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# Task 3

Airframe model

Autopilot -AER 408  
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## Team 4

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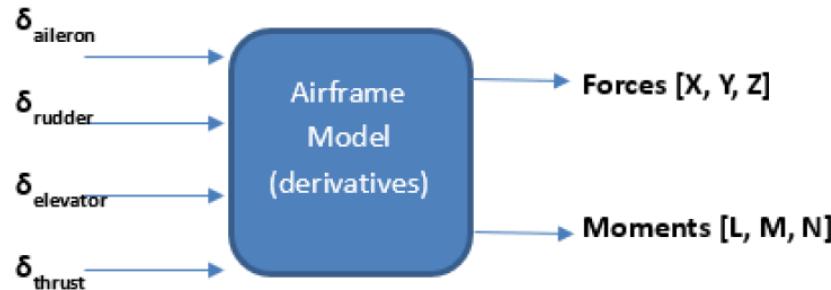
## Task #3

### Introduction

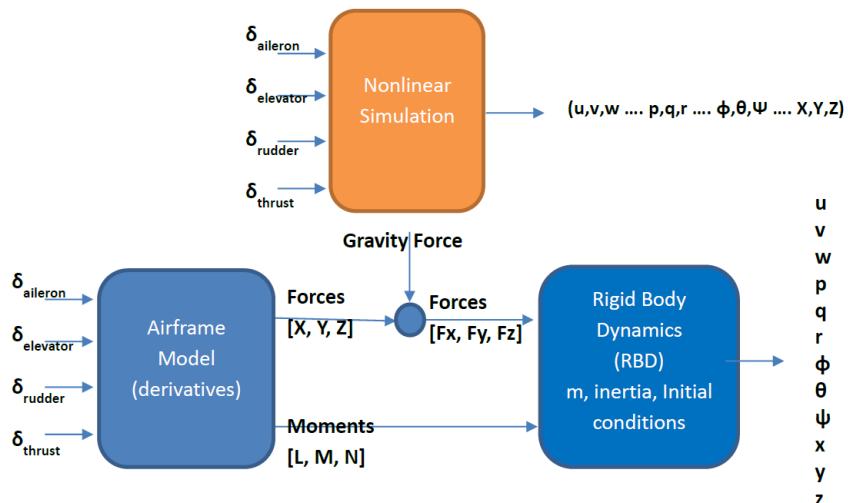
In this task we are concerned about calculating the change in states due to change in control surfaces at certain aircraft data.

We will build an airframe model code that takes the control surfaces deflection values

$$\delta_{\text{aileron}}, \delta_{\text{thrust}}, \delta_{\text{rudder}}, \delta_{\text{elevator}}$$



We will combine the airframe model code with the RBD solver code that we made to make a nonlinear simulator



Equations representing the change in the Aerodynamic & thrust forces & moments:

$$\Delta X = \frac{\partial X}{\partial u} \Delta u + \frac{\partial X}{\partial w} \Delta w + \frac{\partial X}{\partial \delta_e} \Delta \delta_e + \frac{\partial X}{\partial \delta_T} \Delta \delta_T$$

$$\Delta Y = \frac{\partial Y}{\partial v} \Delta v + \frac{\partial Y}{\partial p} \Delta p + \frac{\partial Y}{\partial r} \Delta r + \frac{\partial Y}{\partial \delta_r} \Delta \delta_r,$$

$$\Delta Z = \frac{\partial Z}{\partial u} \Delta u + \frac{\partial Z}{\partial w} \Delta w + \frac{\partial Z}{\partial \dot{w}} \Delta \dot{w} + \frac{\partial Z}{\partial q} \Delta q + \frac{\partial Z}{\partial \delta_e} \Delta \delta_e + \frac{\partial Z}{\partial \delta_T} \Delta \delta_T$$

$$\Delta L = \frac{\partial L}{\partial v} \Delta v + \frac{\partial L}{\partial p} \Delta p + \frac{\partial L}{\partial r} \Delta r + \frac{\partial L}{\partial \delta_r} \Delta \delta_r + \frac{\partial L}{\partial \delta_a} \Delta \delta_a$$

$$\Delta M = \frac{\partial M}{\partial u} \Delta u + \frac{\partial M}{\partial w} \Delta w + \frac{\partial M}{\partial \dot{w}} \Delta \dot{w} + \frac{\partial M}{\partial q} \Delta q + \frac{\partial M}{\partial \delta_e} \Delta \delta_e + \frac{\partial M}{\partial \delta_T} \Delta \delta_T$$

$$\Delta N = \frac{\partial N}{\partial v} \Delta v + \frac{\partial N}{\partial p} \Delta p + \frac{\partial N}{\partial r} \Delta r + \frac{\partial N}{\partial \delta_r} \Delta \delta_r + \frac{\partial N}{\partial \delta_a} \Delta \delta_a$$

## Axes systems

There are three types of body axes

- Principle axes ( $I_{xy} = 0$ )
- Stability Axes ( $w_0 = 0$ ),  $X_b$  axis concides with  $V_T$
- Body axes (fuselage reference axis)

we will transform from stability axes derivatives to body axes

$$\begin{aligned}
 L_B' &= (L_B + I_{xz}N_B/I_X)G & 1/\text{sec}^2 \\
 L_p' &= (L_p + I_{xz}N_p/I_X)G & 1/\text{sec} \\
 L_r' &= (L_r + I_{xz}N_r/I_X)G & 1/\text{sec} \\
 L_{\delta_r}' &= (L_{\delta_r} + I_{xz}N_{\delta_r}/I_X)G & 1/\text{sec}^2 \\
 L_{\delta_a}' &= (L_{\delta_a} + I_{xz}N_{\delta_a}/I_X)G & 1/\text{sec}^2 \\
 N_B' &= (N_B + I_{xz}L_B/I_z)G & 1/\text{sec}^2 \\
 N_p' &= (N_p + I_{xz}L_p/I_z)G & 1/\text{sec} \\
 N_r' &= (N_r + I_{xz}L_r/I_z)G & 1/\text{sec} \\
 N_{\delta_r}' &= (N_{\delta_r} + I_{xz}L_{\delta_r}/I_z)G & 1/\text{sec}^2 \\
 N_{\delta_a}' &= (N_{\delta_a} + I_{xz}L_{\delta_a}/I_z)G & 1/\text{sec}^2 \\
 G &= \frac{1}{1 - \frac{I_{xz}^2}{I_x I_z}}
 \end{aligned}$$

## Codes

```
clc; clear; close all;
```

### Inputs

Forces, Moments and Inertia

```
[Mass, g, I, invI, timeSpan, dt, ICs, ICs_dot0, vt0, ...
dControl, SD_Long, SD_Lat, initialGravity] = Input("NT-33A_4.xlsx");
```

### Solving

```

steps = (timeSpan(2) - timeSpan(1))/dt;

Result = NaN(12, steps);

Result(:,1) = ICs;

time_V = linspace(0, timeSpan(2), steps+1);

```

```

dForces = [0 ; 0; 0];

dMoments = [0 ; 0; 0];

for i =1:steps
    tic
    Result(:, i+1) = RBDSolver(Result(:, i), dt, (initialGravity + dForces),
dMoments, Mass, I, invI, g);

    [dF, dM] = airFrame(SD_Long, SD_Lat, dControl, ICs, ICs_dot0, Result(:, i+1)
, Vt0, ...
        (initialGravity + dForces), dMoments, Mass, I, invI, g);

    toc
    dForces = vpa(dF');
    dMoments = vpa(dM');

end

```

## Plotting

---

### Rearranging Results

```

u = Result(1,:);

v = Result(2,:);

w = Result(3,:);

p = Result(4,:);

q = Result(5,:);

r = Result(6,:);

phi = Result(7,:);

theta = Result(8,:);

psi = Result(9,:);

x = Result(10,:);

y = Result(11,:);

z = Result(12,:);

beta_deg=asin(v/Vt0)*180/pi;

alpha_deg=atan(w./u)*180/pi;

```

```

p_deg=p*180/pi;

q_deg=q*180/pi;

r_deg=r*180/pi;

phi_deg=phi*180/pi;

theta_deg=theta*180/pi;

psi_deg=psi*180/pi;

figure

plot3(x,y,z);

title('Trajectory')
figure
subplot(4,3,1)
plot(time_V,u)
title('u (ft/sec)')
xlabel('time (sec)')
subplot(4,3,2)
plot(time_V,beta_deg)
title('\beta (deg)')
xlabel('time (sec)')
subplot(4,3,3)
plot(time_V,alpha_deg)
title('\alpha (deg)')
xlabel('time (sec)')
subplot(4,3,4)
plot(time_V,p_deg)
title('p (deg/sec)')
xlabel('time (sec)')
subplot(4,3,5)
plot(time_V,q_deg)
title('q (deg/sec)')
xlabel('time (sec)')
subplot(4,3,6)
plot(time_V,r_deg)
title('r (deg/sec)')
xlabel('time (sec)')
subplot(4,3,7)
plot(time_V,phi_deg)
title('\phi (deg)')
xlabel('time (sec)')
subplot(4,3,8)
plot(time_V,theta_deg)
title('\theta (deg)')
xlabel('time (sec)')
subplot(4,3,9)
plot(time_V,psi_deg)
title('\psi (deg)')
xlabel('time (sec)')
subplot(4,3,10)
plot(time_V,x)
title('x (ft)')
xlabel('time (sec)')
subplot(4,3,11)
plot(time_V,y)
title('y (ft)')
xlabel('time (sec)')

```

```

    subplot(4,3,12)
    plot(time_V,z)
    title('z (ft)')
    xlabel('time (sec)')

```

```

function [Mass, g, I, invI, timeSpan, dt, ICs, ICs_dot0, Vt0, ...
dc, SD_Long, SD_Lat, initialGravity] = Input(inputs_filename)
% Inputs
% here B2:B61 means read the excel sheet from cell B2 to cell B61
aircraft_data=xlsread(inputs_filename,'B2:B61');

% Integration time span & Step
dt = aircraft_data(1);
tfinal = aircraft_data(2);
timeSpan = [0 tfinal];

% Initial Conditions
% [u; v; w; p; q; r; phi; theta; epsi; xe0; ye0; ze0]
% ICs = [10; 2; 0; 2*pi/180; pi/180; 0; 20*pi/180; 15*pi/180; 30*pi/180; 2; 4;
7];
ICs = aircraft_data(4:15);
ICs_dot0 = zeros(12,1);
Vt0 = sqrt(ICs(1)^2 + ICs(2)^2 + ICs(3)^2);      % Vto

% control actions values
% D_a, D_r, D_e, D_th
dc = [ aircraft_data(57:59) * pi/180 ; aircraft_data(60) ];

% gravity, mass % inertia
Mass = aircraft_data(51);
g = aircraft_data(52);
Ix = aircraft_data(53);
Iy = aircraft_data(54);
Iz = aircraft_data(55);
Ixz = aircraft_data(56);
Ix=0; Iyz=0;
I = [Ix , -Ix , -Ixz ;...
       -Ix , Iy , -Iyz ;...
       -Ixz , -Iyz , Iz];
invI = inv(I);

% Stability Derivatives Longitudinal motion
SD_Long = aircraft_data(21:36);

% Stability Derivatives Lateral motion
SD_Lat_dash = aircraft_data(37:50);
SD_Lat_dash(9) = SD_Lat_dash(9)*Vt0;      % From dimension-less to dimensional
SD_Lat_dash(10) = SD_Lat_dash(10)*Vt0;    % Form dimension-less to dimensional

SD_Lat = LateralSD2BodyAxes(SD_Lat_dash, I);

% initial gravity force
[S, C, ~] = SCT(ICs(7:9));
initialGravity = Mass*g*[%
    S.theta;
    -S.phi*C.theta;
    -C.phi*C.theta;
];

end
function [dForce, dMoment] = airFrame(SD_Long, SD_Lat, dControl, state0,
state0_dot, state, Vt0 ,forces, moments, Mass, I, invI, g)

