

Trajectory Planning

EE366/CE366/CS380: Introduction to Robotics

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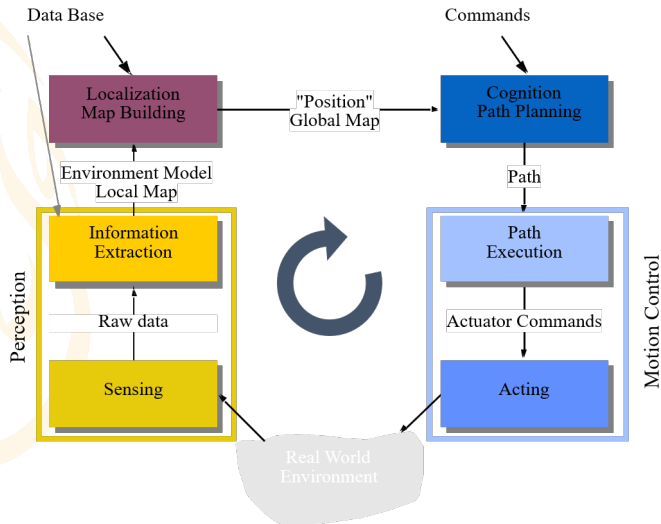
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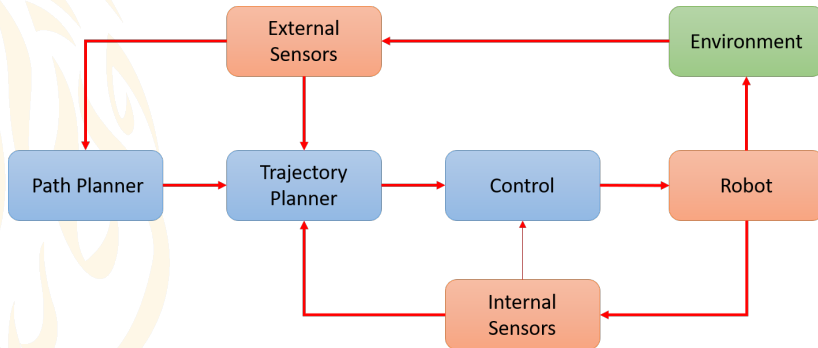


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Functional Decomposition of a Robot



