

3.3. Modeling the Diode Forward Characteristic

- Considering the analysis of circuits employing forward conducting diodes
- To aid in analysis, represent the diode with a model
- Define a robust set of diode models
- Discuss **simplified diode models** better suited for use in circuit analysis and design of diode circuits:
 - **Exponential model**
 - **Constant voltage-drop model**
 - **Ideal diode model**
 - **Small-signal (linearization) model**

3.3.1 The Exponential Model

- Exponential diode model
 - Most accurate
 - Most difficult to employ in circuit analysis
 - Due to nonlinear nature
 - V_{DD} is greater than 0.5V

$$\text{(eq 3.6)} \quad I_D = I_S e^{V_D / V_T}$$

V_D = voltage across diode
 I_D = current through diode

$$\text{(eq 3.7)} \quad I_D = \frac{V_{DD} - V_D}{R}$$

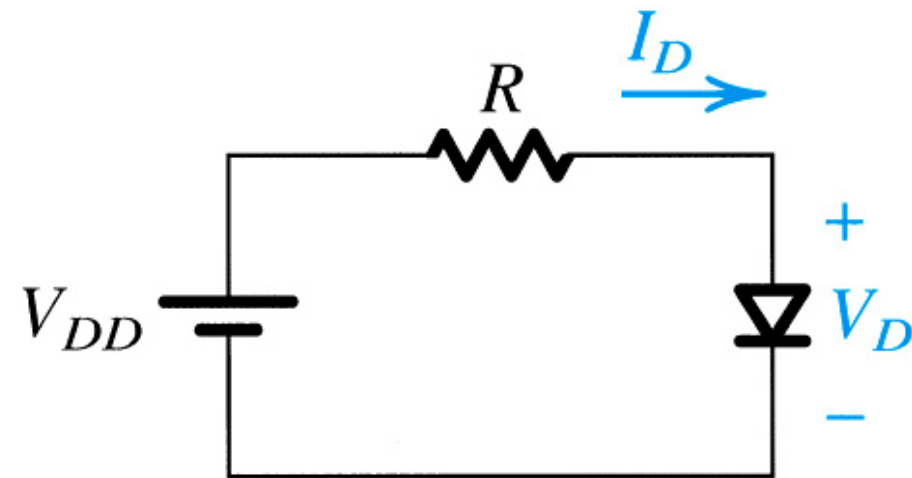


Figure 3.10: A simple circuit used to illustrate the analysis of circuits in which the diode is forward conducting

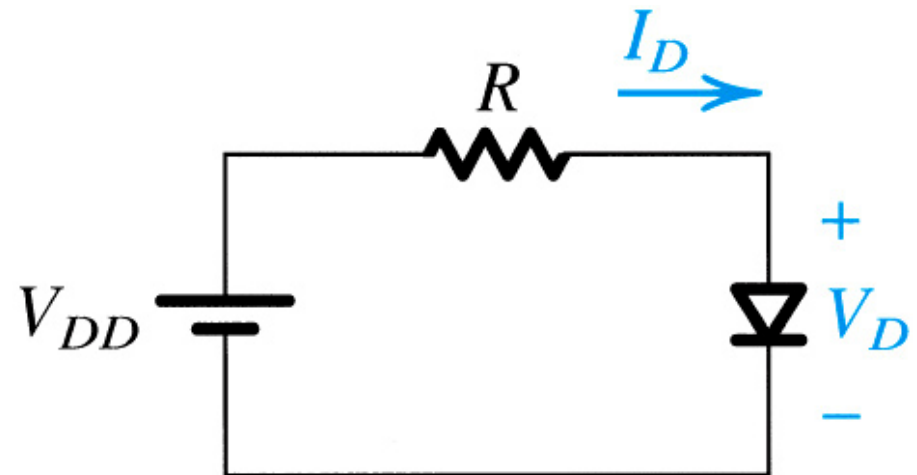
3.3.1 The Exponential Model

- **Q:** How does one solve for I_D in circuit to right?

