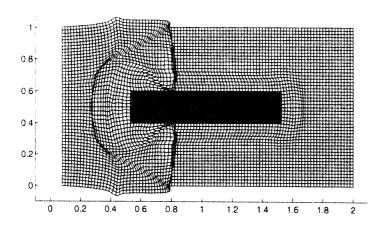
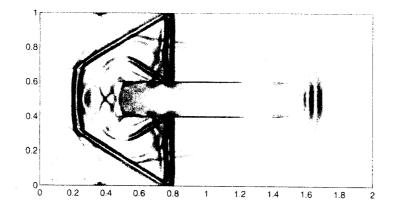
#### Finite Volume Methods for Hyperbolic Problems





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## High-Resolution Methods

In Chapter 4 we developed the basic ideas of Godunov's method, an upwind finite volume method for hyperbolic systems, in the context of constant-coefficient linear systems. Godunov's method is only first-order accurate and introduces a great deal of numerical diffusion, yielding poor accuracy and smeared results, as can be seen in Figure 6.1(a), for example. In this chapter we will see how this method can be greatly improved by introducing correction terms into (4.43), to obtain a method of the form

$$Q_i^{n+1} = Q_i - \frac{\Delta I}{\Delta x} (A^+ \Delta Q_{i-1/2} + A^- \Delta Q_{i+1/2}) - \frac{\Delta I}{\Delta x} (\bar{F}_{i+1/2} - \bar{F}_{i-1/2}). \quad (6.1)$$

The fluxes  $\vec{F}_{i-1/2}$  are based on the waves resulting from the Riemann solution, which have already been computed in the process of determining the fluctuations  $\mathcal{A}^{\pm}\Delta Q_{i-1/2}$ . The basic form of these correction terms is motivated by the Lax-Wendroff method, a standard second-order accurate method described in the next section. The addition of crucial limiters leads to great improvement, as discussed later in this chapter.

## 6.1 The Lax-Wendroff Method

The Lax-Wendroff method for the linear system  $q_t + Aq_x = 0$  is based on the Taylor series expansion

$$q(x, t_{n+1}) = q(x, t_n) + \Delta t \, q_t(x, t_n) + \frac{1}{2} (\Delta t)^2 q_{tt}(x, t_n) + \cdots$$
 (6.2)

From the differential equation we have that  $q_i = -Aq_i$ , and differentiating this gives

$$q_{tt} = -Aq_{xt} = A^2q_{xx},$$

where we have used  $q_{xt} = q_{tx} = (-Aq_x)_x$ . Using these expressions for  $q_t$  and  $q_{tt}$  in (6.2)

$$q(x,t_{n+1}) = q(x,t_n) - \Delta t A q_x(x,t_n) + \frac{1}{2} (\Delta t)^2 A^2 q_{xx}(x,t_n) + \cdots$$
 (6.3)

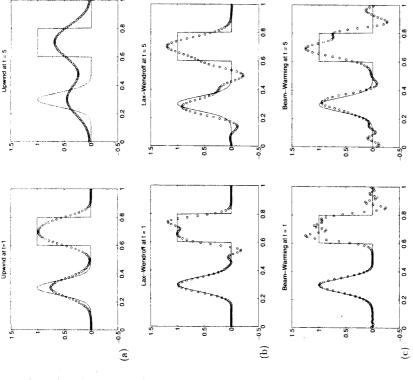


Fig. 6.1. Tests on the advection equation with different linear methods. Results at time t=1 and t=5 are shown, corresponding to 1 and 5 revolutions through the domain in which the equation  $q_t + q_t = 0$  is solved with periodic boundary conditions: (a) upwind, (b) Lax–Wendroff, (c) Beam–Warming. [claw/book/chap6/compareadv]

Keeping only the first three terms on the right-hand side and replacing the spatial derivatives by central finite difference approximations gives the Lax-Wendruff method.

$$Q_i^{n+1} = Q_i^n - \frac{\Delta t}{2\Delta x} A(Q_{i+1}^n - Q_{i-1}^n) + \frac{1}{2} \left(\frac{\Delta t}{\Delta x}\right)^2 A^2(Q_{i-1}^n - 2Q_i^n + Q_{i+1}^n). \quad (6.4)$$

By matching three terms in the Taylor series and using centered approximations, we obtain a second-order accurate method.

This derivation of the method is based on a finite difference interpretation, with  $Q_i^n$  approximating the pointwise value  $q(x_i, t_n)$ . However, we can reinterpret (6.4) as a finite

volume method of the form (4.4) with the flux function

$$F_{i+1,2}^{n} = \frac{1}{2} A(Q_{i-1}^{n} + Q_{i}^{n}) - \frac{1}{2} \frac{\Delta r}{\Delta x} A^{2}(Q_{i}^{n} - Q_{i-1}^{n}).$$
 (6.5)

Note that this looks like the unstable averaged flux (4.18) plus a diffusive flux, but that the the true solution contains a diffusive  $q_{xx}$  term that is missing from the numerical method diffusion chosen exactly matches what appears in the Taylor series expansion (6.3). Indeed, this shows why the averaged flux (4.18) alone is unstable - the Taylor series expansion for when the unstable flux is used.

shows numerical solutions to the scalar advection equation  $q_t + q_v = 0$ , which is solved on the unit interval up to time t = 1 with periodic boundary conditions. Hence the solution should agree with the initial data, translated back to the initial location. The data, shown as a solid line in each plot, consists of both a smooth pulse and a square-wave pulse. Figure 6.1(a) To compare the typical behavior of the upwind and Lax-Wendroff methods. Figure 6.1 shows the results when the upwind method is used. Excessive dissipation of the solution is evident. Figure 6.1(b) shows the results when the Lax-Wendroff method is used instead. The smooth pulse is captured much better, but the square wave gives rise to an oscillatory solution. This can be explained in terms of the Taylor series expansion (6.2) as follows. By matching the first three terms in the series expansion, the dominant error is given by the next term,  $q_{ttt} = -A^3 q_{txt}$ . This is a dispersive term, which leads to oscillations, as explained in more detail in Section 8.6 where modified equations are discussed. In this chapter we will see a different explanation of these oscillations, along with a cure based on

In each of these figures the results were computed using a Courant number  $\Delta t/\Delta x=0.8$ . Each method works best when the Courant number is close to 1 (and in fact is exact if the Courant number is exactly 1 for this simple problem) and less well for smaller values of Choosing different values gives somewhat different results, though the same basic behavior.  $\Delta t/\Delta x$ . The reader is encouraged to experiment with the CLAWPACK codes in the directories referenced in the figures.