```

```

[YV, YB, LB, NB, LP, NP, LR, NR, YDA, YDR, LDA, NDA, LDR, NDR] = feval(@(x)
x{:}), num2cell(SD_Lat));
[XU, ZU, MU, XW, ZW, MW, ZWD, ZQ, MWD, MQ, XDE, ZDE, MDE, XD_TH, ZD_TH, MD_TH]
= feval(@(x) x{:}), num2cell(SD_Long));
[Da, Dr, De, Dth] = feval(@(x) x{:}), num2cell(dControl));

Ixx = I(1,1);
Iyy = I(2,2);
Izz = I(3,3);

state_dot = DOF6(state, forces, moments, Mass, I, invI, g);

ds = state - state0;
ds_dot = state_dot - state0_dot;

beta0 = asin(state0(2)/Vt0);
beta = asin(state(2)/Vt0);
dbeta = beta-beta0;

dX = Mass*(XU*ds(1)+XW*ds(3)+XDE*De+XD_TH*Dth);
dY = Mass*(YV*ds(2)+YB*dbeta+YDA*ds(1)+YDR*Dr);
dZ = Mass*(ZU*ds(1)+ZW*ds(3)+ZWD*ds_dot(3)+ZQ*ds(5)+ZDE*De+ZD_TH*Dth);

dL = Ixx*(LB*dbeta+LP*ds(4)+LR*ds(6)+LDR*Dr+LDA*Da);
dM = Iyy*(MU*ds(1)+MW*ds(3)+MWD*ds_dot(3)+MQ*ds(5)+MDE*De+MD_TH*Dth);
dN = Izz*(NB*dbeta+NP*ds(4)+NR*ds(6)+NDR*Dr+NDA*Da);

dForce = [dX dY dZ];
dMoment = [dL dM dN];

end

```

Function return the set of 12 state of the six degree of freedom system after sub., with given ICs

```

function F = DOF6(ICs, forces, Moments, Mass, Inertia, invI, g)

% (Sin, Cos, Tan) of (phi, theta, epsi)
[S, C, T] = SCT(ICs(7:9));

Forces = forces + Mass*g*[  

    -S.theta;  

    S.phi*C.theta;  

    C.phi*C.theta;  

];

% (u, v, w) dot
F(1:3, 1) = Forces/Mass - cross(...  

    ICs(4:6, 1), ICs(1:3, 1)...  

);

% (p, q, r) dot
F(4:6, 1) = invI*(Moments - cross(...  

    ICs(4:6, 1), Inertia * ICs(4:6, 1)...  

));

% (phi, theta, epsi) dot
F(7:9, 1) = [  

    1, S.phi*T.theta, C.phi*T.theta;  

    0, C.phi, -S.phi;  

    0, S.phi/C.theta, C.phi/C.theta;  

] * ICs(4:6, 1);

% (x, y, z) dot
F(10:12, 1) = [  

    C.theta*C.epsi, (S.phi*S.theta*C.epsi - C.phi*S.epsi),  

    (C.phi*S.theta*C.epsi + S.phi*S.epsi);

```

```

        C.theta*S.epsi, (S.phi*S.theta*S.epsi + C.phi*C.epsi),
(C.phi*S.theta*S.epsi - S.phi*C.epsi);
-S.theta, S.phi*C.theta, C.phi*C.theta
] * ICs(1:3, 1);

end
function SD_Lat = LateralSD2BodyAxes(SD_Lat_dash, I)

[YV, YB, LBd, NBd, LPd, NPd, LRd, NRd, YDA, YDR, LDAd, NDAd, LDRd, NDRd] = feval(@(x) x{:}, ...
num2cell(SD_Lat_dash));

Ixx = I(1);
Izz = I(9);
Ixz = -I(3);

G = 1/(1 - Ixz^2 / Ixx / Izz);

syms LB LP LR LDR LDA NB NP NR NDR NDA
eq1 = (LB+Ixz*NB/Ixx)*G == LBd;
eq2 = (NB+Ixz*LB/Izz)*G == NBD;
eq3 = (LP+Ixz*NP/Ixx)*G == LPd;
eq4 = (NP+Ixz*LP/Izz)*G == NPD;
eq5 = (LR+Ixz*NR/Ixx)*G == LRD;
eq6 = (NR+Ixz*LR/Izz)*G == NRD;
eq7 = (LDR+Ixz*NDR/Ixx)*G == LDRd;
eq8 = (NDR+Ixz*LDR/Izz)*G == NDRd;
eq9 = (LDA+Ixz*NDA/Ixx)*G == LDAd;
eq10 = (NDA+Ixz*LDA/Izz)*G == NDAd;

[A,B] = equationsToMatrix(... ...
[eq1, eq2, eq3, eq4, eq5, eq6, eq7, eq8, eq9, eq10], ...
[LB LP LR LDR LDA NB NP NR NDR NDA]);

X = A\B;

SD_Lat = [
YV YB ...
X(1) X(6) X(2) X(7) ...
X(3) X(8) ...
YDA YDR ...
X(5) X(10) X(4) X(9) ...
];
SD_Lat = vpa(SD_Lat);

end

```

RBD Solver is function that implements Runge-Kutta-4 Algorithm in order to integrate 6 DOF set of equations with a give Initial Conditions ICs, for single dt time step.

```

function state = RBDSolver(ICs, dt, Force, Moments, Mass, I, invI, g)

K = zeros(12, 4);

K(:, 1) = dt*DOF6(ICs, Force, Moments, Mass, I, invI, g);
K(:, 2) = dt*DOF6(ICs+0.5*K(:, 1), Force, Moments, Mass, I, invI, g);
K(:, 3) = dt*DOF6(ICs+0.5*K(:, 2), Force, Moments, Mass, I, invI, g);
K(:, 4) = dt*DOF6(ICs+K(:, 3), Force, Moments, Mass, I, invI, g);

state = ICs + (...
K(:, 1)+...
2*K(:, 2)+...
2*K(:, 3)+...
K(:, 4))/6;

end

```

Calculate Sin, Cos ,Tan for any set of three angles and return results in struct form for easy access in code.

```
function [S, C, T] = SCT(ICs)
    S = struct(...  

        'phi', sin(ICs(1)), ...  

        'theta', sin(ICs(2)), ...  

        'epsi', sin(ICs(3)) ...  

    );  

    C = struct(...  

        'phi', cos(ICs(1)), ...  

        'theta', cos(ICs(2)), ...  

        'epsi', cos(ICs(3)) ...  

    );  

    T = struct(...  

        'phi', tan(ICs(1)), ...  

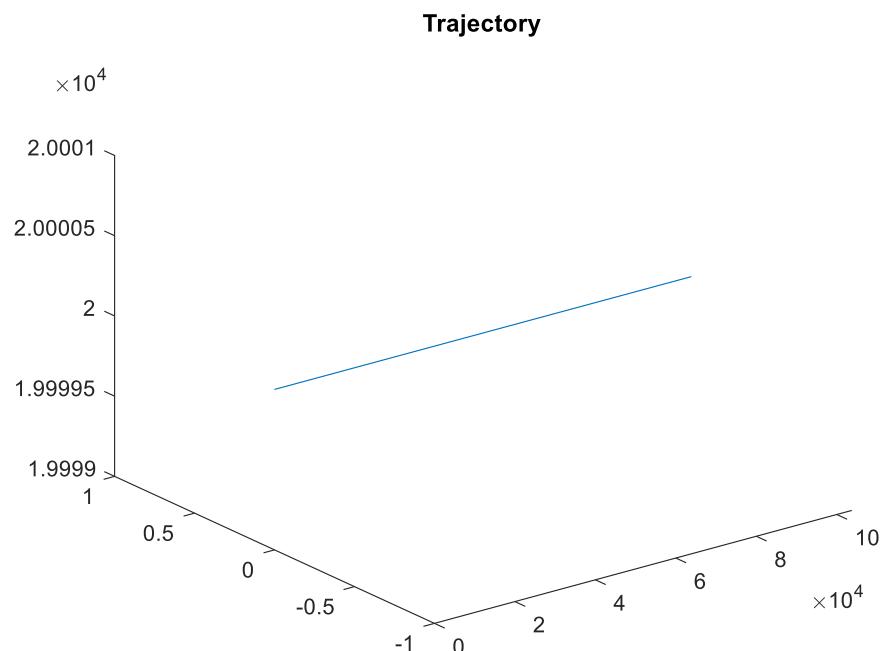
        'theta', tan(ICs(2)), ...  

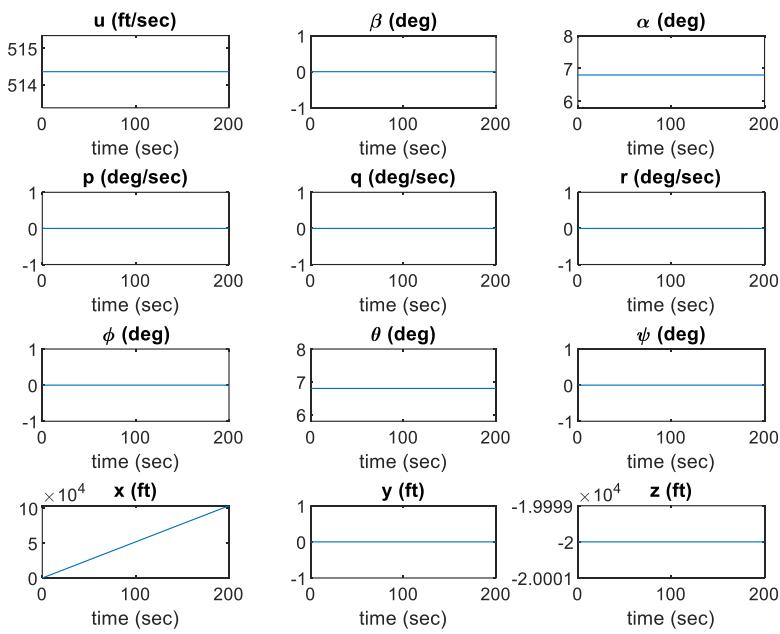
        'epsi', tan(ICs(3)) ...  

    );
end
```

