                 colormap jet
343
                 hold on
344
                 plot(vRFx, vRFy, 'k', 'LineWidth', 1)
plot(vCFx, vCFy, 'k', 'LineWidth', 1)
plot(vMx, vMy, 'k', 'LineWidth', 1)
345
346
347
                 hold off
348
                 m = min([11 12 13]);
349
                  vT = [d1(1:m)' T_RF(1:m)' d2(1:m)' T_CF(1:m)' d3(1:m)' T_M(1:m)'];
350
             end
351
352
             function obj = extremePointsChip(obj)
353
354
                  [y,x] = find(obj.lineChip);
355
                  obj.extPtosLineChip = [x(1) y(1);x(end) y(end)];
356
357
             function obj = displayIsotherms(obj)
358
                 tRF = obj.RakeAngle*pi/180;
359
                 tCF = (90 - obj.ClearanceAngle) *pi/180;
360
361
                 vRF = [-cos(tRF) sin(tRF)];
                 vCF = [-cos(tCF) sin(tCF)];
362
                  %p1 RF direction
363
                 t = (obj.CoordinateToolTip(1) - 1)/vRF(1);
364
365
                 p1 = obj.CoordinateToolTip - t*vRF;
                 %p2 CF direction
366
                 t = (256 - obj.CoordinateToolTip(2))/vCF(2);
367
                 p2 = obj.CoordinateToolTip + t*vCF;
368
                 %auxiliar to plot
```

```
370
                 auxX = [p1(1) obj.CoordinateToolTip(1) p2(1)]';
                 auxY = [p1(2) obj.CoordinateToolTip(2) p2(2)]';
371
                 Tmax = max(max(obj.biImageTool.*obj.frame));
372
                 Tv = obj.validTemperature;
373
                 v = round(Tv:40:Tmax);
374
                 %Display tool and isotherms
375
                 lc = obj.extPtosLineChip;
376
                 figure
377
                 imagesc(obj.frame)
378
                 colormap jet
379
380
                 hold on
                 plot (auxX, auxY,'k')
381
382
                 plot(lc(:,1),lc(:,2),'k--','LineWidth',1)
                 [C,h] = contour(obj.frame,v);
383
                 h.LineColor = [0.247 \ 0.247 \ 0.247];
384
                 clabel(C,h,'manual','FontSize',10);
385
                 x = obj.CoordinateToolTip(1);
386
387
                 y = obj.CoordinateToolTip(2);
                 axis([x-180 x+15 y-60 y+130])
388
                 cb = colorbar('vert');
389
                 zlab = get(cb,'ylabel');
390
                 set(zlab,'String','Temperature (?C)');
391
                 cb.Limits = [0 \ 450];
392
                 cb.FontSize = 10;
393
                 zlab.FontSize = 10;
394
                 daspect([1,1,1])
395
                 ax = gca;
396
                 v = [0.2 \ 0.6 \ 1.0 \ 1.4 \ 1.8 \ 2.2 \ 2.6];
397
                 vt = v/0.015;
398
399
                 vx = x + 15 - vt;
                 ax.XTick = fliplr(vx);
400
                 ax.XTickLabel = fliplr(v);
401
                 ax.XAxisLocation = 'top';
402
                 vy = y - 60 + vt;
403
                 ax.YTick = vy;
404
                 ax.YTickLabel = v;
405
                 ax.YAxisLocation = 'right';
406
                 xlabel('milimeters')
407
                 ylabel('milimeters')
408
                 hold off
409
410
             end
411
412
             function obj = calculateGradient(obj)
                 pp = 15 * 10^{-6};
413
                 tx = zeros(size(obj.frame));
414
                 ty = zeros(size(obj.frame));
415
416
                 k = 0;
                 for j = 1:5
417
                      [auxx,auxy]=gradaux_v2(obj.frame,j);
418
419
                     tx = tx + auxx;
                     ty = ty + auxy;
420
                     k = k + 1;
421
422
                 obj.Tx = tx/(k*pp);
423
424
                 obj.Ty = ty/(k*pp);
425
             end
426
427
             function obj = displayGradient(obj)
                 auxx = [obj.pointCF(1) obj.CoordinateToolTip(1) obj.pointRF(1)];
428
429
                 auxy = [obj.pointCF(2) obj.CoordinateToolTip(2) obj.pointRF(2)];
                 k = 75.4;
430
431
                 qx = -k*obj.Tx;
                 qy = -k*obj.Ty;
432
                 figure
433
                 quiver(qx,qy)
434
435
                 hold on
                 plot (auxx,auxy,'k')
436
                 xmin = obj.CoordinateToolTip(1) - 10;
437
                 xmax = obj.CoordinateToolTip(1) + 5;
438
                 ymin = obj.CoordinateToolTip(2) - 5;
```

```
440