## 6.2 The Beam-Warming Method

The Lax-Wendroff method (6.4) is a centered three-point method. If we have a system for then we might think it is preferable to use a one-sided formula. In place of the centered which all the eigenvalues of A are positive (e.g.. the scalar advection equation with  $ar{u}>0$ ), formula for  $q_{\lambda}$  and  $q_{xx}$ , we might use

$$q_{x}(x_{i},t_{n}) = \frac{1}{2\Delta x} [3q(x_{i},t_{n}) - 4q(x_{i-1},t_{n}) + q(x_{i-2},t_{n})] + \mathcal{O}(\Delta x^{2}),$$

$$q_{xx}(x_{i},t_{n}) = \frac{1}{(\Delta x)^{2}} [q(x_{i},t_{n}) - 2q(x_{i-1},t_{n}) + q(x_{i-2},t_{n})] + \mathcal{O}(\Delta x).$$
(6.6)

Using these in (6.3) gives a method that is again second-order accurate,

$$Q_i^{n+1} = Q_i^n - \frac{\Delta t}{2\Delta x} A(3Q_i^n - 4Q_i^n + Q_{i-2}^n) + \frac{1}{2} \left(\frac{\Delta t}{\Delta x}\right)^2 A^2 (Q_i^n - 2Q_{i-1}^n + Q_{i-2}^n).$$

This is known as the Beam-Warming method. and was originally introduced in [481]. It can he written as a flux-differencing finite volume method with

6.3 Preview of Limiters

$$F_{i-1,2}^n = AQ_{i-1}^n + \frac{1}{2}A\left(1 - \frac{\Delta I}{\Delta X}A\right)(Q_{i-1}^n - Q_{i-2}^n).$$
 (6.8)

Figure 6.1(c) shows the results of the previous advection test using the Beam-Warming method. The behavior is similar to that of the Lax-Wendroff method in that oscillations appear, though the oscillations are now ahead of the discontinuities rather than behind,

#### 6.3 Preview of Limiters

better accuracy on smooth solutions than the upwind method, as seen in Figure 6.1, but fail near discontinuities, where oscillations are generated. In fact, even when the solution is smooth, oscillations may appear due to the dispersive nature of these methods, as evident Second-order accurate methods such as the Lax-Wendroff or Beam-Warming give much in Figure 6.1. Upwind methods have the advantage of keeping the solution monotonically varying in regions where the solution should be monotone, even though the accuracy is not very good. The idea with high-resolution methods is to combine the best features of both methods. Second-order accuracy is obtained where possible, but we don't insist on it in regions where the solution is not behaving smoothly (and the Taylor series expansion is not even valid). With this approach we can achieve results like those shown in Figure 6.2.

The dispersive nature of the Lax-Wendroff method also causes a slight shift in the at the later time t = 5. Another advantage of using limiters is that this phase error can data consists of a wave packet, a high-frequency signal modulated by a Gaussian. With a location of the smooth hump, a phase error, that is visible in Figure 6.1, particularly be essentially eliminated. Figure 6.3 shows a computational example where the initial dispersive method such a packet will typically propagate at an incorrect speed corresponding to the numerical group velocity of the method. The Lax-Wendroff method is clearly quite dispersive. The high-resolution method shown in Figure 6.3(c) performs much better. There is some dissipation of the wave, but much less than with the upwind method. The main goal of this chapter is to develop the class of high-resolution methods used to obtain these results.

 $F_{i-1/2}^n = \left(A^-Q_i^n + A^+Q_{i-1}^n\right) + \frac{1}{2}|A|\left(I - \frac{\Delta I}{\Delta x}|A|\right)\left(Q_i^n - Q_{i-1}^n\right).$ 

A hint of how this can be done is seen by rewriting the Lax-Wendroff flux (6.5) as

flux (4.56) with a correction term. Using this in the flux-differencing method (4.4) gives a using the notation  $A^-$ ,  $A^+$ , |A| defined in Section 4.12. This now has the form of the upwind since it depends on  $Q_i' - Q_{i-1}'$  and has the form of (4.10), but the coefficient is positive method of the form (6.1). Note that the correction term in (6.9) looks like a diffusive flux, if the CFL condition is satisfied. Hence it corresponds to an antidiffusive flux that has the effect of sharpening up the overly diffusive upwind approximation.

changes the magnitude of the correction actually used, depending on how the solution is behaving. The limiting process is complicated by the fact that the solution to a hyperbolic The idea is now to modify the final term in (6.9) by applying some form of limiter that system typically consists of a superposition of waves in several different families. At a given 6.3 Preview of Limiters

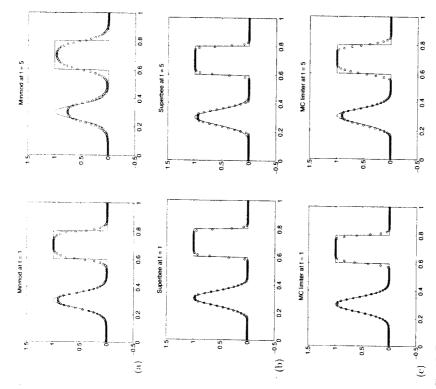


Fig. 6.2. Tests on the advection equation with different high-resolution methods, as in Figure 6.1; (a) minmod limiter, (b) superbee limiter, (c) MC limiter. [claw/book/chap6/compareadv]

point and time, some of the waves passing by may be smooth while others are discontinuous. Ideally we would like to apply the limiters in such a way that the discontinuous portion of the solution remains nonoscillatory while the smooth portion remains accurate. To do so we must use the characteristic structure of the solution. We will see that this is easily accomplished once we have solved the Riemann problem necessary to implement the upwind Godunov method. The second-order correction terms can be computed based on the waves arising in that Riemann solution, with each wave limited independently from the others. This process is fully described later in this chapter.

More generally, one can consider combining any low-order flux formula  $\mathcal{F}_L(Q_{i-1},Q_i)$ (such as the upwind flux) and any higher-order formula  $\mathcal{F}_H(Q_{i-1},Q_i)$  (such as the

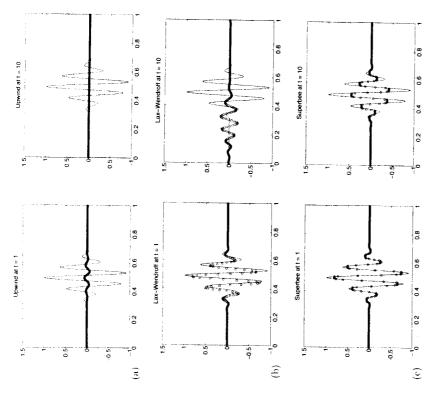


Fig. 6.3. Tests on the advection equation with different methods on a wave packet. Results at time t = 1and t=10 are shown, corresponding to 1 and 10 revolutions through the domain in which the equation  $q_t+q_t=0$  is solved with periodic boundary conditions. [claw/book/chap6/wavepacket]

Lax-Wendroff) to obtain a flux-limiter method with

$$F_{i-1/2}^{"} = \mathcal{F}_{L}(Q_{i-1}, Q_{i}) + \Phi_{i'-1/2}^{"} \{\mathcal{F}_{H}(Q_{i-1}, Q_{i}) - \mathcal{F}_{L}(Q_{i-1}, Q_{i})\}.$$
(6.10)

If  $\Phi_{i-1/2}^n=0$ , then this reduces to the low-order method, while if  $\Phi_{i-1/2}^n=1$ , we obtain the high-order method. This idea of applying limiters to improve the behavior of high-order methods appeared in the early 1970s in the hybrid method of Harten and Zwas [190] and A wide variety of other methods of this form have since been developed, along with better the flux-corrected transport (FCT) method of Boris and Book [38] (see also [348], [496]).

theoretical techniques to analyze them. In this chapter we combine many of these ideas to develop a class of methods that is relatively easy to extend to harder problems.

