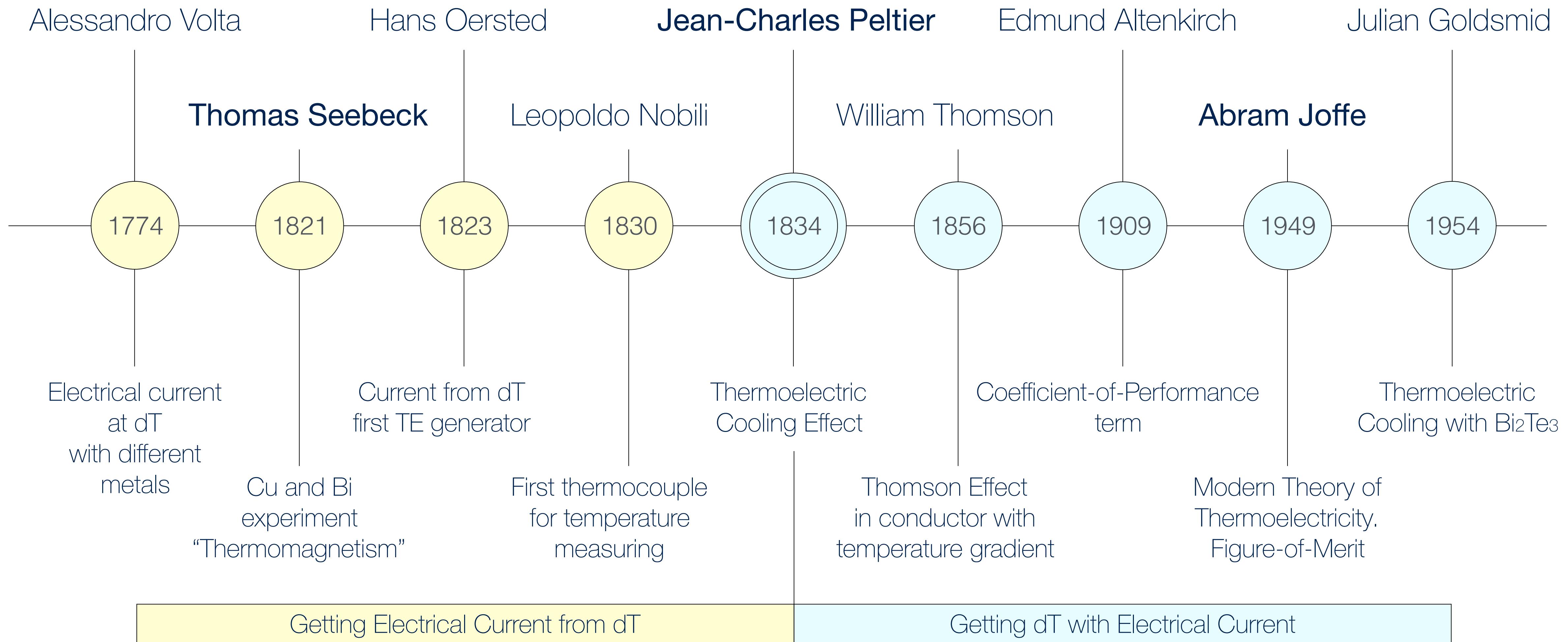


# Thermoelectric Coolers FAQ



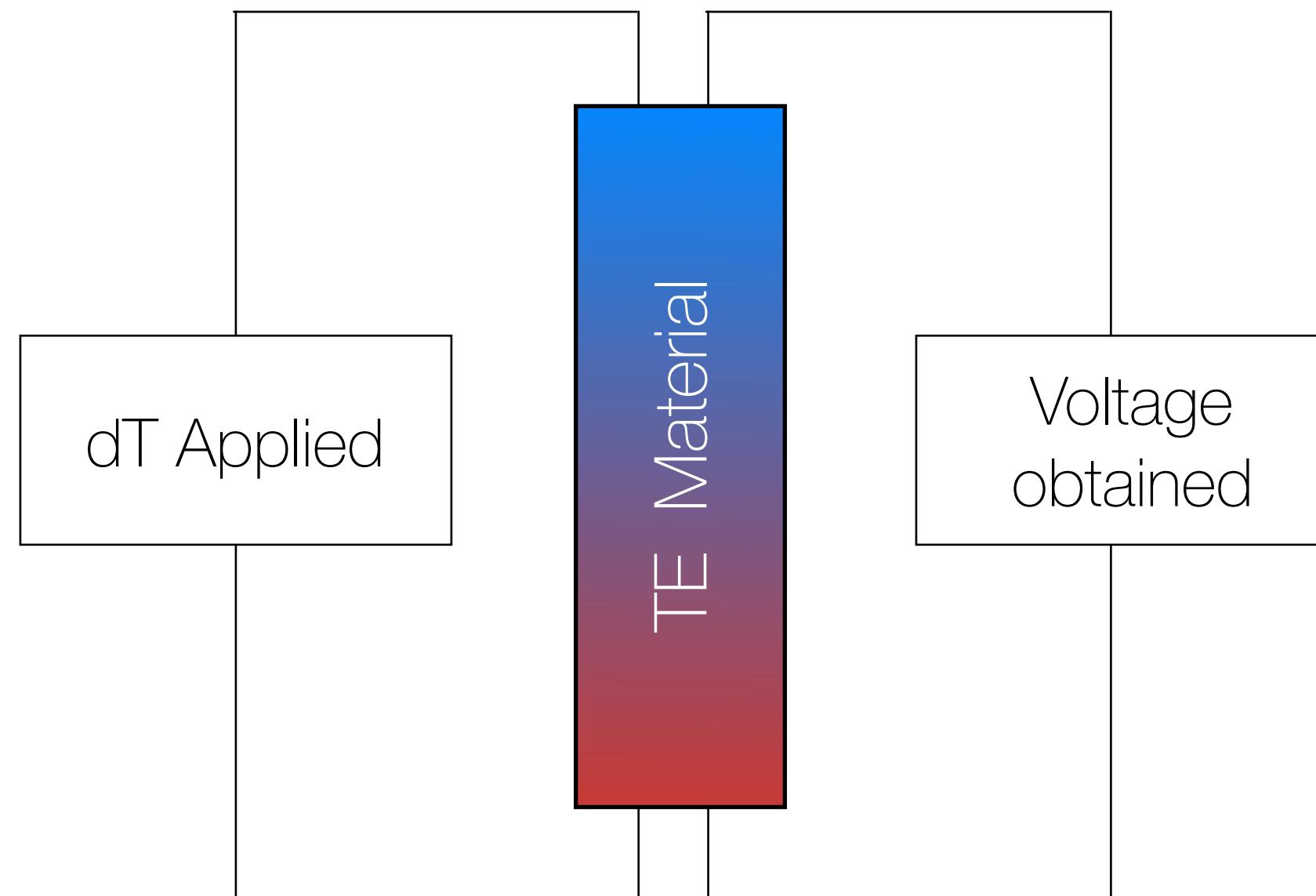
# Brief History of Thermoelectricity





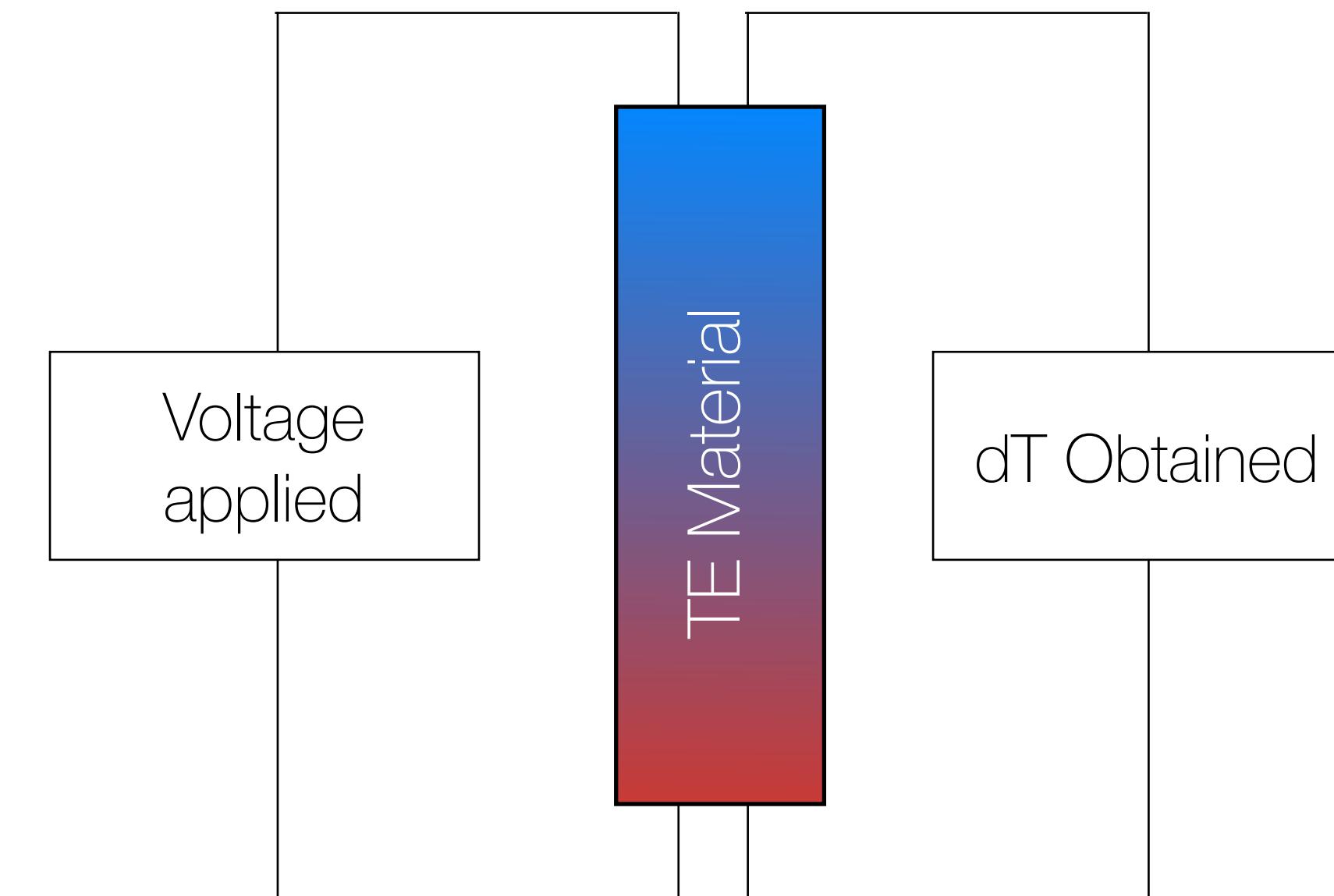
## How does it work - Thermoelectric Pellet

Seebeck Effect - TE Generating



Apply Temperature Difference (dT) to get Voltage

Peltier Effect - TE Cooling



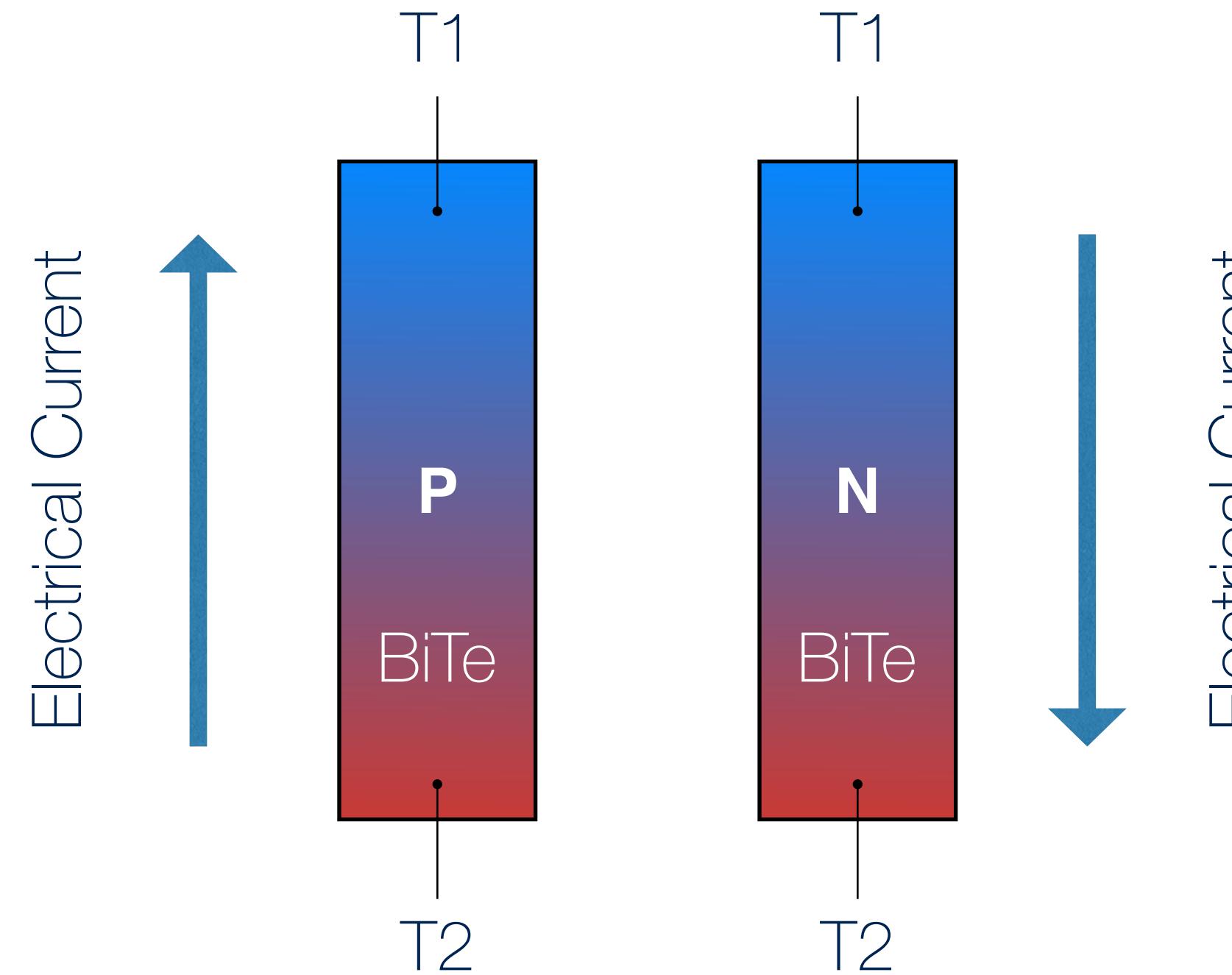
Apply Voltage to get Temperature Difference (dT)

BiTe Material is the most common for TE Coolers manufacturing

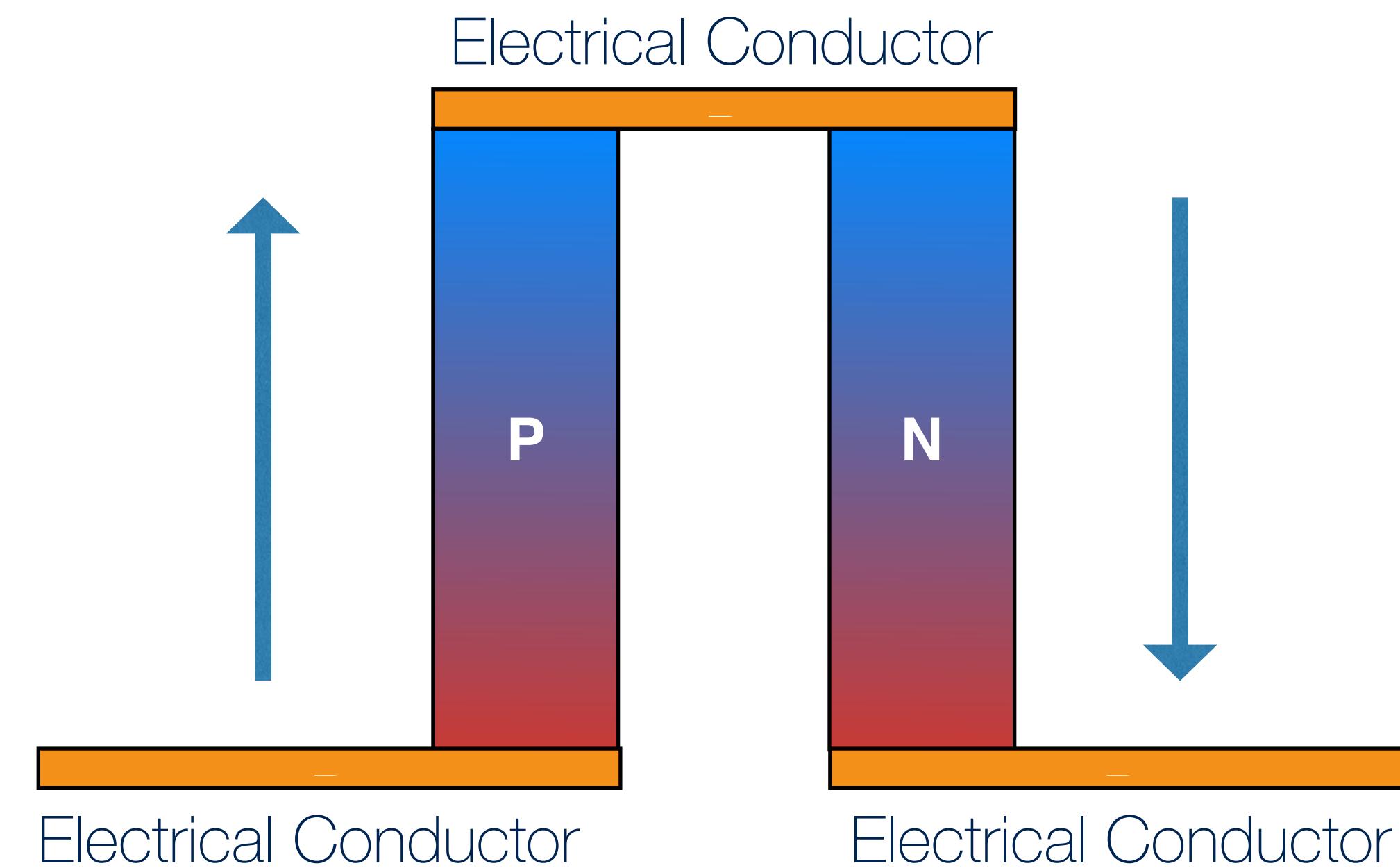


## How does it work - Thermoelectric Couple

### Understanding P and N pellet types



### Forming TE Couple

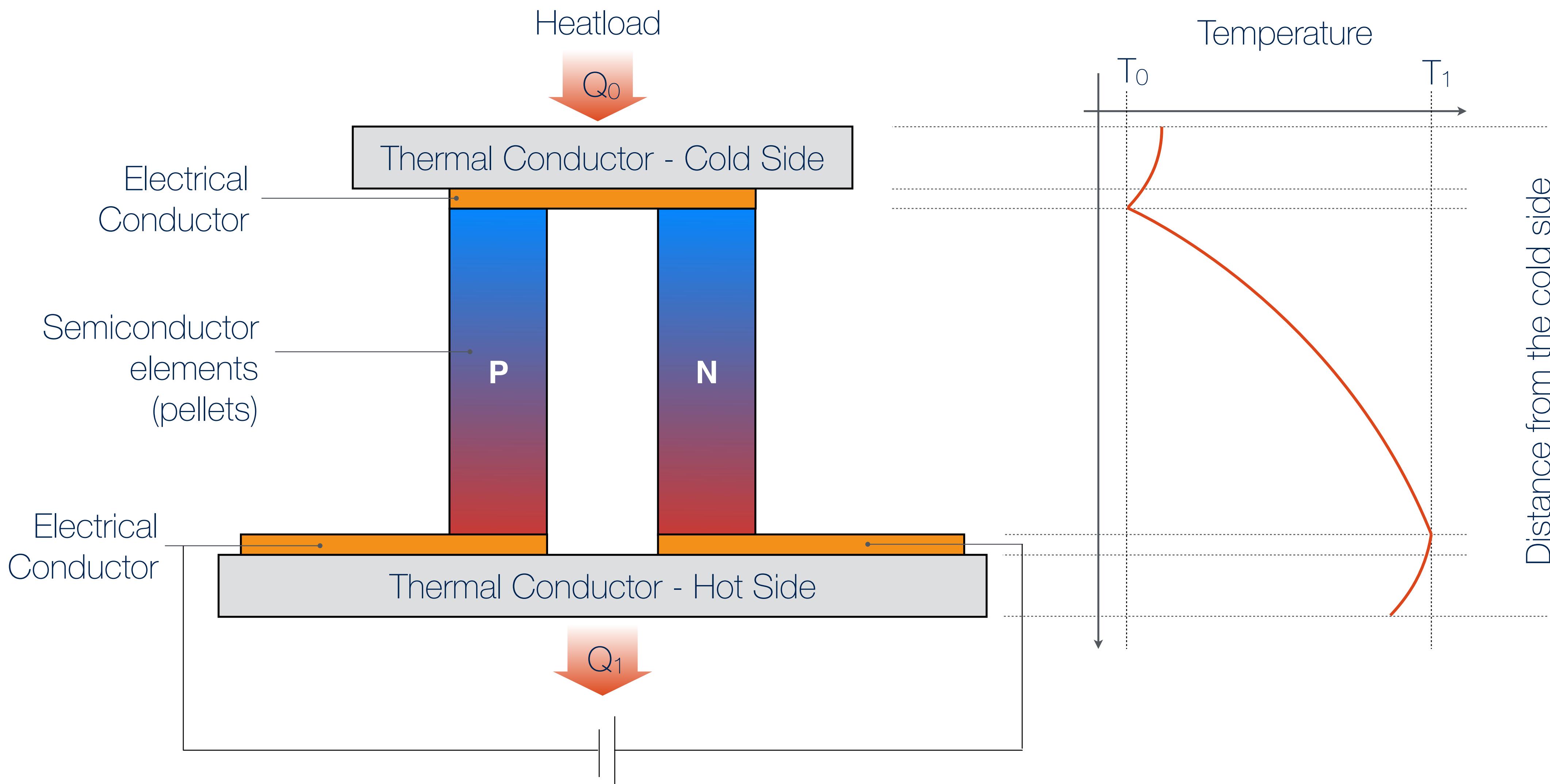


The difference between P and N pellets  
is in cold-hot side orientation under  
Electrical Current applied

P and N pellets form a thermoelectric  
couple - the core of TE cooler  
construction

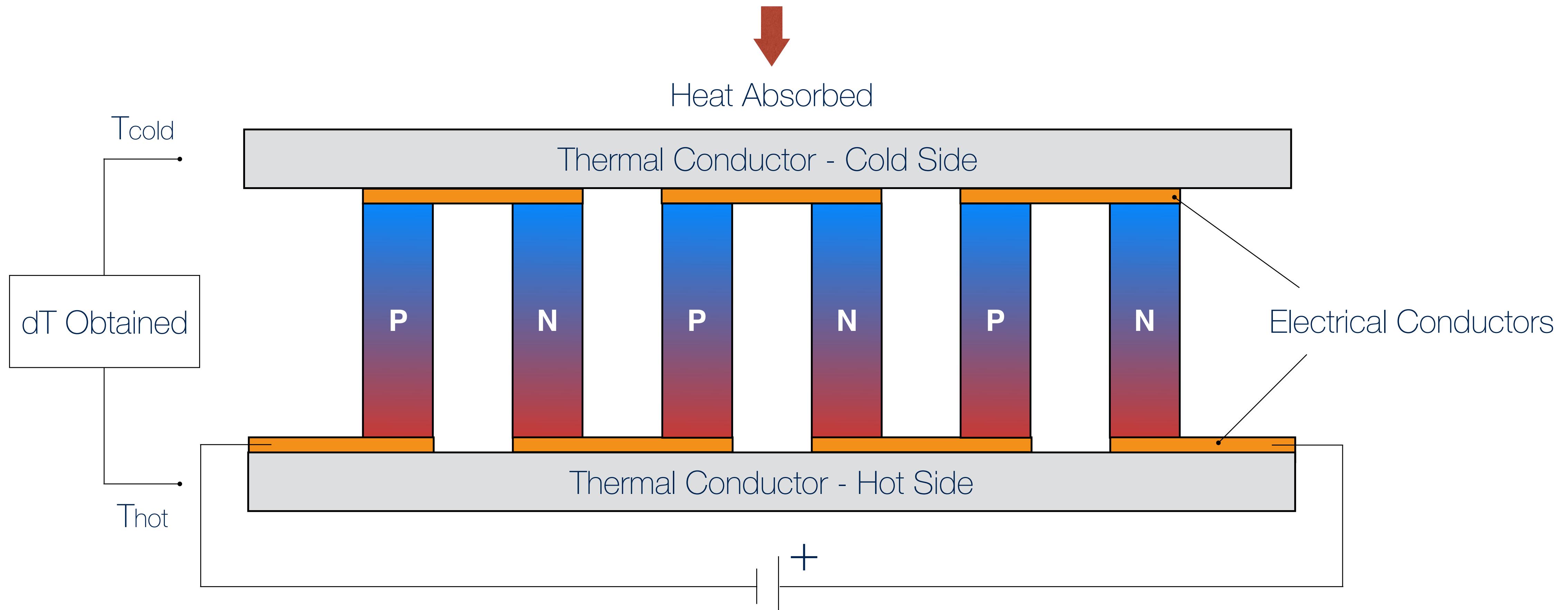


## How does it work - Thermoelectric Couple





## How does It work - Thermoelectric Cooler (TEC) Construction

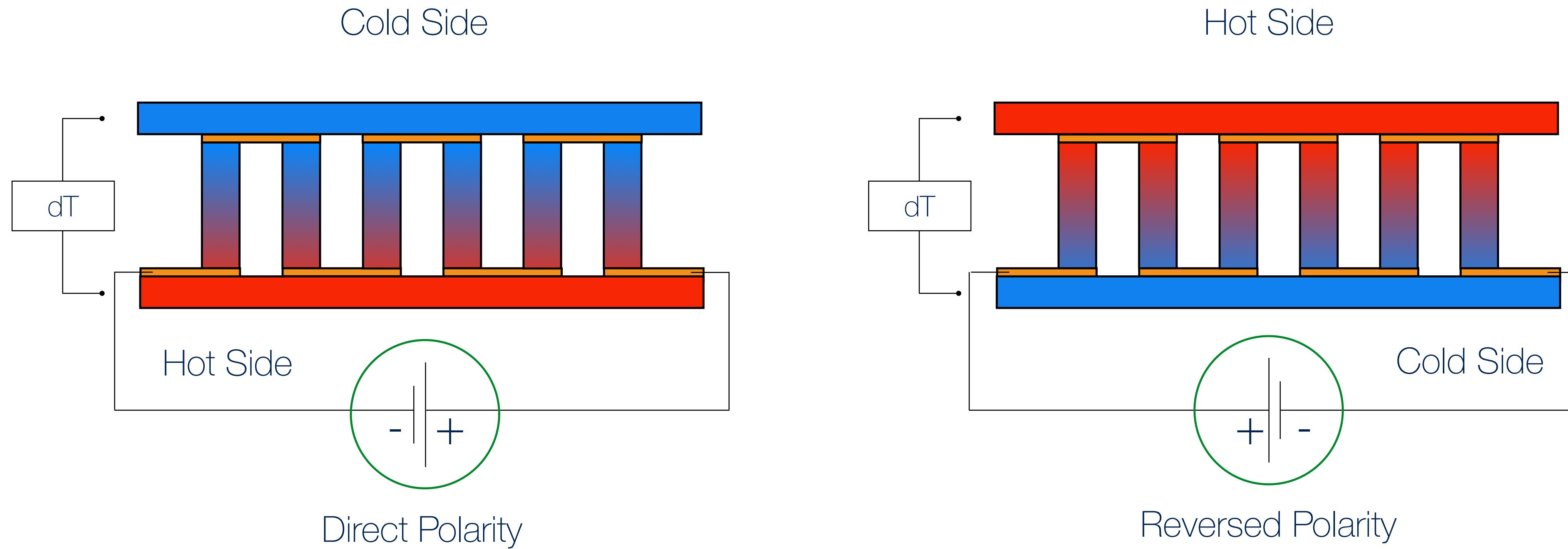


TEC consists of a set of thermoelectric couples assembled between ceramic plates

Heat dissipated



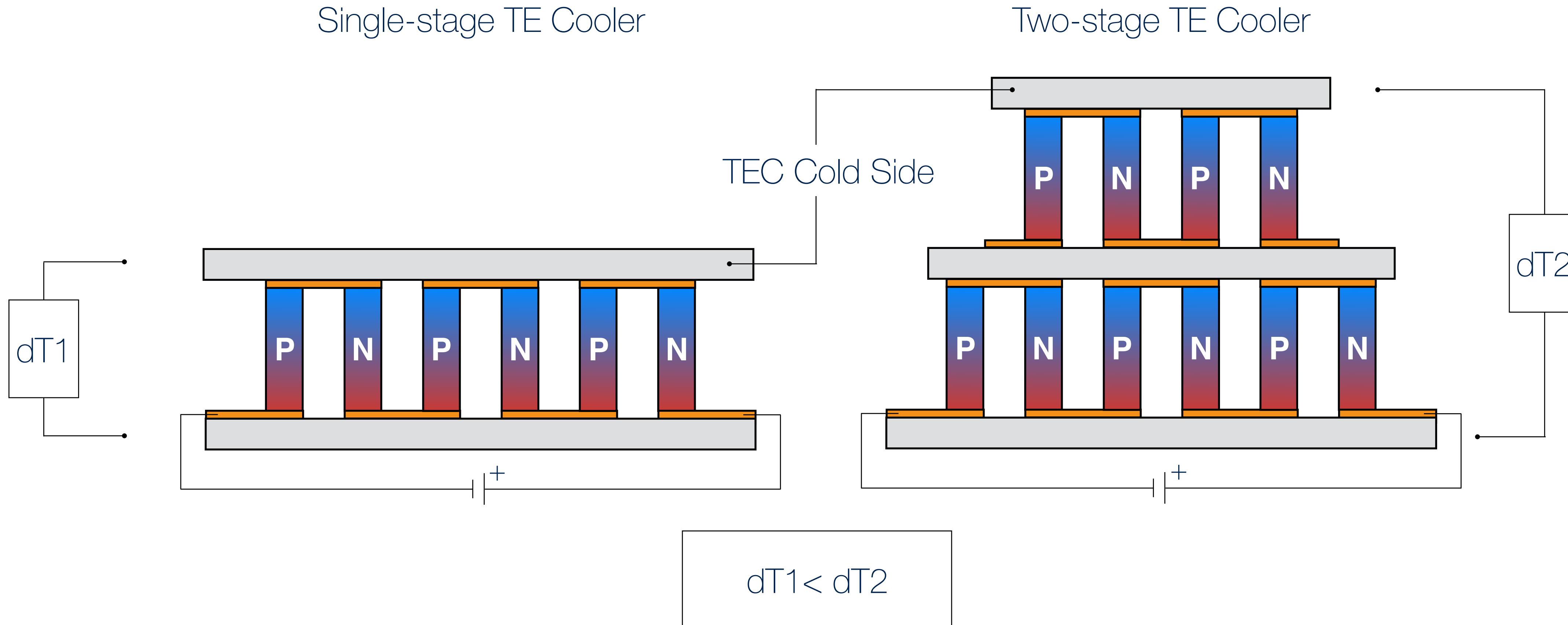
## TE Cooler is bidirectional Device for use in Cooling and Heating Modes



Electrical Current polarity reverse turns TE Cooler (TEC) from Cooling Mode into Heating Mode.  
This property makes TECs optimal for accurate Temperature Stabilization



## How does It work - Single- and Multistage TE Coolers



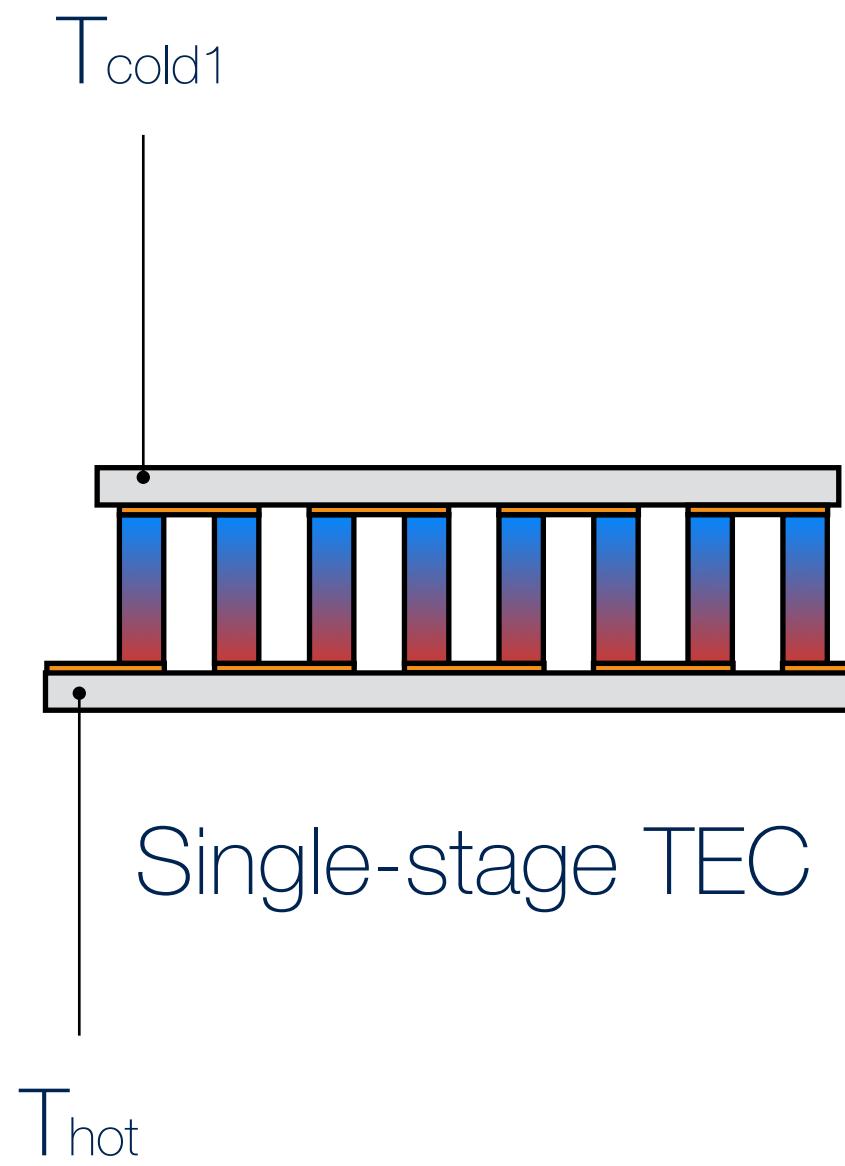
Multistage TE Coolers allow obtaining higher temperature difference between Cold and Hot sides



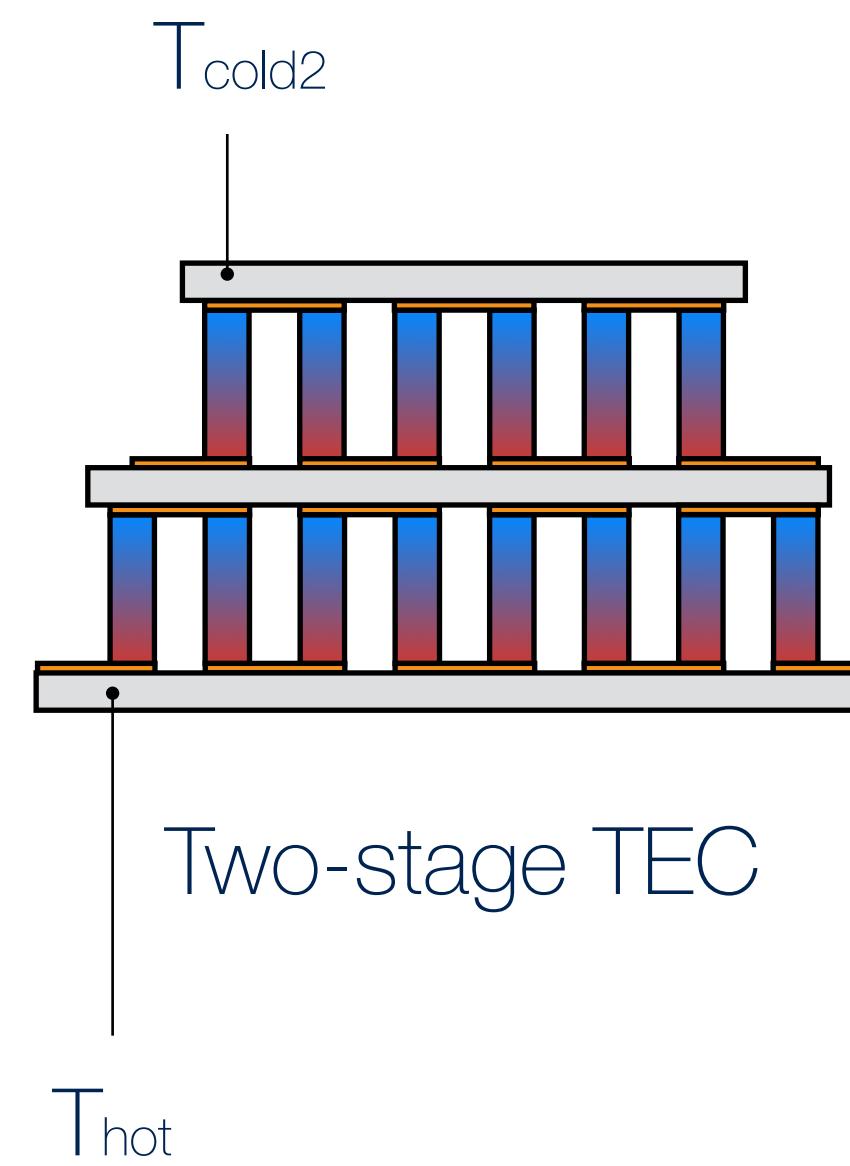
## How does It work - Single- and Multistage TE Coolers

Maximum Temperature Difference between Cold and Hot Sides ( $dT_{max}$ ) at +27°C Ambient

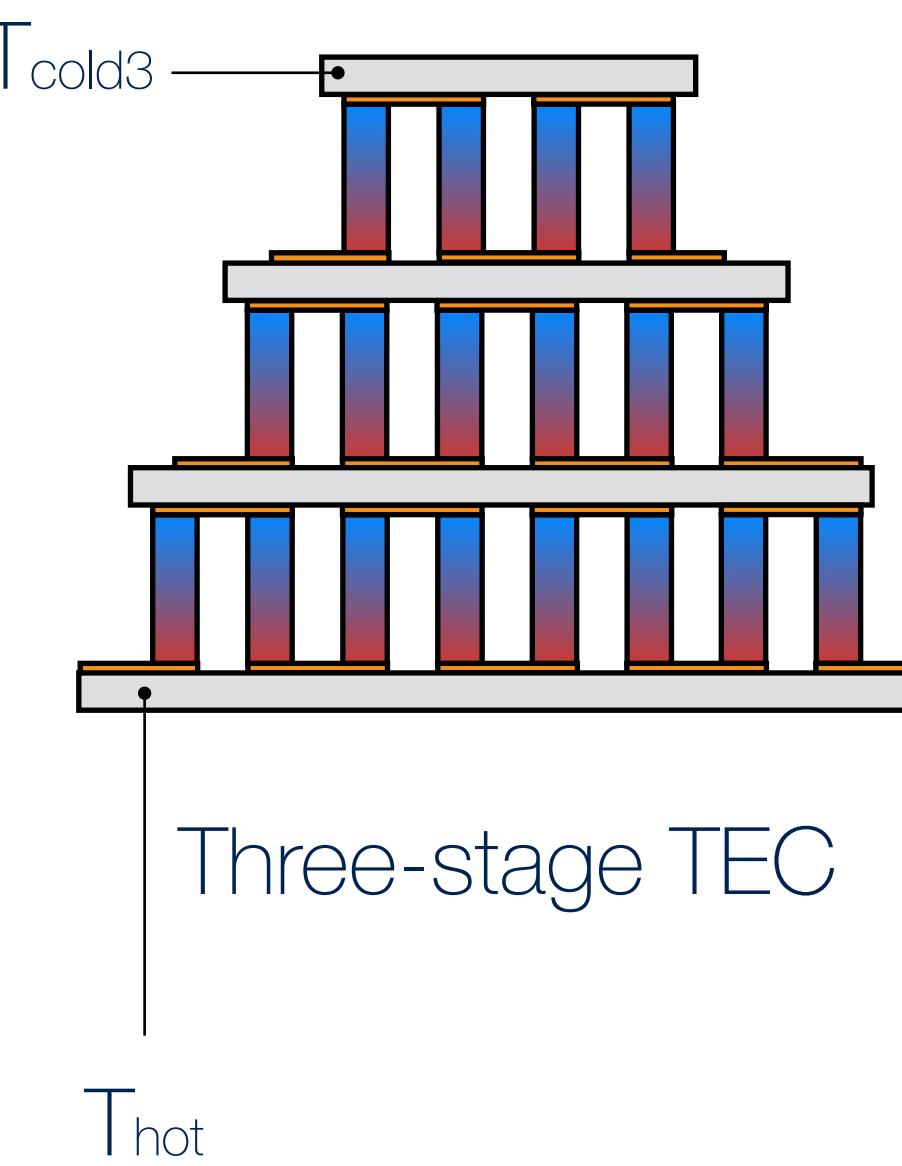
$dT_{max}: 60..72K$



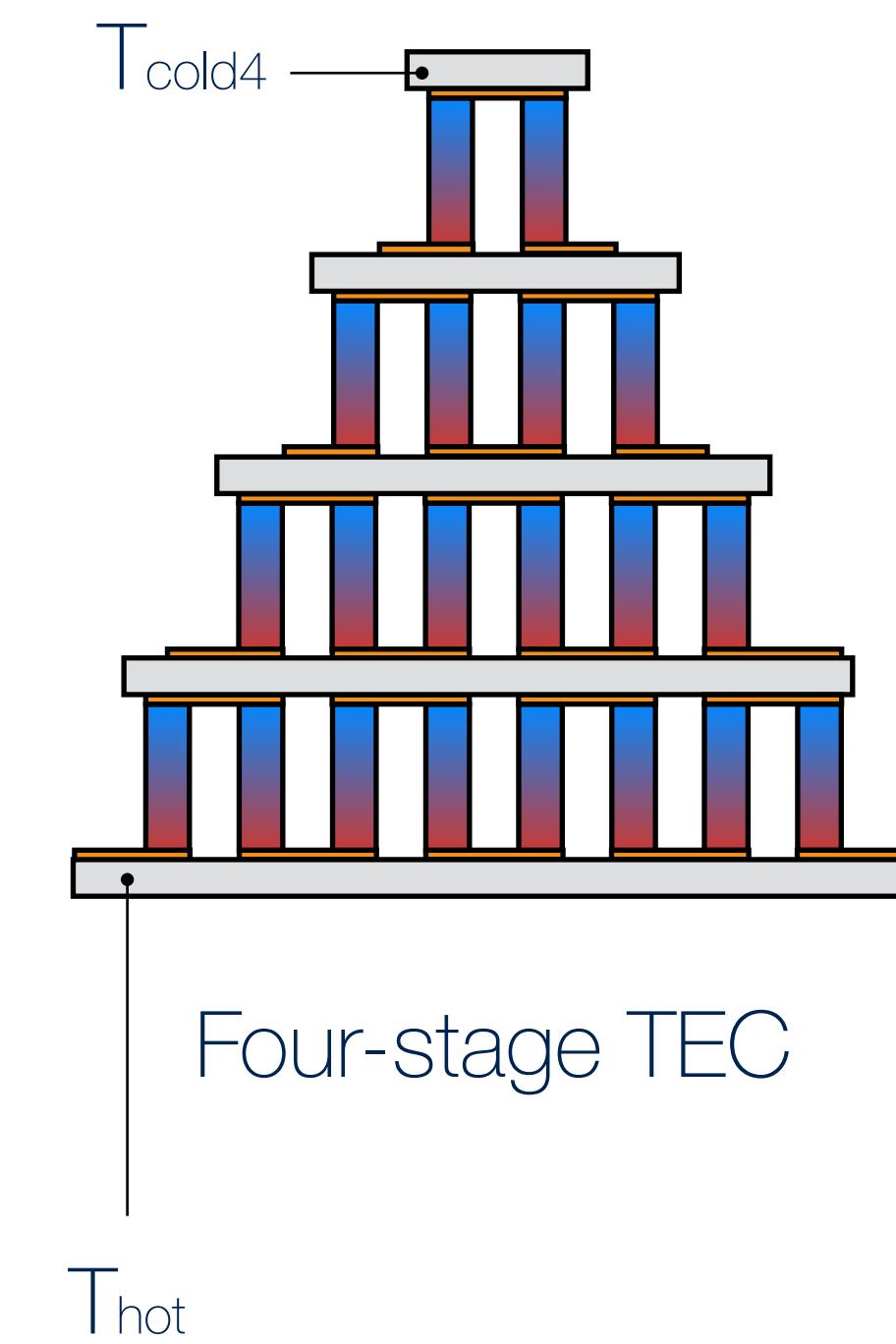
$dT_{max}: 80..100K$



$dT_{max}: 100..110K$



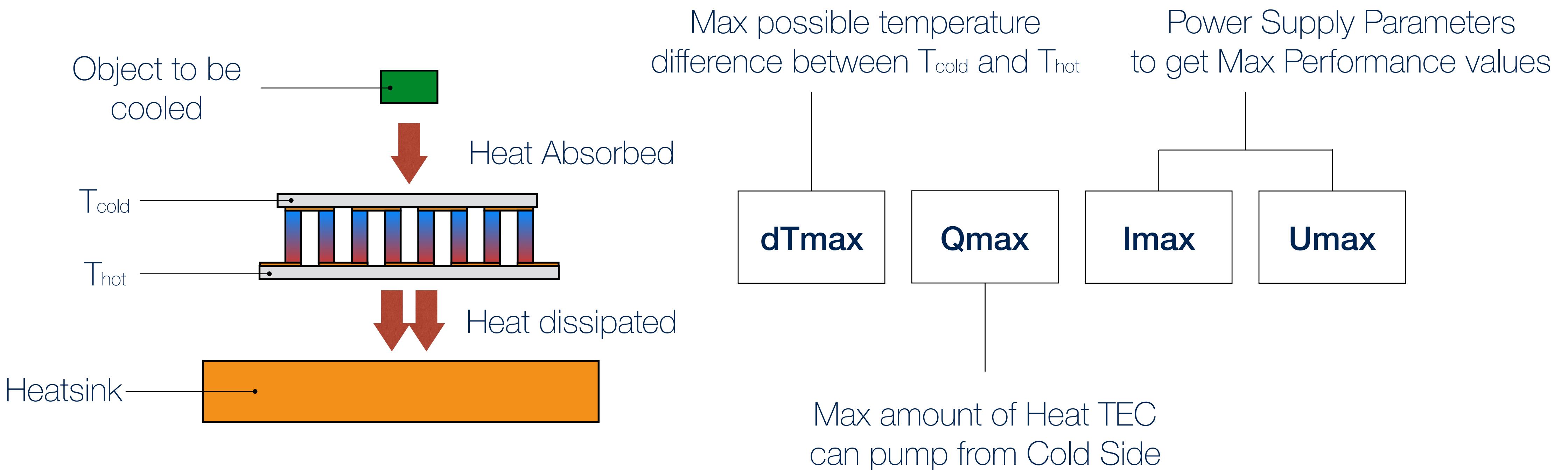
$dT_{max}: 110..130K$



Multistage TEC construction increases max possible  $dT$  in application, but the opposite effect may be in less amount of heat to pump from TEC cold side.



