

Automatic Control Systems

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- **Reading: chapter 9**
 - Sections 9.1, 9.2, 9.3
 - Study **Table 9.6** on pages 704-711

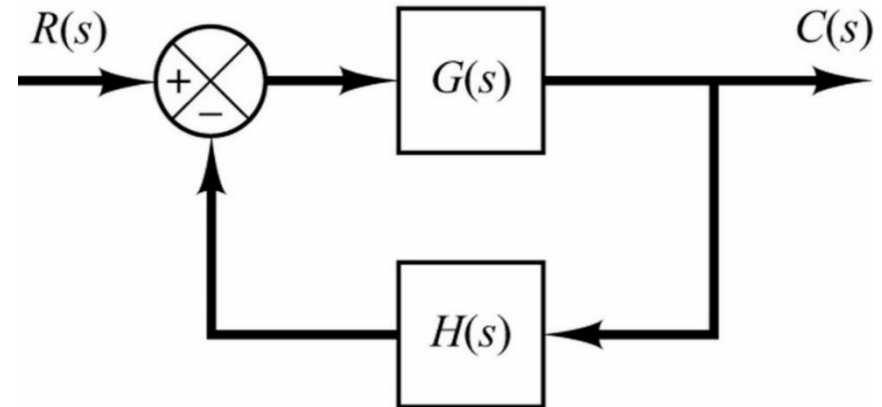
Nyquist Stability Criterion

Stability in the frequency domain

- Open loop system $G(s)H(s)$

Characteristic equation of the Closed-loop system

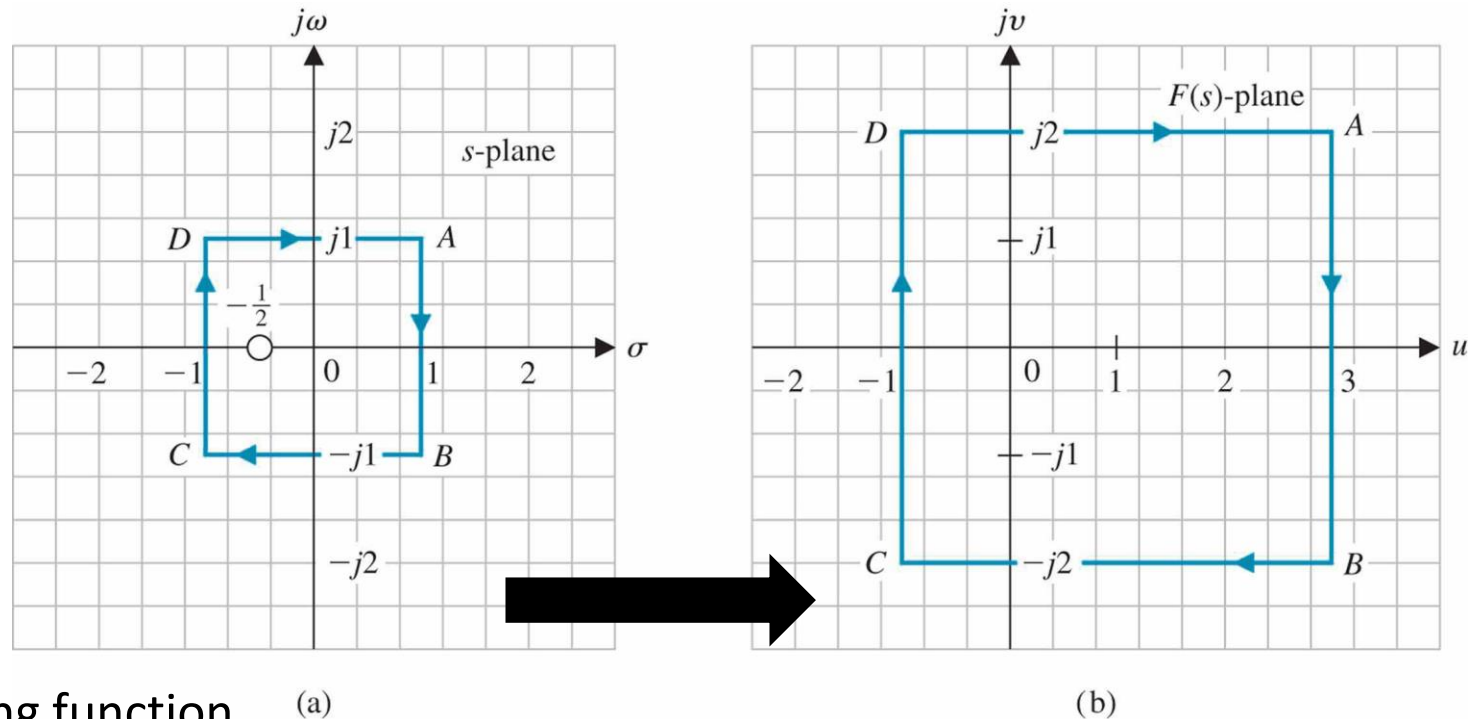
$$F(s) = 1 + G(s)H(s)$$



- The **Nyquist stability criterion**, a graphical method, determines the **stability of a closed-loop system** from its **open-loop system** without determining the closed-loop poles.
- The Nyquist stability criterion relates the open-loop frequency response $G(s)H(s)$ to the **number of zeros of the characteristic equation** that lies in the $1 + G(s)H(s)$ right-half plane
- The **Nyquist stability criterion** is based on **Cauchy's theorem** which is concerned with **mapping contours** in the s-plane

Contour Mapping

A contour map is a trajectory in one plane, s – plane, mapped into another plane, $F(s)$ – plane, by a relation $F(s)$. A **closed contour** in the s – plane produces a **closed contour** in the $F(s)$ -plane



- Mapping function (a)

$$F(s) = 2s + 1$$

- Change of variables

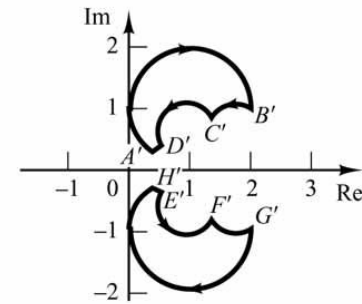
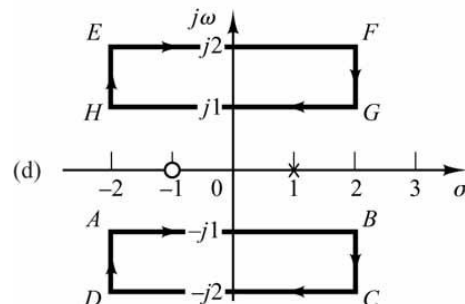
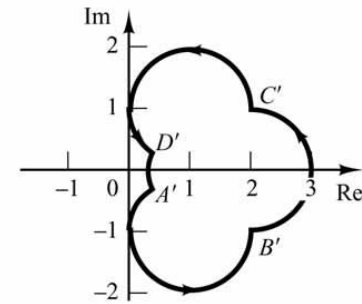
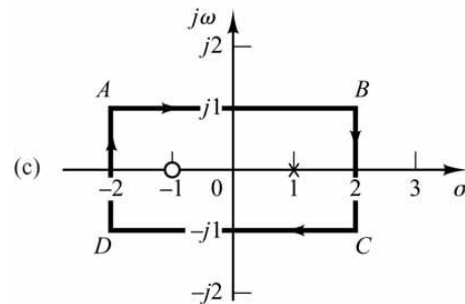
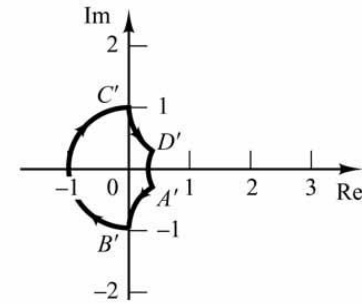
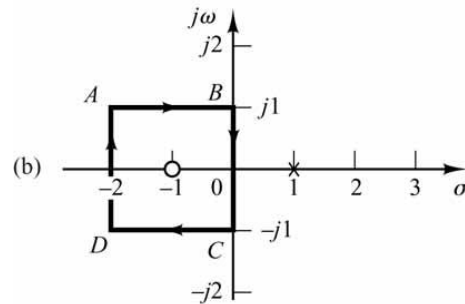
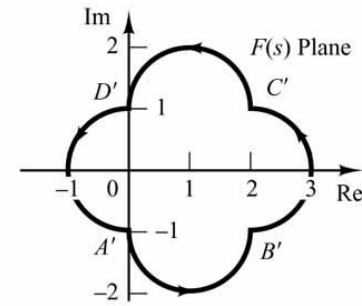
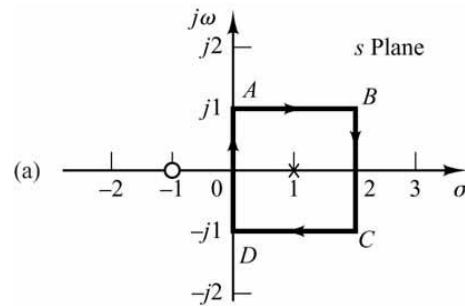
$$u + jv = F(\sigma + j\omega) = 2(\sigma + j\omega) + 1 = (2\sigma + 1) + j\omega$$

$$u = 2\sigma + 1, \quad v = 2\omega$$

- example

Mapping function:

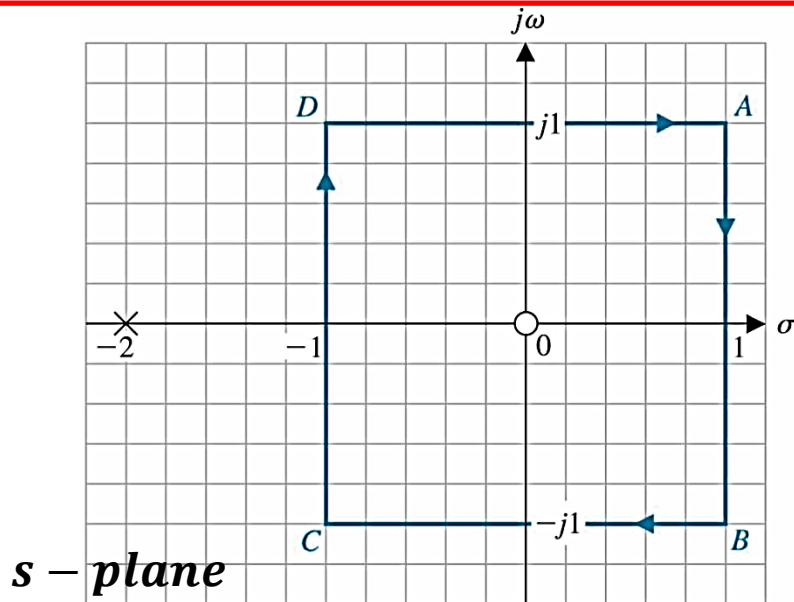
$$F(s) = \frac{(s+1)}{(s-1)}$$



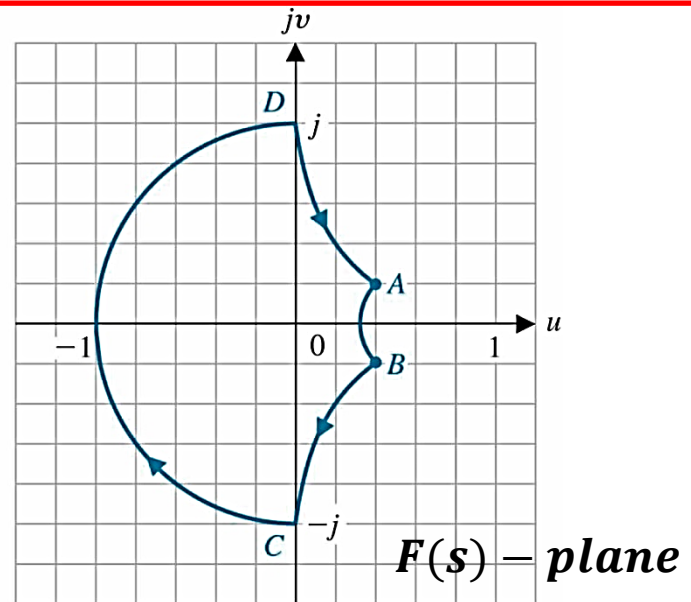
- *example*

$$F(s) = \frac{s}{(s + 2)}$$

- Define the positive direction is the clock-wise direction and the enclosed area is on the right **"CLOCK-WISE AND FACING RIGHT"**