In the next section we start by giving a geometric interpretation for the scalar advection equation, leading to *slope-limiter* methods of the type pioneered in van Leer's work [464]–[468]. For the scalar advection equation there are many ways to interpret the same method, and it is illuminating to explore these. In particular we will see how this relates to flux-limiter methods of the type studied by Sweby [429], who used the algebraic total variation diminishing (TVD) conditions of Harten [179] to derive conditions that limiter functions should satisfy for more general nonlinear conservation laws. We will, however, ultimately use a different approach to apply these limiters to nonlinear problems, closer to the geometric approach in Goodman & LeVeque [160]. This can be interpreted as applying the limiter functions to the waves resulting from the Riemann solution. Extending this to linear systems of equations gives the algorithm introduced in Section 6.13. The method is then easily generalized to nonlinear systems, as described briefly in Section 6.15 and more fully in Chapter 15. Multidimensional versions are discussed in Chapters 19 through 23.

# 6.4 The REA Algorithm with Piecewise Linear Reconstruction

Recall the reconstruct–evolve–average (REA) Algorithm 4.1 introduced in Section 4.10. For the scalar advection equation we derived the upwind method by reconstructing a piecewise constant function  $\tilde{q}''(x,t_n)$  from the cell averages  $Q_i^r$ , solving the advection equation with this data, and averaging the result at time  $t_{n+1}$  over each grid cell to obtain  $Q_i^{n+1}$ . To achieve better than first-order accuracy, we must use a better reconstruction than a piecewise constant function. From the cell averages  $Q_i^r$  we can construct a piecewise linear function of the form

$$\tilde{q}^{n}(x, t_{n}) = Q_{i}^{n} + \sigma_{i}^{n}(x - x_{i})$$
 for  $x_{i-1/2} \le x < x_{i+1/2}$ . (6.11)

where

$$x_i = \frac{1}{2} \left( x_{i-1/2} + x_{i+1/2} \right) = x_{i-1/2} + \frac{1}{2} \Delta x \tag{6.12}$$

is the center of the *i*th grid cell and  $\sigma_i^n$  is the slope on the *i*th cell. The linear function (6.11) on the *i*th cell is defined in such a way that its value at the cell center  $x_i$  is  $Q_i^n$ . More importantly, the average value of  $\bar{q}^n(x,t_n)$  over cell  $C_i$  is  $Q_i^n$  (regardless of the slope  $\sigma_i^n$ ), so that the reconstructed function has the cell average  $Q_i^n$ . This is crucial in developing conservative methods for conservation laws. Note that steps 2 and 3 are conservative in general, and so Algorithm 4.1 is conservative provided we use a *conservative reconstruction* in step 1, as we have in (6.11). Later we will see how to write such methods in the standard conservation

For the scalar advection equation  $q_t + i\bar{t}q_x = 0$ , we can easily solve the equation with this data, and compute the new cell averages as required in step 3 of Algorithm 4.1. We have

$$\tilde{q}^n(x,t_{n+1}) = \tilde{q}^n(x - \tilde{u} \Delta t, t_n).$$

Until further notice we will assume that  $\bar{u} > 0$  and present the formulas for this particular case. The corresponding formulas for  $\bar{u} < 0$  should be easy to derive, and in Section 6.10 we will see a better way to formulate the methods in the general case.

6.5 Choice of Stopes

Suppose also that  $|\vec{n} \Delta x/\Delta x| \le 1$ , as is required by the CFL condition. Then it is straightforward to compute that

$$Q_{i}^{n+1} = \frac{\bar{u} \Delta I}{\Delta x} \left( Q_{i-1}^n + \frac{1}{2} (\Delta x - \bar{u} \Delta I) \sigma_{i-1}^n \right) + \left( 1 - \frac{\bar{u} \Delta I}{\Delta x} \right) \left( Q_i^n - \frac{1}{2} \bar{u} \Delta I \sigma_i^n \right)$$

$$= Q_i^n - \frac{\bar{u} \Delta I}{\Delta x} \left( Q_i^n - Q_{i-1}^n \right) - \frac{1}{2} \frac{\bar{u} \Delta I}{\Delta x} \left( \Delta x - \bar{u} \Delta I \right) \left( \sigma_i^n - \sigma_{i-1}^n \right). \tag{6.13}$$

Again note that this is the upwind method with a correction term that depends on the slopes.

#### 6.5 Choice of Slopes

Choosing slopes  $\sigma_i^n \equiv 0$  gives Godunov's method (the upwind method for the advection equation), since the final term in (6.13) drops out. To obtain a second-order accurate method we want to choose nonzero slopes in such a way that  $\sigma_i^n$  approximates the derivative  $q_i$  over the ith grid cell. Three obvious possibilities are

Centered slope: 
$$\sigma_i^n = \frac{Q_{i+1}^n - Q_{i-1}^n}{2 \Delta x}$$
 (Fromm), (6.14)

Upwind slope: 
$$\sigma_i^n = \frac{Q_i^n - Q_{i-1}^n}{\Delta x}$$
 (Beam–Warming), (6.15)

Downwind slope: 
$$\sigma_i^n = \frac{Q_{i+1}^n - Q_i^n}{\Delta x}$$
 (Lax-Wendroff). (6.16)

The centered slope might seem like the most natural choice to obtain second-order accuracy, but in fact all three choices give the same formal order of accuracy, and it is the other two choices that give methods we have already derived using the Taylor series expansion. Only the downwind slope results in a centered three-point method, and this choice gives the Lax—Wendroff method. The upwind slope gives a fully-upwinded 3-point method, which is simply the Beam—Warming method.

The centered slope (6.14) may seem the most symmetric choice at first glance, but because the reconstructed function is then advected in the positive direction, the final updating formula turns out to be a nonsymmetric four-point formula,

$$Q_i^{n+1} = Q_i^n - \frac{\vec{u}}{4} \frac{\Delta t}{\Delta x} (Q_{i+1}^n + 3Q_i^n - 5Q_{i-1}^n + Q_{i-2}^n)$$

$$- \frac{\vec{u}^2 \Delta t^2}{4 \Delta x^2} (Q_{i+1}^n - Q_i^n - Q_{i-1}^n + Q_{i-2}^n). \tag{6.17}$$

This method is known as Fromm's method.

