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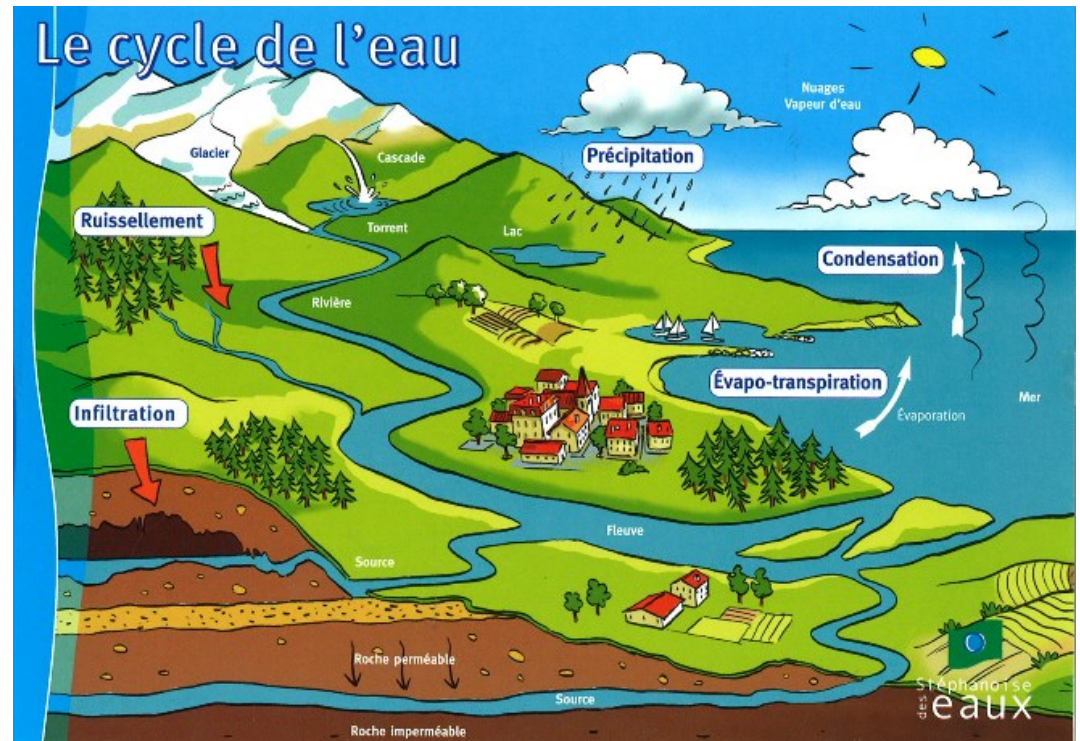
# **Water distribution**

## **Basic concepts**

Sandra Soares-Frazão  
2018

# Where does water come from ?

- Hydrology
  - Natural equilibrium
    - Quantity
    - Quality



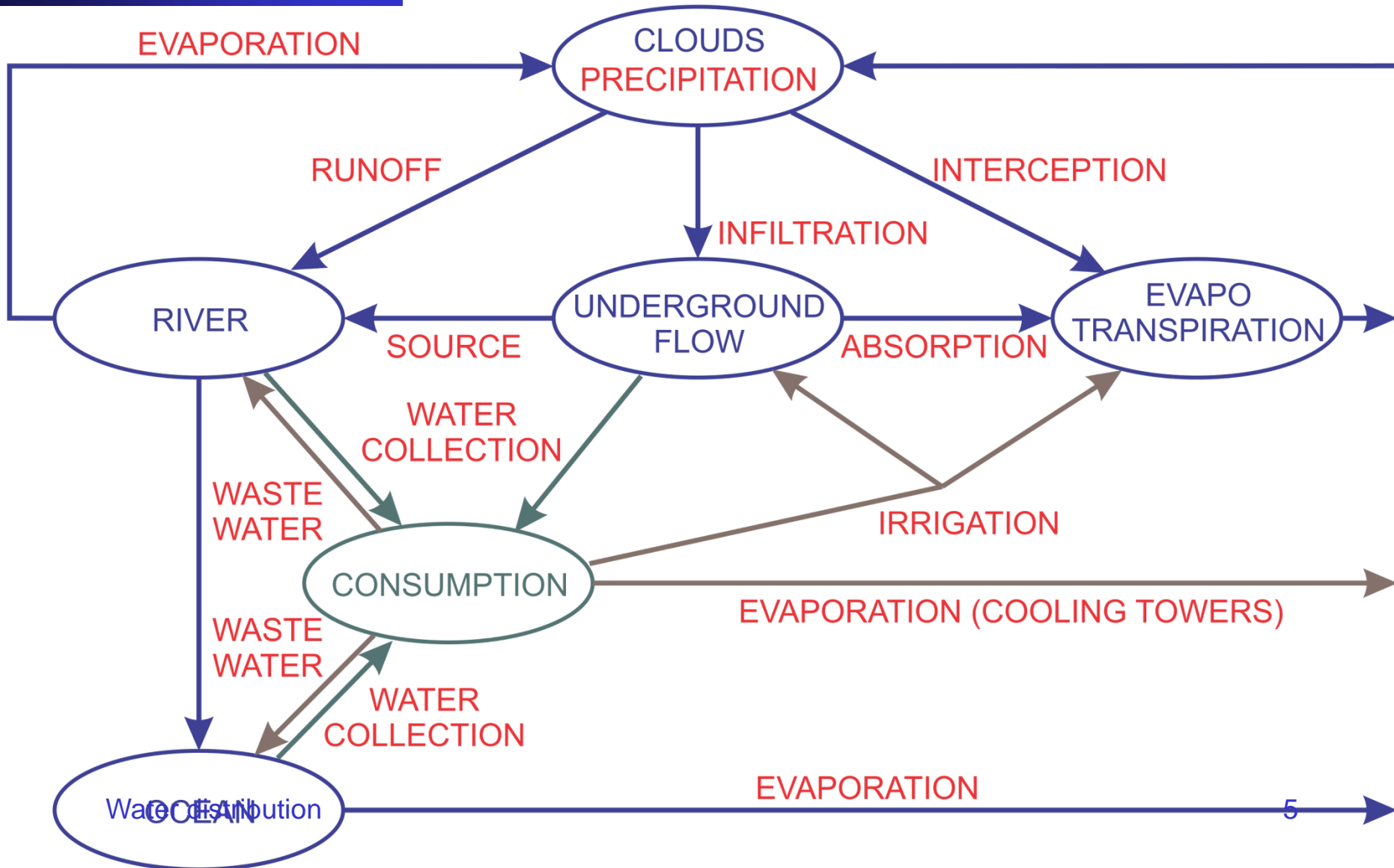
# Water in the ecosystem

- 1 400 000 000 km<sup>3</sup>
  - Salt water      97.30 %      1 362 200 000 km<sup>3</sup>
  - Fresh water      2.70 %      37 800 000 km<sup>3</sup>

# Water in the ecosystem

- 1 400 000 000 km<sup>3</sup>
  - Salt water      97.30 %      1 362 200 000 km<sup>3</sup>
  - Fresh water      2.70 %      37 800 000 km<sup>3</sup>
- 37 800 000 km<sup>3</sup> fresh water
  - Unusable      99.64 %
    - Frost water      29 181 600 km<sup>3</sup>
    - Too deep groundwater      8 647 000 km<sup>3</sup>
  - Usable      0.36 %
    - Lakes, marshes      132 000 km<sup>3</sup>
    - Atmosphere      15 120 km<sup>3</sup>
    - Waterways      3 780 km<sup>3</sup>

# The hydrological cycle



# Use of water

- Water as a liquid
  - Transport
  - Energy
  - Industry
  - Wastewater drainage
- Water with all its properties
  - Water supply
  - Agriculture

# Transport

- Navigation
  - Maritime
  - Fluvial
    - Canals
    - Rivers
- Floating of timber
- Transport by pipes

Wandre bridge  
Meuse





# Energy: hydropower

- 15 % of the world's electricity production



Hoover Dam  
Colorado, USA

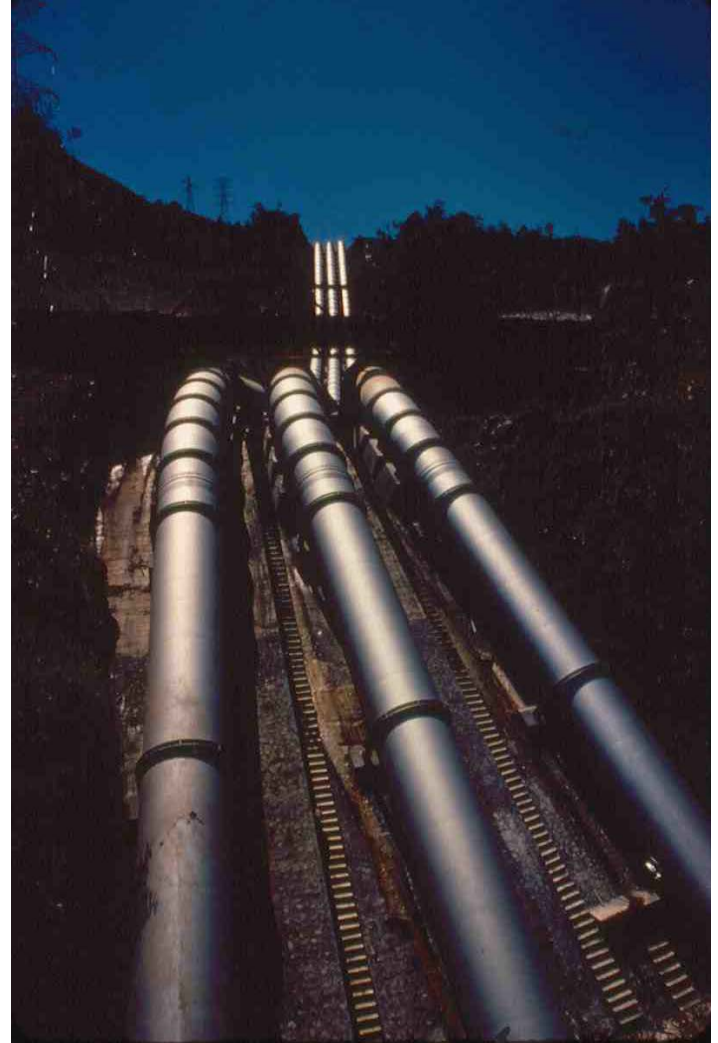




# Hydropower – water intake

- Pennstocks

San Francisco  
Colombie



# Hydropower – water intake

- Water hammer

Bear Creek  
CA - USA

Water distribution



# Industry

- Paper: 1 kg paper = 40 ... 500 litres
- Steel industry: 1 kg steel = 300 ... 600 litres
- Chemistry: 1 litre fuel = 200 litres
- Agro-food industry: 1 kg sugar =  
300 ... 400 litres
- Agrofuel  
1 litre ethanol from corn  
= 1200...3400 litres water

# Wastewater drainage





# Wastewater drainage





# Wastewater drainage





# Wastewater drainage





# Water supply

- Water intake
- Adduction
  - Ducts
  - Channels

Pont du Gard  
France



© H. Chanson 1998

# Irrigation

- Haiti



# For the present work

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- Water distribution
  - Drinkwater: pressurized flow
  - Irrigation: free-surface flow
- Wastewater drainage
  - Free-surface flow