## Benchmark test plots B-747 airplane

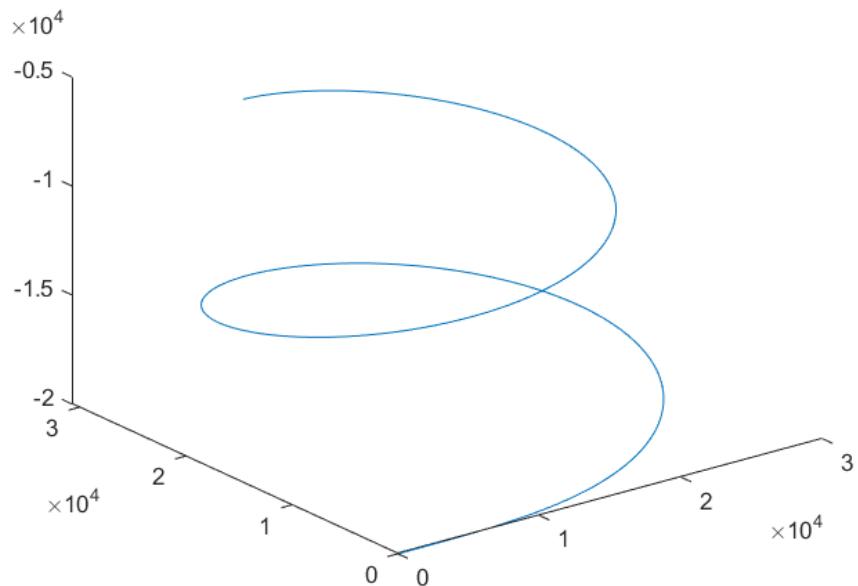
For No input

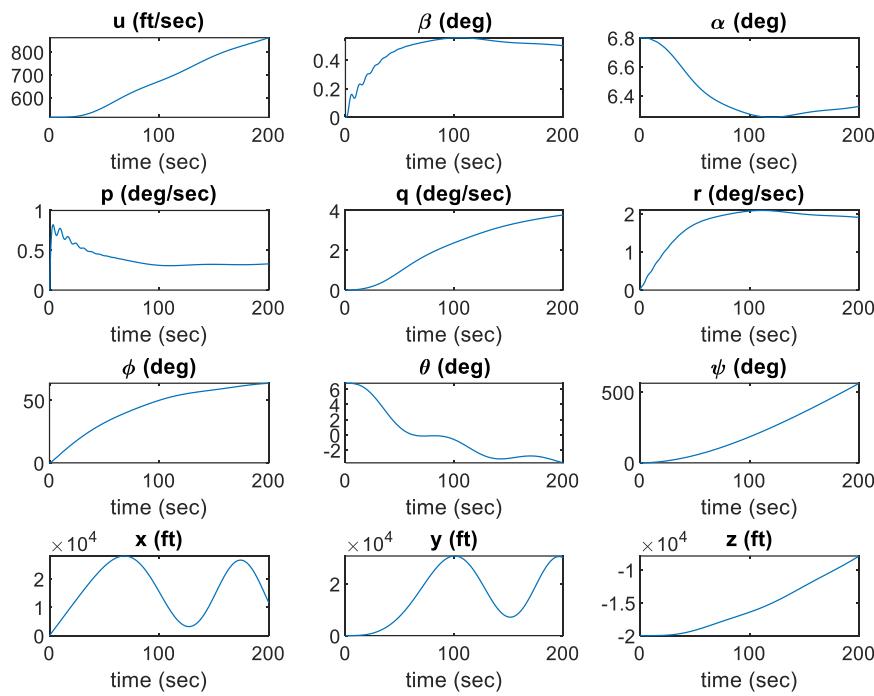




For +ve 5 degree aileron

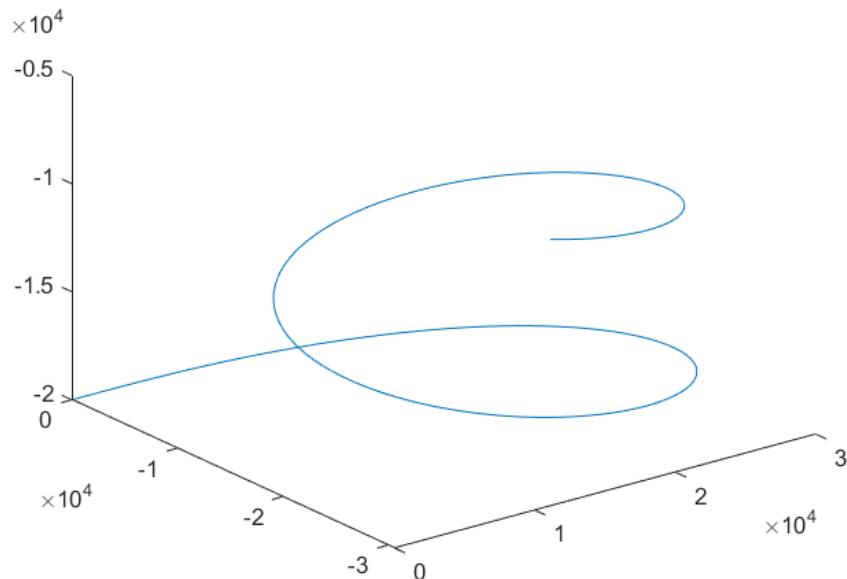
**Trajectory**

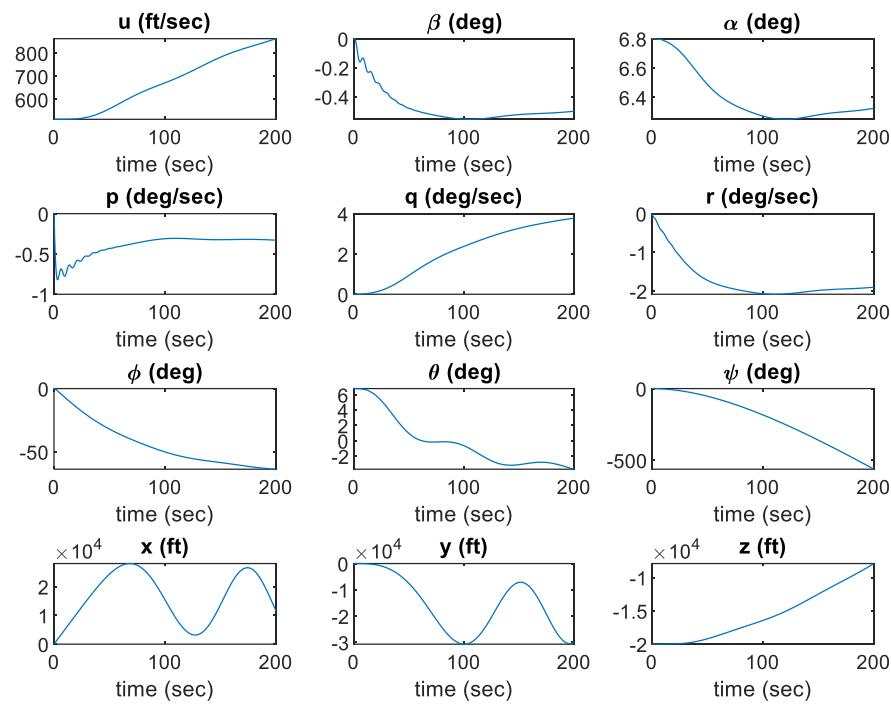




For -ve 5-degree aileron

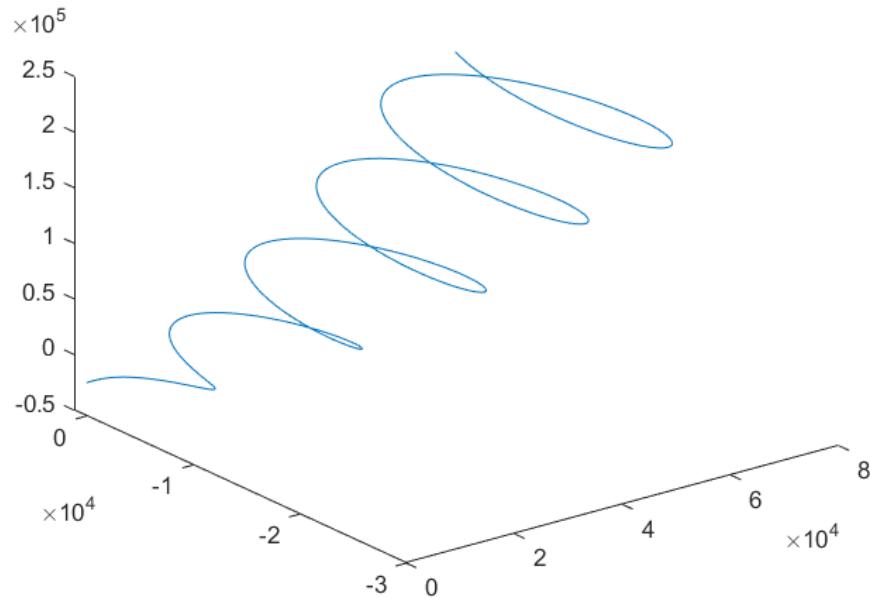