- $V_{DD} = 5V$
- $R = 1k\Omega$
- $I_D = 1mA @ 0.7V$

- **A:** Two methods exist...

- **graphical method**
- **iterative method**



3.3.2 Graphical Analysis using Exponential Model

- Step 1: Plot the relationships of (3.6) and (3.7) on single graph
- Step 2: Find intersection of
 - **load line** and diode characteristic intersect at **operating point (Q)**

$$\text{(eq 3.6)} \quad I_D = I_S e^{V_D / V_T}$$

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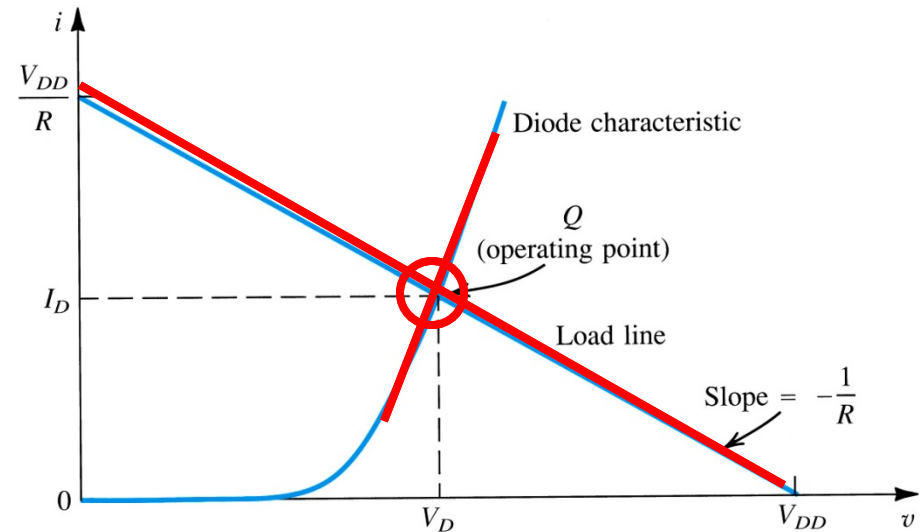


Figure 3.11: Graphical analysis of the circuit in Fig. 3.10 using the exponential diode model.

3.3.2 Graphical Analysis using Exponential Model

- **Pro's**

- Intuitive
 - b/c of visual nature

- **Con's**

- Poor **Precision**
- Not **Practical** for Complex Analyses
 - Multiple lines required

3.3.3 Iterative Analysis using Exponential Model

- Ex 3.4
- **Step 1:** Start with **initial guess** of V_D .
 - $V_D^{(0)}$
- **Step 2:** Use **nodal / mesh analysis** to solve I_D
- **Step 3:** Use exponential model to **update V_D**
 - $V_D^{(1)} = \mathbf{f}(V_D^{(0)})$
- **Step 4:** **Repeat these steps** until $V_D^{(k+1)} = V_D^{(k)}$
 - Upon convergence, the new and old values of V_D will **match**