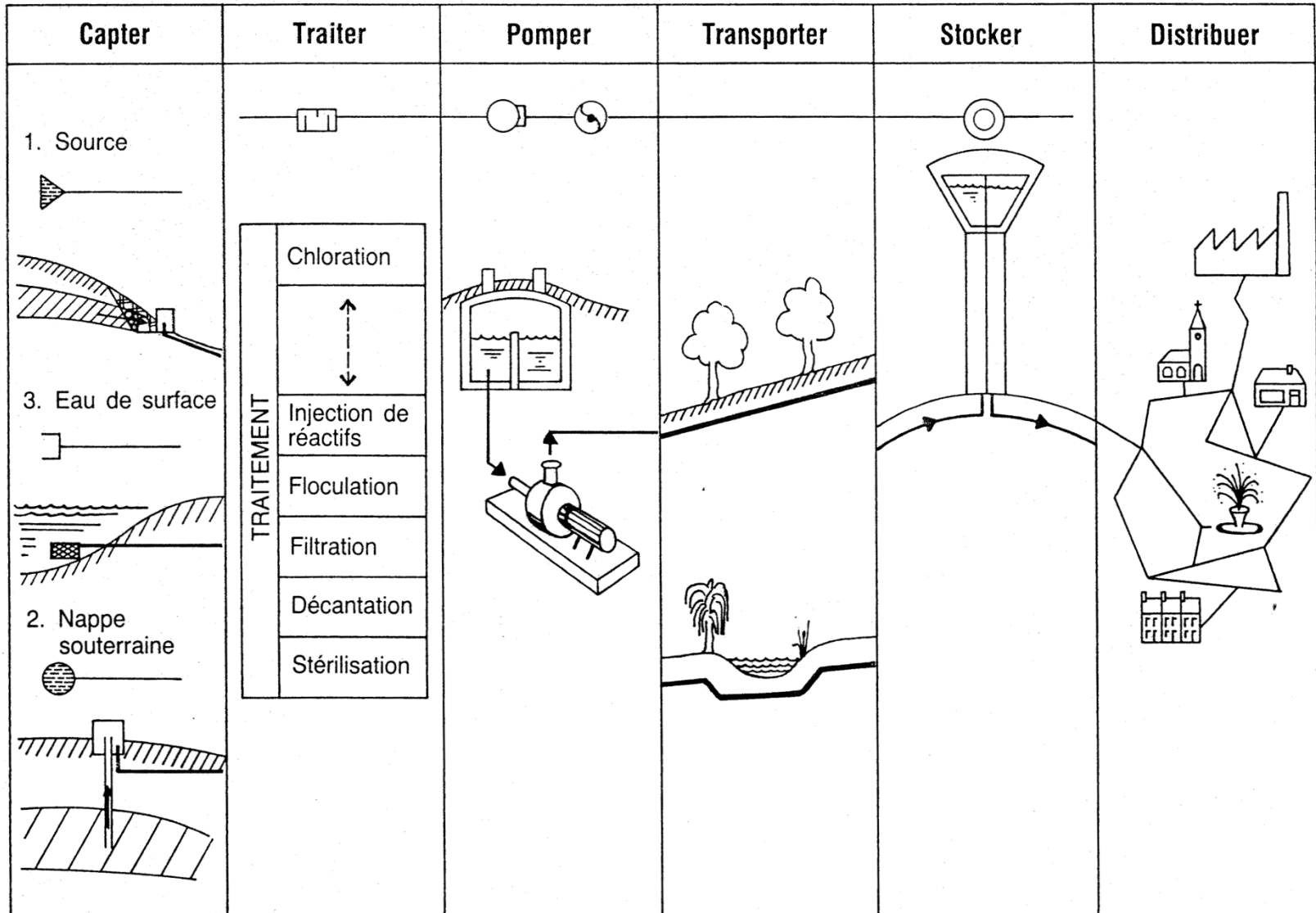
# Pressurized flow

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- Basic concepts
- Example of calculation
- Definition of the water demand



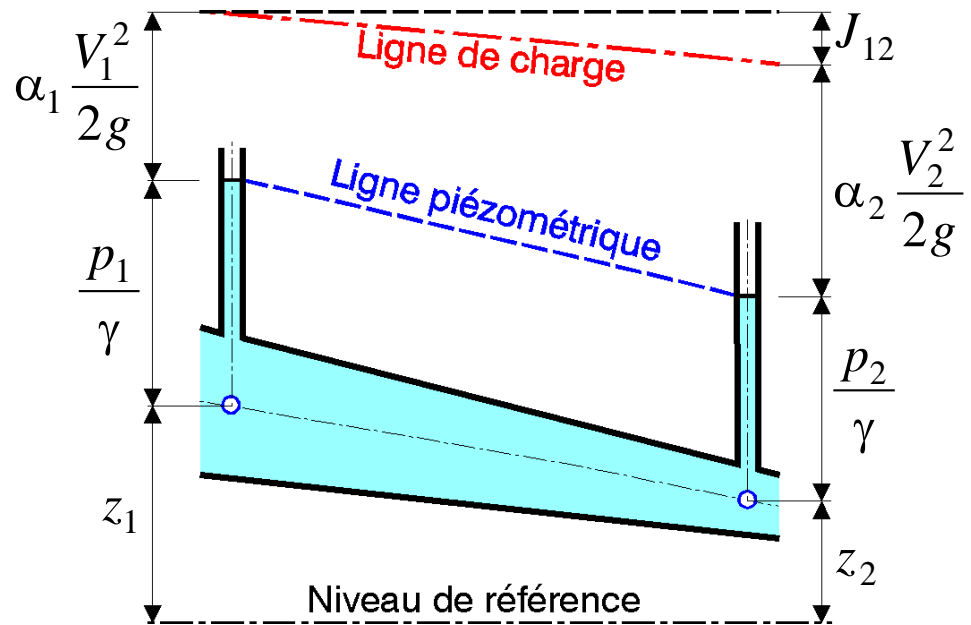
# Water distribution



# Pertes de charge

- Bernoulli equation

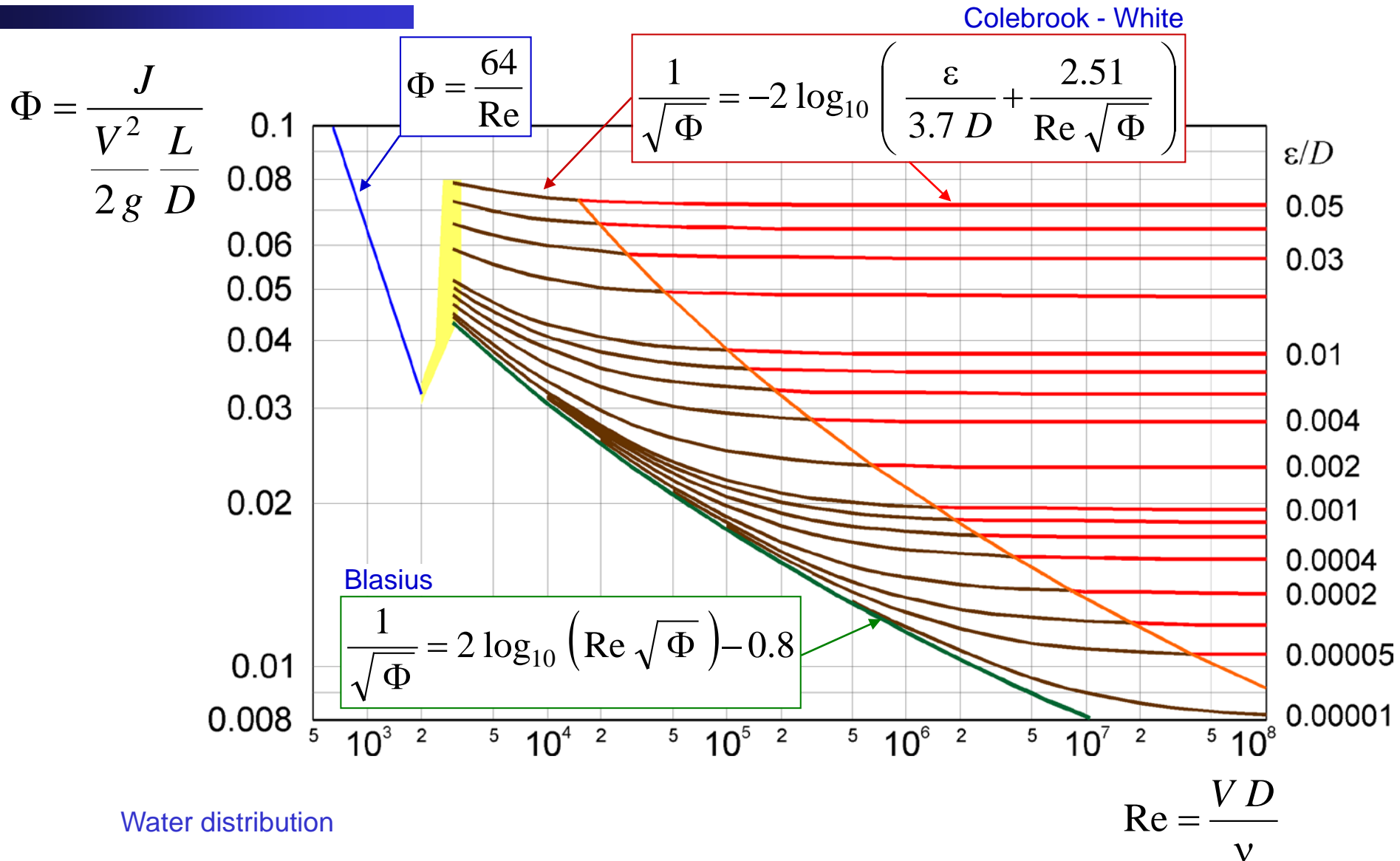
$$z_1 + \frac{p_1}{\gamma} + \frac{V_1^2}{2g} = z_2 + \frac{p_2}{\gamma} + \frac{V_2^2}{2g} + J_{12}$$



- Headlosses: Darcy

$$J = \frac{V^2}{2g} \frac{L}{D} \Phi \left( \text{Re}, \frac{\varepsilon}{D} \right)$$

# Moody-Nikuradse





# Pertes de charge générales

- Rugosité

| Matériau             | Rugosité $\varepsilon$ (mm) |
|----------------------|-----------------------------|
| Ciment               | 0.30 ... 3.0                |
| Fonte                | 0.25                        |
| Fonte asphaltée      | 0.12                        |
| Acier riveté         | 0.90 ... 9.0                |
| Acier galvanisé      | 0.15                        |
| Tube cintré en acier | 0.046                       |
| Tube étiré           | 0.0015                      |

# Pertes de charge

- Pertes de charge générales : Darcy

$$J_{gen} = \frac{V^2}{2g} \frac{L}{D} \Phi \left( \text{Re}, \frac{\varepsilon}{D} \right)$$

