

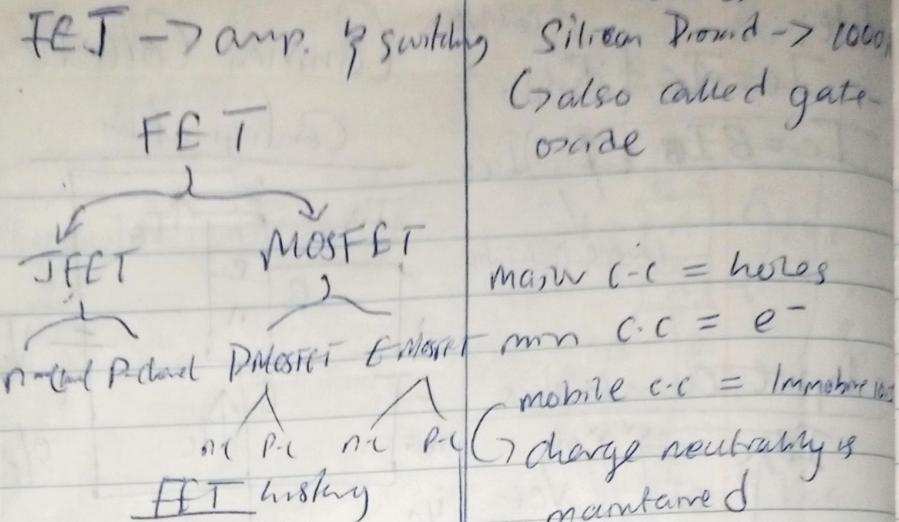
MOSFET

↳ active device
control flow of e⁻

Metal Oxide Semiconductor Field-Effect Transistor

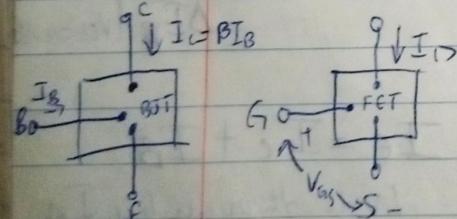
- ch btw D & S n-channel
- 1.) Depletion type < p-channel
 - 2.) Enhancement type < p
- ↳ no channel btw D & S

Construction & Working of Enhancement-Type MOSFET



Field-Effect Transistors

BJT → 3 terminal FET



BJT → current control device

FET → Voltage control device

BJT → bipolar

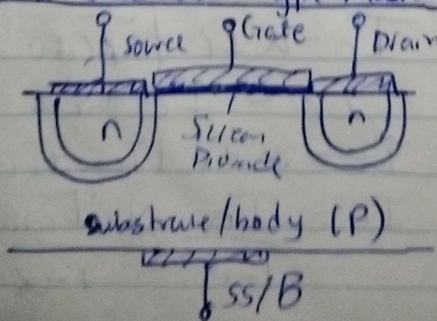
FET → Unipolar (e⁻)

n-channel & p-channel

n-p-n
(e⁻)

p-n-p
(holes)

Construction & Working of Enhancement-Type MOSFET



Inversion =>

$$V_{GS} > 0V \Rightarrow$$

Conductive channel is formed between Source and Drain.

$\Delta V_{GS} \Rightarrow$ width of channel ↑.

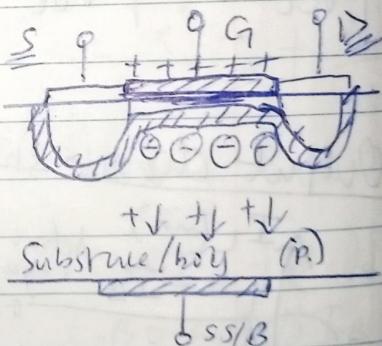
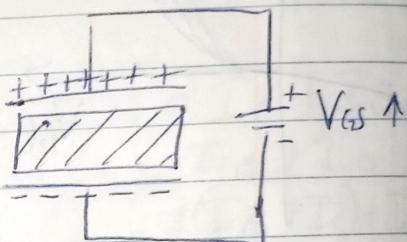
If $V_{GS} >$ particular voltage
→ current flow (I_D)