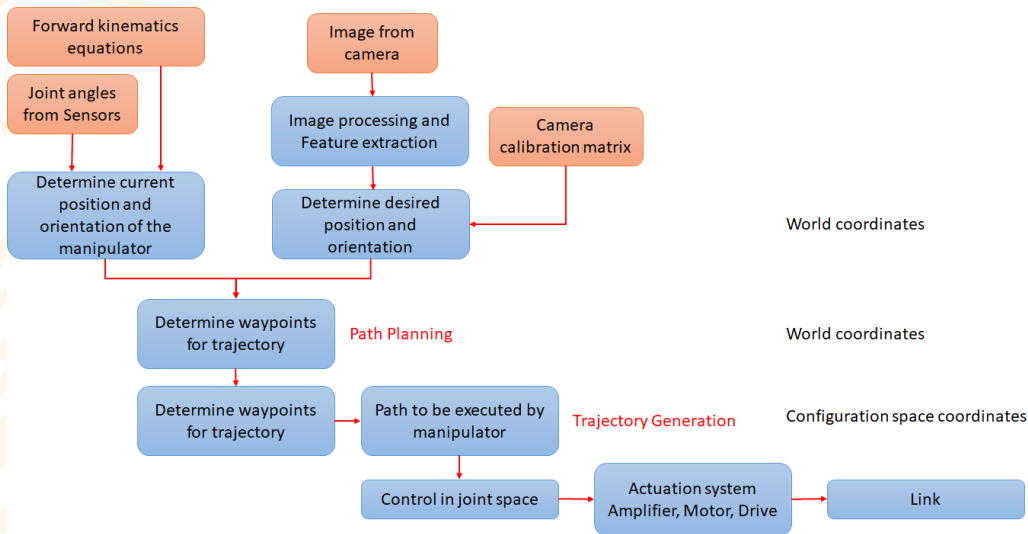




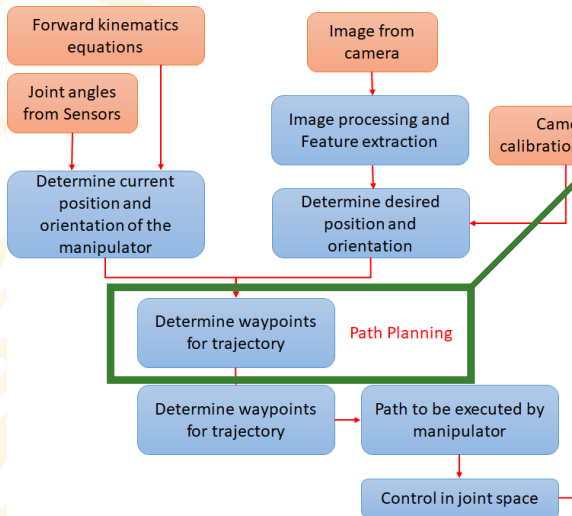
What are we missing?

- The FK and IK problems solved are point problems, dependent only on intrinsic geometry of robot.
- Given an initial and final configuration of robot, what could happen in between?
 - Transition should not make robot collide with obstacles, boundary of the map, or itself, at minimum.
 - Transition should require the actuators to exert generalized torques that don't violate their saturation limits, at minimum.
 - What else? Minimum time; Shortest distance; Avoiding singularities

What is needed to go point-point for pick & place, using camera?



What is path planning?

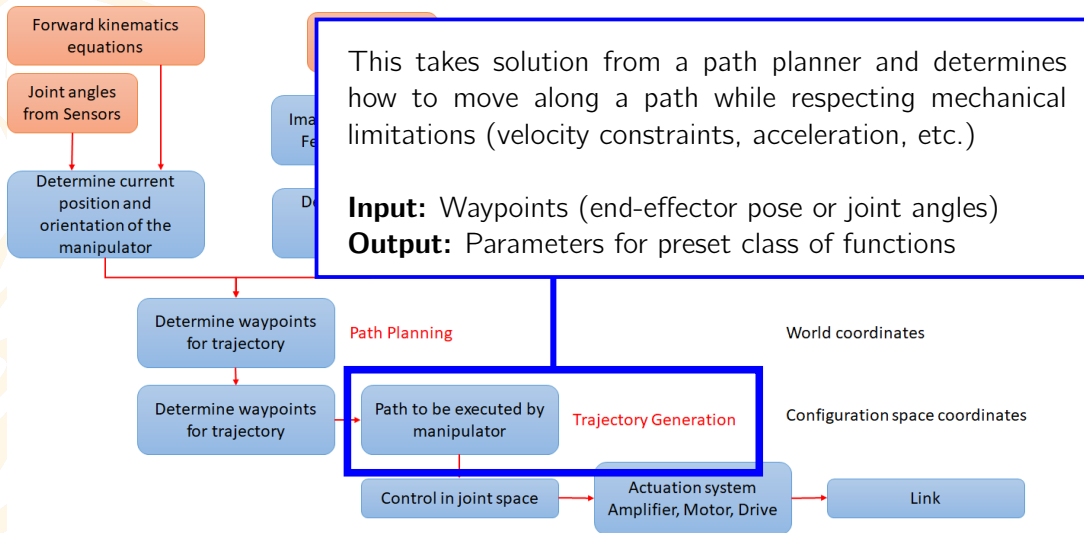


This is the purely geometric problem of finding a collision-free path between starting configuration and goal configuration, without concern for dynamics, duration of motion, constraints. It is also sometimes called piano mover's problem.

Input: Initial and final configurations, Map

Output: Waypoints

What is **trajectory** planning?





Trajectory vs Path

Path

Geometric description of sequence of configurations or end-effector poses achieved by the robot.

Trajectory

The specification of the robot configurations or end-effector poses as a function of time is called a trajectory. It is combination of path and timing law.