$$J_{gen} = Q^2 K L$$

$$K = \frac{\Phi}{2g D A^2}$$

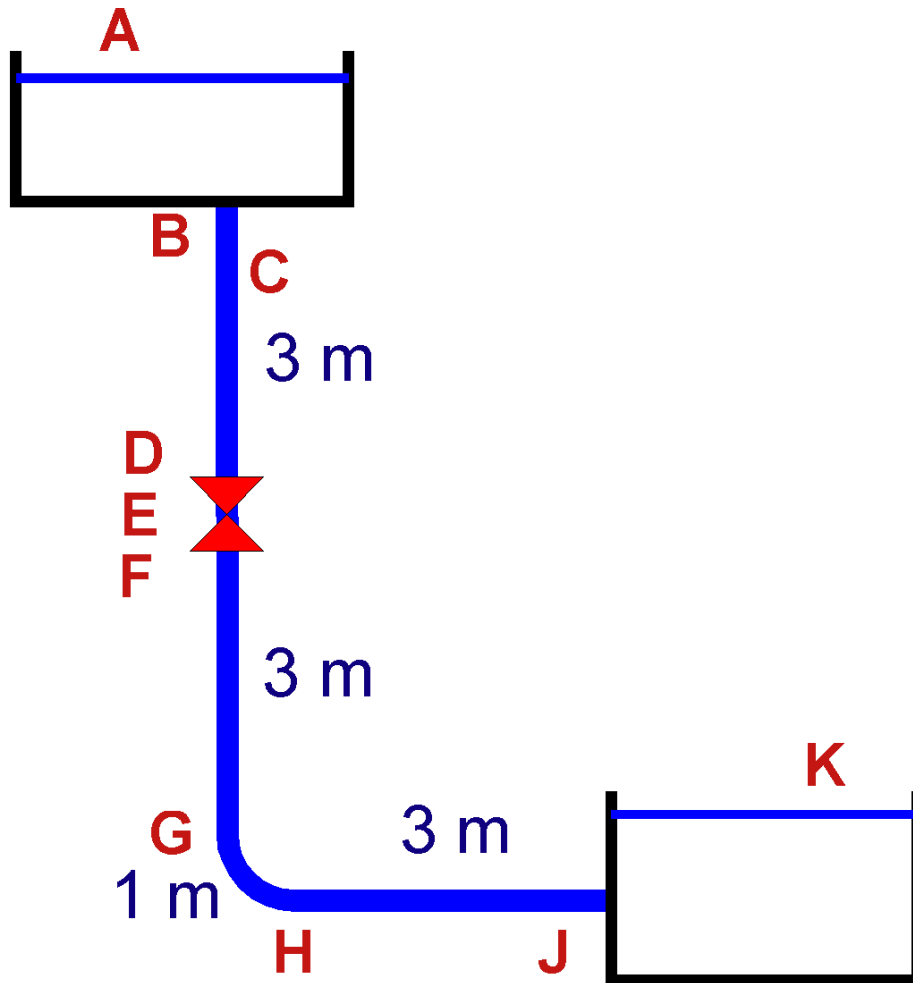
- Pertes de charge locales

$$J_{loc} = \zeta \frac{V^2}{2g}$$

$$J_{loc} = Q^2 K' N$$

$$K' = \frac{1}{2g A^2}$$

# Conduite simple

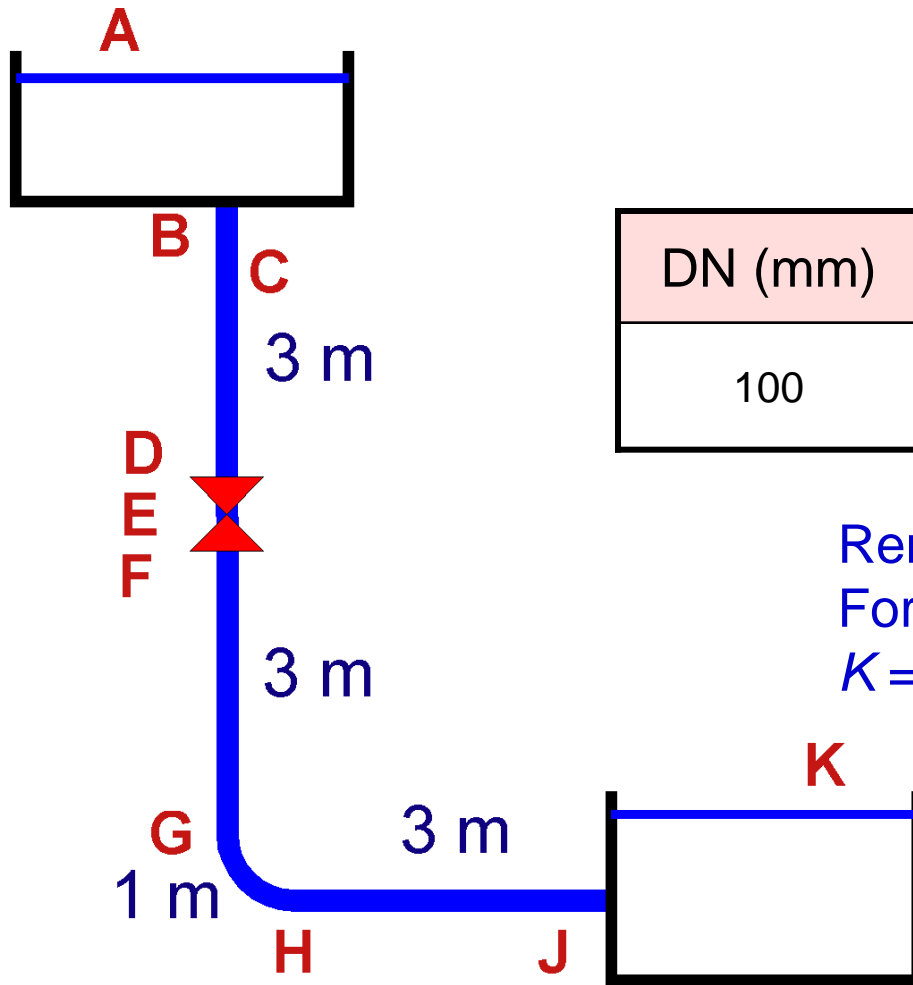


|   | $z$ (m) |
|---|---------|
| A | 7.800   |
| B | 6.637   |
| C | 6.637   |
| D | 3.637   |
| E | 3.637   |
| F | 3.637   |
| G | 0.637   |
| H | 0.000   |
| J | 0.000   |
| K | 0.800   |

$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

# Conduite simple

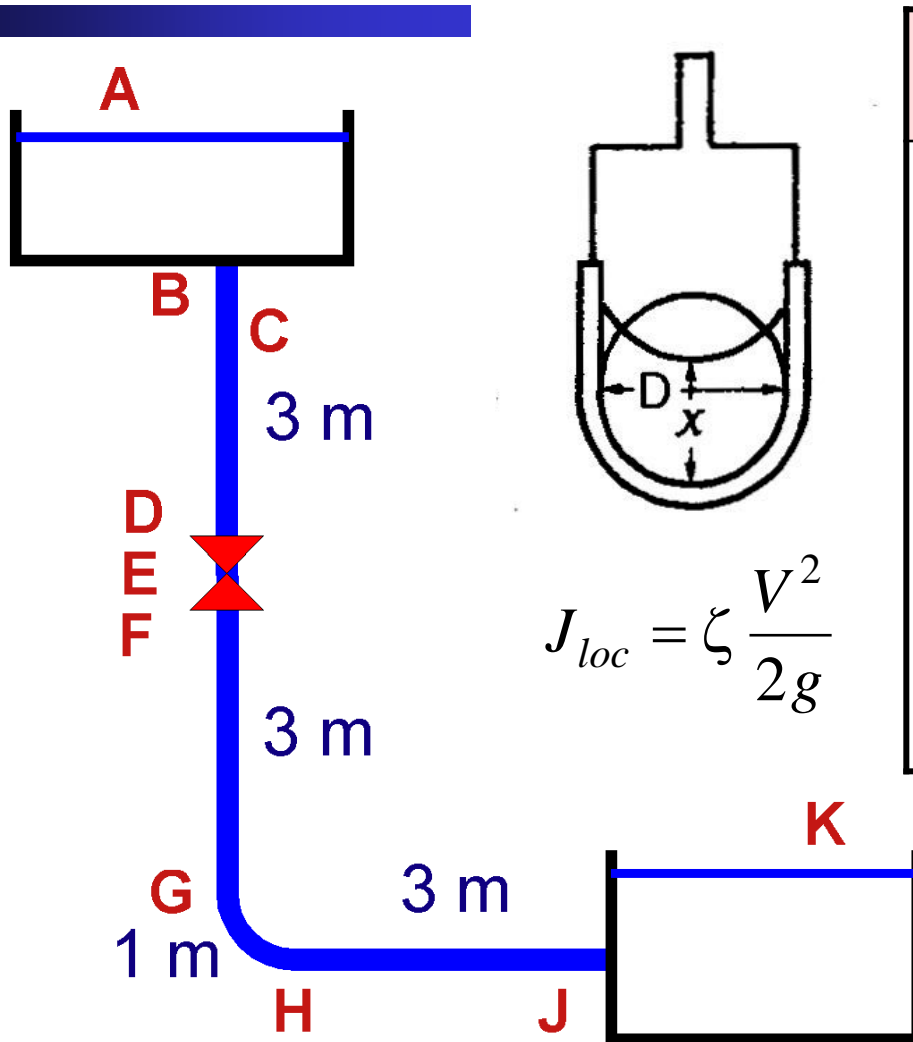


| DN (mm) | $K \text{ (m}^{-6} \text{ s}^2)$ | $K' \text{ (m}^{-5} \text{ s)}$ |
|---------|----------------------------------|---------------------------------|
| 100     | 205.5                            | 826.3                           |

Remarque :  
Formule utilisée = Colebrook – White  
 $K = 211.1 \text{ m}^{-6} \text{ s}^2$

$D = 100 \text{ mm}$   
 $\varepsilon = 0.25 \text{ mm (fonte neuve)}$

# Conduite simple



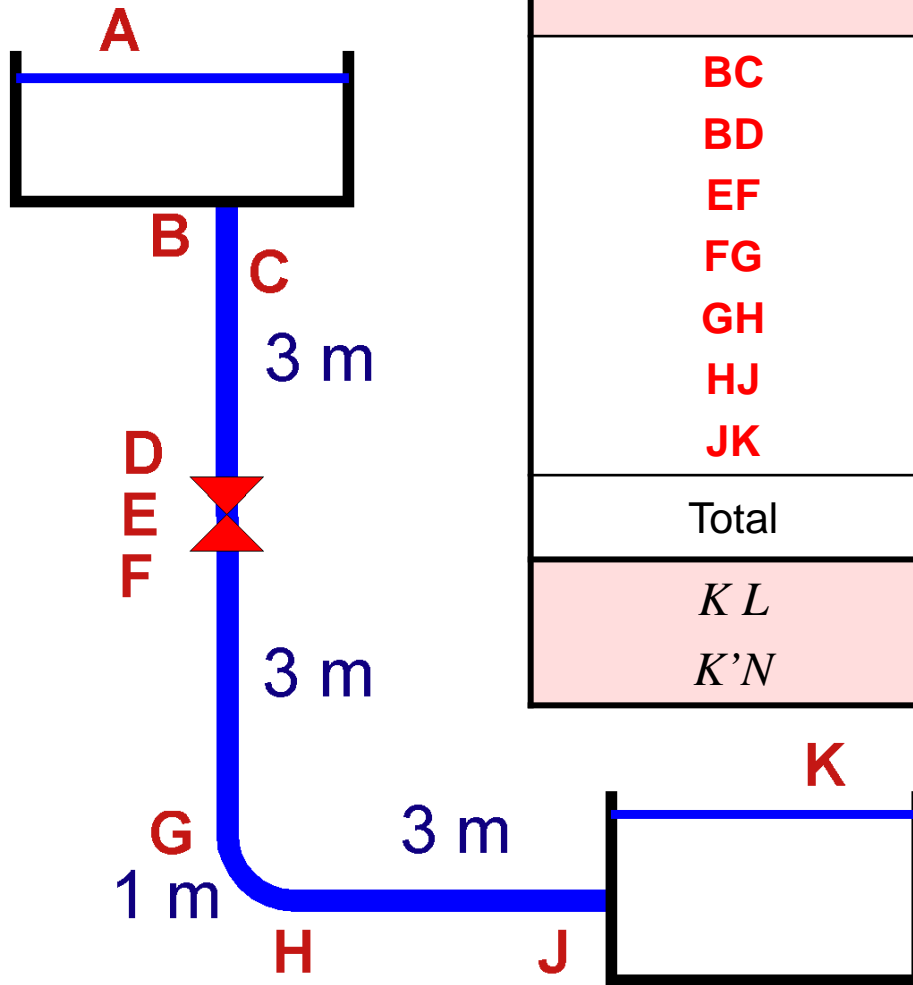
| $x/D$ | $\zeta$ |
|-------|---------|
| 0.181 | 41.21   |
| 0.208 | 31.35   |
| 0.250 | 22.68   |
| 0.333 | 11.89   |
| 0.375 | 8.63    |
| 0.500 | 3.27    |
| 0.583 | 1.55    |
| 0.667 | 0.77    |
| 1.000 |         |