                 ymax = obj.CoordinateToolTip(2) + 10;
                 axis([xmin xmax ymin ymax])
441
                 title('Tool Tip')
442
                 daspect([1,1,1])
443
                 figure
444
                 quiver(qx,qy)
445
                 hold on
446
                 plot(auxx,auxy,'k')
447
                 xmin = obj.CoordinateToolTip(1) - 30;
448
                 xmax = obj.CoordinateToolTip(1) - 10;
449
                 ymin = obj.CoordinateToolTip(2) - 5;
450
                 ymax = obj.CoordinateToolTip(2) + 15;
451
452
                 axis([xmin xmax ymin ymax])
453
                 title('Rake Face')
454
                 daspect([1,1,1])
455
                 figure
                 quiver(qx,qy)
456
457
                 hold on
                 plot (auxx, auxy, 'k')
458
459
                 xmin = obj.CoordinateToolTip(1) - 10;
                 xmax = obj.CoordinateToolTip(1) + 10;
460
461
                 ymin = obj.CoordinateToolTip(2) + 10;
                 ymax = obj.CoordinateToolTip(2) + 20;
462
                 axis([xmin xmax ymin ymax])
463
                 title('Clearance Face')
464
                 daspect([1,1,1])
465
            end
466
467
             function obj = displayGradientContour(obj)
468
469
                 auxx = [obj.pointCF(1) obj.CoordinateToolTip(1) obj.pointRF(1)];
                 auxy = [obj.pointCF(2) obj.CoordinateToolTip(2) obj.pointRF(2)];
470
                 k = 75.4;
471
472
                 qx = -k*obj.Tx;
                 qy = -k*obj.Ty;
473
474
                 figure
475
                 quiver (qx, qy)
476
                 hold on
                 plot (auxx, auxy, 'k')
477
478
                 contour(obj.frame, 10)
                 xmin = obj.CoordinateToolTip(1) - 20;
479
480
                 xmax = obj.CoordinateToolTip(1) + 5;
                 ymin = obj.CoordinateToolTip(2) - 5;
481
                 ymax = obj.CoordinateToolTip(2) + 20;
482
                 axis([xmin xmax ymin ymax])
483
                 daspect([1,1,1])
484
            end
485
486
             function obj = findLineChip(obj)
487
                 [m,n] = size(obj.frame);
488
                 o = obj.RakeAngle*pi/180;
489
                 l = obj.ContactLength/(15*10^-6);
490
                 c = obj.CoordinateToolTip + l*[-cos(o) sin(o)];
491
                 xm = c(1);
492
493
                 ym = c(2);
494
                 x1 = xm - tan(o) * (ym - 1);
                 x2 = x1 + tan(0) * (m - 1);
495
                 vx = round(linspace(x1, x2, m));
496
497
                 vy = linspace(1, m, m);
                 B1 = zeros(m,n);
498
                 for i = 1:m
499
                     B1(vy(i), vx(i)) = 1;
500
501
                 end
                 B2 = B1 == 1 & obj.biImageChip == 1;
502
503
                 obj.lineChip = B2;
            end
504
505
             function obj = findLineTool(obj)
506
507
                 [m,n] = size(obj.frame);
                 Tmax = max(max(obj.biImageTool.*obj.frame));
508
                 Tv = obj.validTemperature;
```

```
510
                 v = round(Tv:40:Tmax);
                 if length(v) == 1
511
                     v = round([Tv Tmax]);
512
                 end
513
                 [C,~] = contour(obj.frame, v);
514
515
                 close
                 1 = length(v);
516
                 B = zeros(m,n,1);
517
                 C = round(C);
518
                 for k = 1:1
519
                      [\sim, J] = find(C == v(k));
520
                     [\sim,p] = \max(C(2,J));
521
522
                     J = J(p);
                     for z = J+1:J+C(2,J)
523
                          B(C(2,z),C(1,z),k) = 1;
524
525
                     end
                     if k == 1
526
                          obj.line200 = C(:,J+1:J+C(2,J));
527
528
529
                     B(:,:,k) = B(:,:,k).*obj.biImageTool;
                 end
530
531
                 obj.lineTool = B;
             end
532
533
             function obj = heatBalance(obj,tuc,Vc,w)
534
                 k = 75.4; %heat conductivity
535
                 pp = 15*10^-6; %pixel pitch
536
537
                 %First part - Heat carried away by the chip
538
                  cp = [-4.39956806034758e-07 \ 0.000707314520321484...
