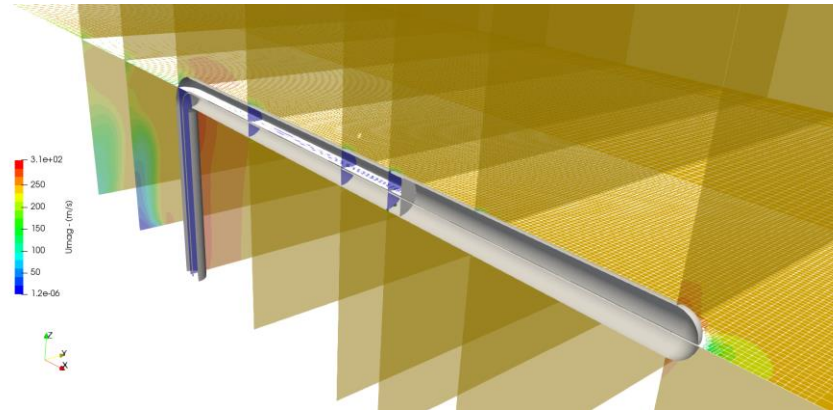


## SIMULATION OF A PITOT TUBE WITH OPENFOAM®

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Open-source environnement

**Geometry** : Salome®

**Meshing** : blockMesh and snappyHexMesh

**OpenFOAM® Solver** : simpleFoam and sonicFoam

**Post-processing** : Paraview® and Python

# □ GENERAL CONSIDERATIONS AND PITOT TUBE 3D GEOMETRY

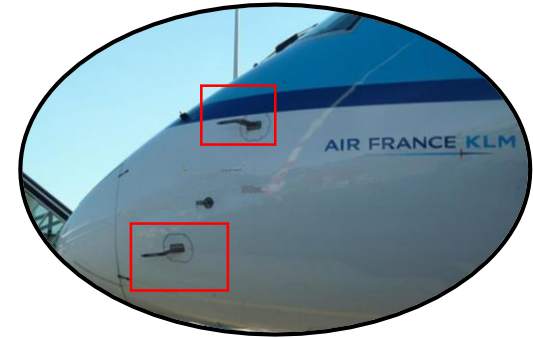
**Aim of the study : Compare theoretical and CFD pressure difference  $\Delta P_{THE}$  vs  $\Delta P_{CFD}$ .**  
**5 configurations : 0.1 ; 1 ; 67 ; 100 and 240 m/s**  
**Free geometry, fluid properties and physics**

*Pitot tube was invented by Henri PITOT in 1732 (French engineer)*

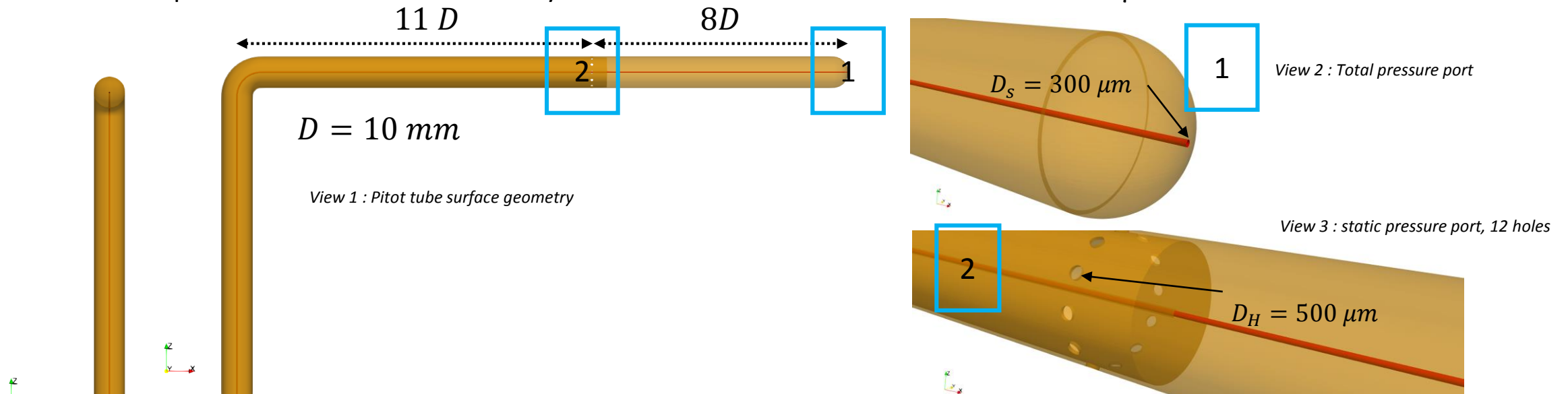
*Improved design by Prandtl and Darcy in the mid-19th century*