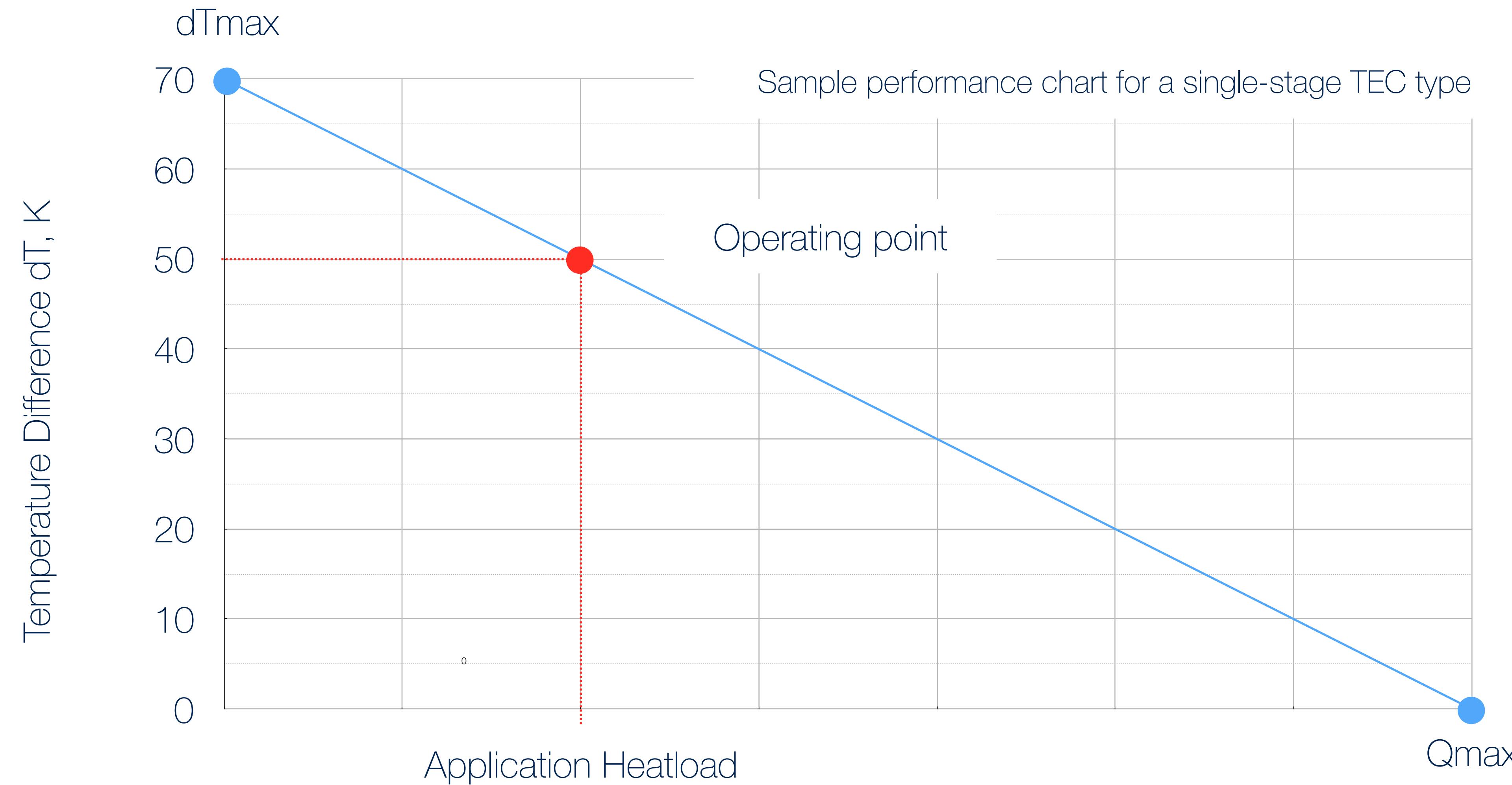
## How does It work - TE Cooler Key Parameters



TE Cooler operates as a Heatpump. It transfers the Heat from Cold side to Hot Side and provides  $dT$  if required



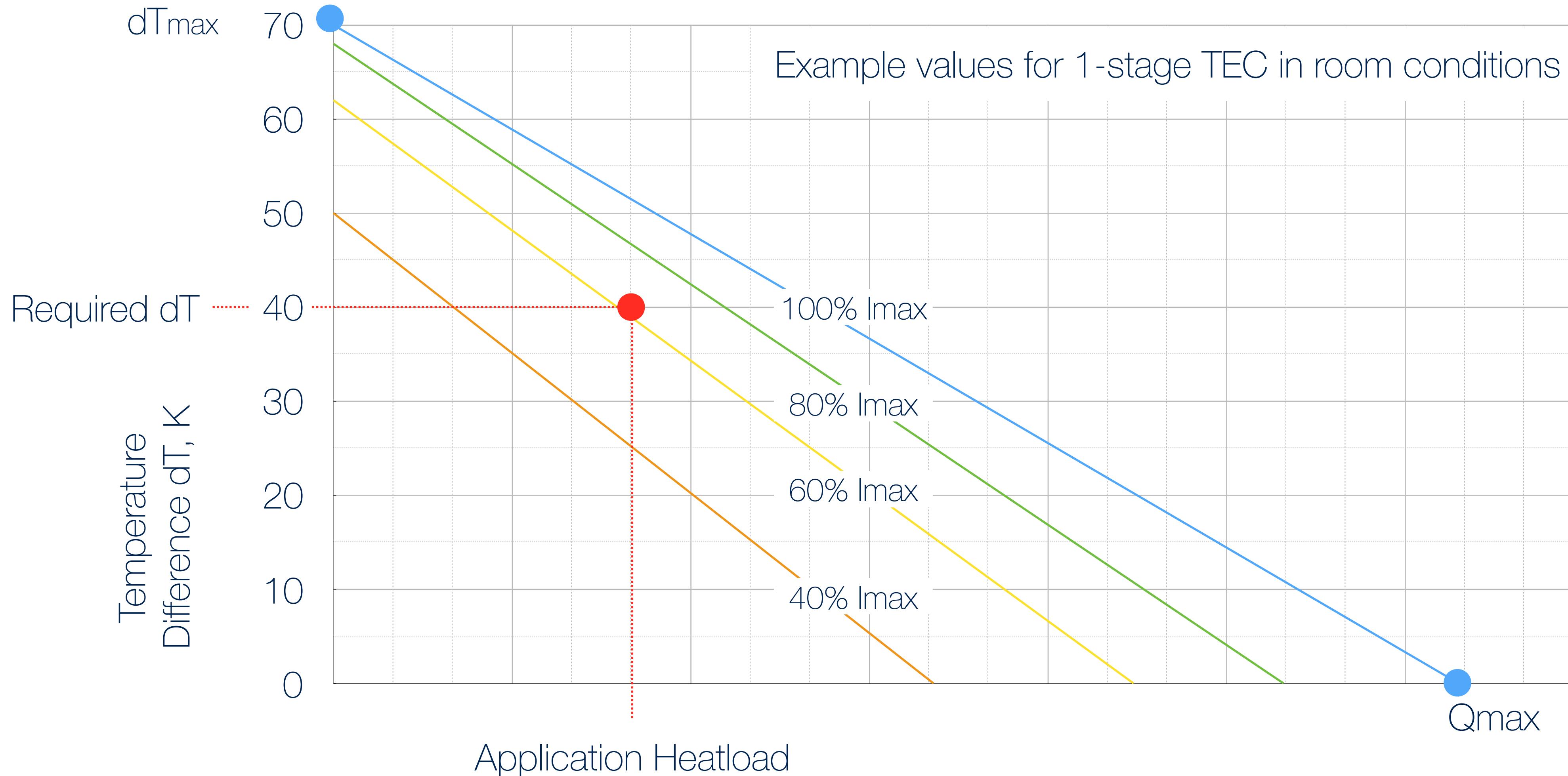
## Understanding TE Cooler General Parameters, $dT_{max}$ and $Q_{max}$



$dT_{max}$  for TEC is specified without Heatload.  $Q_{max}$  is specified at  $dT=0$ . The application point is in between.



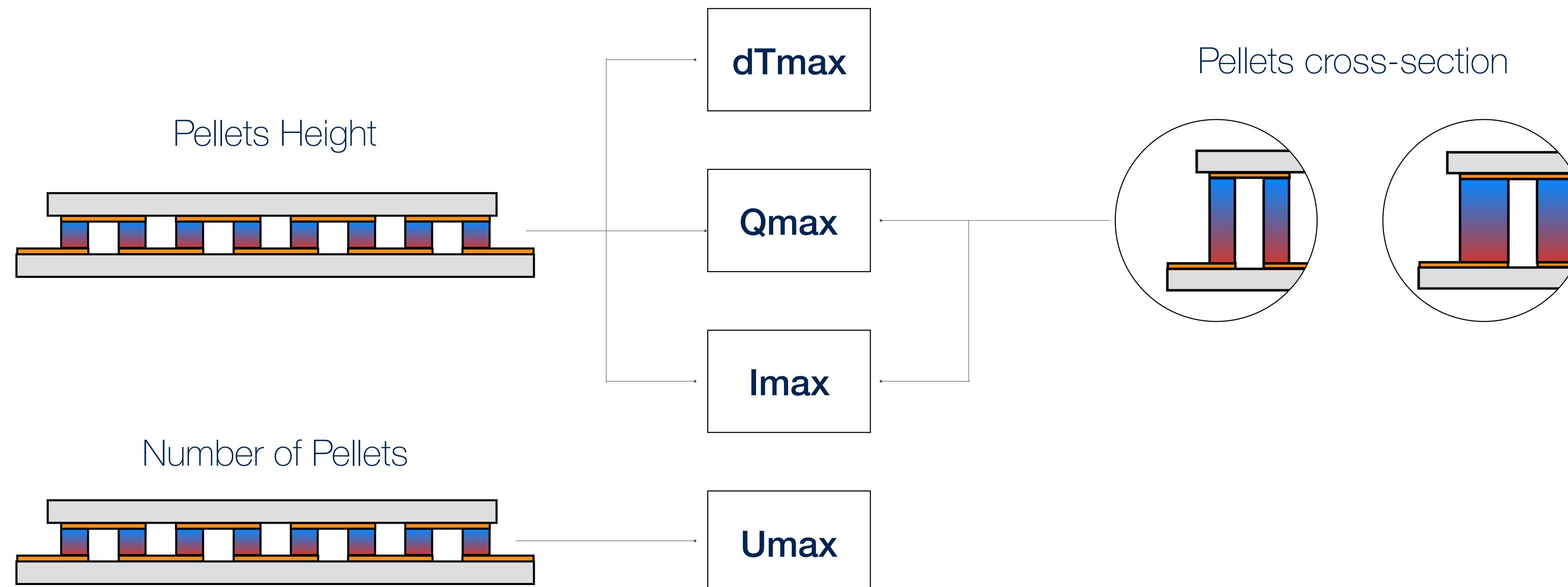
## TEC is DC Current regulated Device



TEC Cold Side Temperature and Cooling Capacity in Application are regulated by applied electrical DC Current



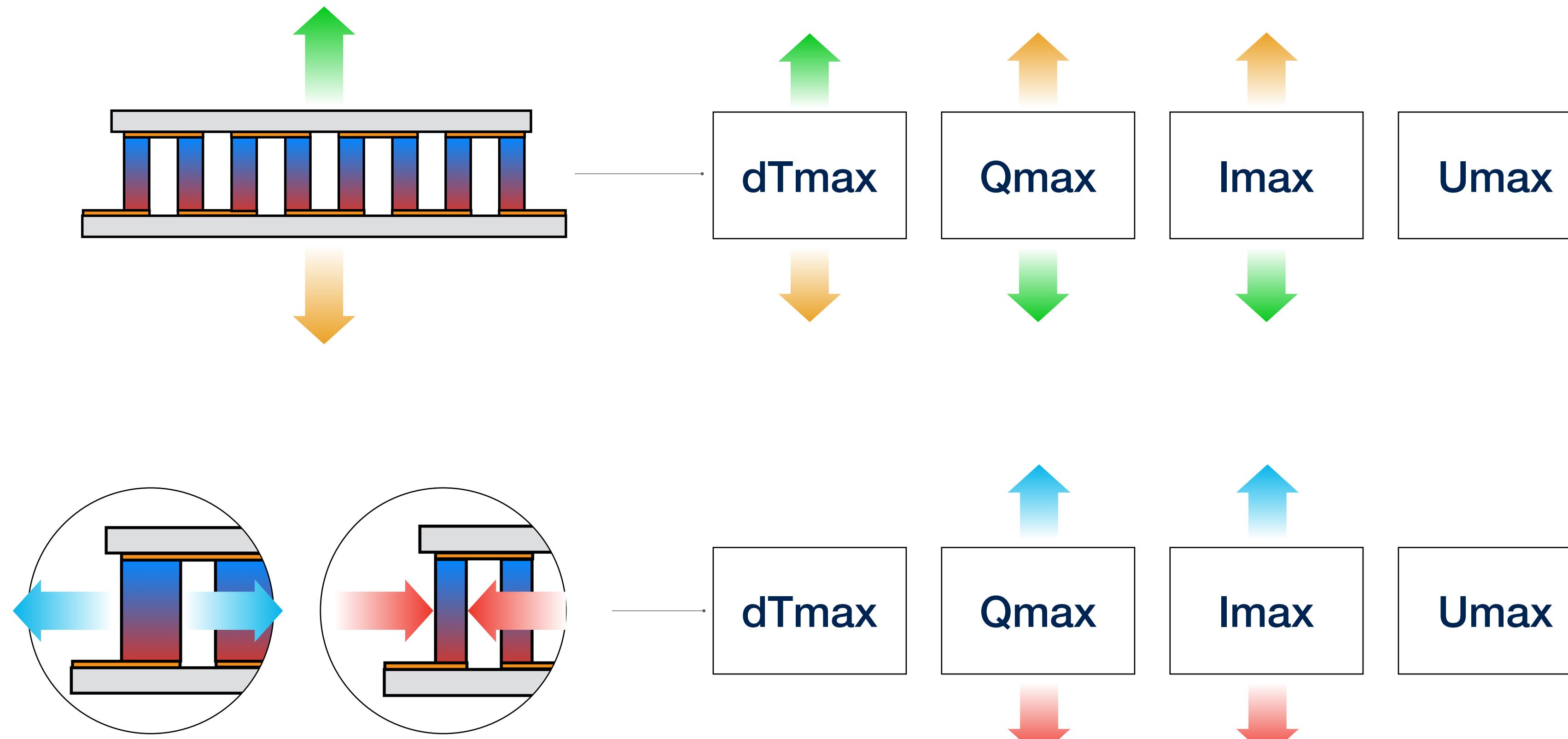
# TE Cooler Performance Parameters and Pellets Geometry



TEC General Parameters are directly connected to the number of pellets and pellets geometry



## TE Cooler Performance Parameters and Pellets Geometry

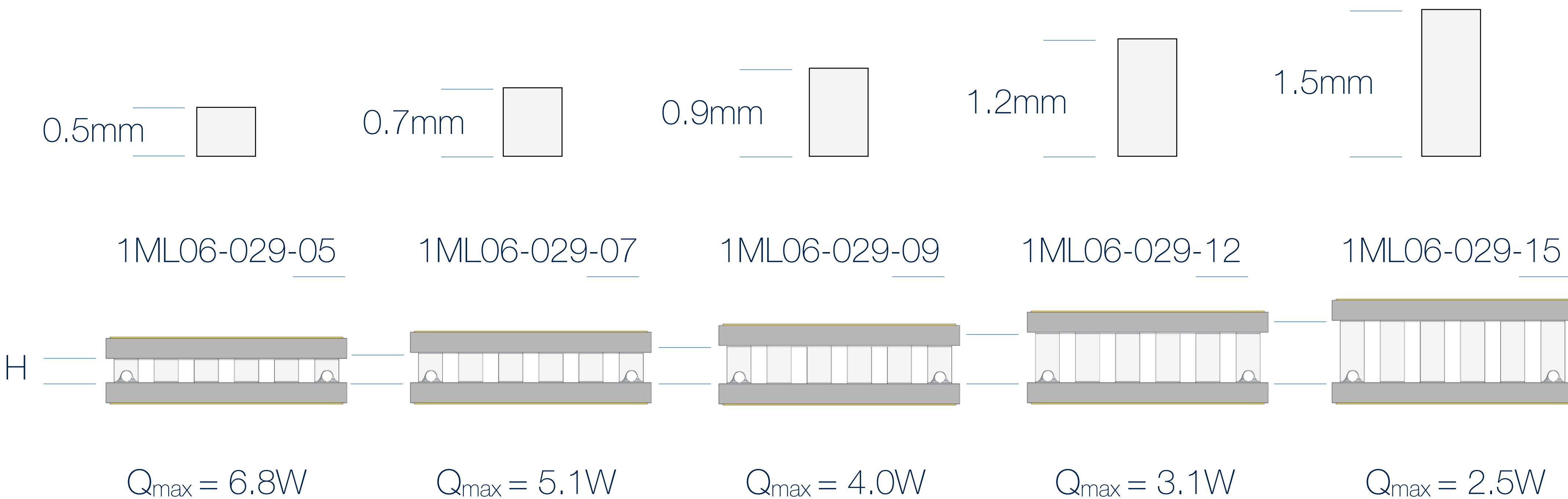


Lower pellets make TEC cooling capacity higher, but increase the parameter  $I_{\max}$ .  
The same effect has pellets cross-section increasing (w/o height change).



## TEC Microsystems TE Cooler Datasheet - Standard Pellets Height Variations

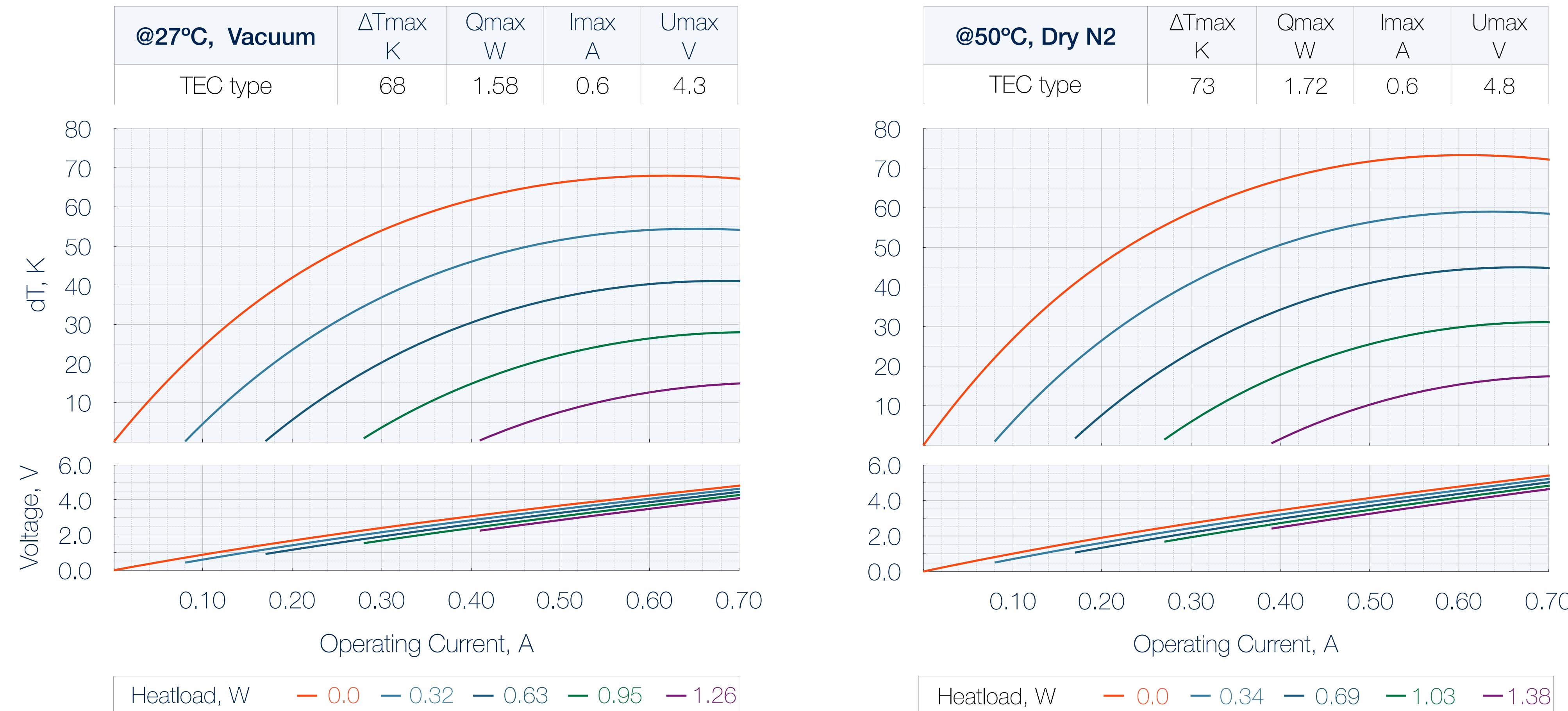
BiTe Pellets Height (H) is directly connected to TEC Cooling Capacity parameter



TEC Microsystems TE Coolers have several height and performance versions for one particular TEC type.



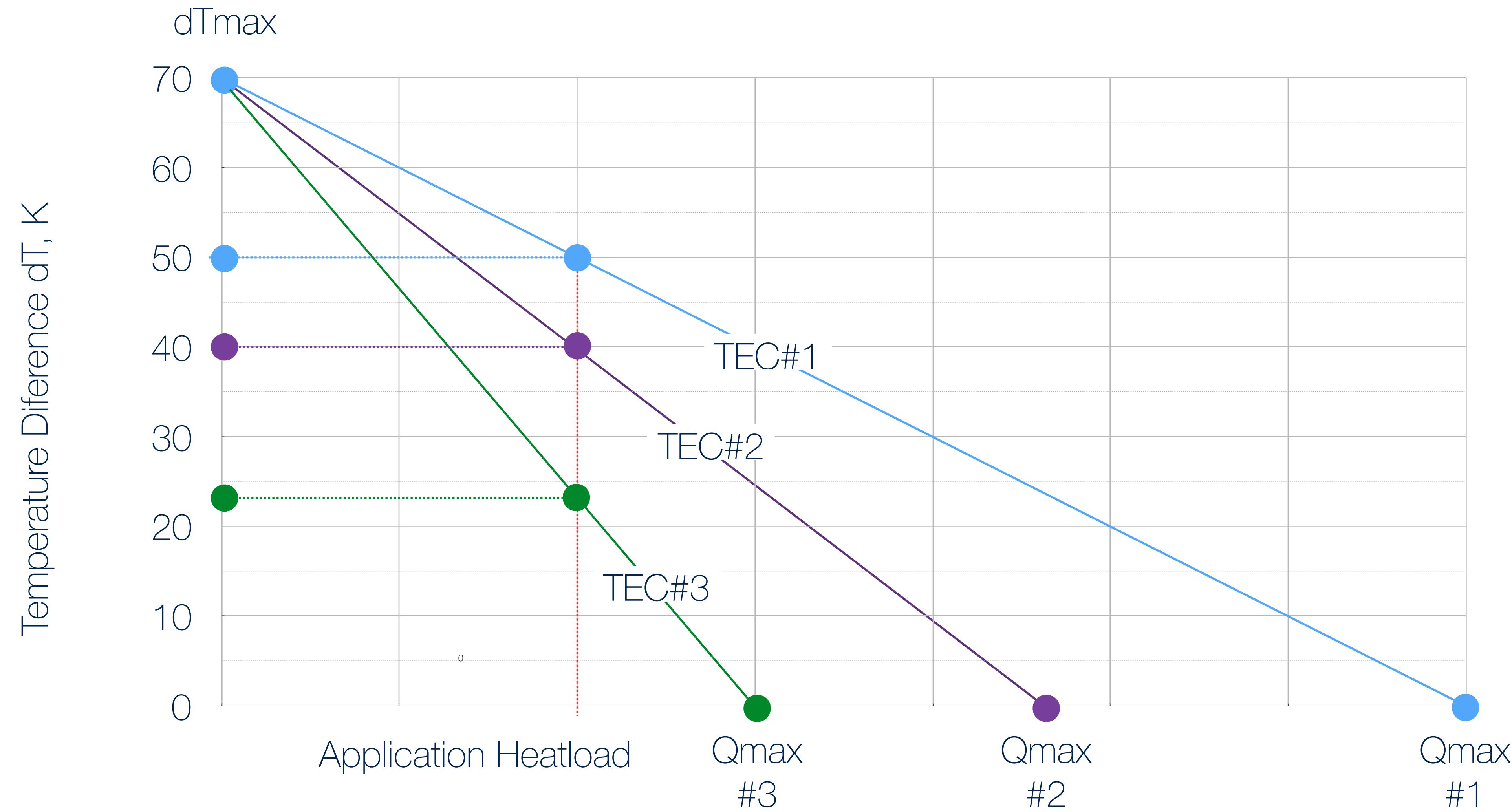
## TEC Microsystems TE Cooler Performance Plots Example



TEC Microsystems Datasheets show standard TEC Performance in typical ambient condition modes.  
TEC Performance plots can be recalculated for special ambient conditions by request.



## Understanding TE Cooler General Parameters, dTmax and Qmax

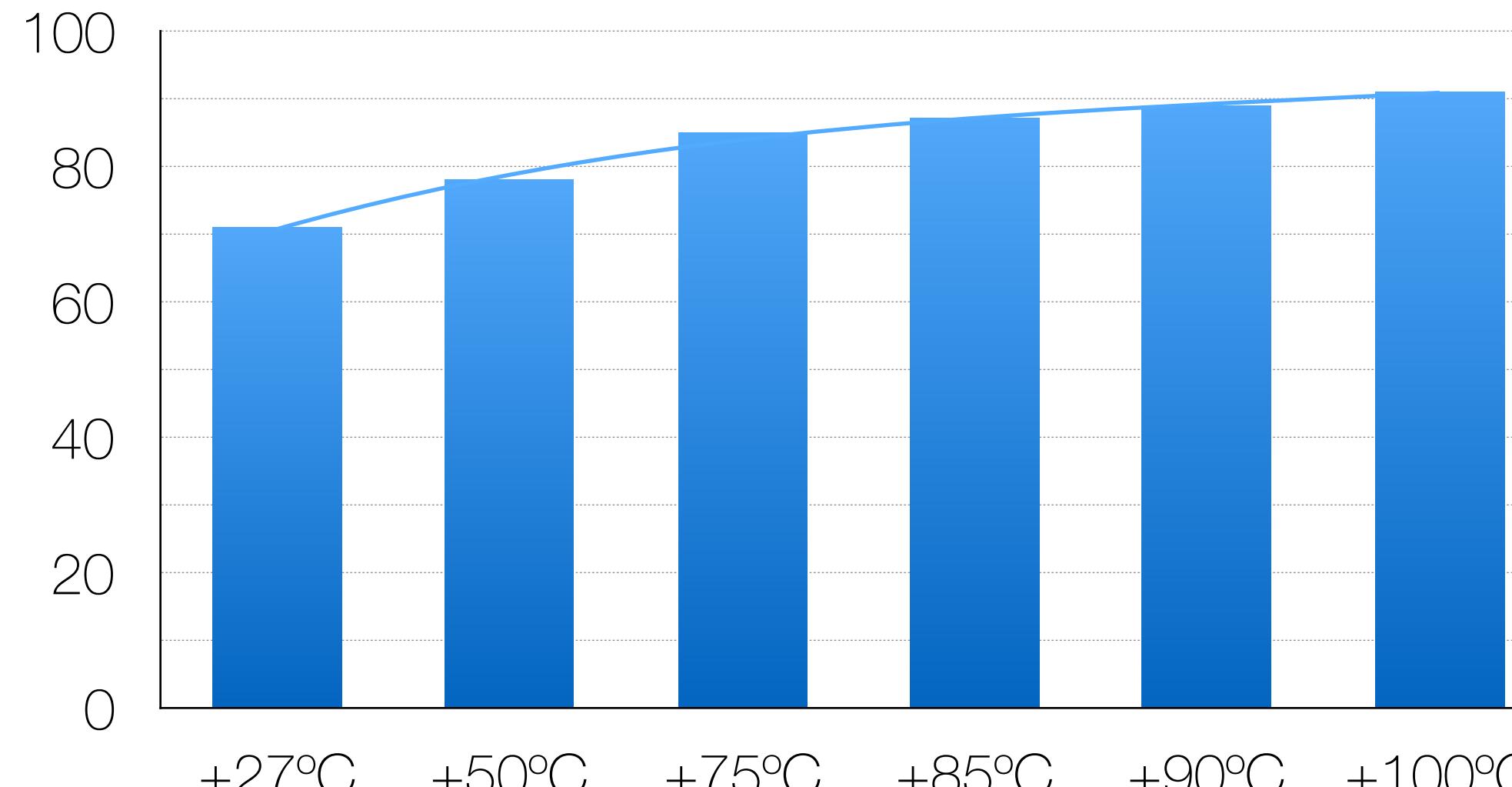


Different TEC types may have the same  $dT_{max}$ , but different  $Q_{max}$ . Thus the max achievable  $dT$  in application may vary.

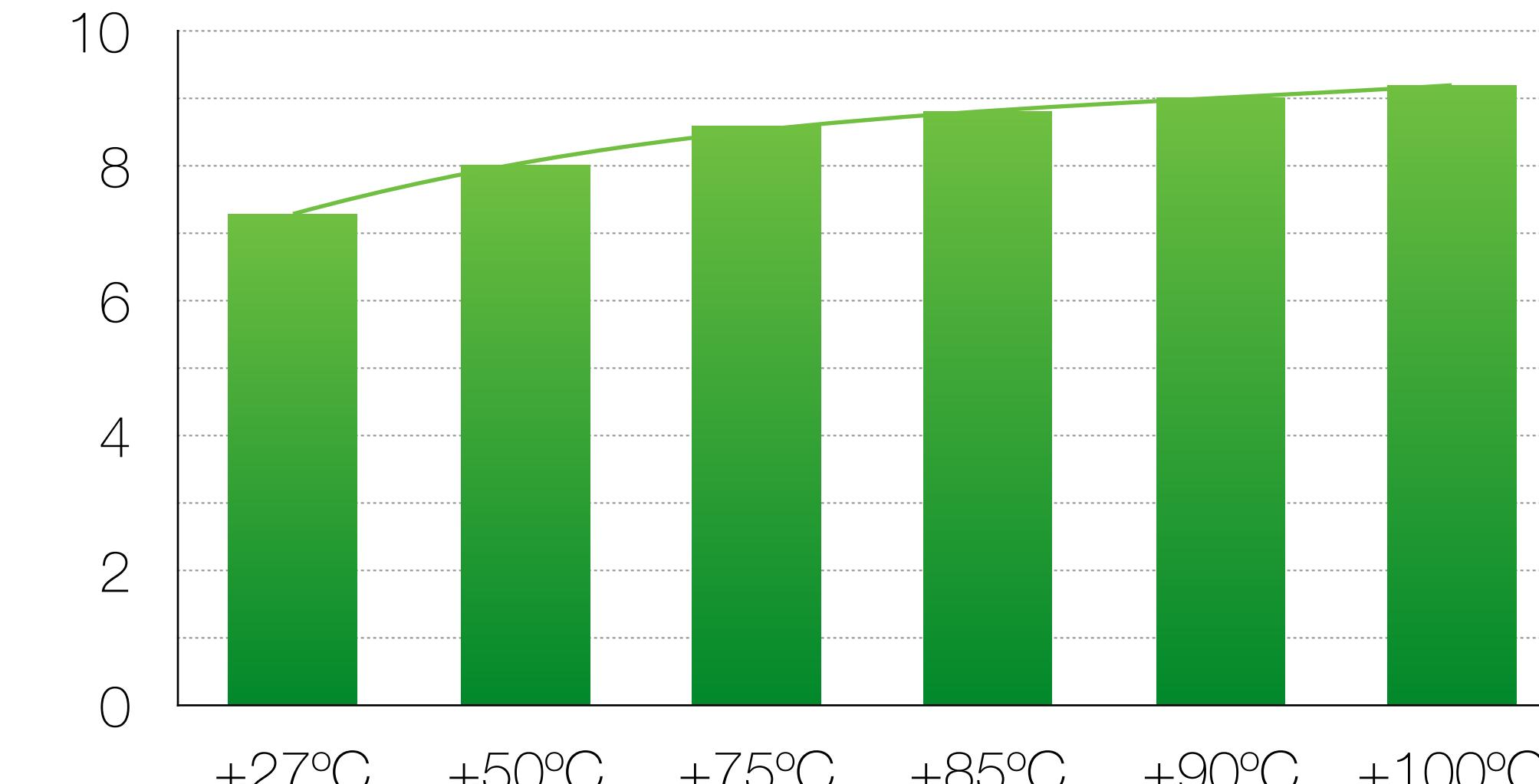


## TEC dTmax and Qmax parameters are connected to Ambient Temperature

TEC dTmax and Qmax grow with Ambient Temperature. Example data for a single-stage TEC.



TEC dTmax, K

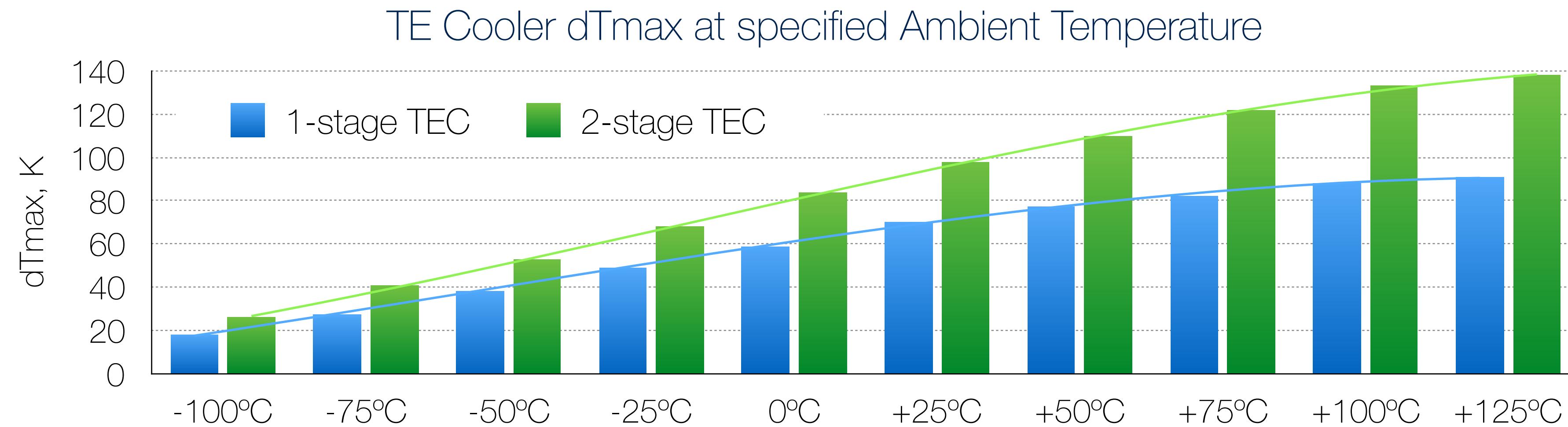


TEC Qmax, W

Qmax and dTmax values depends on ambient temperature. It's important to keep in mind.  
Typical TEC datasheet has dTmax and Qmax values usually specified at +27°C ambient and/or +50°C



## Ambient Temperature and TEC Performance



BiTe material in TE Cooler has the best performance at near room temperature and higher.

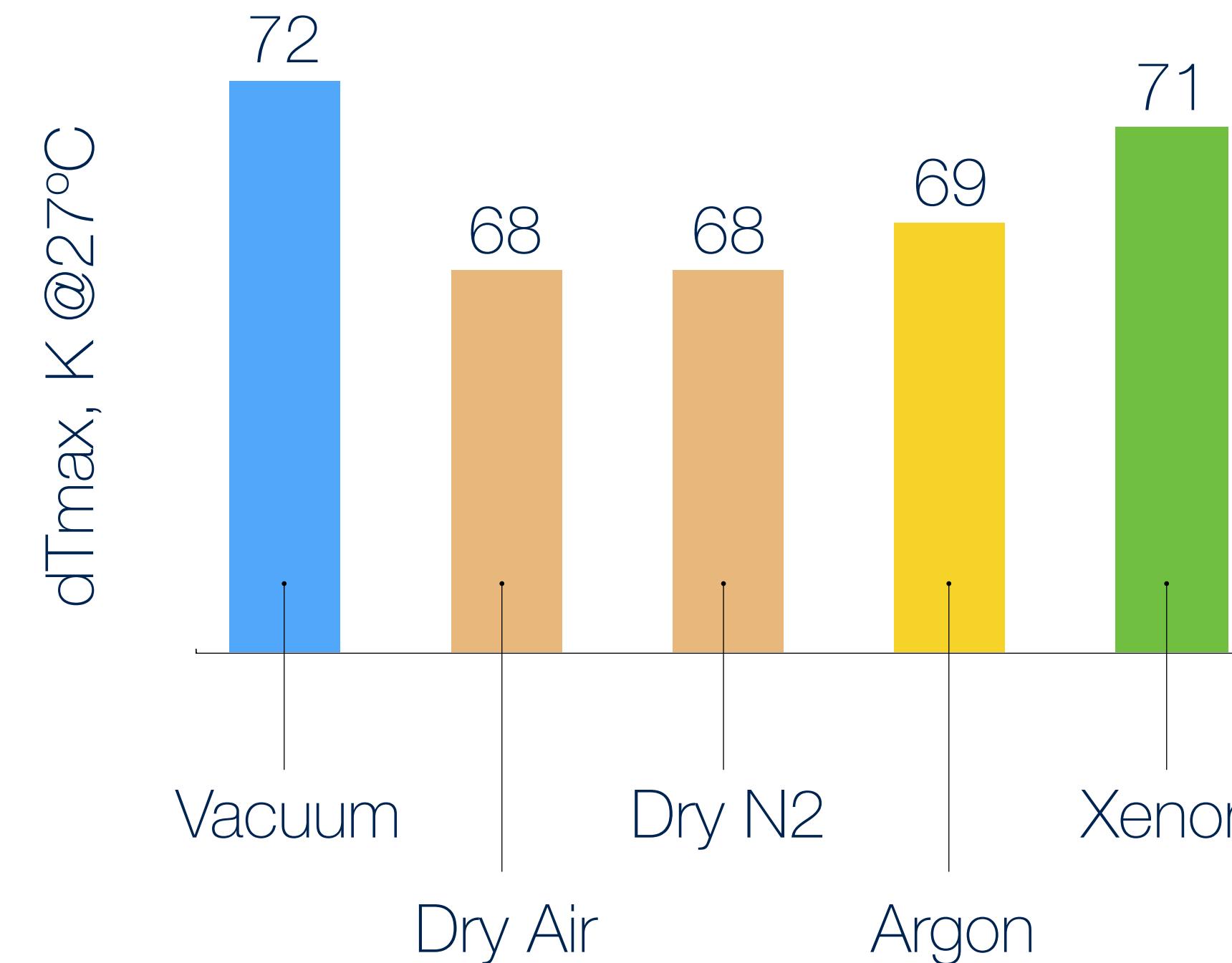
Lower temperatures reduce TE Performance. High temperatures (after +150°C) affect TEC Lifetime crucially.