max C.C = holes

min C.C = e⁻

mobile C.C = immobile

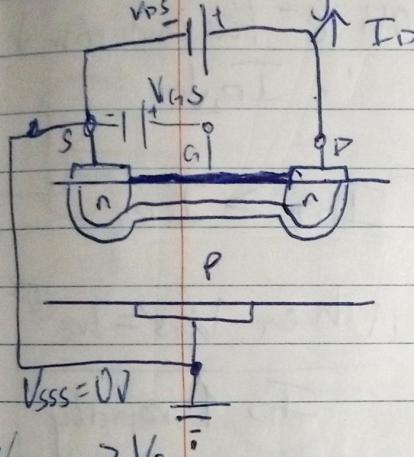
charge neutrality is maintained



Threshold voltage

V_T is the voltage that results in the significant amount of current to flow from source to drain.

$$V_{GS} > V_T \Rightarrow \text{Significant}$$



$$V_{GS} > V_T \Rightarrow \text{Sig } \uparrow I_D$$

$$V_{GD} = V_{GS} - V_{DS}$$

$$\text{Case 1: } V_{DS} = 0$$

$$V_{GD} = V_{GS}$$

uniform
d.s

$$\text{Case 2: } V_{DS} > 0$$

$$V_{GD} \neq V_{GS}$$

not

\rightarrow +ve channel reduces
 V_{DS} on right side

$$\text{Case 3: } V_{DS} = V_{GS} - V_T$$

$$V_{GD} = V_T$$

channel will become extremely narrow on right side (Pinch-OFF)