3.3.3 Iterative Analysis using Exponential Model

- Pro's

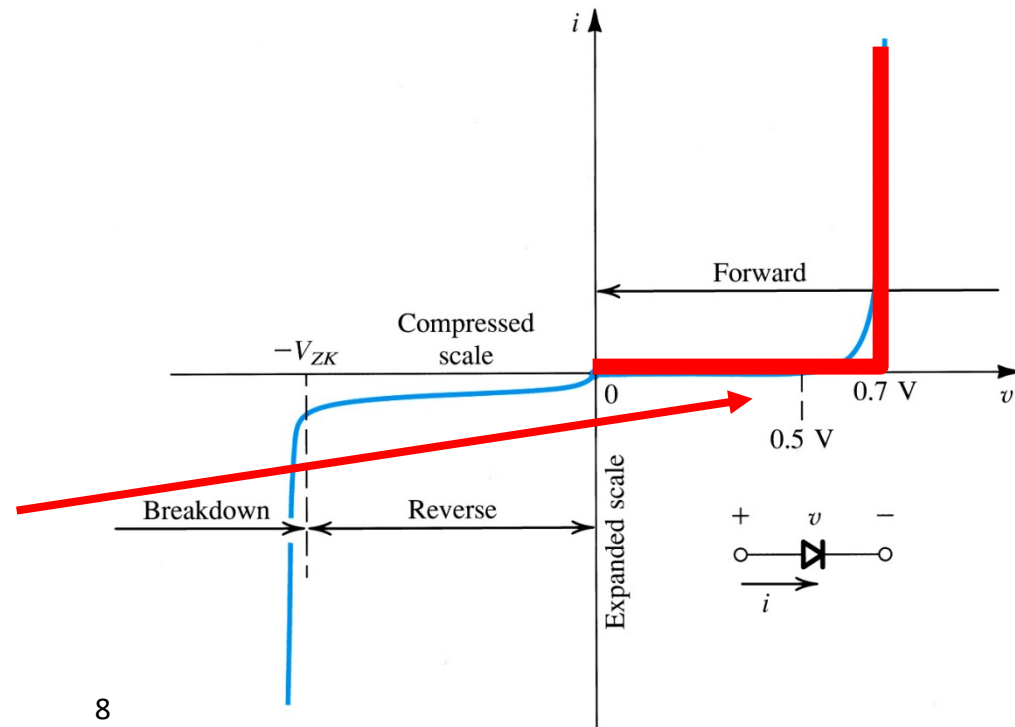
- High Precision

- Con's

- Not Intuitive
- Not Practical for Complex Analysis
 - 10+ iterations may be required

3.3.4 The Need for Rapid Analysis

- Analyze the diode-based circuit more efficiently
 - Rapid circuit analysis with a simpler model
 - Further refine and “fine-tune” the design in almost final design
 - Perform with the aid of a computer circuit analysis program (SPICE)
- One example is assume that voltage drop across the diode is constant



3.3.5 The Constant Voltage-Drop Model

- Voltage drop of a forward-conducting diode varies in a relatively narrow range (0.6-0.8V)
- The **constant voltage-drop diode model** assumes that the slope of I_D vs. V_D is vertical @ 0.7V
- Not very different
- Employed in the initial phases of analysis and design
- **Ex3.4:** solution change if CVDM is used?
 - **A:** 4.262mA to 4.3mA

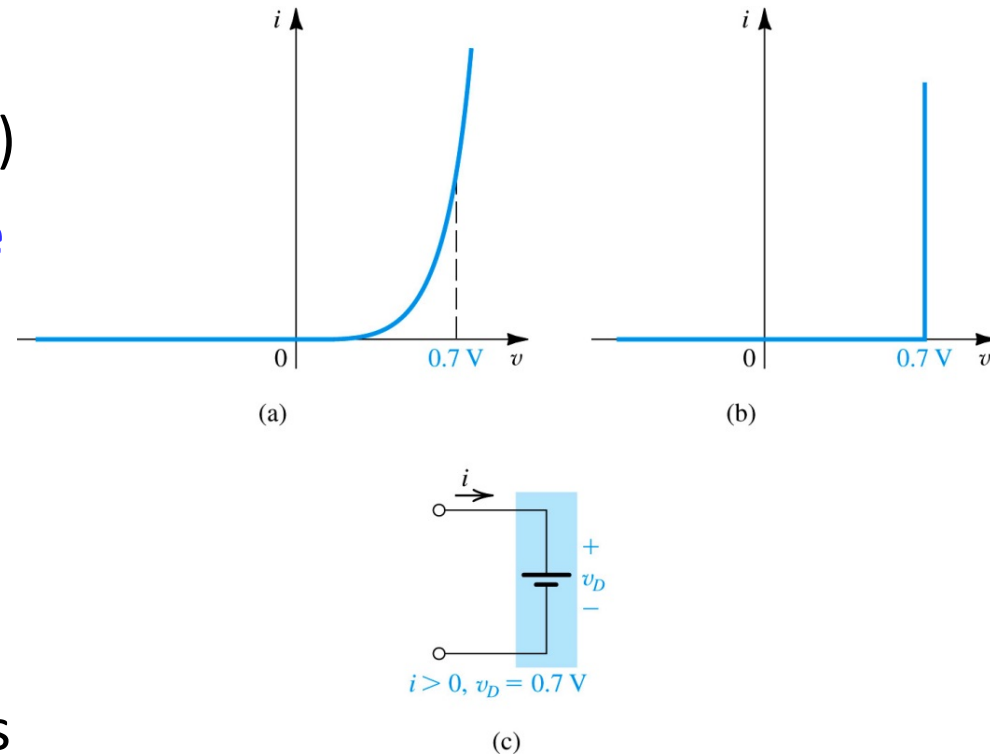
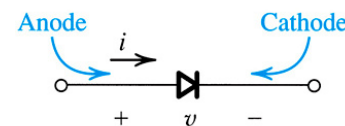