TEC doesn't work at CRYO-temperatures

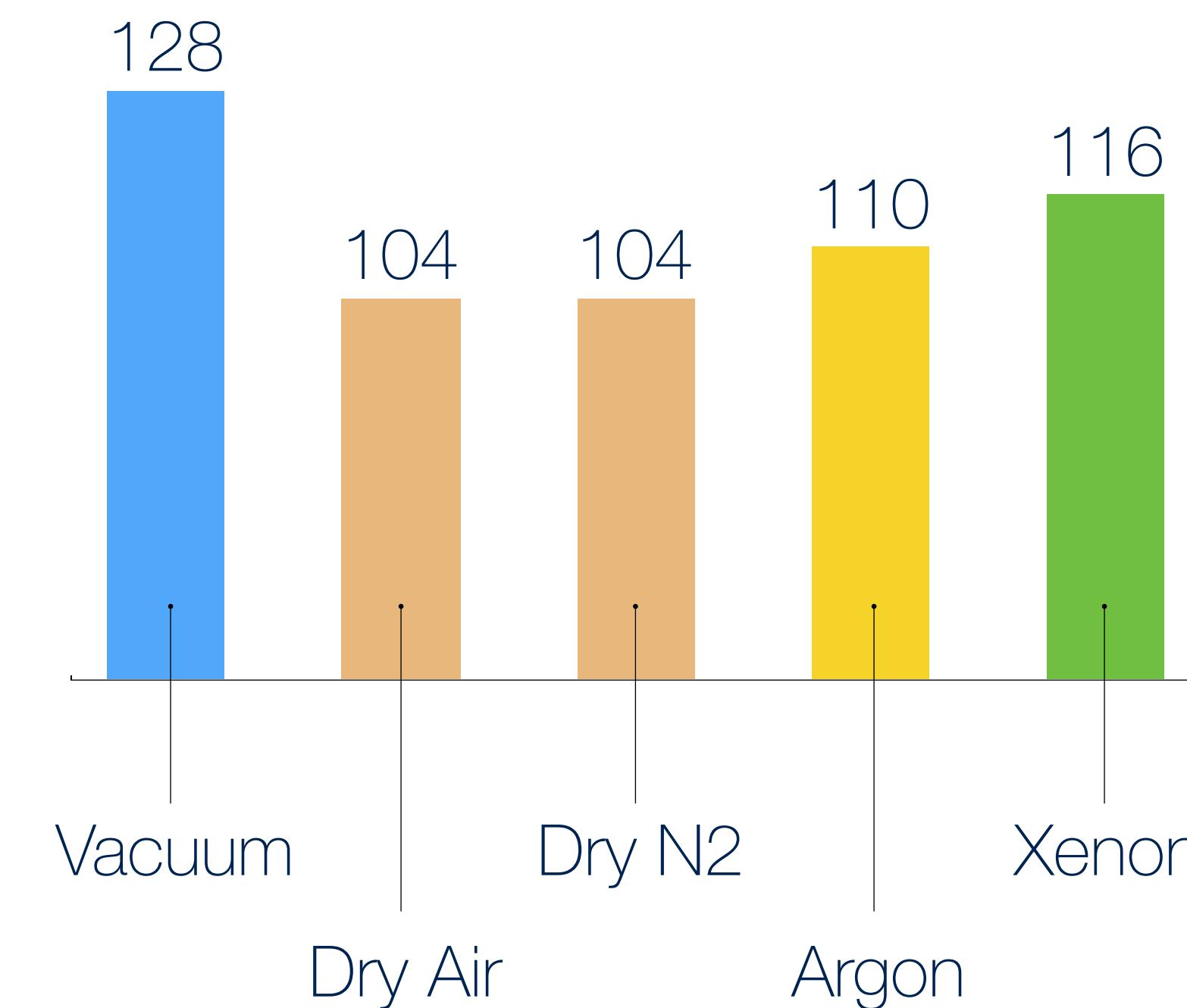


## TEC dTmax parameter is affected by Ambience

Sample Single-stage TEC



Sample Four-stage TEC



Multistage TE Coolers are more sensitive to convectional heatload from gas-filled Ambience.  
For multistage TE Coolers best performance it's recommended to use Vacuum or inert gases Ambience.



## Typical Level of TEC dTmax parameter Reduction in Gas-Filled Ambience

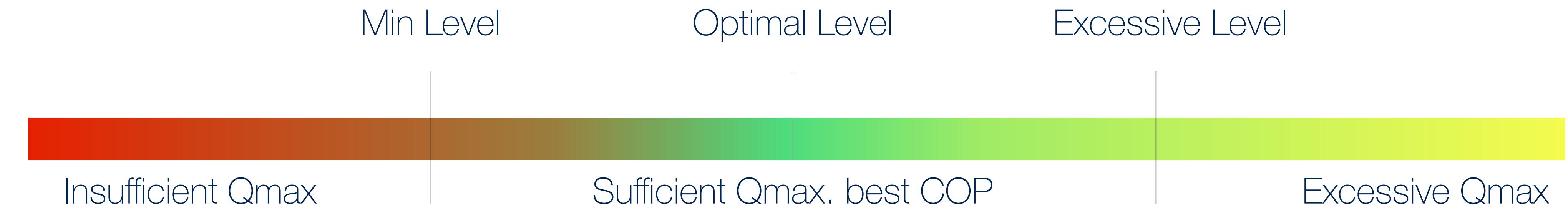
Gas Type	Thermal Conductivity W/mK	Mean Level of dTmax Reduction (comparing to dTmax in Vacuum), K			
		1-stage	2-stage	3-stage	4-stage
Dry Air	0.026	-4	-9	-12	-18
Dry N2	0.024	-4	-9	-12	-18
Argon	0.016	-3	-6	-9	-14
Xenon	0.006	-2	-4	-5	-10

Additional Passive Heatload by Gas Convection affect TEC performance. The affect is usually not so critical for single-stage TE Coolers, but may be significant for multistage TECs.



## Selecting TE Cooler for the required Application Parameters

### TEC Cooling Capacity Qmax for Application



Min value for TEC Qmax  
to meet Heatload and dT  
requirements in application

$$Q_{\max} = \frac{Q}{1 - \frac{dT}{dT_{\max}}}$$

$dT_{\max}$  Standard Values

1- stage TEC	2- stage TEC	3- stage TEC	4- stage TEC
70	90	110	120

In application with required dT and heatload Q TEC must have Qmax at least meeting Min. level.

It doesn't mean the optimal solution, but at least TEC can provide the required performance in application.



## Selecting TE Cooler for Application, Example

### Application Requirements

Heatload —  $Q = 1.5W$

Required  $\frac{dT}{dT} = 50K$

### Estimations for a single-stage TEC suitable by Qmax parameter

$$Q_{max} = \frac{1.5}{1 - \frac{50}{70}} = 5.25W$$

$Q_{max} < 5.25W$   
not sufficient

5.25W  
Min Level

Optimal Level to  
be defined

1- stage TEC	2- stage TEC	3- stage TEC	4- stage TEC
70	90	110	120

sufficient

optimal

The example of brief estimations: Application Heatload 1.5W, required  $dT=50K$ .

The suitable TEC that can meet the required  $dT$  in application must be with  $Q_{max}=5.25W$  at least.



## Selecting TE Cooler for Application, Example

Application

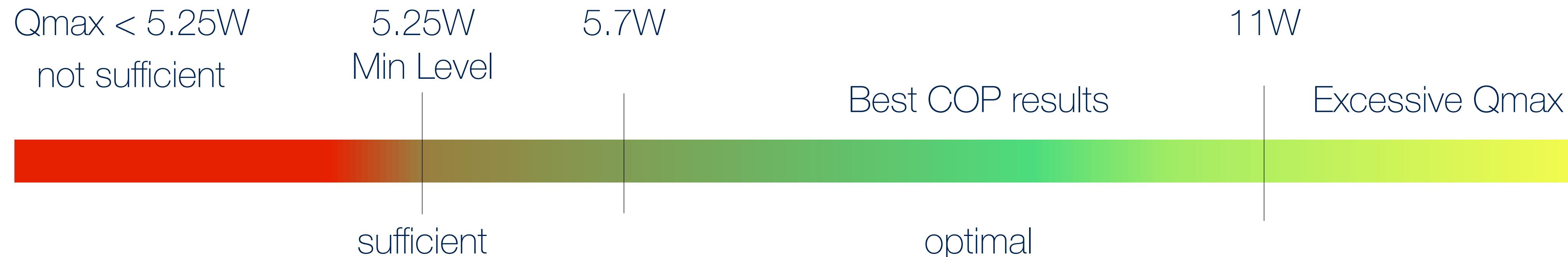
$$Q = 1.5W$$

$$dT = 50K$$

Optimal TEC estimations are more complex and need PRO-level analysis

Optimal  $Q_{max}$  5.7W ... 11 W

Optimal TEC may have 4x .. 10x higher Qmax than Heatload



$Q_{max}=5.25W$  is the Minimum Level to meet application requirements. It's sufficient, but it doesn't mean TEC is the optimal one. Optimal TEC estimations are more complex and require experienced specialists.



## The Balance of Powers - Optimal C.O.P. - Application Example

TE Coolers in testing

Application Conditions

Required dT from Ambient

Most powerful by Qmax

Not optimal

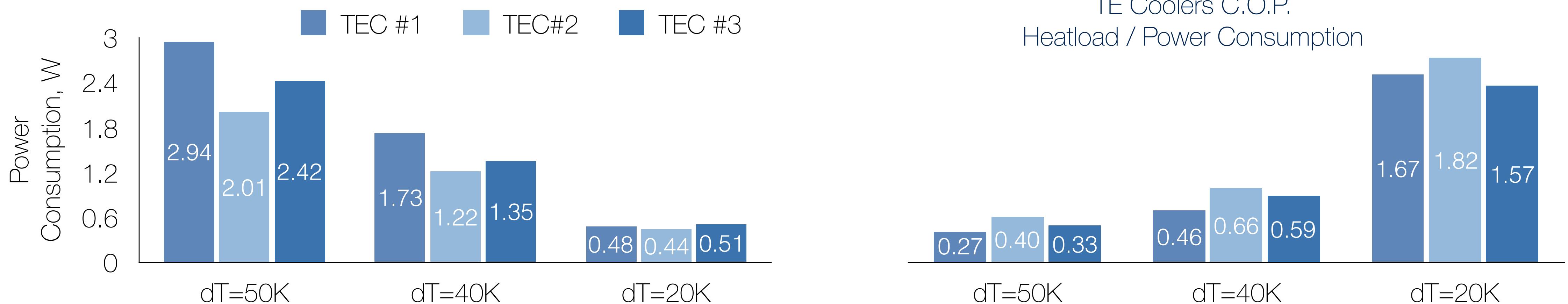
TE Cooler	Qmax, W
TEC#1	6.7
TEC#2	4.3
TEC#3	1.9

→

Application Conditions (Example)	
Ambient Temperature	+75°C
Heatload	800mW
Ambience	Dry N2

→

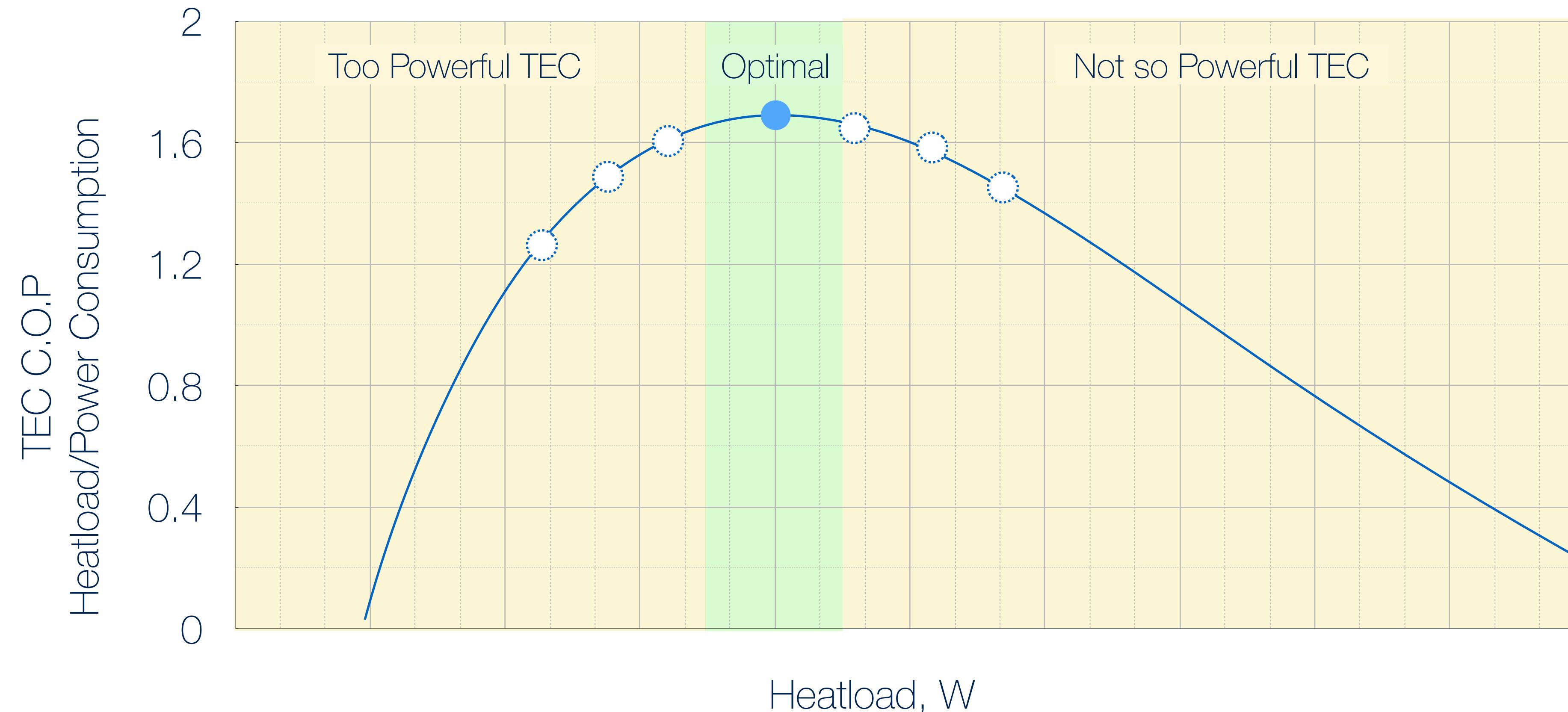
C.O.P.	dT=50K	dT=40K	dT=20K
TEC#1	0.27	0.46	1.67
TEC#2	0.40	0.66	1.82
TEC#3	0.33	0.59	1.57



Bottom Line: the most powerful (by Qmax) TEC doesn't mean the most optimal one in the application



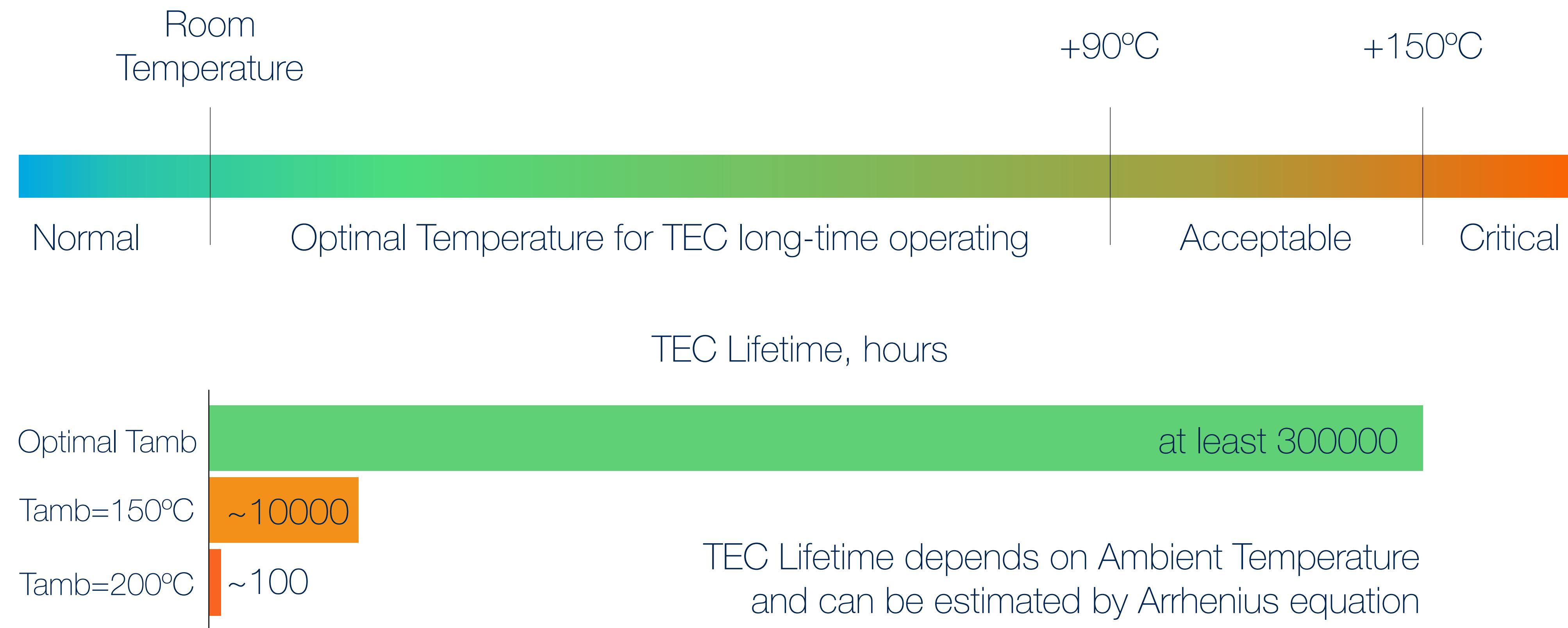
## The Balance of Powers - Optimal C.O.P.



1. The most powerful TEC doesn't mean the most optimal one. A lot depends on application.
2. For an application with specified Heatload and  $dT$  there is always an optimal solution by C.O.P.
3. Every TEC type has an optimal heatload range (with the highest C.O.P.) at required  $dT$  specified



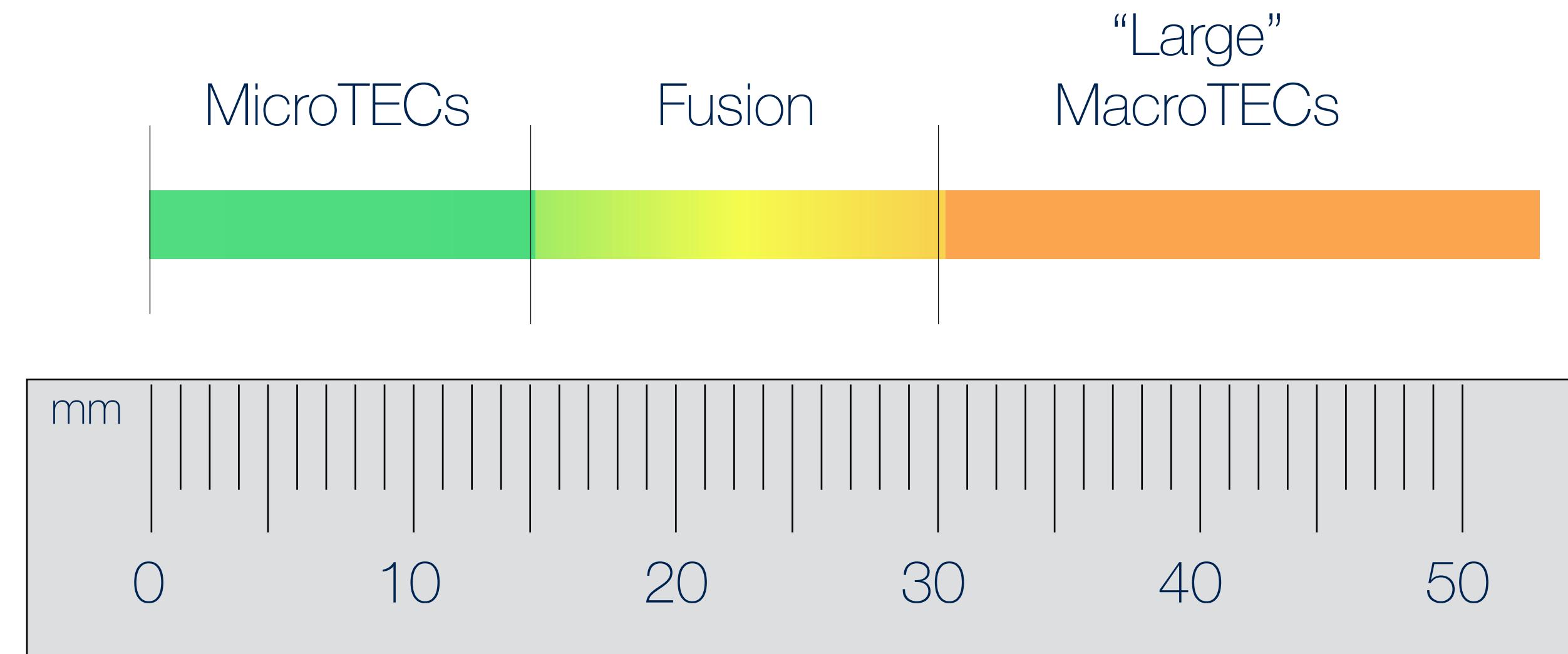
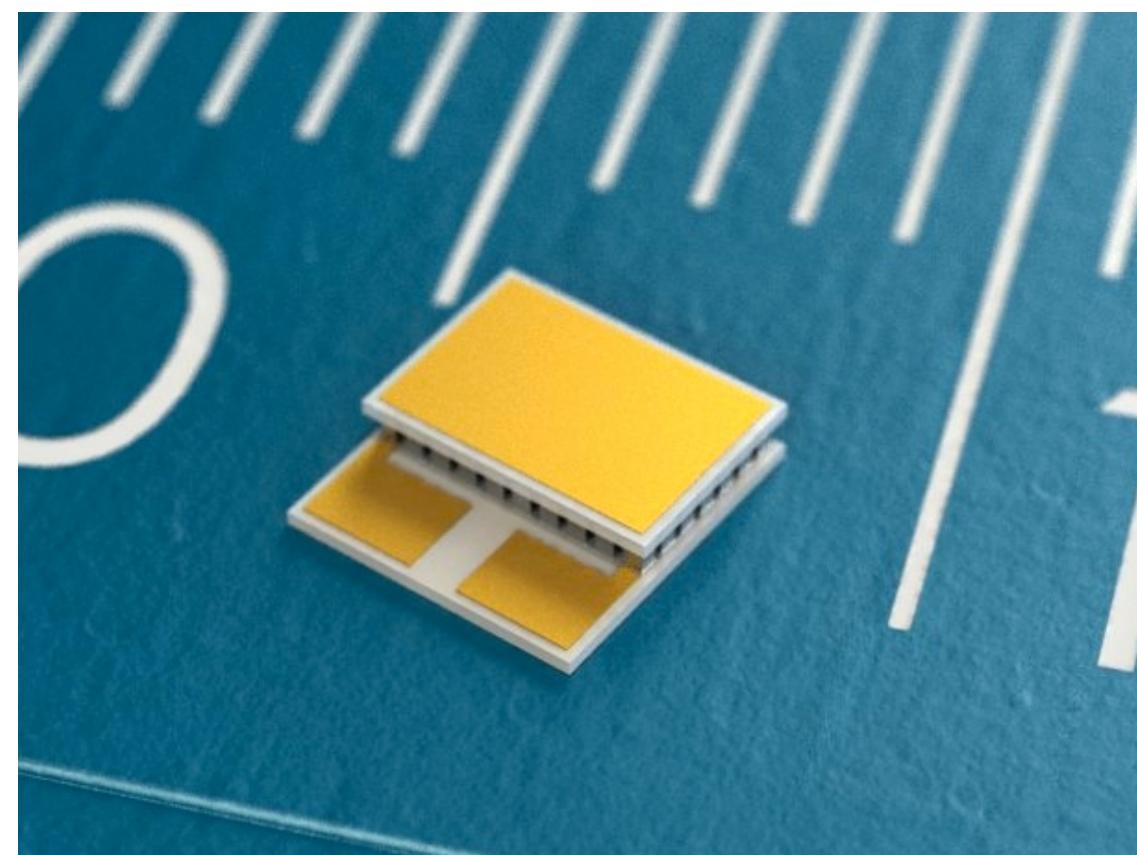
## Ambient Temperature and TEC Lifetime



Term “Lifetime” for TEC is from Telcordia GR-468 Standard. The criteria of failure is TEC AC Resistance change for more than 5%. It doesn’t mean TEC stops operating, but certain performance degradation appears.



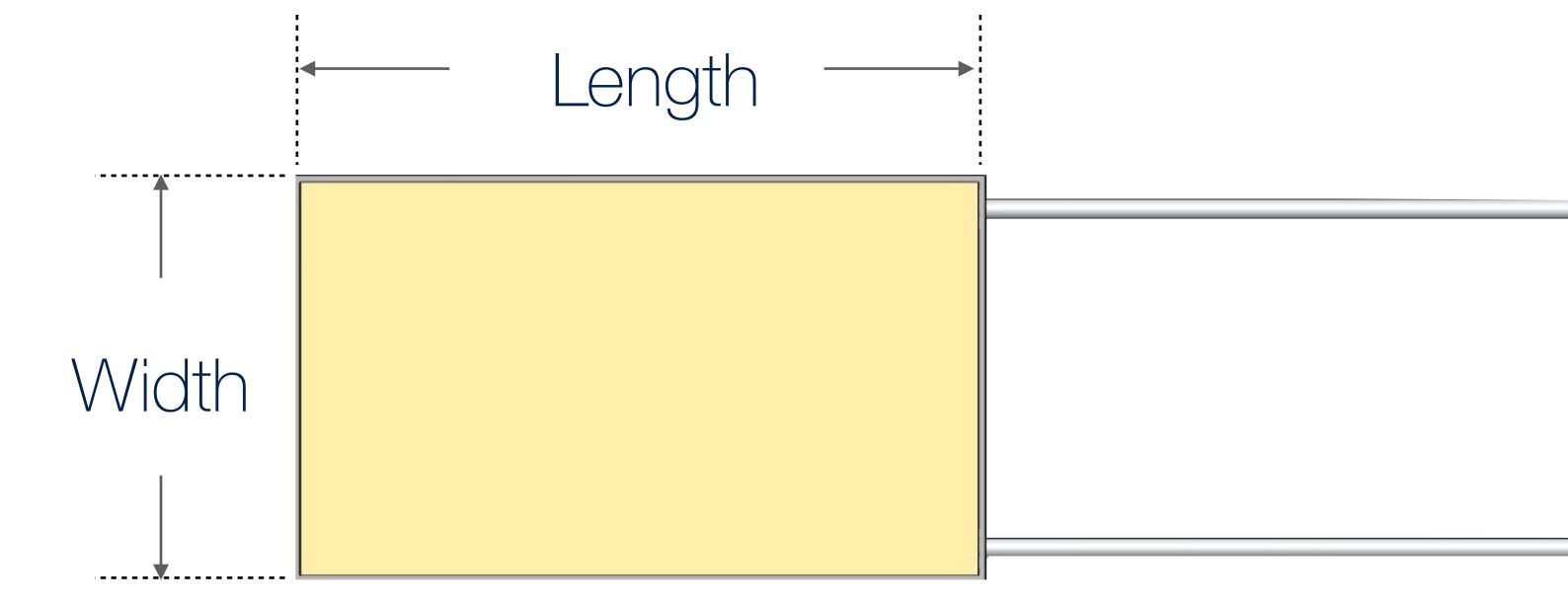
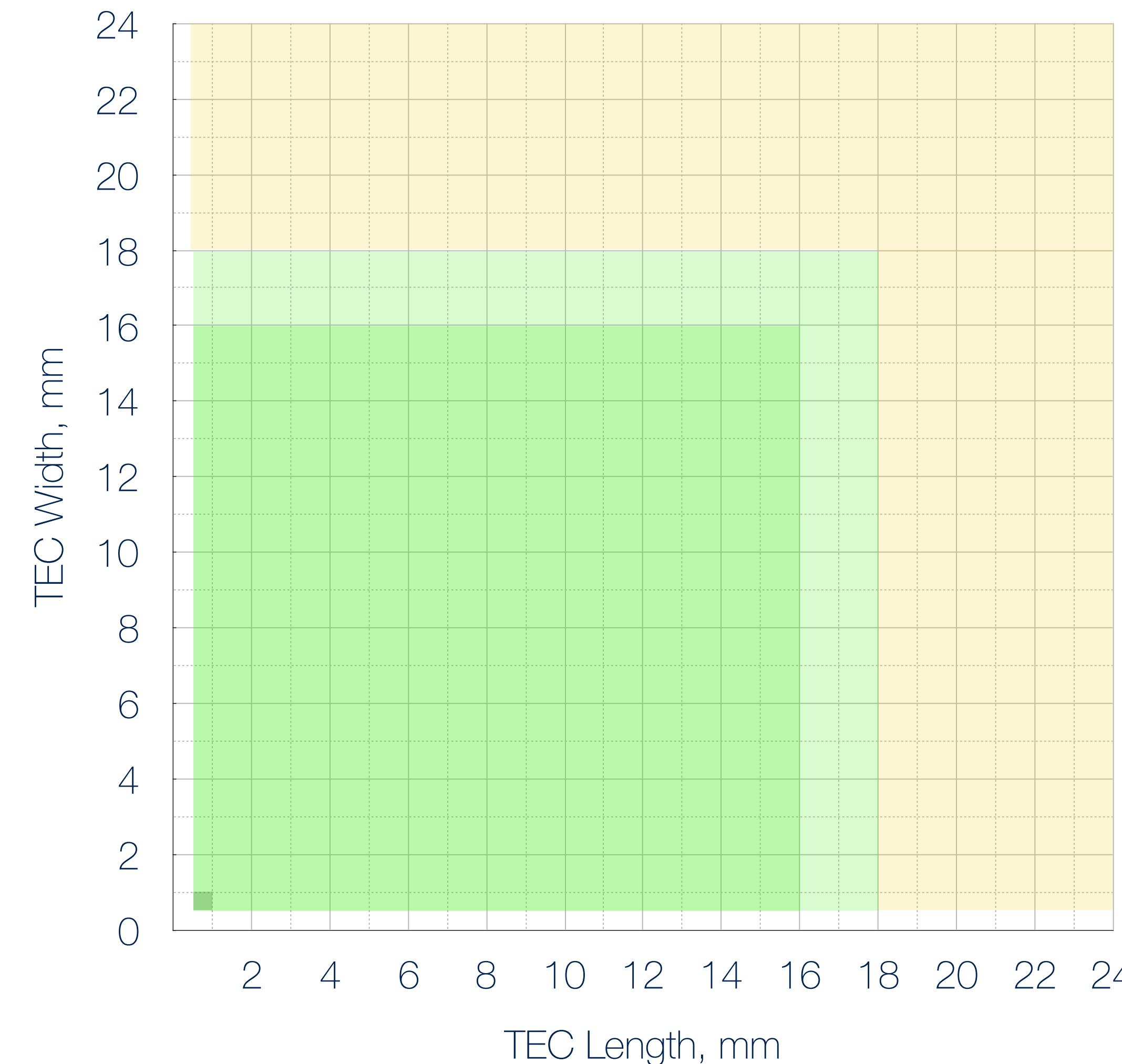
## What means "Miniature" or "Micro" TE cooler



The main difference between miniature and large TE Coolers (besides the size) is in application areas and manufacturing technologies.



# TEC Microsystems Standard TE Coolers Dimensions Coverage Map

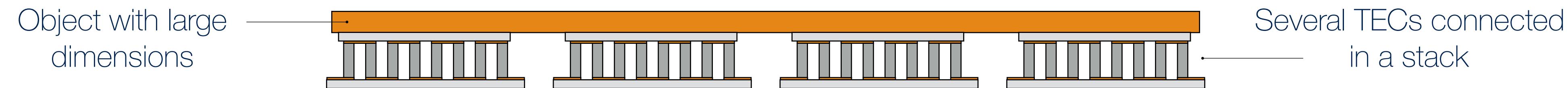
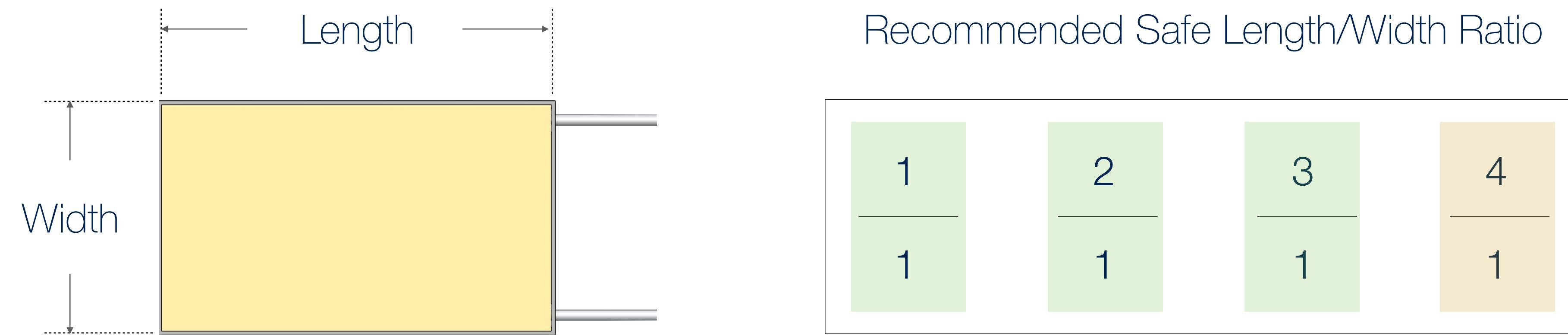


Dimensions	Width mm	Length mm
Min	0.5	0.5
Most Common	< 16	< 16
Available	18	18
Max	24	24



## TE Cooler Length / Width Safe Proportions

TECs with elongated shapes have additional risks of mechanical strains due to thermal expansion

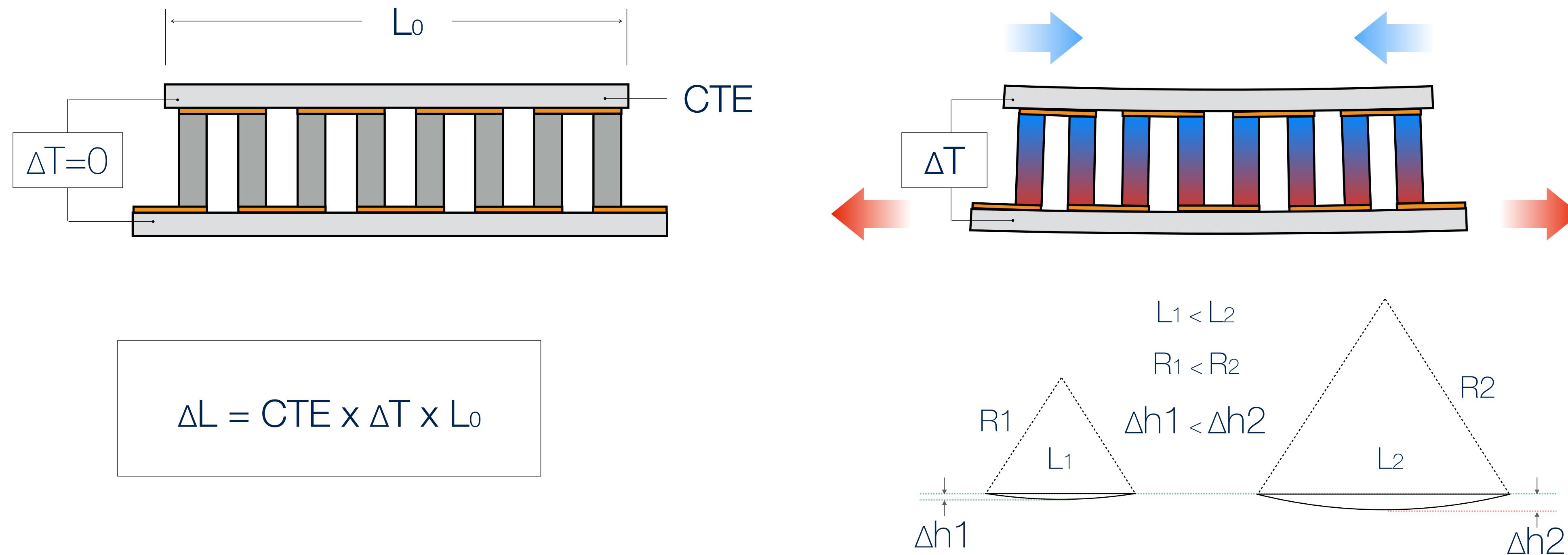


In case of large dimensions of object to be cooled it's better to apply several TECs connected in a stack.



## TEC Length / Width Safe Proportions

The larger TEC initial linear dimensions  $L_0$ , the more significant values of thermal expansions  $\Delta L$



$\Delta L$  - Linear Dimension change due to expansion

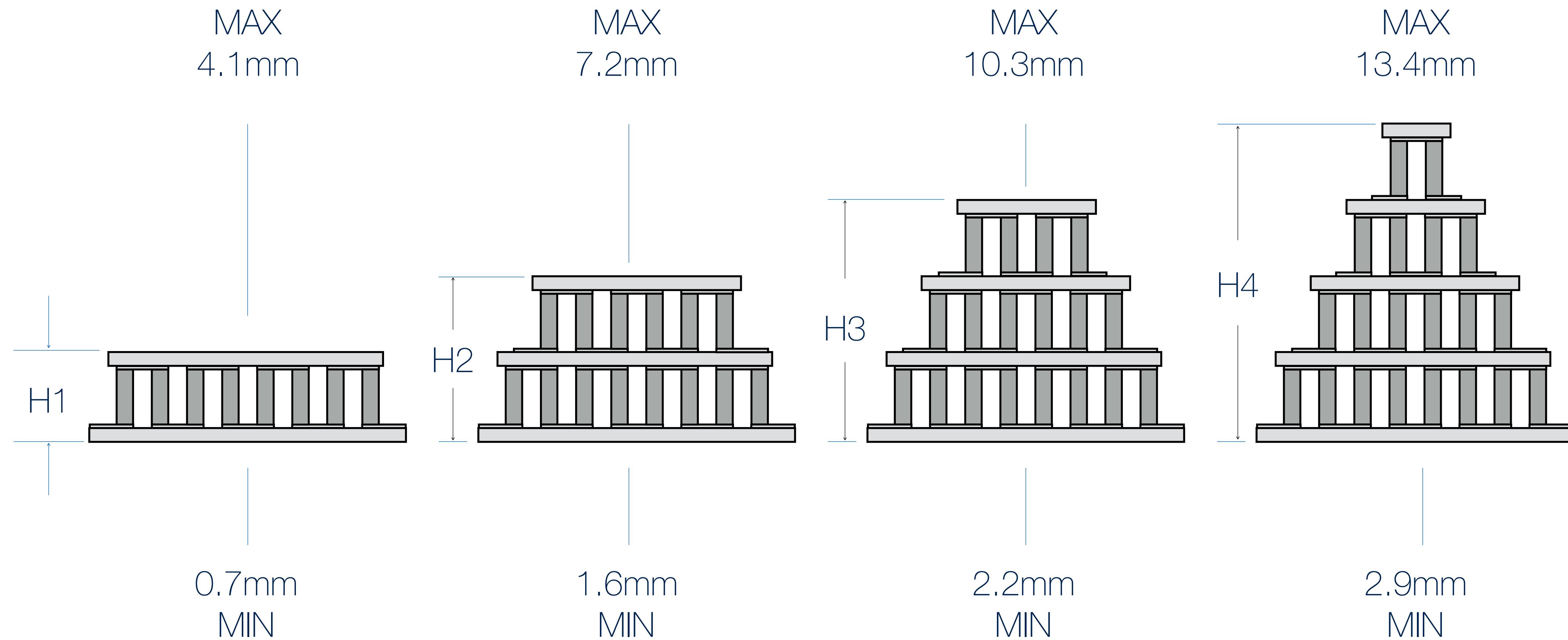
CTE - Material Thermal Expansion Coefficient

$\Delta T$  - Temperature Difference

The bigger TEC linear dimensions  $L_0$  is, the bigger is bending force affect and mechanical strains inside TEC



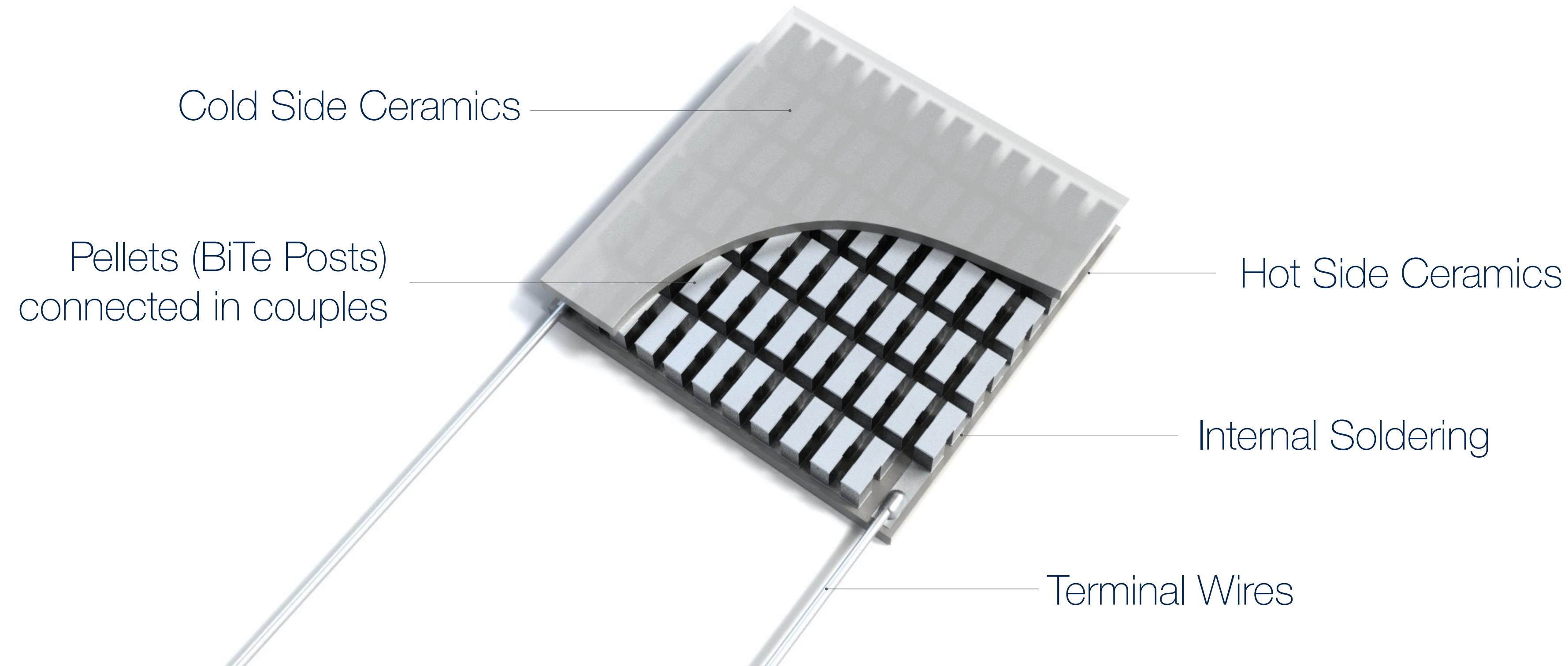
## Minimum and Maximum possible TEC Heights for TEC Microsystems TE Coolers



The values specified are absolute MIN and MAX Height values for TEC Microsystems TE Coolers.