### Trajectory

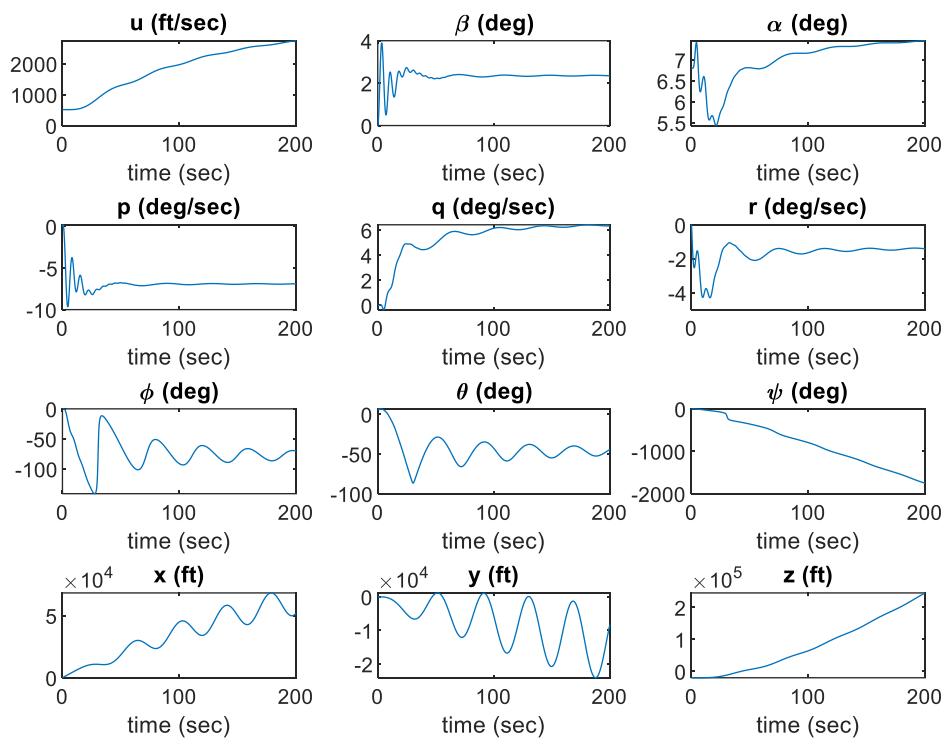




For +ve 5-degree rudder

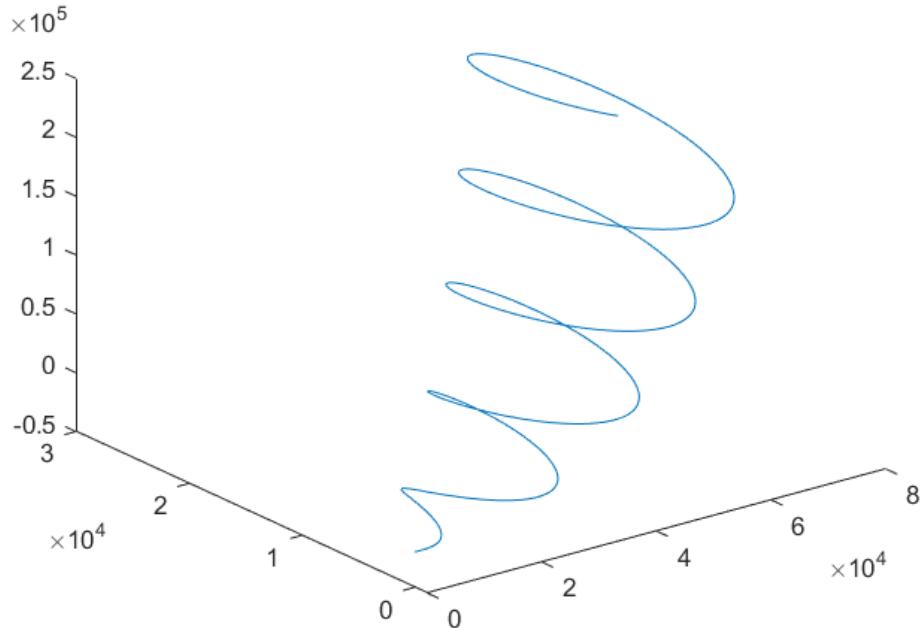
### Trajectory

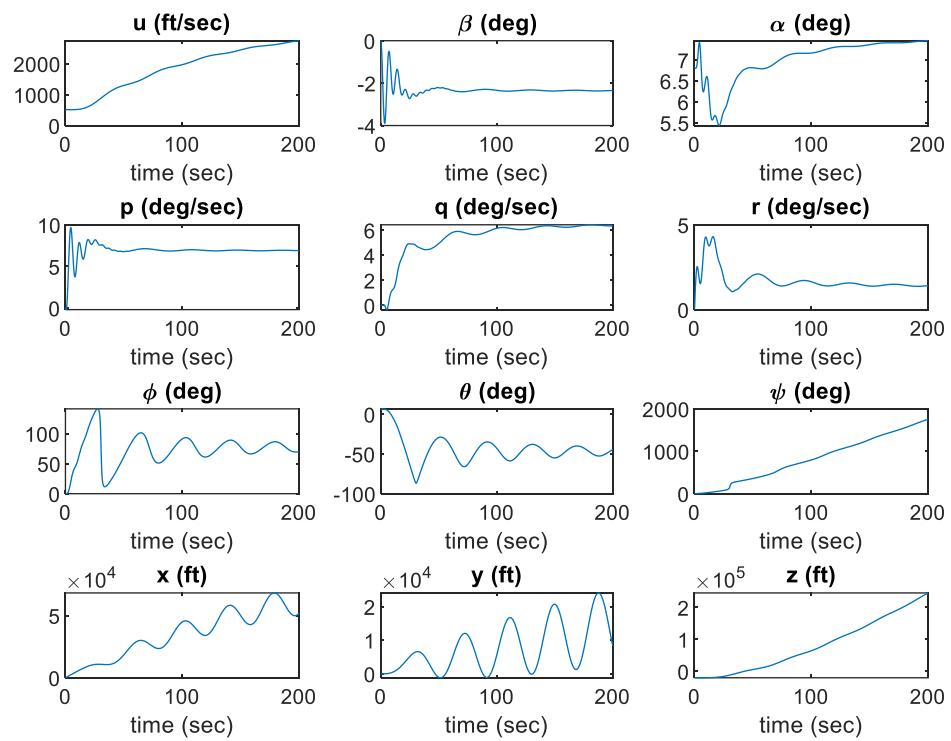




For -ve 5-degree rudder

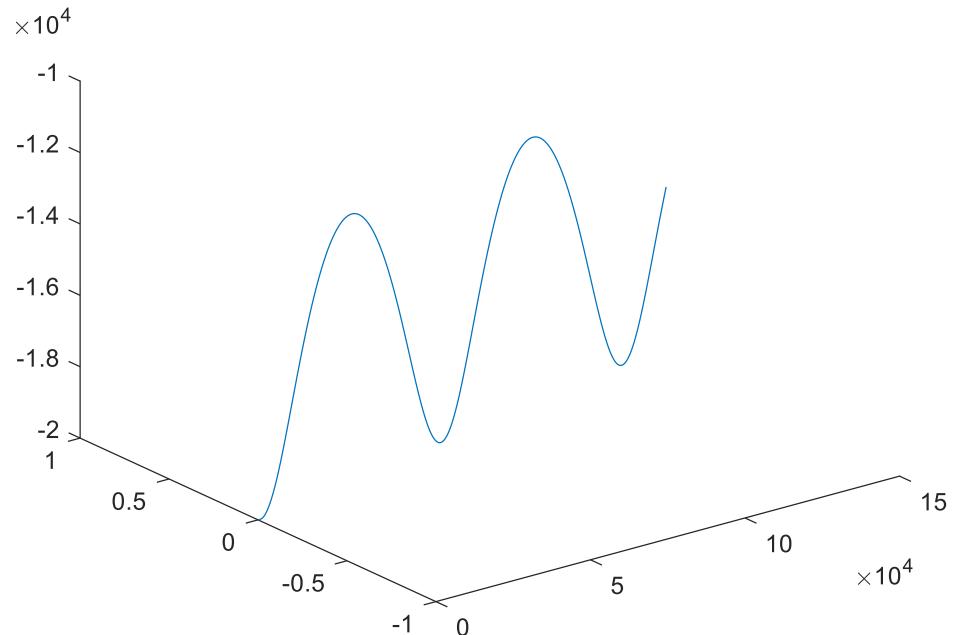
### Trajectory

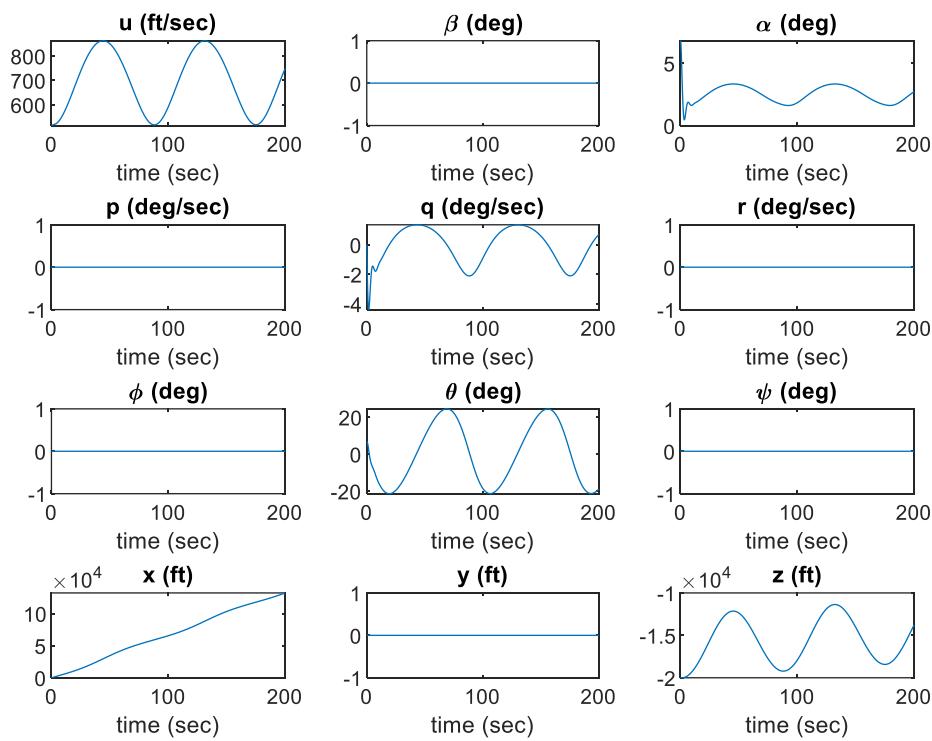




For +ve 5-degree elevator