(a)



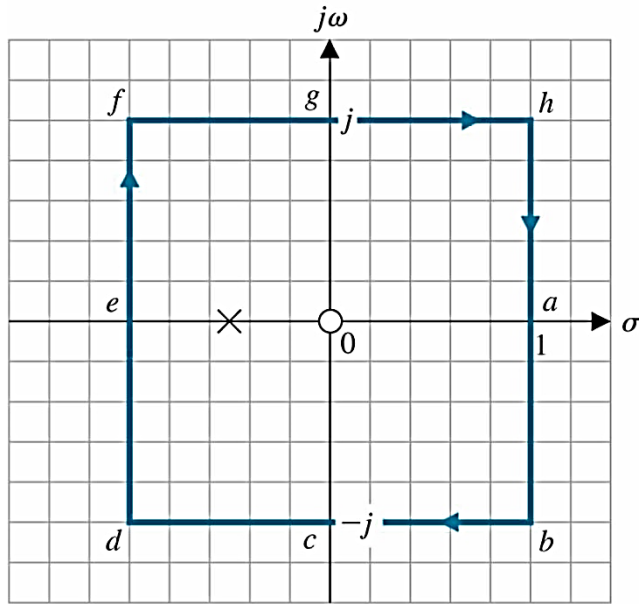
(b)

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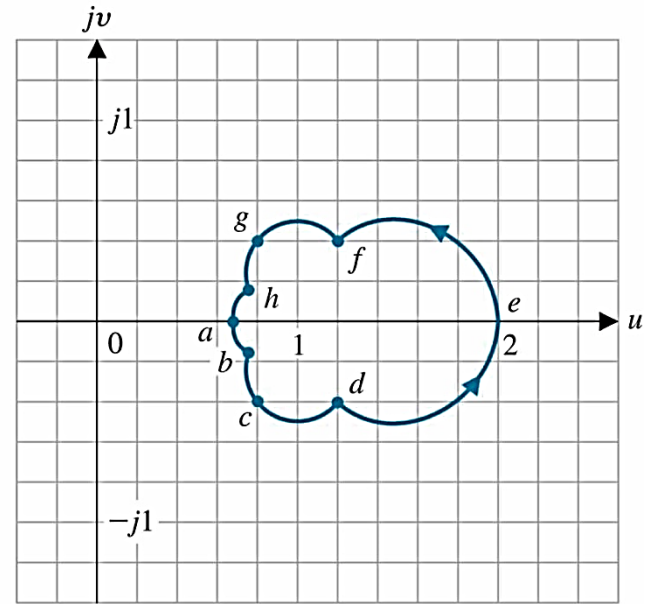
The contour in the *F(s)* – plane encloses (encircles) the origin of the ***F(s)* – plane**

- *example*

$$F(s) = \frac{s}{(s + 0.5)}$$



s – plane (a)



(b) *F(s)* – plane

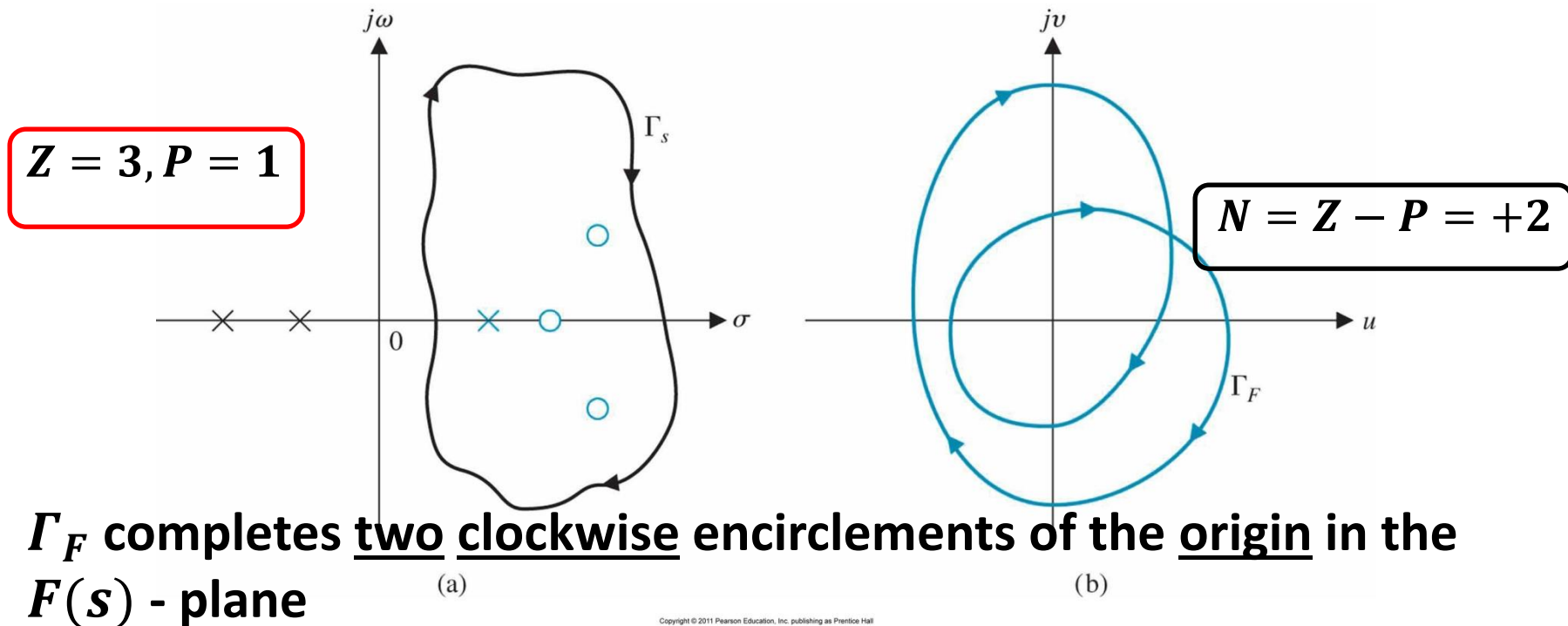
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The contour in the *F(s)* – plane does not enclose (encircle) the origin of the *F(s)* – plane

Cauchy's Theorem

“Cauchy's Argument Principle”

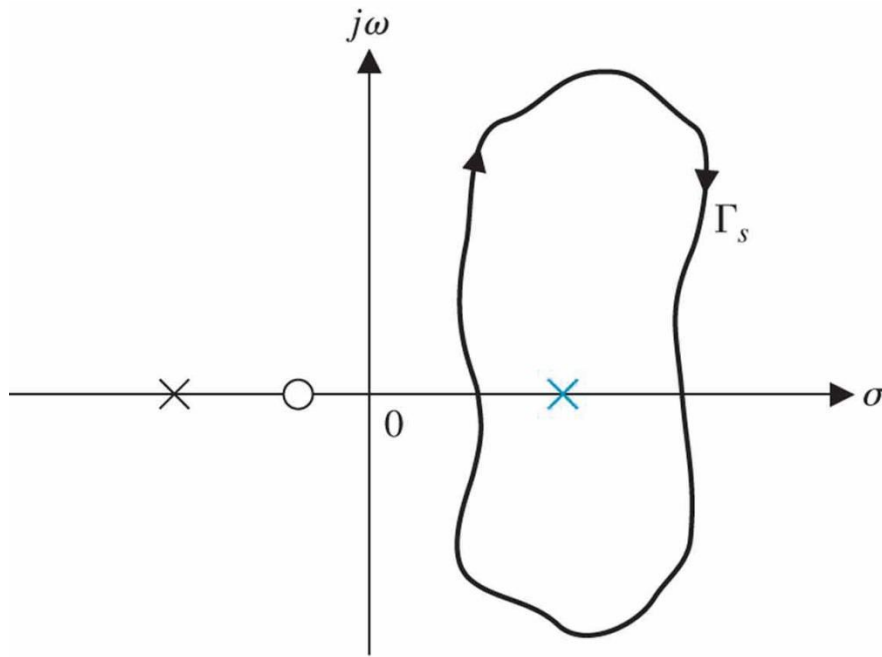
“if a contour Γ_s in the s -plane encircles Z zeros and P poles of $F(s)$ and does not pass through any poles or zeros of $F(s)$ and the transversal is in the clockwise direction along the contour, the corresponding contour Γ_F in the $F(s)$ -plane encircles the origin of the $F(s)$ -plane $N = Z - P$ times in the clockwise direction”



- *example*

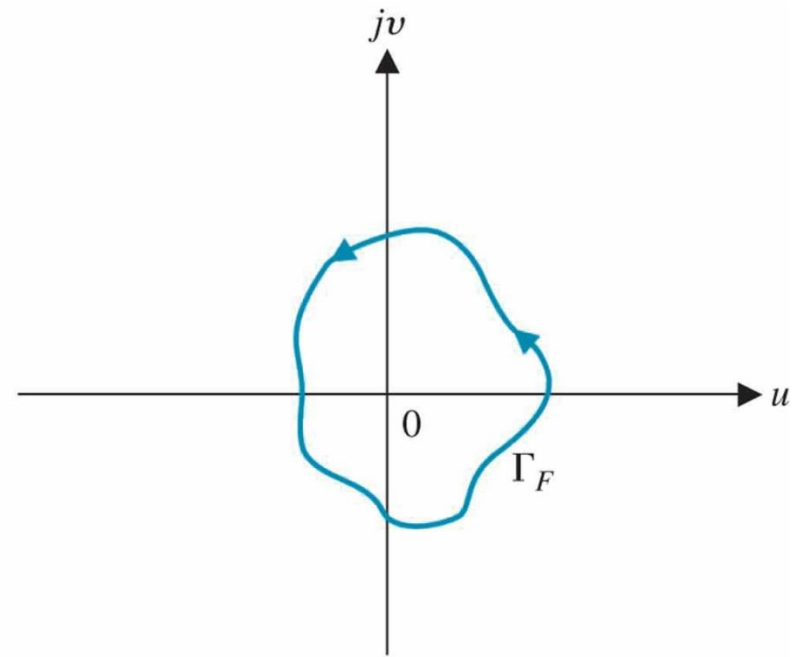
The contour Γ_F encircles the origin in the $F(s)$ -plane once in the counterclockwise direction

$$Z = 0, P = 1$$



(a)

$$N = Z - P = -1$$



(b)

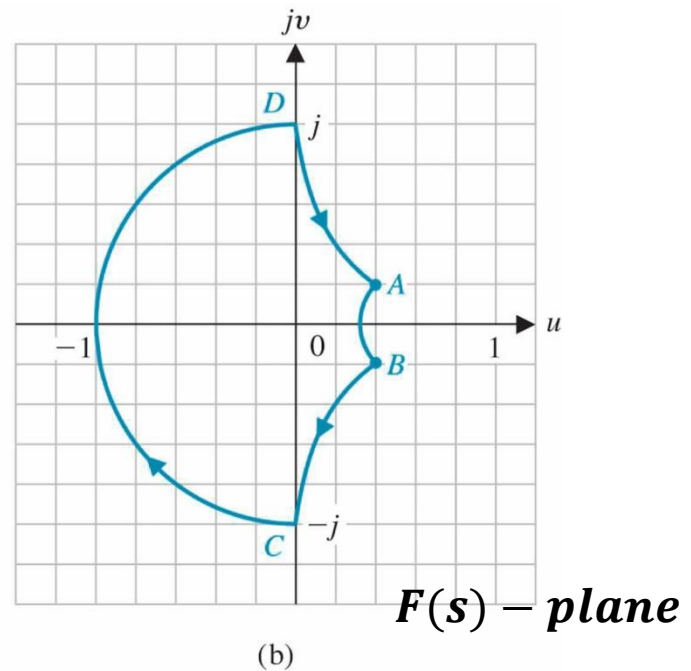
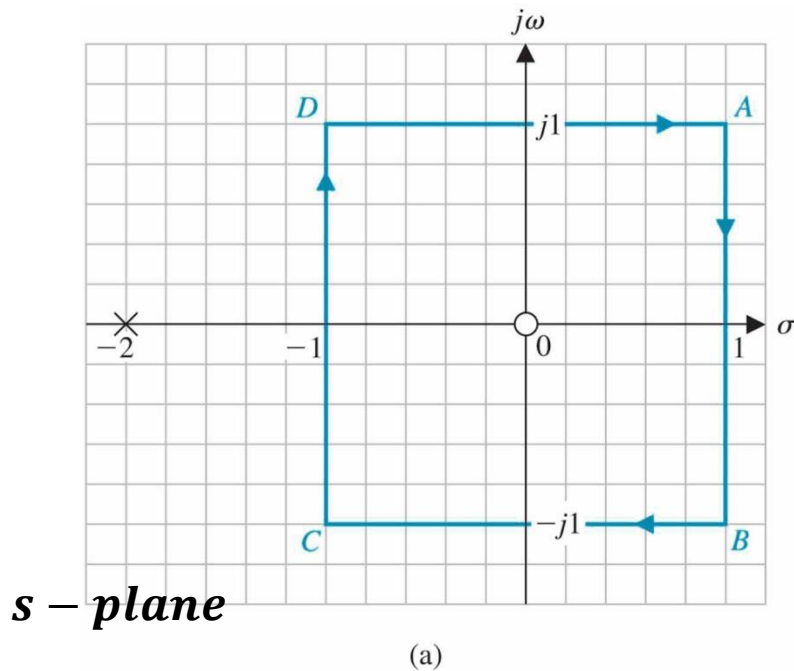
- *example*

$$F(s) = \frac{s}{(s + 2)}$$

$$Z = 1, P = 0$$

\Rightarrow

$$N = Z - P = +1$$



- The contour in the *F(s)* –plane encircles the origin of the *F(s)* –plane once in the clockwise direction