539
                  -0.0488770693887544 481.214007868631]; %AISI 1045
540
541
                 %Heat capacity for the workpiece
                 M = obj.lineChip.*obj.frame;
542
                 MH = polyval(cp, M);
543
                 MH (MH == cp (4)) = 0;
544
                 Ht = MH.*(obj.frame-22); %J/kg - 22 is the temperature of the environment
545
546
                 Ht = sum(sum(Ht));
547
                 n = sum(sum(obj.lineChip));
                 Hc = Ht/n; %mean entalpy on the line chip
548
                   Vchip = 100 \times 200 / (60 \times n \times 15);
549
550
                 p = 7874; %kg/m^3
                 Qc = Hc*Vc*tuc*p; %Vc*tuc is the same for Vchip*tchip
551
552
                 obj.HeatCarriedAwayByChip = Qc*w;
553
                 %Second part - Heat carried away by the tool
                 dT = ((obj.Tx).^2 + (obj.Ty).^2).^(1/2);
555
556
                 Q = zeros(size(obj.lineTool, 3), 1);
                 for i = 1:size(obj.lineTool,3)
557
                     L = obj.lineTool(:,:,i);
558
559
                     Q(i) = sum(sum(L.*dT))*pp*w*k;
560
                 obj.heatAccumulatedPerLine = Q;
561
562
                 Qm = mean(Q(1:2));
                 obj.HeatFluxAwayFromToolTip = Qm;
563
564
565
566
             function n = exceedingPoints(obj, Temperature)
567
                 B = obj.frame.*obj.biImageTool > Temperature;
                 n = sum(sum(B));
568
569
             end
570
571
             function obj = internalEnergyTool(obj,w)
                 pp = 15*10^-4; %in cm
572
                 cp = [2.50542895559373e-10 -1.99579761670655e-06 0.00274369536032376
573
        3.09265830398264];%J/(K*cm3)
574
                 %Heat capacity for tool
                 Te = 22;
575
                 B = obj.frame.*obj.biImageTool > obj.validTemperature;
576
                 B1 = obj.frame.*B;
577
                 B2 = polyval(cp,B1); %Heat capacity for each pixel (J/kgK)
```

```
B2(B2 == cp(4)) = 0;
579
                 H = B2.*(obj.frame - Te)*(pp^2)*100; %Heat Amount for each pixel(J/m)
580
                 Ha = sum(sum(H)); % Mean value for the entire tool
581
                 obj.InternalEnergyTool = Ha*w;
582
583
584
             function B = passBinaryImageTool(obj)
585
                 B = obj.biImageTool;
586
587
588
             function B = passBinaryImageChip(obj)
589
                 B = obj.biImageChip;
590
591
592
             function obj = shearLine(obj)
593
594
                 B = obj.biImageChip;
                 v1 = sum(B);
595
                 v1(v1 == 0) = [];
596
                 11 = length(v1);
597
                 C = imcrop(B, [20 20 11 100]);
598
                 [m,n] = size(C);
599
600
                 pto = zeros(1000, 2);
                 count = 1;
601
                 for i = 2:m-1
602
                      for j = 2:n-1
603
                          if C(i,j+1) == 1 \&\& C(i,j-1) == 1 \&\& C(i+1,j) == 1 \&\& C(i-1,j)
604
        == 1
                               pto(count,:) = [i j];
605
                               count = count + 1;
606
607
                          end
                      end
608
609
                 end
                 for i =1000:-1:1
610
                      if isequal(pto(i,:),[0 0]) == 1
611
612
                          pto(i,:) = [];
613
614
                 end
                 1 = size(pto, 1);
615
                 for i = 1:1