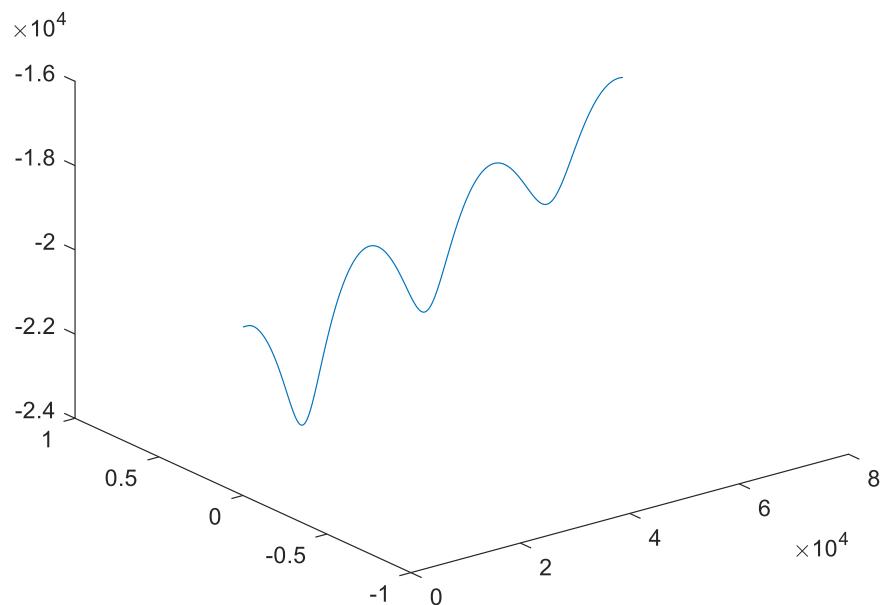
### Trajectory

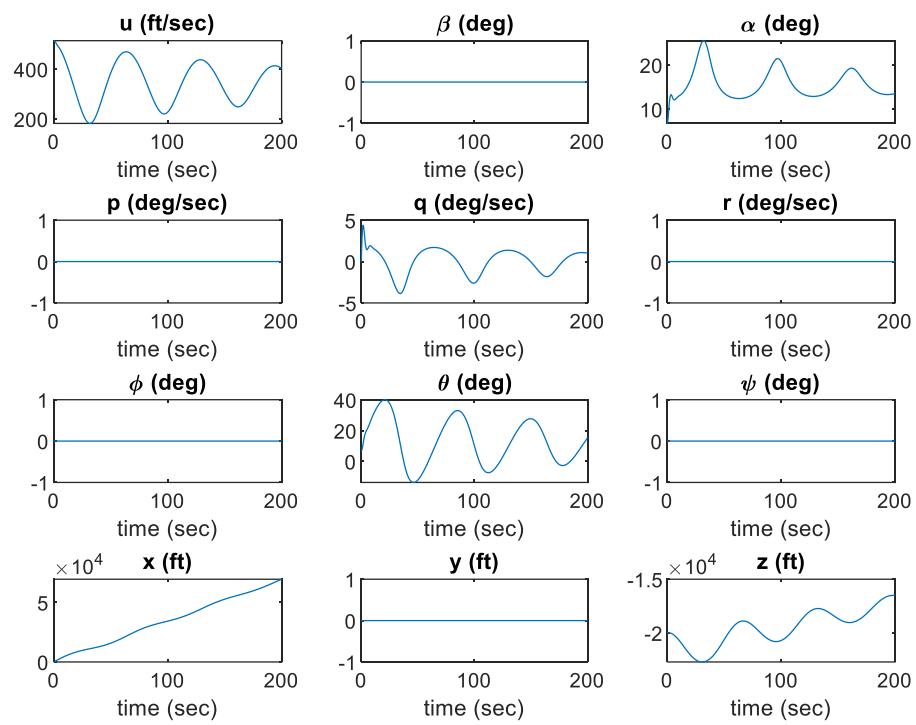




For -ve 5-degree elevator

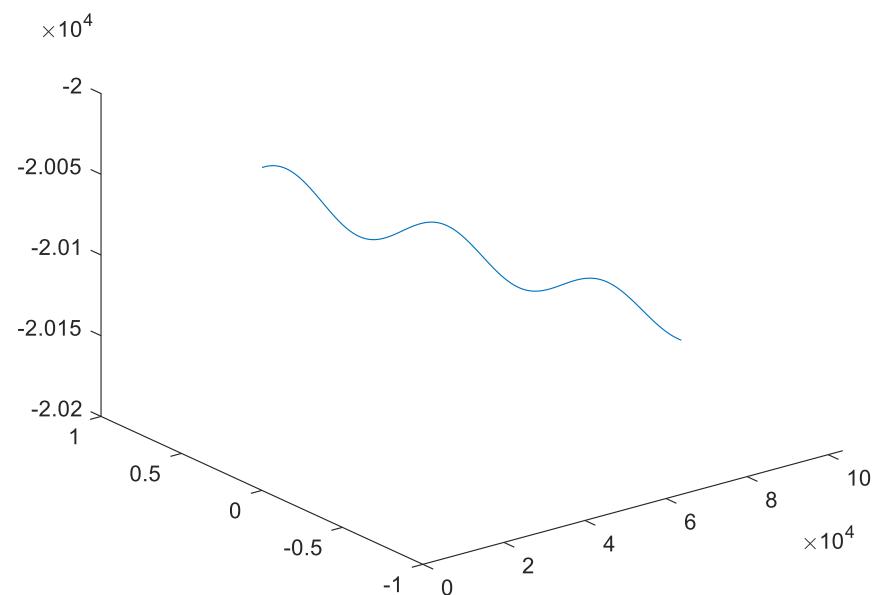
### Trajectory

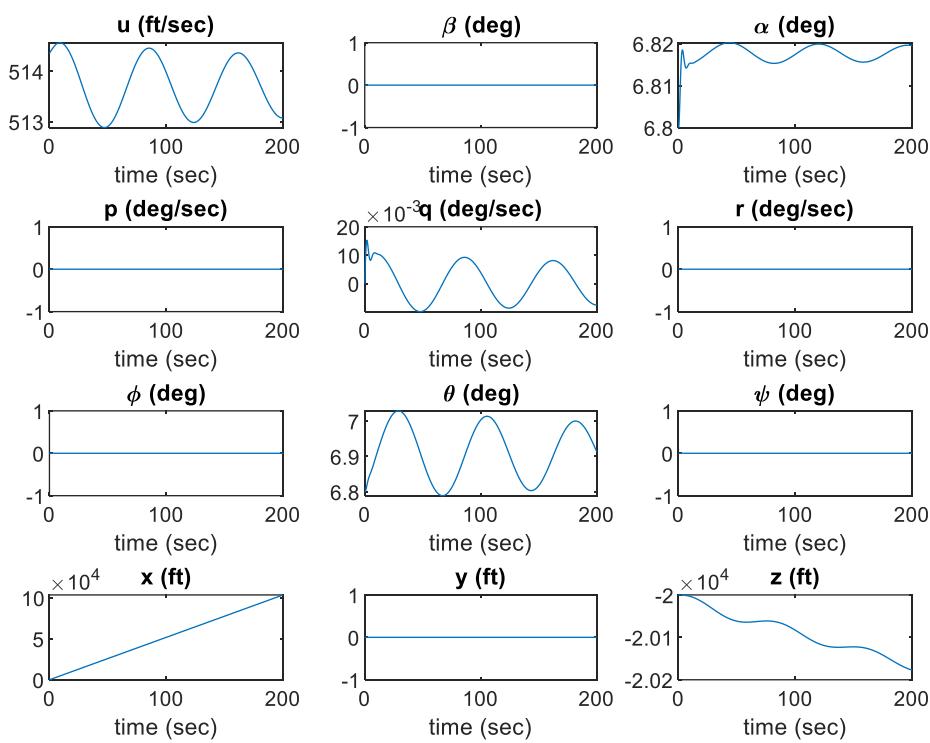




For 1000 in thrust

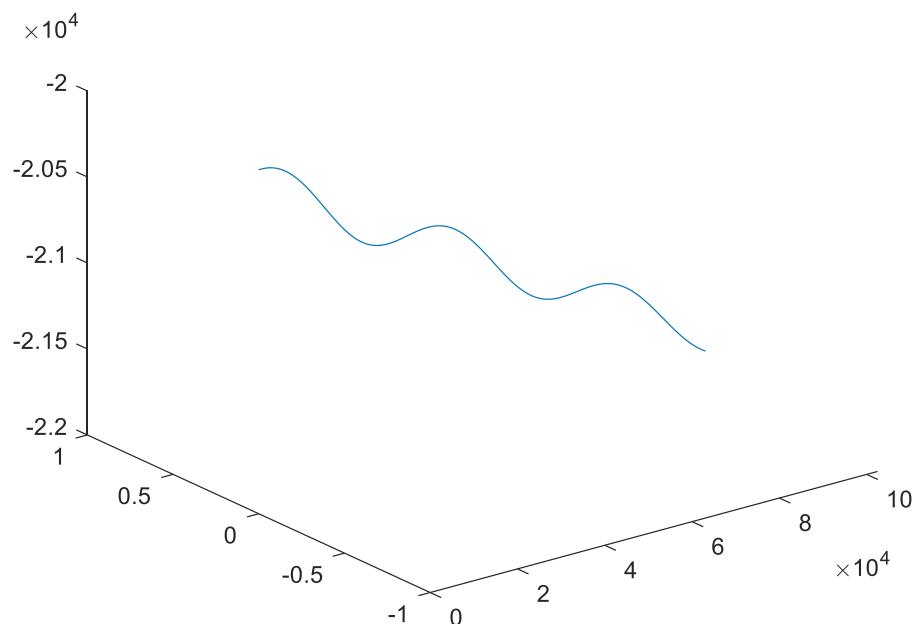
**Trajectory**

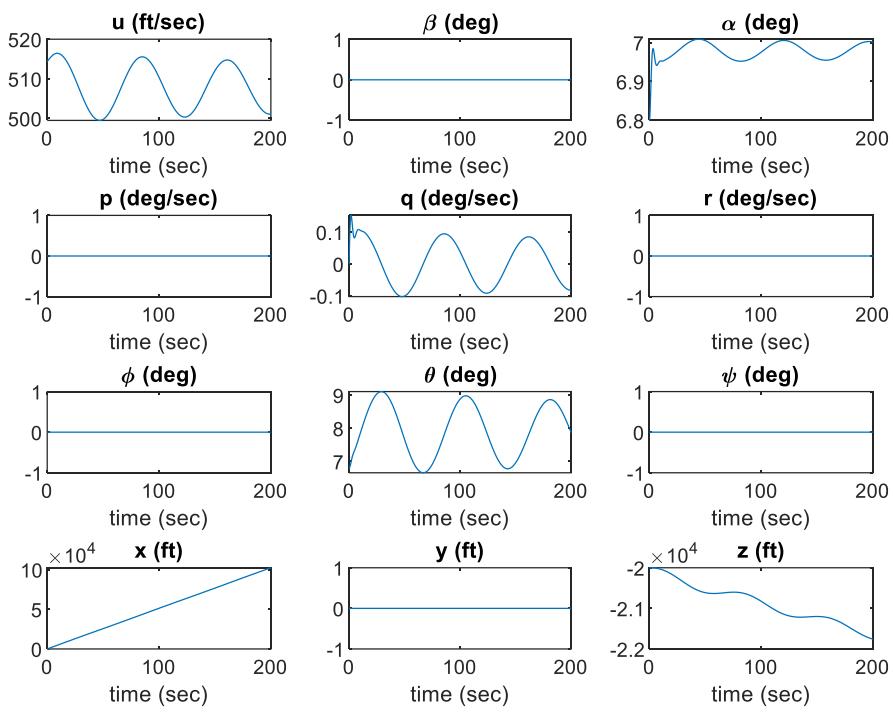