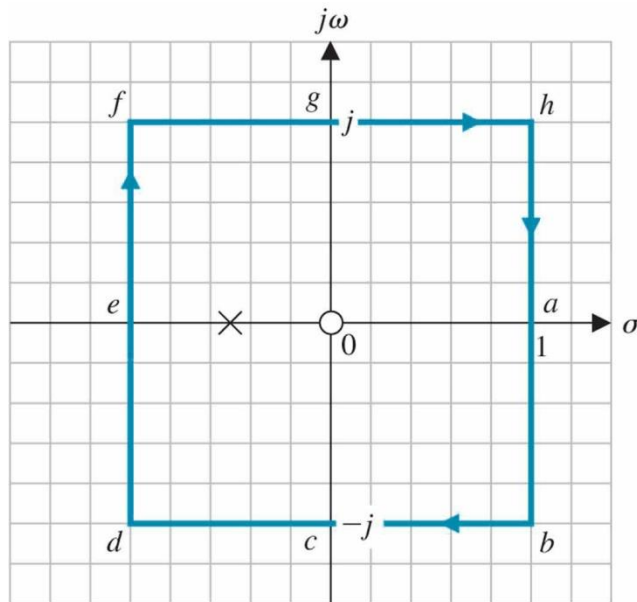
- *example*

$$F(s) = \frac{s}{(s + 0.5)}$$

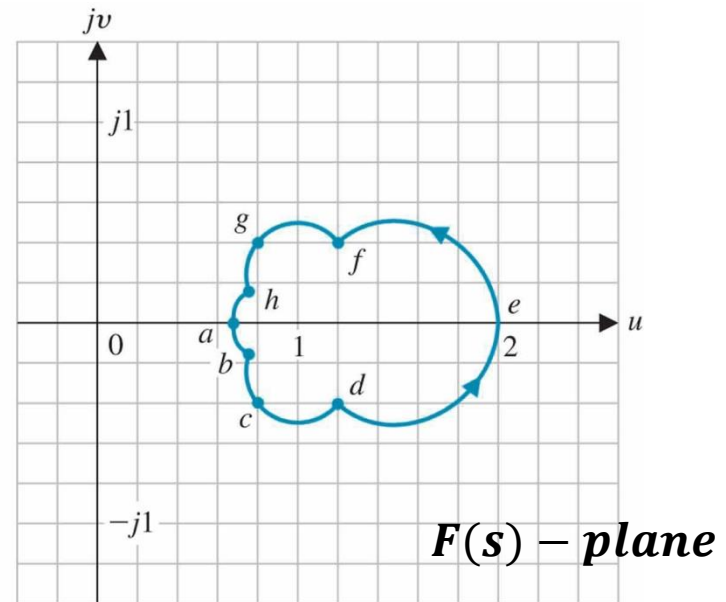
$$Z = 1, P = 1$$

\Rightarrow

$$N = Z - P = 0$$



s – plane (a)

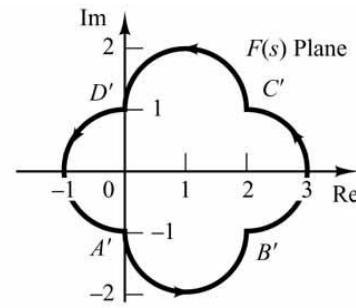
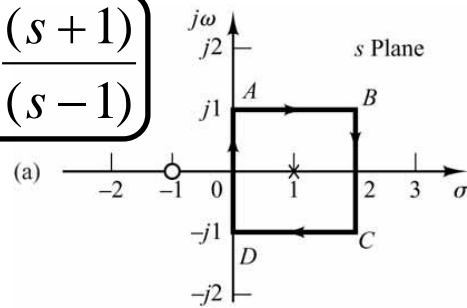


(b)

The contour in the $F(s)$ – plane does not encircle the origin of the $F(s)$ – plane

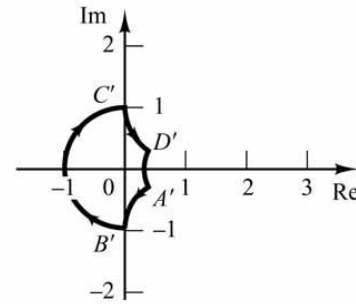
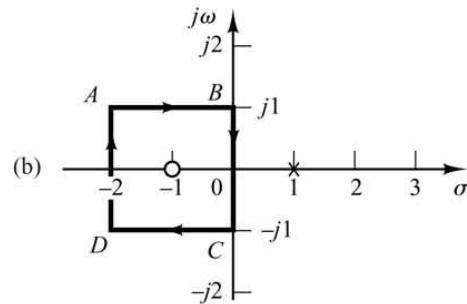
• **example**

$$F(s) = \frac{(s+1)}{(s-1)}$$



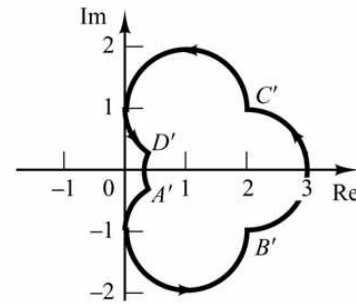
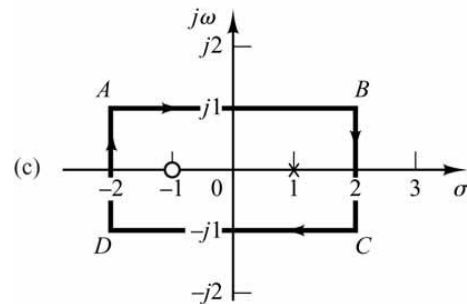
$$N = Z - P = -1$$

• **$P = 1, Z = 0$**



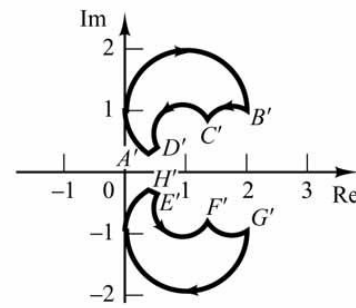
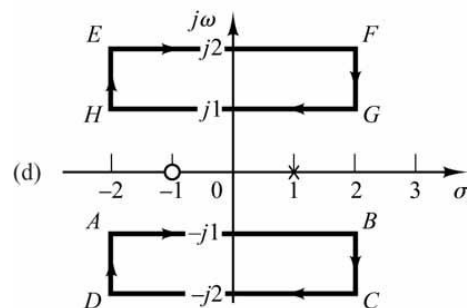
$$N = Z - P = 1$$

• **$P = 0, Z = 1$**



$$N = Z - P = 0$$

• **$P = 1, Z = 1$**

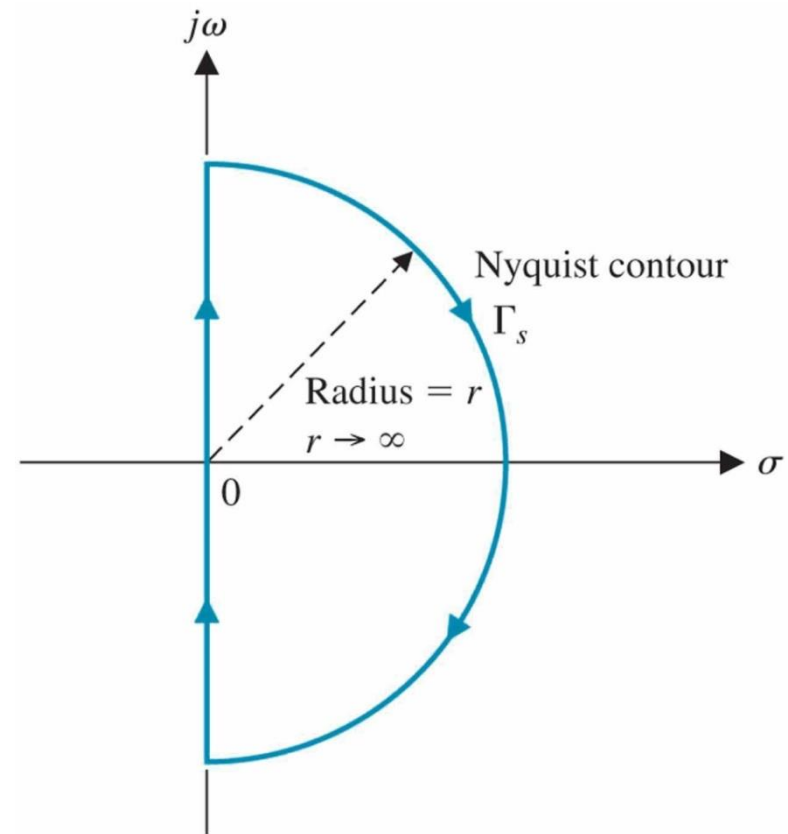


$$N = Z - P = 0$$

• **$P = 0, Z = 0$**

The Nyquist Stability Criterion

- To ensure stability, we must ascertain that all the **zeros** of the characteristic equation $F(s) = 1 + G(s)H(s)$ would lie in the **left-half-plane (LHP)** of the s-plane, i.e., the left of the $j\omega$ – axis.
- Nyquist chose the contour Γ_s in the s-plane that **encloses the entire right-half s-plane (RHP)**.
- Use Cauchy's theorem to determine if there are any zeros of $F(s)$ that would lie within Γ_s .
- Plot Γ_F in the $F(s)$ -plane and determine the number of encirclements of the **origin** N
- Nyquist plot is a **POLAR** plot