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#### 6.6 Oscillations

Warming (and also Fromm's method) give oscillatory approximations to discontinuous As we have seen in Figure 6.1, second-order methods such as the Lax--Wendroff or Beamsolutions. This can be easily understood using the interpretation of Algorithm 4.1.

Consider the Lax-Wendroff method, for example, applied to piecewise constant data

$$Q_i^n = \begin{cases} 1 & \text{if } i \le J, \\ 0 & \text{if } i > J. \end{cases}$$

Choosing slopes in each grid cell based on the Lax-Wendroff prescription (6.16) gives the piecewise linear function shown in Figure 6.4(a). The slope  $\sigma_i''$  is nonzero only for i=J.

we will get a value that is greater than 1 for any  $\Delta t$  with  $0 < \bar{u} \Delta t < \Delta x$ . The worst case is In the next time step this overshoot will be accentuated, while in cell J-1 we will now have a positive slope, leading to a value  $Q_{J-1}^{n+1}$  that is less than 1. This oscillation then grows The function  $\tilde{q}^n(x,t_n)$  has an overshoot with a maximum value of 1.5 regardless of  $\Delta x_n$ When we advect this profile a distance  $\bar{n} \Delta t$ , and then compute the average over the Jth cell. when  $\tilde{u} \Delta t = \Delta x/2$ , in which case  $\tilde{q}^n(x, t_{n+1})$  is shown in Figure 6.4(b) and  $Q_J^{n+1} = 1.125$ .

The slopes proposed in the previous section were based on the assumption that the stope will improve the accuracy. On the contrary, if one of our goals is to avoid nonphysical  $\sigma_J'' < 0$  will lead to  $Q_J''^{+1} > 1$ , while a positive slope wouldn't make much sense. On the from smearing out too far, and hence will significantly increase the resolution and keep solution is smooth. Near a discontinuity there is no reason to believe that introducing this oscillations, then in the above example we must set the slope to zero in the Jth cell. Any smeared out over more than one cell, introducing nonzero slopes can help keep the solution other hand we don't want to set all slopes to zero all the time, or we simply have the first-order upwind method. Where the solution is smooth we want second-order accuracy, Moreover, we will see below that even near a discontinuity, once the solution is somewhat discontinuities fairly sharp, as long as care is taken to avoid oscillations.

This suggests that we must pay attention to how the solution is behaving near the ith nonlinear even for the linear advection equation). Where the solution is smooth, we want to cell in choosing our formula for  $\sigma_i''$ . (And hence the resulting updating formula will be choose something like the Lax-Wendroff slope. Near a discontinuity we may want to limit this slope, using a value that is smaller in magnitude in order to avoid oscillations. Methods based on this idea are known as slope-limiter methods. This approach was introduced by van



Fig. 6.4. (a) Grid values Q'' and reconstructed  $\tilde{q}''(\cdot,t_n)$  using Lax–Wendroff slopes. (b) After advection with  $\bar{u} \Delta t = \Delta x/2$ . The dots show the new cell averages  $Q''^{-1}$ . Note the overshoot.

6.7 Total Variation

Leer in a series of papers, [464] through [468], where he developed the approach known as AUSCL (monotonic upstream-centered scheme for conservation laws) for nonlinear conservation laws.

#### 6.7 Total Variation

tion that will allow us to use the Lax-Wendroff slope whenever possible, for second-order accuracy, while guaranteeing that no nonphysical oscillations will arise. To achieve this we How much should we limit the slope? Ideally we would like to have a mathematical prescripneed a way to measure oscillations in the solution. This is provided by the notion of the total variation of a function. For a grid function Q we define

$$TV(Q) = \sum_{i=-\infty}^{\infty} |Q_i - Q_{i-1}|,$$
 (6.18)

For an arbitrary function q(x) we can define

$$TV(q) = \sup_{j=1}^{N} |q(\xi_j) - q(\xi_{j-1})|.$$
 (6.19)

where the supremum is taken over all subdivisions of the real line  $-\infty=\xi_0<\xi_1<\cdots<$  $\xi_N=\infty$  . Note that for the total variation to be finite, Q or q must approach constant values.  $q^{\pm}$  as  $x \to \pm \infty$ .

Another possible definition for functions is

$$TV(q) = \limsup_{\epsilon \to 0} \frac{1}{\epsilon} \int_{-\infty}^{\infty} |q(x) - q(x - \epsilon)| dx.$$
 (6.20)

If q is differentiable, then this reduces to

$$TV(q) = \int_{-\infty}^{\infty} |q'(x)| dx. \tag{6.21}$$

We can use (6.21) also for nondifferentiable functions (distributions) if we interpret q'(x)as the distribution derivative (which includes delta functions at points where q is discontinuous). Note that if we define a function  $ilde{q}(x)$  from a grid function Q using a piecewise constant approximation, then  $TV(\tilde{q}) = TV(Q)$ .

The true solution to the advection equation simply propagates at speed  $ec{n}$  with unchanged shape, so that the total variation  $TV(q(\cdot,t))$  must be constant in time. A numerical solution to the advection equation might not have constant total variation, however. If the method introduces oscillations, then we would expect the total variation of  $Q^n$  to increase with time. We can thus attempt to avoid oscillations by requiring that the method not increase the total variation:

Definition 6.1. A two-level method is called total variation diminishing (TVD) if, for any set of data  $Q^n$  , the values  $Q^{n+1}$  computed by the method satisfy

$$\mathsf{TV}(Q^{n+1}) \leq \mathsf{TV}(Q^n).$$

Note that the total variation need not actually diminish in the sense of decreasine; it may remain constant in time. A better term might be total variation nonincreasing. In who introduced the use of this tool in developing and analyzing numerical methods for fact this term (and the abbreviation TVM) was used in the original work of Harten [179], conservation laws, It was later changed to TVD as a less cumbersome term.

If a method is TVD, then in particular data that is initially monotone, say

$$Q_i'' \ge Q_{i+1}''$$
 for all *i*.

will remain monotone in all future time steps. Hence if we discretize a single propagating but cannot become oscillatory. This property is especially useful, and we make the following discontinuity (as in Figure 6.4), the discontinuity may become smeared in future time steps

Definition 6.2. A method is called monotonicity-preserving if

$$Q_i^n \ge Q_{i+1}^n$$
 for all  $i$ 

implies that

$$Q_i^{n+1} \ge Q_{i+1}^{n+1}$$
 for all i.

Any TVD method is monotonicity-preserving: see Exercise 6.3.