For 10000 in thrust

Trajectory

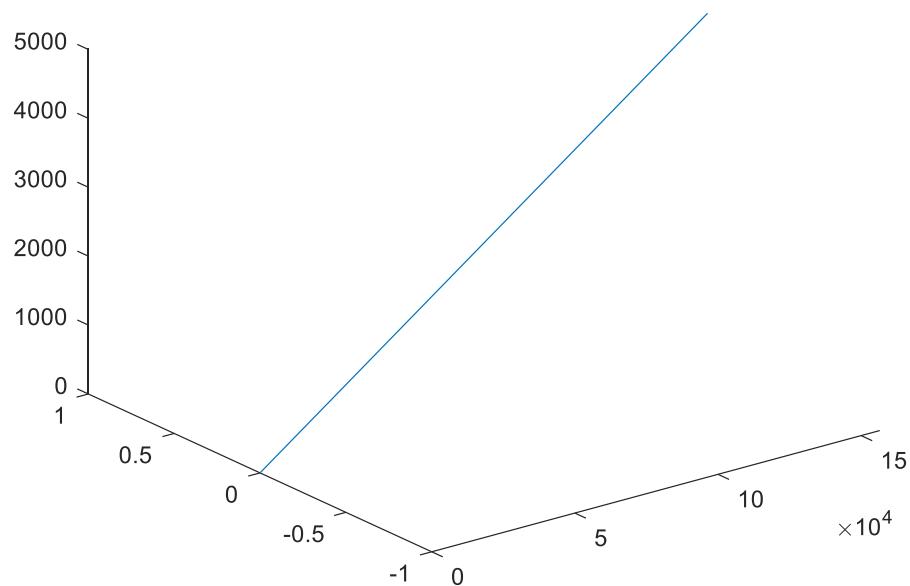


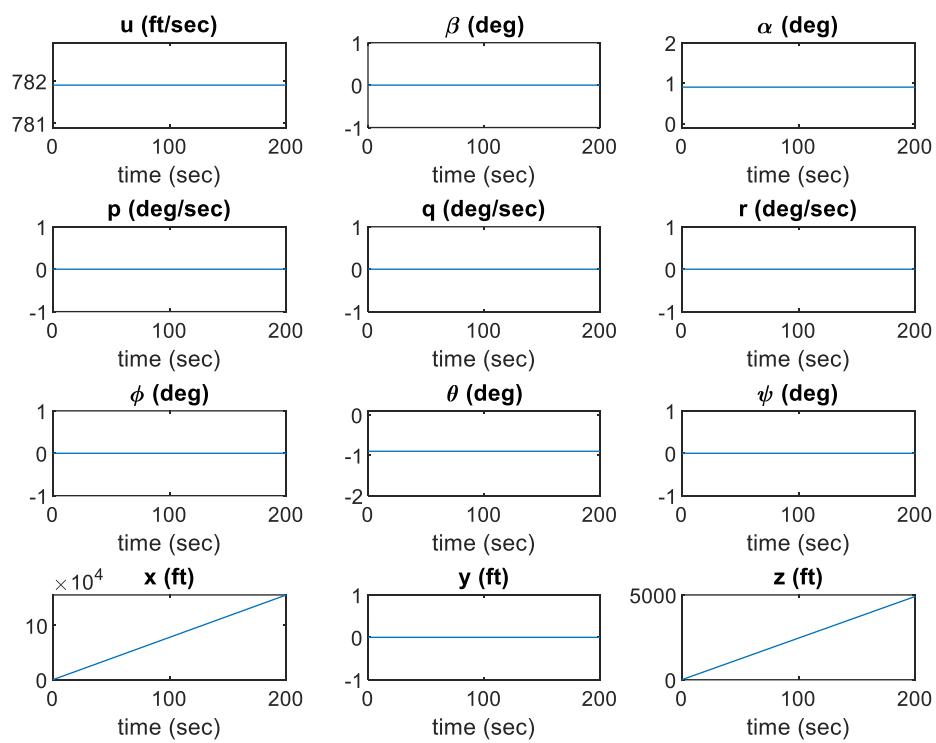


## Our airplane Plots (NT-33A)

For No input

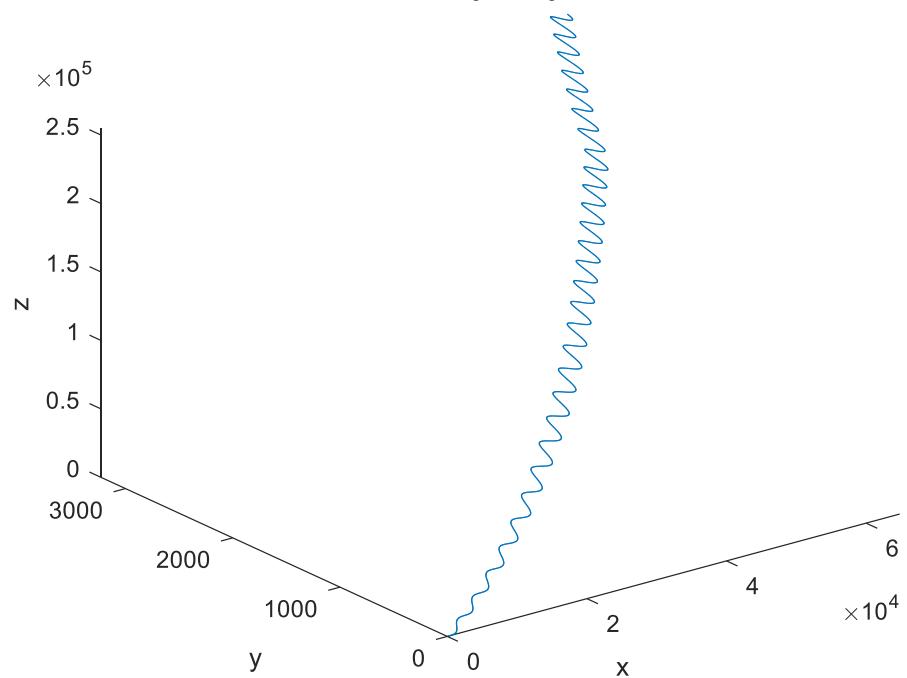
**Trajectory**

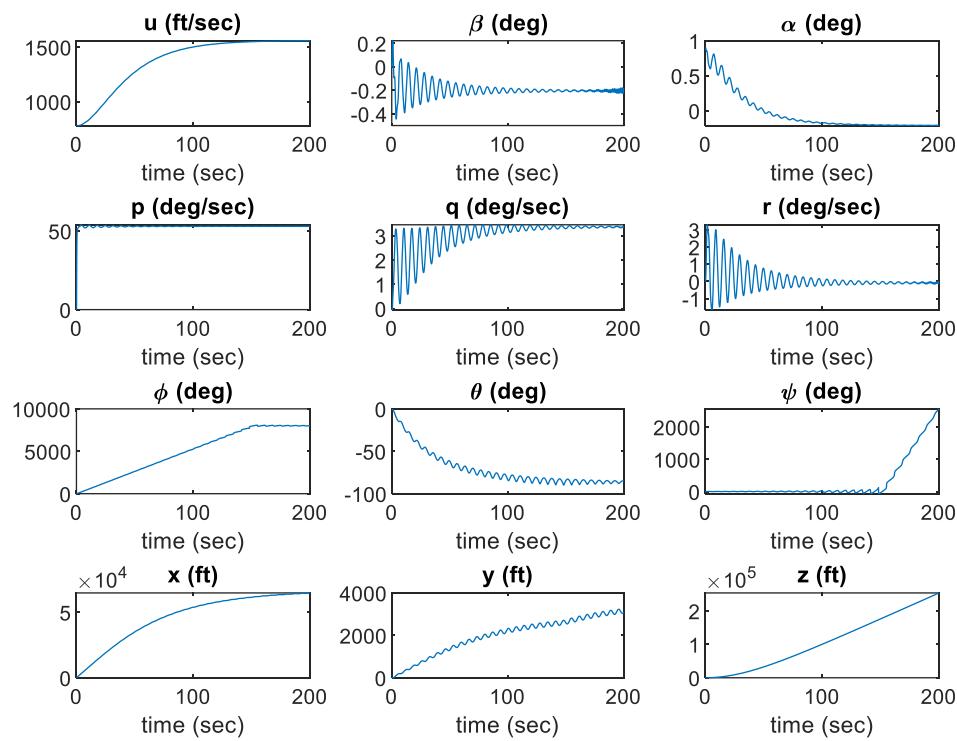




For +ve 5 degree aileron