## “Micro” and “Macro” TE Coolers, Technologies and Differences

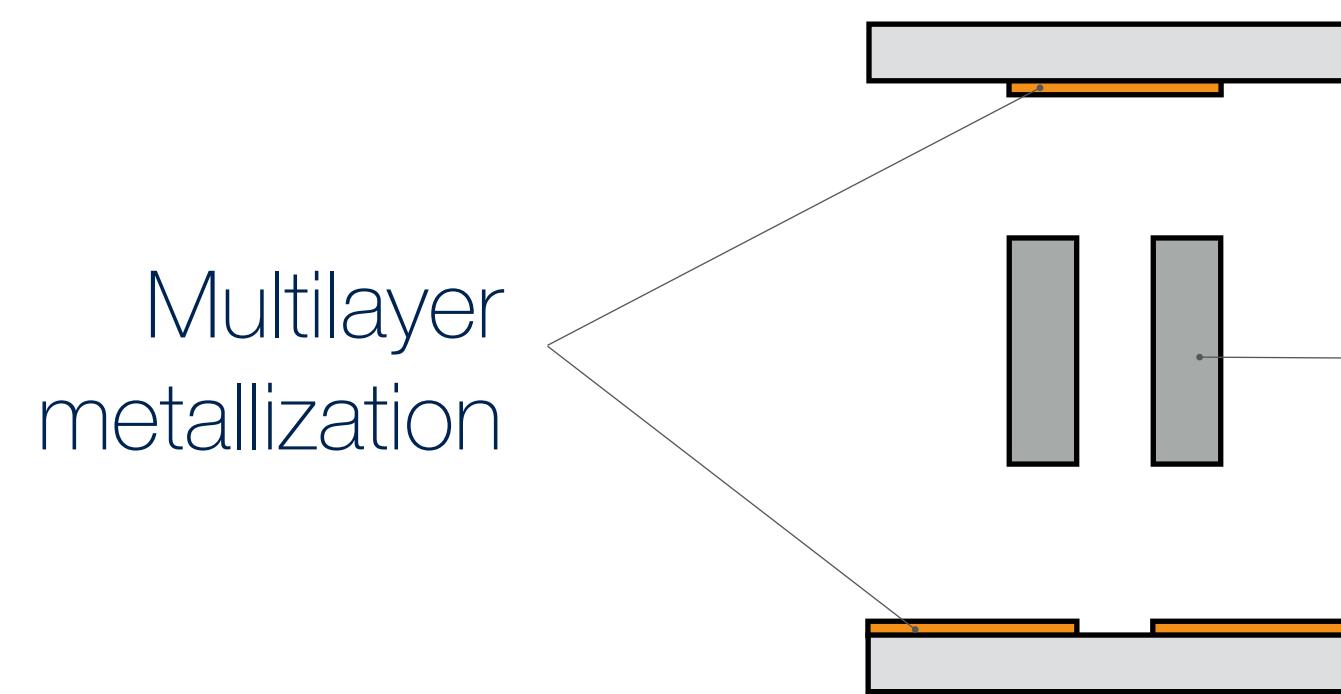


The differences between miniature “micro” TECs and large “macro” TECs (besides the size) are in assembly technology, pellets junctions methods and in BiTe material growing process



## BULK Technology - “Micro” and “Macro” TE Coolers, General Technology Differences

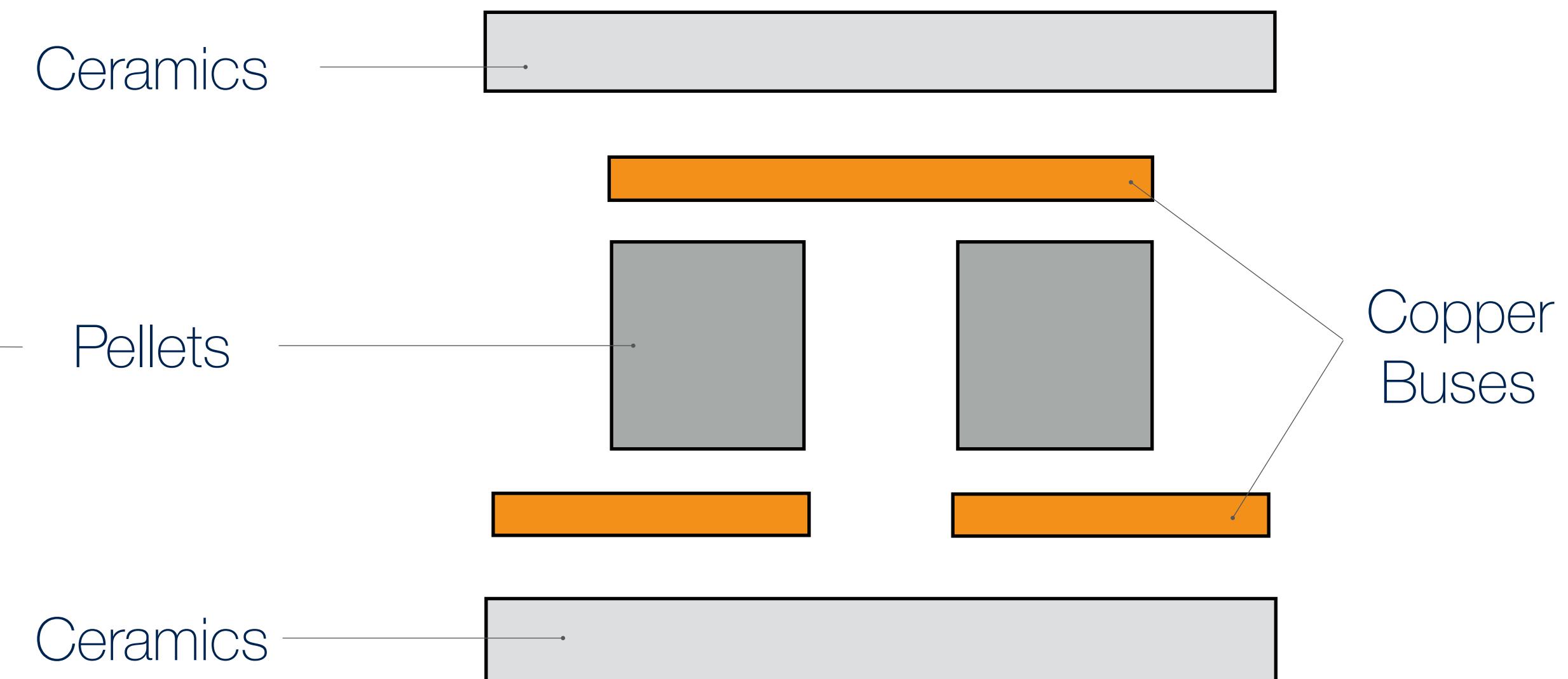
“Micro” TEC



Junctions are created by metallization sputtering on ceramics

Small pellets, precise pellets positioning, small distances between elements

“Macro” TEC

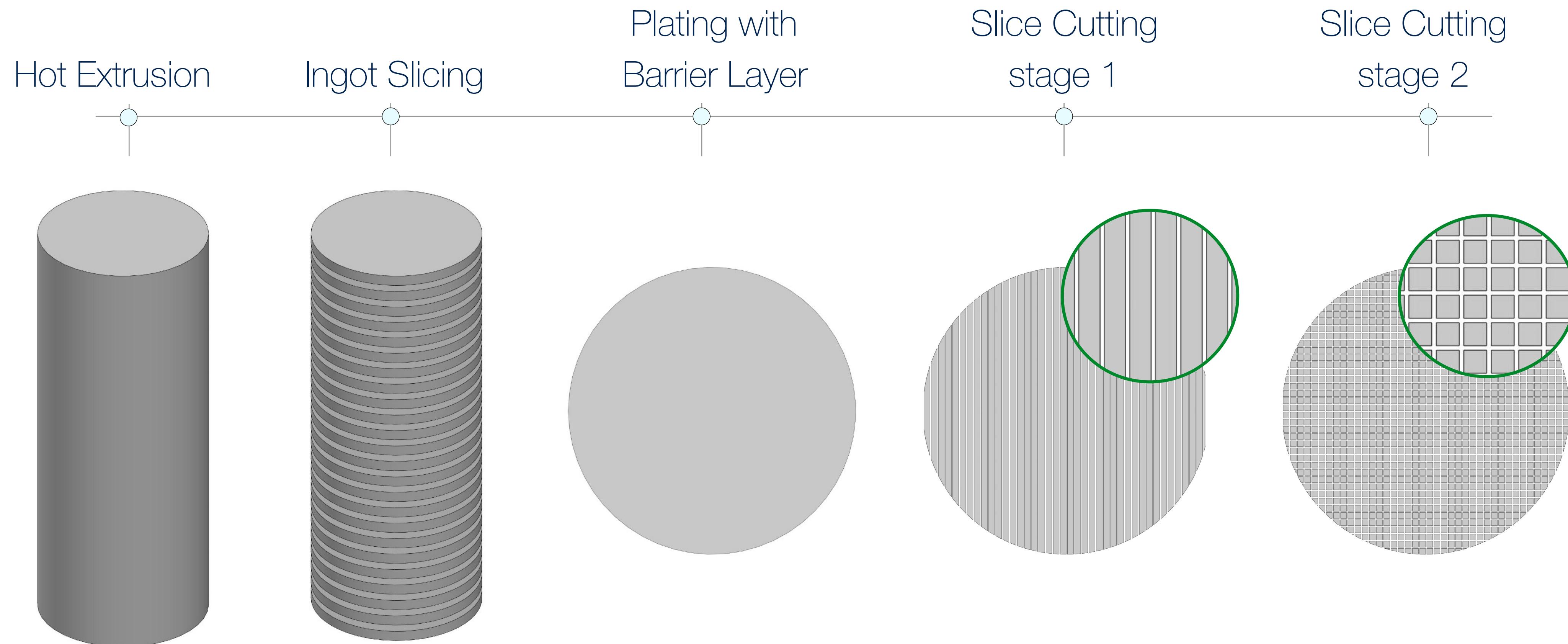


Junctions are created by Copper buses brazed onto ceramics with metallization

Large pellets, large distances between elements, high-precision is not required.



## Thermoelectric Cooler Pellets Material - BiTe



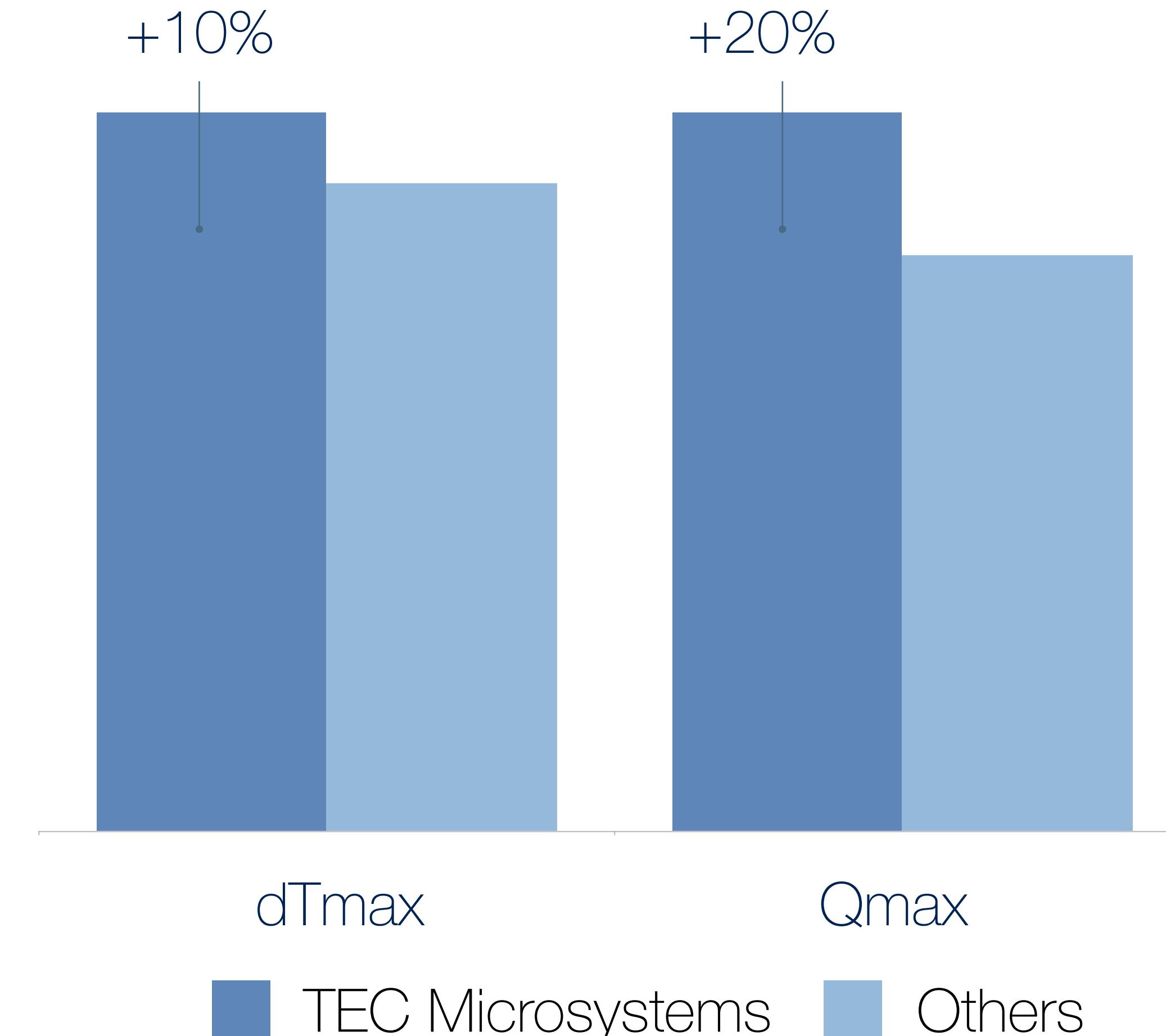
TEC Microsystems TECs use the best method for BiTe manufacturing - Hot Extrusion with several know-how



# High-Quality BiTe Material for Bulk Technology TE Coolers



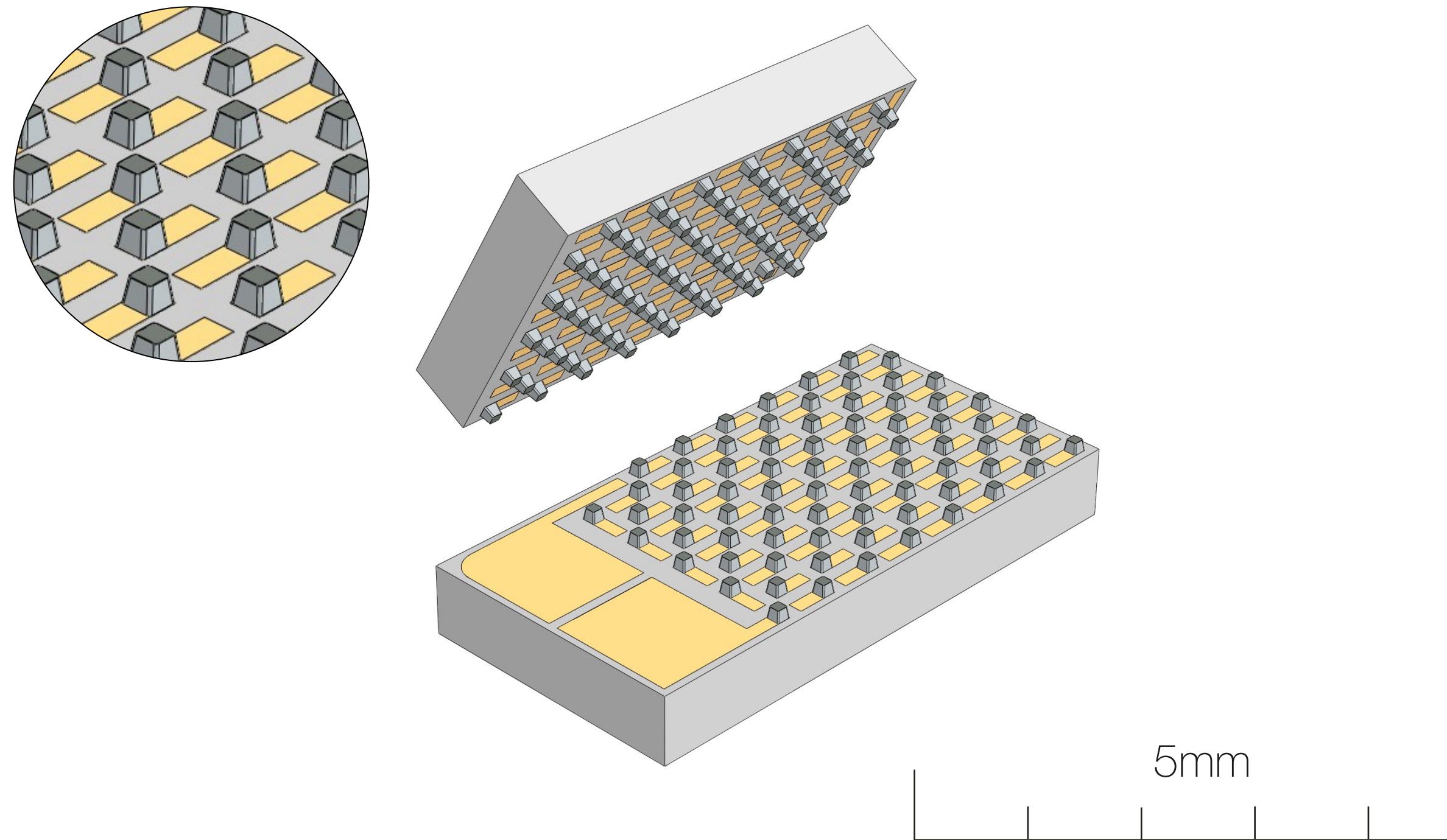
- In-house Manufacturing
- Hot Extrusion Process
- Advanced Performance
- Processing with nanotechnology





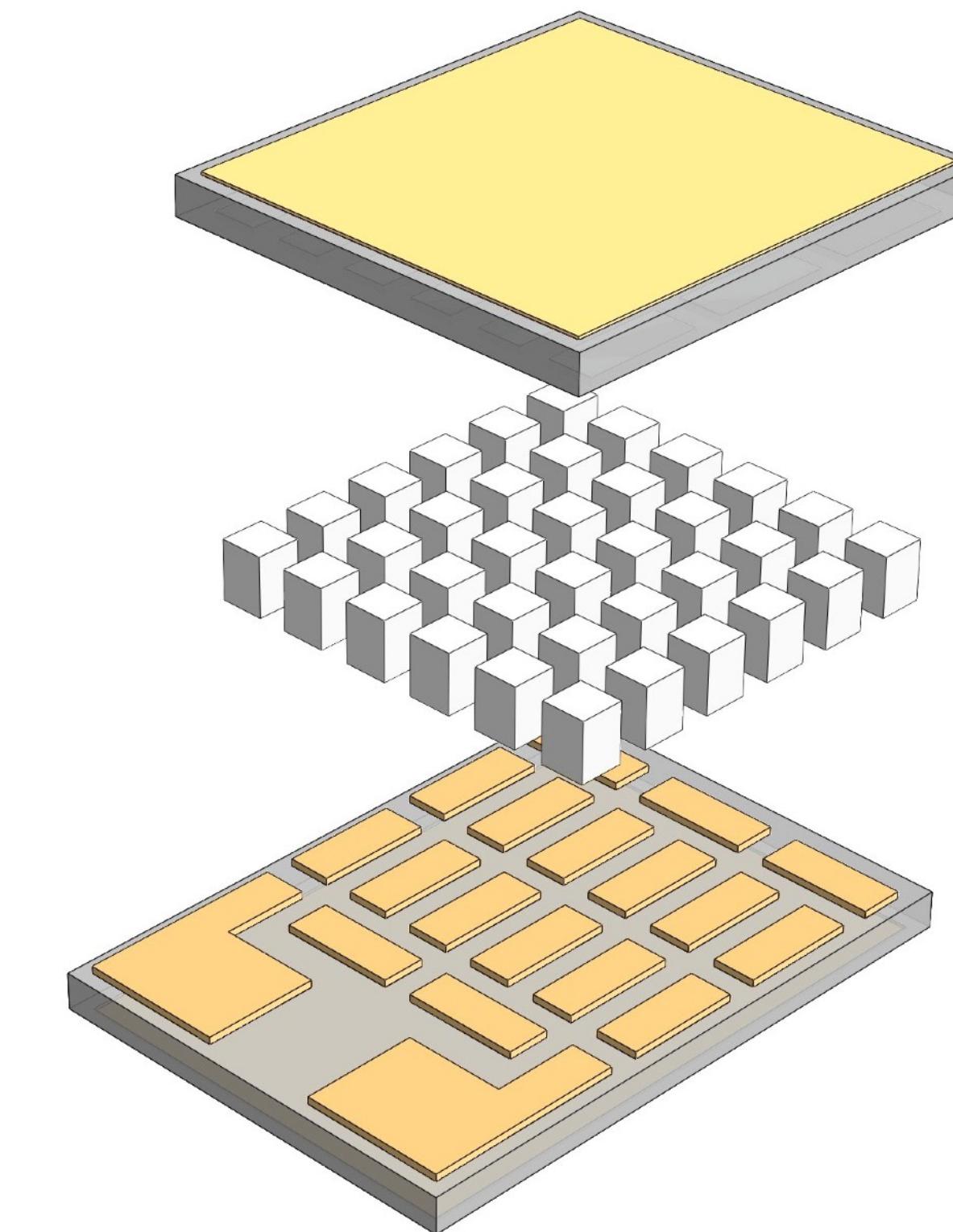
## Miniature TE Coolers: BULK TECs and Thin-film TECs

Thin-film TE Cooler



BiTe pellets are grown on a substrate  
by thin-film process

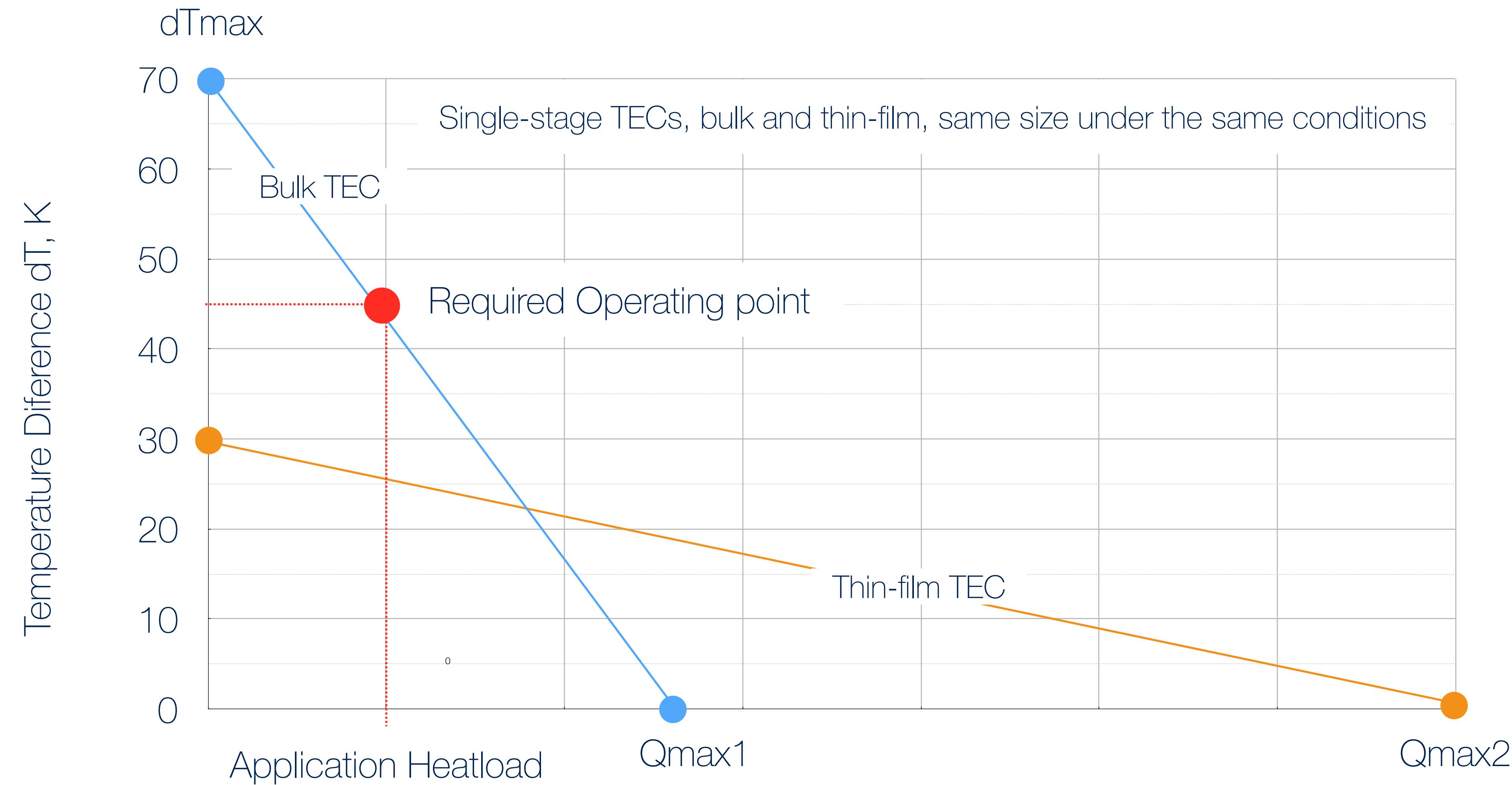
Bulk Technology TE Cooler



BiTe material is manufactured in ingots,  
cut into pellets and soldered to metallization on ceramics



## Thin-film and Bulk TECs Performance Differences

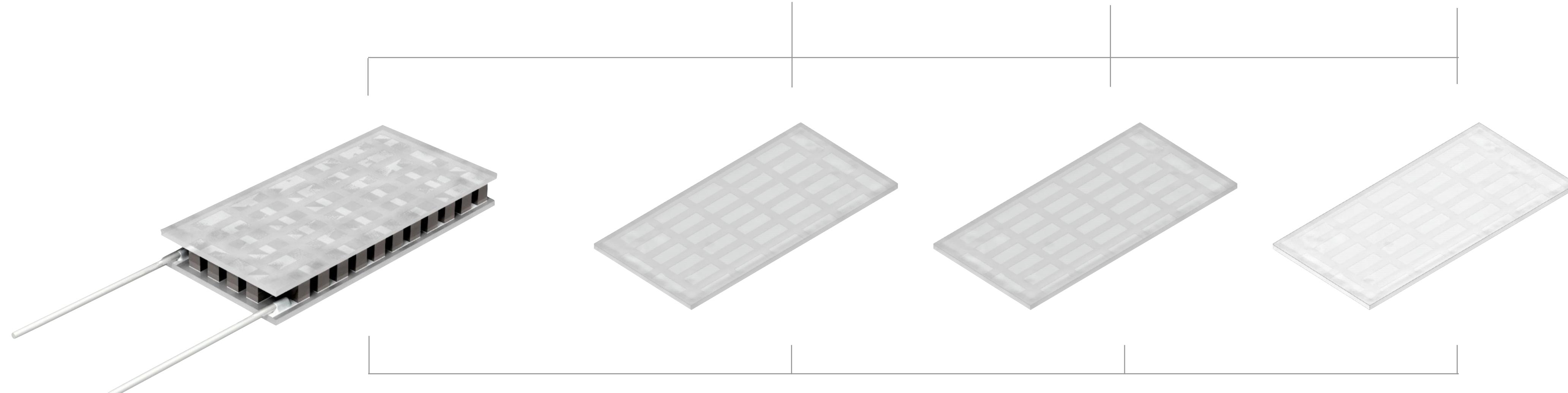


Thin-film TECs may have higher cooling capacity than bulk TEC on the same size, but way lower  $dT_{max}$



## Thermoelectric Cooler Ceramics Materials

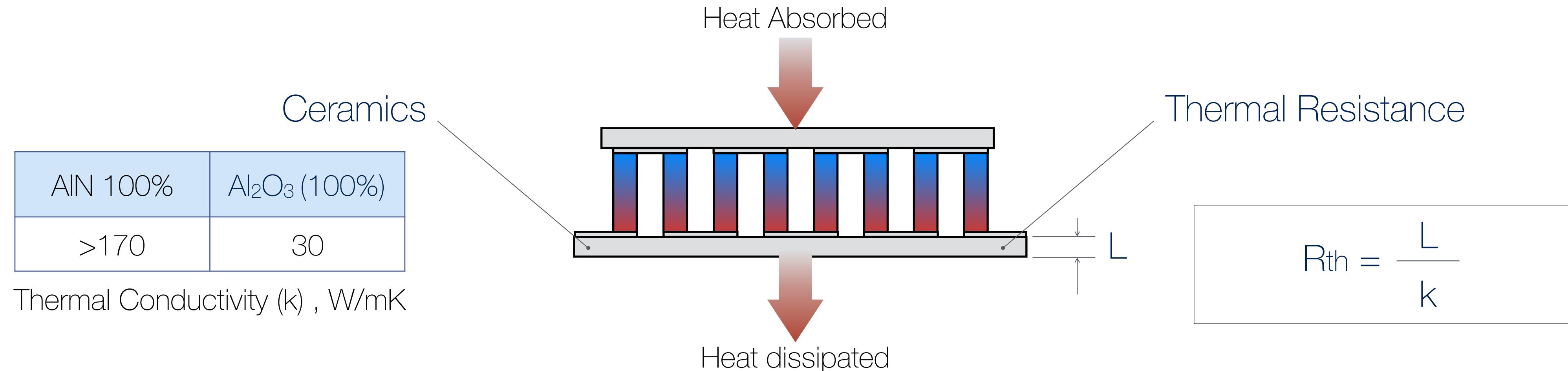
Property	Units	AlN 100%	Al2O3 100%	Al2O3 96%
Thermal Conductivity	W/(m x K)	>170	30	24
Thermal Expansion	$10^{-6}K^{-1}$	4.8	7.2	7
Electrical Resistivity	Ohm x cm	> $10^{14}$	> $10^{14}$	> $10^{14}$



TEC Microsystems uses 100% Al<sub>2</sub>O<sub>3</sub> and AlN Ceramics for thermoelectric cooler manufacturing



## TEC Ceramics Material and Performance Parameters



Parameters	1MD03-015-04	1ML06-023-05	1MC06-126-03
Dimensions, mm <sup>2</sup>	2.5 x 3.9	6.0 x 8.2	16.0 x 18.0
Ceramics Material	Al <sub>2</sub> O <sub>3</sub> → AlN	Al <sub>2</sub> O <sub>3</sub> → AlN	Al <sub>2</sub> O <sub>3</sub> → AlN
dTmax, K (@27°C)	71 → 72	69 → 71	67 → 69
Qmax, W (@27°C)	1.18 → 1.23	5.4 → 5.8	46.15 → 51.60

+4%

+7%

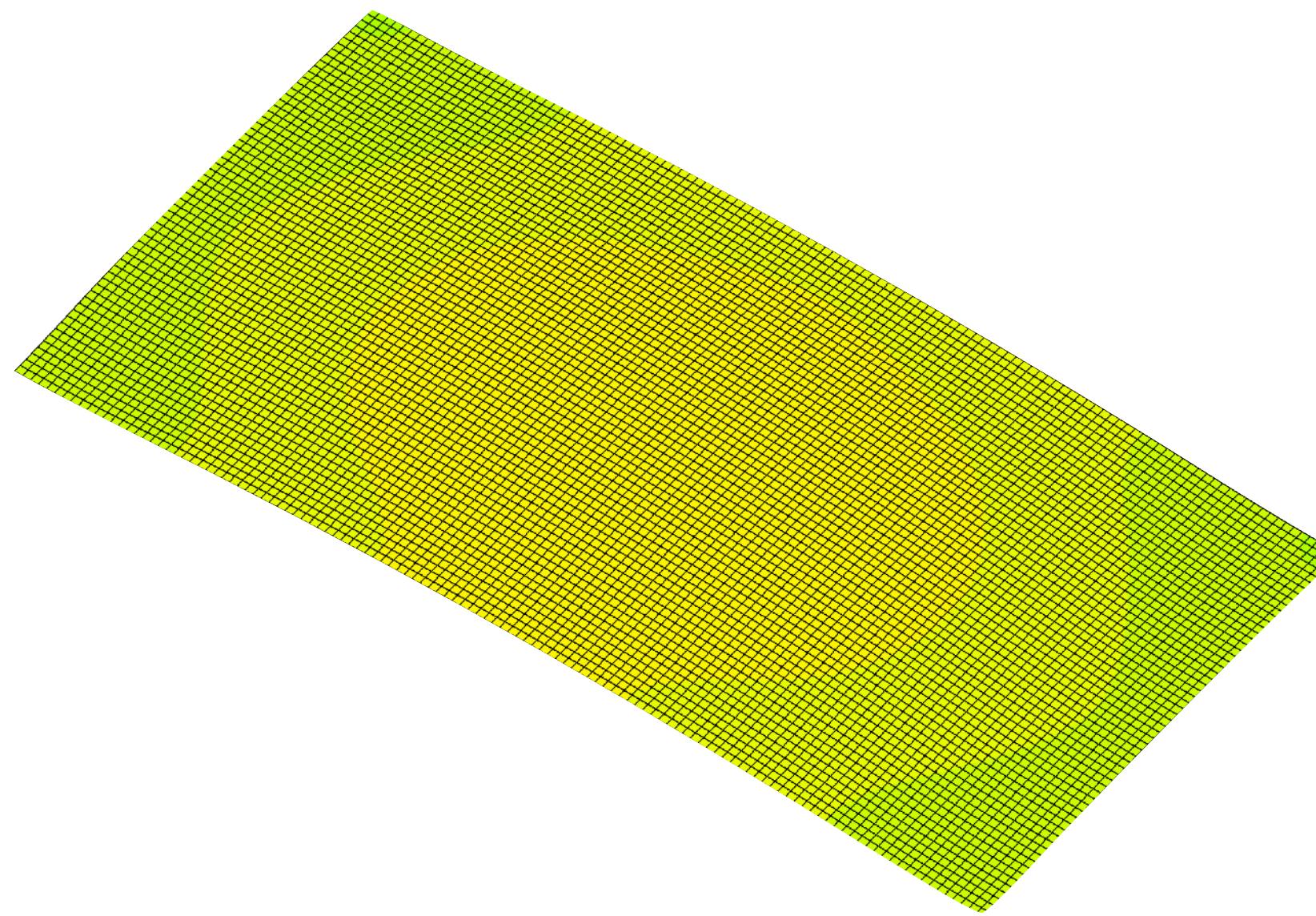
+12%

AlN Ceramics can increase TEC cooling performance, especially for powerful (by Qmax) TECs. In case of micro-TECs for low-power applications it's less visible.