## 6.8 TVD Methods Based on the REA Algorithm

How can we derive a method that is TVD? One easy way follows from the reconstructevolve-average approach to deriving methods described by Algorithm 4.1. Suppose that we perform the reconstruction in such a way that

$$\mathsf{TV}(\vec{q}^n(\cdot,t_n)) \le \mathsf{TV}(Q^n).$$
 (6.23)

Then the method will be TVD. The reason is that the evolving and averaging steps cannot possibly increase the total variation, and so it is only the reconstruction that we need to

In the evolve step we clearly have

$$TV(\tilde{q}^n(\cdot,t_{n+1})) = TV(\tilde{q}^n(\cdot,t_n))$$
(6.24)

for the advection equation, since  $\tilde{q}^n$  simply advects without changing shape. The total for we will see later that a wide class of nonlinear scalar conservation laws also have this variation turns out to be a very useful concept in studying nonlinear problems as well: property, that the true solution has a nonincreasing total variation.

It is a simple exercise (Exercise 6.4) to show that the averaging step gives

$$TV(Q^{n-1}) \le TV(\bar{q}^n(\cdot, t_{n+1})).$$
 (6.25)

Combining (6.23), (6.24), and (6.25) then shows that the method is TVD,

### 6.9 Slope-Limiter Methods

6.9 Slope-Limiter Methods

tion, and consider how to limit the slopes so that (6.23) is satisfied. Note that setting  $\sigma_i^n \equiv 0$ works, since the piecewise constant function has the same TV as the discrete data. Hence We now return to the derivation of numerical methods based on piecewise linear reconstructhe first-order upwind method is TVD for the advection equation. The upwind method may smear solutions but cannot introduce oscillations.

One choice of slope that gives second-order accuracy for smooth solutions while still satisfying the TVD property is the minmod slope

$$\sigma_i'' = \operatorname{minmod}\left(\frac{Q_i'' - Q_{i'-1}'}{\Delta x}, \frac{Q_{i'+1}' - Q_i''}{\Delta x}\right). \tag{6.26}$$

where the minmod function of two arguments is defined by

minmod(a, b) = 
$$\begin{cases} a & \text{if } |a| < |b| \text{ and } ab > 0, \\ b & \text{if } |b| < |a| \text{ and } ab > 0, \\ 0 & \text{if } ab \le 0, \end{cases}$$
 (6.27)

If a and b have the same sign, then this selects the one that is smaller in modulus, else it

Rather than defining the slope on the ith cell by always using the downwind difference (which would give the Lax-Wendroff method), or by always using the upwind difference (which would give the Beam-Warming method), the minmod method compares the two sign, then the value  $Q_i''$  must be a local maximum or minimum, and it is easy to check in slopes and chooses the one that is smaller in magnitude. If the two slopes have different this case that we must set  $\sigma_i^n = 0$  in order to satisfy (6.23).

Figure 6.2(a) shows results using the minmod method for the advection problem considered previously. We see that the minmod method does a fairly good job of maintaining good accuracy in the smooth hump and also sharp discontinuities in the square wave, with no oscillations. Sharper resolution of discontinuities can be achieved with other limiters that do not reduce the slope as severely as minmod near a discontinuity. Figure 6.5(a) shows some sample data representing a discontinuity smeared over two cells, along with the minmod slopes. Figure 6.5(b) shows that we can increase the slopes in these two cells to twire the value of the minmod slopes and still have (6.23) satisfied. This sharper reconstruction will lead to sharper resolution of the discontinuity in the next time step than we would obtain with the minmod slopes.



Fig. 6.5. Grid values  $Q^n$  and reconstructed  $\bar{q}^n(\cdot,t_n)$  using (a) minmod slopes. (b) superbee or MC slopes. Note that these steeper slopes can be used and still have the TVD property.

6.10 Flux Formulation with Piecewise Linear Reconstruction

, One choice of limiter that gives the reconstruction of Figure 6.5(b), while still giving second order accuracy for smooth solutions, is the so-called *superbee limiter* introduced by Roe 13781.

$$a_i^n = \max(a_i^{(1)}, a_i^{(2)}).$$
 (6.28)

where

$$\sigma_i^{(1)} = \operatorname{minmod}\left(\left(\frac{Q_{i+1}^n - Q_i^n}{\Delta x}\right), \ 2\left(\frac{Q_i^n - Q_{i-1}^n}{\Delta x}\right)\right).$$

$$\sigma_i^{(2)} = \operatorname{minmod}\left(2\left(\frac{Q_{i+1}^n - Q_i^n}{\Delta x}\right), \ \left(\frac{Q_i^n - Q_{i-1}^n}{\Delta x}\right)\right).$$

Each one-sided slope is compared with *twice* the opposite one-sided slope. Then the maxmod function in (6.28) selects the argument with *larger* modulus. In regions where the solution is smooth this will tend to return the *larger* of the two one-sided slopes, but will still be giving an approximation to  $q_x$ , and hence we expect second-order accuracy. We will see later that the superbee limiter is also TVD in general.

Figure 6.2(b) shows the same test problem as before but with the superbee method. The discontinuity stays considerably sharper. On the other hand, we see a tendency of the smooth hump to become steeper and squared off. This is sometimes a problem with superbee – by choosing the larger of the neighboring slopes it tends to steepen smooth transitions near inflection points.

Another popular choice is the *monotonized central-difference limiter* (MC limiter), which as proposed by van Leer [467]:

$$\sigma_i^n = \operatorname{minmod}\left(\left(\frac{Q_{i+1}^n - Q_{i-1}^n}{2\Delta x}\right), 2\left(\frac{Q_i^n - Q_{i-1}^n}{\Delta x}\right), 2\left(\frac{Q_{i+1}^n - Q_i^n}{\Delta x}\right)\right).$$
(6.29)

This compares the central difference of Fromm's method with *nvice* the one-sided slope to either side. In smooth regions this reduces to the centered slope of Fromm's method and hence does not tend to artificially steepen smooth slopes to the extent that superbee does. Numerical results with this limiter are shown in Figure 6.2(c). The MC limiter appears to be a good default choice for a wide class of problems.

# 6.10 Flux Formulation with Piecewise Linear Reconstruction

The slope-limiter methods described above can be written as flux-differencing methods of the form (4.4). The updating formulas derived above can be manipulated algebraically to determine what the numerical flux function must be. Alternatively, we can derive the numerical flux by computing the exact flux through the interface  $x_{i-1/2}$  using the piecewise linear solution  $\vec{q}^n(x, t)$ , by integrating  $i\vec{q}^n(x_{i-1/2}, t)$  in time from  $t_n$  to  $t_{n+1}$ . For the advection

equation this is easy to do and we find that

$$F_{i-1,2}^{n} = \frac{1}{\Delta t} \int_{t_{n}}^{t_{n-1}} d\tilde{q}^{n} (x_{i-1/2}, t) dt$$

$$= \frac{1}{\Delta t} \int_{t_{n}}^{t_{n-1}} d\tilde{q}^{n} (x_{i-1/2} - \tilde{u}(t - t_{n}), t_{n}) dt$$

$$= \frac{1}{\Delta t} \int_{t_{n}}^{t_{n-1}} d\left[ Q_{i-1}^{n} + (x_{i-1/2} - \tilde{u}(t - t_{n}) - x_{i-1}) \sigma_{i-1}^{n} \right] dt$$

$$= \tilde{u} Q_{i-1}^{n} + \frac{1}{2} \tilde{u} (\Delta x - \tilde{u} \Delta t) \sigma_{i-1}^{n}.$$

Using this in the flux-differencing formula (4.4) gives

$$Q_i^{n+1} = Q_i^n - \frac{\vec{u} \Delta t}{\Delta x} \left( Q_i^n - Q_{i-1}^n \right) - \frac{1}{2} \frac{\vec{u} \Delta t}{\Delta x} (\Delta x - \vec{u} \Delta t) \left( \sigma_i^n - \sigma_{i-1}^n \right).$$

which agrees with (6.13).