*Flow device used to measure fluid flow velocity (widely used for ship, aircraft and other applications)*

- The surface geometry of the device is generated using **SALOME®**
- The static pressure port is located  $8D$  behind the pitot noze ( $D$  being the Pitot's tube diameter)
- The total pressure port consists of a tube of diameter  $300 \mu m$
- The static port consists of an internal cavity linked to outside with 12 holes of diameter  $500 \mu m$



Example of Aircraft Pitot tubes for speed measurement  
Source : Toulouse University



# PHYSICS AND NUMERICAL SETTINGS

- At low **Mach number (Ma < 0.3)** CFD results can be compared to either  $p_t - p_s = \frac{1}{2} \rho v^2$  or  $\frac{p_t}{p_s} = \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{\gamma}{\gamma-1}}$
- Using **air** as working fluid leads to a **Mach number** of approximatively 0.64 for  $V = 240$  m/s. (Assuming  $\rho = 1$  kg/m<sup>3</sup> and  $P = 1$  bar:  $c = 376.6$  m/s). Thus a **compressible solver** of OpenFOAM® should be used to take into account compressibility effects. In this configuration the CFD pressure ratio has to be compared to  $\frac{p_t}{p_s} = \left(1 + \frac{\gamma-1}{2} M^2\right)^{\frac{\gamma}{\gamma-1}}$

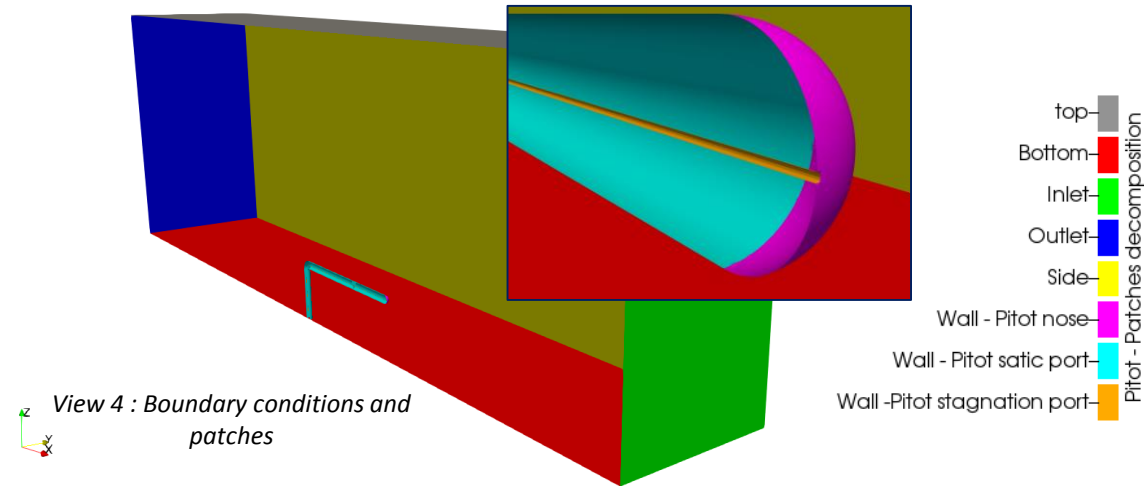
- The following table resume the main **physical characteristics** for each case :