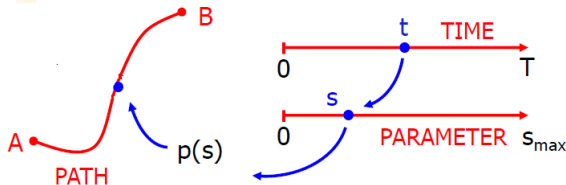




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Trajectory Planning and Generation

Sequence of poses
or configurations



Trajectory
Planner



Trajectories for
controller

Constraints:

Velocity, Acceleration

Actuator limits

Time

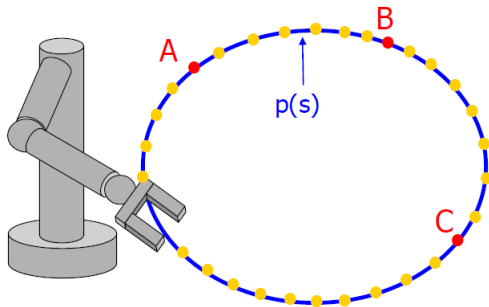
Path constraints



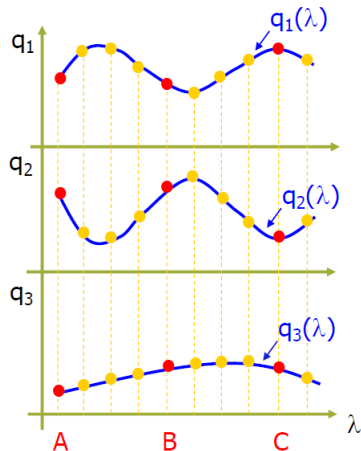
Where does input to trajectory planner come from?

- User typically specifies initial and desired final pose, because of complexity.
- An automatic path planner will also only provide a sequence of points along desired path (via points).
- Paths for industrial robots in static situations are specified by physically leading the robot through the desired motion with a teach pendant, the so-called **teach and playback mode**.

IK is used to transform trajectories to joint space.



Cartesian space



joint space



IK is used to transform trajectories to joint space.

- 1 Sequence of poses in Cartesian space (yellow points)
- 2 Interpolation in Cartesian space ($p(s)$)
- 3 Sampling and IK to move to joint space (red points)
- 4 Sequence of configurations in joint space
- 5 Interpolation in Joint space ($q(\lambda)$)



What other constraints does trajectory planner have?

- Timing law is not typically specified, but total trajectory time.
- Constraints on maximum velocities and accelerations, and specific values at points of interest.
- Saturation limits of actuators shouldn't be violated.



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Point-to-Point Motion

Given: Initial and Final configuration in joint space.



Desired properties of trajectories

- Joints positions and velocities, at least, should be continuous.
- Smooth trajectories are desirable.
 - Rough, jerky motions tend to cause increased wear on the mechanism and cause vibrations by exciting resonances in the manipulator.
- Trajectory generation happens at run-time, so generator shouldn't be computationally intensive.



Trajectories for point-point motion

- $q(t)$: Scalar Joint Variable

- Constraints:

$$q(t_0) = q_0$$

$$\dot{q}(t_0) = v_0$$

$$q(t_f) = q_f$$

$$\dot{q}(t_f) = v_f$$

- Other possible constraints:

$$\ddot{q}(t_0) = \alpha_0$$

$$\ddot{q}(t_f) = \alpha_f$$

- Infinitely many trajectories passing through these constraints.

- Choose parameterized family of functions, e.g. polynomials based on number of constraints.



Only position and velocity constraints: Cubic Polynomials

$$q(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

$$q_0 = a_0 + a_1 t_0 + a_2 t_0^2 + a_3 t_0^3$$

$$v_0 = a_1 + 2a_2 t_0 + 3a_3 t_0^2$$

$$q_f = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3$$

$$v_f = a_1 + 2a_2 t_f + 3a_3 t_f^2$$

$$\begin{bmatrix} 1 & t_0 & t_0^2 & t_0^3 \\ 0 & 1 & 2t_0 & 3t_0^2 \\ 1 & t_f & t_f^2 & t_f^3 \\ 0 & 1 & 2t_f & 3t_f^2 \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \end{bmatrix} = \begin{bmatrix} q_0 \\ v_0 \\ q_f \\ v_f \end{bmatrix}$$

- Determinant of coefficient matrix is $(t_f - t_0)^4$
 - Unique solution exists for every non-zero time interval.

Cubic Polynomial Trajectories have a jump in acceleration.