If we also consider the case  $\bar{n} < 0$ , then we will find that in general the numerical flux for a slope-limiter method is

$$F_{i-1/2}^{n} = \begin{cases} \bar{u} Q_{i-1}^{n} + \frac{1}{2} \bar{u} (\Delta x - \bar{u} \Delta t) \sigma_{i-1}^{n} & \text{if } \bar{u} \ge 0, \\ \bar{u} Q_{i}^{n} - \frac{1}{2} \bar{u} (\Delta x + \bar{u} \Delta t) \sigma_{i}^{n} & \text{if } \bar{u} \le 0. \end{cases}$$
(6.30)

where  $\sigma_i^n$  is the slope in the *i*th cell *C*<sub>i</sub>, chosen by one of the formulas discussed previously.

Rather than associating a slope  $o_i^n$  with the ith cell the idea of writing the method in terms of fluxes between cells suggests that we should instead associate our approximation to  $q_x$  with the cell interface at  $x_{i-1/2}$  where  $F_{i-1/2}^n$  is defined. Across the interface  $x_{i-1/2}$  we have a jump

$$\Delta Q_{i-1/2}'' = Q_i'' - Q_{i-1}''. \tag{6.31}$$

and this jump divided by  $\Delta x$  gives an approximation to  $q_i$ . This suggests that we write the flux (6.30) as

$$F_{i-1/2}^n = \bar{u}^- Q_i^n + \bar{u}^+ Q_{i-1}^n + \frac{1}{2} |\bar{u}| \left( 1 - \left| \frac{\bar{u} \, \Delta t}{\Delta x} \right| \right) \delta_{i-1/2}^n. \tag{6.32}$$

where

$$\delta_{i-1/2}^n = a$$
 limited version of  $\Delta Q_{i-1/2}^n$ . (6.33)

If  $\delta_{r-1/2}^{-}$  is the jump  $\Delta Q_{r-1/2}^{-}$  itself, then (6.32) gives the Lax-Wendroff method (see Exercise 6.6). From the form (6.32), we see that the Lax-Wendroff flux can be interpreted as a modification to the upwind flux (4.33). By limiting this modification we obtain a different form of the high-resolution methods, as explored in the next section.

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6.12 TVD Limiters

#### 6.11 Flux Limiters

second-order method based on piecewise linear reconstruction, since defining the jump method. Other second-order methods have fluxes of the form (6.32) with different choices From the above discussion it is natural to view the Lax-Wendroff method as the basic  $\delta_{t+1,2}^n$  in (6.33) in the most obvious way as  $\Delta Q_{t+1,2}^n$  at the interface  $x_{t+1,2}$  results in that of  $\delta_{i+1,2}^n$ . The slope-limiter methods can then be reinterpreted as  $extit{flux-limiter}$  methods by choosing  $\delta_{k=1,2}^n$  to be a limited version of (6.31). In general we will set

$$\delta_{i-1/2}^n = \phi(\theta_{i-1/2}^n) \Delta Q_{i-1/2}^n.$$
 (6.34)

where

$$\theta_{i-1/2}^n = \frac{\Delta Q_{i-1/2}^n}{\Delta Q_{i-1/2}^n}.$$
 (6.35)

The index I here is used to represent the interface on the upwind side of  $x_{1-1/2}$ :

$$I = \begin{cases} i - 1 & \text{if } \vec{u} > 0, \\ i + 1 & \text{if } \vec{u} < 0. \end{cases}$$
 (6.36)

The ratio  $\theta_{i-1/2}^n$  can be thought of as a measure of the smoothness of the data near  $x_{i-1/2}$ . Where the data is smooth we expect  $\theta_{j-1/2}^n \approx 1$  (except at extrema). Near a discontinuity we expect that  $\theta_{i-1,2}^n$  may be far from 1.

Setting  $\phi(\theta) \equiv 1$  for all  $\theta$  gives the Lax-Wendroff method, while setting  $\phi(\theta) \equiv 0$  gives The function  $\phi(\theta)$  is the flux-limiter function, whose value depends on the smoothness. upwind. More generally we might want to devise a limiter function  $\phi$  that has values near

For  $heta \approx 1$ , but that reduces (or perhaps increases) the slope where the data is not smooth. There are many other ways one might choose to measure the smoothness of the data besides the variable  $\theta$  defined in (6.35). However, the framework proposed above results in very simple formulas for the function  $\phi$  corresponding to many standard methods, including all the methods discussed so far.

In particular, note the nice feature that choosing

$$(\theta) = \theta \tag{6.37}$$

results in (6.34) becoming

$$\delta_{r-1/2}^n = \left(\frac{\Delta Q_{r-1/2}^n}{\Delta Q_{r-1/2}^n}\right) \Delta Q_{r-1/2}^n = \Delta Q_{r-1/2}^n.$$

Hence this choice results in the jump at the interface upwind from  $x_{i=1,2}$  being used to define  $\delta_{i-1/2}^n$  instead of the jump at this interface. As a result, the method (6.32) with the choice of limiter (6.37) reduces to the Beam-Warming method.

Since the centered difference (6.14) is the average of the one-sided slopes (6.15) and (6.16), we also find that Fromm's method can be obtained by choosing

$$\phi(\theta) = \frac{1}{2}(1+\theta).$$
 (6.38)

**Also** note that  $\phi(\theta) = 2$  corresponds to using  $\delta_{t+1,2}^n = 2 \Delta Q_{t+1,2}^n$ , i.e., twice the jump at **his** interface, while  $\phi(\theta) = 2\theta$  results in using twice the jump at the upwind interface. Recall Translating the various slope limiters into flux-limiter functions, we obtain the functions that these are necessary ingredients in some of the slope limiters discussed in Section 6.9, found below for the methods previously introduced.

Linear methods:

$$upwind: \phi(\theta) = 0,$$

Lax–Wendroff : 
$$\phi(\theta) = 1$$
.  
Beam–Warming :  $\phi(\theta) = \theta$ .

From 
$$\theta(\theta) = \frac{1}{2}(1 + \theta)$$
.