Free stream velocity – m/s	Reynolds number (L = 0.2 m)	Turbulence	Mach number $\rho = 1, c = 376.6$ m/s	Compressibility effect
0.1	1280	OFF (Laminar)	$2.6 \cdot 10^{-4}$	OFF - simpleFoam
1	12820	On (k-omega SST)	$2.6 \cdot 10^{-3}$	OFF - simpleFoam
67	$8.59 \cdot 10^5$	On (k-omega SST)	0.18	OFF - simpleFoam
100	$1.28 \cdot 10^6$	On (k-omega SST)	0.27	OFF - simpleFoam
240	$3.08 \cdot 10^6$	On (k-omega SST)	0.64	ON – sonicFoam OFF – simpleFoam

Both simpleFoam and sonicFoam will be run for this speed

- Numerical schemes are second order for **div(phi,U)** (Gauss linearUpwindV grad(U) with limiter on grad(U) : cellLimited Gauss linear 1) and first order for other quantities such as turbulence (Gauss upwind)

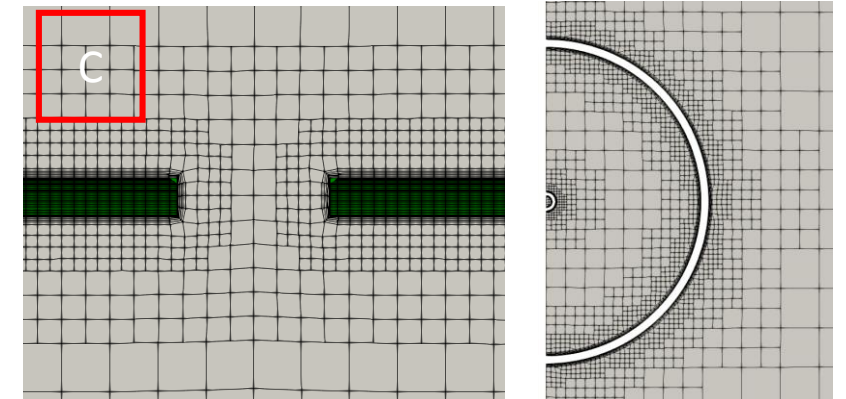
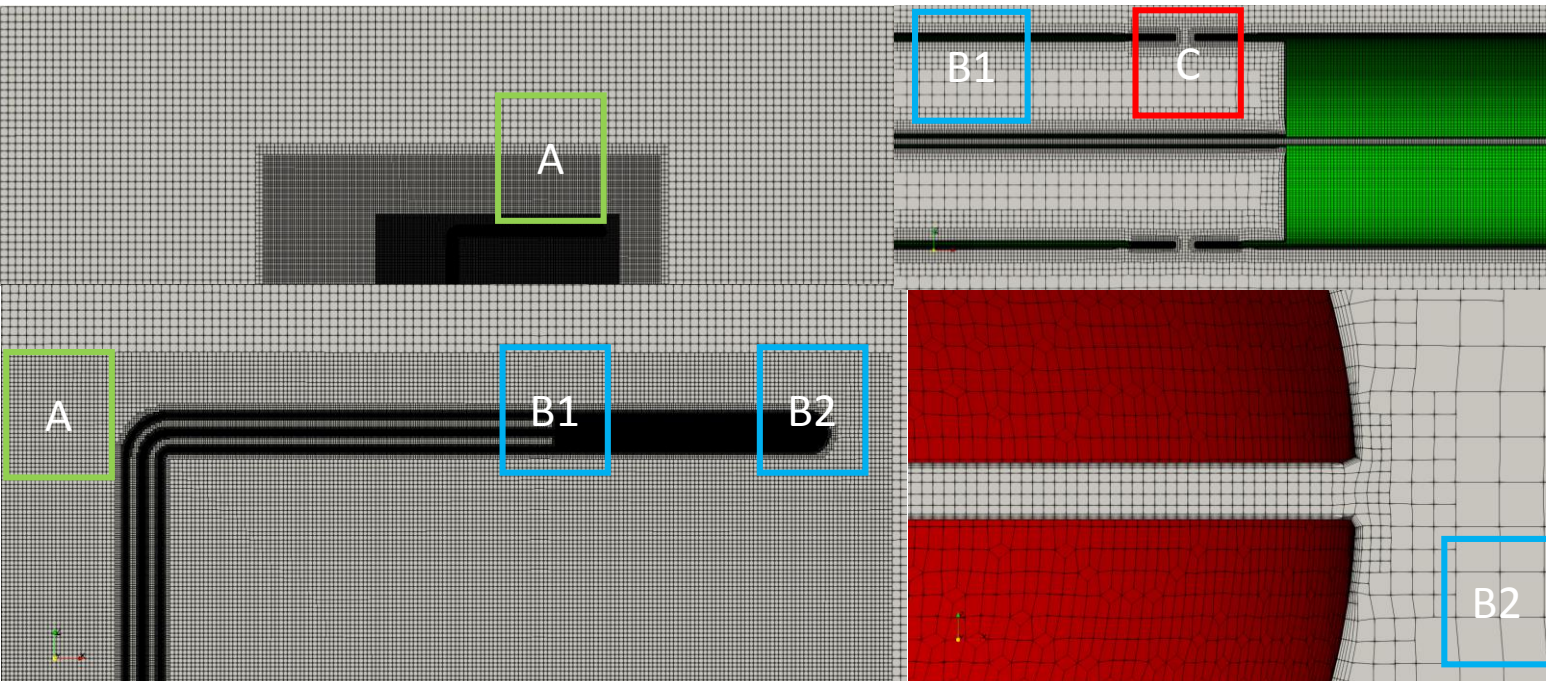
# □ BOUNDARY CONDITIONS AND 3D MESHING WITH SNAPPYHEXMESH (SHM)