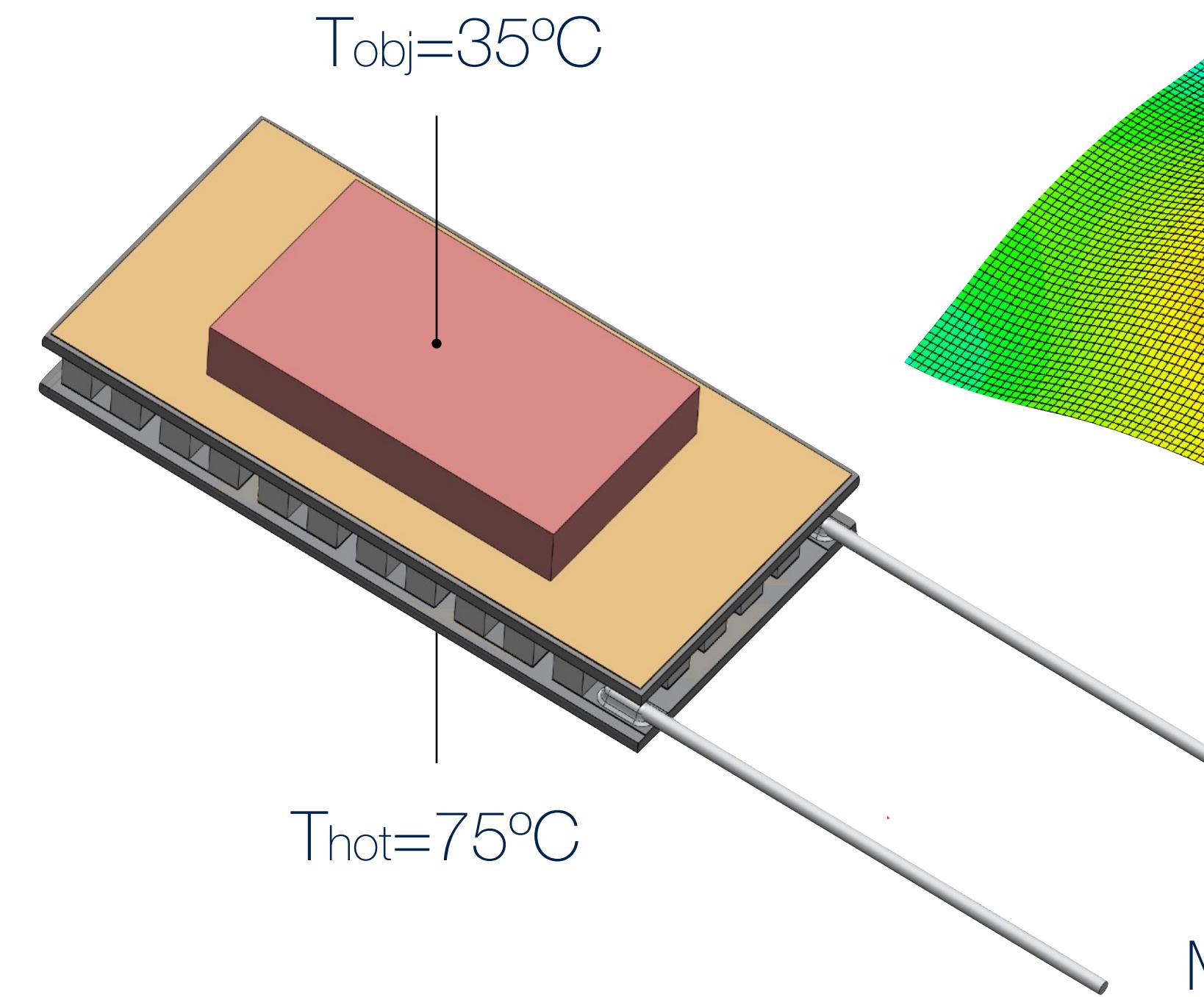
## Ceramics Material and Temperature Uniformity (Example #1)

AlN 0.25mm Ceramics

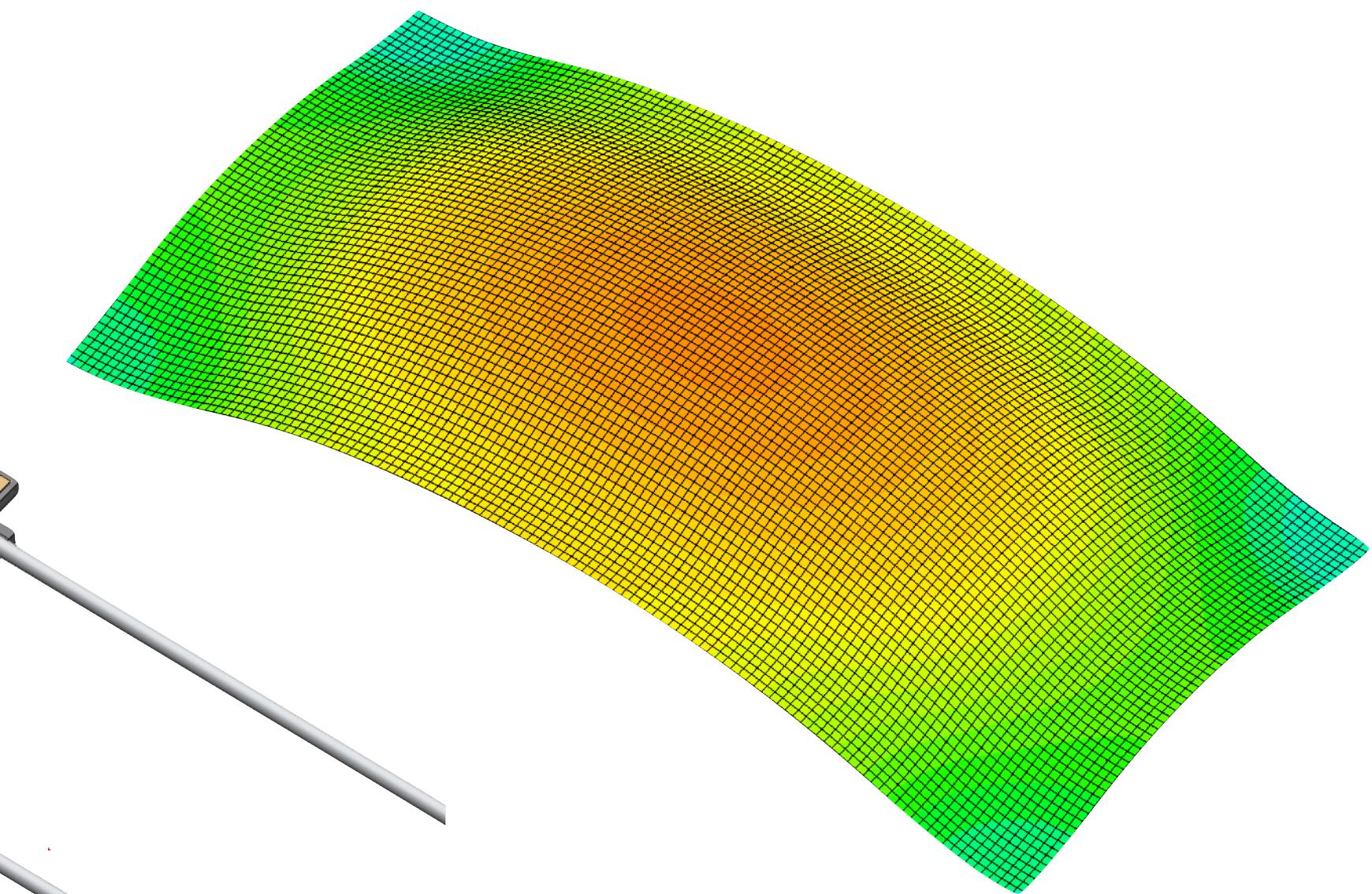


Mean temperature difference  
(among surface)  
0.26 °C

Heatload 0.6W



$\text{Al}_2\text{O}_3$  0.25mm Ceramics



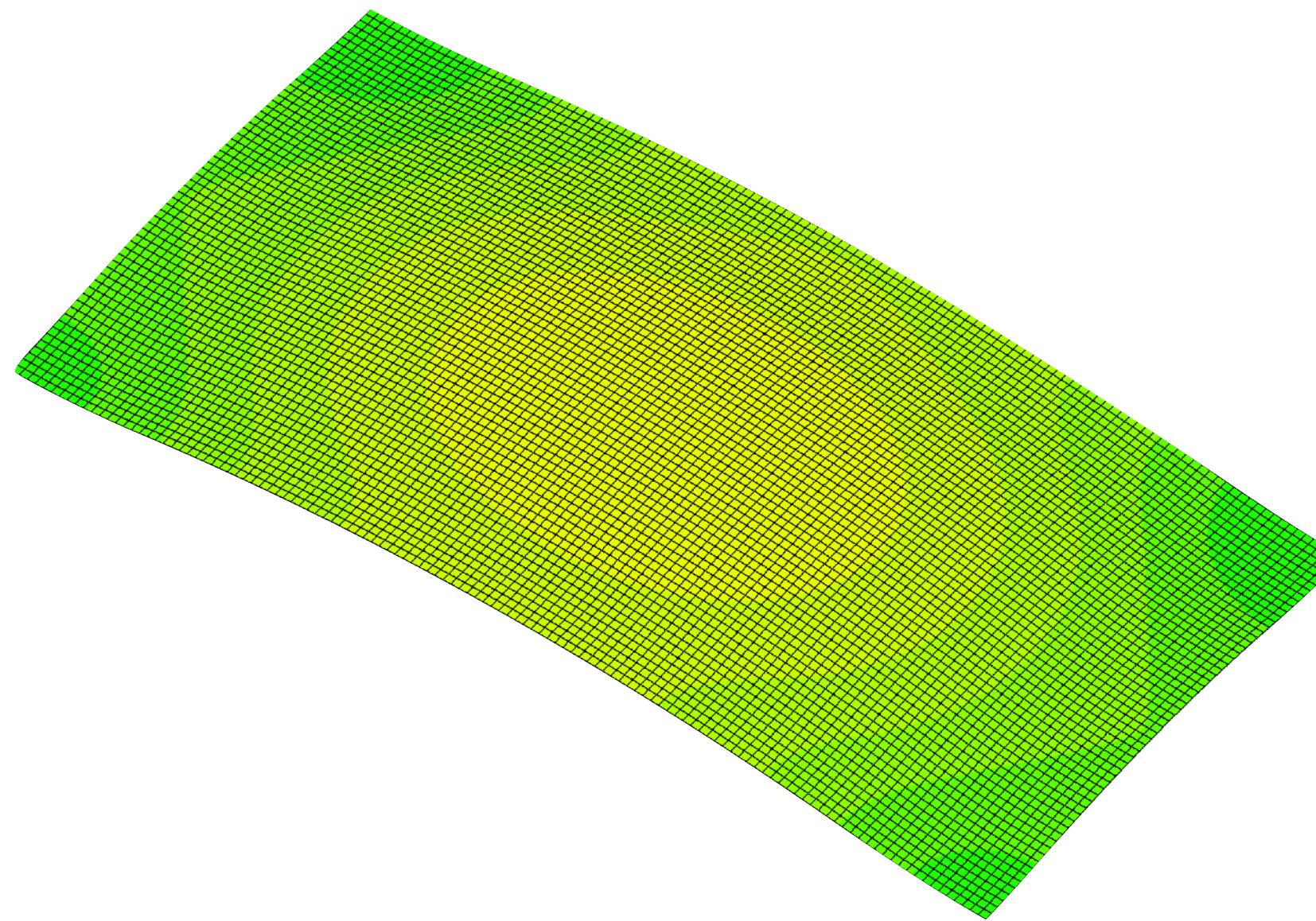
Mean temperature difference  
(among surface)  
1.48 °C

The difference in temperature uniformity among surface between  $\text{Al}_2\text{O}_3$  and AlN ceramics may be valuable.



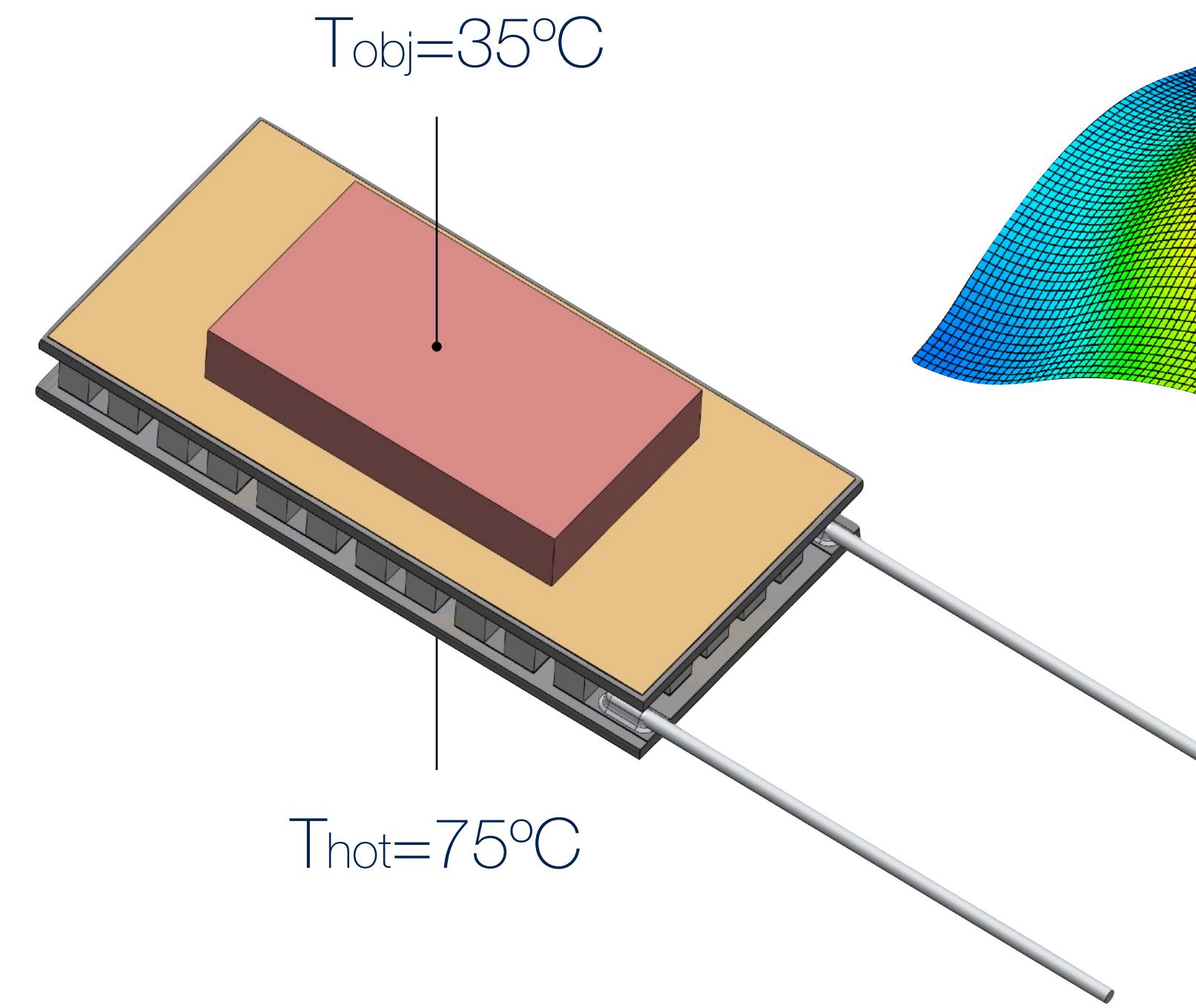
## Ceramics Material and Temperature Uniformity (Example #2)

AlN 0.25mm Ceramics

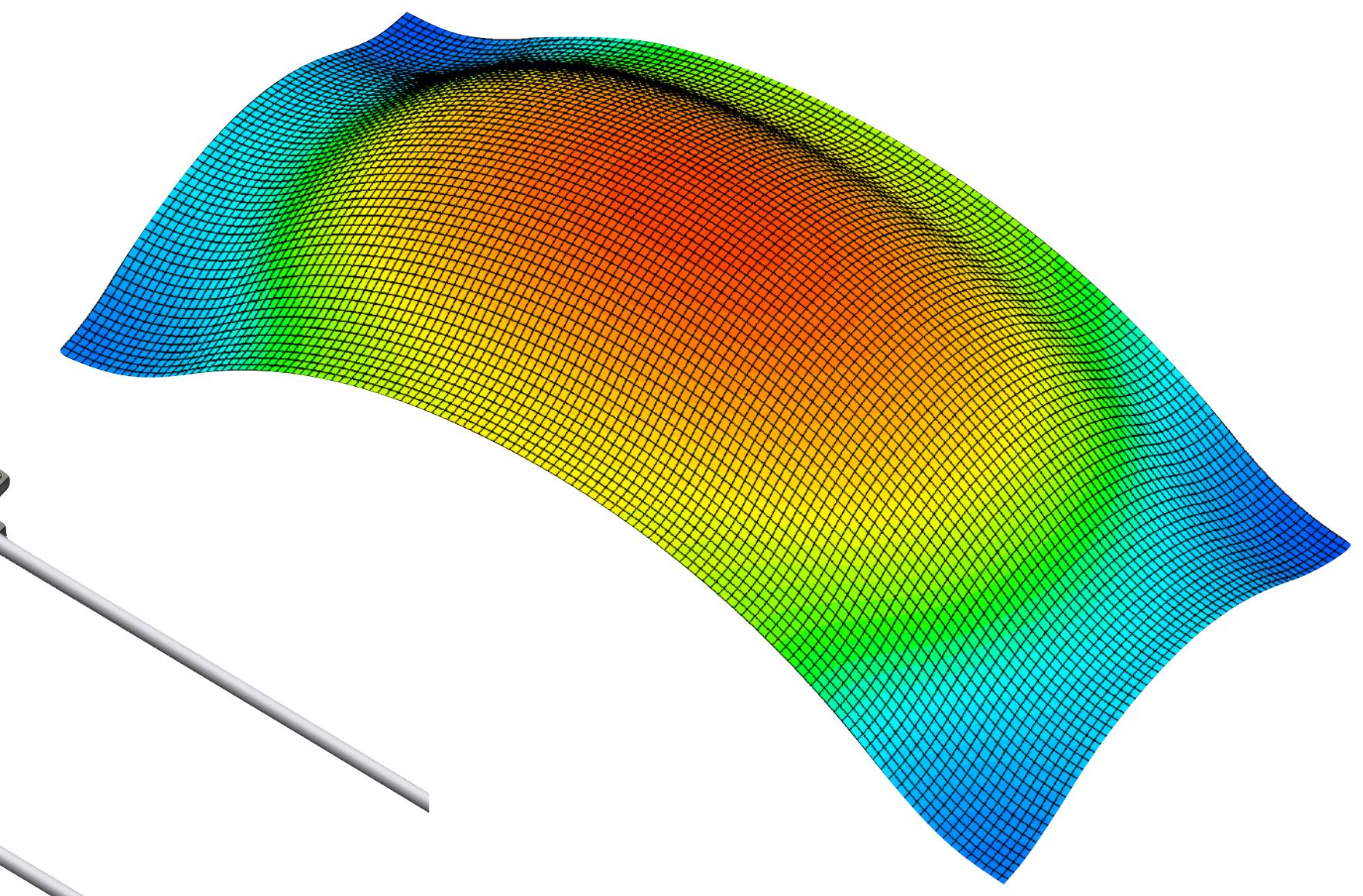


Mean temperature difference  
(among surface)  
0.53 °C

Heatload 1.2W



$\text{Al}_2\text{O}_3$  0.25mm Ceramics



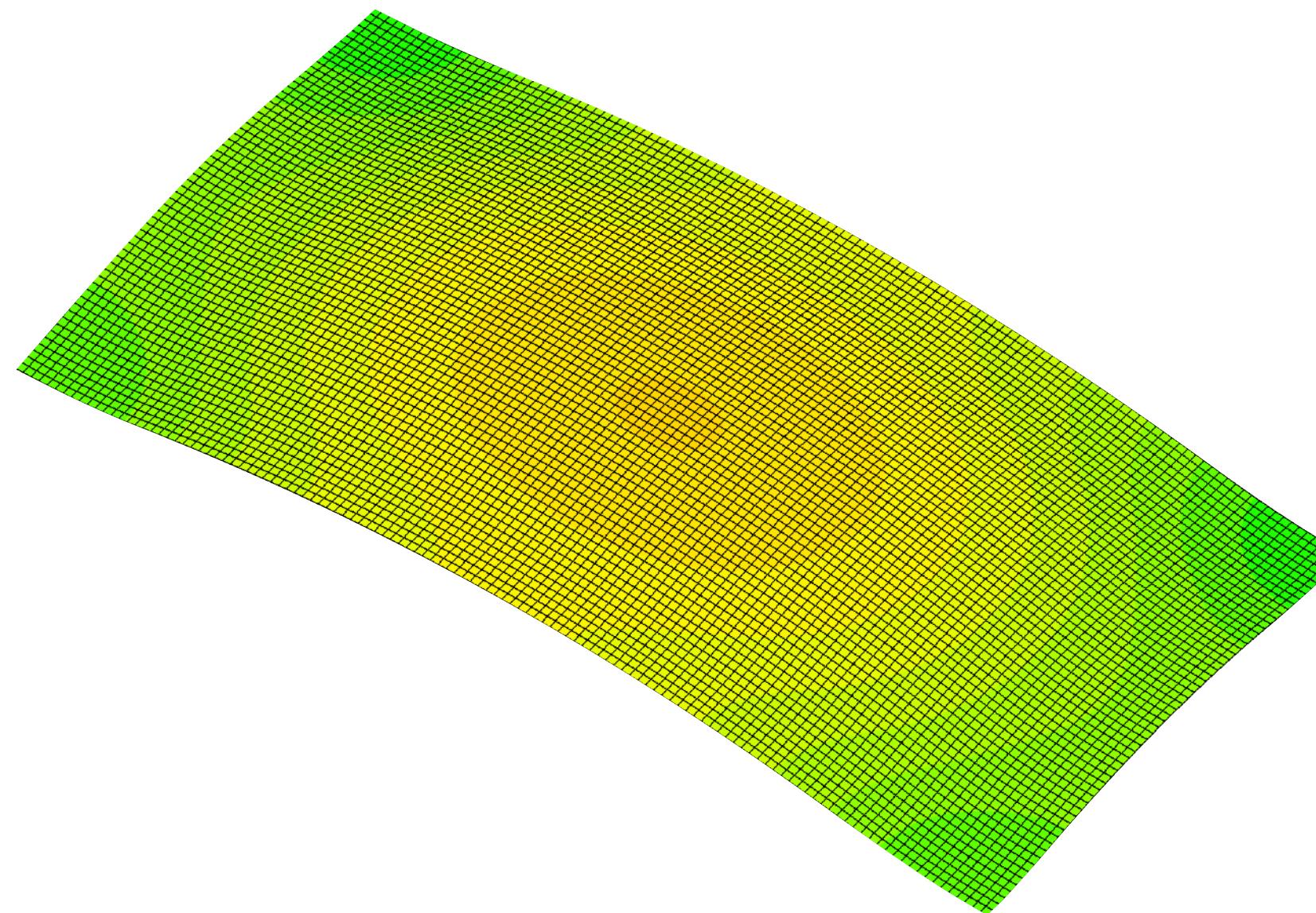
Mean temperature difference  
(among surface)  
2.95 °C

The difference in temperature uniformity among surface between  $\text{Al}_2\text{O}_3$  and AlN ceramics may be valuable.



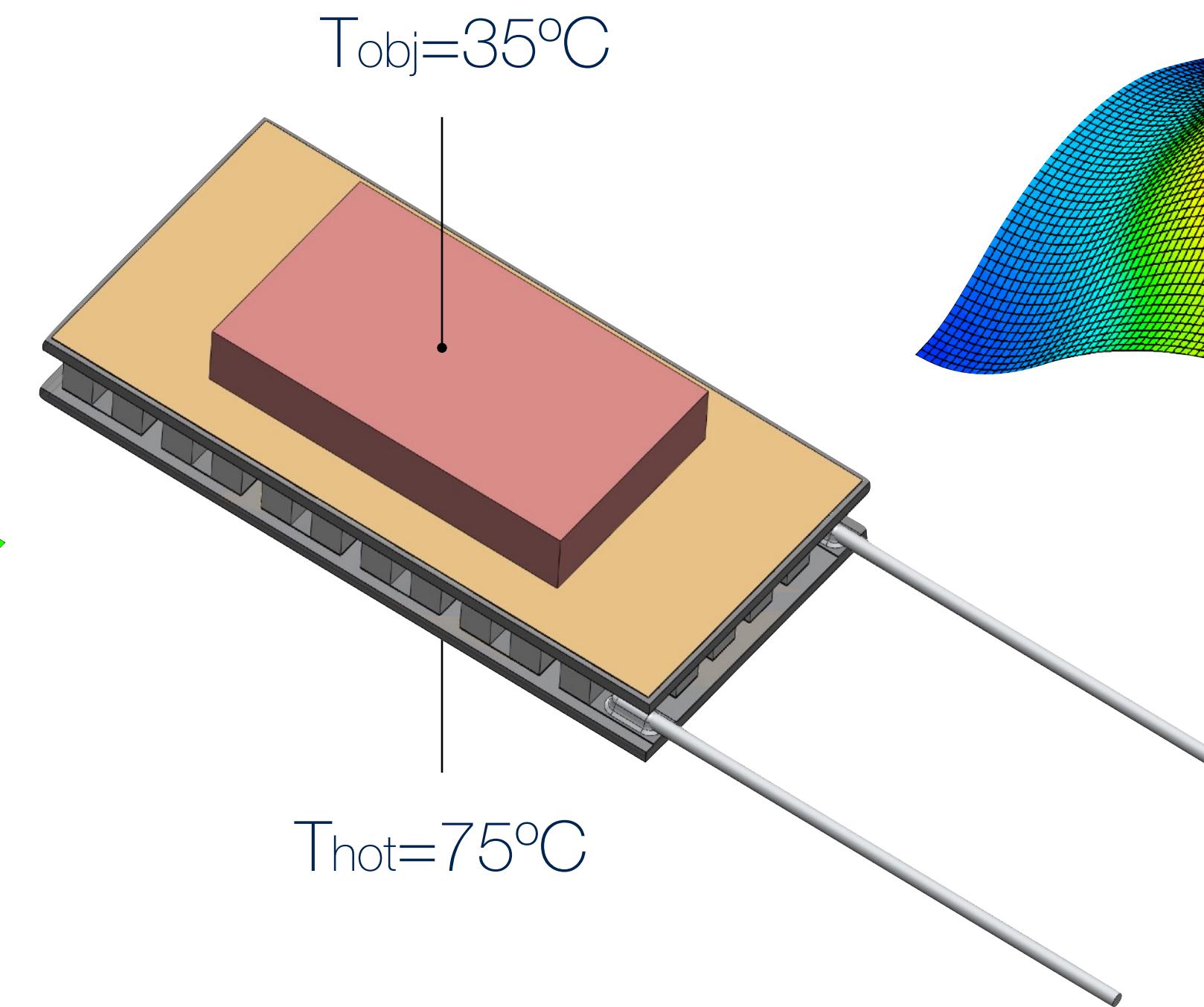
## Ceramics Material and Temperature Uniformity (Example #3)

AlN 0.25mm Ceramics

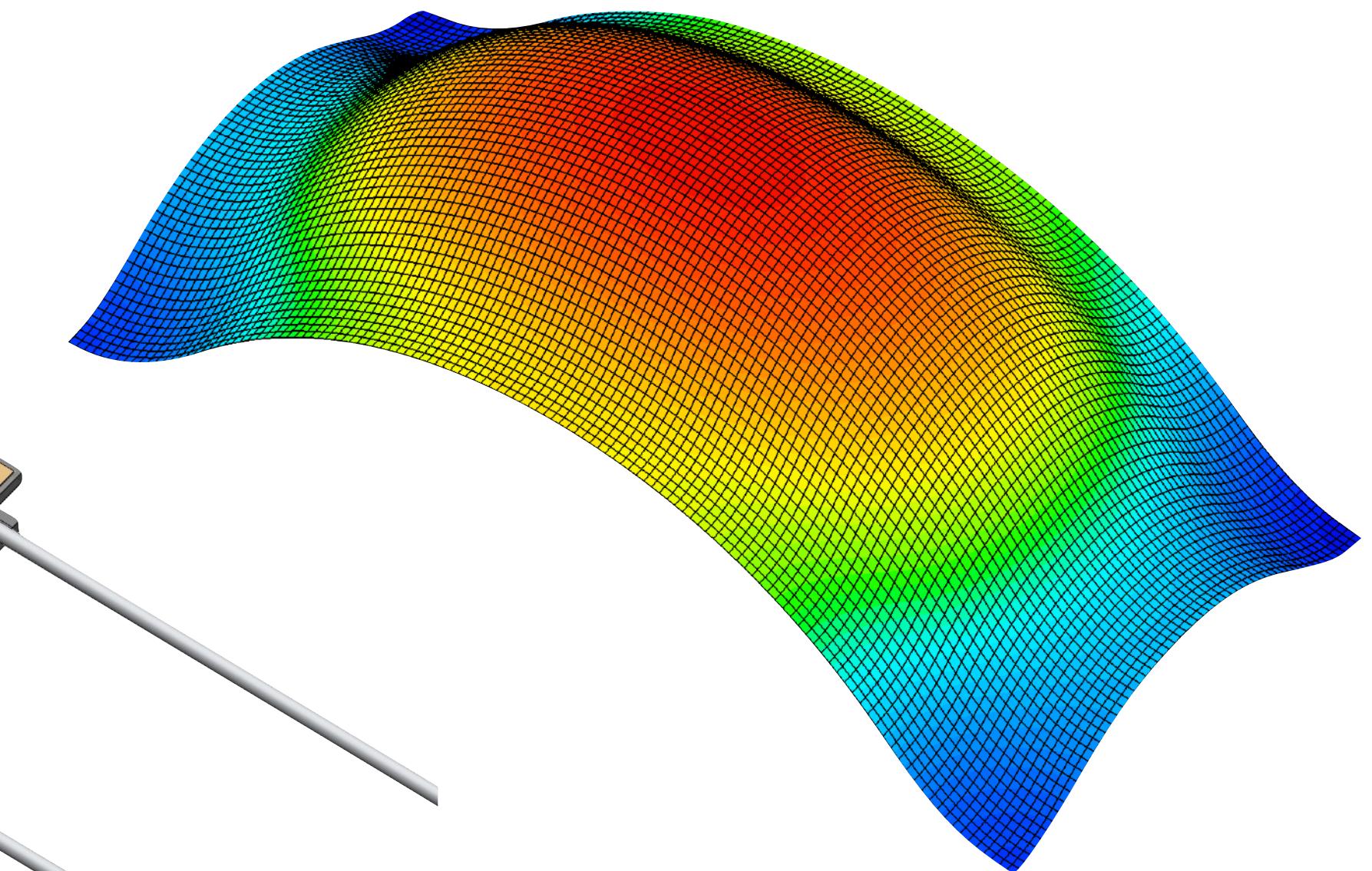


Mean temperature difference  
(among surface)  
0.66 °C

Heatload 1.5W



$\text{Al}_2\text{O}_3$  0.25mm Ceramics



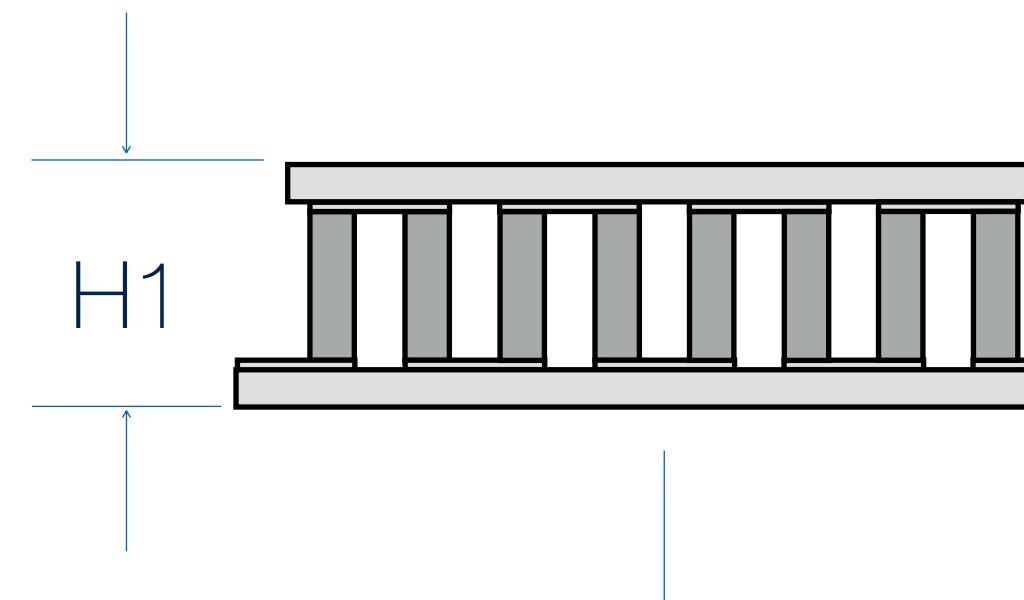
Mean temperature difference  
(among surface)  
3.67 °C

The difference in temperature uniformity among surface between  $\text{Al}_2\text{O}_3$  and AlN ceramics may be valuable.



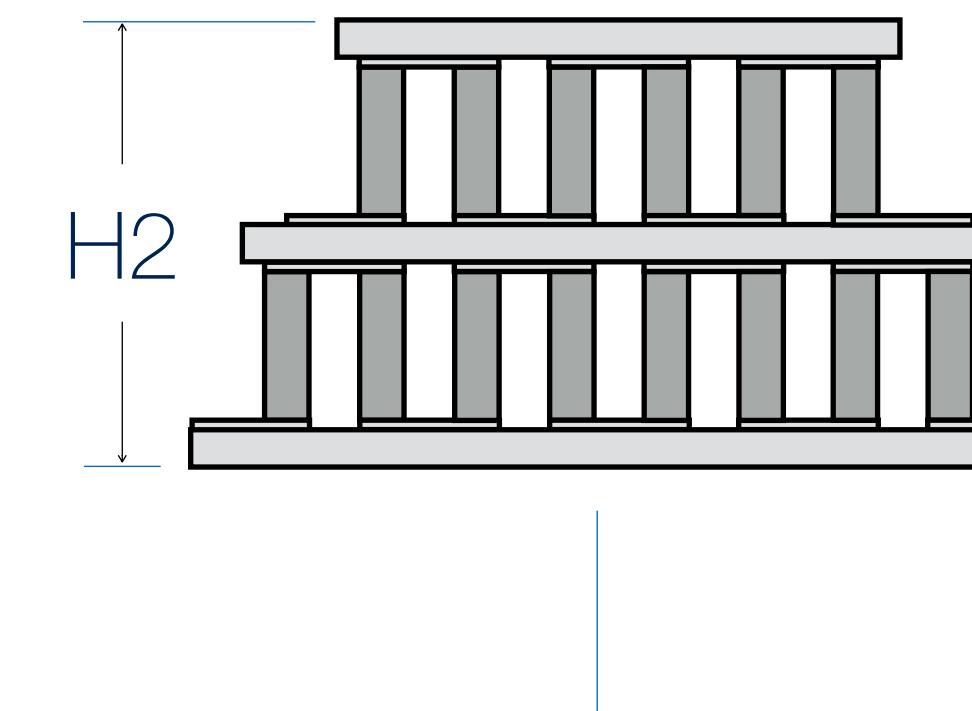
## Standard TEC Microsystems TEC Height Tolerances

Single-stage TECs



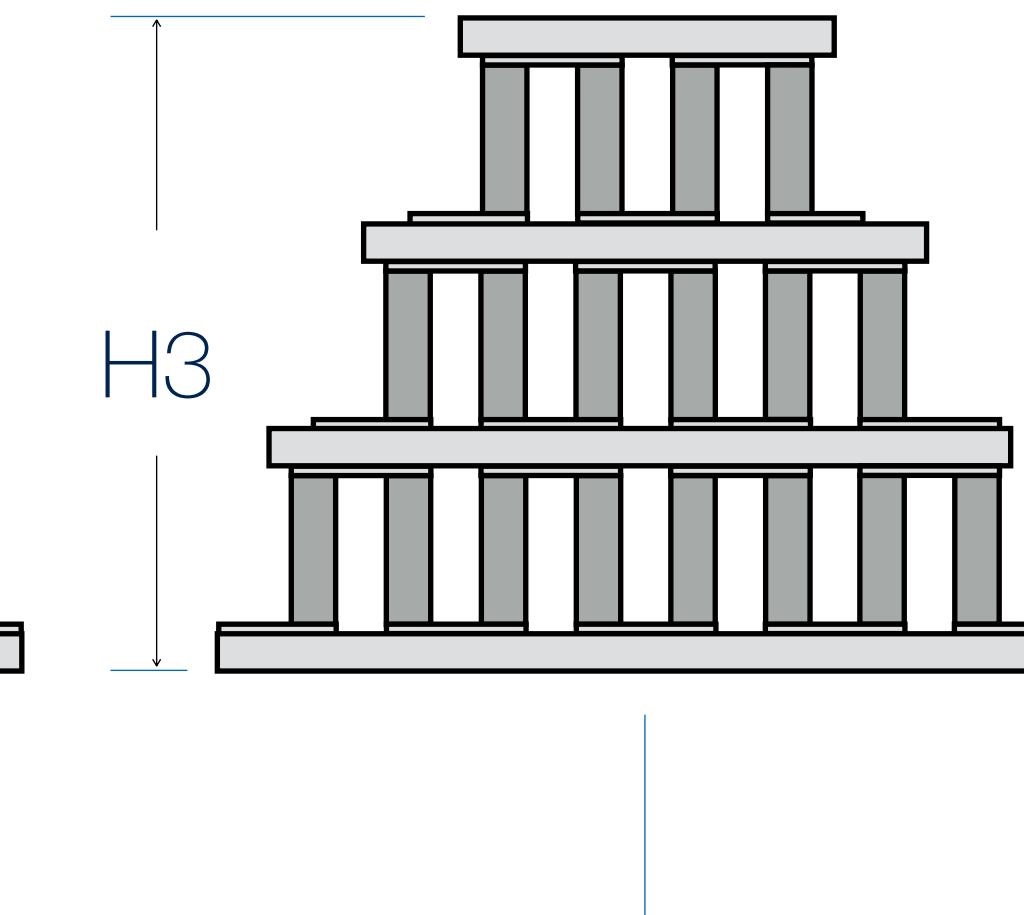
$H_1 \pm 0.1\text{mm}$

Two-stage TECs



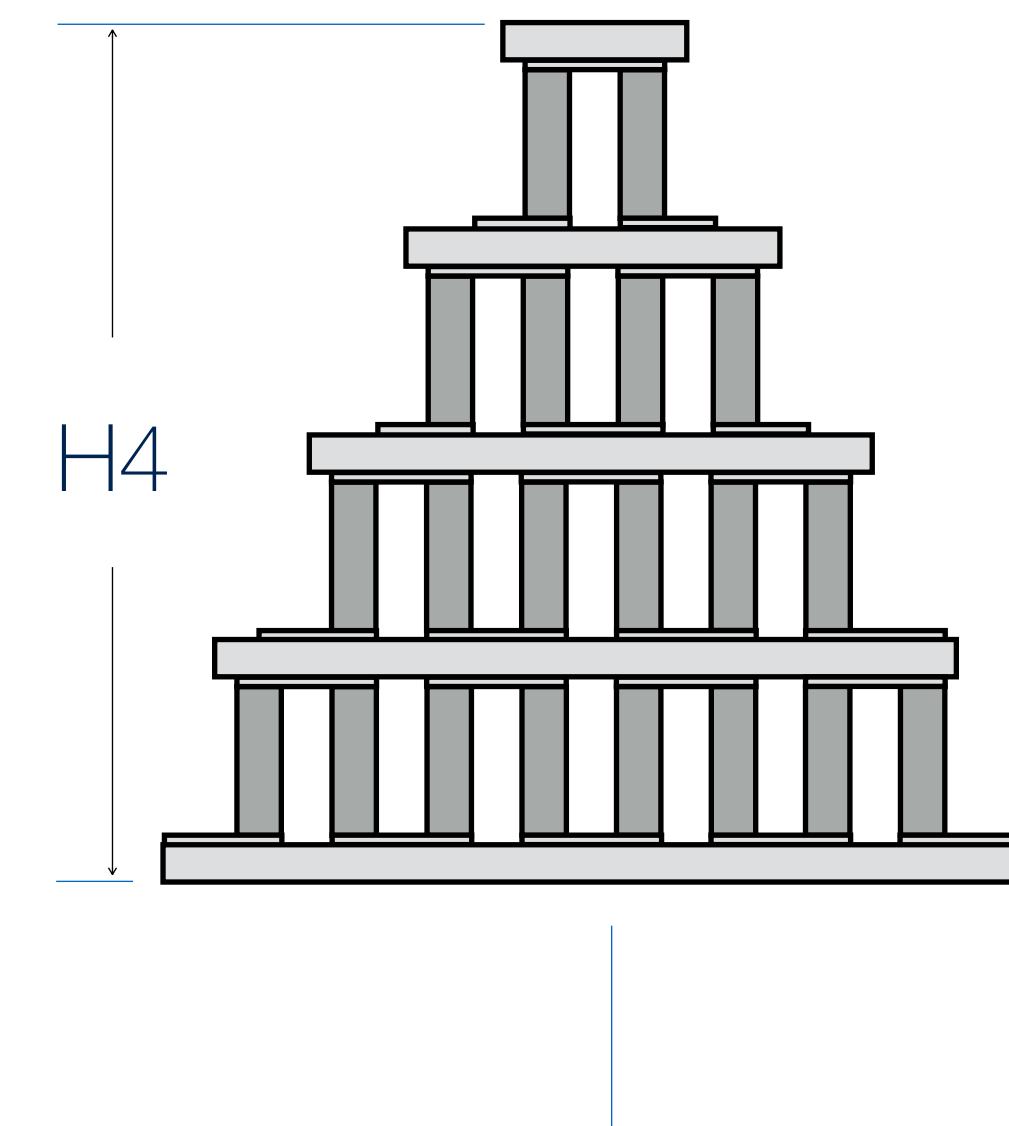
$H_2 \pm 0.1\text{mm}$

Three-stage TECs



$H_3 \pm 0.15\text{mm}$

Four-stage TECs

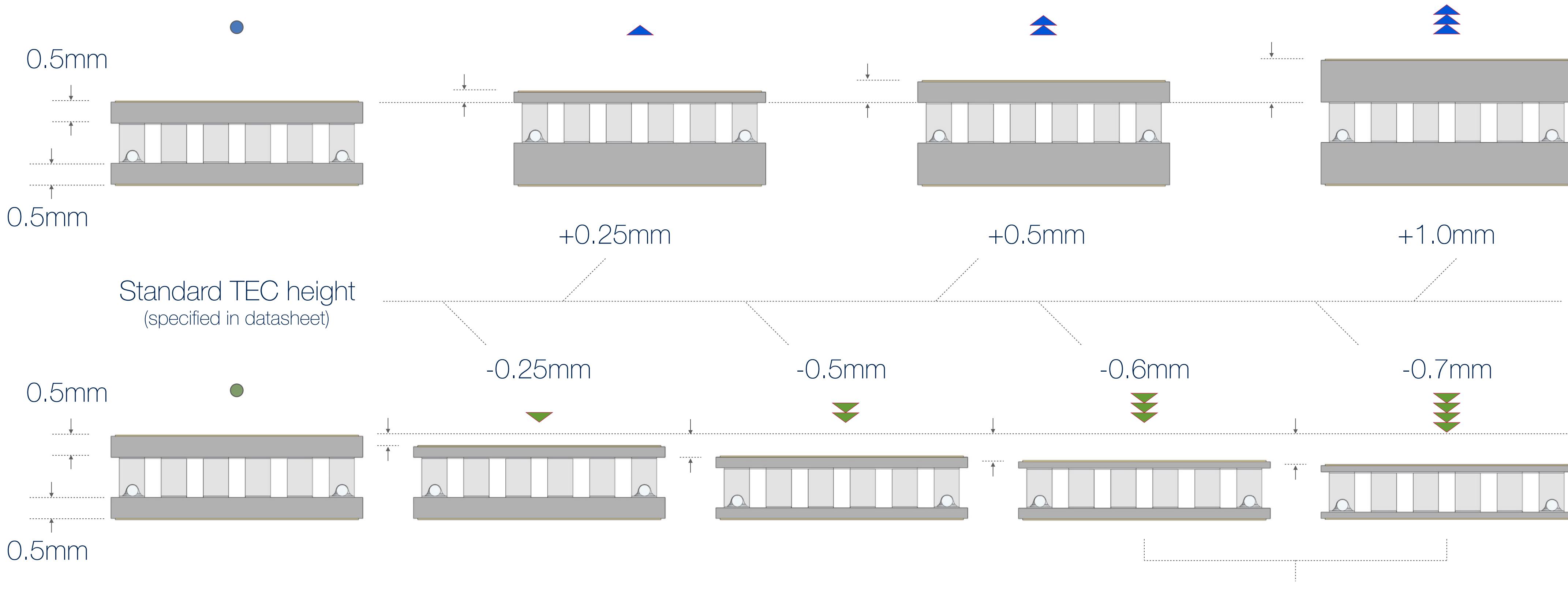


$H_4 \pm 0.2\text{mm}$

The specified Height Tolerances are provided by default for all TEC Microsystems TECs.  
Advanced TEC Height Optimization and Tolerances enhancements are available if required.