Dram Characteristics of Enhancement-Type MOSFET

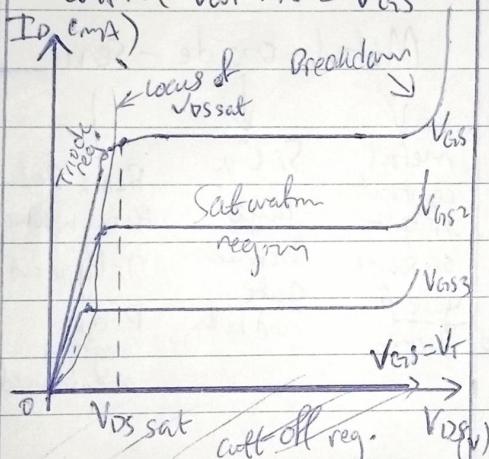
\hookrightarrow Output channel

$$\text{o/p } i = I_D$$

$$\text{o/p } v = V_{DS}$$

i/p voltage

$$\text{Control Variable} = V_{GS}$$



$$\text{Case 1: } V_{GS1} > V_T$$

$$V_{off} = V_{GS1} - V_T$$

$$V_{DSsat} = V_{GS1} - V_T$$

$$I_D = \text{constant (Pinch-off)}$$

$$V_{DS} = 0 \Rightarrow V_D = V_S$$

$$\uparrow V_{DS} \Rightarrow I_D \uparrow$$

$$V_{GD} = V_{GS} - V_{DS}$$

$$V_{DS} = V_{GS} - V_T$$

$$\therefore V_{GD} = V_T$$

$$\text{say } V_{GS} = 2V$$

$$\& V_T = 1V$$

$$V_{DS} = V_{GS} - V_T$$

$$V_{eff} = 2 - 1 = 1V$$

Case II :-

$$V_{GS2} < V_{GS1}$$

$$P_2 < P_1$$

$$R_2 > R_1$$

slope 2 < slope 1

Saturation Region \Rightarrow

region in which I_D is constant

$$\Rightarrow V_{DS} = V_{GS} - V_T$$

$$I_D = k(V_{GS} - V_T)^2$$

↓ constant

$$k = \frac{I_D \text{ cons}}{(V_{GS} - V_T)^2}$$

Triode Region

$$V_{DS} < V_{GS} - V_T$$

$$I_D = 2k(V_{GS} - V_T)V_{DS}$$

$$I_D = 2k[(V_{GS} - V_T)V_{DS} - \frac{V_{DS}^2}{2}]$$

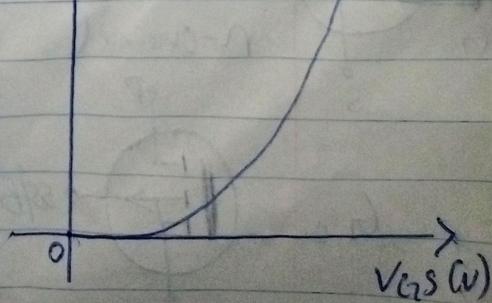
Cut-off Region

$$V_{GS} < V_T$$

$$\therefore I_D = 0A$$

Transfer characteristics

$$I_D(\text{cont})$$



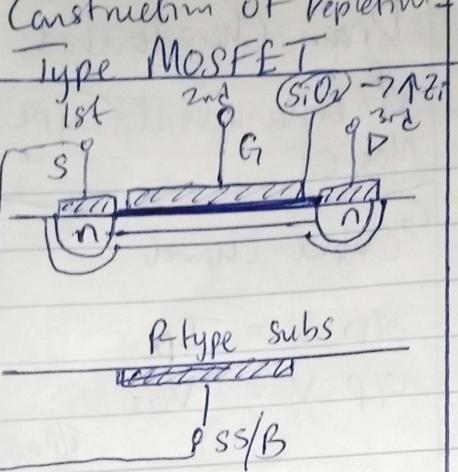
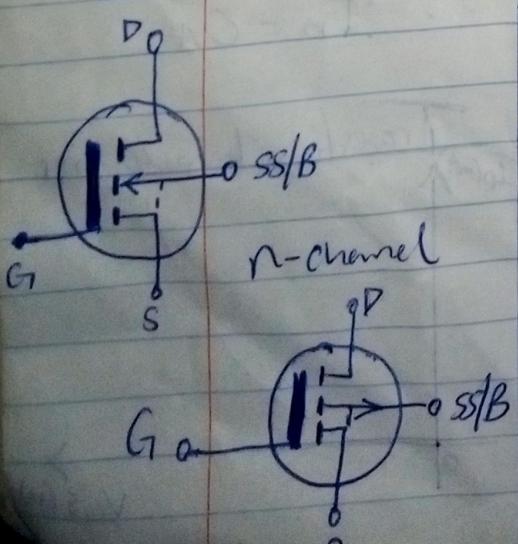
SiO_2 works as an insulator
Due to this the input impedance at the gate terminal is high and no current flows through drain terminal (gate current must be 0 for maximum current)

why drain terminal is insulated from drain, substrate & source.

We use SiO_2 to separate controlling terminal (gate) from the substrate, so that gate current will become zero. As a result, Z_m is higher \Rightarrow gain higher

n-channel \rightarrow
current flows from drain to source.

p-channel \rightarrow
current flows from source to drain.



I_D now becomes constant.
 $I_{DS} \rightarrow$ when $V_{GS} = 0V$

When $V_{GS} = -1V$

$qV_i e^-$ for conduction
 $\therefore I_{D2} \downarrow$

$\therefore I_{D1} > I_{D2}$

When $V_{GS} = 1V$

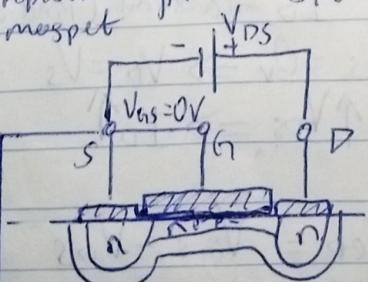
$I_D \uparrow$ rapidly

Metal-Oxide-Semi

metal contact of gate of source gate of drain. \downarrow \downarrow \downarrow
 SiO_2 layer between n-type and p-type regions are diffused
 Base shading through whole

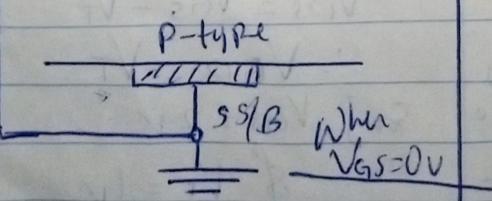
Working of Depletion-type MOSFET

n-channel \approx n-channel Depletion-type MOSFET



Drain & Transfer Characteristics of Depletion-Type MOSFET

Drain characteristics
 $I_D \uparrow$ to V_S V_{DS} or for various V_{GS} (i/p V)