Figure 3.12: Development of the diode constant-voltage-drop model: (a) the exponential characteristic; (b) approximating the exponential characteristic by a constant voltage, usually about 0.7 V; (c) the resulting model of the forward-conducting diodes

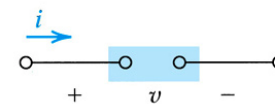
3.3.6 Ideal Diode Model

- When involving voltages much greater than the diode voltage drop
- Very quick analysis for a gross estimate
- For determine which diodes are on/off in a multidiode circuit
- The **ideal diode model** assumes that the slope of I_D vs. V_D is vertical @ $0V$
- **Ex3.4:** solution change if ideal model is used?
 - **A:** $4.262mA$ to $5mA$

device symbol
with two nodes



(a)

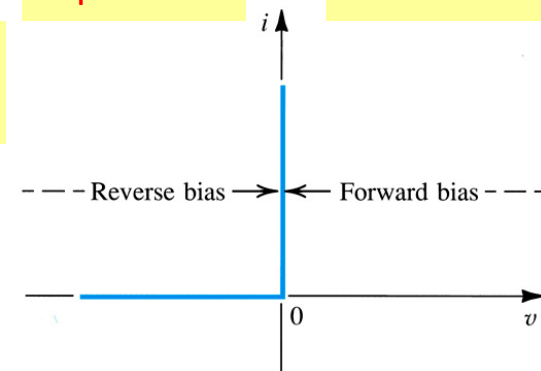


$$v < 0 \Rightarrow i = 0$$

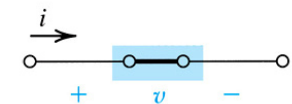
(c)

mode #2:
reverse
bias =
open ckt.

mode #1:
forward
bias =
short ckt



(b)