616
                      C(pto(i,1),pto(i,2)) = 0;
617
618
                 end
619
620
                 [H, THETA, RHO] = hough (C, 'Theta', -40:-30); %Hough transformation
                 P = houghpeaks(H, 5);
621
                 lin = houghlines(C, THETA, RHO, P, 'FillGap', 15,'MinLength',10);
622
                 l=length(lin);
623
                 p1 = [];
624
                 p2 = [];
625
                 for i=1:1
626
                      Theta=lin(i).theta;
627
                      t1 = lin(i).point1;
628
                      t2 = lin(i).point2;
629
                      y = abs(t1(2)-t2(2));
630
                      if isempty(p1) && isempty(p2) && abs(Theta + 34) < 5
631
632
                          p1 = t1 + [19 \ 19];
                          p2 = t2 + [19 \ 19];
633
                          ym = y;
634
635
                          obj.ShearAngle = abs(Theta);
                      end
636
                      if abs(Theta + 34) < 5 \&\& y > ym
637
                          p1 = t1 + [19 \ 19];
638
                          p2 = t2 + [19 \ 19];
639
                          obj.ShearAngle = abs(Theta);
640
641
                      end
                 end
642
643
                 if isempty(obj.ShearAngle)
                      obj.ShearAngle = 30;
644
645
                 end
             end
646
647
```

```
function obj = forcesValues(obj,Fp,Fq,w,tuc)
648
                 phi = obj.ShearAngle*pi/180; % shear angle
649
                 gamma = obj.RakeAngle*pi/180;%Rake angle
650
                 Fs = Fp * cos(phi) - Fq * sin(phi); %Cutting force component parallel to
651
        shear plane
                 Ns = Fq \star cos(phi) + Fp \star sin(phi); \& Cutting force component perpendicular to
652
         shear plane
                 Fc = Fp \times sin(gamma) + Fq \times cos(gamma); %Cutting force component parallel to
653
                 Nc = Fp*cos(gamma) - Fq*sin(gamma); %Cutting force component
654
        perpendicular to tool face
                 mu = Fc/Nc; % coefficient of friction
655
656
                 As = w*tuc/sin(phi); %Area shear plane
                 tau = Fs/As;%shear stress
657
658
                 sigma = Ns/As; %Normal stress
659
                 r = \sin(phi)/\cos(phi - gamma); %ratio r = t/tc = lc/l
                 ss = cos(gamma)/(sin(phi)*cos(phi-gamma)); %shear strain
660
661
                 us = tau*ss; %shear energy per volume
                 uf = Fc*r/(tuc*w); %friction energy per volume
662
663
                 beta = atan(Fc/Nc); %friction angle on tool face
                 obj.CuttingForceParallelToolFace = Fc;
664
665
                 obj.CuttingForcePowerDirection = Fp;
                 obj.CuttingForceUncutChipThicknessDirection = Fq;
666
                 obj.CuttingForceParallelShearPlane = Fs;
667
                 obj.CuttingForcePerpendicularShearPlane = Ns;
668
                 obj.CuttingForcePerpendicularToolFace = Nc;
669
                 obj.CoefficientFriction = mu;
670
                 obj.ShearStress = tau;
671
                 obj.NormalStress = sigma;
672
673
                 obj.RatioR = r;
                 obj.ShearEnergyVolume = us;
674
                 obj.FrictionEnergyVolume = uf;
675
676
                 obj.FrictionAngle = beta*180/pi;
677
678
             function obj = calculatePecletNumber(obj)
679
680