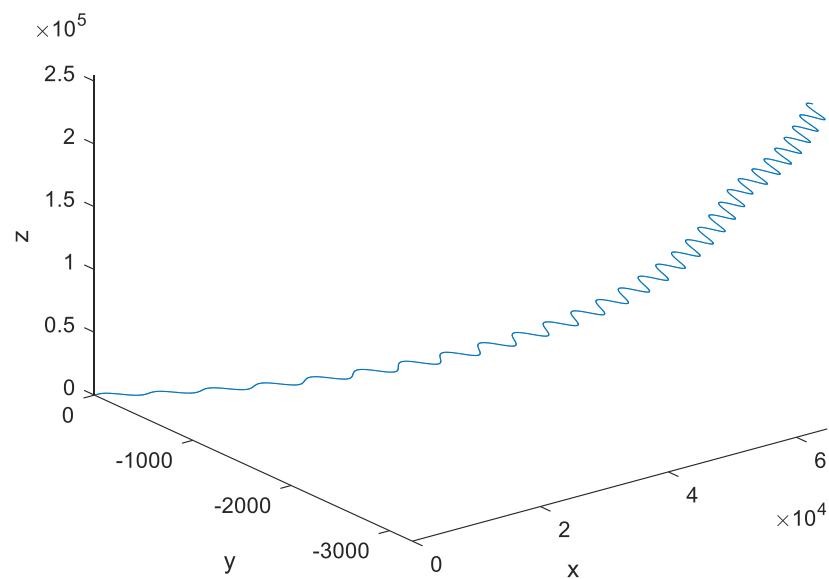
Trajectory

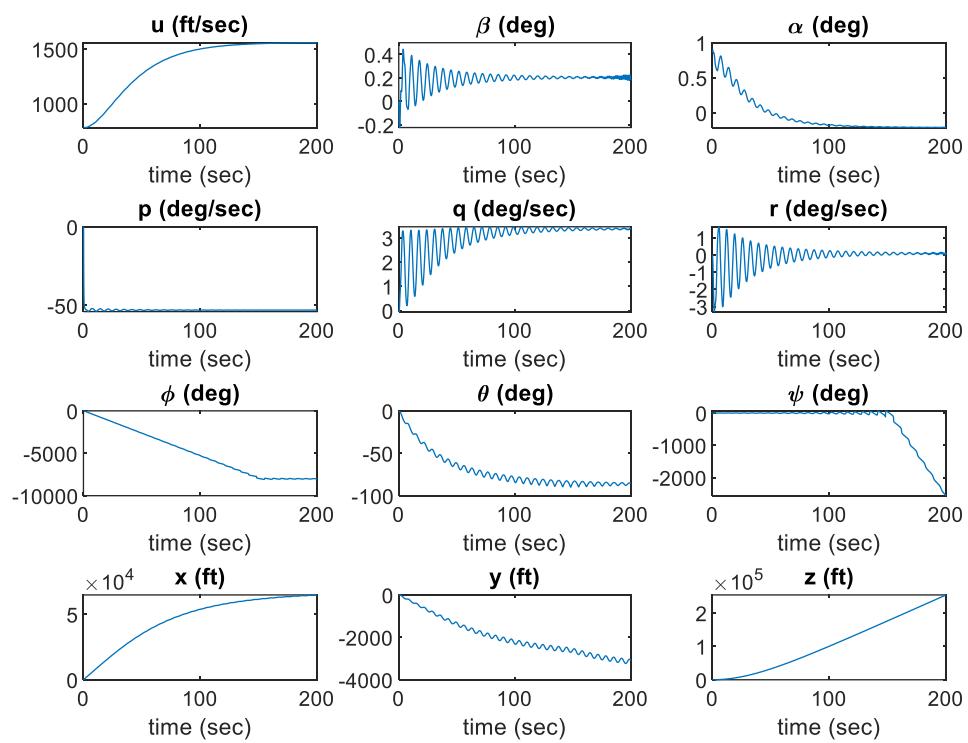




For -ve 5-degree aileron

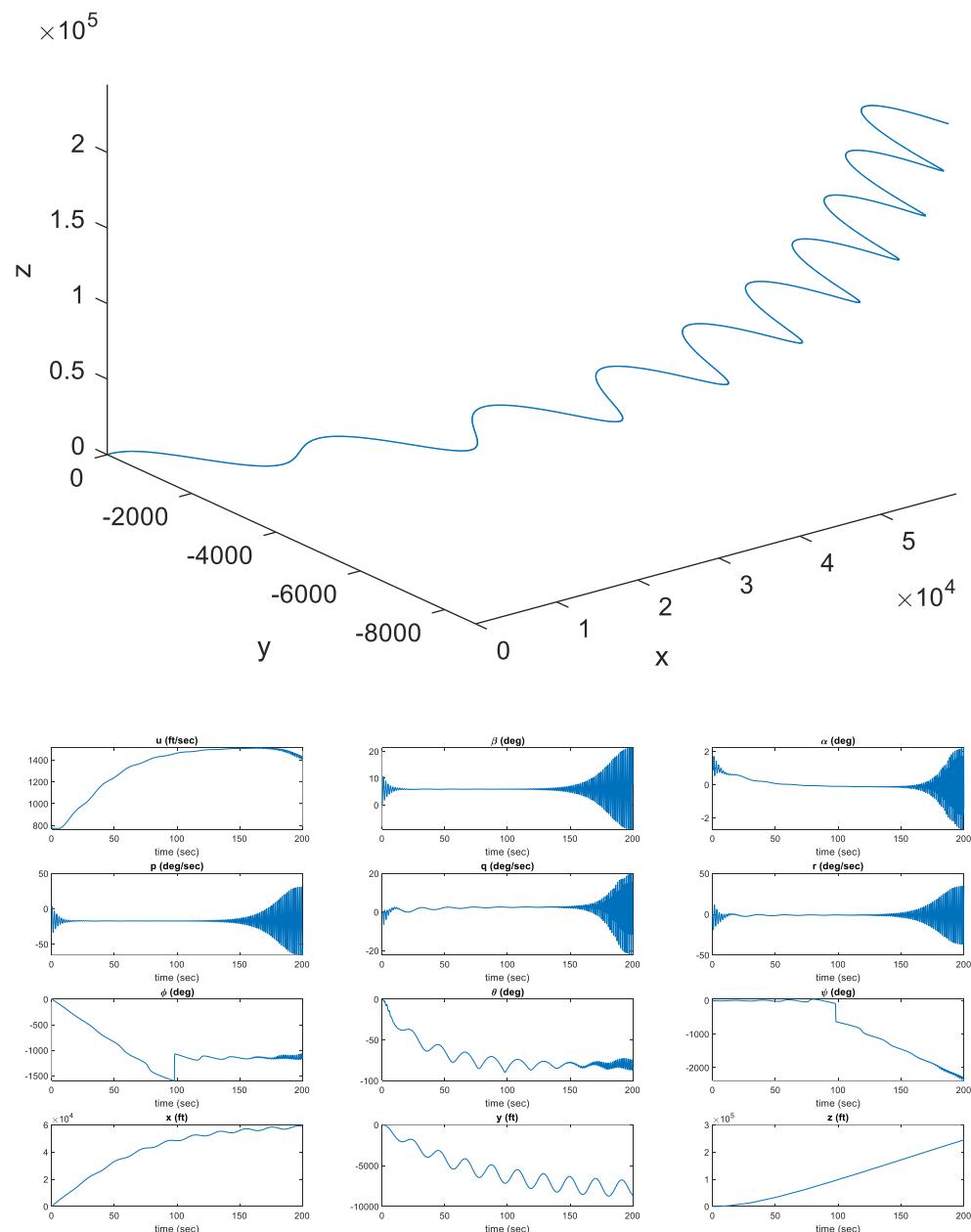
**Trajectory**



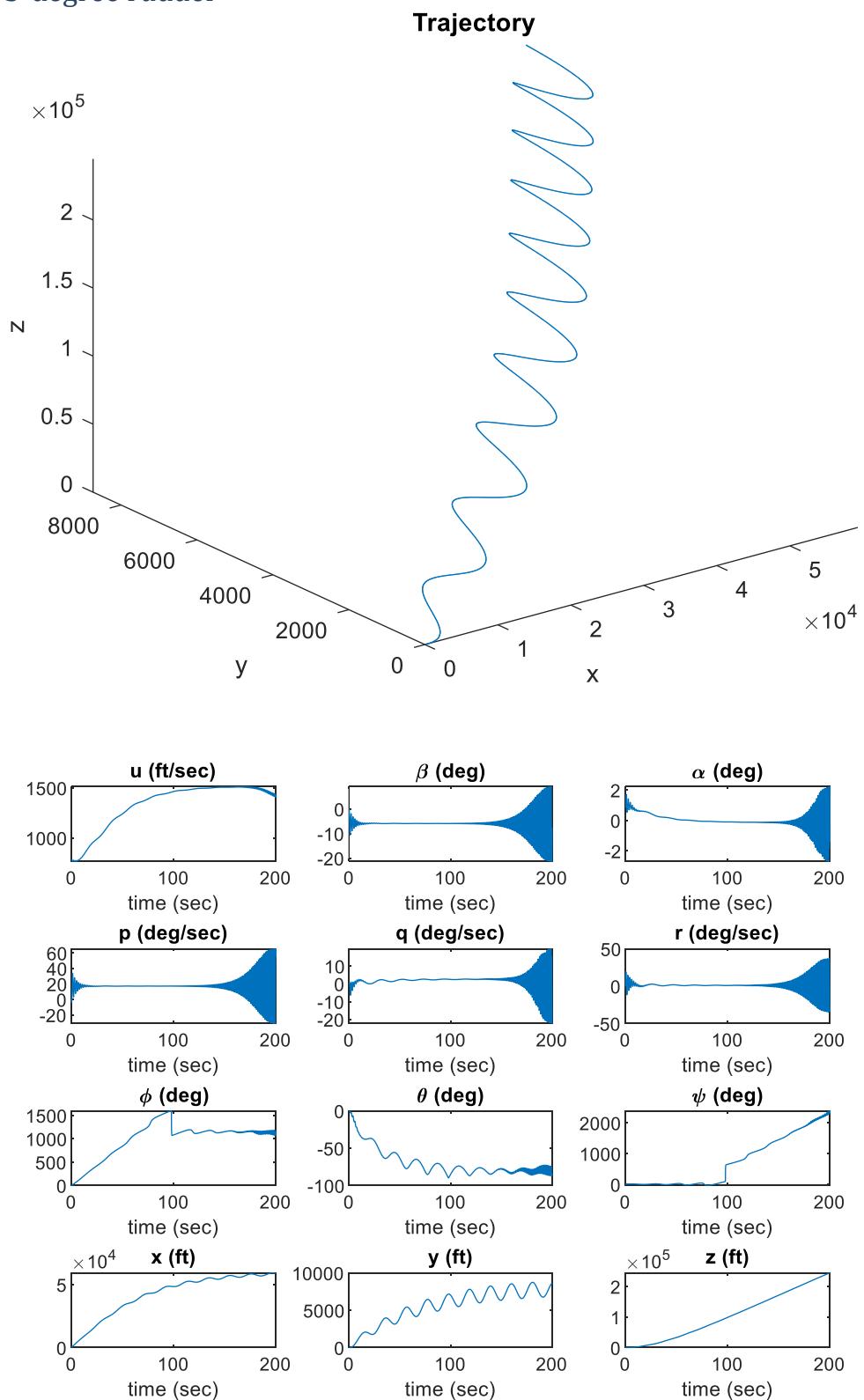


For +ve 5-degree rudder

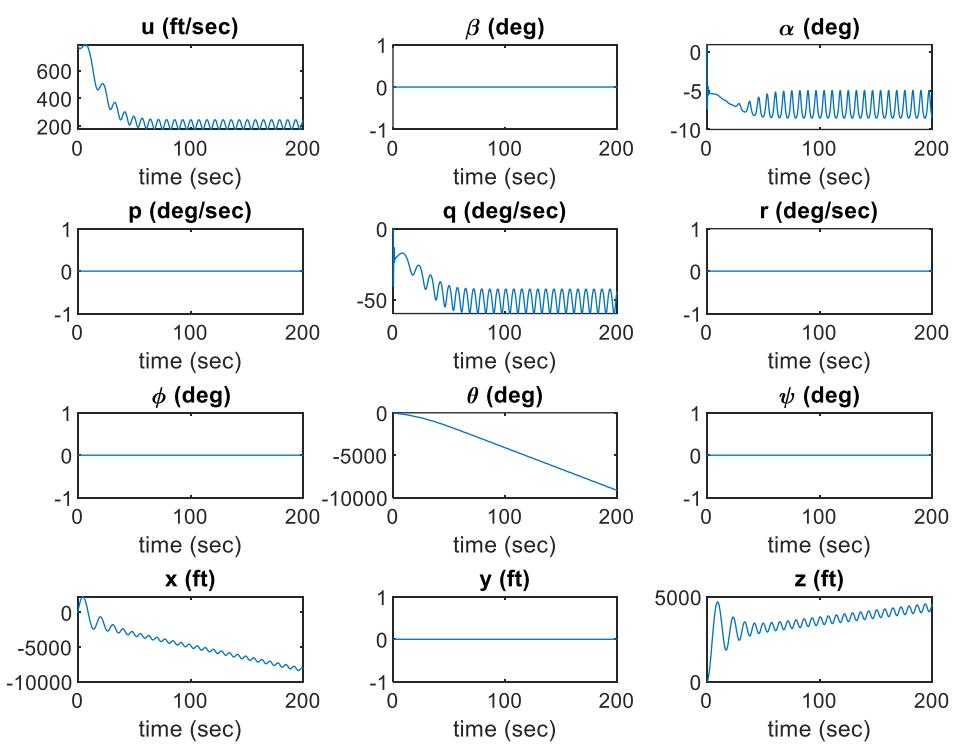
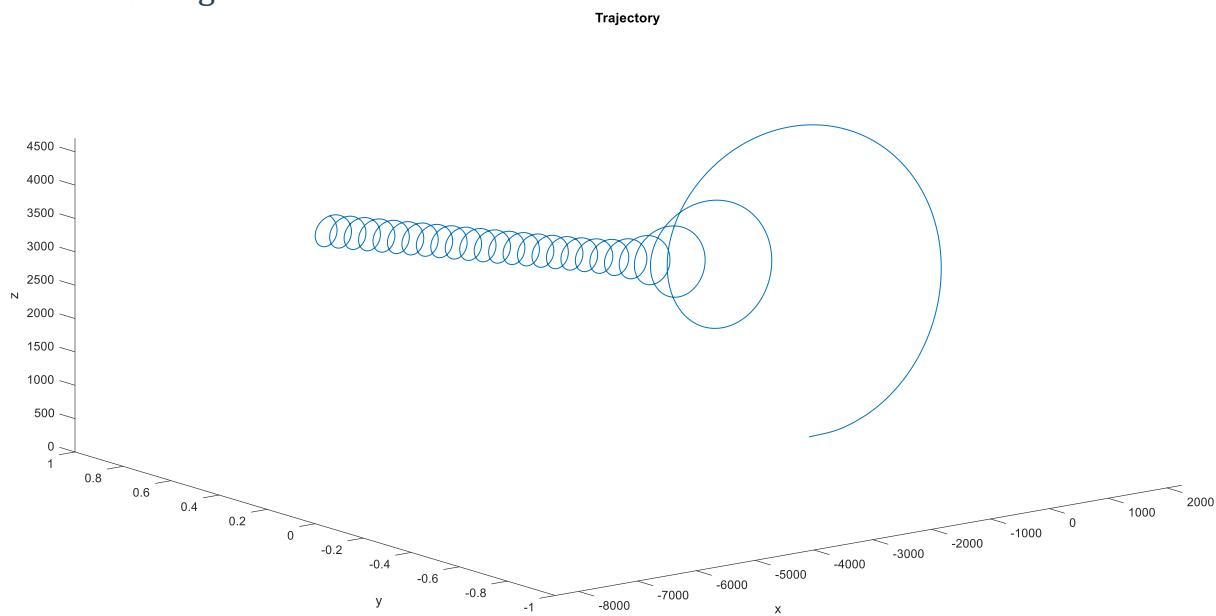
### Trajectory