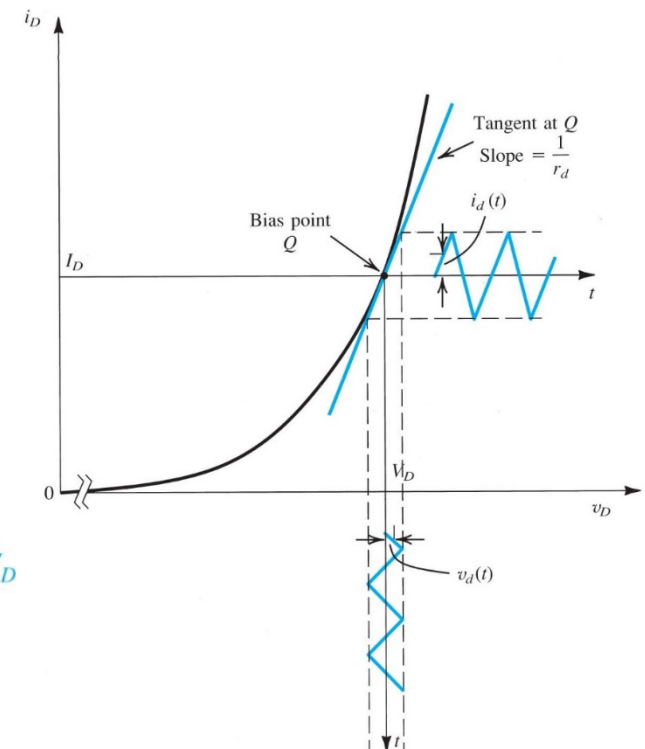
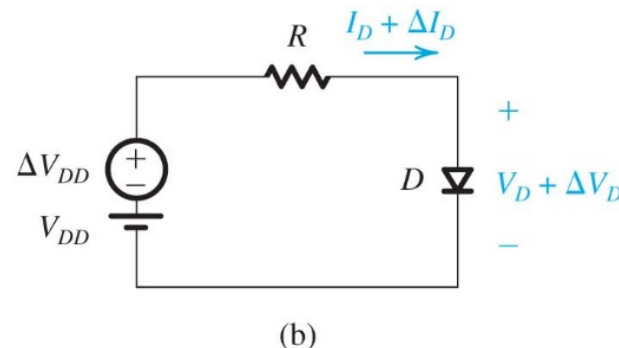
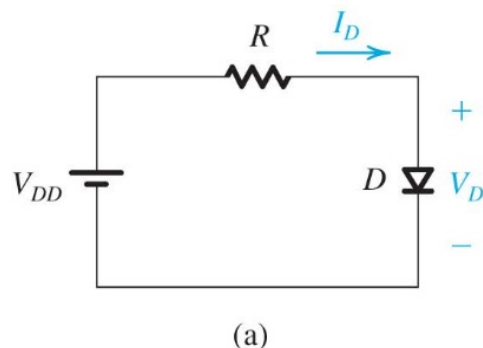


$$i > 0 \Rightarrow v = 0$$

(d)

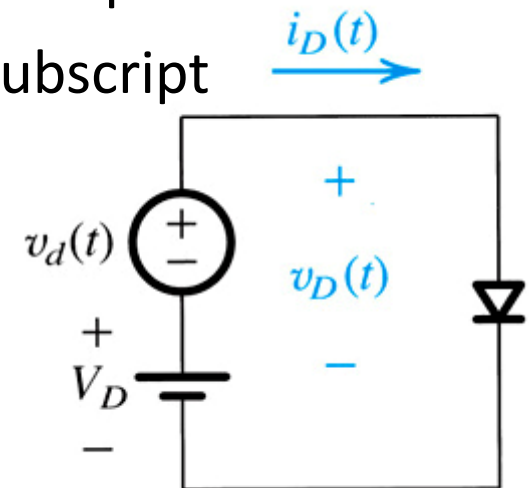
3.3.7 Small-Signal Model

- Operate at a dc biased point on the forward i - v characteristic and a small ac signal superimposed on dc
- dc operating point (I_D , V_D) by other model
- And then, modeled as **variable resistor** = inverse of the slope of the tangent to exponential i - v characteristic at the bias point
- Whose value is defined via **linearization** of exponential model
- Around **bias point** defined by constant voltage drop model



3.3.7 Small-Signal Model

- Define the small-signal diode model
- Step 1: consider the conceptual circuit of figure 3.13(b)
 - DC voltage (V_D) is applied to diode
 - Upon V_D , arbitrary time-varying signal $v_d(t)$ is superimposed
- **DC only** – upper-case w/ upper-case subscript
- **Time-varying only** – lower-case w/ lower-case subscript
- **Total instantaneous** – lower-case w/ upper-case subscript
 - DC + time-varying



3.3.7 Small-Signal Model

- Step 2: define **DC current** as in (3.8)
- Step 3: Define **total instantaneous voltage** (v_D) as composed of V_D and v_d
- Step 4: Define **total instantaneous current** (i_D) as function of v_D

$$\text{(eq 3.8)} \quad I_D = I_S e^{V_D / V_T}$$

$$\text{(eq 3.9)} \quad \underbrace{v_D(t) = V_D + v_d(t)}$$

$v_D(t)$ = total instantaneous voltage across diode

V_D = dc component of $v_D(t)$

$v_d(t)$ = time varying component of $v_D(t)$

$$\text{(eq 3.10)} \quad \underbrace{i_D(t) = I_S e^{v_D / V_T}}$$

note that this is different from (3.8)