## TEC Height Variation by Ceramics Thickness - Single-stage type

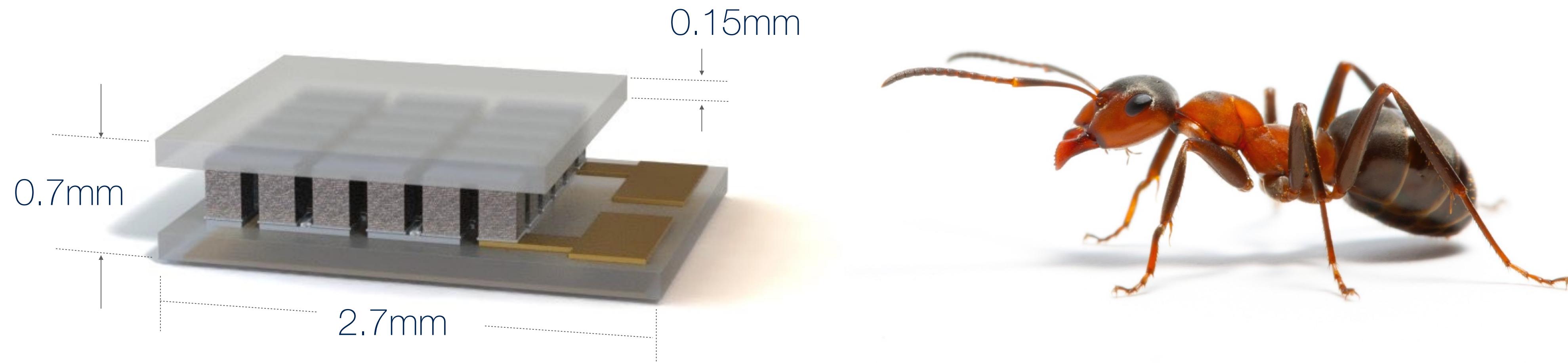


TEC Microsystems can change TEC height in a certain range by Ceramics Thickness without parameters changing



## Miniature Ultra-thin TE Coolers on 0.15mm AlN Ceramics - "ANt"

Example: 1MD02-018-03ANt - Index "ANt" indicates 0.15mm AlN Ceramics using



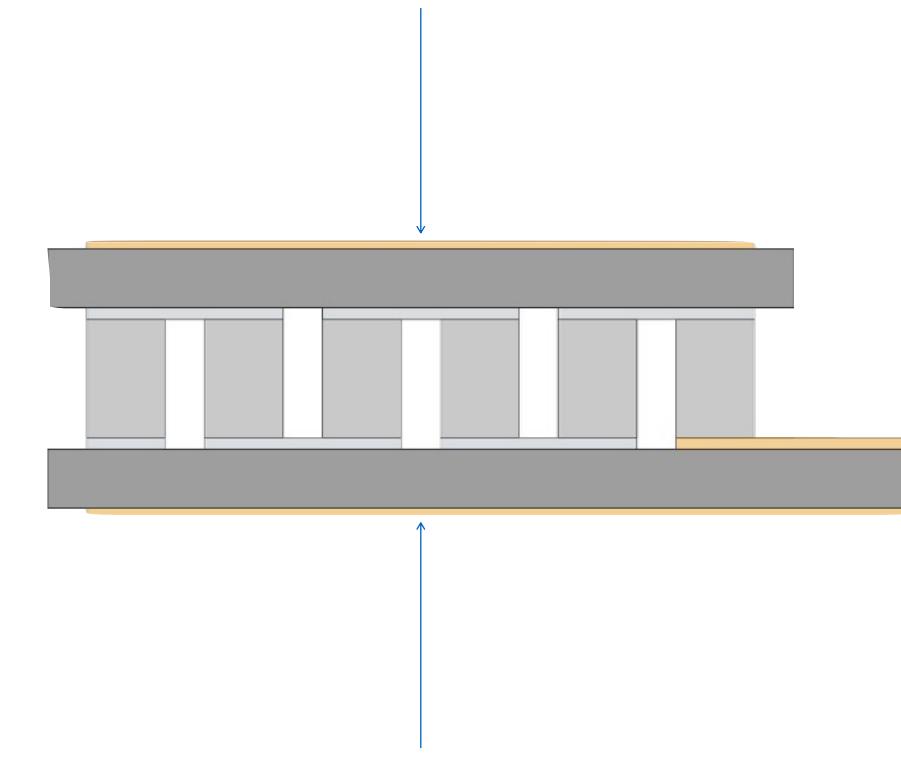
TEC Microsystems "ANt" Series of ultra-compact and ultra-thin TECs starts from 1x1mm<sup>2</sup> size and 0.7mm Height



## TEC Microsystems “ANt” TECs - Ultra-thin TEC types with precise Height Control

Example with 1MD02-012-xx/1ANt TEC Type

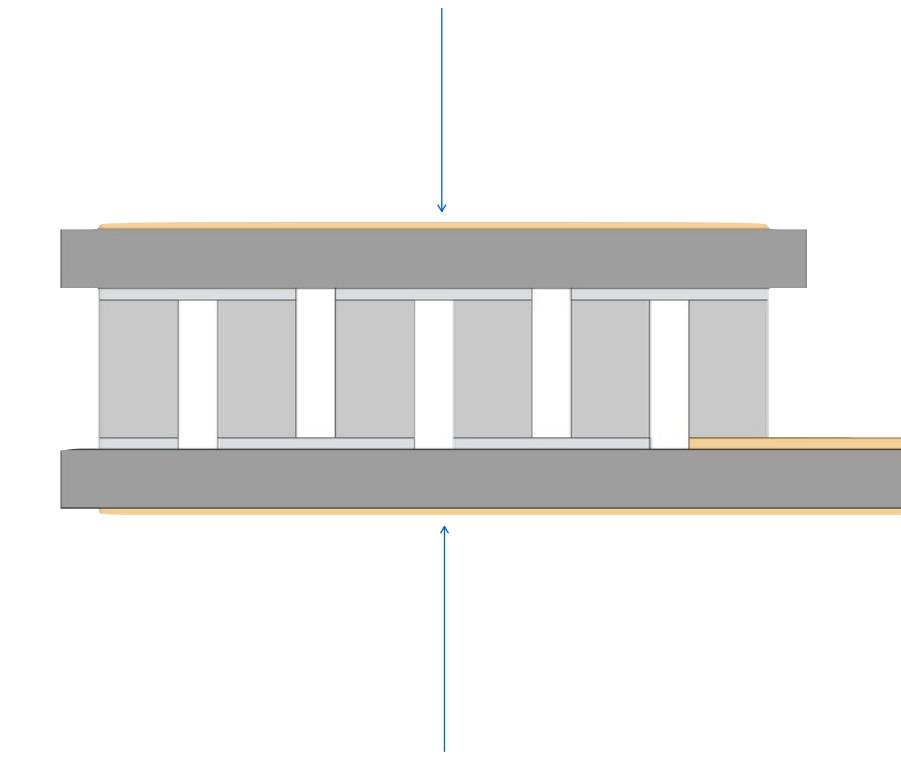
1MD02-012-03/1ANt



$H=0.69 \pm 0.05\text{mm}$

$\pm 0.03\text{mm}$   
(optional)

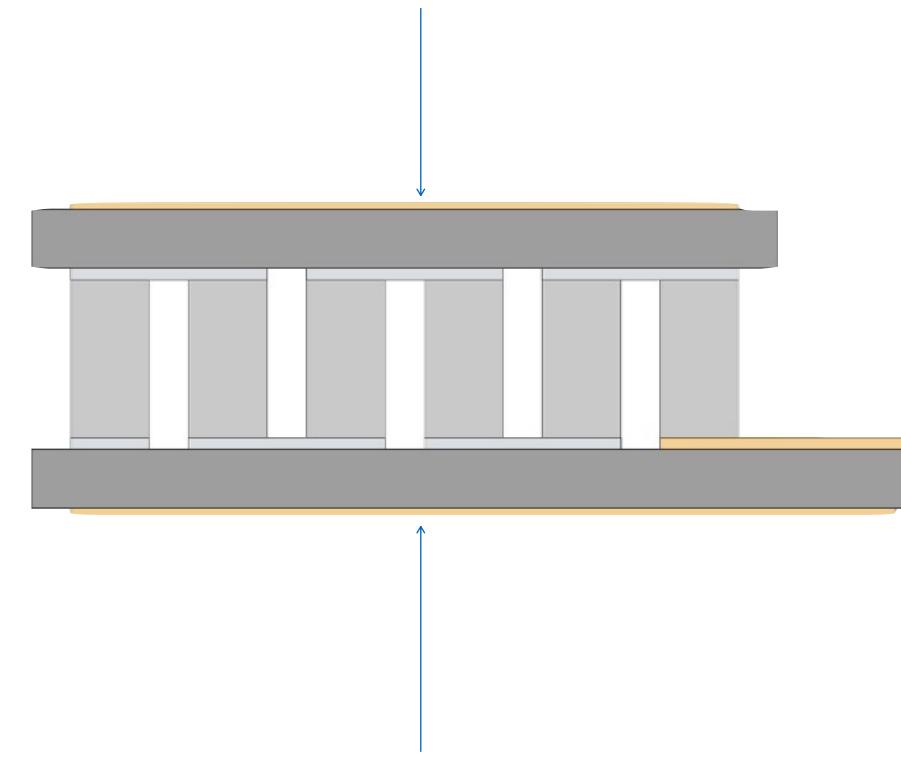
1MD02-012-035/1ANt



$H=0.74 \pm 0.05\text{mm}$

$\pm 0.03\text{mm}$   
(optional)

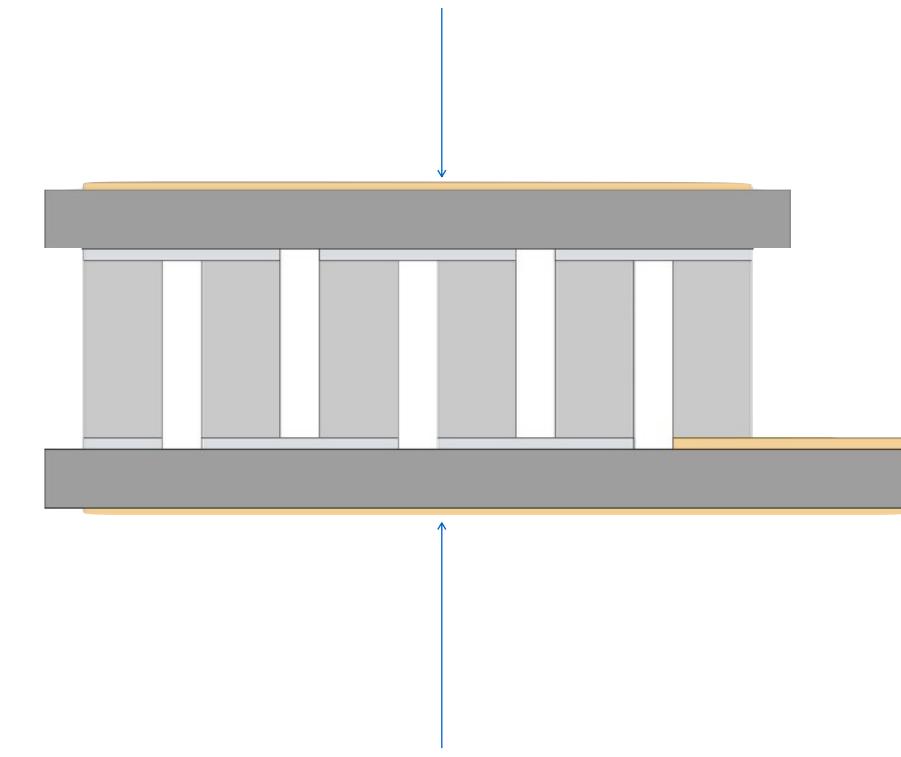
1MD02-012-04/1ANt



$H=0.79 \pm 0.05\text{mm}$

$\pm 0.03\text{mm}$   
(optional)

1MD02-012-045/1ANt



$H=0.85 \pm 0.05\text{mm}$

$\pm 0.03\text{mm}$   
(optional)

TEC Microsystems provides ultra-thin TEC Solutions from “ANt” Series - ultra-thin TECs with precise height control



## TEC Microsystems Thermoelectric Coolers Assembly Solders

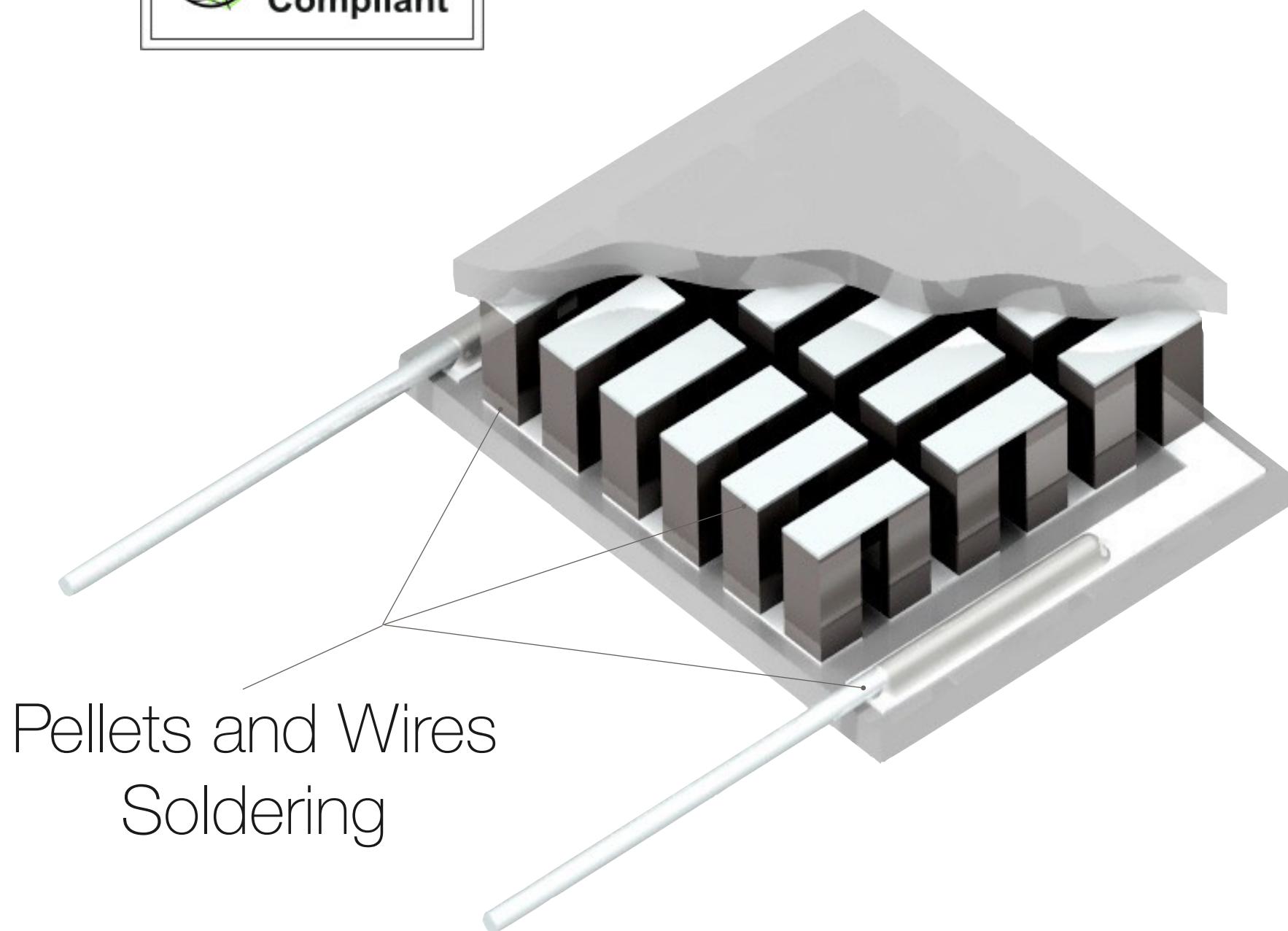
### TEC Microsystems Standard TEC Internal Assembly Solder

Antimony-Tin	Sn-Sb (95%-5%)	230°C
--------------	----------------	-------



### Optional TEC Internal Assembly Solders

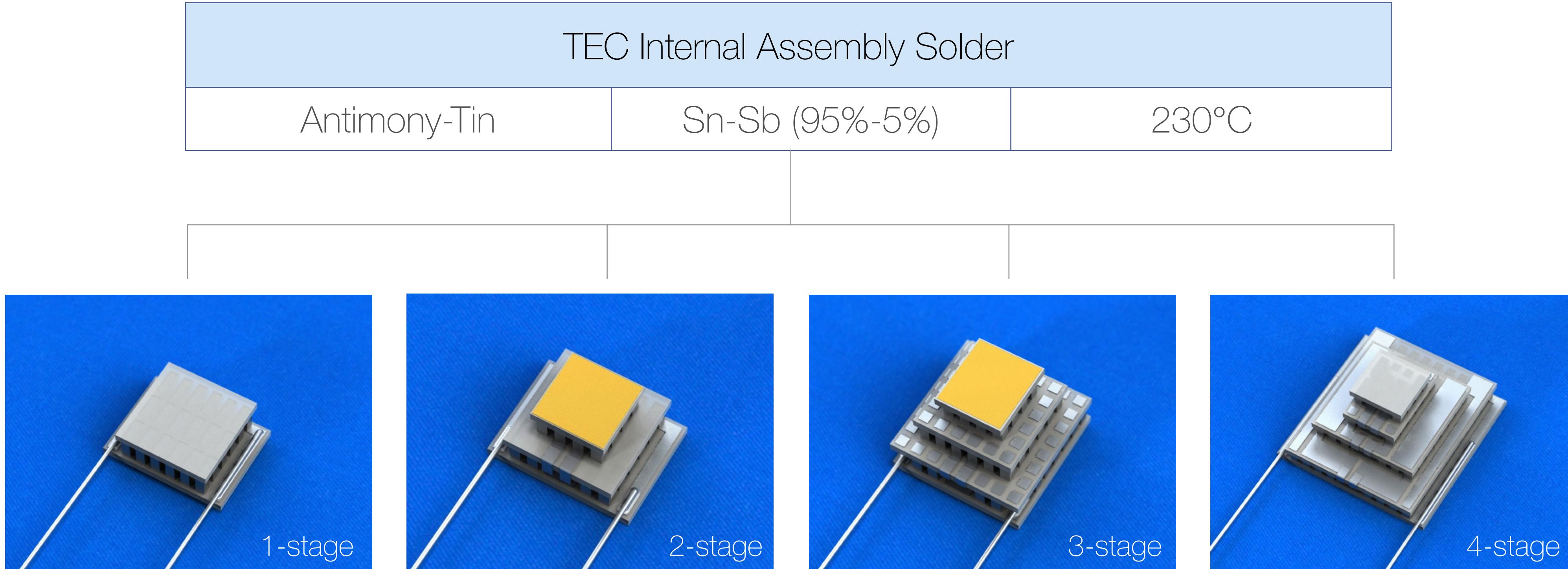
Gold-Tin	Au-Sn (80%-20%)	280°C
Lead-Tin	Pb-Sn (37%-63%)	183°C
Bismuth-Tin	Bi-Sn (57%-43%)	138°C



TEC Microsystems uses Solder 230 by default for TEC Assembly. Other solutions are available by request.



TEC Microsystems TECs are assembled with RoHS compliant Solder 230 by default

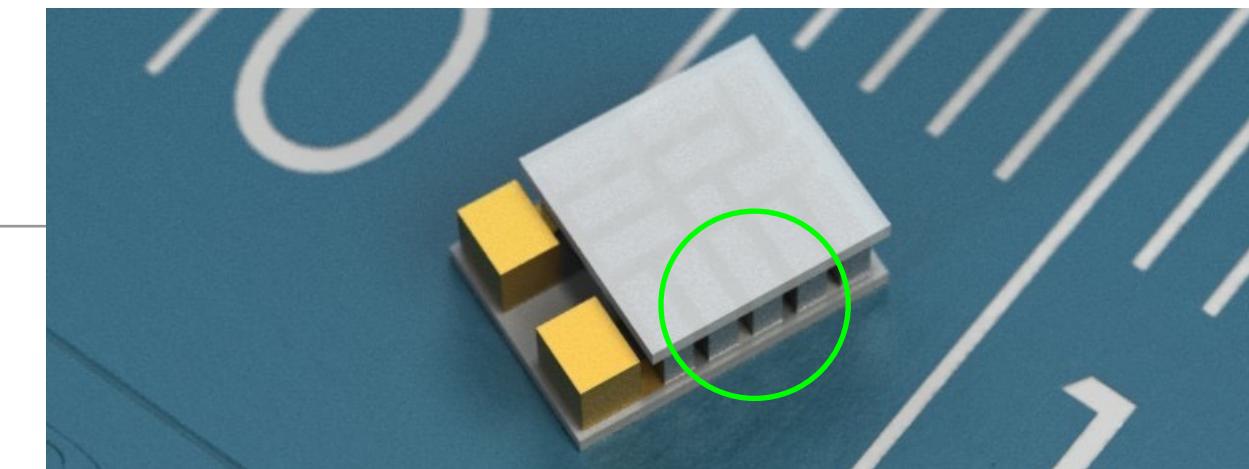


Solder 230 requires very high technology level in volume manufacturing, especially for multistage TE Coolers. Other vendors multistage TECs are assembled commonly with Solder 183 or Solder 138



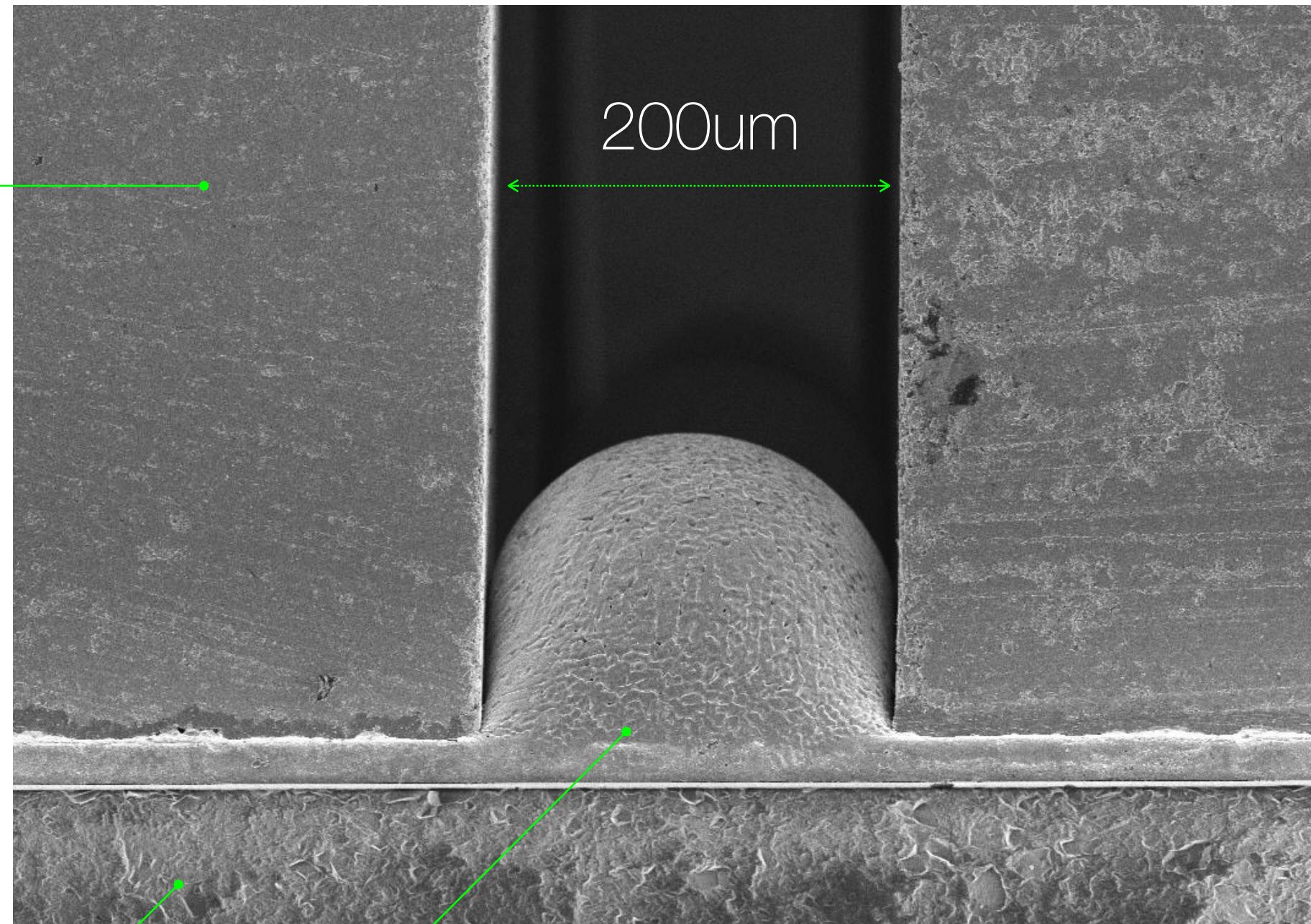
# High-Quality Soldering Assembly for Thermoelectric Modules

TEC from  
TEC Microsystems

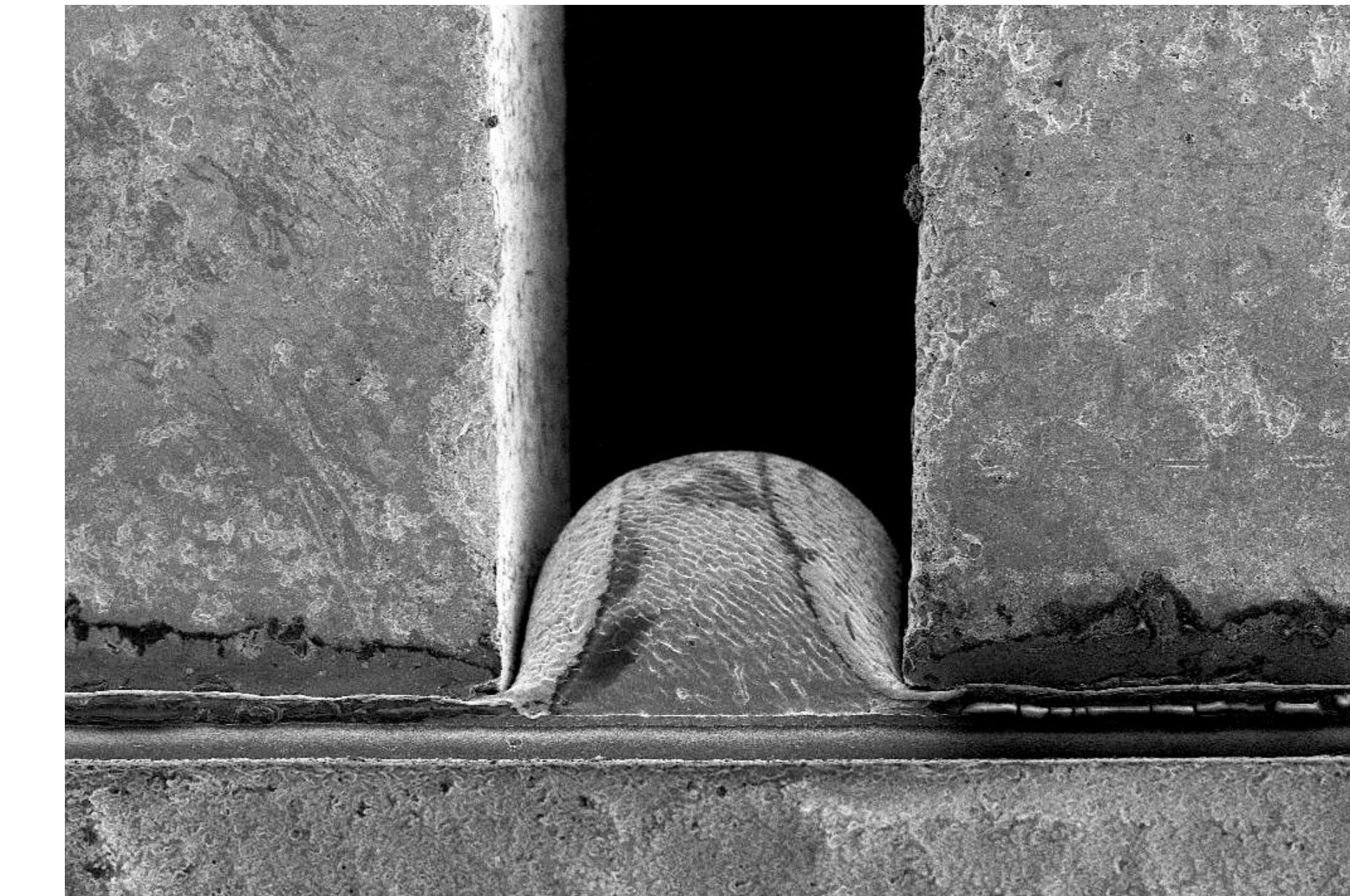


TEC from another vendor

BiTe Pellet



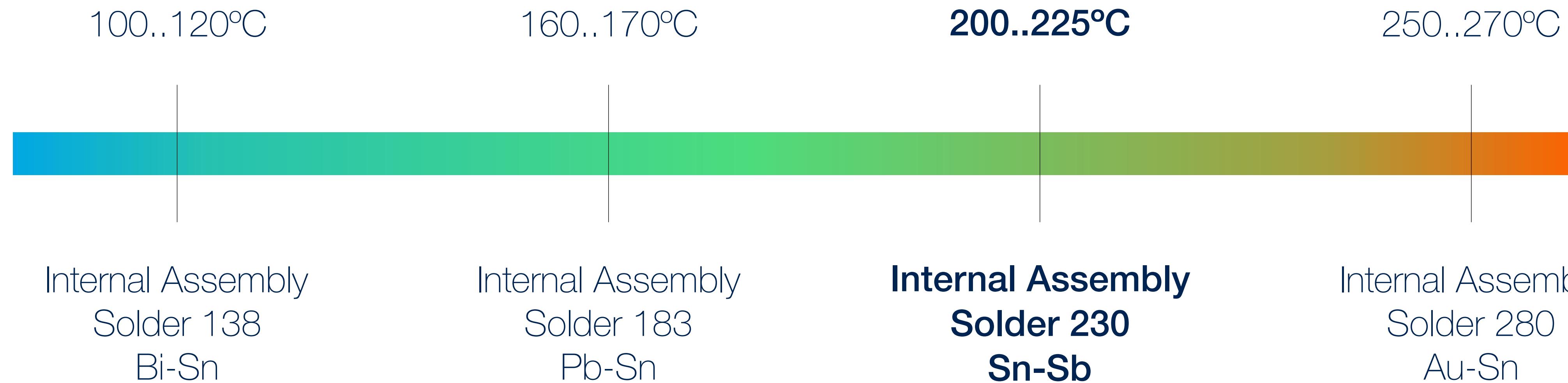
Ceramics      Solder      GOOD



NOT GOOD



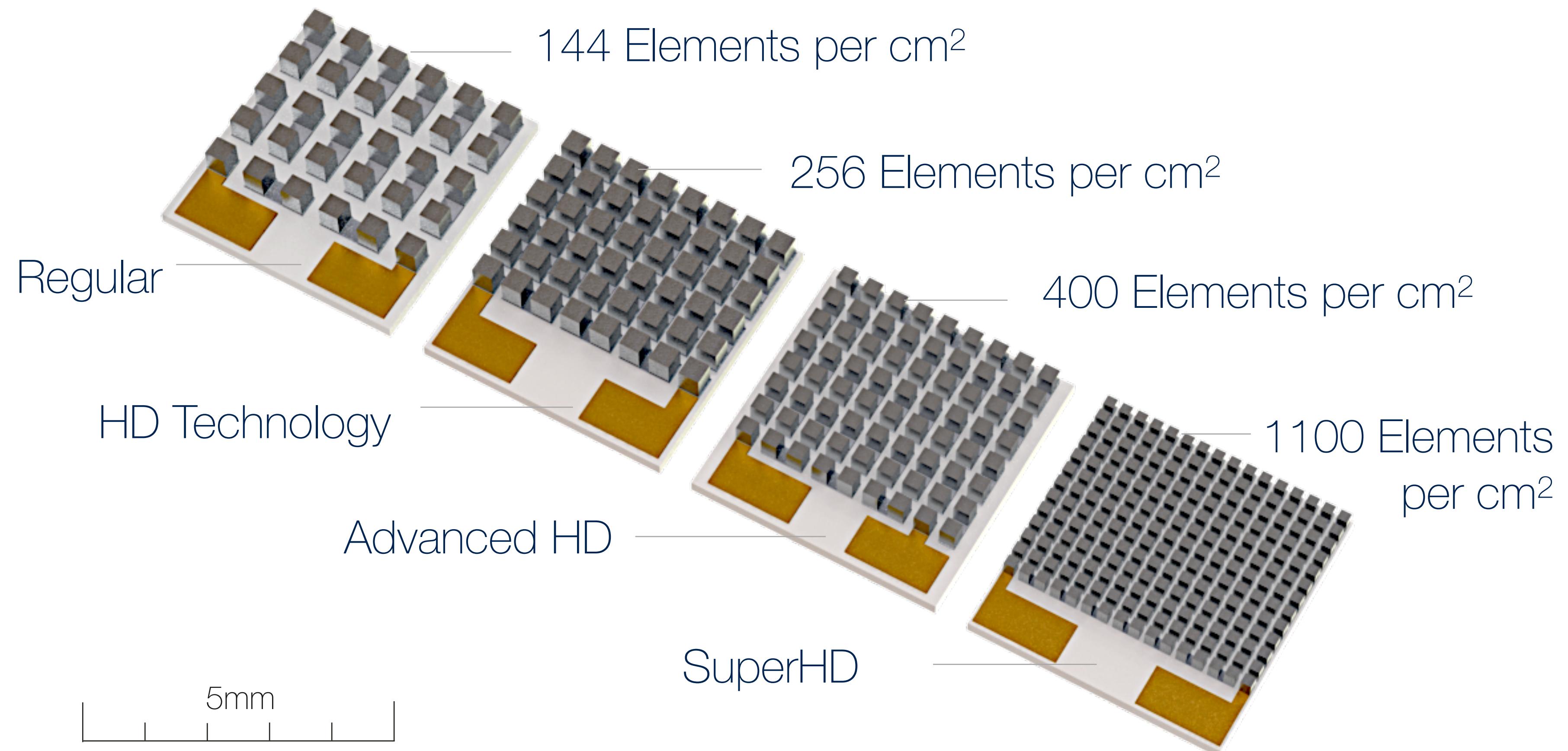
## Max TEC Processing Temperature (short time) during mounting



TEC Internal Assembly Solder is usually specified in datasheet or batch specification. It can be also identified by max recommended mounting processing temperature (short time)



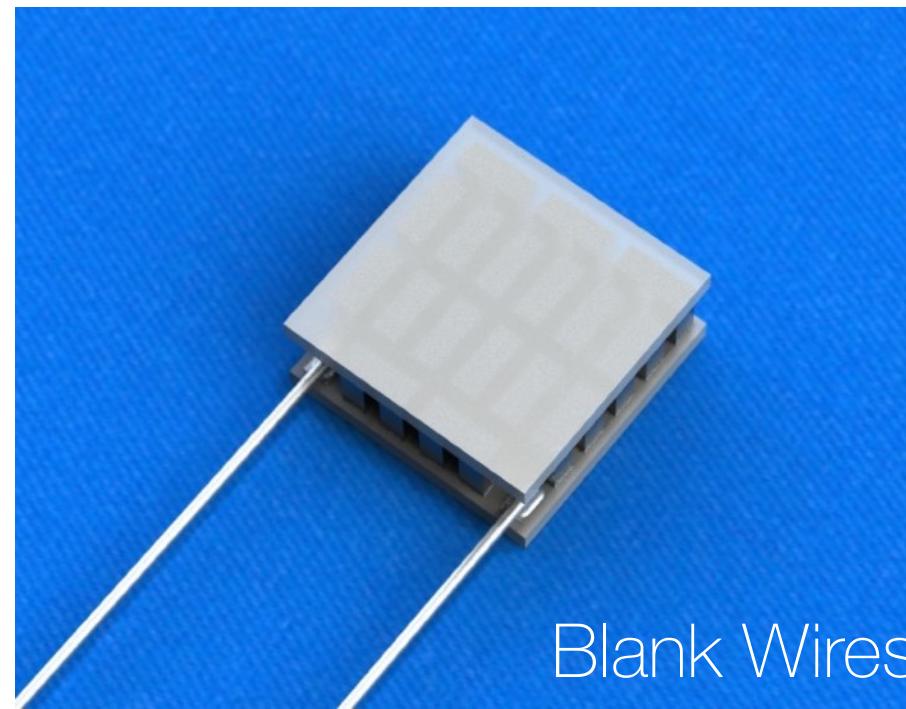
## TEC Microsystems Bulk TEC Assembly - Pellets Placement Technologies



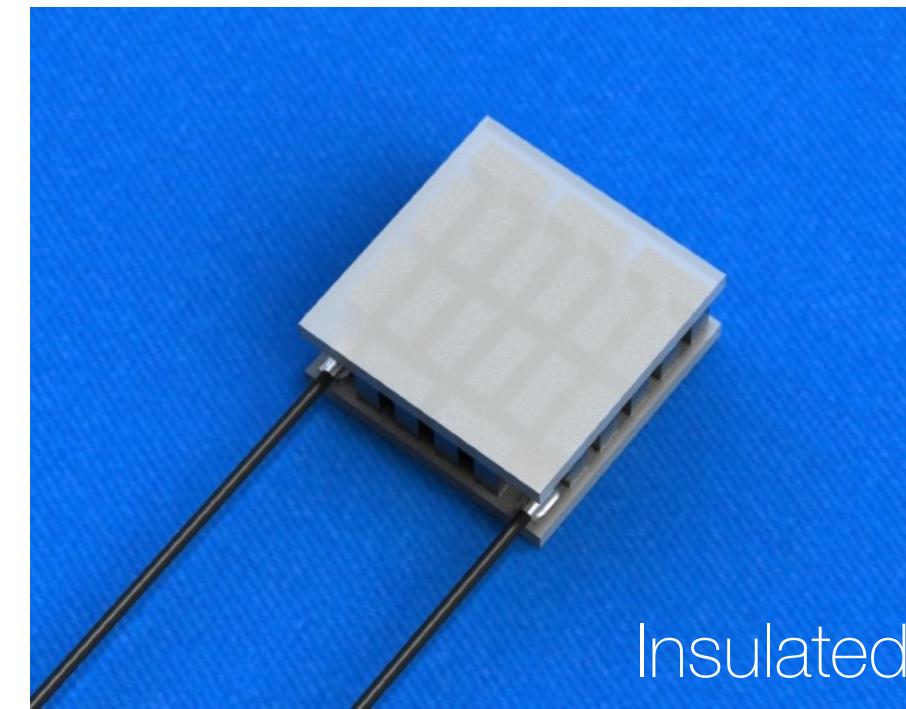
Unique HD technologies allow creating high-performance TECs with low power consumption.



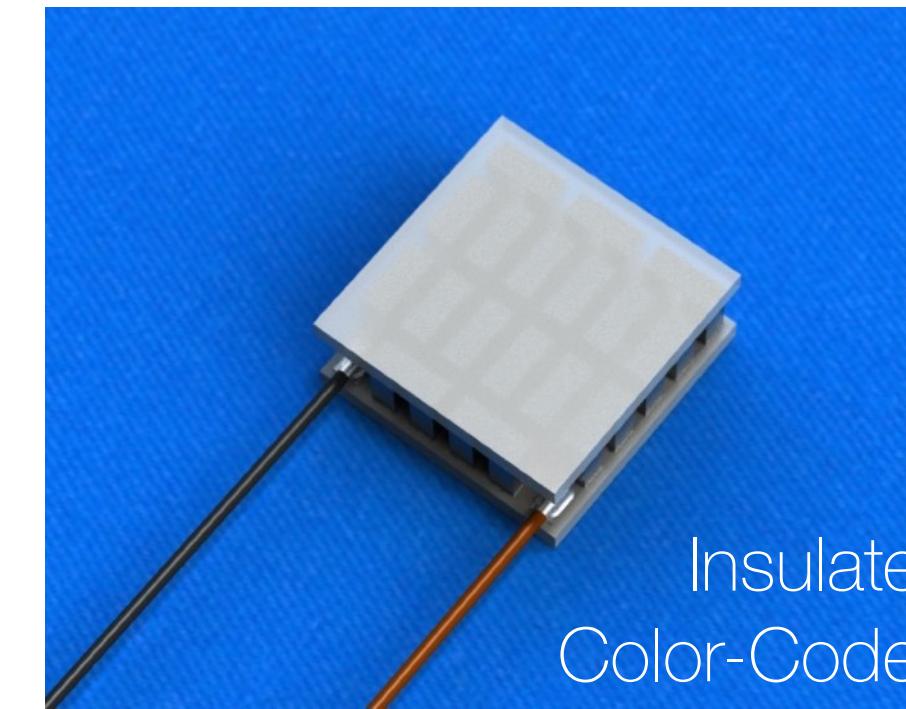
## Terminal Connection Solutions for TE Coolers



