

Upheavle Buckling

This shows the basic calculations for upheaval buckling for:

- Project: Tibr Houshi Development Phase 2B FEED+DD
- Doc. No.: TIB-17-PDFEED-LA-0515-00001-0000

V0.2:

Inconsistency of thermal force units

/Other inconsistencies (force, energy) ==> | FIXED|

— inputs —

Height of imperfection

$$\delta := 0.1 \text{ m}$$

Installation temperature

$$T_i := 21 \text{ } ^\circ\text{C}$$

Design pressure

$$P := 95 \text{ bar}$$

Max. Design temperature

$$T_{2_{max}} := 85 \text{ } ^\circ\text{C}$$

Selected wall thickness

$$t := 4.8 \text{ mm}$$

Difference between Max. design temperature & Installation temperature ($T_2 - T_i$)

$$\Delta T := T_{2_{max}} - T_i = 64 \text{ } ^\circ\text{C}$$

Outside diameter of the pipe

$$D := 6.625 \text{ in} = 0.1683 \text{ m}$$

the depth of cover from the top of the pipe to the soil surface above the pipe centerline

Inside diameter of the pipe

$$D_i := D - 2 \cdot t = 0.1587 \text{ m}$$

$$H := 0.6 \text{ m}$$

Soil Density

$$\gamma := 1600 \frac{\text{kg}}{\text{m}^3}$$

an uplift resistance coefficient

$$f := 0.15$$

Modulus of elasticity

$$E := 2.394 \cdot 10^{10} \frac{\text{N}}{\text{m}^2}$$

Steel density

$$\rho_s := 7800 \frac{\text{kg}}{\text{m}^3}$$

Poisson's Ratio

$$\nu := 0.3$$

Coefficient of thermal expansion

$$\alpha := 0.000011 \frac{\frac{\text{mm}}{\text{mm}}}{\Delta \text{ } ^\circ\text{C}} = 1.1 \cdot 10^{-5} \cdot \frac{1}{\text{K}}$$

pipe content density

$$\rho_f := 935 \frac{\text{kg}}{\text{m}^3}$$

Pressure Force

$$F_P := P \cdot \frac{\pi \cdot D_i^2}{4} = 19156.2204 \text{ kgf}$$

Poisson's effect Force

$$F_v := \frac{P \cdot D}{2 \cdot t} \cdot v \cdot \frac{\pi \cdot (D^2 - D_i^2)}{4} = 12557.8418 \text{ kgf}$$

Thermal Force

$$F_T := E \cdot \alpha \cdot \Delta T \cdot \frac{\pi \cdot (D^2 - D_i^2)}{4} = 41546.9609 \text{ N}$$

Effective Axial Force

$$F_{EAF} := F_P + F_v + F_T = 3.5256 \cdot 10^5 \text{ N}$$

Pipeline weight including content per unit length

$$w := \frac{\rho_s \cdot \pi \cdot (D^2 - D_i^2)}{4} + \frac{\rho_f \cdot \pi \cdot (D - 2 \cdot t)^2}{4} = 37.7173 \frac{\text{kg}}{\text{m}}$$

Moment of inertia

$$I := \frac{\pi \cdot (D^4 - D_i^4)}{64} = 8.2419 \cdot 10^{-6} \text{ m}^4$$

Required downforce for uplift resistance

$$W := \left(1.16 \cdot \frac{4.76 \cdot \left(\frac{E \cdot I \cdot w}{\delta} \right)^{\frac{1}{2}}}{F_{EAF}} \right) \cdot F_{EAF} \cdot \left(\frac{\delta \cdot w}{E \cdot I} \right)^{\frac{1}{2}} = 208.2601 \frac{\text{kg}}{\text{m}}$$

Downward force per unit length required to hold pipeline in position

$$q := H \cdot \gamma \cdot D \cdot \left(1 + \frac{f \cdot H}{D} \right) = 247.944 \frac{\text{kg}}{\text{m}}$$

◻—if statement

Check the pipeline stability against upheaval Buckling

$$\psi := \begin{cases} \text{"stable"} & \text{if } w + q > W \\ \text{"not stable"} & \text{otherwise} \end{cases}$$

$$\psi = \text{"stable"}$$