                 cp = polyval(obj.heatCapacity,obj.MaximumTemperatureCuttingZone);
                 k = 75.4;
681
                 d = 7.85 * 10^3;
682
                 obj.PecletNumber = ((obj.CuttingVelocity/60)*obj.UnCutChipThickness)/(k
683
        /(cp*d));
            end
684
685
             function vH = displayHeatCumulateperLine(obj)%Fix this function
686
                 d = zeros(size(obj.ptosLines,1),1);
687
                 d2 = zeros(size(obj.ptosLines,1)-1,1);
688
                 pp = 15*10^{-3}; %mm/pixel
                 for i = 1:size(obj.ptosLines,1)
690
                     d(i) = pp*((obj.CoordinateToolTip(1) - obj.ptosLines(i,1))^2 + ((obj
691
        .CoordinateToolTip(2) - obj.ptosLines((i,2))^2))^(1/2);
692
                 for i = 1:size(obj.ptosLines,1)-1
693
                     d2(i) = pp*((obj.ptosLines(i+1,1) - obj.ptosLines(i,1))^2 + ((obj.
694
        ptosLines(i+1,2) - obj.ptosLines(i,2))^2))^(1/2);
695
                 end
                 d2 = mean(d2)*10^-3;
696
697
                 figure
                 plot(d,obj.heatAccumulatedPerLine,'-x')
698
                 hold on
699
                 q = gradient(obj.heatAccumulatedPerLine,d2);
700
                 plot (d, q, '-*r')
701
702
                 vH = [d obj.heatAccumulatedPerLine];
            end
703
        end
704
    end
705
```

FOLHA DE REGISTRO DO DOCUMENTO

1. CLASSIFICAÇÃO/TIPO	2. DATA	3. DOCUMENTO Nº	^{4.} Nº DE PÁGINAS
TC	21 de novembro de 2017	DCTA/ITA/TC-031/2017	39

^{5.} TÍTULO E SUBTÍTULO:

Analysis method of temperatures and heat flows for orthogonal cutting 1045 steel by thermal imaging

6. AUTORA(ES):

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7. INSTITUIÇÃO(ÕES)/ÓRGÃO(S) INTERNO(S)/DIVISÃO(ÕES): Instituto Tecnológico de Aeronáutica – ITA/IEM

8. PALAVRAS-CHAVE SUGERIDAS PELA AUTORA:

Manufacture; Image Processing; Matlab; Thermal Analysis; Orthogonal Cutting; Software.

9. PALAVRAS-CHAVE RESULTANTES DE INDEXAÇÃO:

Fabricação; Processamento de Imagens; Programas; Análise Térmica; Engenharia mecânica.

^{10.} APRESENTAÇÃO:

(X) Nacional () Internacional

ITA, São José dos Campos. Curso de Graduação em Engenharia Mecânica. Orientador: Anderson Vicente Borille; coorientador: Thorsten Augspurger. Publicado em 2017.

^{11.} RESUMO:

The handling of geometry files is usually associated with the usage of CAD software, which commonly have costly licenses due to the amount of sophisticated features that they offer. This expense is easily justifiable when the work involves thorough application of a number of these functions, for example, when developing a new geometry for a given project. However, for many users, the task is simple and only requires a small amount of features, for example, when generating a regular pattern of projections along a surface to obtain a set of points to guide the path of a turning or milling tool throughout a machining process. These clients usually have to spend a lot of money on licenses, only to use a small portion of what the program has to offer. This paper presents a solution which can directly read an IGES geometry file and generate a specific set of points using simple open source functions. Although it is programmed using $MATLAB^{TM}$, it is compiled to an independent executable file, thus being capable of running without any license at all.

^{12.} GRAU DE SIG	GILO:
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