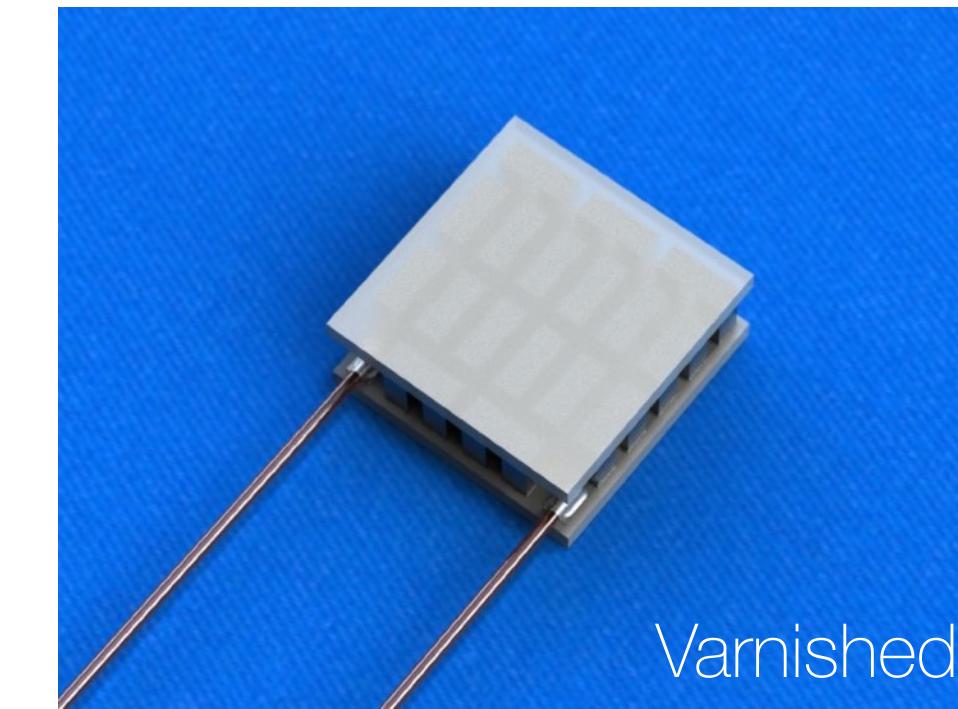
Blank Wires



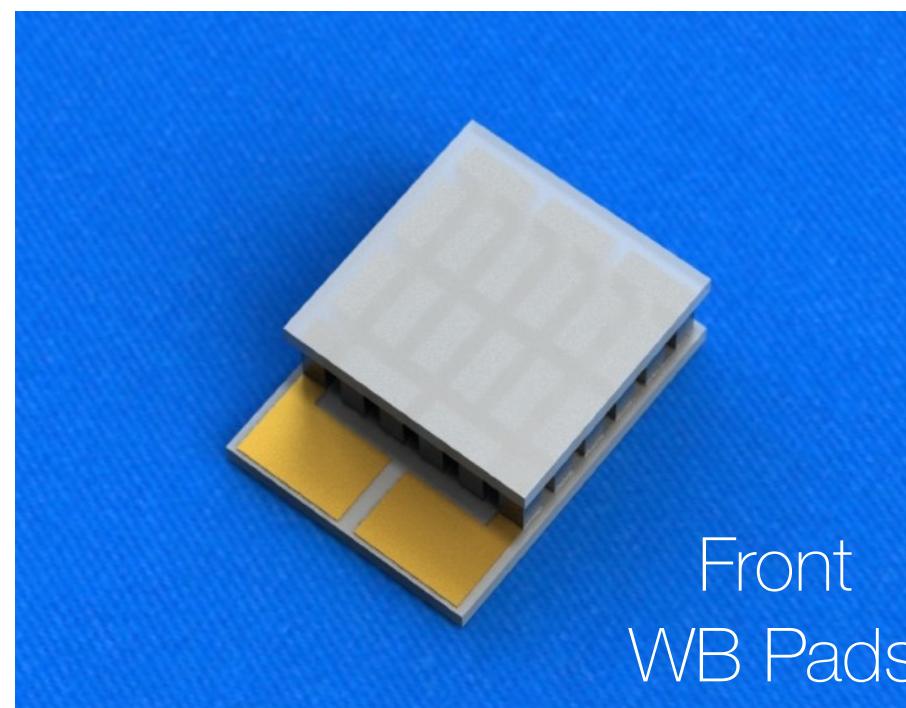
Insulated



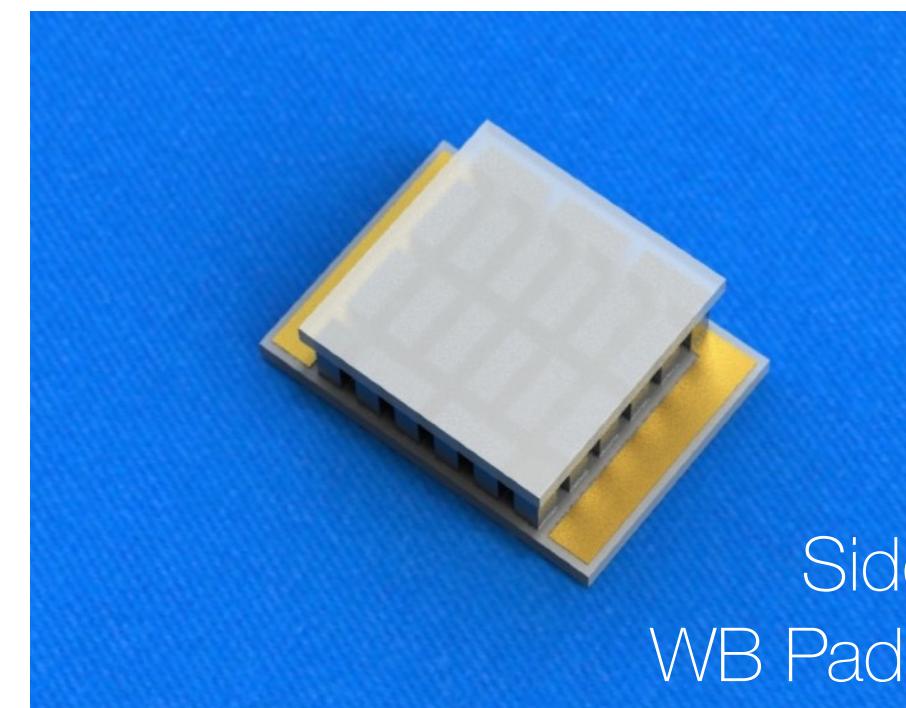
Insulated  
Color-Coded



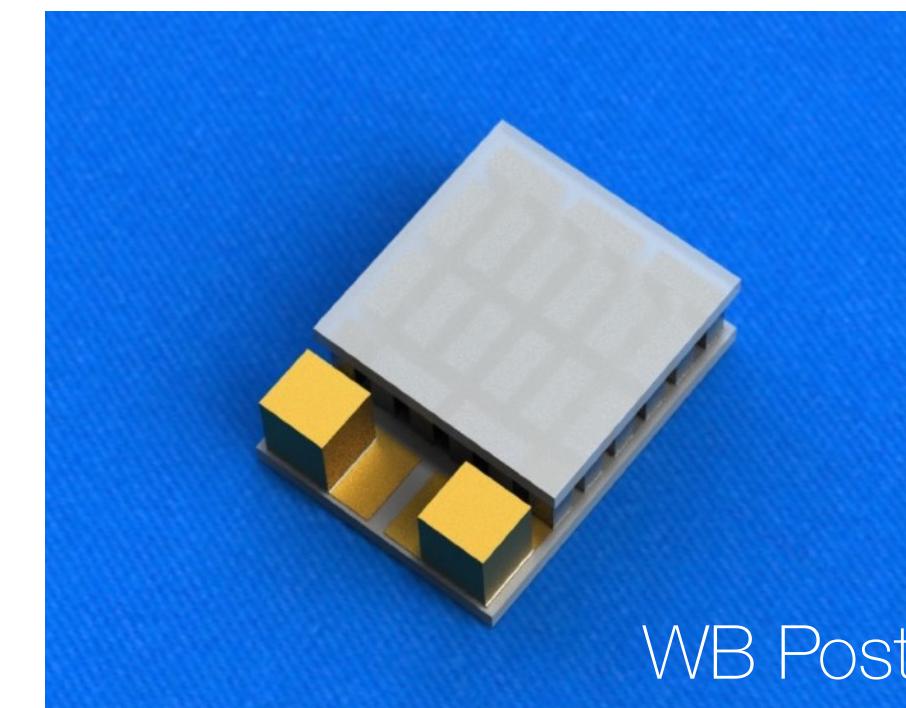
Varnished



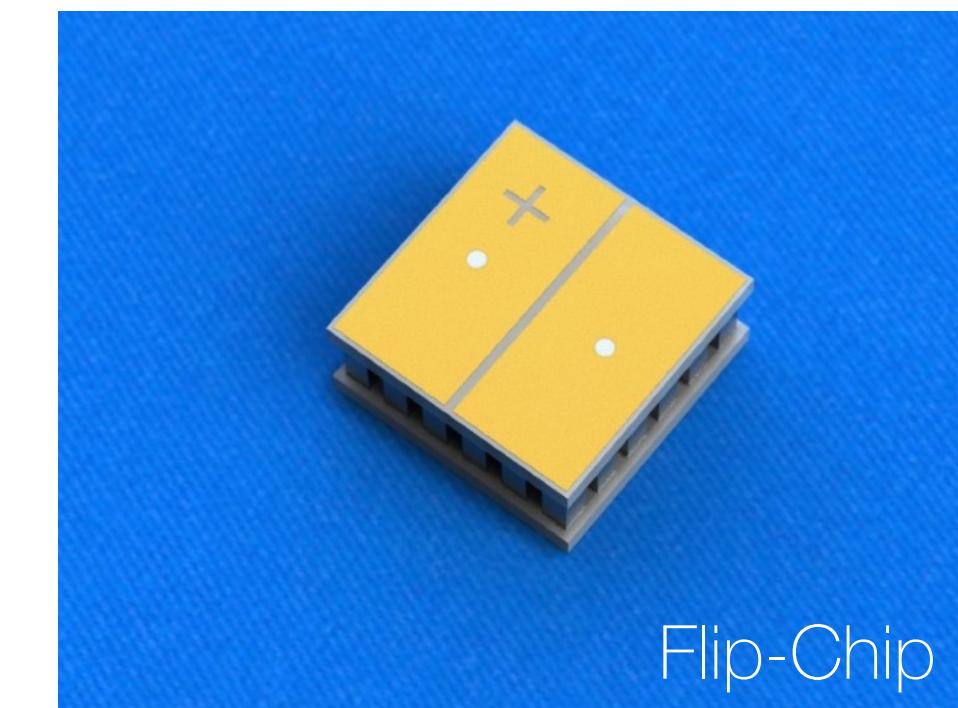
Front  
WB Pads



Side  
WB Pads



WB Posts



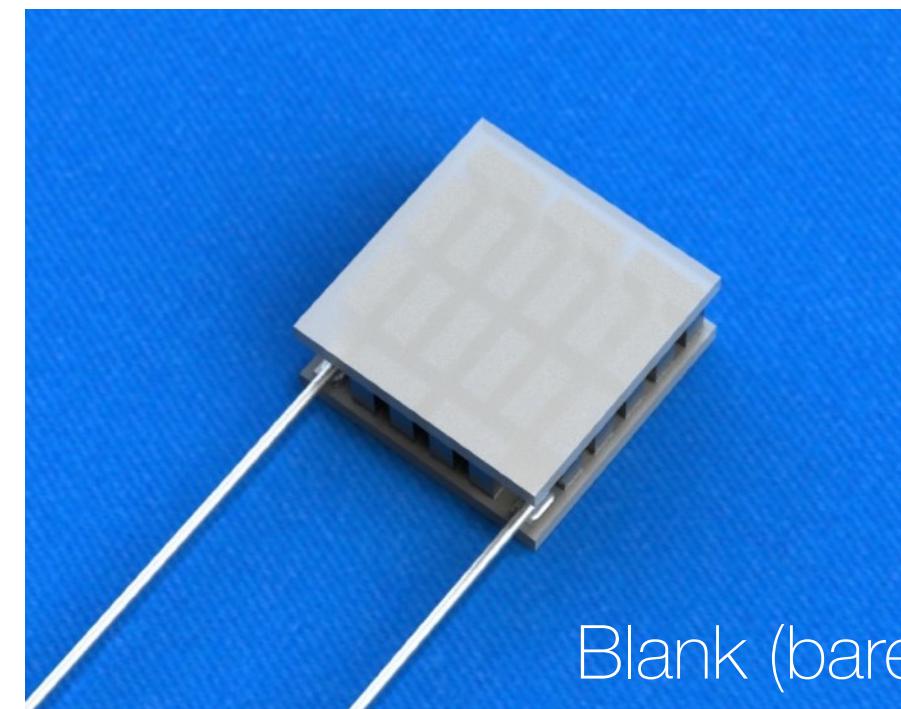
Flip-Chip

TEC can be manufactured with Wired terminal connection or optimized for Wire Bonding (WB) process. TEC Microsystems has a full flexibility with terminal connection solution for TECs. TEC Flip-Chip optimization is available.

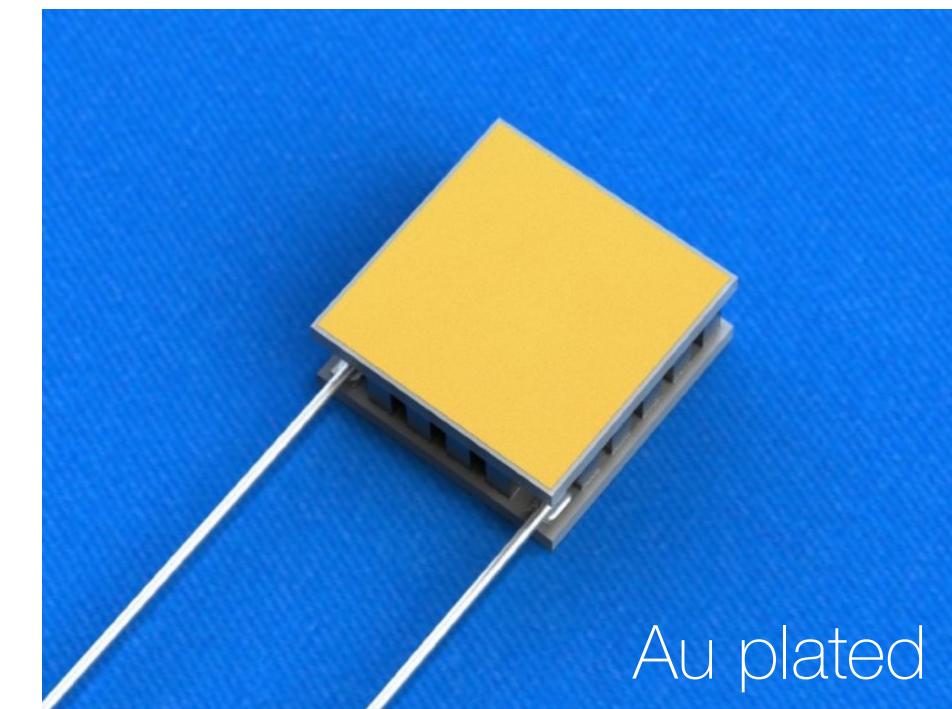


## TE Cooler Ceramics Surface Solutions

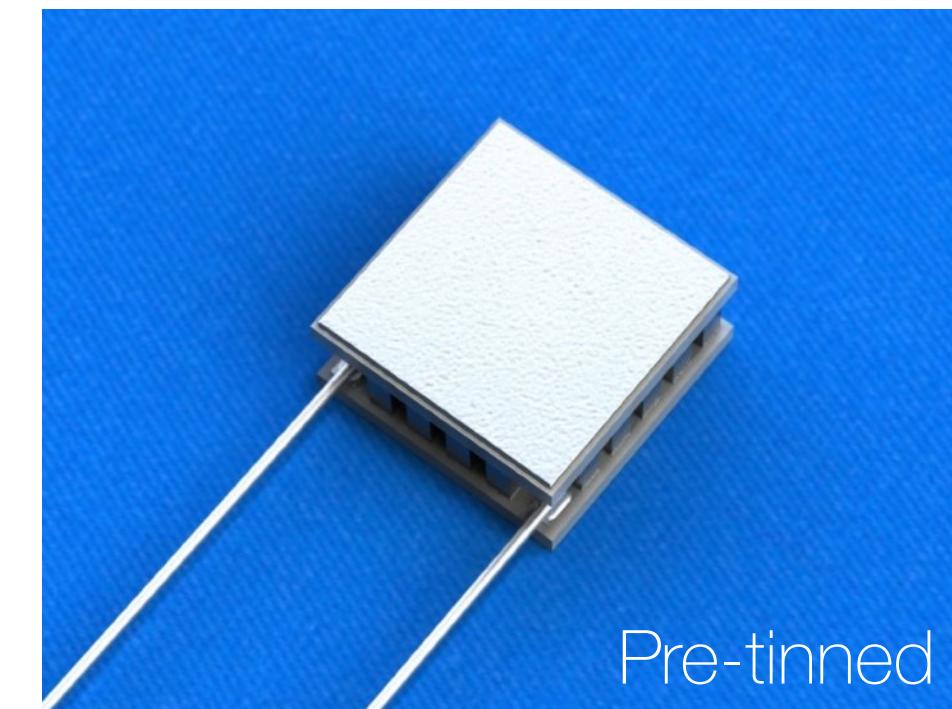
### Standard Surface Solutions



Blank (bare)

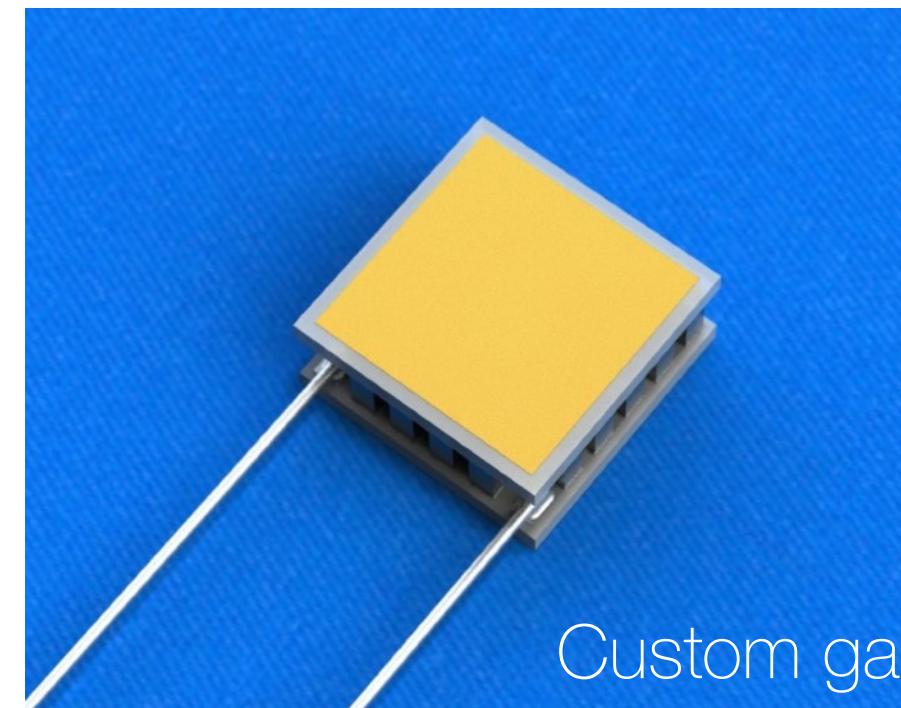


Au plated

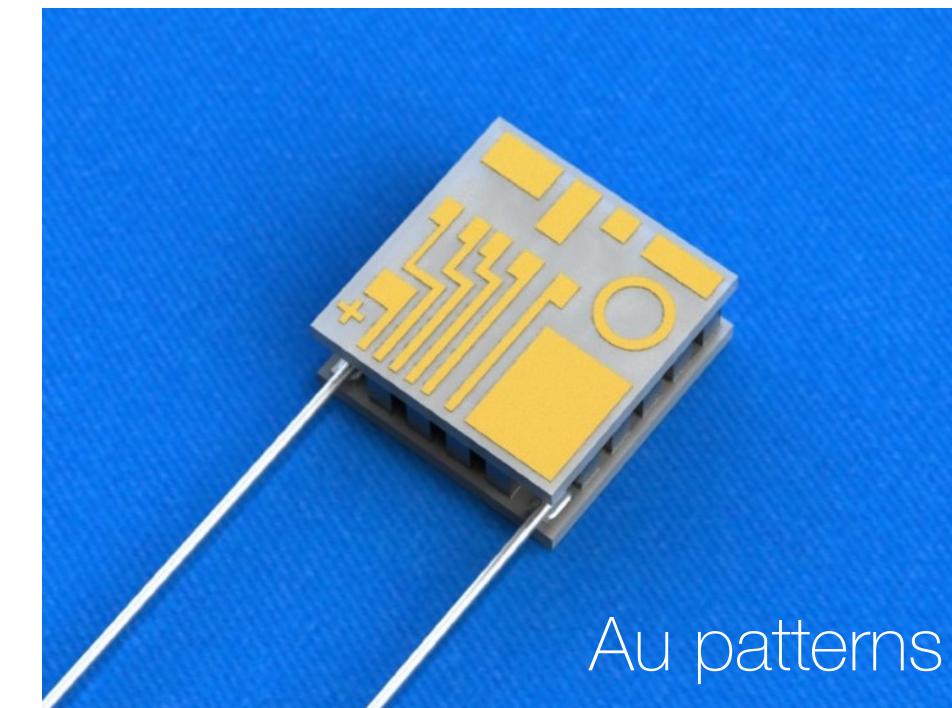


Pre-tinned

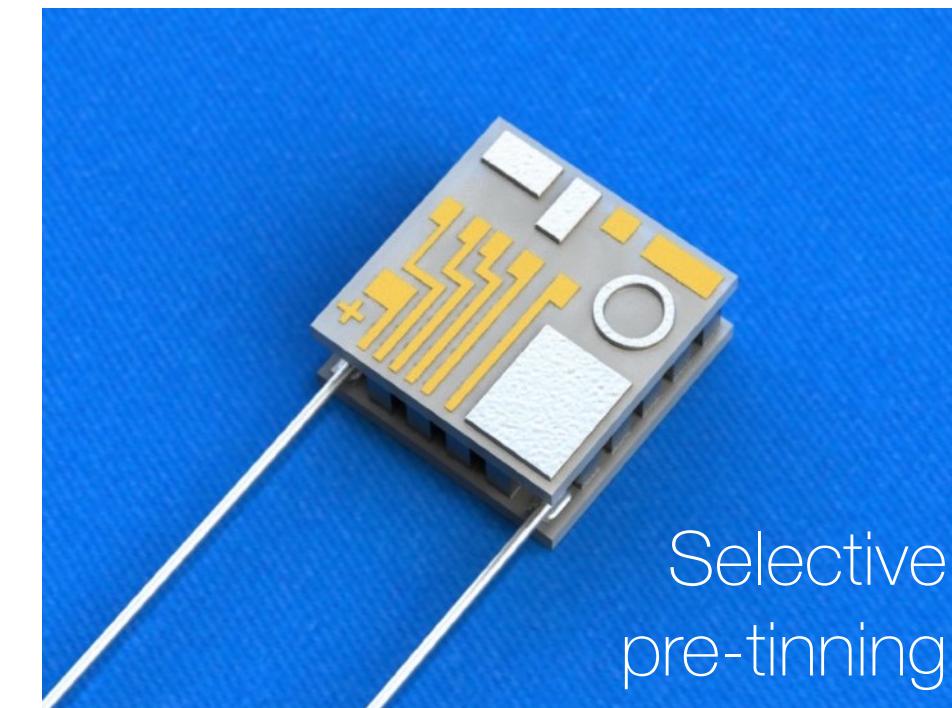
### Advanced Surface Solutions



Custom gap



Au patterns

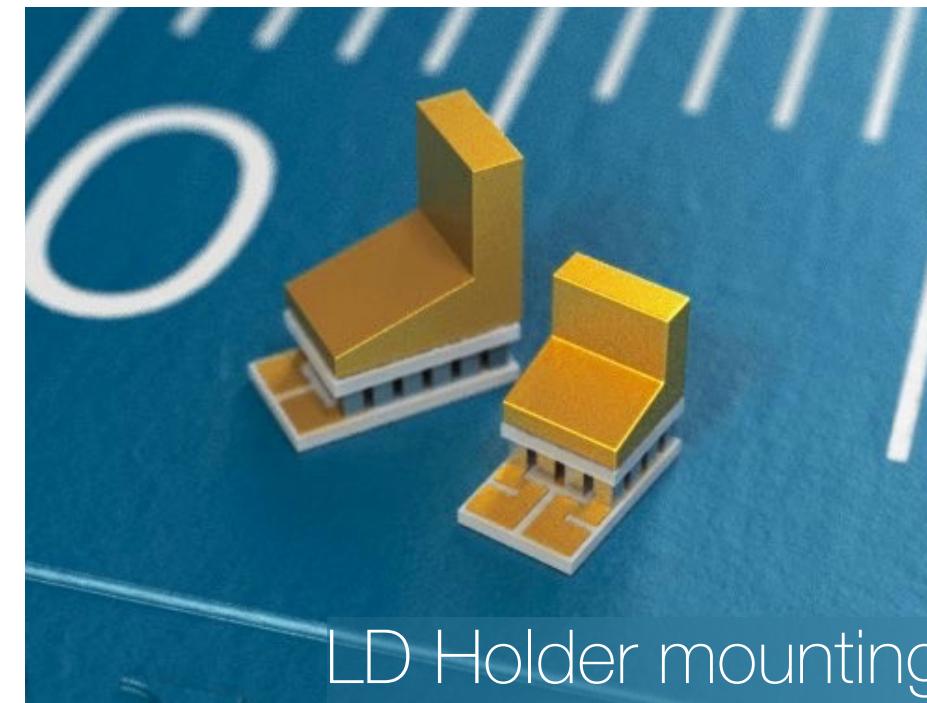


Selective pre-tinning

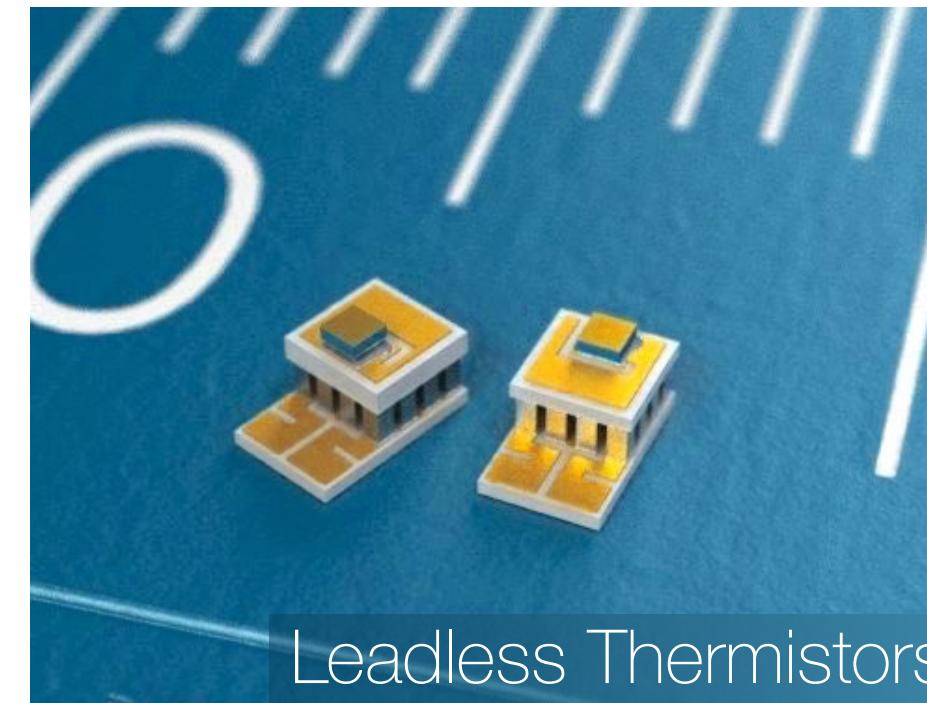
Ceramics surface solution can be the same for both TEC sides, or can be specified for each side separately.



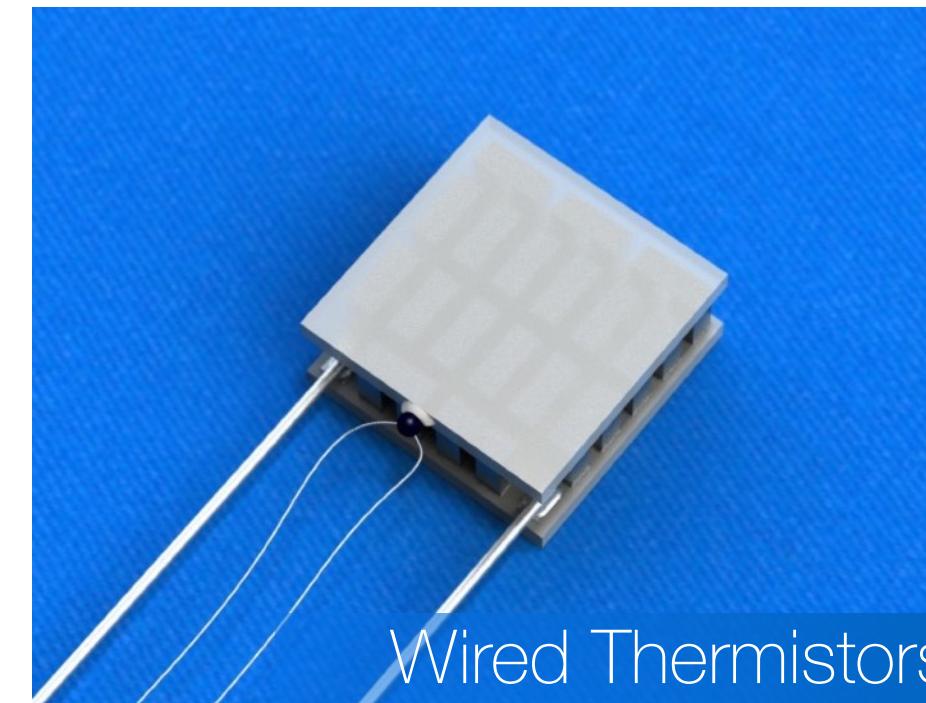
## Additional Value-added Services for TEC Microsystems TE Coolers



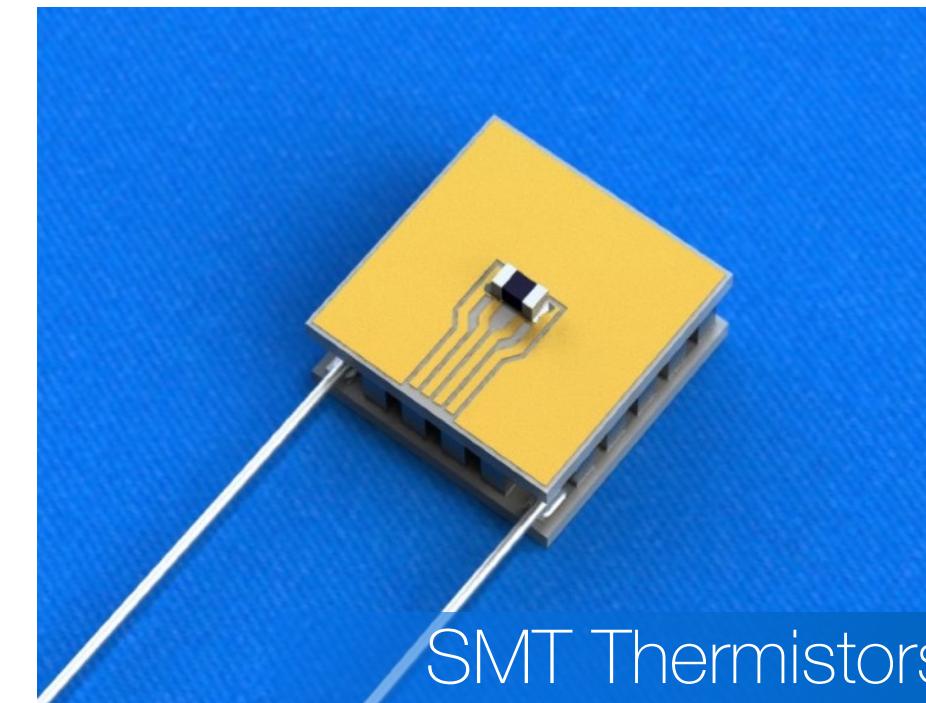
LD Holder mounting



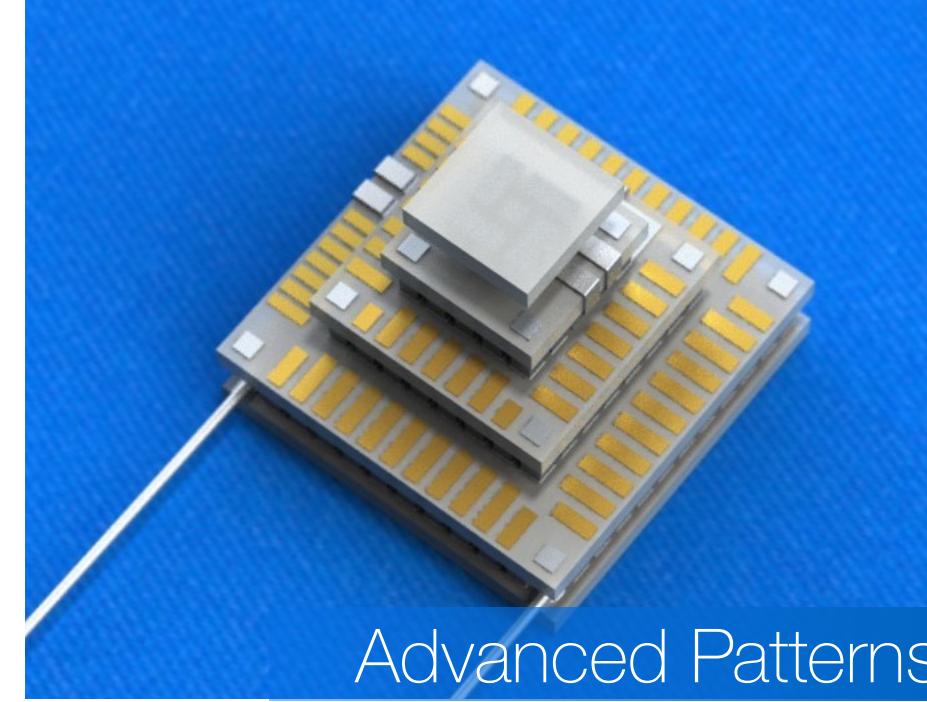
Leadless Thermistors



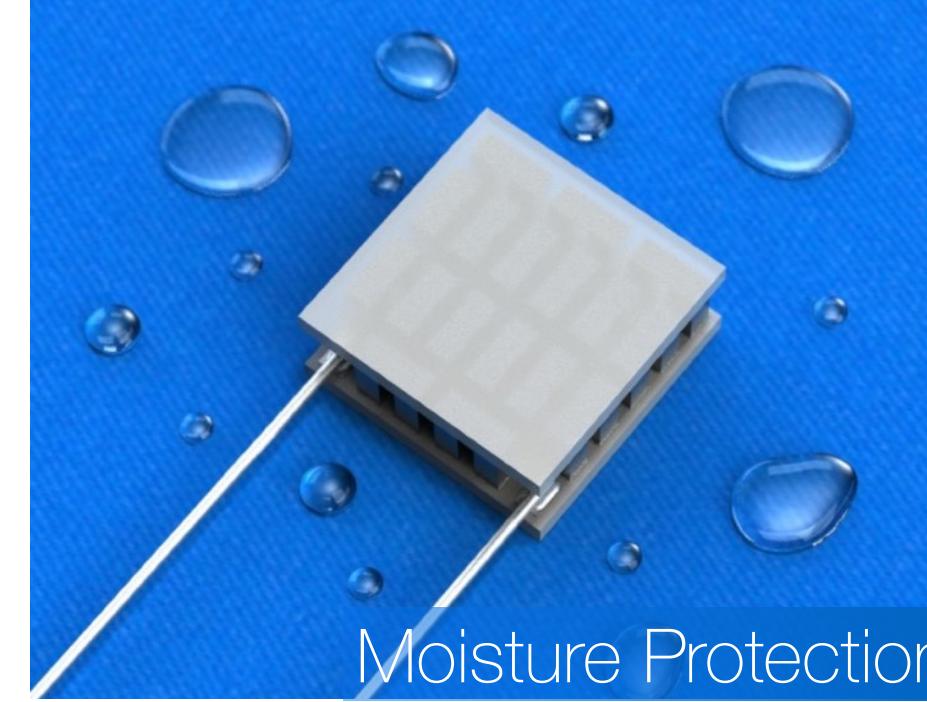
Wired Thermistors



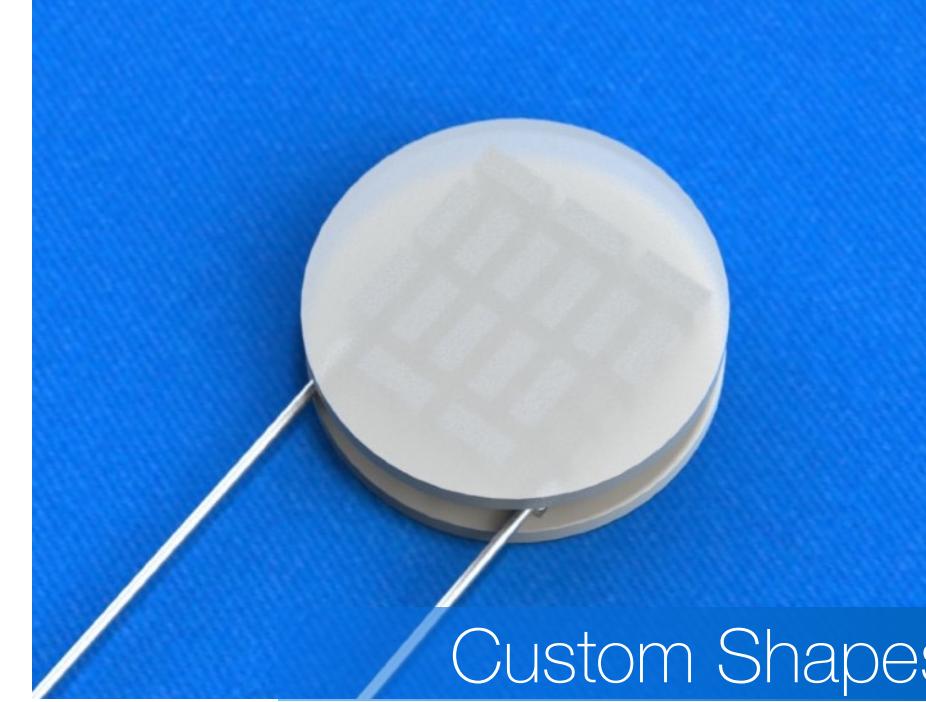
SMT Thermistors



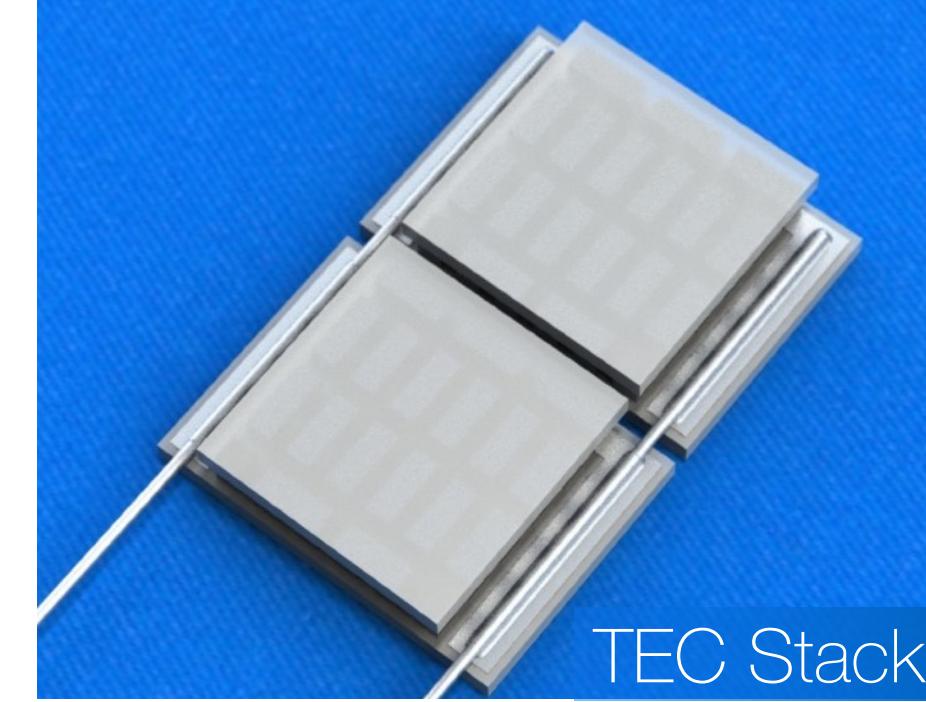
Advanced Patterns



Moisture Protection



Custom Shapes



TEC Stacks

TEC Microsystems provides a wide range of additional modification and mounting services for TE Coolers. It saves costs and simplifies TEC integrating into Customer application.