3.3.7 Small-Signal Model

- Step 5: **Redefine (3.10)** as function of both V_D and v_d
- Step 6: **Split** this exponential in two
- Step 7: **Redefine total instant current** in terms of DC component (I_D) and time-varying current (i_d)

(eq 3.11) $i_D(t) = I_S e^{(V_D + v_d)/V_T}$

action: split this exponential using appropriate laws

(eq 3.11) $i_D(t) = \underbrace{I_S e^{V_D/V_T}}_{I_D} e^{v_d/V_T}$

(eq 3.12) $i_D(t) = I_D e^{v_d/V_T}$

3.3.7 Small-Signal Model

example: $e^x = 1 + x + \frac{x^2}{2!} + \frac{x^3}{3!} + \frac{x^4}{4!} + \dots$

- Step 8: Apply **power series expansion** to (3.12)

action: apply power series expansion to (4.12)

because $v_d / V_T \ll 1$, these terms are assumed to be negligible

(eq 3.12) $i_D(t) = I_D \left(1 + \frac{v_d}{V_T} + \left[\left(\frac{v_d}{V_T} \right)^2 \frac{1}{2!} \right] + \left[\left(\frac{v_d}{V_T} \right)^3 \frac{1}{3!} \right] + \dots \right)$

power series expansion of e^{v_d/V_T}

- Step 9: Because $v_d/V_T \ll 1$, certain terms may be **neglected**

action: eliminate negligible terms

(eq 3.14) $i_D(t) = I_D \left(1 + \frac{v_d}{V_T} \right)$

3.3.7 Small-Signal Model

• Small signal approximation

- Shown to right for exponential diode model
 - Total instant current (i_D)
 - Small-signal current (i_d)
 - Diode small-signal resistance / incremental resistance (r_d)
- Valid for $v_d < 5mV$ amplitude (not peak to peak)
- Inversely proportional to the bias current I_D

$$i_D(t) = I_D + \underbrace{\left(\frac{I_D}{V_T} \right)}_{i_d} v_d$$

$$i_D(t) = I_D + i_d$$

$$i_d = \frac{1}{r_d} v_d$$

$$r_d = \frac{V_T}{I_D}$$

3.3.7 Small-Signal Model

- Assuming that the signal amplitude is sufficiently small such that the excursion along the i - v curve is limited to a short almost-linear segment

$$r_d = 1 / \left[\frac{\partial i_D}{\partial v_D} \right]_{i_D = I_D}$$

- This method may be used to **approximate any function** $y = \mathbf{f}(x)$ around an operating point (x_0, y_0) .

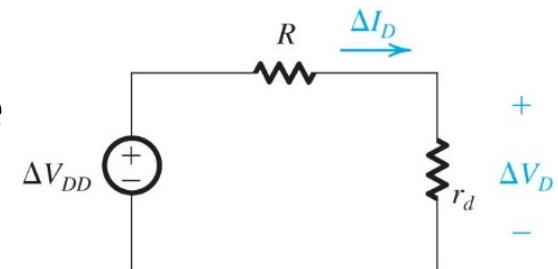
$$y(t) = y_0 + \left(\frac{\partial y}{\partial x} \bigg|_{y=y_0} \right)^{-1} \overbrace{(x(t) - x_0)}^{\Delta x}$$

3.3.7 Small-Signal Model

- **Q:** How is **small-signal resistance** r_d defined?
 - **A:** From steady-state current (I_D) and thermal voltage (V_T) as below
 - Note this approximation is only valid for small-signal voltages $v_d < 5mV$

$$r_d = \frac{V_T}{I_D}$$

- After dc analysis (define the dc bias point = quiescent point) of the diode,
- Eliminating all dc sources (short-circuiting dc voltage sources and open-circuiting dc current sources)
- Replacing the diode by its small-signal resistance