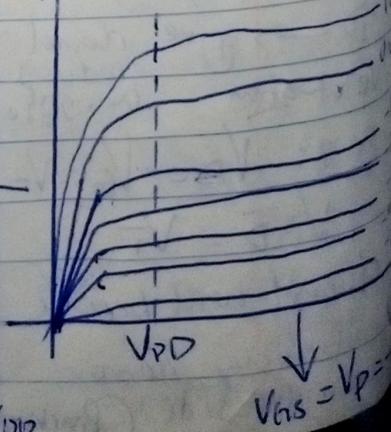


$\uparrow V_{DS} \Rightarrow I_D \uparrow$

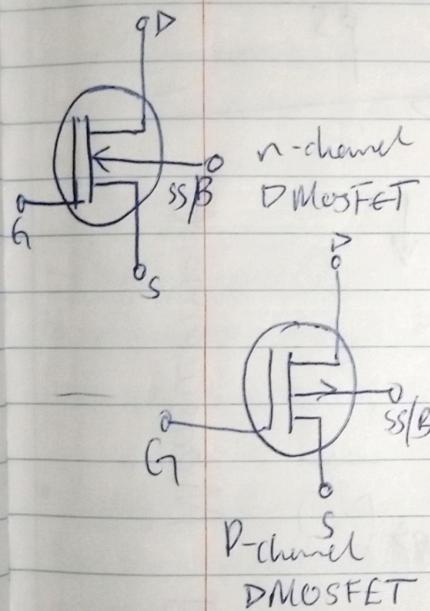
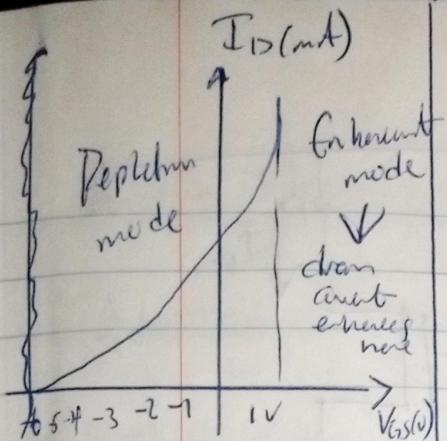
$$V_{DS} = V_D - V_S$$

$$V_D \uparrow \Rightarrow V_D \uparrow$$

$$V_{DS} = V_D - V_S$$



$$V_{GS} = V_P - V_D$$



Same rate
Since
 $C(V_{GS} - c) \rightarrow C(V_{GS} - c)$

Given $k = 0.4 \times 10^{-3} \text{ A/V}^2$
and $I_D(\text{sat}) = 3.5 \text{ mA}$ with
 $V_{GS(\text{sat})} = 4 \text{ V}$, determine V_t .

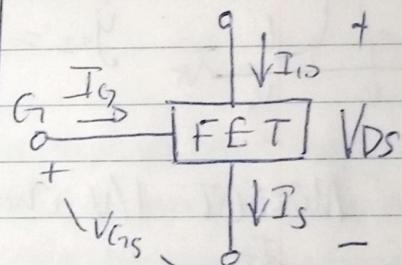
$$k = \frac{I_D}{(V_{GS} - V_t)^2}$$

$$\text{then } V_t = \sqrt{\frac{I_D}{k}} + V_{GS}$$

$$V_t = \sqrt{\frac{3.5 \times 10^{-3}}{0.4 \times 10^{-3}}} + 4 \\ = \sqrt{\frac{35}{4}} + 4 \\ = 1.042 \text{ V}$$

Introduction to FET Biasing

output, input
 $I_D = f(V_{GS})$
Relationship is non-linear



$$I_G \approx 0 \text{ A}$$

$$\therefore I_D = I_S$$

Example
1) Does the current of an enhancement-type MOSFET increase at the same rate as a depletion-type MOSFET for the conduction region?