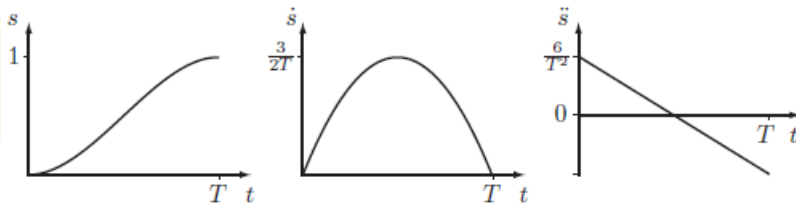


Figure: Plots of q , \dot{q} , \ddot{q} for cubic time scaling

- In cubic case, there is jump in acceleration at $t = 0$ and $t = t_f$.
- Infinite jerk \rightarrow Possible vibrations.



Position, Velocity, Acceleration constraints: Quintic Polynomials

$$q(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3 + a_4 t^4 + a_5 t^5$$

$$q_0 = a_0 + a_1 t_0 + a_2 t_0^2 + a_3 t_0^3 + a_4 t_0^4 + a_5 t_0^5$$

$$v_0 = a_1 + 2a_2 t_0 + 3a_3 t_0^2 + 4a_4 t_0^3 + 5a_5 t_0^4$$

$$\alpha_0 = 2a_2 + 6a_3 t_0 + 12a_4 t_0^2 + 20a_5 t_0^3$$

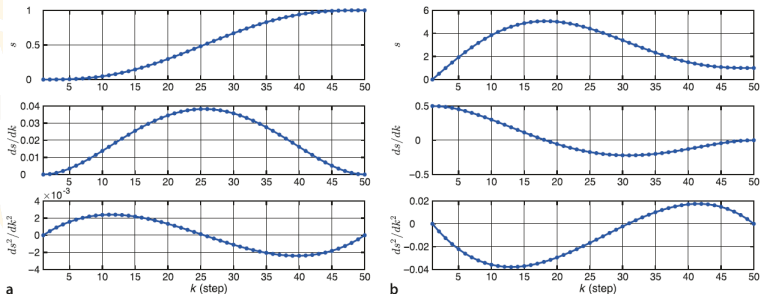
$$q_f = a_0 + a_1 t_f + a_2 t_f^2 + a_3 t_f^3 + a_4 t_f^4 + a_5 t_f^5$$

$$v_f = a_1 + 2a_2 t_f + 3a_3 t_f^2 + 4a_4 t_f^3 + 5a_5 t_f^4$$

$$\alpha_f = 2a_2 + 6a_3 t_f + 12a_4 t_f^2 + 20a_5 t_f^3$$

$$\begin{bmatrix} 1 & t_0 & t_0^2 & t_0^3 & t_0^4 & t_0^5 \\ 0 & 1 & 2t_0 & 3t_0^2 & 4t_0^3 & 5t_0^4 \\ 0 & 0 & 2 & 6t_0 & 12t_0^2 & 20t_0^3 \\ 1 & t_f & t_f^2 & t_f^3 & t_f^4 & t_f^5 \\ 0 & 1 & 2t_f & 3t_f^2 & 4t_f^3 & 5t_f^4 \\ 0 & 0 & 2 & 6t_f & 12t_f^2 & 20t_f^3 \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \\ a_2 \\ a_3 \\ a_4 \\ a_5 \end{bmatrix} = \begin{bmatrix} q_0 \\ v_0 \\ \alpha_0 \\ q_f \\ v_f \\ \alpha_f \end{bmatrix}$$

Issues with Quintic Polynomial Trajectories



- Velocity is less than maximum most of time.
- For non-zero initial velocity, trajectory overshoots the end values.

Linear Segments with Parabolic Blends (LSPB)

- Common for control of motors.
- Velocity profile is trapezoidal – constant acceleration phase (a), constant velocity phase (v), constant deceleration phase
- The q profile is concatenation of parabola, linear, and parabola.