3.3.7 Small-Signal Model

- **Q:** How is the small-signal diode model defined?
 - **A:** The **total instantaneous circuit is divided into steady-state and time varying components**, which may be analyzed separately and solved via algebra
 - In steady-state, diode represented as CVDM
 - In time-varying, diode represented as resistor

Neither of these circuits employ the exponential model – simplifying the “solving” process

Example 3.5:

- $R = 10k\Omega$
- Power supply V^+ : dc value of $10V$ + $60Hz$ sinusoid of $1V$ peak amplitude (known as the power supply ripple)
- Assume diode to have $0.7V$ drop at $1mA$ current
- **Q:** Calculate both amplitude of the dc and sine-wave signal observed across the diode
 - **A:** $v_d(\text{peak}) = 2.68mV$

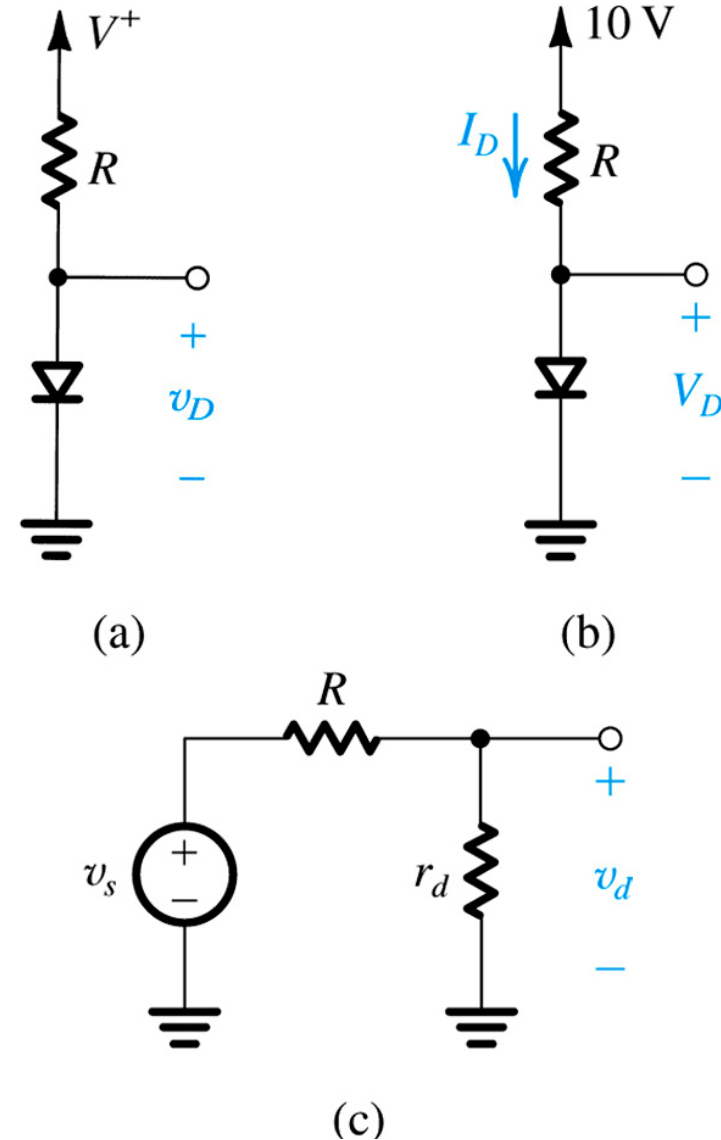


Figure 3.16: (a) circuit for Example 3.5. (b) circuit for calculating the dc operating point. (c) small-signal equivalent circuit.