$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

Vanne :  $x/D = 0.25 \quad \zeta = 22.68$

# Conduite simple



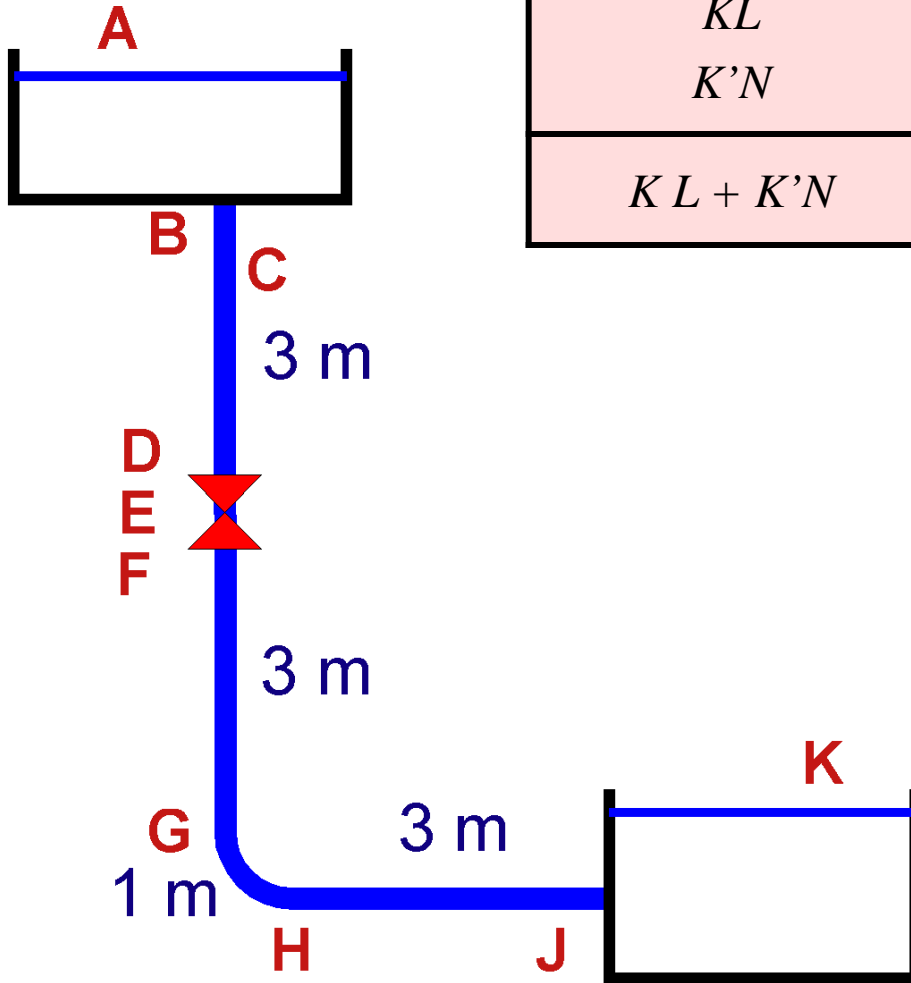
|                | $L \text{ (m)}$ | $N$    |
|----------------|-----------------|--------|
| BC             | 3.00            | 0.49   |
| BD             |                 | 22.68  |
| EF             |                 |        |
| FG             | 3.00            | 0.13   |
| GH             | 1.00            |        |
| HJ             | 3.00            |        |
| JK             |                 | 1.00   |
| Total          | 10.00           | 24.30  |
| $K L$<br>$K'N$ | 2 111           | 20 076 |

$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Conduite simple



|            |        |        |
|------------|--------|--------|
| $KL$       | 2 111  |        |
| $K'N$      |        | 20 076 |
| $KL + K'N$ | 22 187 |        |

$$J = 7.00 \text{ m}$$

$$Q = 0.0178 \text{ m}^3/\text{s}$$

$$V = 2.26 \text{ m/s}$$

$$\text{Re} = 226\,156$$

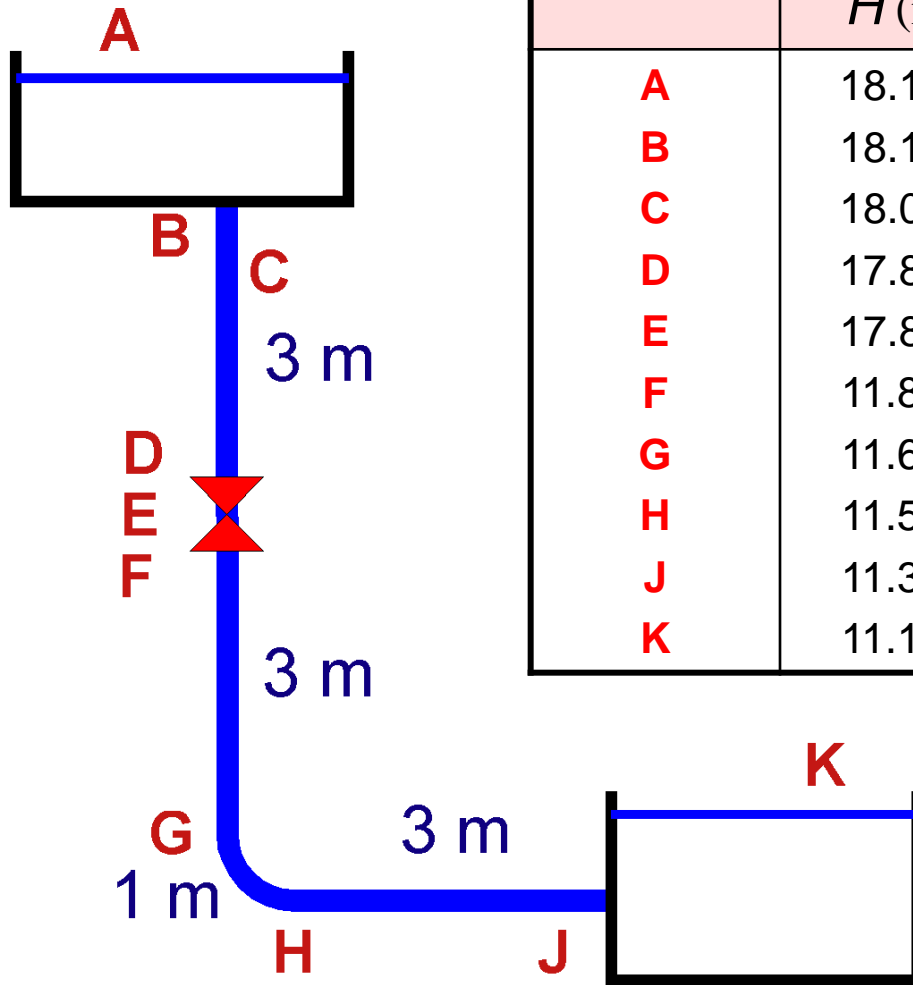
$$D = 100 \text{ mm}$$

$$\varepsilon = 0.25 \text{ mm (fonte neuve)}$$

$$\text{Vanne : } x/D = 0.25 \quad \zeta = 22.68$$



# Conduite simple



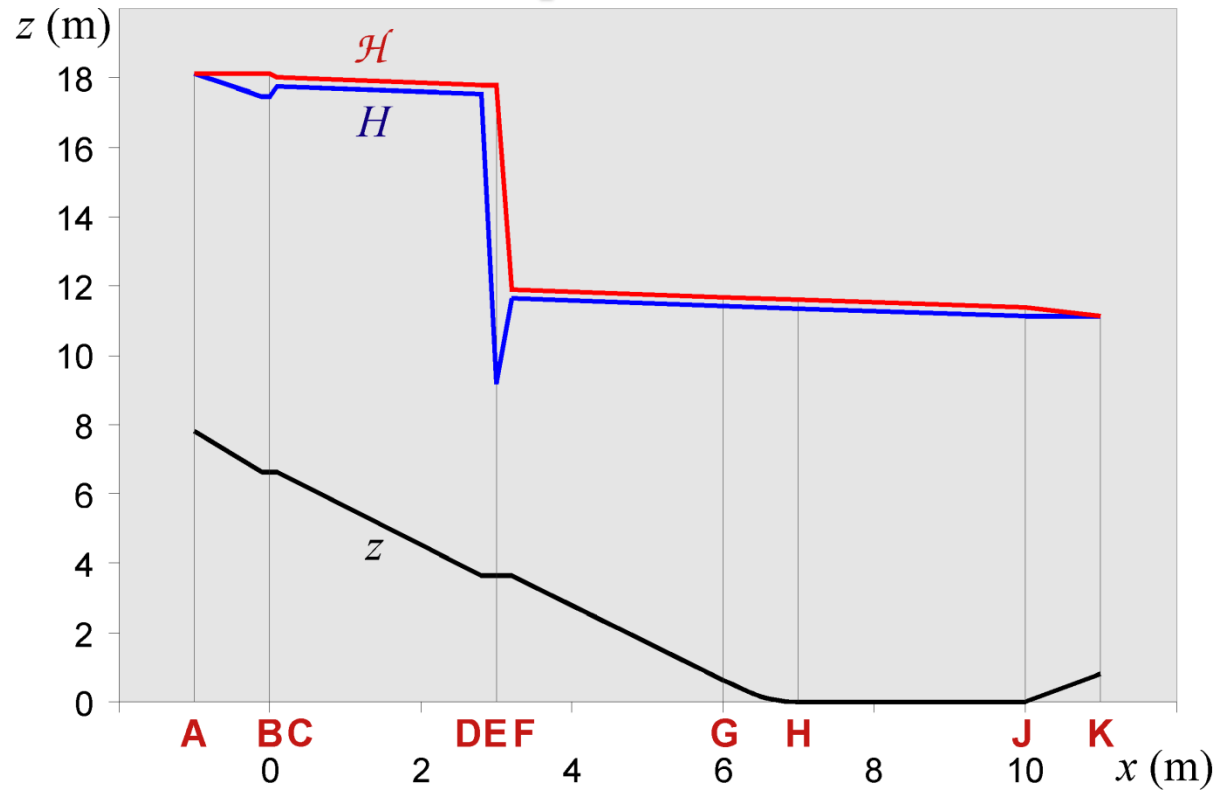
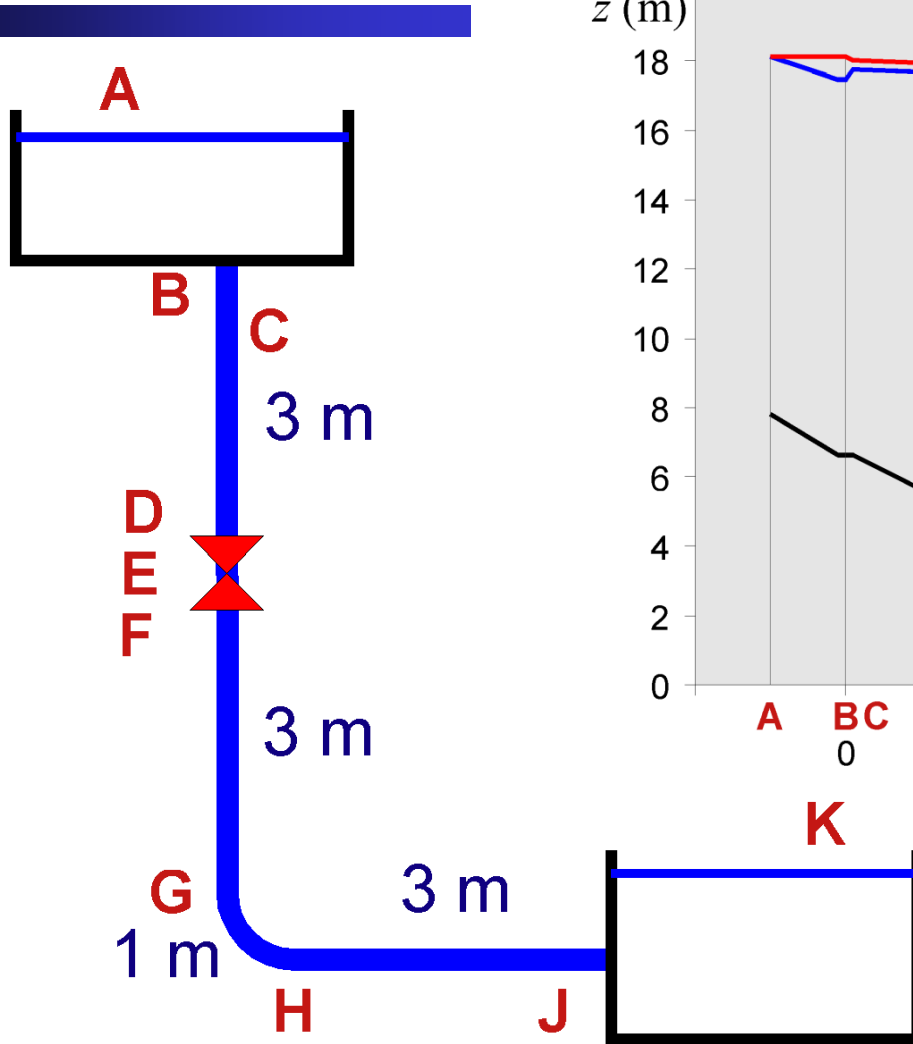
|   | $H \text{ (m)}$ | $z \text{ (m)}$ | $p/\gamma$ | $V^2/2g$ |
|---|-----------------|-----------------|------------|----------|
| A | 18.132          | 7.800           | 10.332     | 0.000    |
| B | 18.132          | 6.637           | 10.817     | 0.678    |
| C | 18.005          | 6.637           | 11.108     | 0.261    |
| D | 17.806          | 3.637           | 13.908     | 0.261    |
| E | 17.806          | 3.637           | 5.548      | 8.621    |
| F | 11.893          | 3.637           | 7.996      | 0.261    |
| G | 11.693          | 0.637           | 10.796     | 0.261    |
| H | 11.593          | 0.000           | 11.332     | 0.261    |
| J | 11.393          | 0.000           | 11.132     | 0.261    |
| K | 11.132          | 0.800           | 10.332     | 0.000    |

