# Kinematic Singularities

EE366/CE366/CS380: Introduction to Robotics

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1 What are Kinematic Singularities?

2 Finding singularities for 6DOF Manipulators

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#### The Jacobian



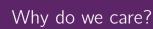
- $\blacksquare$  Jacobian relates joint velocities  $\dot{q}$  to end-effector velocities.  $\xi = (v^T, \omega^T)^T$
- $\xi = J_1 \dot{a}_1 + \cdots + J_n \dot{a}_n$ 
  - End-effector velocities are linear combinations of columns of Jacobian
- For any arbitrary velocity, Jacobian should have 6 linearly independent columns, since  $\xi \in \mathbb{R}^6$
- Rank of the Jacobian matrix depends on q



#### Singular Configurations

#### Definition

Configurations for which rank J(q) is less than its maximum value are called singularities or singular configurations.



- Basit Memon
- At singularities, motion in some directions will not be instantaneously possible.
- At/Near singularities, bounded end-effector velocities may require unbounded/large joint velocities.
- At singularities, bounded joint torques may produce unbounded end-effector forces and torques.
- At singularities, infinite solutions to the inverse kinematic problem may exist.
- Singularities often occur along workspace boundary.



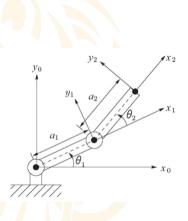
#### How do we determine singularities?



- Find out where the Jacobian loses its rank.
- Solve det J(q) = 0 for q.
- Generally, complicated equations.
- Singularities of analytical Jacobian includes representational singularities as well.



#### Example: Two-links Planar Arm

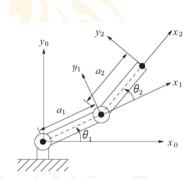


$$J = \begin{bmatrix} -a_1s_1 - a_2s_{12} & -a_2s_{12} \\ a_1c_1 + a_2c_{12} & a_2c_{12} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 1 & 1 \end{bmatrix}$$

- Maximal rank can be 2 here.
- If we consider the first 4 entries, then determinant of  $4 \times 4$  matrix is  $a_1 a_2 s_2$
- Assuming  $a_1, a_2 \neq 0$ , singular for  $\theta_2 = 0, \pi$



#### At singularity, motion in some directions is impossible.



At singularity, we cannot move in direction of  $x_1$ .

$${}^{1}J = {}^{1}R_{0} {}^{0}J$$

$$= \begin{bmatrix} c_{1} & s_{1} \\ -s_{1} & c_{1} \end{bmatrix} \begin{bmatrix} -a_{1}s_{1} - a_{2}s_{12} & -a_{2}s_{12} \\ a_{1}c_{1} + a_{2}c_{12} & a_{2}c_{12} \end{bmatrix}$$

$$= \begin{bmatrix} -a_{2}s_{2} & -a_{2}s_{2} \\ a_{1} + a_{2}c_{2} & a_{2}c_{2} \end{bmatrix}$$

At singularity,

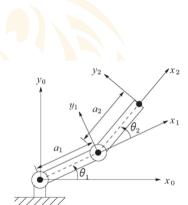
$${}^{1}J = \begin{bmatrix} 0 & 0 \\ a_{1} + a_{2} & a_{2} \end{bmatrix}$$

$$\Rightarrow {}^{1}\delta\dot{x} = 0$$

$${}^{1}\delta\dot{y} = (a_{1} + a_{2})\delta\dot{\theta}_{1} + a_{2}\delta\dot{\theta}_{2}$$



## Large joint velocity may be needed for (small) some end-effector v



$${}^{1}J^{-1} = \frac{1}{a_{1}a_{2}s_{2}} \begin{bmatrix} a_{2}c_{2} & a_{2}s_{2} \\ -a_{1} - a_{2}c_{2} & -a_{2}s_{2} \end{bmatrix}$$

$$\delta \dot{\theta}_1 = \frac{c_2}{a_1 s_2} {}^1 \delta \dot{x} + \frac{1}{a_1} {}^1 \delta \dot{y}$$

$$\delta \dot{\theta}_2 = \frac{-(a_1 + a_2 c_2)}{a_1 a_2 s_2} {}^1 \delta \dot{x} - \frac{1}{a_1} {}^1 \delta \dot{y}$$

- When  $\theta_2$  is close to zero,  $\sin \theta_2 \approx 0$ 
  - $\delta \dot{\theta}_1$  and  $\delta \dot{\theta}_2$  are large even for small  ${}^1\delta \dot{x}$  and  ${}^1\delta \dot{y}$ .



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## Do we really have to solve determinant equations?

- Singular configurations are independent of the choice of base or end frames, or the representation used for Jacobian.
- We can assign frames to make computation of determinant easier for us.
- For arms with spherical wrists, we can decouple the problem into arm singularities and wrist singularities.



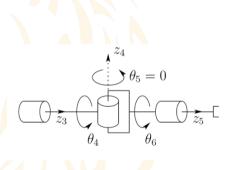
## Decoupling Singularities [1]

- Wrist axes intersect at one point. We can assign frames such that  $o_3 = o_4 = o_5 = o_6 = o$
- $J_O = \begin{bmatrix} 0 & 0 & 0 \\ z_3 & z_4 & z_5 \end{bmatrix}$

- $\blacksquare$  det  $J = \det J_{11} \det J_{22}$
- $\blacksquare$  det  $J_{11} = 0$  gives arm singularities and det  $J_{22} = 0$  gives wrist singularities.
- J in this form will not give you the correct relation between velocities. Only used



## Spherical wrist is singular when $heta_5=$ 0, $\pi$



- Singularity occurs when  $z_3$ ,  $z_4$ , and  $z_5$  are linearly dependent
- This happens when  $z_3$  and  $z_5$  are colinear or  $\theta_5 = 0$ ,  $\pi$
- In general, whenever two revolute joint axes are collinear, a singularity results.



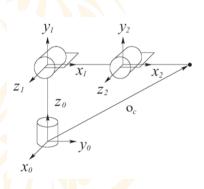
#### Arm Singularities



- Need to compute determinant of  $J_{11}$ , but with  $O_n$  at the wrist center O.
  - $J_{11}$  has ith column  $z_{i-1} \times (o o_{i-1})$  if joint i is revolute and  $z_{i-1}$  if it is prismatic.
- Let's look at specific examples



#### Arm Singularities – Articulated

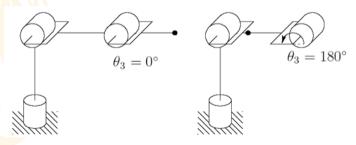


- For indicated frame assignment, det  $J_{11} = a_2 a_3 s_3 (a_2 c_2 + a_3 c_{23})$
- Singular, if
  - $s_3 = 0$  or  $\theta_3 = 0$ ,  $\pi$
  - $a_2c_2 + a_3c_{23} = 0$



#### Arm Singularities – Articulated

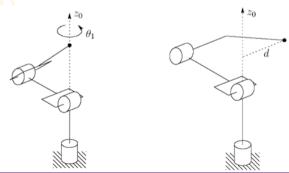
- $s_3 = 0$
- Elbow singularity





### Arm Singularities – Articulated

- $a_2c_2 + a_3c_{23} = 0$
- Shoulder singularity
- Not possible with an offset, but the points become unreachable





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1] Mark W Spong, Seth Hutchinson, and Mathukumalli Vidyasagar.

Robot modeling and control.

John Wiley & Sons, 2020.