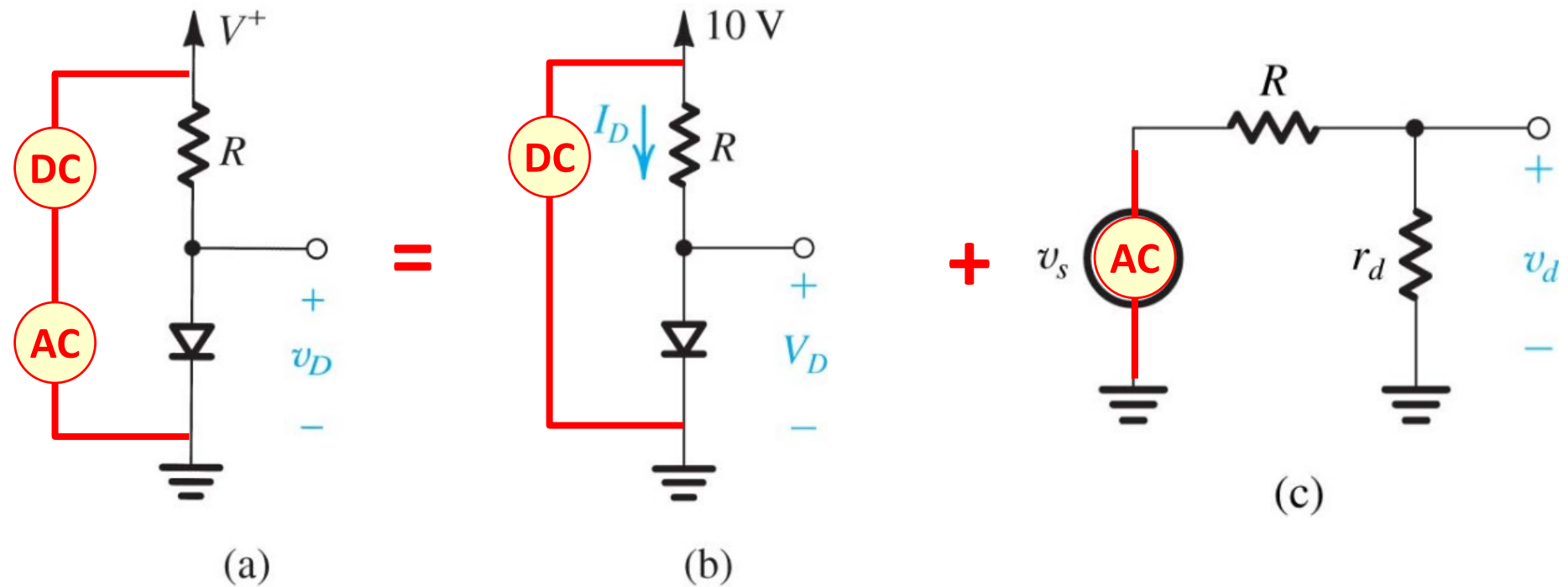


Figure 3.14: (a) Circuit for Example 3.5. (b) Circuit for calculating the dc operating point. (c) Small-signal equivalent circuit.

When to use these models?

- Exponential model
 - Low voltages
 - Less complex circuits
 - Emphasis on accuracy over practicality
- constant voltage-drop mode:
 - Medium voltages = $0.7V$
 - More complex circuits
 - Emphasis on practicality over accuracy
- Ideal diode model
 - High voltages $\gg 0.7V$
 - Very complex circuits
 - Cases where a difference in voltage by $0.7V$ is negligible
- Small-signal model

3.3.8 Diode Forward Drop in Voltage Regulation

- **Voltage regulator**
 - Provide a constant dc voltage between its output terminals
 - To remain output as constant as possible in spite of changes in dc power supply voltage and load current
- **Q:** What characteristic of the diode facilitates voltage regulation?
 - **A:** The approximately constant voltage drop across it ($0.7V$)

Example 3.6: Diode-Based Voltage Regulator

- Consider circuit shown in Figure 3.17. A string of three diodes is used to provide a constant voltage of 2.1V
 - Q:** What is the change in this regulated voltage caused by
 - (a) a $\pm 10\%$ change in supply voltage and
 - (b) connection of $1\text{k}\Omega$ load resistor