$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Conduite simple

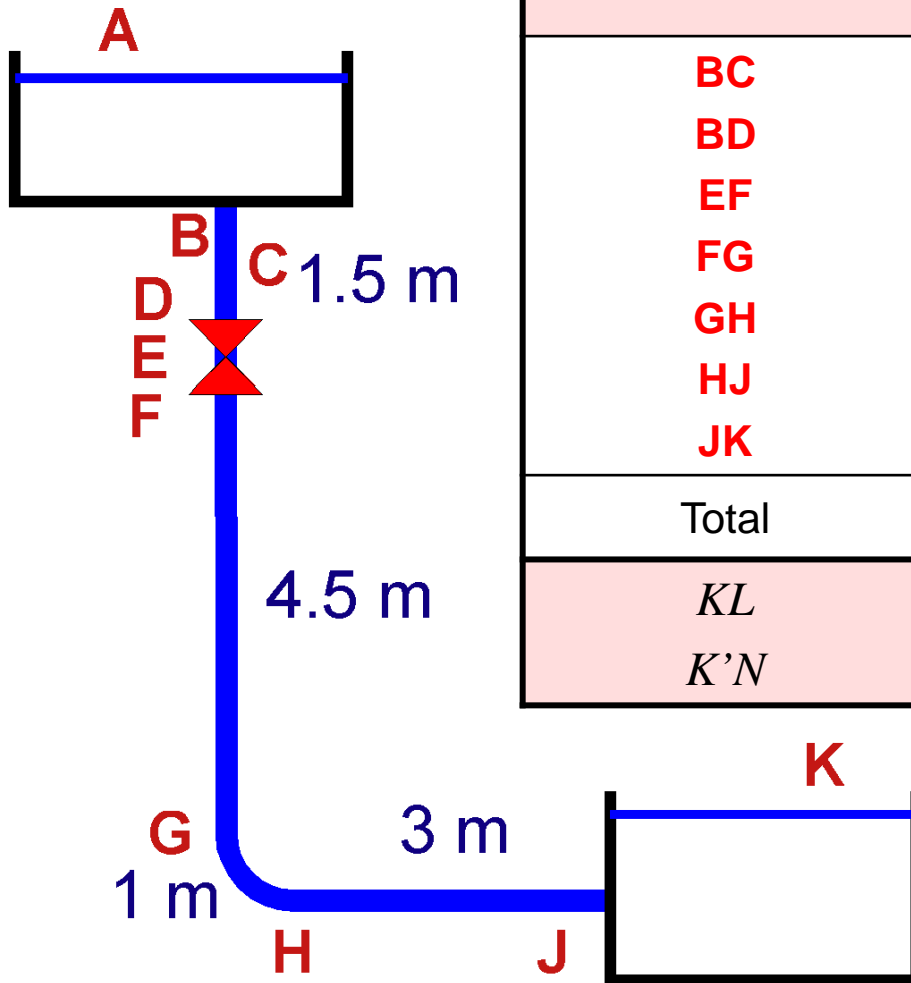


$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Conduite simple



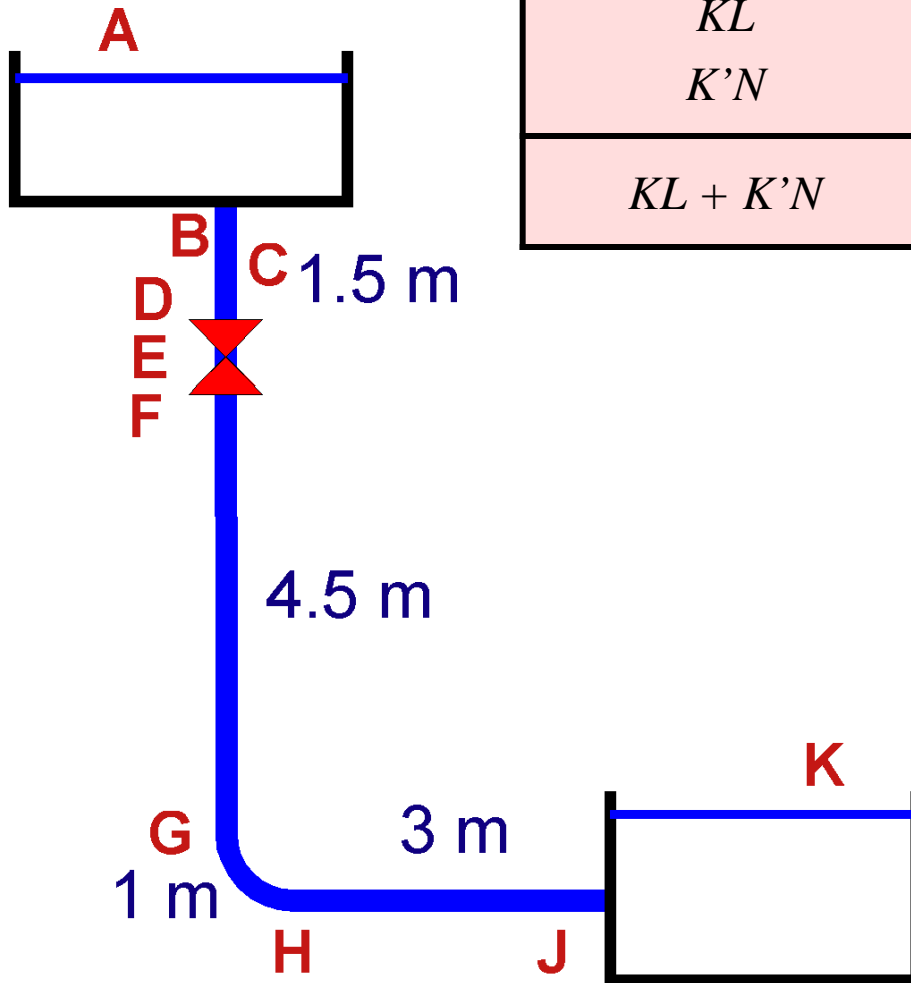
|           | $L$ (m) | $N$    |
|-----------|---------|--------|
| <b>BC</b> |         | 0.49   |
| <b>BD</b> | 1.50    |        |
| <b>EF</b> |         | 22.68  |
| <b>FG</b> | 4.50    |        |
| <b>GH</b> | 1.00    | 0.13   |
| <b>HJ</b> | 3.00    |        |
| <b>JK</b> |         | 1.00   |
| Total     | 10.00   | 24.30  |
| $KL$      | 2 111   |        |
| $K'N$     |         | 20 076 |

$$D = 100 \text{ mm}$$

$\varepsilon = 0.25$  mm (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Conduite simple



|            |        |        |
|------------|--------|--------|
| $KL$       | 2 111  |        |
| $K'N$      |        | 20 076 |
| $KL + K'N$ | 22 187 |        |