$$I_D = k(V_{GS} - V_t)^2$$

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$$

Pinch off voltage

$$\frac{dI_D}{dV_{GS}} = 2k(V_{GS} - V_t)$$

$$\frac{dI_D}{dV_{GS}} = \frac{2I_{DSS}(V_t - V_p)}{V_p^2}$$

D MOSFET
3.) Given $I_D = 4 \text{ mA}$ at $V_{GS} = -2 \text{ V}$, determine the saturation current I_S
 $V_p = -4 \text{ V}$

$$I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$$

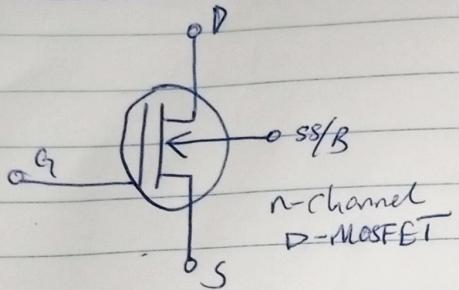
$$I_{DSS} = \frac{I_D}{\left(1 - \frac{V_{GS}}{V_p}\right)^2}$$

$$= \frac{4 \times 10^{-3}}{\left(1 - \left(-\frac{2}{4}\right)\right)^2}$$

JFET $\xrightarrow{\sim}$ DMOSFET
 $I_D = I_{DSS} \left(1 - \frac{V_{GS}}{V_p}\right)^2$
Shockley's equation

FET
 $I_D = k(V_{GS} - V_t)^2$

Introduction to Depletion-Type MOSFET Biasing



Operating point

$$Q\text{-pt} \equiv (V_{GSQ}, I_{DQ})$$

→ Transfer char. & load line plot to get Q-point

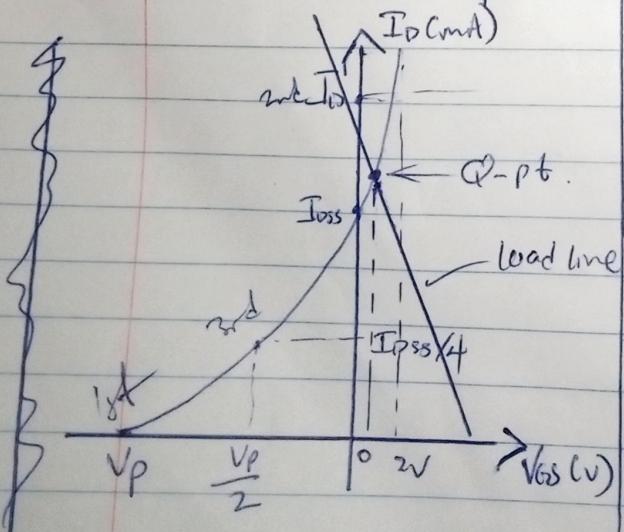
$$V_{GS} < 0$$

$$V_{GS} = 0$$

$$V_{GS} > 0$$

$$I_{DS} \times \text{max.}$$

$$Q\text{-pt} \rightarrow \Theta^{\text{ve}} \text{ or zero or positive}$$



$$V_{GSQ} \rightarrow \Theta^{\text{ve}}$$

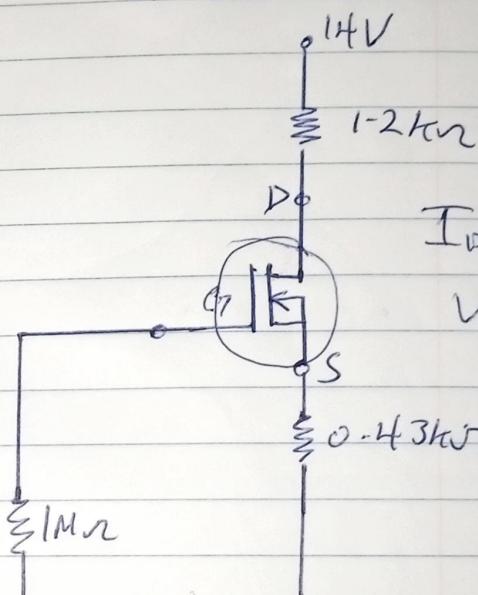
$$I_{DQ} \rightarrow \Theta^{\text{ve}}$$

Self-Bias Configuration of Depletion-Type MOSFET

Problem: For the self-bias configuration determine

$$a) I_{DSQ} \text{ and } V_{GSQ}$$

$$b) V_{DS} \text{ and } V_D$$



$$I_{DSQ} = 6 \text{ mA}$$

$$V_P = -4V$$

For biasing
To plot graph points characteris.