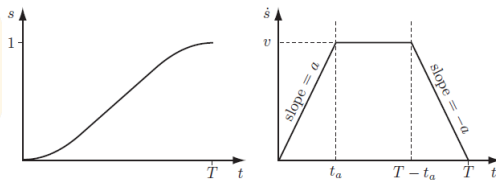


Figure: Plots of s , \dot{s} for trapezoidal time scaling

■ **Assuming, motion is possible**

- For simplicity: $t_0 = 0$, $t_f = T$,
 $\dot{q}(t_0) = \dot{q}(t_f) = 0$

$$q(t) = a_0 + a_1 t + a_2 t^2$$

$$\Rightarrow \dot{q}(t) = a_1 + 2a_2 t$$

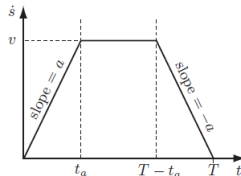
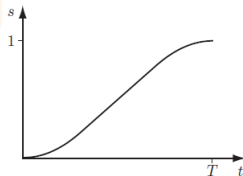
For $0 \leq t \leq t_a = \frac{v}{a}$,

$$\dot{q}(t_a) = v$$

$$\Rightarrow \dot{q}(t) = \frac{v}{t_a} t = at,$$

$$\ddot{q}(t) = a,$$

$$q(t) = q_0 + \frac{at^2}{2}$$



■ Assuming, motion is possible

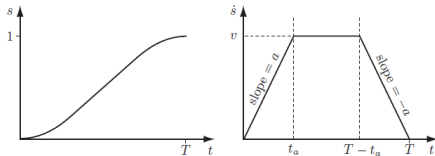
For $t_a \leq t \leq T - t_a$,

$$\ddot{q}(t) = 0,$$

$$\dot{q}(t) = v,$$

$$q(t) = q(t_a) + v(t - t_a)$$

$$\begin{aligned} q(t) &= q_0 + \frac{at_a^2}{2} + v(t - t_a) \\ &= q_0 + vt + \frac{v^2}{2a} - \frac{v^2}{a} \\ &= q_0 + vt - \frac{v^2}{2a} \end{aligned}$$



■ Assuming, motion is possible

For $T - t_a \leq t \leq T$,

$$q(t) = a_0 + a_1 t + a_2 t^2$$

$$\dot{q}(t) = a_1 + 2a_2 t$$

$$\ddot{q}(t) = 2a_2$$

$$\Rightarrow q(t) = q_f - \frac{aT^2}{2} + aTt - \frac{at^2}{2}$$

Constraints

$$\ddot{q}(t) = -a$$

$$\Rightarrow a_2 = -\frac{a}{2}$$

$$\dot{q}(T) = 0$$

$$a_1 + 2a_2 T = 0 \Rightarrow a_1 = aT$$

$$q(T) = q_f$$

$$\Rightarrow a_0 + a_1 T + a_2 T^2 = q_f$$

$$\Rightarrow a_0 = q_f - aT^2 + \frac{aT^2}{2}$$



There is still one more constraint!

$$q_2(T - t_a) = q_3(T - t_a)$$

$$q_0 - \frac{v^2}{2a} + v(T - t_a) = q_f - \frac{aT^2}{2} + aT(T - t_a) - \frac{a(T - t_a)^2}{2}$$

$$q_f - q_0 = \frac{a^2 T^2 - v^2}{2a} + (T - t_a)(v - aT + aT/2 - at_a/2)$$

Substituting $t_a = v/a$,

$$q_f - q_0 = -\frac{v^2 - a^2 T^2}{2a} - \frac{1}{2a}(v - aT)(v - aT)$$

$$q_f - q_0 = -\frac{1}{2a}(v - aT)(v + aT + v - aT) = \frac{v(aT - v)}{a}$$



Only two of v , a , and T can be independently chosen.

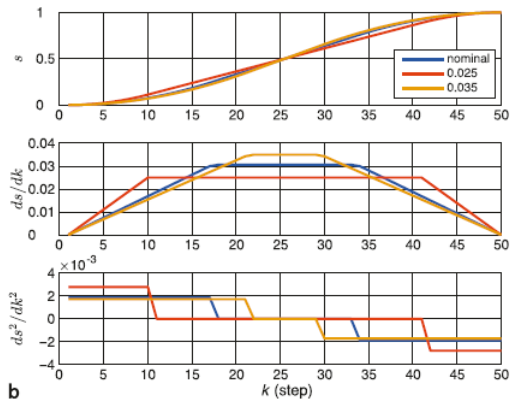
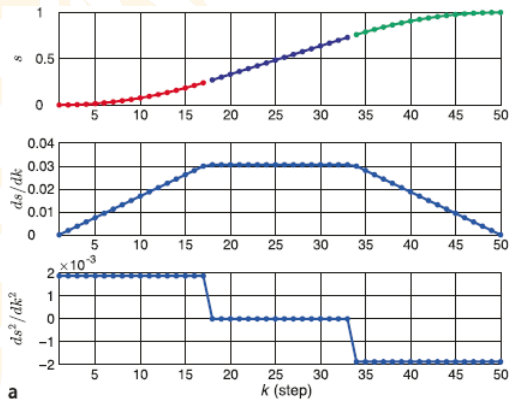
Constraint.