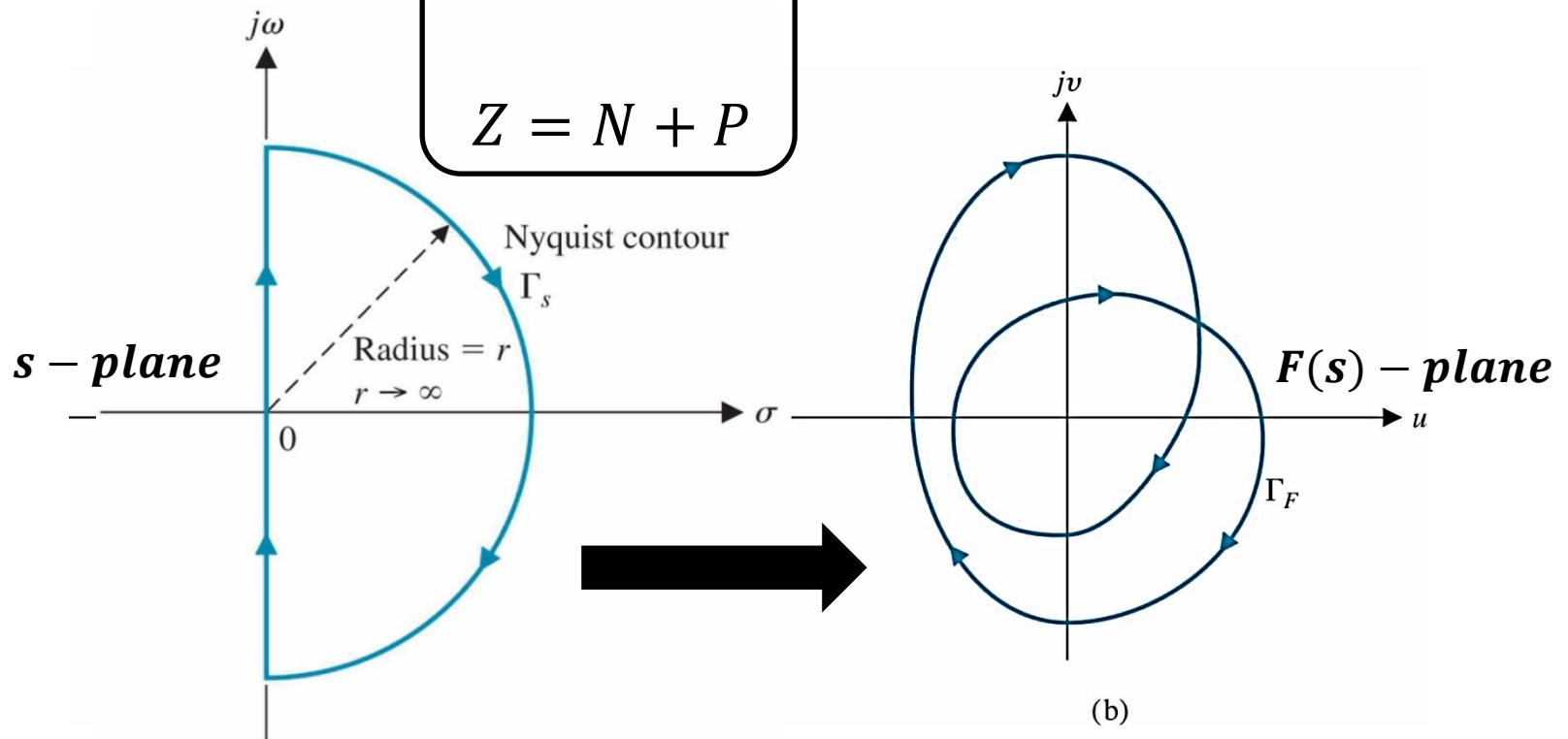
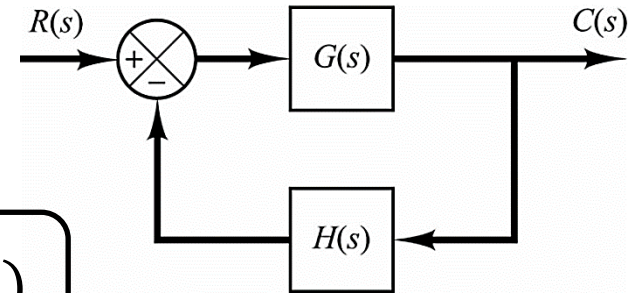
The Nyquist Stability Criterion

- Characteristic equation $F(s)$ of the system

$$F(s) = 1 + G(s)H(s)$$

$$N = Z - P$$

$$Z = N + P$$



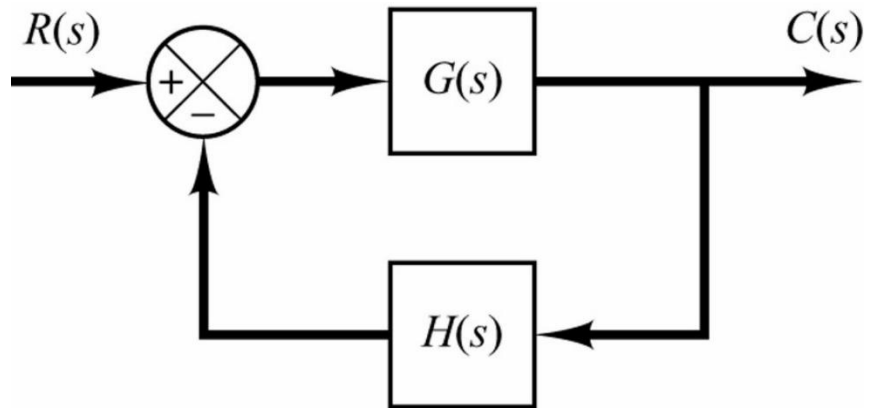
The Nyquist Stability Criterion

- In order to determine the stability of a closed-loop system we must investigate the **characteristic equation** $F(s)$ of the system

- $$F(s) = 1 + G(s)H(s)$$

$$N = Z - P$$

$$Z = N + P$$



- ✓ Z = number of **zeros** of $1 + G(s)H(s)$ in the **right-half s -plane**

- P = number of **poles** of $1 + G(s)H(s)$ in the **right-half s -plane !!**

- N = number of **clockwise** encirclement of the origin in the $F(s)$ -plane

- Then, the number of zeros of the **characteristic equation** $F(s)$ in the **RHP** $Z = N + P$

- Note that, $P = \text{the number of OPEN - LOOP poles in the RHP}$

WHY?

$$F(s) = 1 + G(s)H(s)$$

$$G(s)H(s) = \frac{N(s)}{D(s)}$$

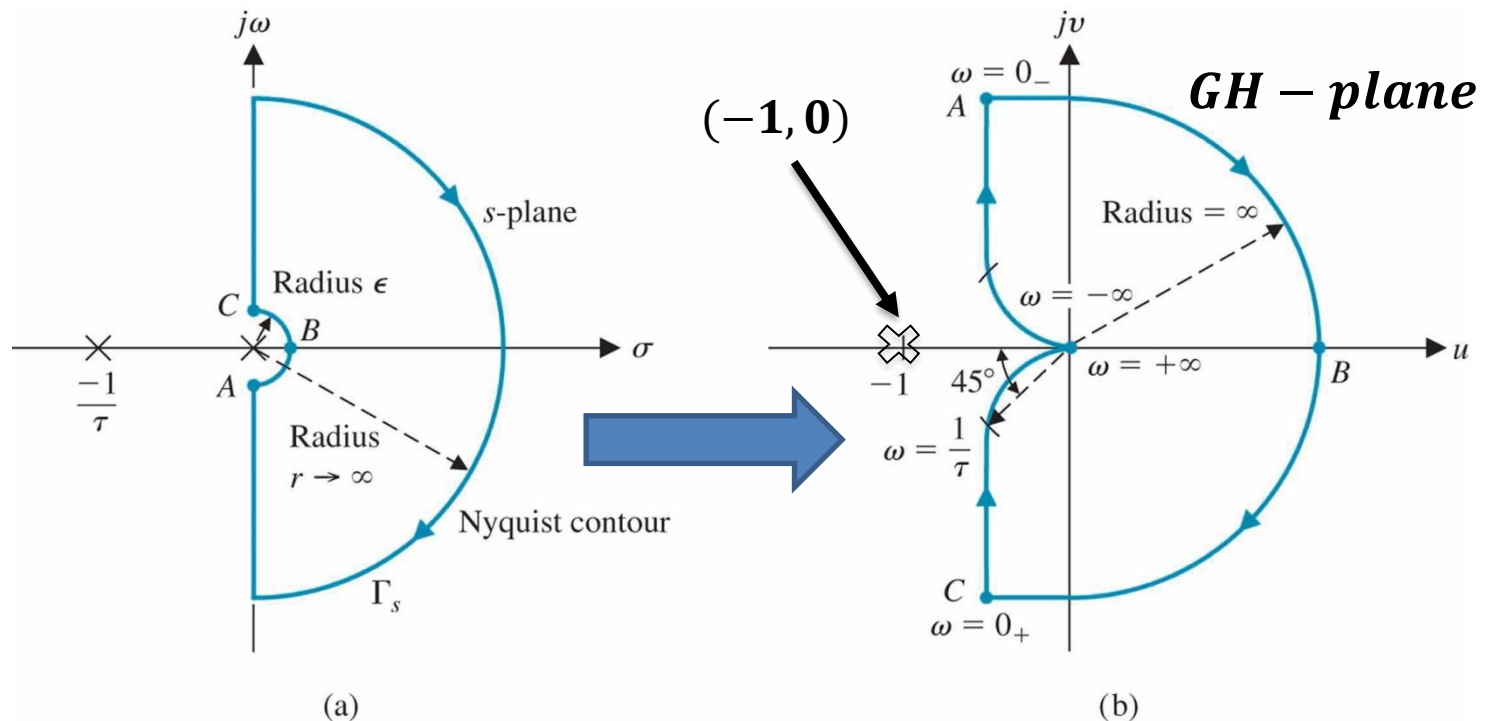
$$F(s) = 1 + \frac{N(s)}{D(s)} = \frac{D(s) + N(s)}{D(s)}$$

- P : OPEN-LOOP POLES** (*poles of $G(s)H(s)$*)
 - Case 1: $P = 0 \Rightarrow Z = N$
 - Case 2: $P \neq 0 \Rightarrow Z = N + P$
- Z : CHARACTERISTIC EQUATION ZEROS** (*roots of $1 + G(s)H(s)$*)

- Because $G(s)H(s)$ is typically available in factored form, consider

Mapping function	Plane	Encirclement
$F(s) = 1 + G(s)H(s)$	$1 + G(s)H(s)$	$(0, 0)$
$F(s) - 1 = G(s)H(s)$	$G(s)H(s)$	$(-1, 0)$

- The number of **clockwise encirclements** of the origin of the $F(s)$ -plane becomes the number of **clockwise encirclements** of the $(-1, 0)$ point in the $G(s)H(s)$ -plane.



The Nyquist Stability Criterion

Case 1

$L(S) = G(s)H(s)$ has no open-loop poles in the RHP, ($P = 0$)

“A feedback system is stable if and only if the contour Γ_L in the $G(s)H(s)$ -plane **DOES NOT** encircle the $(-1, 0)$ point when the number of poles of $L(s)$ in the RHP is zero ($P = 0$)”

$$Z = N + P = N$$

$$\therefore Z = 0$$

$$\Rightarrow N = 0$$

- For no zeros of the characteristic equation on the RHP, then there should be no encirclement of the point -1 in the $L(s)$ plane

- example**

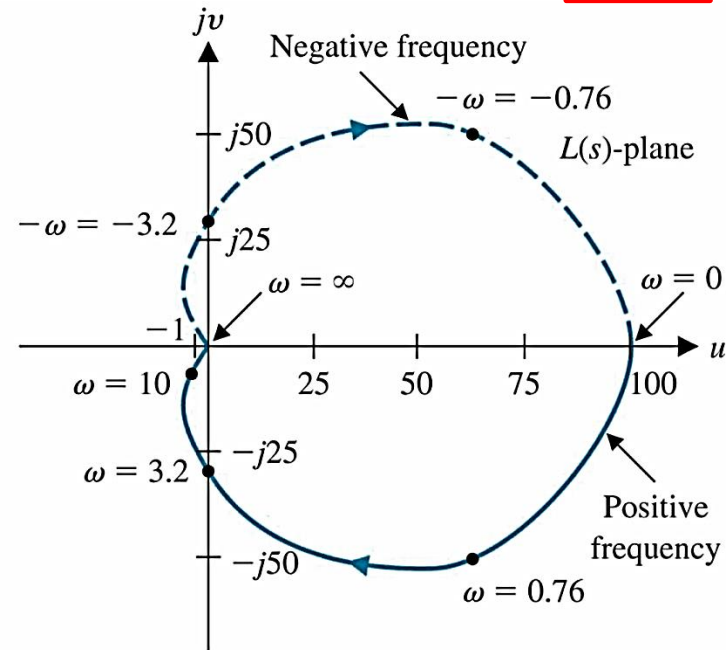
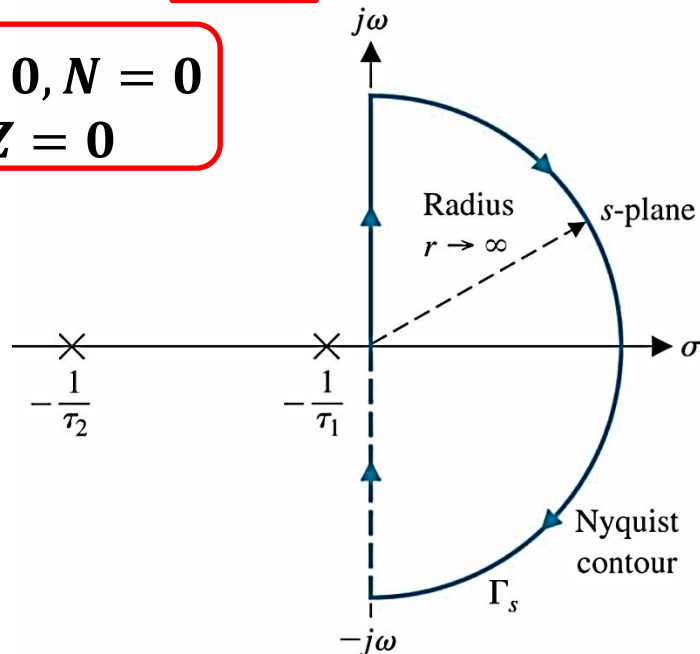
$$L(s) = \frac{K}{(\tau_1 s + 1)(\tau_2 s + 1)} = \frac{100}{(s + 1)(0.1s + 1)}$$