Case 1 when $I_D = 0$

$$0 = I_{DS} \left(1 - \frac{V_{GS}}{V_P} \right)^2$$

$$\Rightarrow V_{GS} = V_P = -4V$$

Case 2 when $V_{GS} = 0$:

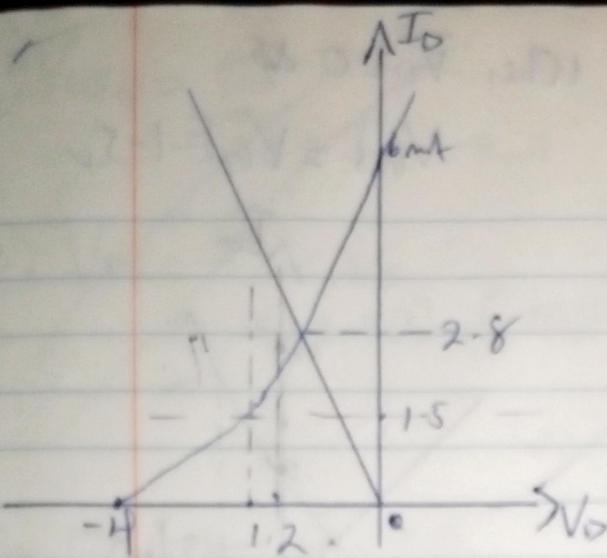
$$I_D = I_{DS} \left(1 - 0 \right)^2$$

$$= I_{DSQ} = 6 \text{ mA}$$

Case 3 when $V_{GS} = \frac{V_P}{2}$

$$I_D = I_{DS} \left(1 - \frac{V_P}{2V_P} \right)^2$$

$$I_D = \frac{6}{4} = 1.5 \text{ mA}$$



For load line:

$$V_G - V_{GS} - I_S R_S = 0$$

$$I_S = I_D$$

$$V_G = 0$$

$$\therefore 0 - V_{GS} - I_D (0.43) = 0$$

$$V_{GS} = - 0.43 I_D$$

$$V_{GS} = - R_S I_D$$

$$1. I_{DD} = 2.8 \text{ mA}$$

$$V_{GS} = 1.2 \text{ V}$$

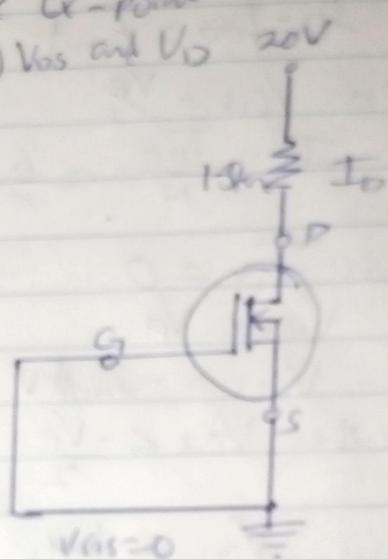
b.) V_{DS} and V_D

$$\begin{aligned} V_D &= 14 - I_D R_D \\ &= 14 - (2.8 \text{ mA})(1.2 \text{ k}\Omega) \\ &= 10.64 \text{ V} \end{aligned}$$

$$\begin{aligned} V_{DS} &= V_D - V_S \\ &= 10.64 - I_S R_S \\ &= 10.64 - (2.8 \times 0.43) \\ &= 9.4436 \text{ V} \end{aligned}$$