- At inlet : velocity *fixedValue* ; *zeroGradient* condition for pressure. turbulence quantities are assessed using following expressions:

$$I_t = 0.01 \quad k = 0.5(U I_t)^2 \quad \omega = \frac{k^{\frac{3}{2}}}{l_t} \quad l_t = 20 \text{ cm}$$

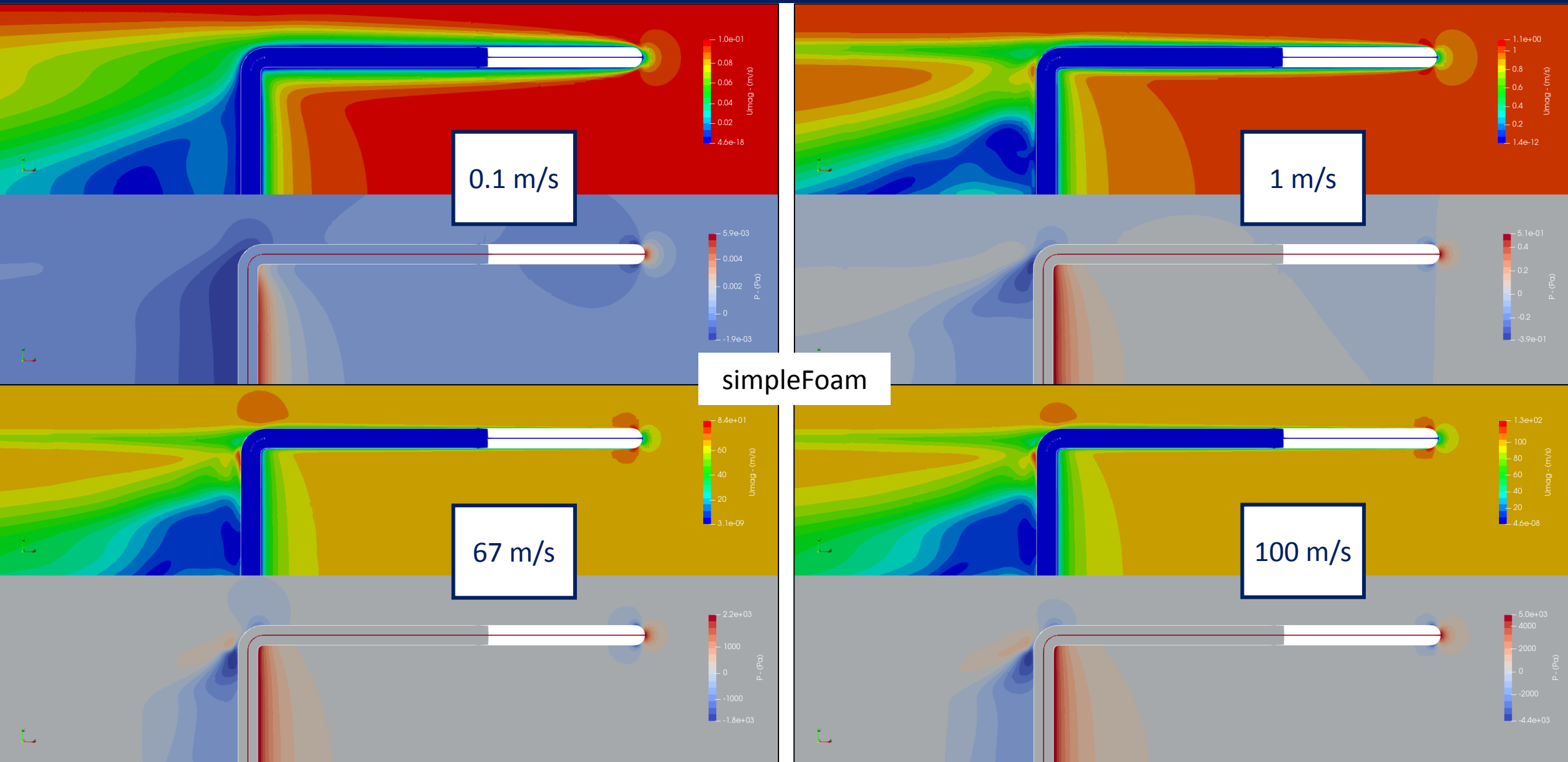
- Side, bottom and top patches are assumed to behave as “*slip wall*”
- Outlet : *fixedValue* for pressure and *zeroGradient* for other variables