Table 9.2 Magnitude and Phase of $L(j\omega)$

ω	0	0.1	0.76	1	2	10	20	100	∞
$ L(j\omega) $	100	96	79.6	70.7	50.2	6.8	2.24	0.10	0
$\angle L(j\omega)$ (degrees)	0	-5.7	-41.5	-50.7	-74.7	-129.3	-150.5	-173.7	-180

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$$P = 0, N = 0 \\ \Rightarrow Z = 0$$



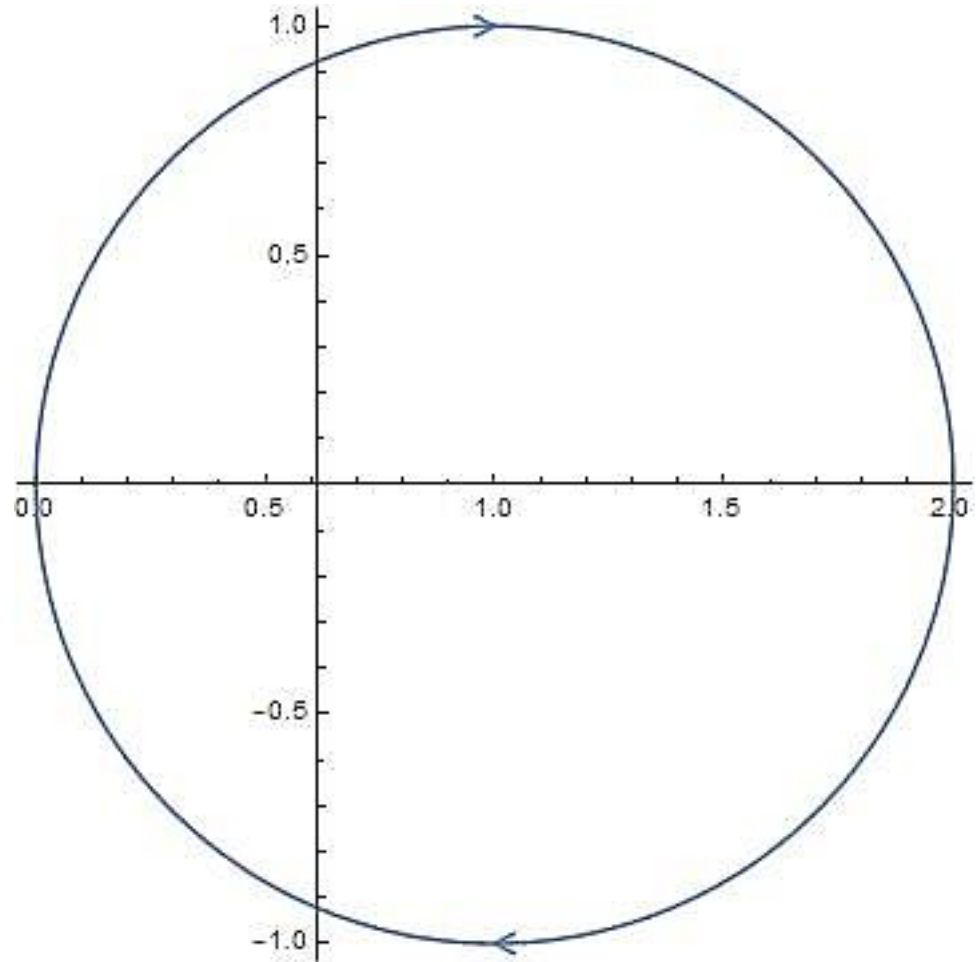
- The system is **always stable for all values of $K \geq 0$, (why?)**

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$$G(s) = 10/(s + 5)$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	+2
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0\angle -90^\circ$

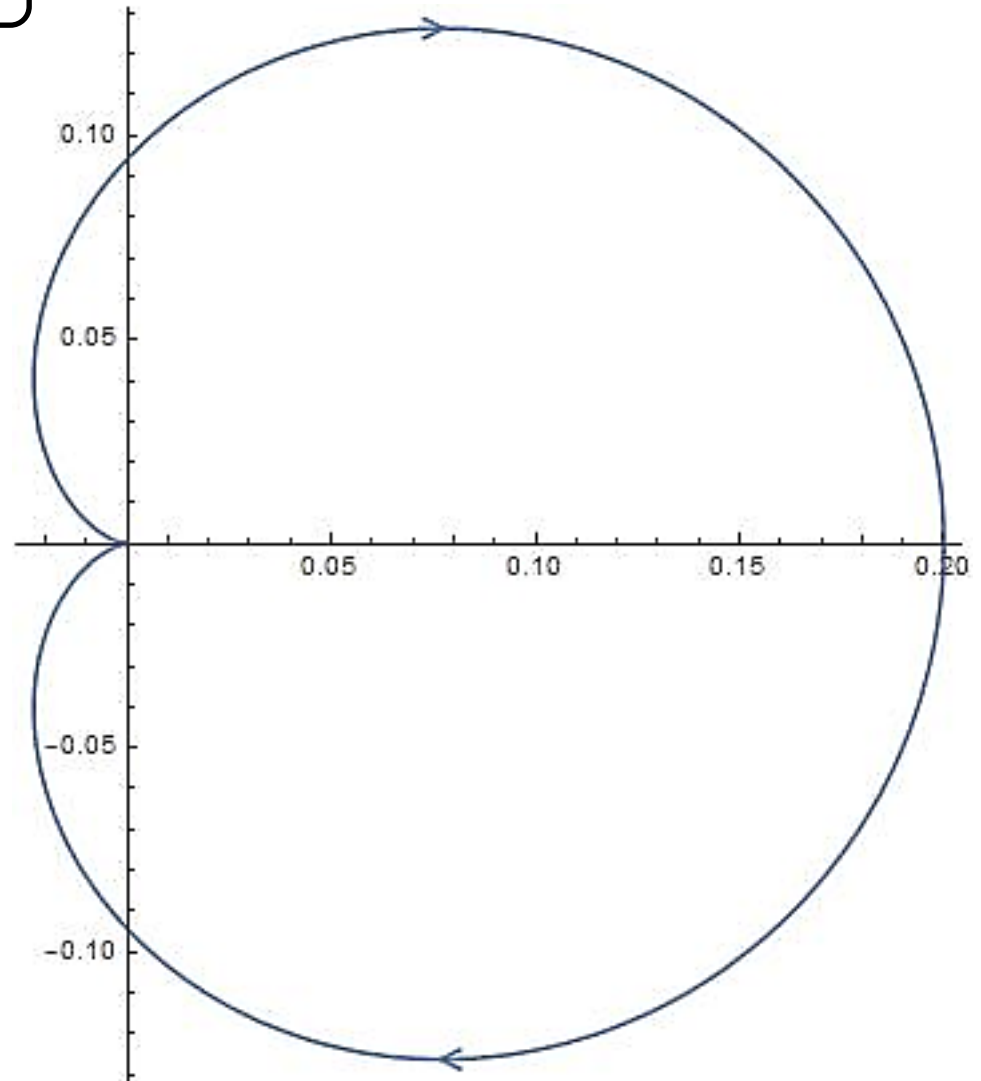
$$P = 0, N = 0 \Rightarrow Z = 0 \text{ (stable)}$$



$$G(s) = 10/(s + 10)(s + 5)$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	+0.2
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -180^\circ$

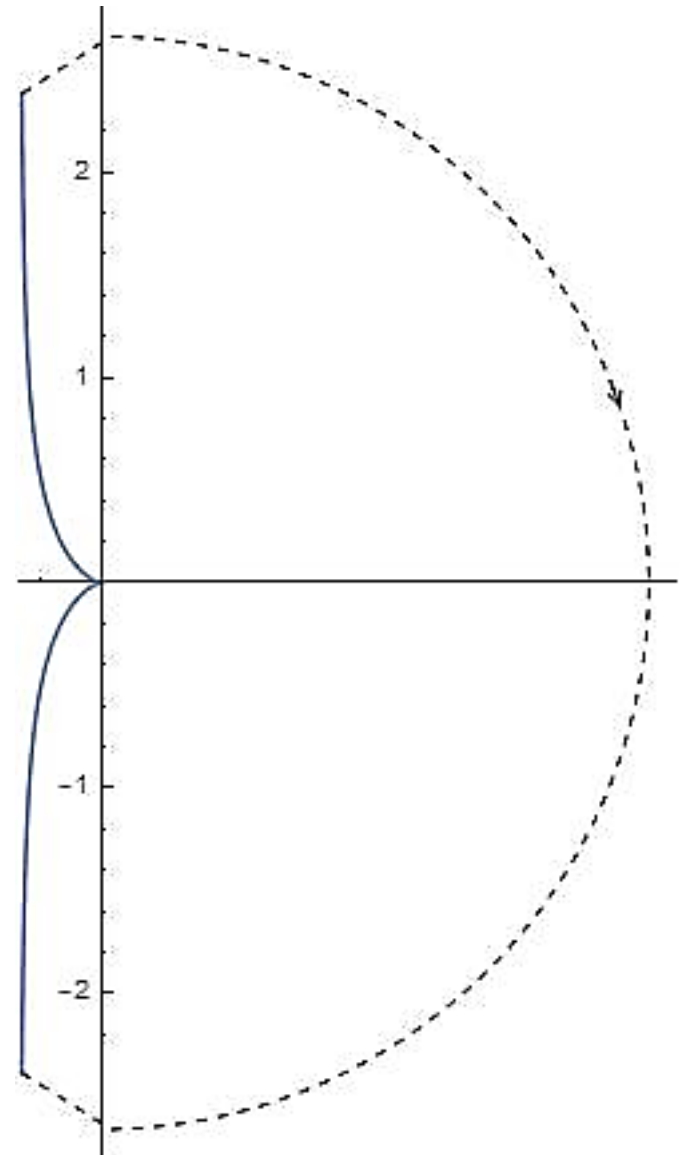
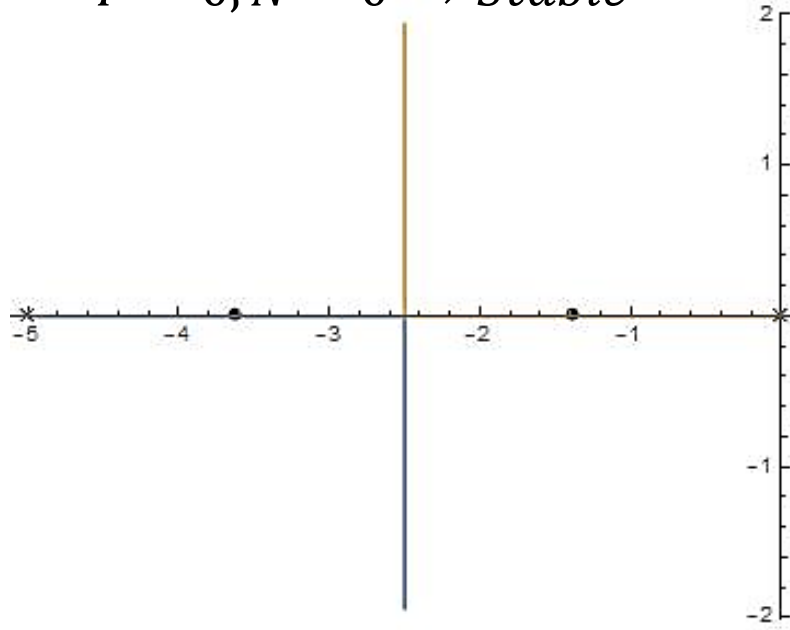
$P = 0, N = 0 \Rightarrow$
System is always stable



$$G(s) = 10/s(s + 5)$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	$\infty \angle -90^\circ$
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -180^\circ$