Special Case

- a) For the network shown, determine the Q-point.
- b) V_{GS} and V_D 20 V



$$V_{GS} = 0 \text{ V}$$

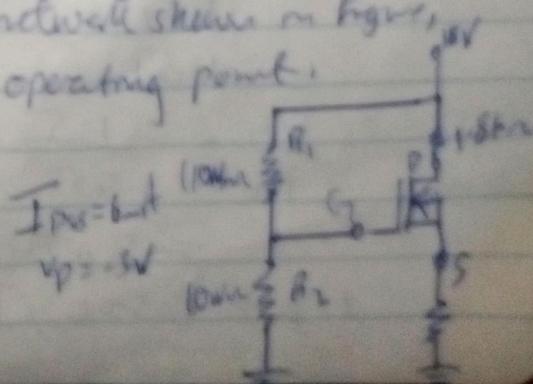
$$\sqrt{I_{DD}} = I_{DS} = 10 \text{ mA}$$

$$\begin{aligned} b.) \quad V_D &= 20 - (1.5)(10) \\ &= 5 \text{ V} \end{aligned}$$

$$\begin{aligned} V_{DS} &= V_D - V_S \\ &= V_D - 0 \\ &= V_D = 5 \text{ V} \end{aligned}$$

Voltage-Divider Biasing of depletion-type MOSFET

For the network shown in figure, determine operating point.



For transfer curve;

Case 1; when $V_{GS} = 0$;

$$I_D = I_{DQ} = 6 \text{ mA}$$

Case 2; when $V_{GS} > \frac{V_P}{2}$

$$I_D = \frac{I_{DQ}}{H} = \frac{6}{10} = 0.6 \text{ mA}$$

Case 3; when $I_D = 0$

$$V_{GS} = V_P$$

$$V_{GS} = -3 \text{ mA} \times V$$

Case 4; when $V_{GS} < -\frac{V_P}{2}$

say $V_{GS} = 1 \text{ mA}$
 $\star I_D = 10.67 \text{ mA}$

For load line;

$$V_{GS} = V_G - V_S$$

$$V_{GS} = V_G - I_D R_S$$

$$I_D = -\frac{V_{GS}}{R_S} + \frac{V_G}{R_S}$$

To get Intercept $\frac{V_G}{R_S}$,

$$V_{GS} = \frac{R_2}{R_1 + R_2} V_{PD}$$

$$V_{PD} = 20 \text{ V}$$

$$V_{GS} = \left(\frac{10}{110 + 10} \right) 18 = 1.5 \text{ V}$$

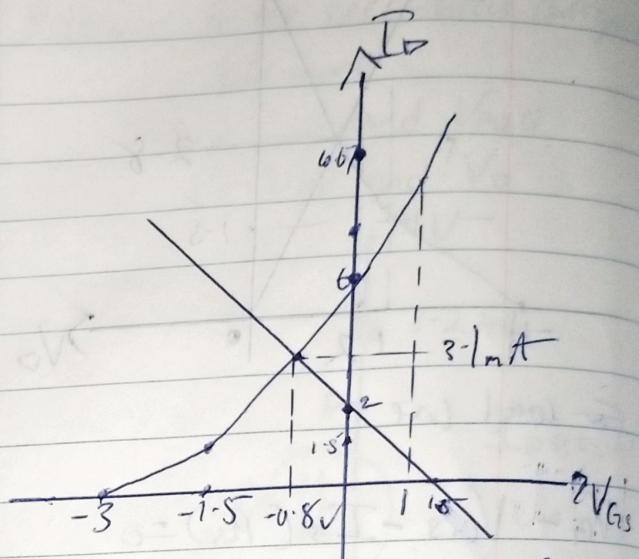
$$\therefore \frac{V_G}{R_S} = \frac{1.5}{250}$$

$$= 2 \text{ mA}$$

∴ When $V_{GS} = 0$, $I_D = 2 \text{ mA}$

When $I_D = 0$

$$V_{GS} = V_G = 1.5 \text{ V}$$

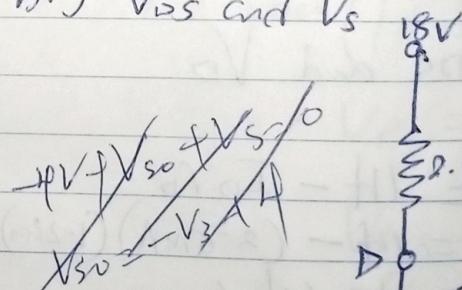


∴ Operating point is at $(0.8 \text{ V}, 3.1 \text{ mA})$

Class Activities

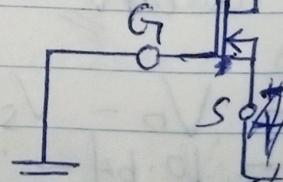
For the network shown in figure,
determine