$$q_f - q_0 = \frac{v(aT - v)}{a}$$

$$T = \frac{v}{a} + \frac{q_f - q_0}{\frac{v}{v^2}}$$

$$a = \frac{v^2}{vT - (q_f - q_0)}$$

$$v = \frac{1}{2} \left(aT - \sqrt{a} \sqrt{aT^2 - 4(q_f - q_0)} \right)$$





LSPB – When is motion possible?

- We assumed that

$$0 < t_a \leq \frac{T}{2}$$

- Or, specified velocity and time must satisfy the following relation or motion is not possible:

$$\frac{q_f - q_0}{T} < v \leq \frac{2(q_f - q_0)}{T}.$$

- Or, specified time and acceleration must satisfy the following relation or motion is not possible:

$$4|q_f - q_0| \leq aT^2.$$

- Or, specified acceleration and velocity must satisfy the following relation or motion is not possible:

$$\frac{v^2}{a} \leq (q_f - q_0).$$



LSPB – Choose parameters in one of three ways:

- Choose v and T such that $q_f - q_0 < vT \leq 2(q_f - q_0)$,

$$a = \frac{v^2}{vT - (q_f - q_0)}$$

- Choose v and a such that $\frac{v^2}{a} \leq (q_f - q_0)$,

$$T = \frac{v}{a} + \frac{q_f - q_0}{v}.$$

- Choose a and T such that $4|q_f - q_0| \leq aT^2$,

$$v = \frac{1}{2} \left(aT - \sqrt{a} \sqrt{aT^2 - 4(q_f - q_0)} \right)$$



Minimum-time trajectories or Bang-bang trajectories

- Minimize T , given a .
- Special case of LSPB.
- Keep acceleration at maximum till a suitable switching time, t_s , at which time switch to maximum deceleration.
- $v = \frac{aT}{2}$, and so

$$T = 2\sqrt{\frac{q_f - q_0}{a}}$$



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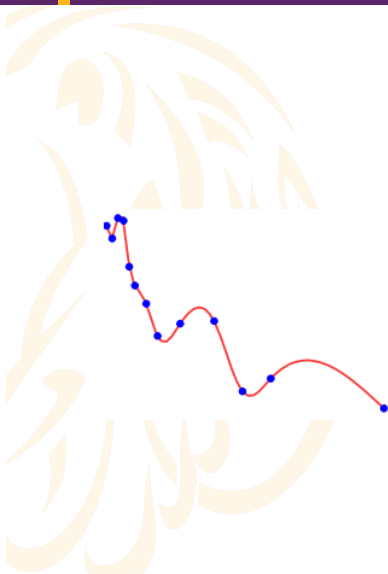
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Sequence of Points/ Via Points

Given: Initial, Final, and some intermediate configurations in joint space.



Fitting a common polynomial



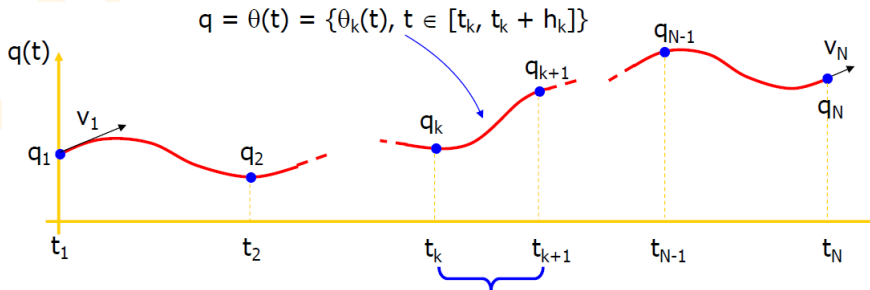
- Trajectory should pass through a sequence of configurations at specified times
- **Position Constraints:** $q(t_0) = q_0$,
 $q(t_1) = q_1, \dots, q(t_{n-1}) = q_{n-1}$
- There could be velocity or acceleration constraints at end points or even intermediate points.
- If there are N constraints in total, choose an $N - 1$ degree polynomial and solve for its coefficients.