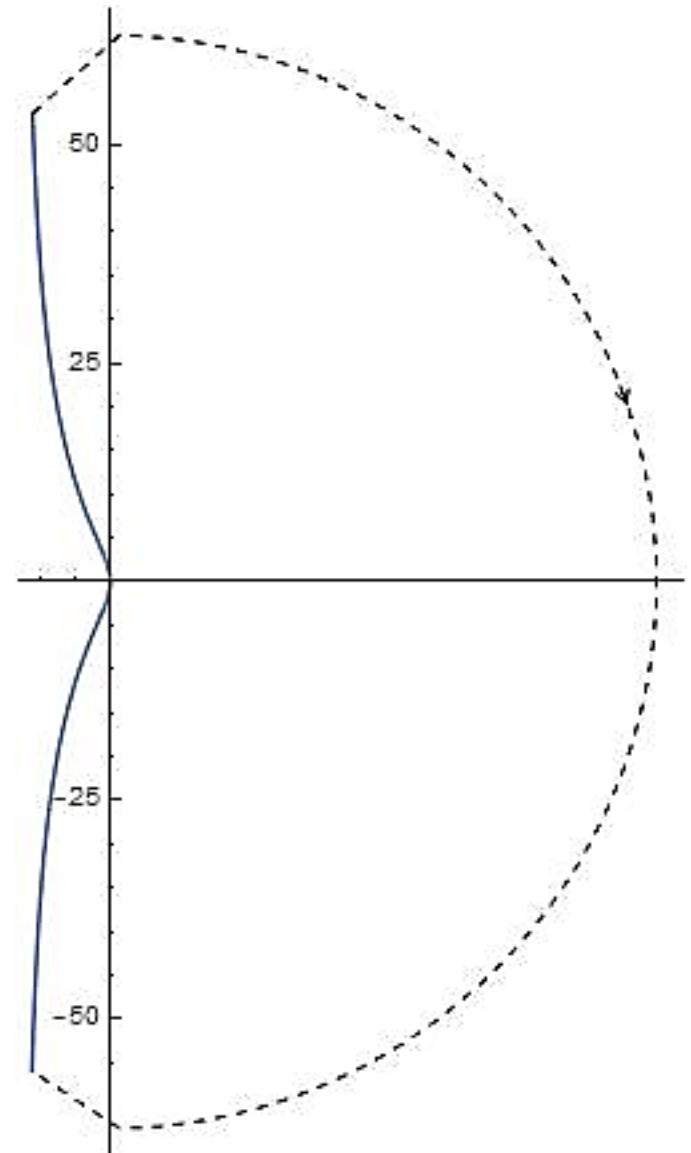
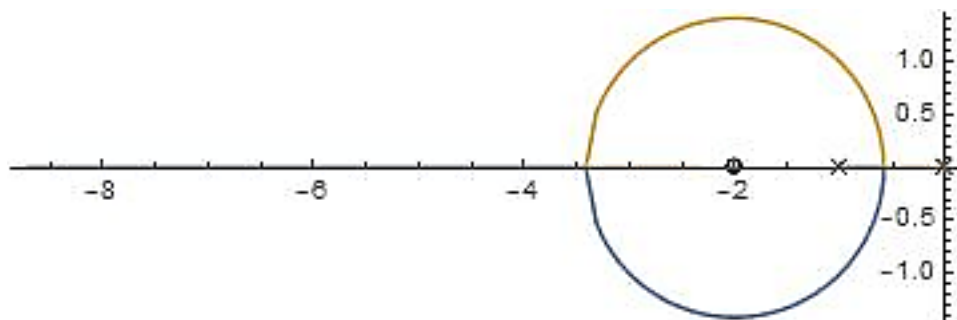
- $P = 0, N = 0 \Rightarrow \text{Stable}$



$$G(s) = 10(s + 2)/s(s + 1)$$

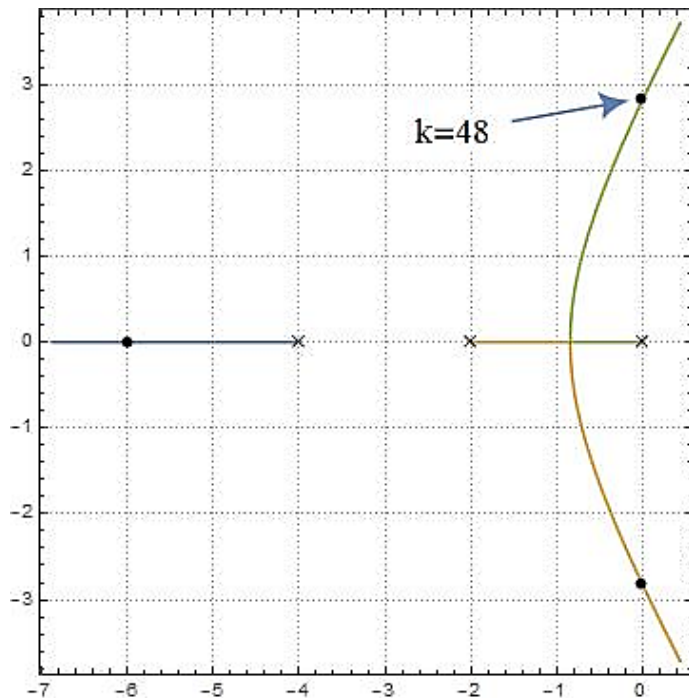
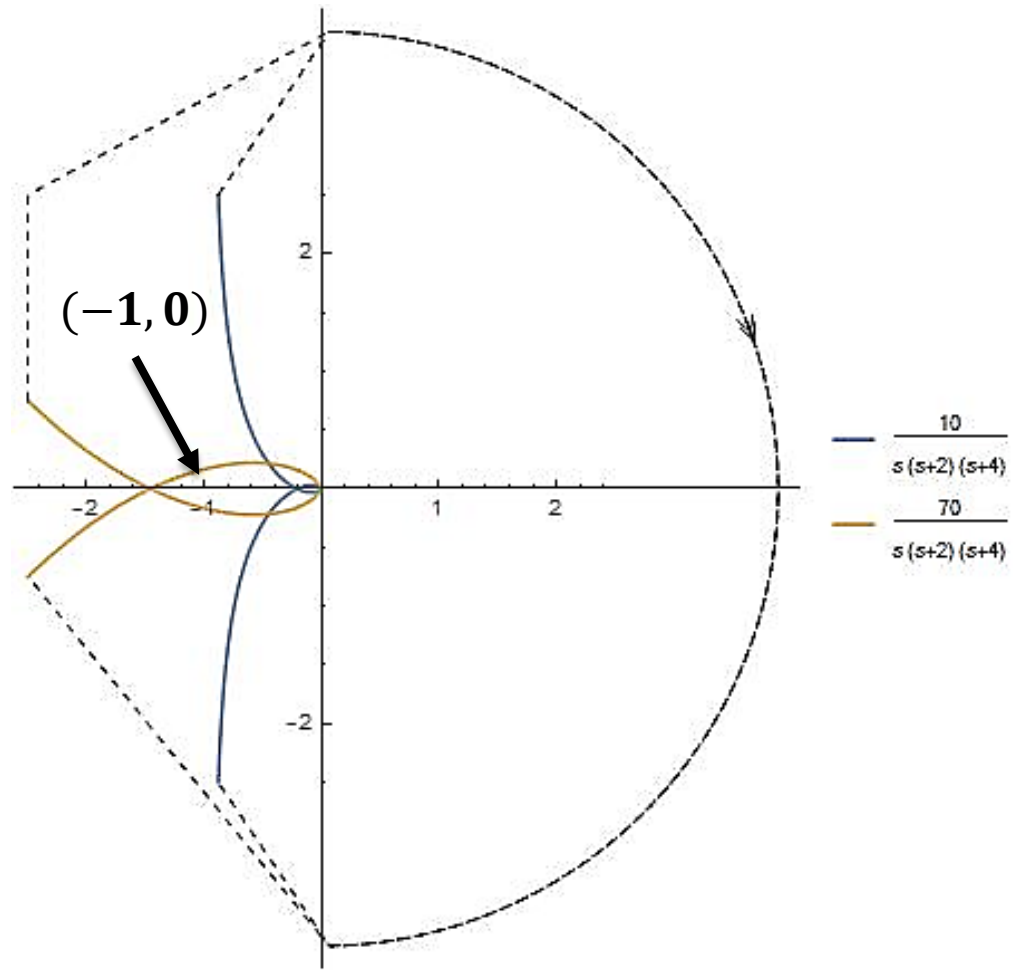
$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	$\infty \angle -90^\circ$
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -90^\circ$

- $N = 0, P = 0 \Rightarrow \text{Stable}$



$$G(s) = K/s(s + 2)(s + 4)$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	$\infty \angle -90^\circ$
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -270^\circ$



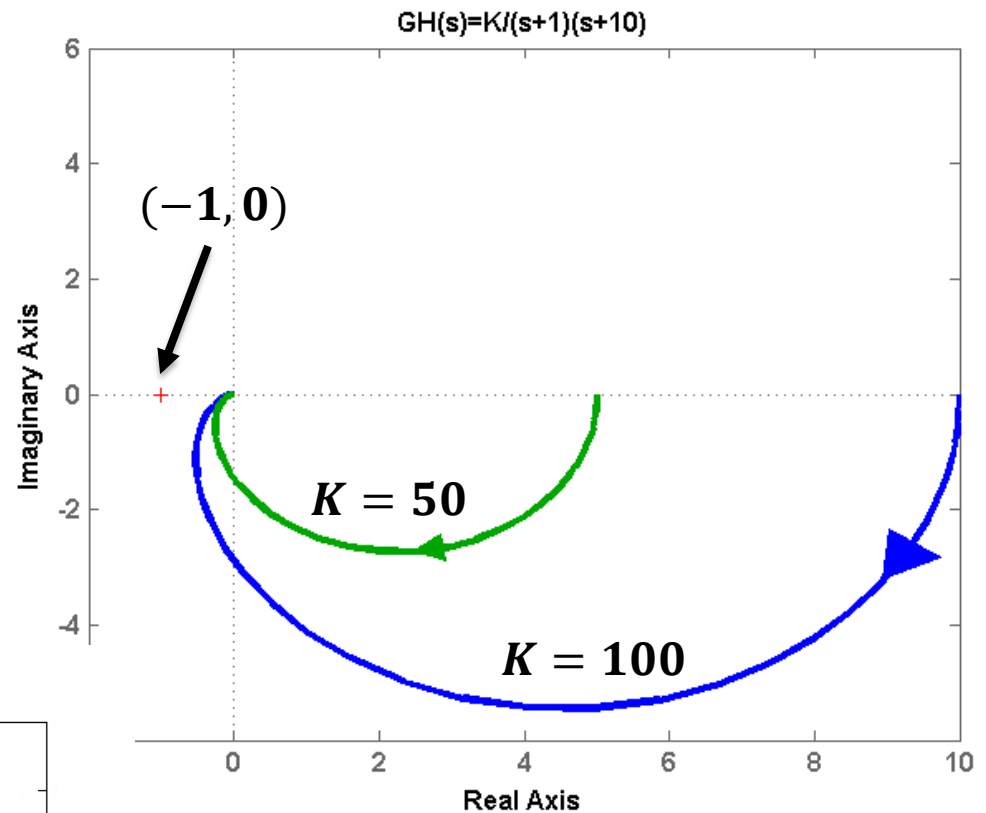
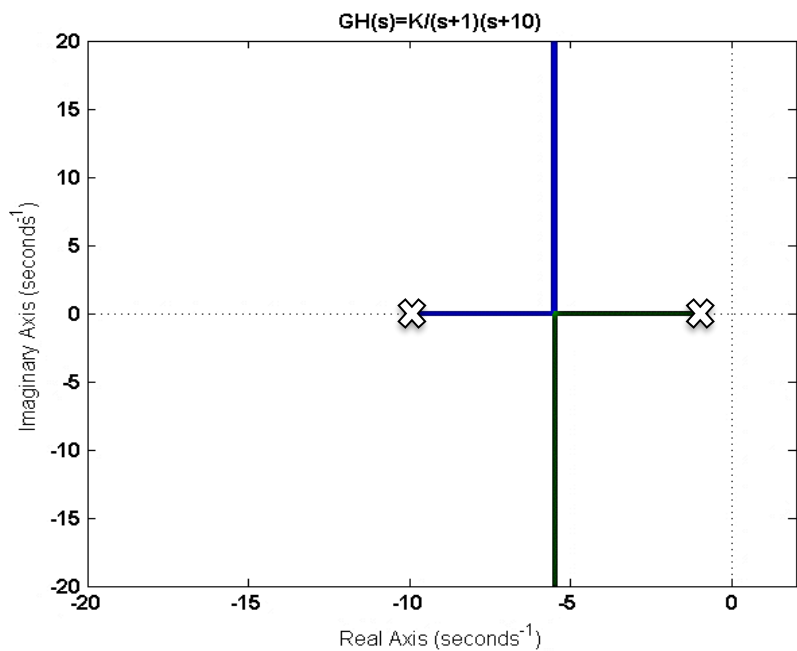
$$K = 10 \Rightarrow N = 0, P = 0 \Rightarrow Z = 0 (\text{Stable})$$