For -ve 5-degree rudder

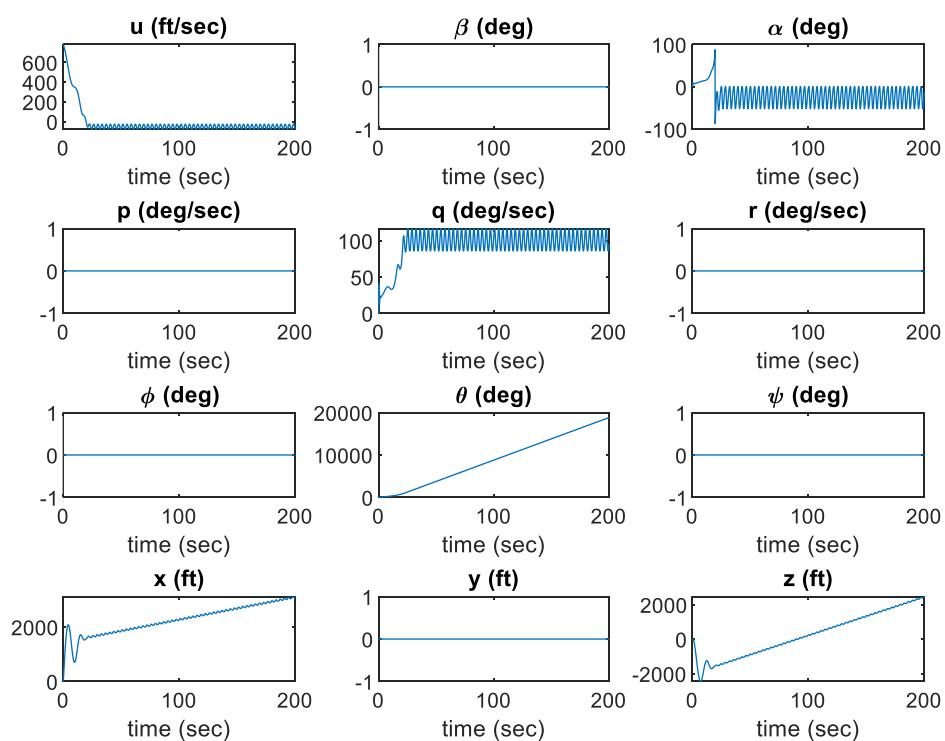
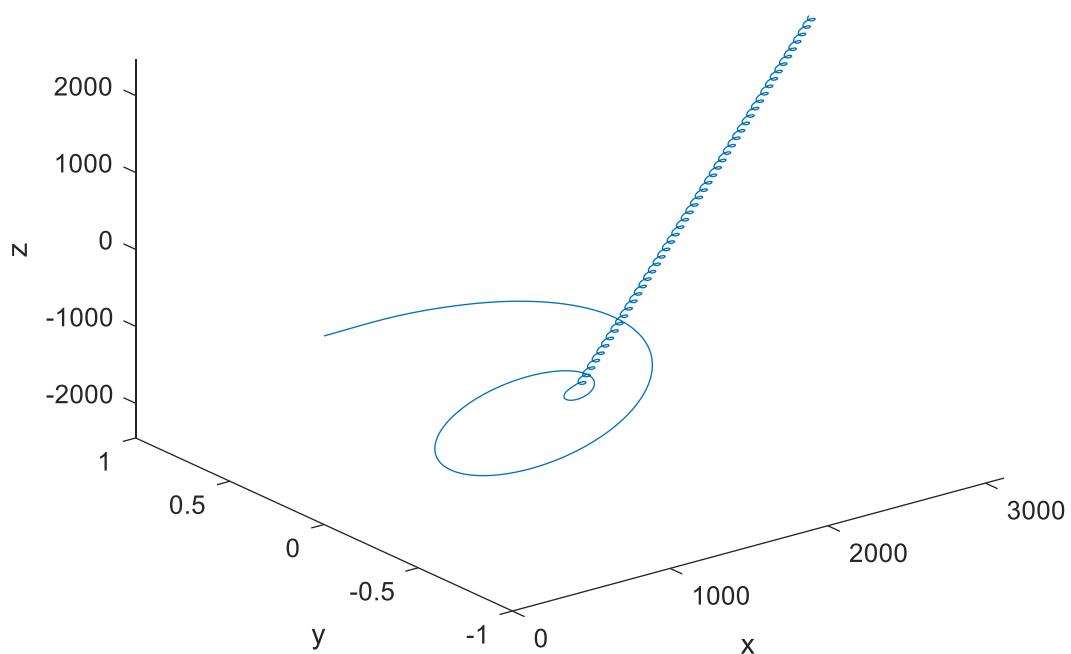


For +ve 5-degree elevator



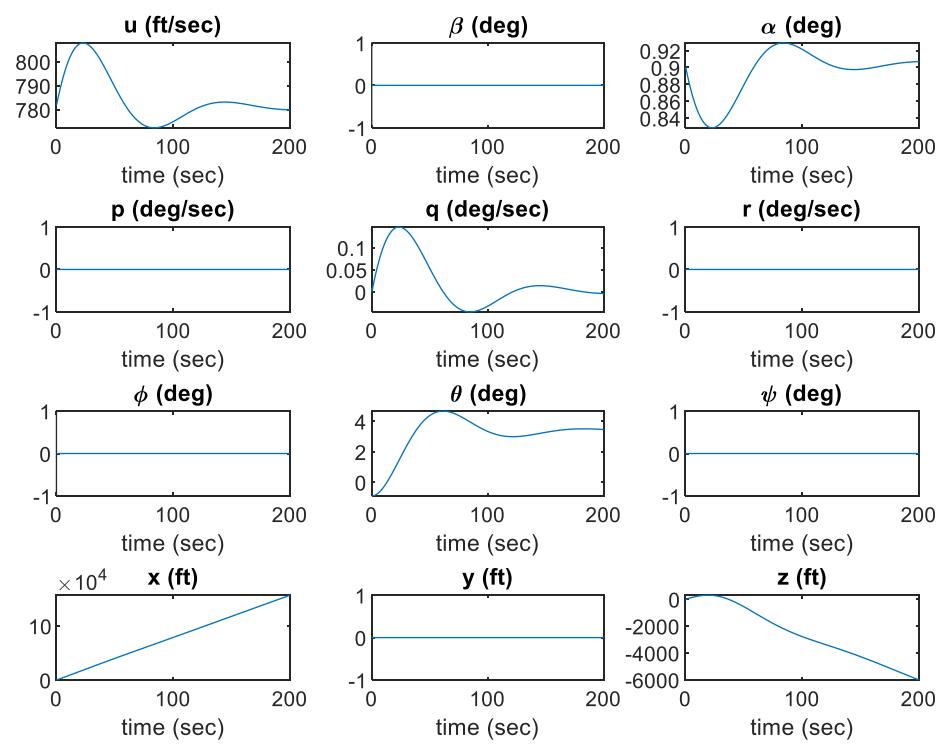
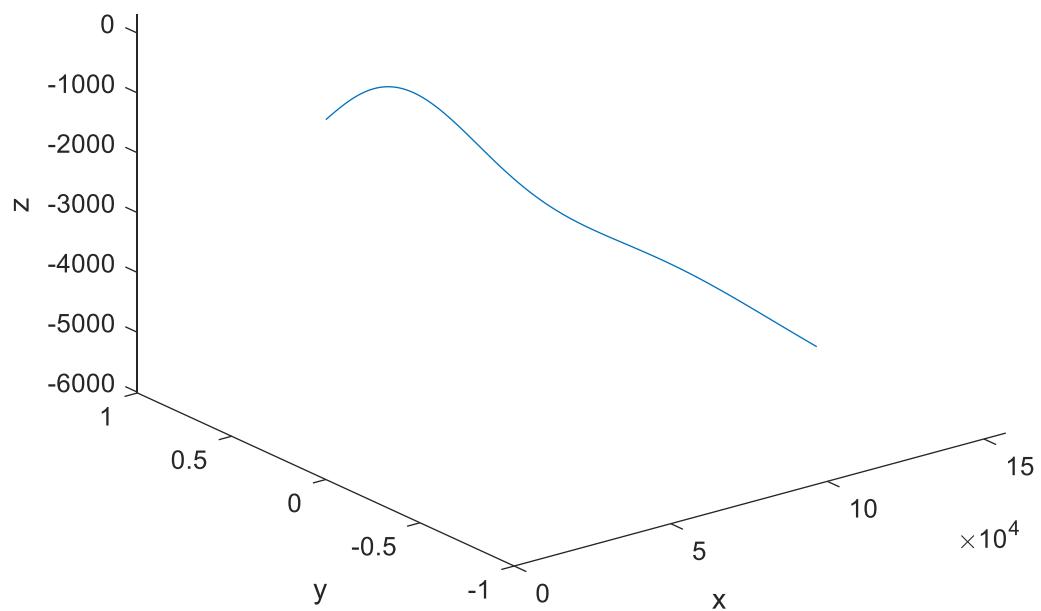
For -ve 5-degree elevator

### Trajectory



For 1000 in thrust

### Trajectory



For 10000 in thrust

### Trajectory