- I_{DSQ} and V_{GSQ}
- V_{DS} and V_S



$$I_{DSQ} = 8 \text{ mA}$$

$$V_P = -8 \text{ V}$$



$$-V_S - 0.39 R_S + 4 V = 0$$

$$V_{DSQ} = -V_S + 4 \text{ V}$$

$$1) V_{GSQ} = 0V$$

~~V_{GS}~~

$$\therefore I_{DQ} = I_{DSS} = 8mA$$

$$2) V_{DS} = V_D - V_S$$

$$= 18 - 2 \cdot 2(8) - (0.39(8) + 4)$$

$$=$$

Case 1 : when $V_{GS} = 0$

$$I_D = 8mA$$

Case 2 : when $I_{DQ} = 0$

$$V_{GS} = V_P = -8V$$

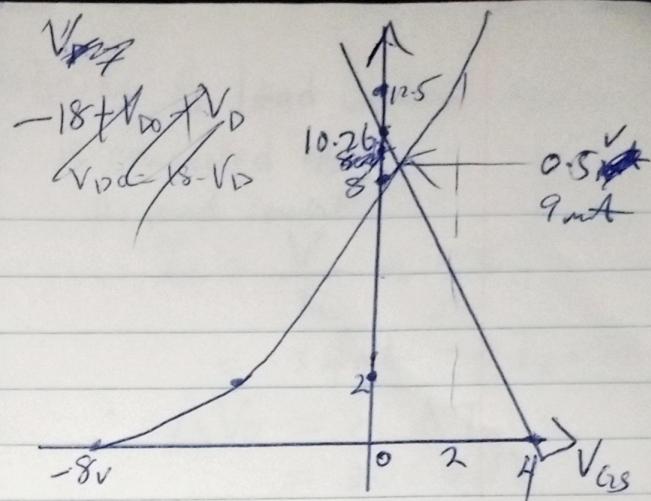
Case 3 : when $V_{GS} = \frac{V_P}{2} = -4V$

$$V_{DS} \quad I_D = \frac{8}{14} = 2mA$$

Case 4 : when $V_{GS} < -\frac{V_P}{2}$

$$\text{say } V_{GS} = 2V$$

$$\therefore I_D = 12.5mA$$



$$\therefore V_{GSQ} = 0.5V; I_{DQ} = 9mA$$

$$V_{GS}$$

$$V_S = 0.39(9) \bar{A} 4$$

$$= 0.351 - 4 = -0.169V$$

$$V_{DS} = V_D - V_S$$

$$= 18 - 0.169 + 0.49$$

$$= \underline{-1.31V}$$

For load line ;

$$V_{DS} = V_D + V_S -$$

$$V_{GS} = V_G - V_S + 4$$

$$V_G = 0$$

$$V_{GS} + V_S = 4$$

$$V_{GS} \neq I_D R_S = 2V$$

$$I_D = -\frac{V_{GS}}{R_S} + \frac{4}{R_S}$$

$$\text{Inferent at } \frac{4}{R_S} \Rightarrow \frac{4}{0.39} \\ \text{when } V_{GS} = 0 \quad = 10.26mA$$

$$\text{at when } I_D = 0; V_{GS} = 4$$

Introduction to Enhancement-Type MOSFET Biasing

eMOSFET (4 points)

$$I_D = k(V_{GS} - V_T)^2$$

$$V_{GS(\text{on})} \geq I_D(\text{on}) - V_T$$

$$P_1 \equiv (V_T, 0A)$$

$$P_2 \equiv (V_{GS(\text{on})}, I_{D(\text{on})})$$

$$P_3 \equiv (V_{GS1}, I_{D1}) \quad V_T < V_{GS1} < V_{GS2}$$

$$P_4 \equiv (V_{GS2}, I_{D2}) \quad \hookrightarrow V_{GS2} > V_{GS(\text{on})}$$