$$K = 70 \Rightarrow N = 2, P = 0 \Rightarrow Z = 2 (\text{unstable})$$

- example**

$$GH(s) = K/(s + 1)(s + 10)$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	$K/10$
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -180^\circ$

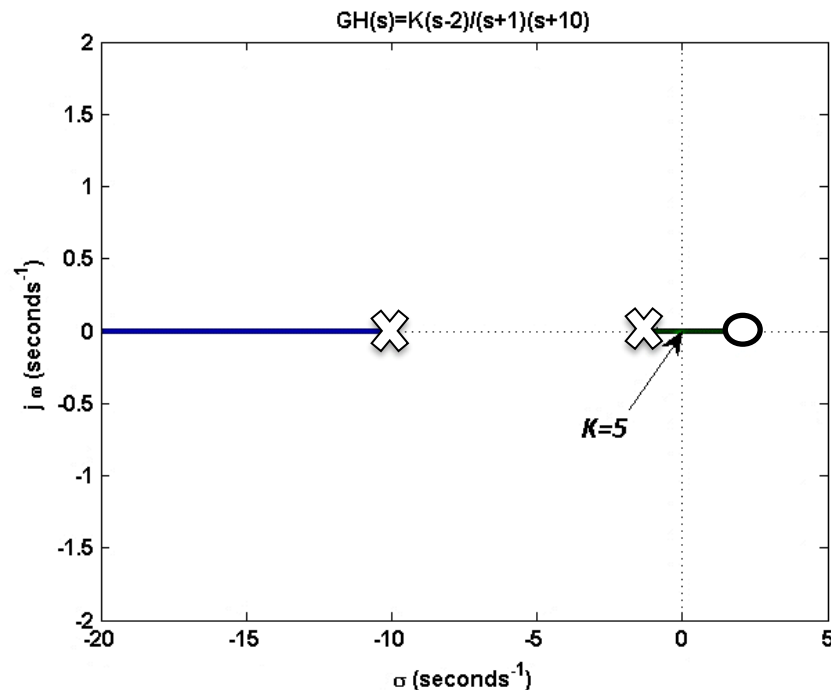
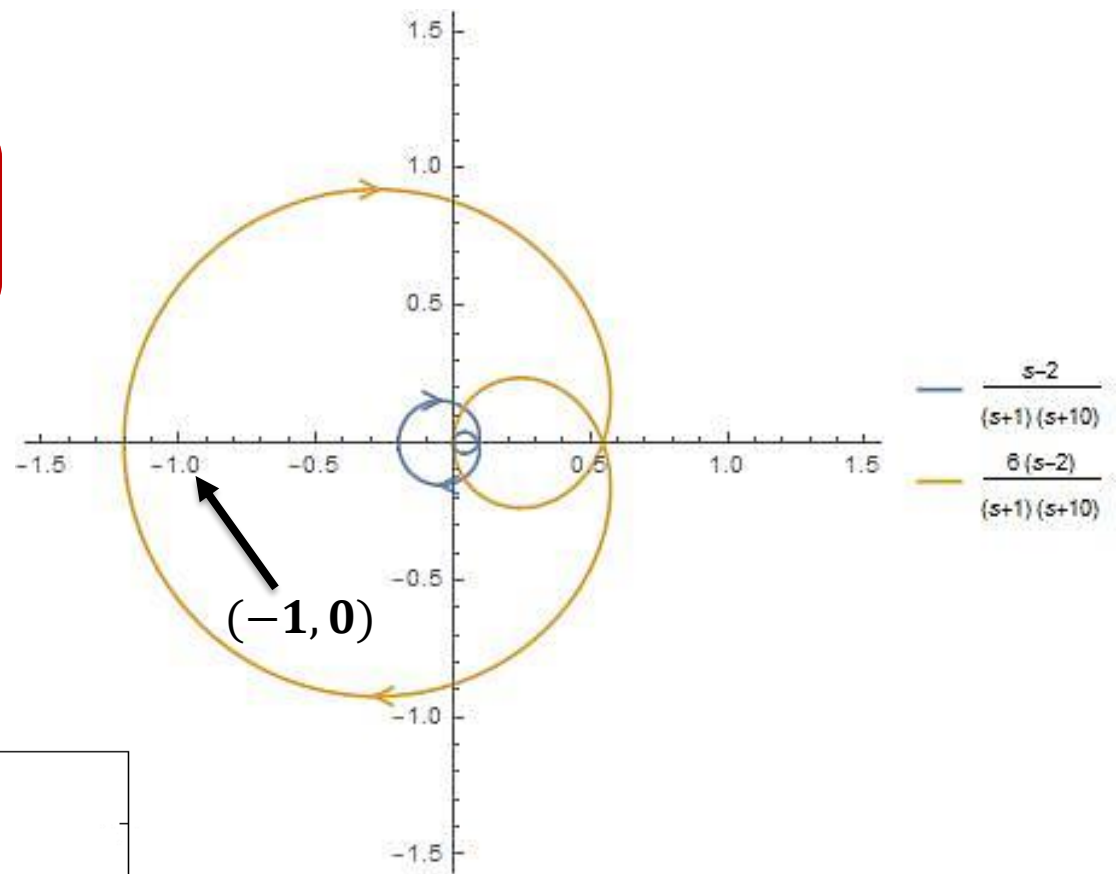


System is always stable for all values of K

- example

$$GH(s) = \frac{K(s-2)}{(s+1)(s+10)}$$

$j\omega$	$GH(j\omega)$
$\lim_{j\omega \rightarrow 0+} GH(s)$	$-0.2K$
$\lim_{j\omega \rightarrow +\infty} GH(s)$	$0 \angle -90^\circ$

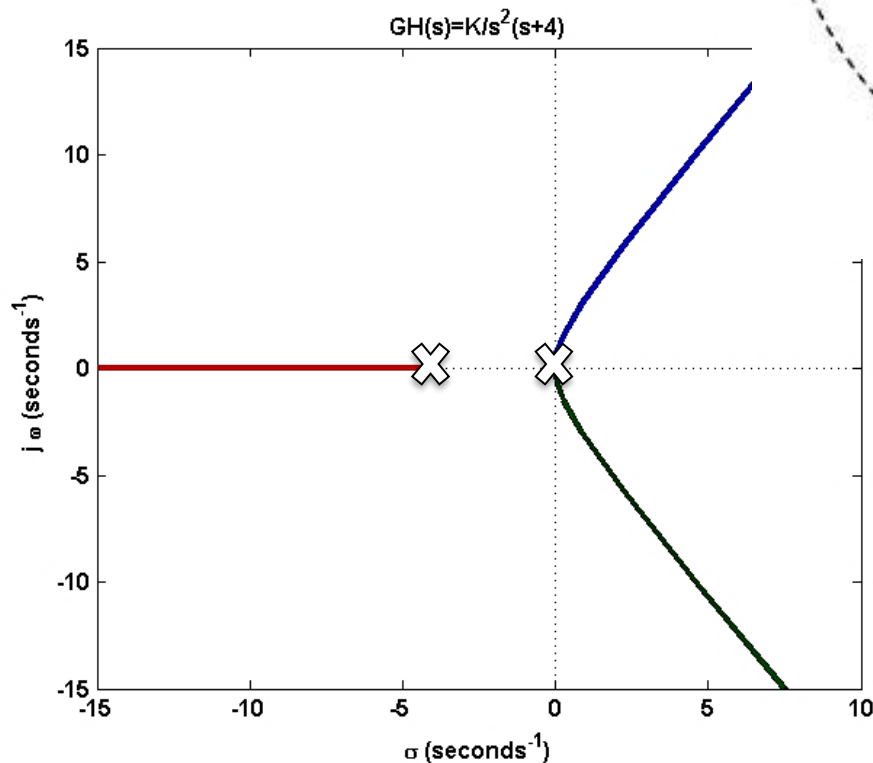
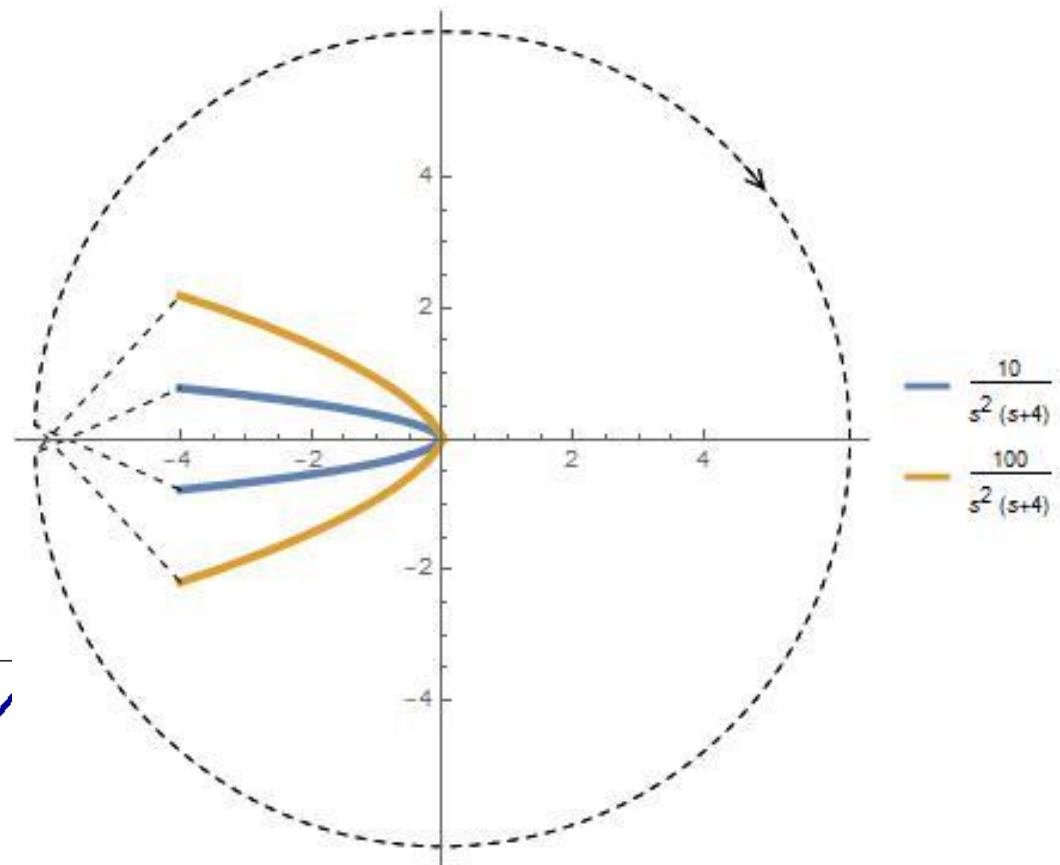