Fitting a polynomial through via points

- **Advantage:** The velocity and acceleration are guaranteed to be continuous at intermediate points.
- **Disadvantages:**
 - Oscillatory behavior increases with order of polynomial.
 - Polynomial coefficients depend on all points. So, if one point changes all coefficients are recomputed.
 - Numerical accuracy decreases as order increases.
- **Alternate:** We can build trajectory using low-order polynomials between specified points.

Low-order polynomials between points



- Fit a cubic or quintic polynomial between any two successive via points
- Velocities and accelerations may be specified at intermediate points or not.



Cubic Spline

- Any $q(t)$ segment is:

$$q(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3, \quad t \in [t_k, t_{k+1}]$$

- Four unknowns for each cubic segment.
- $q(t_k)$ and $q(t_{k+1})$ are known.
- Two coefficients left undetermined.
- If $\dot{q}(t_k)$ and $\dot{q}(t_{k+1})$ are also given, then remaining two coefficients can be determined.



Cubic Spline

- Any $q(t)$ segment is:

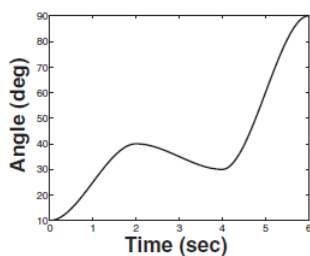
$$q(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3, \quad t \in [t_k, t_{k+1}]$$

- If only $\dot{q}(t_0)$ and $\dot{q}(t_f)$ are given, but via points velocities are not specified
- We can impose continuity constraints:

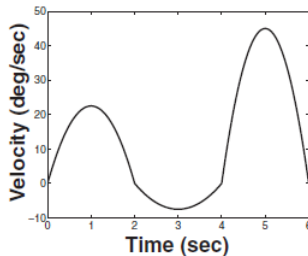
$$\dot{q}_k(t_k) = \dot{q}_{k+1}(t_k)$$

$$\ddot{q}_k(t_k) = \ddot{q}_{k+1}(t_k)$$

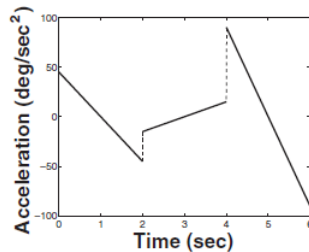
Cubic Spline between 4 via points



(a)



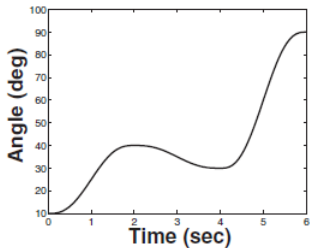
(b)



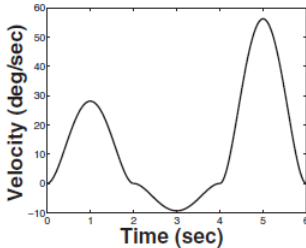
(c)

Figure 7.23: (a) Cubic spline trajectory made from three cubic polynomials. (b) Velocity profile for multiple cubic polynomial trajectory. (c) Acceleration profile for multiple cubic polynomial trajectory.

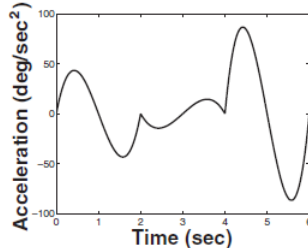
Quintic Spline between 4 via points



(a)



(b)



(c)

Figure 7.24: (a) Trajectory with multiple quintic segments. (b) Velocity profile for multiple quintic segments. (c) Acceleration profile for multiple quintic segments.