$$J = 7.00 \text{ m}$$

$$Q = 0.0178 \text{ m}^3/\text{s}$$

$$V = 2.26 \text{ m/s}$$

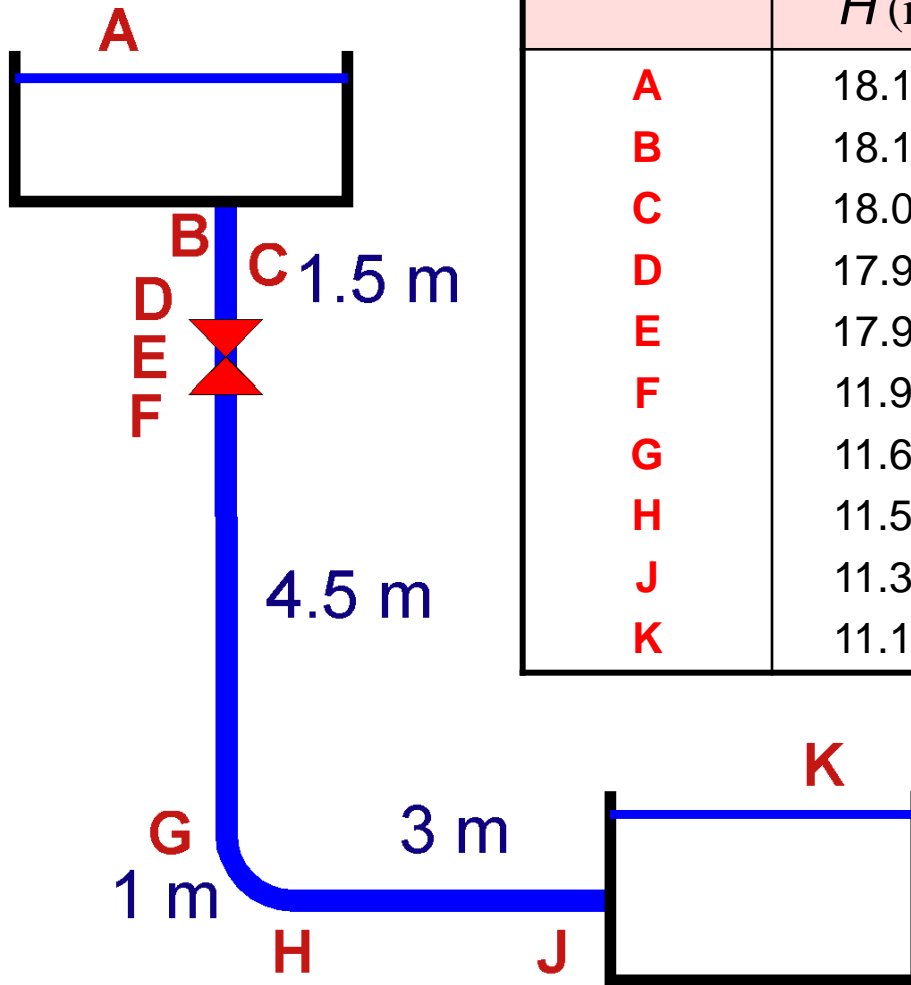
$$\text{Re} = 226\,156$$

$$D = 100 \text{ mm}$$

$$\varepsilon = 0.25 \text{ mm (fonte neuve)}$$

$$\text{Vanne : } x/D = 0.25 \quad \zeta = 22.68$$

# Conduite simple



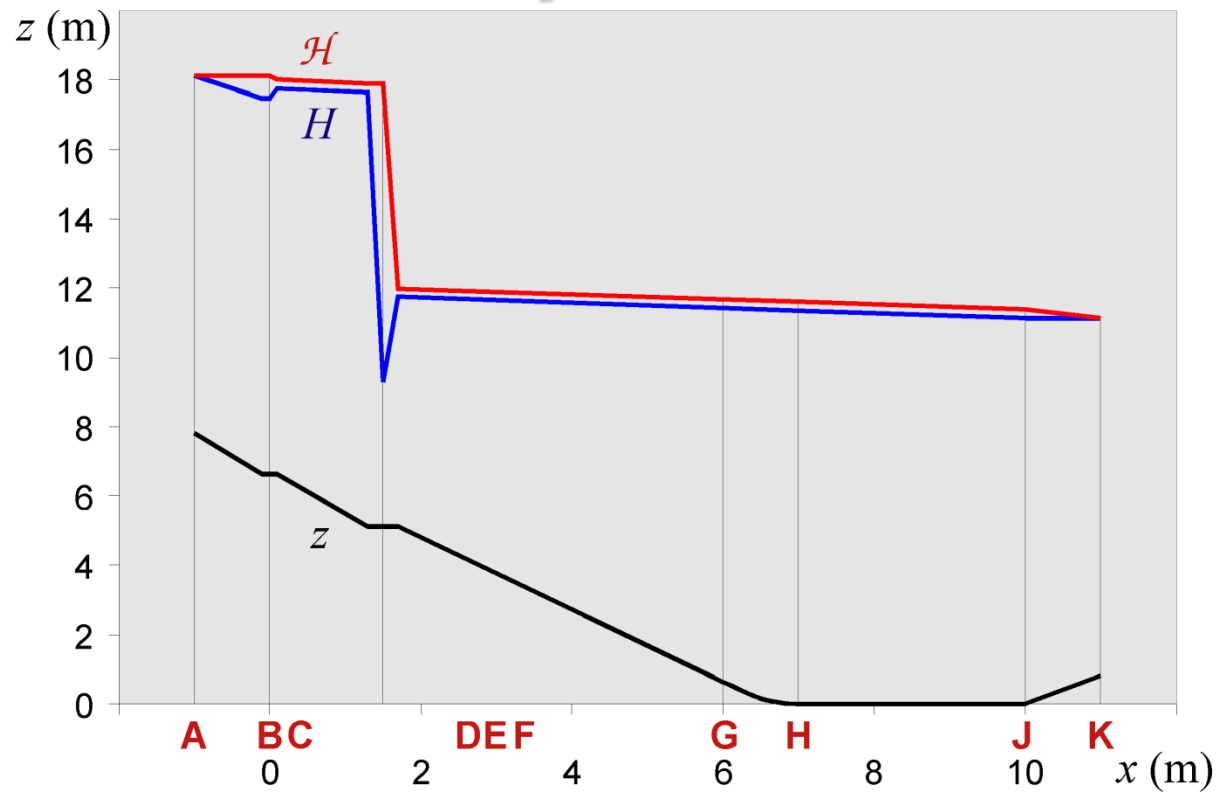
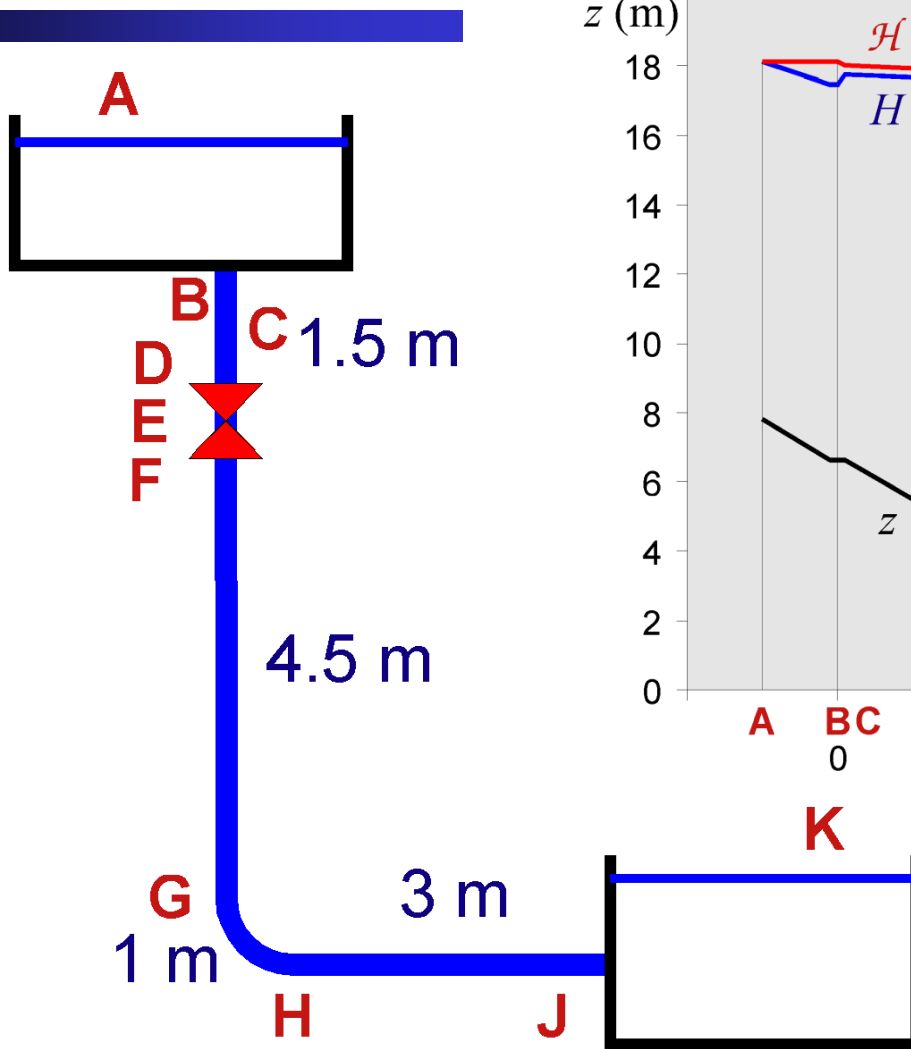
|          | $H$ (m) | $z$ (m) | $p/\gamma$ | $V^2/2g$ |
|----------|---------|---------|------------|----------|
| <b>A</b> | 18.132  | 7.800   | 10.332     | 0.000    |
| <b>B</b> | 18.132  | 6.637   | 10.817     | 0.678    |
| <b>C</b> | 18.005  | 6.637   | 11.108     | 0.261    |
| <b>D</b> | 17.905  | 5.137   | 12.508     | 0.261    |
| <b>E</b> | 17.905  | 5.137   | 4.148      | 8.621    |
| <b>F</b> | 11.993  | 5.137   | 6.596      | 0.261    |
| <b>G</b> | 11.693  | 0.637   | 10.796     | 0.261    |
| <b>H</b> | 11.593  | 0.000   | 11.332     | 0.261    |
| <b>J</b> | 11.393  | 0.000   | 11.132     | 0.261    |
| <b>K</b> | 11.132  | 0.800   | 10.332     | 0.000    |

$D = 100$  mm

$\varepsilon = 0.25$  mm (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Conduite simple



$D = 100 \text{ mm}$

$\varepsilon = 0.25 \text{ mm}$  (fonte neuve)

Vanne :  $x/D = 0.25$   $\zeta = 22.68$

# Consommations (normes françaises)

- Communes rurales (< 2000 habitants)  
125 ... (200) litres / jour / habitant

|                       |                  |                             |
|-----------------------|------------------|-----------------------------|
| Besoins domestiques   |                  | 60 litres/jr/hab.           |
| Elevage               | Cheval ou bovidé | 50 litres/jr                |
|                       | Porc             | 20 litres/jr                |
|                       | Mouton           | 5 litres/jr                 |
| Arrosage des jardins  |                  | 3.6 ... 9 litres/jr         |
| Exploitation agricole | Fromagerie       | 5 litres par litre de lait  |
|                       | Cidrerie         | 4 litres par litre de cidre |
|                       | Vinification     | 2 litres par litre de vin   |
|                       | Brasserie        | 5 litres par litre de bière |
|                       | Sucrierie        | 100 litres par kg de sucre  |



# Consommations (normes françaises)

- Communes urbaines (> 2000 habitants)
  - < 20000 habitants : 125 ... 200 litres / jr / hab.
  - 20000 à 100000 hab. : 200 ... 300 litres / jr / hab.
  - > 100000 hab. : 300 ... 400 litres / jr / hab.

|                       |  |
|-----------------------|--|
| Ecole                 | 100 litres/jr par élève                    |
| Sanatorium            | 250 litres/jr par lit                      |
| Hôpital               | 500 litres/jr par lit                      |
| Colonie de vacances   | 100 litres/jr par personne                 |
| Urinoir               | 20 litres/jr par place                     |
| Lavoir                | 1200 litres/jr par place                   |
| Bain-douche           | 200 litres/jr par poste                    |
| Abattoir              | 500 litres/jr par tête de bétail           |
| Nettoyage des marchés | 5 litres/m <sup>2</sup> par jour de marché |
| Lavage des caniveaux  | 25 litres/m par jour                       |

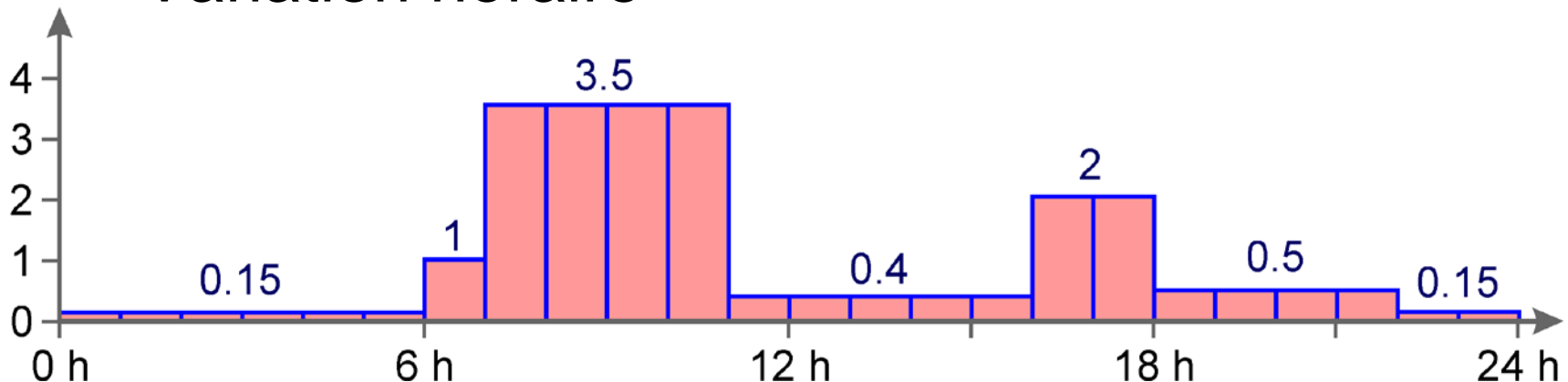
# Consommations (normes françaises)

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- Pertes : 25 ... 35 ... 50 %
- Incendies : 60 m<sup>3</sup>/h pendant 2 heures
- Marge : + 20 ... 30 % sur 25 ans

# Coefficient de pointe

- Estimation moyenne :  $p = 2.$
- Estimation différenciée
  - En tête de réseau :  $p = 2.$
  - Aux points de distribution :  $p = 3.$
- Estimation globale  $p = 1.5 + \frac{2.4}{\sqrt{Q_n}}$   $Q_{\text{moy}}$  en litres/s
- Variation horaire



# Consommations (normes OMS)

- Eau potable :  $\geq 1$  à 2 litres/jour par personne
- Eau pour l'hygiène et la nourriture :  
52 à 54 litres/jour par personne

| Haïti<br>Accès à l'eau<br>et à<br>l'assainissement |          | Population<br>urbaine<br>(46 % de la<br>population) | Population<br>rurale<br>(54 % de la<br>population) | Population<br>totale |
|--|----------|---|--|----------------------|
| Eau  | Accès    | 52 %  | 56 %   | 54 %                 |
|  | Domicile | 24 %  | 3 %  | 14 %                 |
| Assainissement                                     |          | 57 %  | 14 %   | 30 %                 |