$K = 1 \Rightarrow N = 0, P = 0 \Rightarrow Z = 0$ (stable)

$K = 6 \Rightarrow N = 1, P = 0 \Rightarrow Z = 1$ (unstable)

- $GH(s) = K/s^2(s + 4)$

ω	$GH(j\omega)$
$j\omega \rightarrow 0_+$	$\infty \angle -180^\circ$
$j\omega \rightarrow +\infty$	$0 \angle -270^\circ$



The system is **always unstable**

$$K = 10 \Rightarrow N = 2, P = 0 \Rightarrow Z = 2(\text{unstable})$$

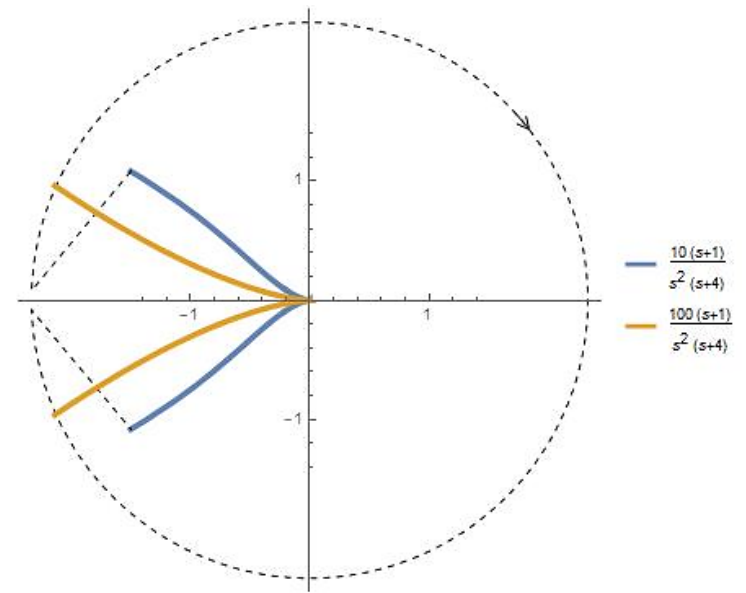
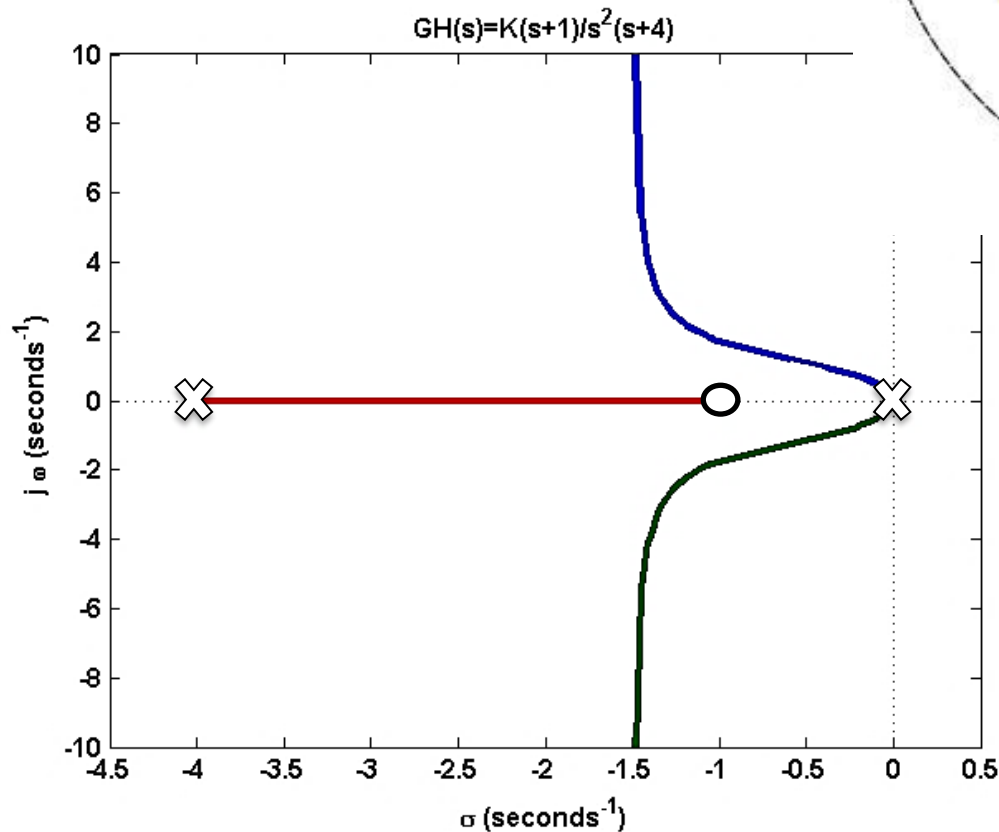
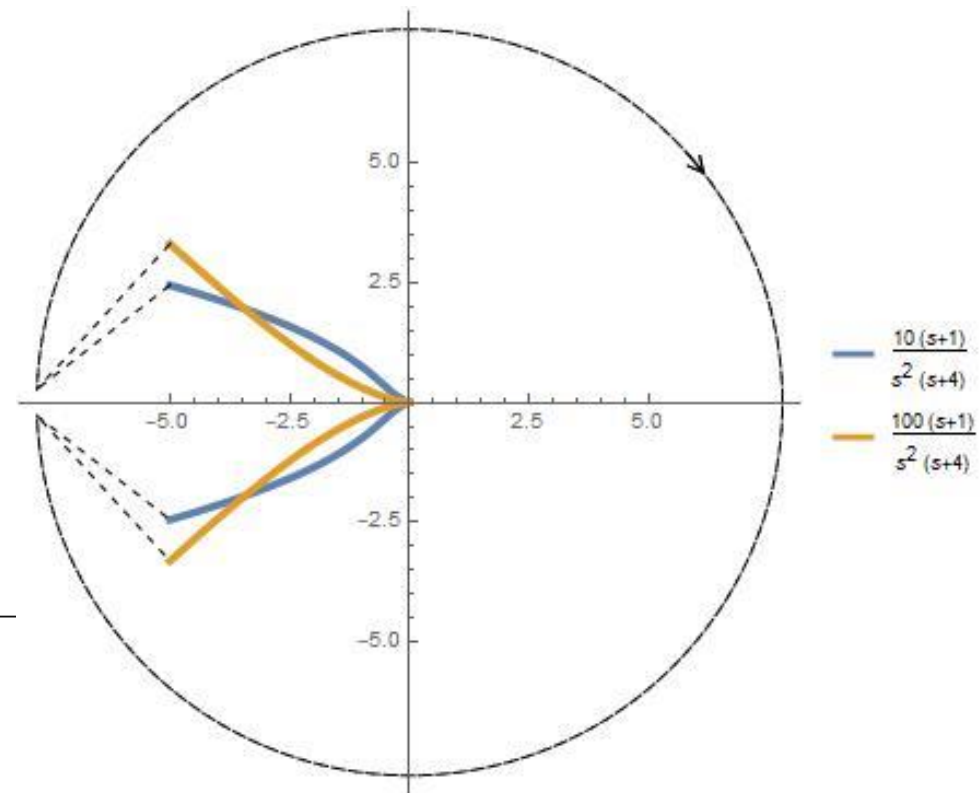
$$K = 100 \Rightarrow N = 2, P = 0 \Rightarrow Z = 2(\text{unstable})$$

- adding a **differentiator**

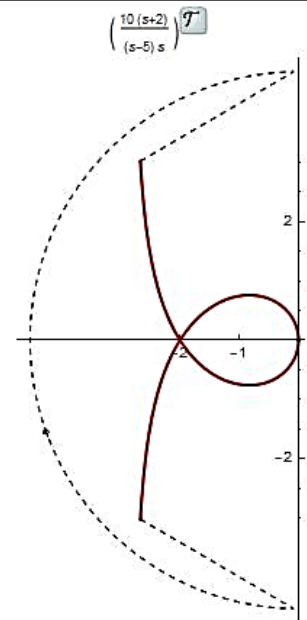
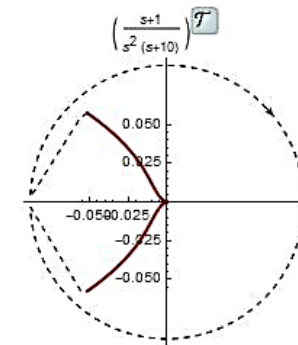
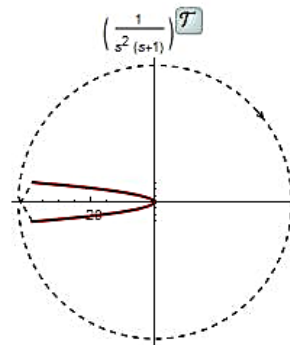
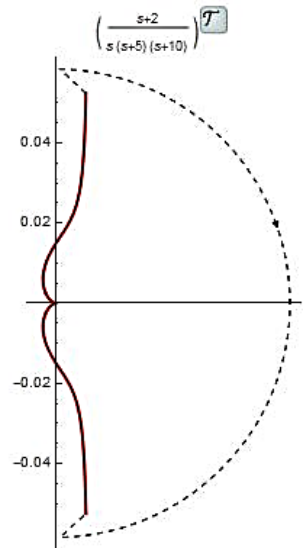
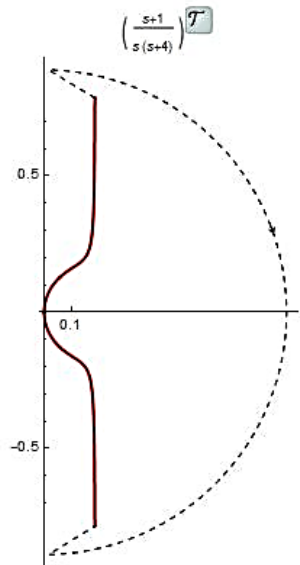
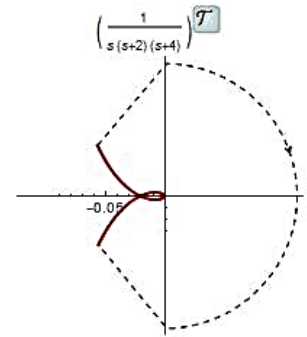
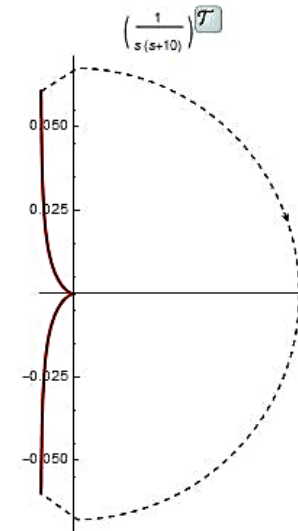
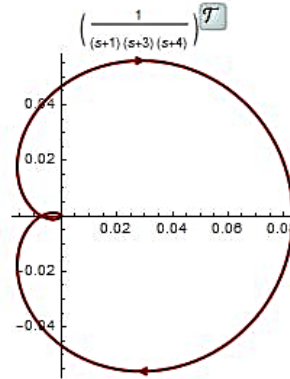
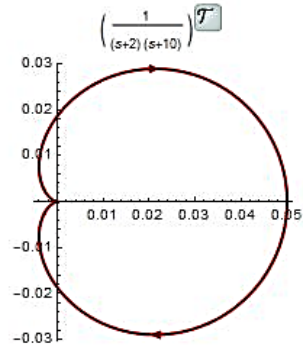
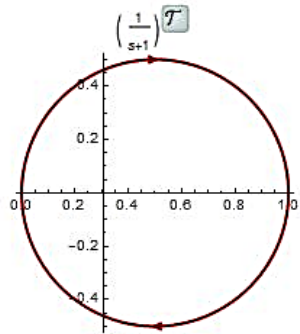
$$GH(s) = K(s + 1)/s^2(s + 4)$$

ω	$GH(j\omega)$
$j\omega \rightarrow 0_+$	$\infty \angle -\pi$
$j\omega \rightarrow +\infty$	$0 \angle -\pi$

- The system is **always stable**



Nyquist plot examples



Equivalent root locus plots