High-resolution limiters:

minmod: 
$$\phi(\theta) = \min \operatorname{minmod}(1, \theta)$$
,

superbee: 
$$\phi(\theta) = \max(0, \min(1, 2\theta), \min(2, \theta))$$
.  
MC:  $\phi(\theta) = \max(0, \min((1 + \theta)/2, 2, 2\theta))$  (6.39b)

van Leer: 
$$\phi(\theta) = \frac{\theta + |\theta|}{1 + |\theta|}$$
.

The van Leer limiter listed here was proposed in [465]. A wide variety of other limiters have also been proposed in the literature. Many of these limiters are built into CLAWPACK. The parameter mthlim in clawlez (see Section 5.4.6) determines which limiter is used. Other limiters are easily added to the code by modifying the file claw/clawpack/1d/lib/

The flux-limiter method has the flux (6.32) with  $\delta_{l-1/2}^n$  given by (6.34). Let  $v = i \bar{l} \Delta t / \Delta x$  be the Courant number. Then the flux-limiter method takes the form

$$Q_i^{n+1} = Q_i^n - \operatorname{rr}(Q_i^n - Q_{i-1}^n)$$

$$= \frac{1}{2} v(1-v) \left[ \phi(\theta_{i+1/2}^n) (Q_{i+1}^n - Q_i^n) - \phi(\theta_{i-1/2}^n) (Q_i^n - Q_{i+1}^n) \right] \quad (6.40)$$

$$Q_i^{n+1} = Q_i^n - v(Q_{i+1}^n - Q_i^n)$$

$$+ \frac{1}{2}v(1+v) \left[ \phi(\theta_{i+1/2}^n) (Q_{i+1}^n - Q_i^n) - \phi(\theta_{i-1/2}^n) (Q_i^n - Q_{i-1}^n) \right]$$
 (6.41)

#### 6.12 TVD Limiters

For simple limiters such as minmod, it is clear from the derivation as a slope limiter (Section 6.9) that the resulting method is TVD, since it is easy to check that (6.23) is satisfied. For more complicated limiters we would like to have an algebraic proof that the 6 12 TVD Limiters

resulting method is TVD. A fundamental tool in this direction is the following theorem of Harten [179], which can be used to derive explicit algebraic conditions on the function  $\phi$  required for a TVD method. For some other discussions of TVD conditions, see [180], [349], [429], [435], [465].

Theorem 6.1 (Harten). Consider a general method of the form

$$Q_i^{n+1} = Q_i^n - C_{i-1}^n (Q_i^n - Q_{i-1}^n) + D_i^n (Q_{i+1}^n - Q_i^n)$$
 (6.42)

over one time step, where the coefficients  $C_{i-1}^n$  and  $D_i^n$  are arbitrary values (which in particular may depend on values of  $Q^n$  in some way, i.e., the method may be nonlinear). Then

$$\mathsf{TV}(Q^{n+1}) \leq \mathsf{TV}(Q^n)$$

provided the following conditions are satisfied:

$$C_{i-1}^n \ge 0 \quad V_i,$$

$$D_i^n \ge 0 \quad V_i,$$

$$C_i^n + D_i^n \le 1 \quad V_i.$$
(6.43)

Note: the updating formula for  $Q_i^{n+1}$  uses  $C_{i-1}^n$  and  $D_i^n$ , but the last condition involves  $C_i^n$  and  $D^n$ 

For the proof see Exercise 8.5. We can apply this theorem to the flux-limiter method for  $q_1 + \mu q_2 = 0$ . We consider the case  $\bar{u} > 0$  here (see Exercise 6.7 for the case  $\bar{u} < 0$ ), so that the method has the form (6.40). There are many ways to rewrite this in the form (6.42), since  $C_{i-1}$  and  $D_i^n$  are allowed to depend on  $Q^n$ . The obvious choice is

$$C''_{i-1} = v - \frac{1}{2}v(1-v)\phi(\theta''_{i-1/2}),$$
  
$$D'_i = -\frac{1}{2}v(1-v)\phi(\theta''_{i+1/2}),$$

but this can i be effectively used to prove the method is TVD, as there is no hope of satisfying the condition (6.43) using this. If  $0 \le v \le 1$  then  $D_r' < 0$  when  $\phi$  is near 1. Instead note that

$$Q_{i+1}^n - Q_i^n = (Q_i^n - Q_{i-1}^n)/\theta_{i+1/2}^n$$

and so the formula (6.40) can be put into the form (6.42) with

$$C_{i-1}^n = v + \frac{1}{2}v(1-v) \left( \frac{\phi(\theta_{i+1/2}^n)}{\theta_{i+1/2}^n} - \phi(\theta_{i-1/2}^n) \right),$$
  
$$D_i^n = 0.$$

The conditions (6.43) are then satisfied provided that

$$0 \le C''_{r-1} \le 1.$$

This in turn holds provided that the CFL condition  $0 \le \nu \le 1$  holds, along with the bound

$$\left| \frac{\phi(\theta_1)}{\theta_1} - \phi(\theta_2) \right| \le 2 \quad \text{for all values of } \theta_1, \theta_2. \tag{6.44}$$

If  $\theta \le 0$ , then we are at an extremum, and we know from our previous discussion that we should take  $\phi(\theta) = 0$  in this case to achieve a TVD method. Also, when  $\theta > 0$  we want  $\phi(\theta) > 0$ , since it generally doesn't make sense to negate the sign of the slope in applying the limiter. Since  $\theta_1$  and  $\theta_2$  in (6.44) are independent, we then see that we must require

$$0 \le \frac{\phi(\theta)}{\theta} \le 2 \quad \text{and} \quad 0 \le \phi(\theta) \le 2 \tag{6.45}$$

for all values of  $\theta \ge 0$  in order to guarantee that condition (6.44) is satisfied (along with  $\phi(\theta) = 0$  for  $\theta < 0$ ). These constraints can be rewritten concisely as

$$0 \le \phi(\theta) \le \min \operatorname{mod}(2, 2\theta). \tag{6.46}$$

This defines the *TVD region* in the  $\theta$ - $\phi$  plane: the curve  $\phi(\theta)$  must lie in this region, which is shown as the shaded region in Figure 6.6(a). This figure also shows the functions  $\phi(\theta)$ 

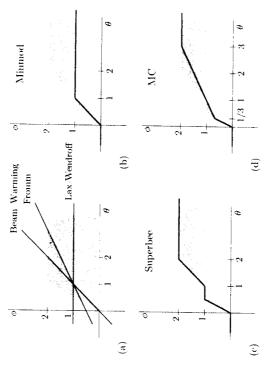


Fig. 6.6. Limiter functions  $\phi(\theta)$ . (a) The shaded regions shows where function values must lie for the method to be TVD. The second-order linear methods have functions  $\phi(\theta)$  that leave this region. (b) The shaded region is the Sweby region of second-order TVD methods. The minmod limiter lies along the lower boundary. (c) The superbec limiter lies along the upper boundary. (d) The MC limiter is snooth at  $\theta = 1$ .