- The surrounding box and background mesh are generated with **blockMesh** utility
- The mesh consists of approximately **6.3 M** hexahedral and prism layer cells and was generated with **snappyHexMesh** (semi-automated mesher).
- Insertion of **5 boundary layer elements** (cover layer of at least **99 %**)
- Small holes** are challenging with SHM and handled locally using the “**thin gap**” option of SHM.

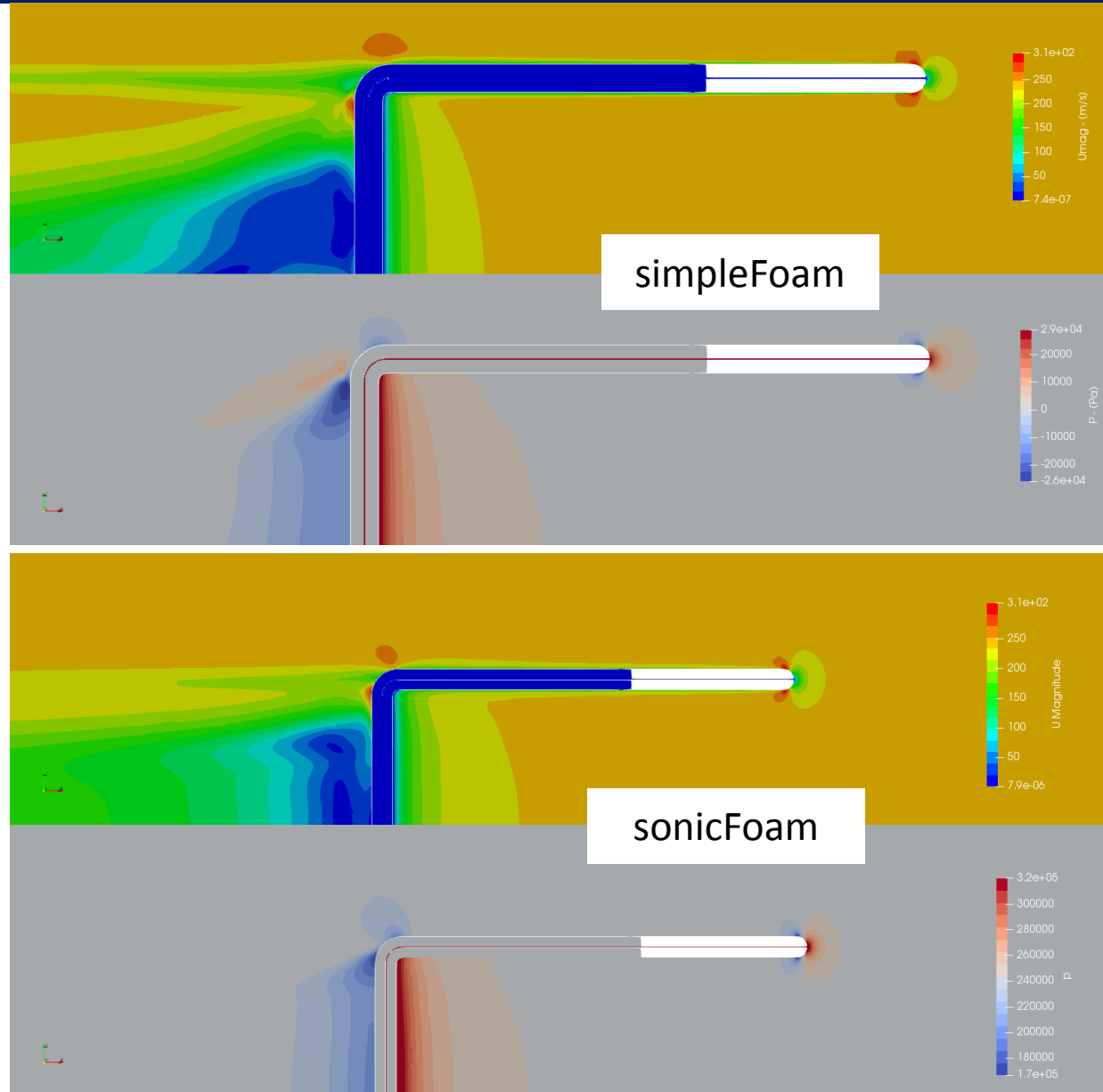


# ❏ RESULTS – PRESSURE AND VELOCITY FIELDS

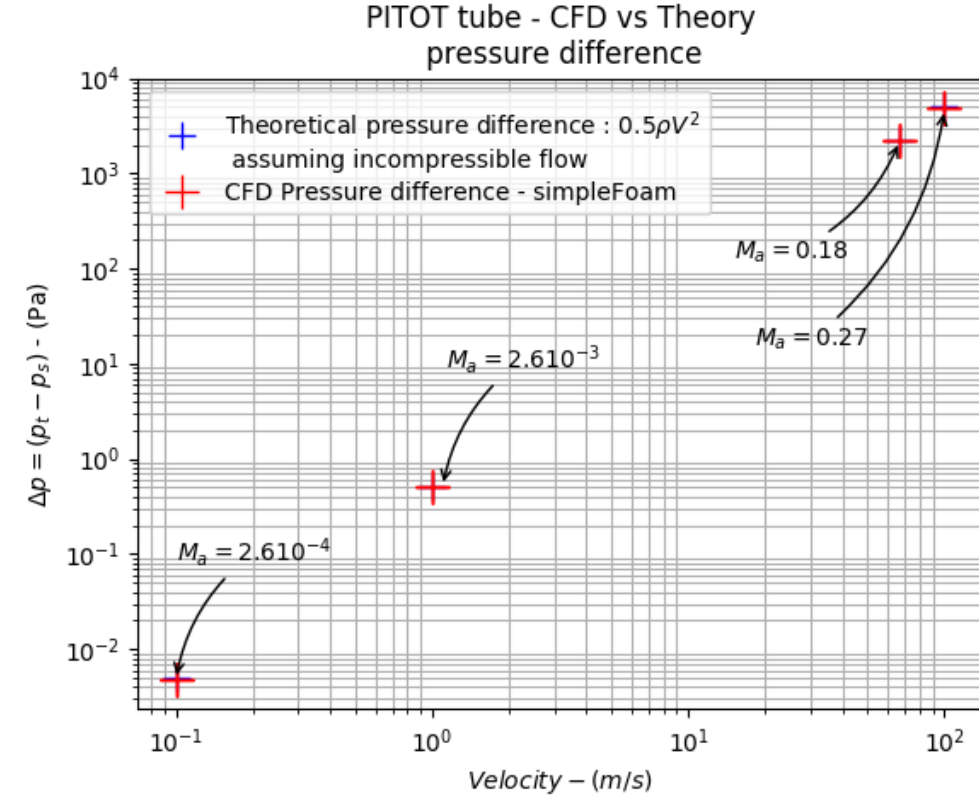
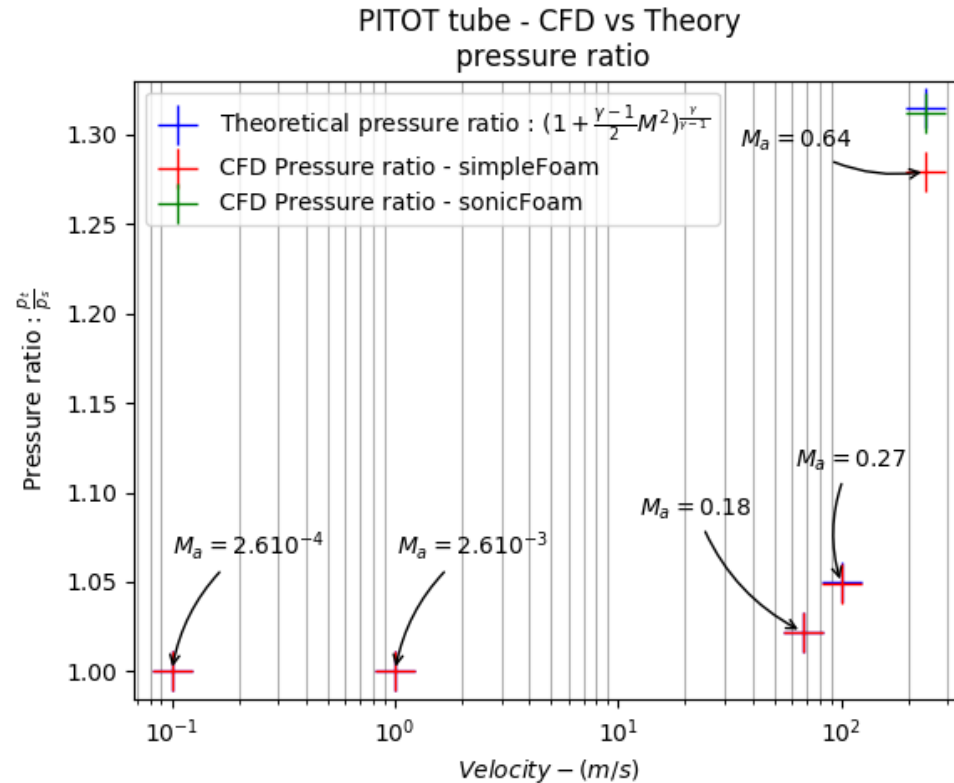


# ❏ RESULTS – PRESSURE AND VELOCITY FIELD

240 m/s



# RESULTS – CFD vs THEORY - COMPARISON



- Pressure difference is evaluated at the bottom of static and total pressure ports and compared to theoretical values.
- Results obtained with incompressible solver *simpleFoam* are in agreement with analytical pressure ratio if  $Ma < 0.3$ .
- At  $Ma 0.67$  ( $V = 240$  m/s) compressibility has to be taken into account. As expected results obtained with *simpleFoam* don't match theoretical pressure ratio
- Error with theory is significantly reduced using compressible solver *sonicFoam*.

The tutorial case is available at [www.cfd-training.com](http://www.cfd-training.com) !