Linear segments with parabolic blends

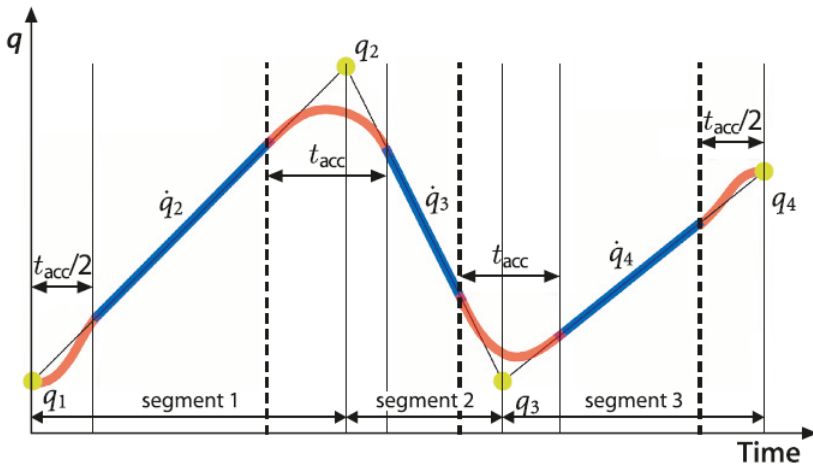




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Joint Space vs Task Space

- The path points could be specified in the joint space, i.e. in terms of joint variables, or in task space (Cartesian space/Operational Space), i.e. in terms of pose (position and orientation of end-effector).



Should you plan in joint space or task space? [1, Section 4.1]

- Trajectory planning can happen in joint space or task space.
 - Trajectory planning in the task space allows for easy accommodation of any path constraints, e.g. obstacles.
 - Trajectory planning in the joint space allows for easy handling of kinematic singularities, redundant dof.



Trajectory Generation in Task Space

- We now have a sequence of poses – position and orientation
- The same techniques (polynomials, LSPB) can be used to interpolate position
- The same techniques can be used to interpolate orientation described in Euler angles form.
- Linear interpolation applied to rotation matrices will result in intermediate matrices that are not necessarily rotation matrices. So, Euler angle representation is used.

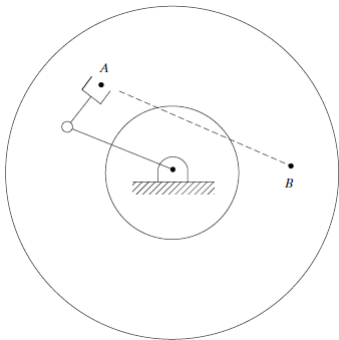


Figure: Intermediate points unreachable. Source: Craig

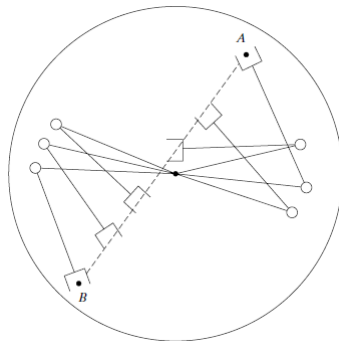


Figure: High joint rates near singularities. Source: Craig

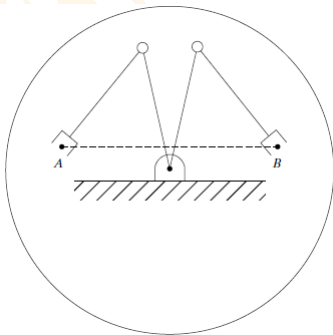
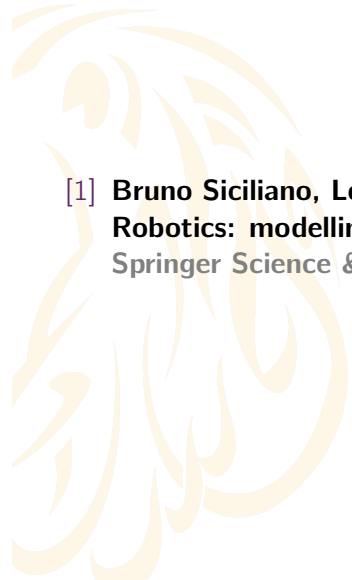


Figure: Start and goal reachable in different solutions.
Source: Craig



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- [1] **Bruno Siciliano, Lorenzo Sciavicco, Luigi Villani, and Giuseppe Oriolo.**
Robotics: modelling, planning and control.
Springer Science & Business Media, 2010.