*WHO/UNICEF Joint Monitoring Program, 2004*

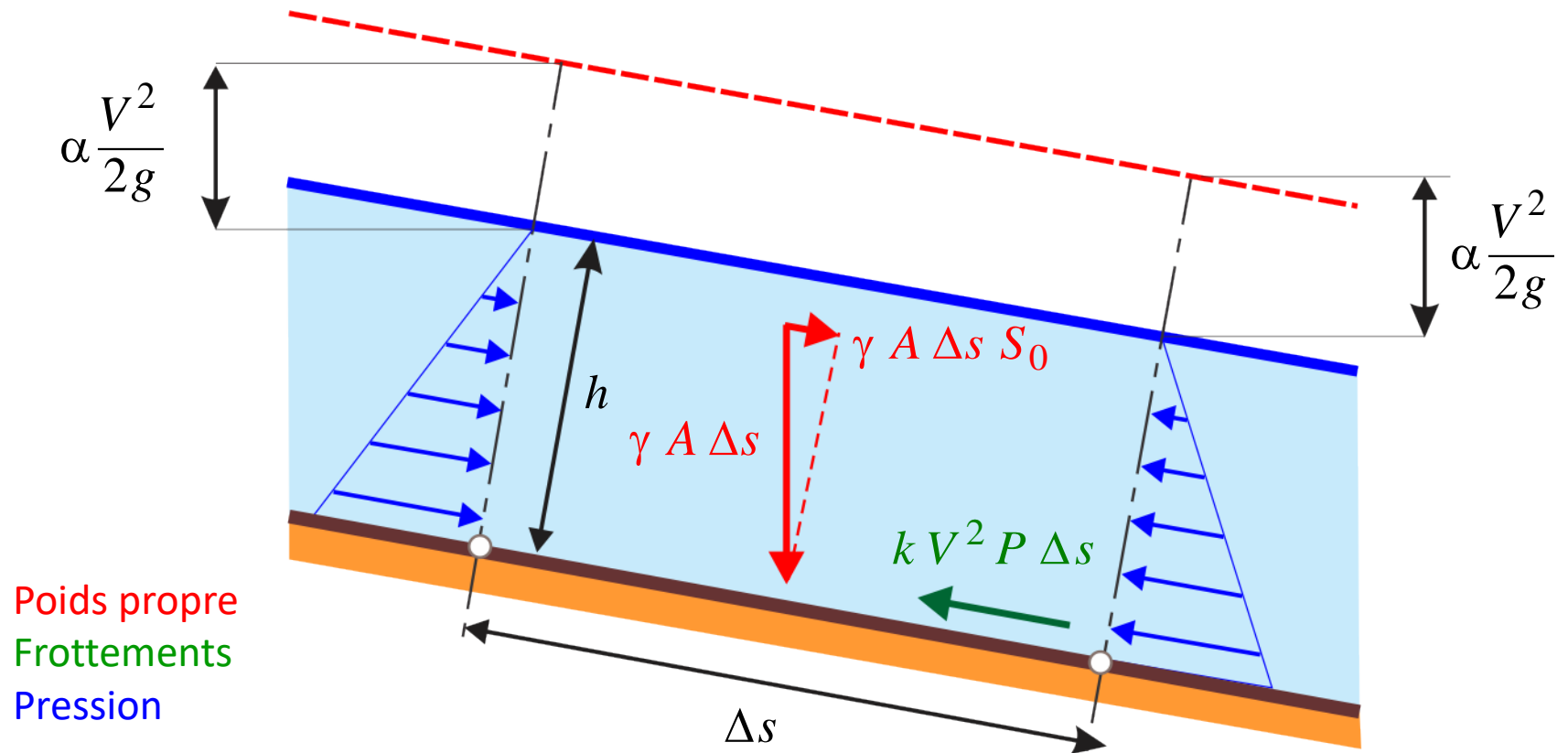
# Open-channel flow

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- Reference flow for
  - Urban drainage
  - Irrigation
- Uniform flow
  - General case
  - Urban sewer