6.13 High Resolution Methods for Systems

functions lie outside the shaded region for some values of  $\theta$ , and indeed these methods are not TVD. This graphical analysis of  $\phi$  was first presented by Sweby [429], who analyzed a from (6.39a) for the Lax. Wendroff, Beam-Warming, and Fromm methods. All of these wide class of flux-limiter methods (for nonlinear conservation laws as well as the advection

smooth data such as a sine wave tends to turn into a square wave as time evolves, as is already seen to happen with the superbee limiter. Imposing this additional restriction gives Note that for any second-order accurate method we must have  $\phi(1) = 1$ . Sweby found, moreover, that it is best to take  $\phi$  to be a convex combination of  $\phi = 1$  (Lax-Wendroff) and  $\phi = \theta$  (Beam–Warming). Other choices apparently give too much compression, and the second-order TVD region of Sweby, which is shown in Figure 6.6(b).

The high-resolution limiter functions from (6.39b) are all seen to satisfy the constraints Note that minmod lies along the lower boundary of the Sweby region. while superbee lies along the upper boundary. The fact that these functions are not smooth at  $\theta=1$  corresponds (6.46), and these limiters all give TVD methods. The functions  $\phi$  are graphed in Figure 6.6. to the fact that there is a switch in the choice of one-sided approximation used as  $\theta$  crosses this point. For full second-order accuracy we would like the function  $\phi$  to be smooth near  $\theta=1$ , as for the MC limiter. The van Leer limiter is an even smoother version of this.

We also generally want to impose a symmetry condition on the function  $\phi(\theta)$ . If the data  $Q^n$  is symmetric in x, then we might expect the reconstructed piecewise linear function to have this same property. It can be shown (Exercise 6.8) that this requires that the function

$$\phi(1/\theta) = \frac{\phi(\theta)}{\theta}.$$
 (6.47)

All of the high-resolution functions listed in (6.39b) satisfy this condition.

## 6.13 High-Resolution Methods for Systems

The stope-limiter or flux-limiter methods can also be extended to systems of equations. This is most easily done in the flux-limiter framework. First recall that the Lax-Wendroff method (6.4) can be written in flux-differencing form (4.4) if we define the flux by

$$\mathcal{F}(Q_{i-1}, Q_i) = \frac{1}{2} A(Q_{i-1} + Q_i) - \frac{1}{2} \frac{\Delta t}{\Delta x} A^2(Q_i - Q_{i-1}). \tag{6.48}$$

Since  $A = A^+ + A^-$ , we can rewrite this as

$$\mathcal{F}(Q_{i-1}, Q_i) = (A^{-}Q_{i-1} + A^{-}Q_i) + \frac{1}{2}|A| \left(I - \frac{\Delta_I}{\Delta_X}|A|\right) (Q_i - Q_{i-1}). \tag{6.49}$$

of the upwind flux (4.56) plus a correction term, just as for the scalar advection equation. To In the form (6.49), we see that the Lax-Wendroff flux can be viewed as being composed define a flux-limiter method we must limit the magnitude of this correction term according and it is not so clear how to compare this vector with the neighboring jump vector  $\Delta Q_{l-3,2}$ to how the data is varying. But for a system of equations,  $\Delta Q_{i-1/2} = Q_i - Q_{i-1}$  is a vector,

or  $\Delta Q_{t+1}$ ; to generalize (6.34). It is also not clear which neighboring jump to consider. since the "upwind" direction is different for each eigencomponent. The solution, of course, is that we must decompose the correction term in (6.49) into eigencomponents and limit each scalar eigencoefficient separately, based on the algorithm for scalar advection.

$$\frac{1}{2}|A|\left(I - \frac{\Delta I}{\Delta X}|A|\right)(Q_i - Q_{i-1}) = \frac{1}{2}|A|\left(I - \frac{\Delta I}{\Delta X}|A|\right)\sum_{p=1}^m \alpha_{i-1,2}^p r^p,$$

where  $r^p$  are the eigenvectors of A and the coefficients  $\alpha_{i-1/2}^p$  are defined by (4.38). The flux-limiter method is defined by replacing the scalar coefficient  $lpha_{i-1/2}^p$  by a limited version. based on the scalar formulas of Section 6.11. We set

$$\tilde{\alpha}_{l-1/2}^{p} = \alpha_{l-1/2}^{p} \phi(\theta_{l-1/2}^{p}), \tag{6.50}$$

where

$$\theta_{i-1/2}^{P} = \frac{\alpha_{i-1/2}^{P}}{\alpha_{i-1/2}^{P}} \quad \text{with } I = \begin{cases} i-1 & \text{if } \lambda^{P} > 0, \\ i+1 & \text{if } \lambda^{P} < 0, \end{cases}$$
 (6.51)

and  $\phi$  is one of the limiter functions of Section 6.11. The flux function for the flux-limiter

$$F_{i-1/2} = A^{+} Q_{i-1} + A^{\circ} Q_{i} + \tilde{F}_{i-1/2}. \tag{6.52}$$

where the first term is the upwind flux and the correction flux  $ilde{F}_{i-1/2}$  is defined by

$$\tilde{F}_{t-1/2} = \frac{1}{2} |A| \left( 1 - \frac{\Delta t}{\Delta x} |A| \right) \sum_{p=1}^{m} \tilde{\alpha}_{t-1/2}^{p} r^{p}. \tag{6.53}$$

that  $\Delta Q_{i-1/2} = \alpha_{i-1/2}^{\dagger}$ , which is what we called  $\delta_{i-1/2}$  in Section 6.11. The formula (6.52) then reduces to (6.32). Also note that the flux  $\tilde{F}_{i-1/2}$  (and hence  $F_{i-1/2}$ ) depends not only Note that in the case of a scalar equation, we can take  $r^{-1} = 1$  as the eigenvector of  $A = \bar{u}$ , so on  $Q_{i-1}$  and  $Q_i$ , but also on  $Q_{i-2}$  and  $Q_{i+1}$  in general, because neighboring jumps are used in defining the limited values  $\tilde{a}_{l-1/2}^p$  in (6.50). The flux-limiter method thus has a fivestencil gives a relaxation of the CFL restriction on the time step. For a five-point method the CFL condition requires only that the Courant number be less than 2. However, the CFL condition gives only a necessary condition on stability, and in fact these high-resolution does not lead to a greater stability limit because the additional information is used only to point stencil rather than the three-point stencil of the Lax-Wendroff. This is particularly important in specifying boundary conditions (see Chapter 7). Note that this widening of the methods are generally not stable for Courant numbers between 1 and 2. The larger stencil limit the second-order correction terms

Note that  $|A|r^n = |\lambda^n|r^n$ , so that (6.53) may be rewritten as

$$\tilde{F}_{j-1/2} = \frac{1}{2} \sum_{n=1}^{m} |\lambda^{p}| \left( 1 - \frac{\Delta t}{\Delta x} |\lambda^{p}| \right) \tilde{q}_{j-1/2}^{p} r^{p}. \tag{6.54}$$