# Uniform flow

- Equilibrium flow



# Uniform flow

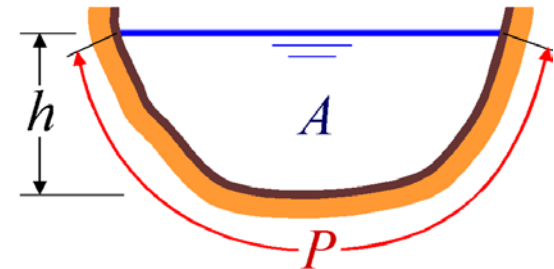
- Chézy

$$V = C \sqrt{R S_0} = C \sqrt{R S_f}$$

- Manning-Strickler

$$C = \frac{1}{n} R^{1/6} = K R^{1/6}$$

$$V = \frac{1}{n} R^{2/3} S_0^{1/2} = K R^{2/3} S_0^{1/2}$$



$A$  aire mouillée

$P$  périmètre mouillé

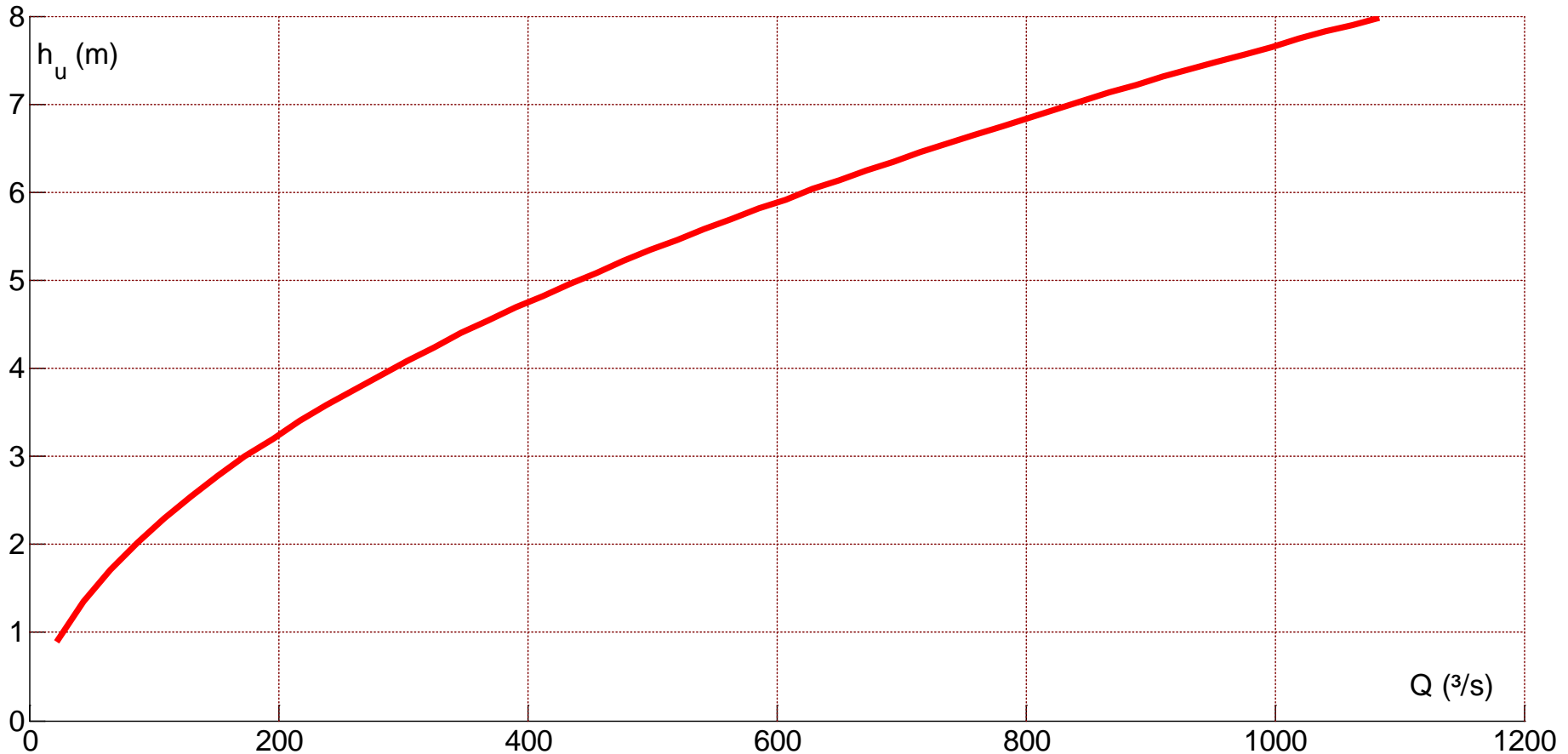
$R = A/P$  rayon hydraulique

$n$  en  $\text{m}^{-1/3} \text{s}$

$K$  en  $\text{m}^{1/3} \text{s}^{-1}$

# Uniform flow

- $h_u = f(Q)$

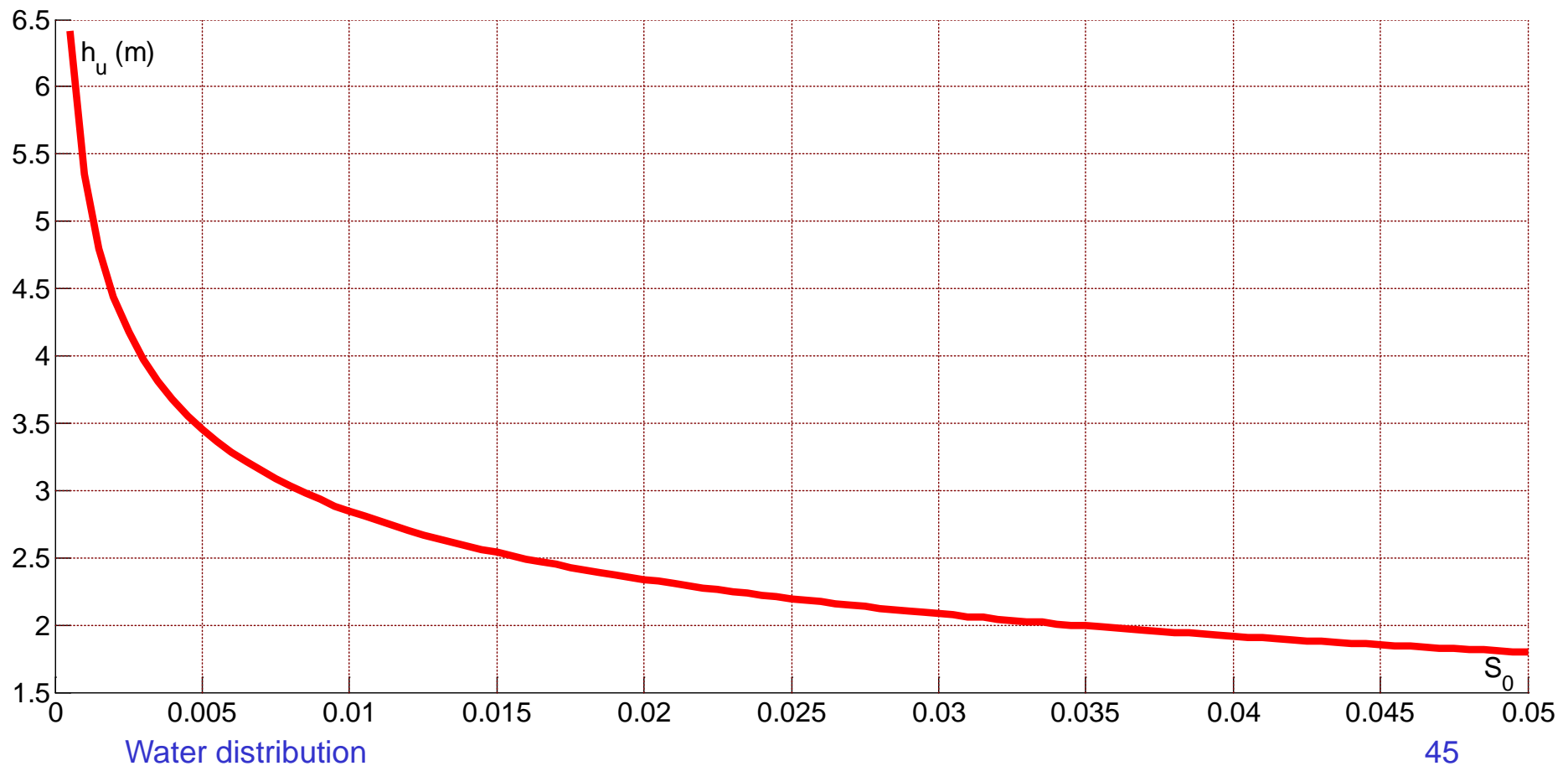


Water distribution



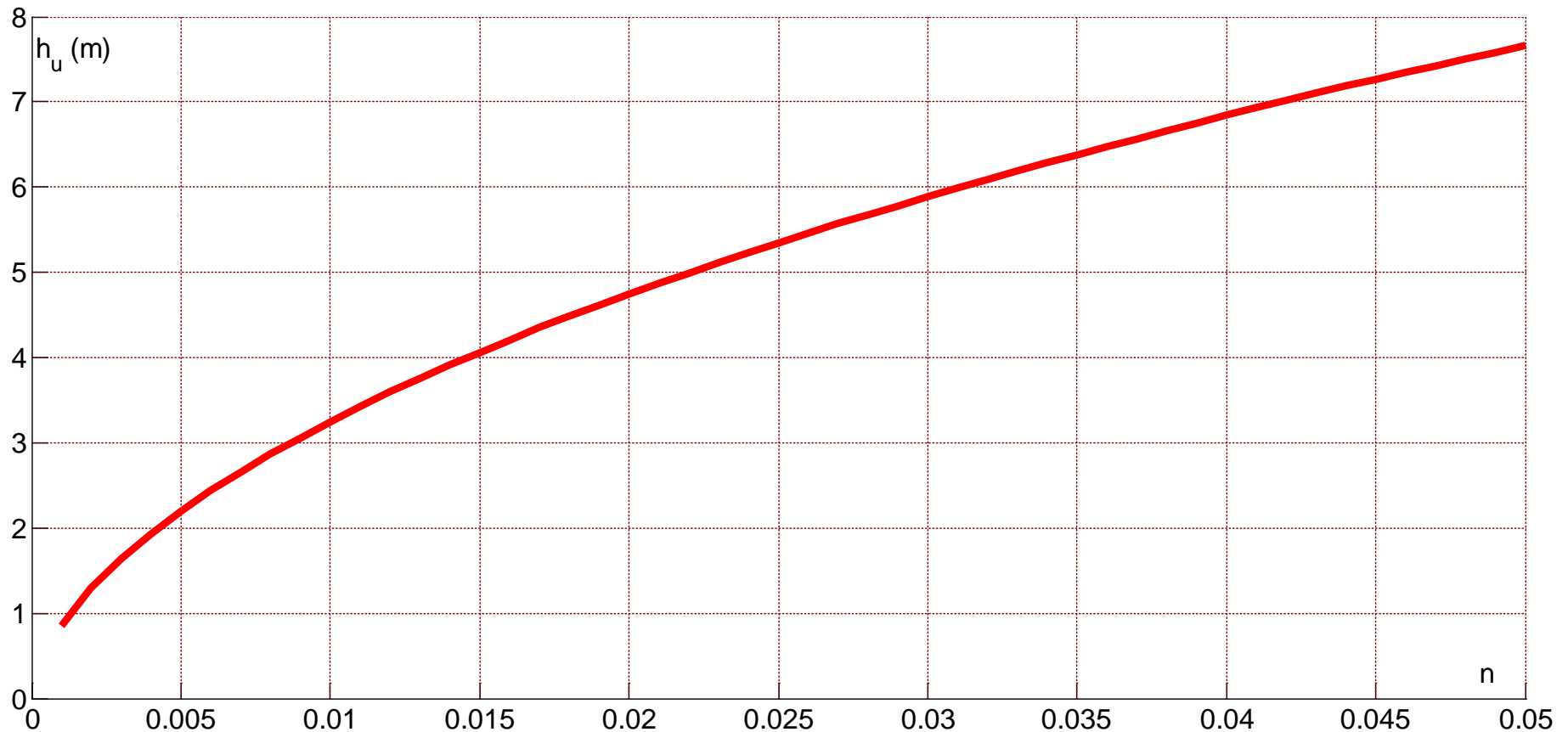
# Uniform flow

- $h_u = f(S_0)$



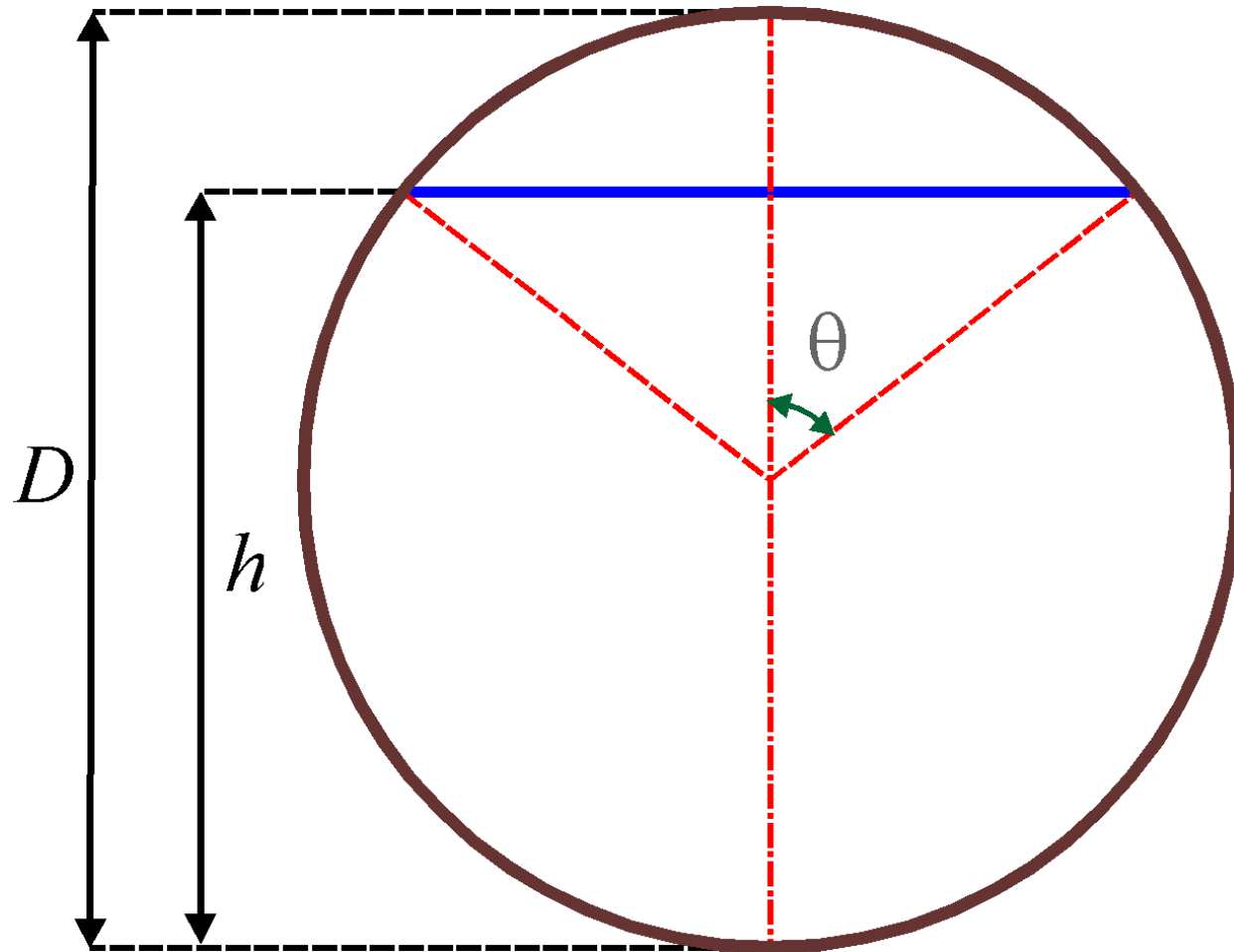
# Uniform flow

- $h_u = f(n)$

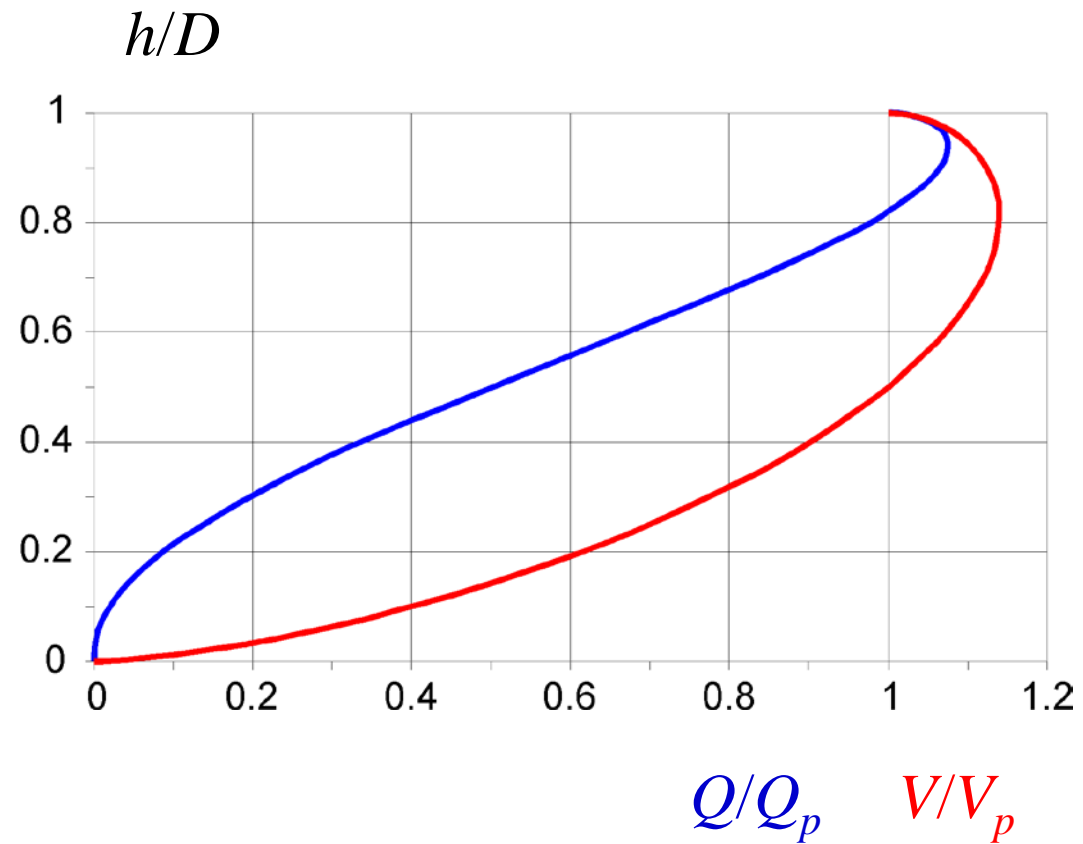
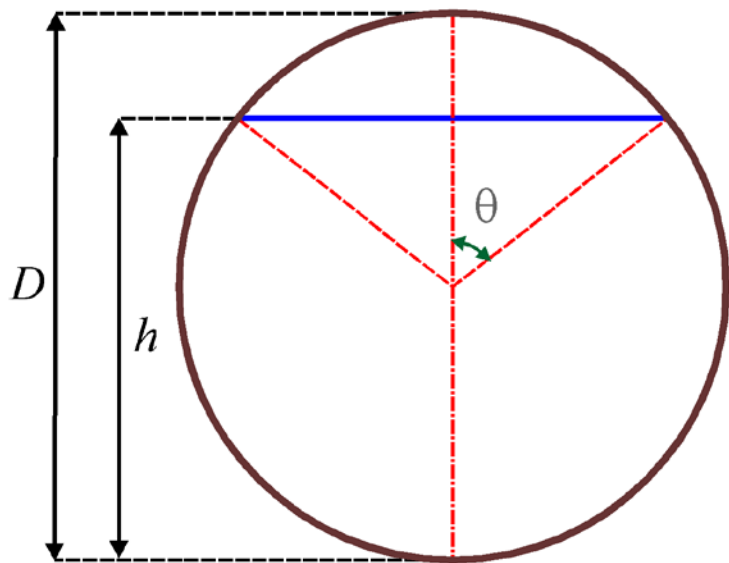


Water distribution

# Urban drainage hydraulics



# Urban drainage hydraulics



# Constraints

- Velocity
  - Self-cleaning:  $V \geq 0.60 \text{ m/s}$  for  $Q = 0.1 Q_{\max}$   
 $V \geq 0.30 \text{ m/s}$  for  $Q = 0.01 Q_{\max}$
  - Attrition:  $V \leq 2 \text{ m/s}$
- Slope
  - Installation accuracy :  $S_0 \geq 0.005$
  - Earthwork volume limitation:  $S_0 \leq 0.04 \dots 0.05$
- Diameter
  - Non obstruction :  $D \geq 0.20 \text{ m}$  at the head of the network  
 $D \geq 0.30 \text{ m}$  inside the network
- Inspection manholes: inter-distance 10 ... 35 m

# Avoid pressurized flow

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- <https://www.youtube.com/watch?v=10dSbmtq1cU>