## TEC Microsystems TE Coolers Mounting Service - Flux-Free Soldering in Vacuum



TO-46



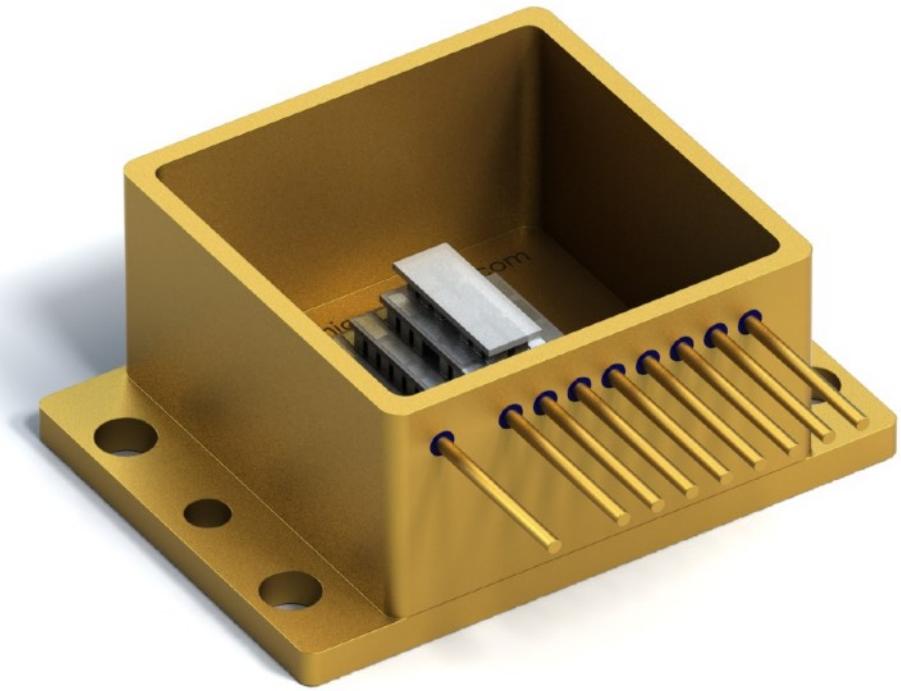
TO-39



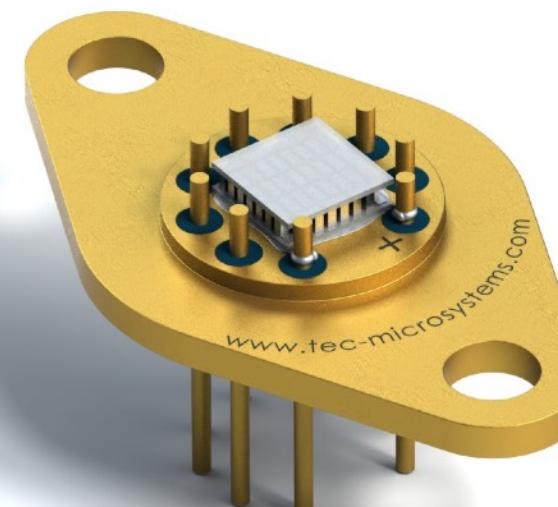
TO-8



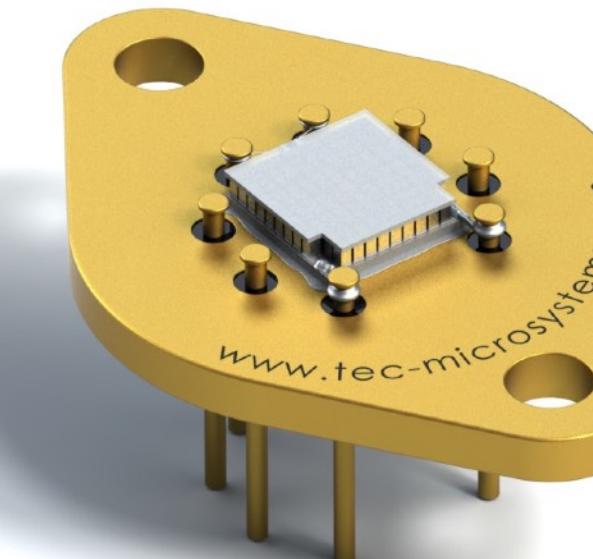
TO-822



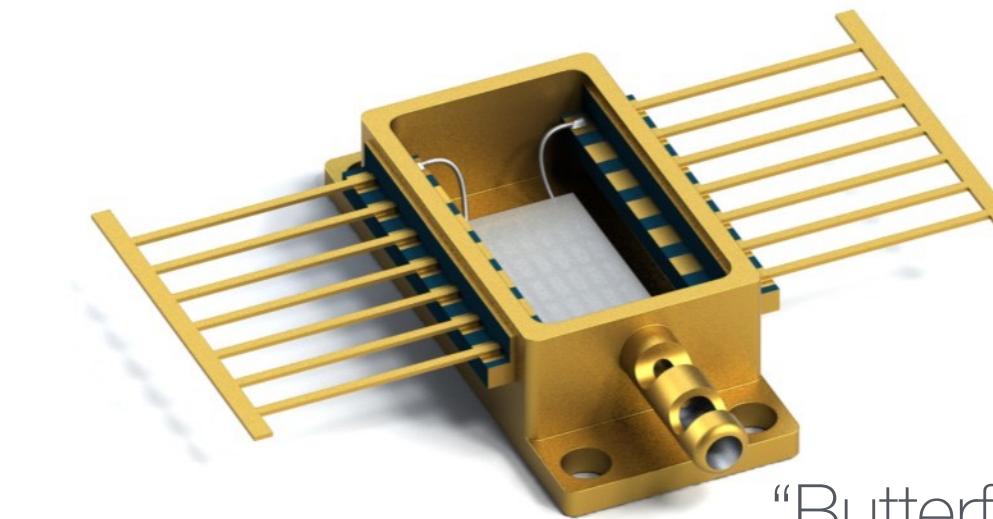
HHL



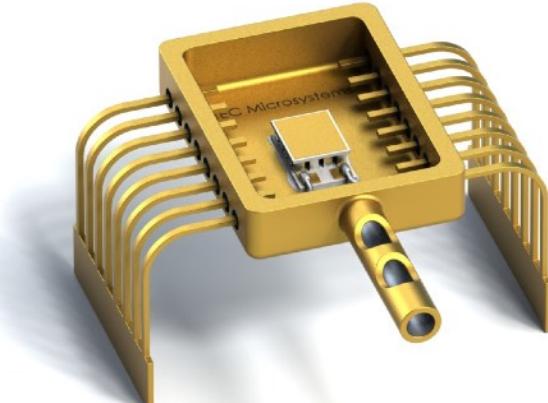
TO-66



TO-3



"Butterfly"

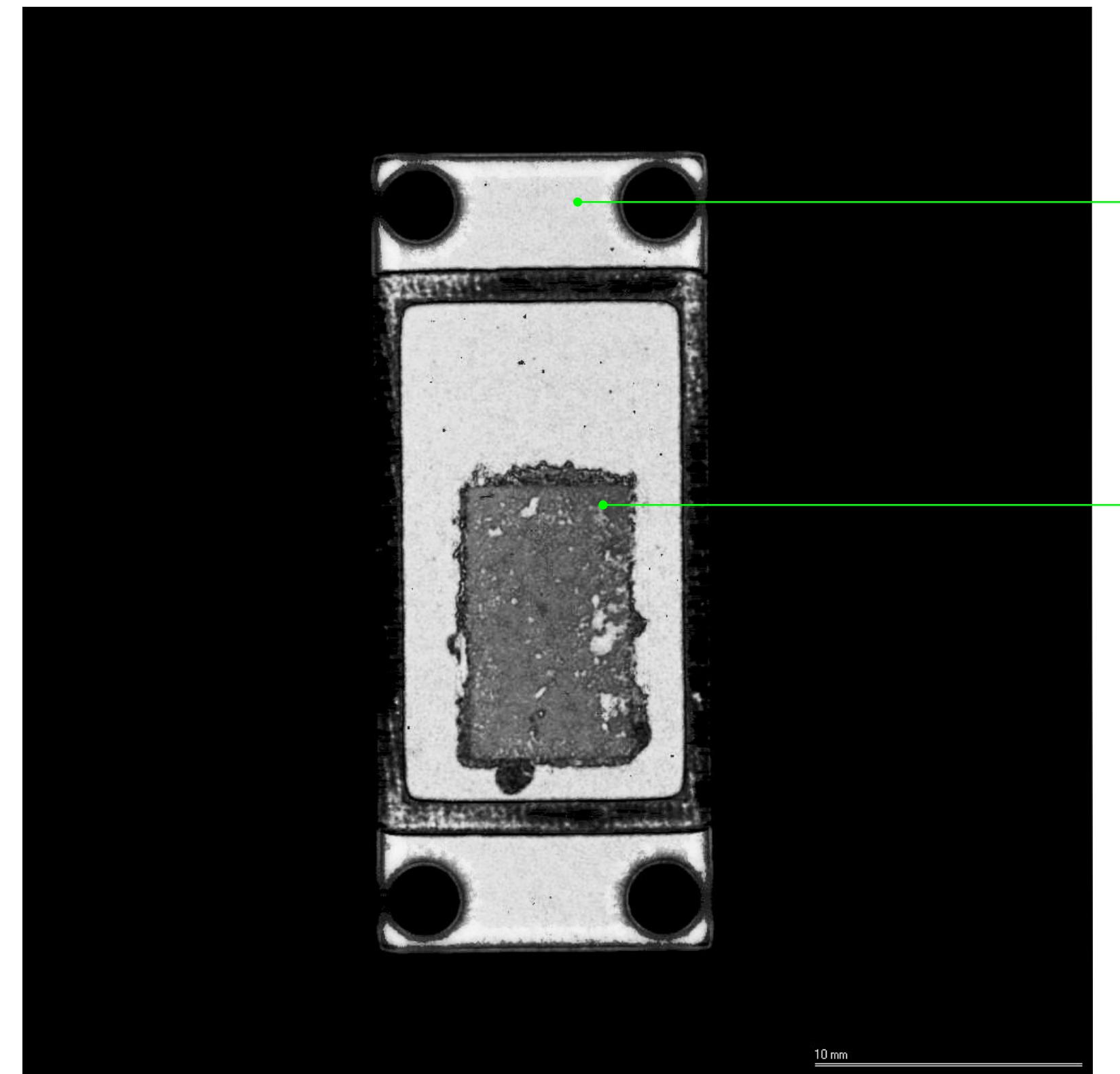


Customized

TEC Microsystems provides TEC mounting and Integrating Services. TECs can be mounted onto Standard or Customer provided headers/packages using flux-free RoHS compliant soldering process with 100% Quality Control



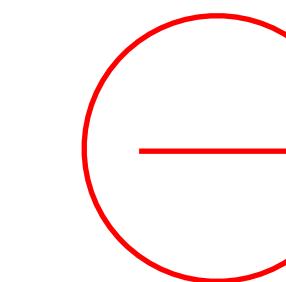
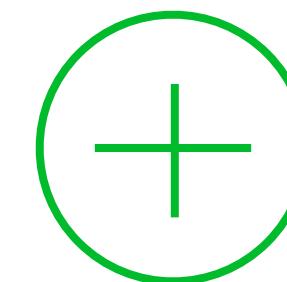
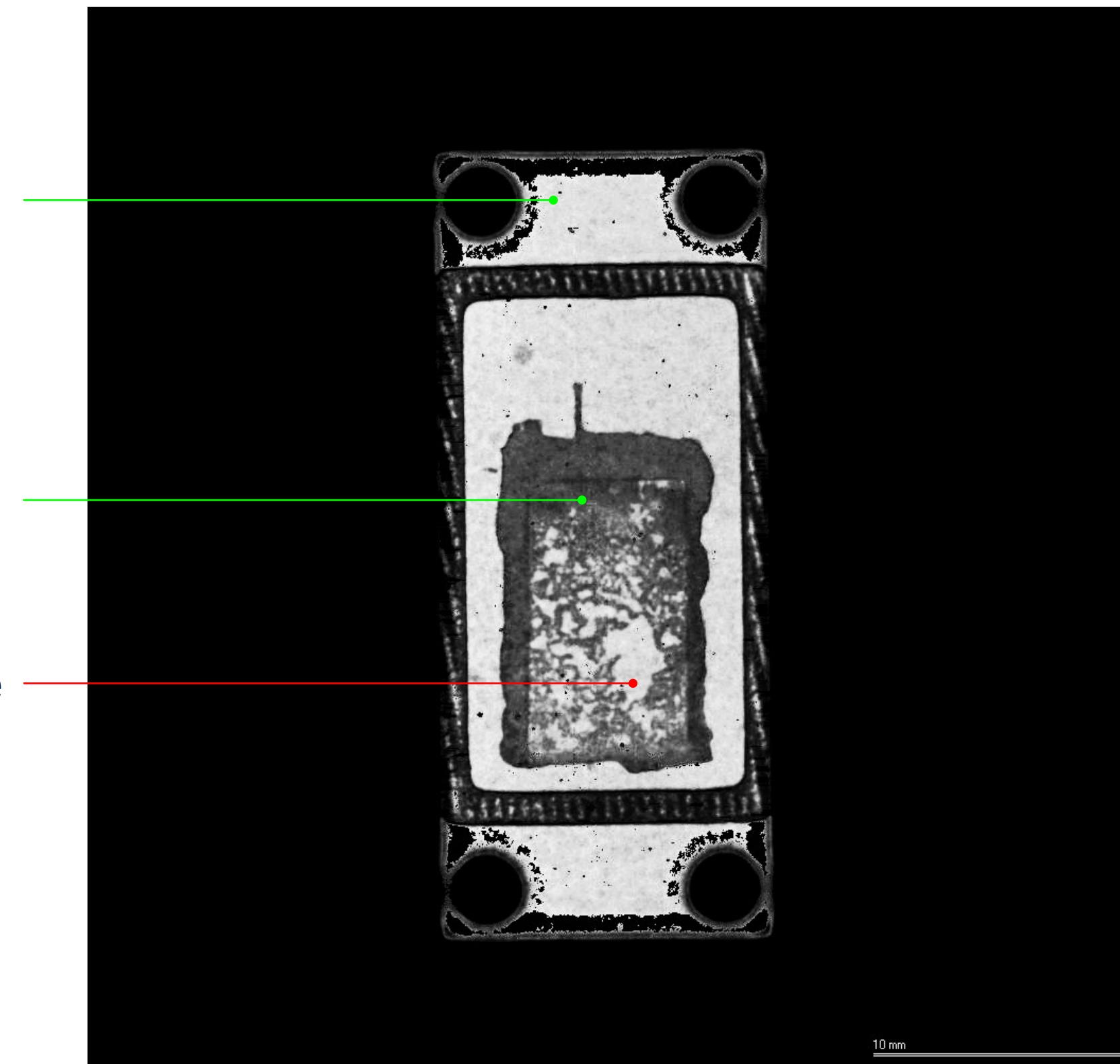
## Acoustic Microscope Analysis Example - Internal voids and caverns in solder layer



BTF Package

Grey area is  
the solder  
under TEC

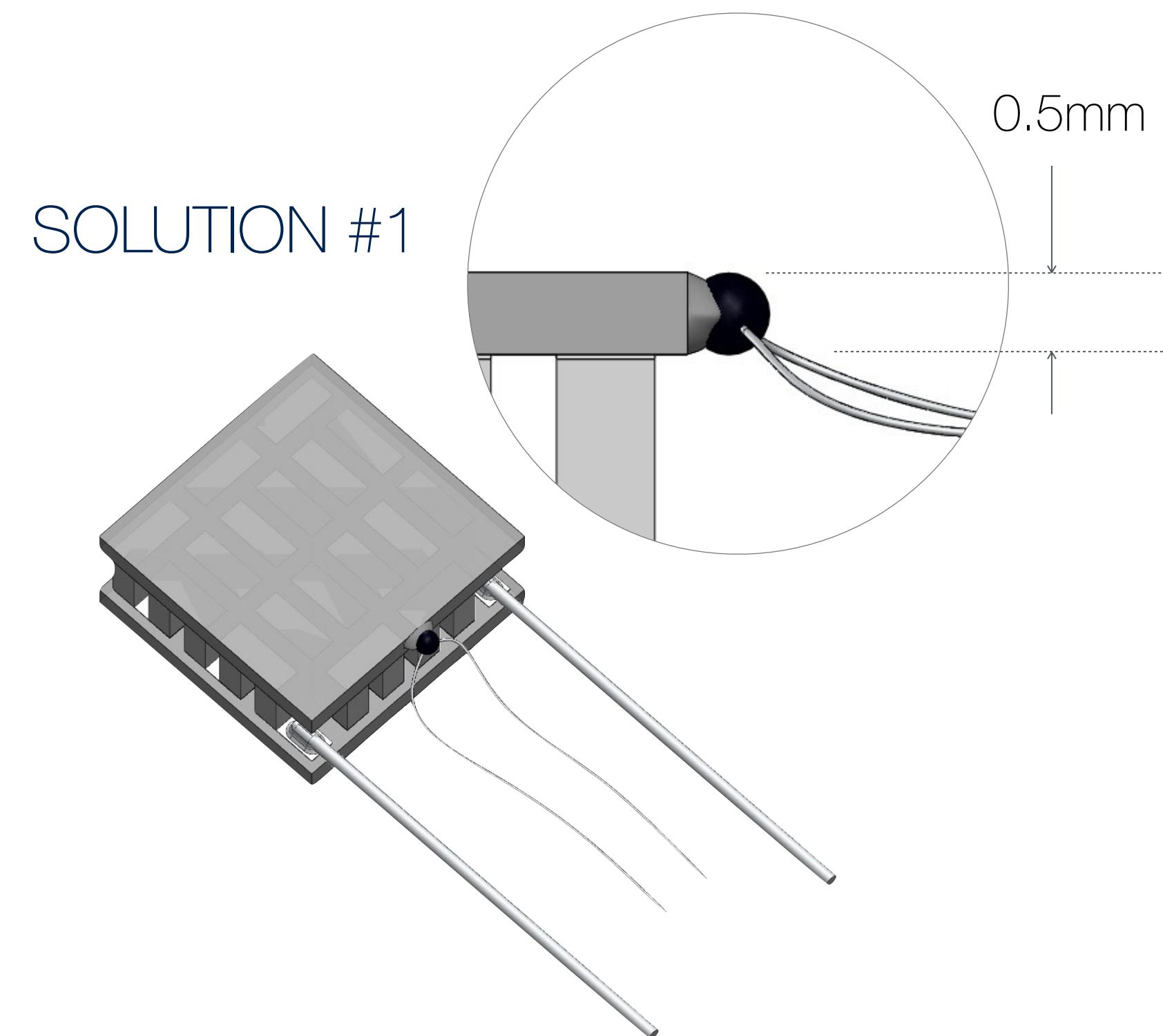
White areas are  
voids in solder



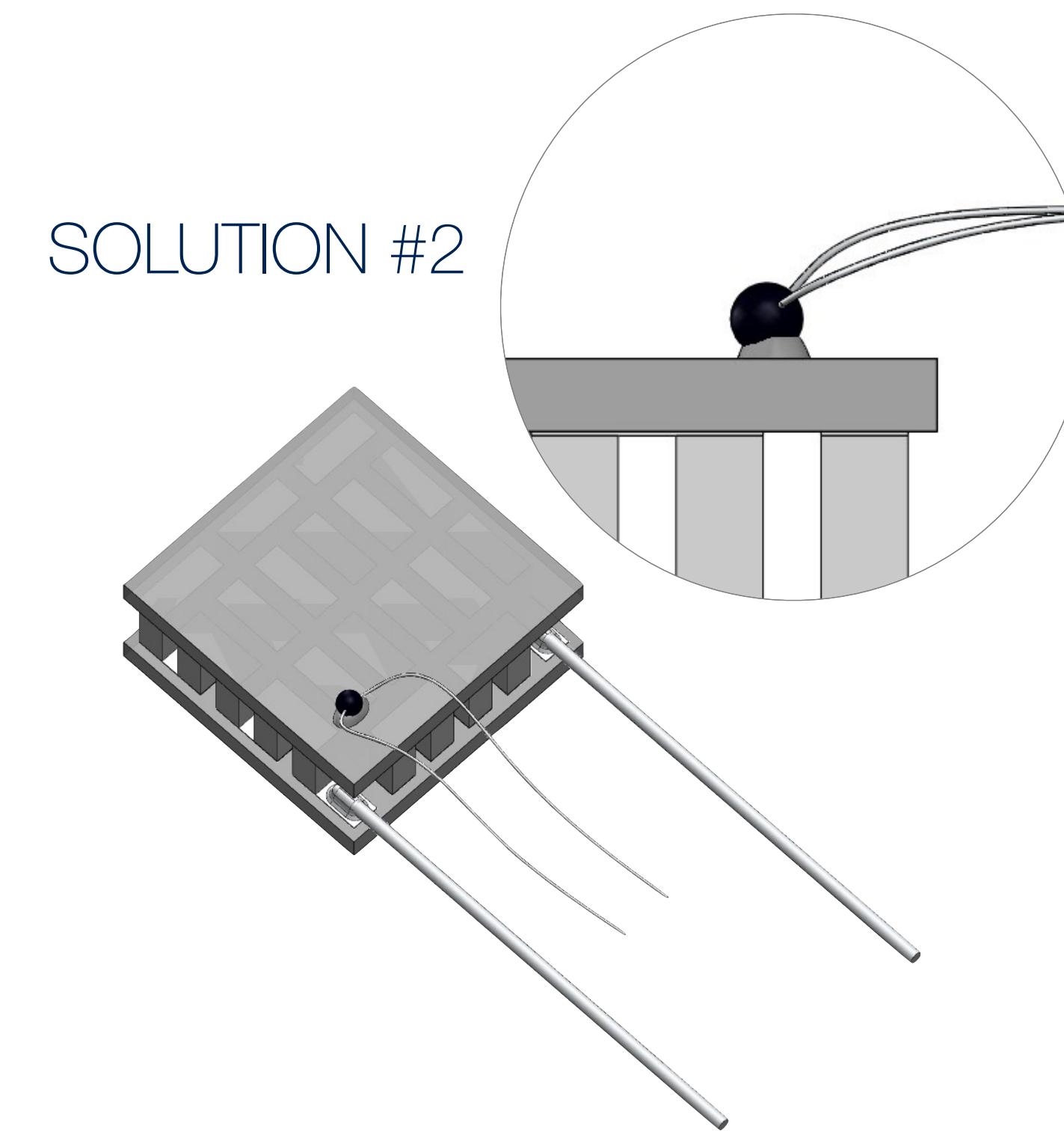
Acoustic Microscopy analysis of soldering joint connection between TEC and BTF package



## Thermistors - Glass-beaded NTC Solutions

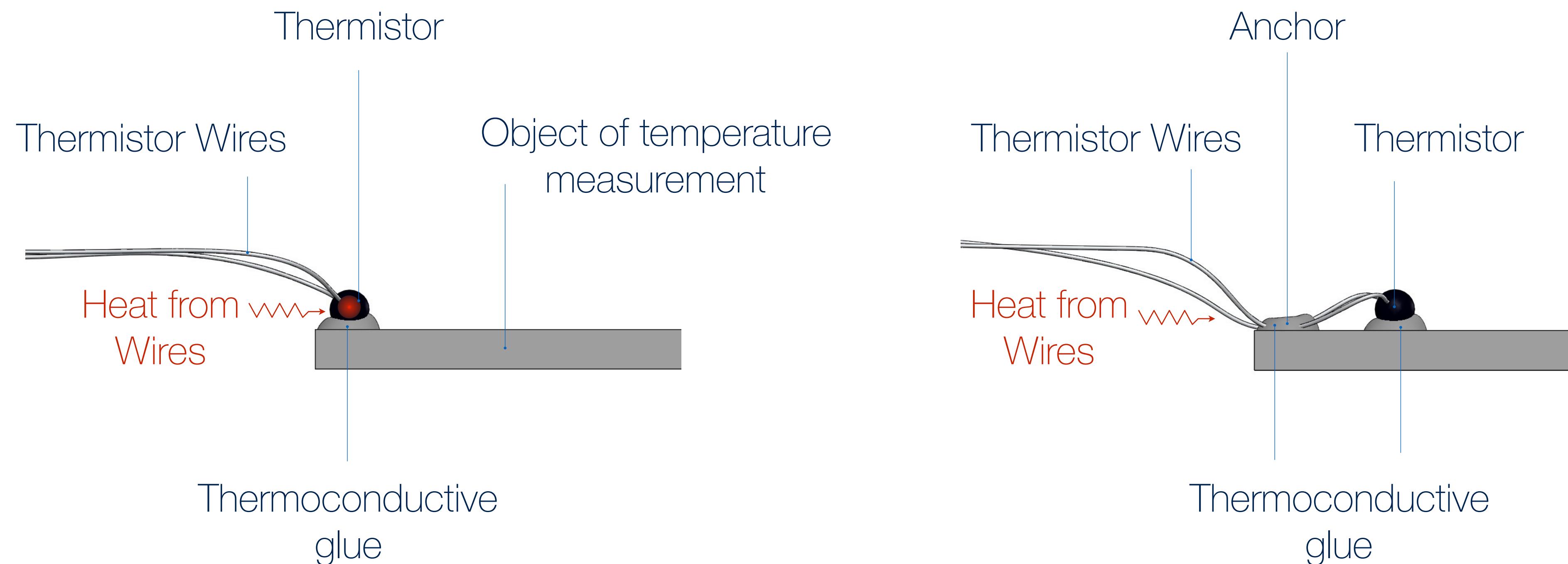


Mounting to TEC Cold Ceramics Edge





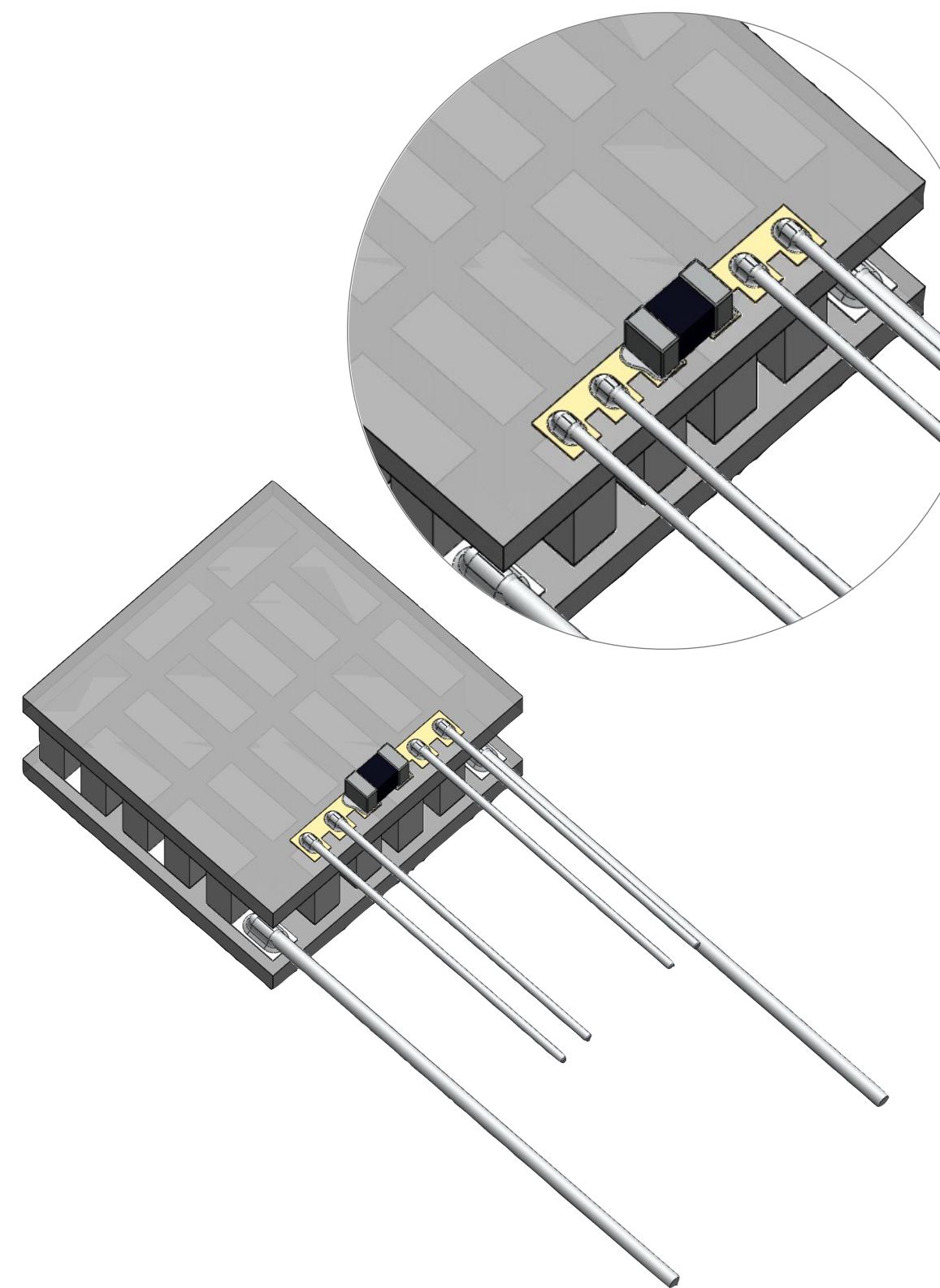
## Thermistor Mounting - Anchoring Thermistor Wires (EXAMPLE)



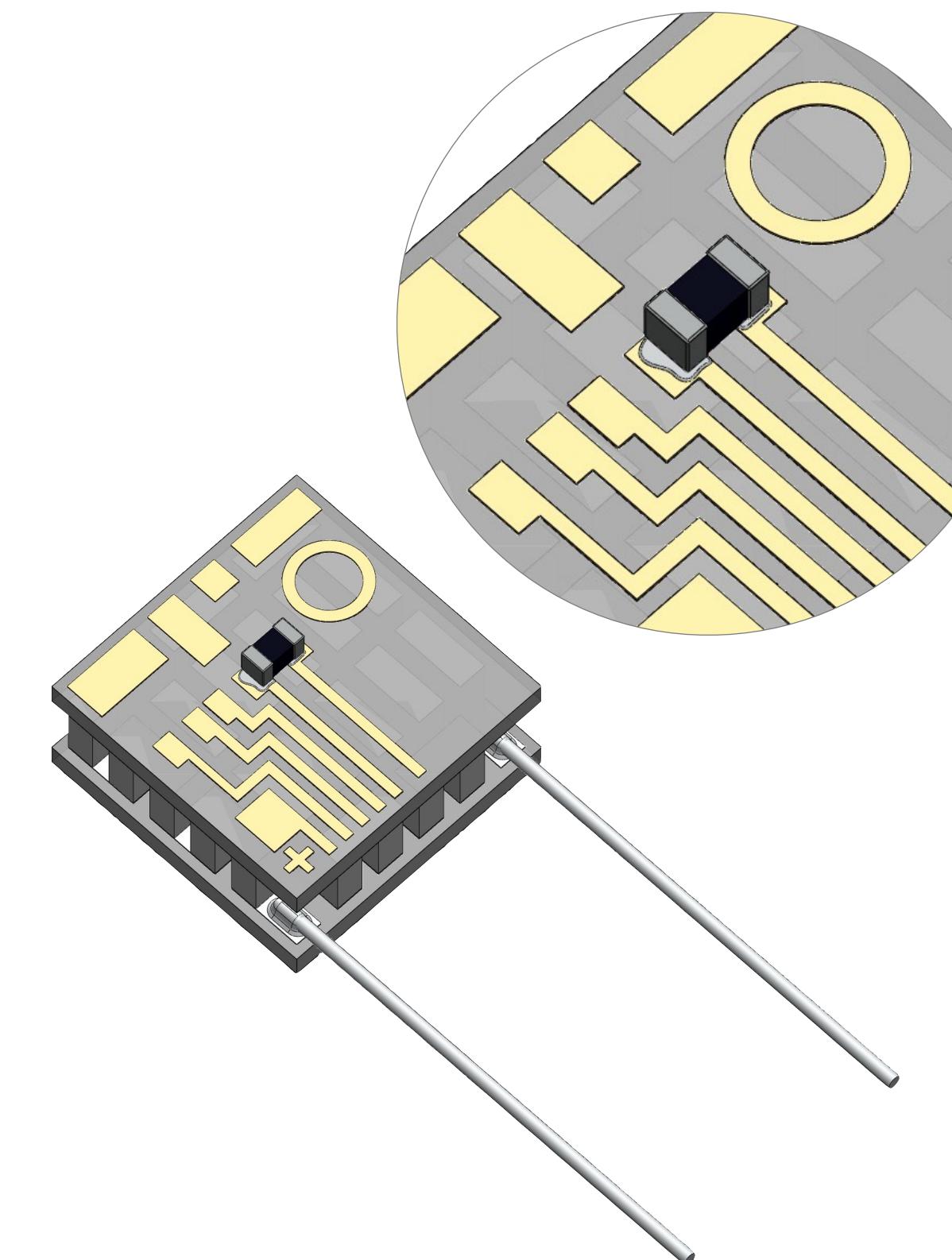
Certain amount of heat coming from thermistor wires may distort temperature measurement results.  
It's recommended to anchor thermistor wires for better temperature measurement results.



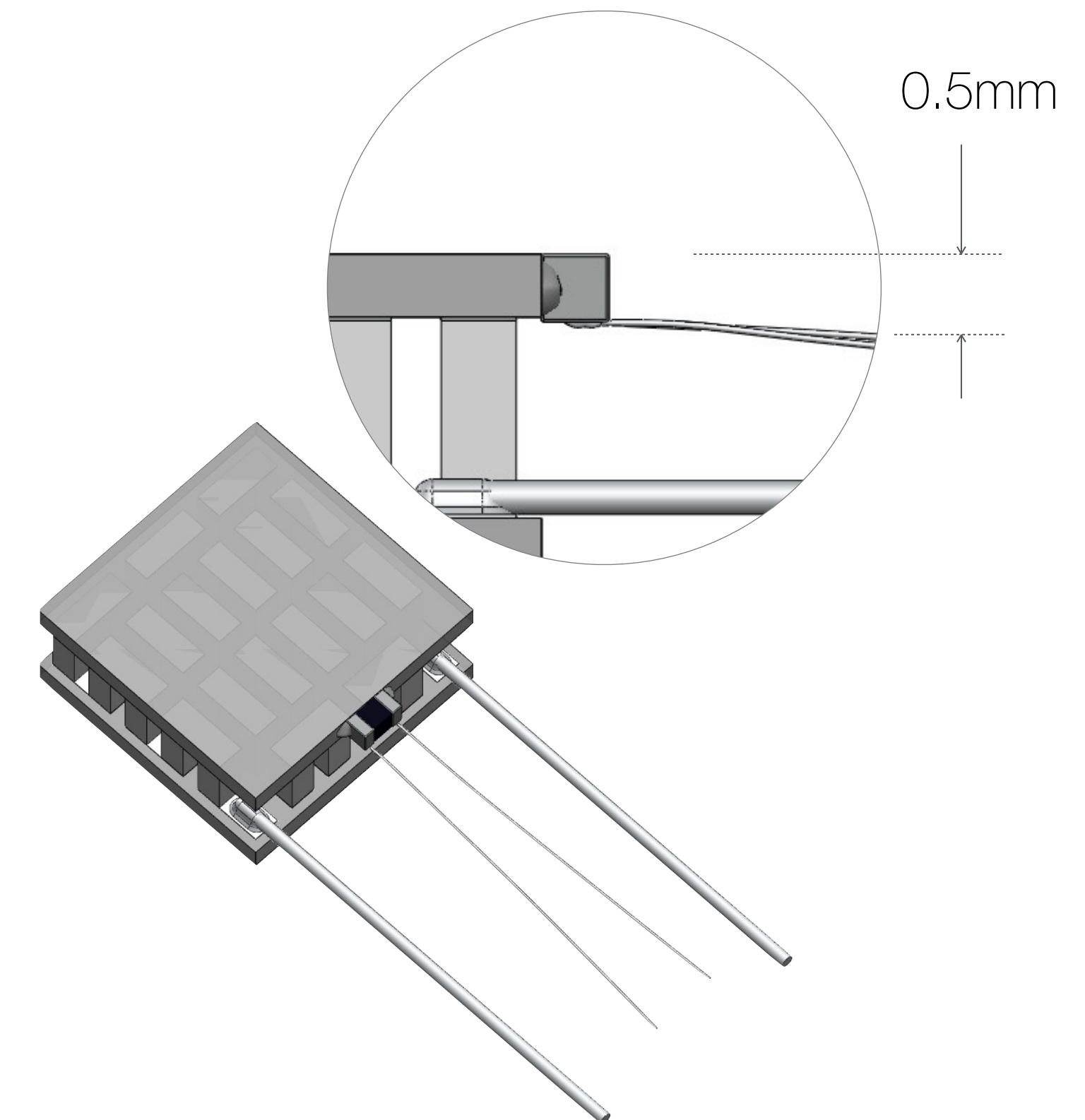
## Thermistors - SMT-type NTC Solutions



SOLUTION #1  
Soldering to TEC Cold Side  
Au Pattern for thermistor



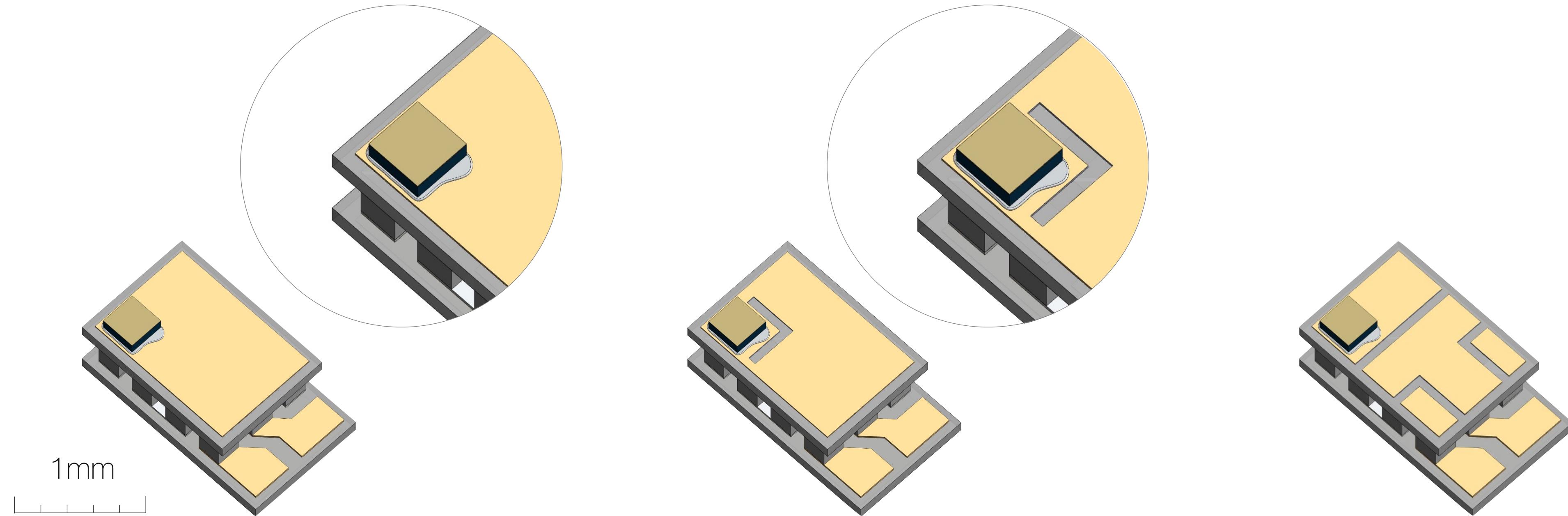
SOLUTION #2  
Soldering to TEC Cold Side  
Application Special Au pattern



SOLUTION #3  
Gluing Method with Wires  
soldered to SMT Thermistor

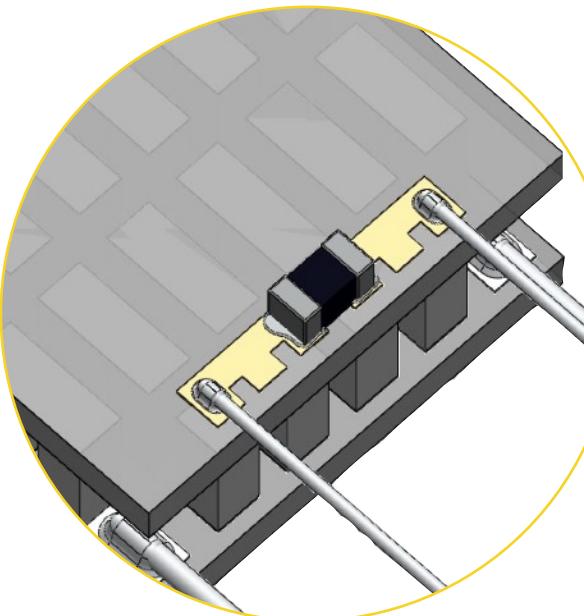
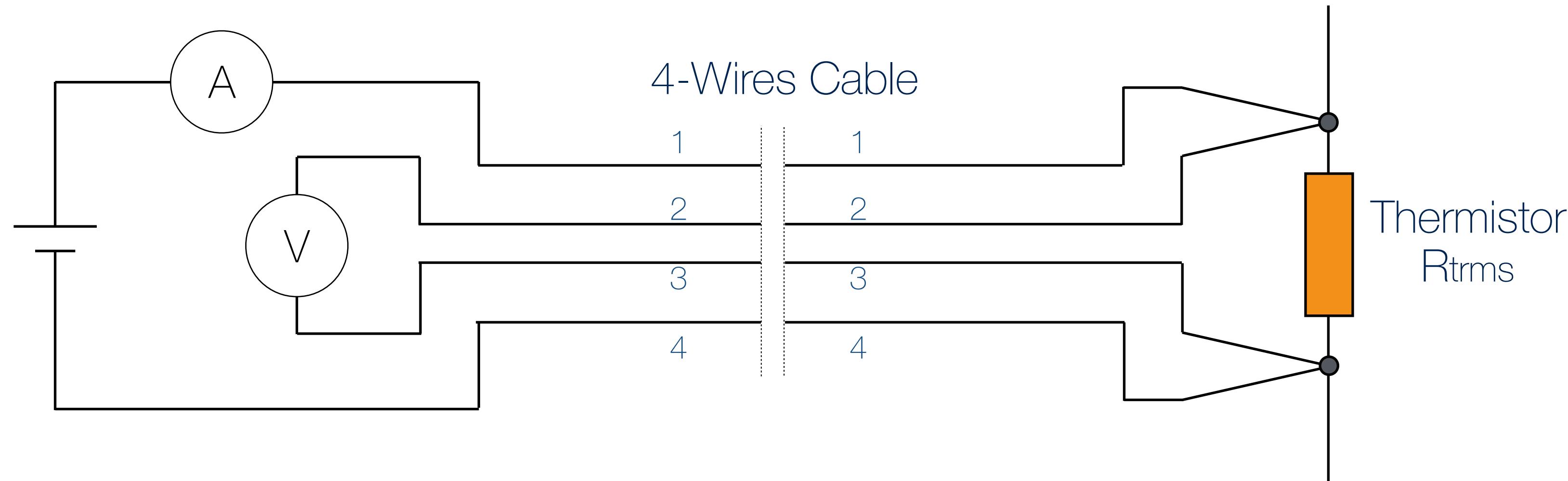


## Thermistors - Miniature Lead-less Thermistors for WB process

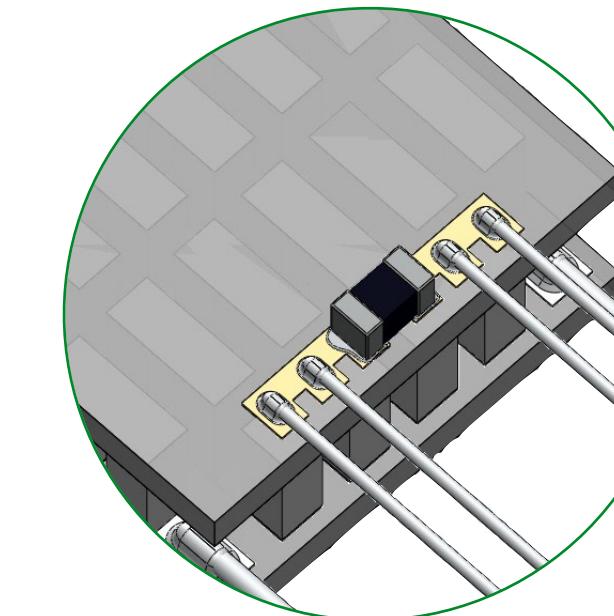




## Thermistor Resistance Measurement - 4-Wires Measurement Scheme



2-Wires Method



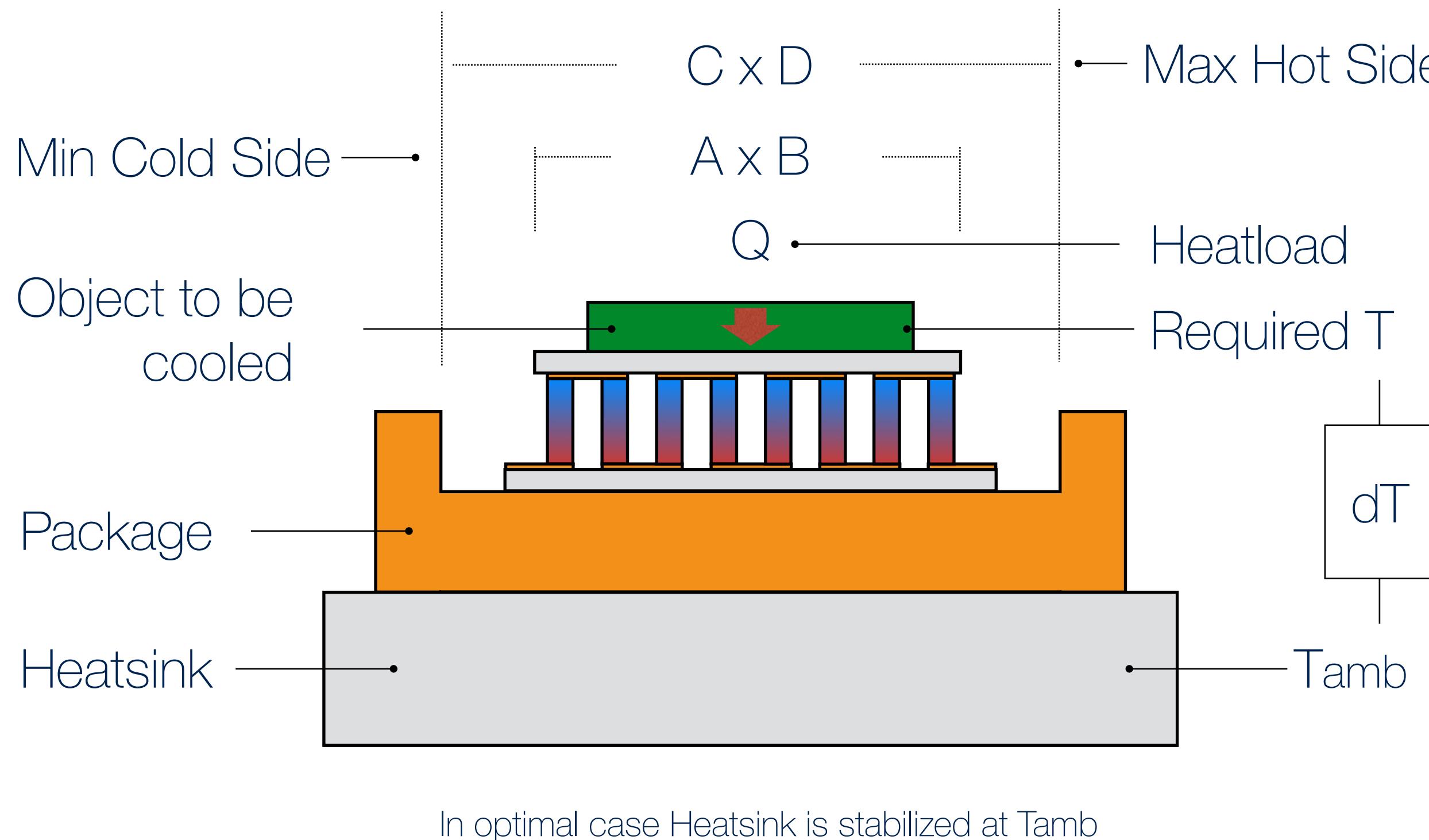
4-Wires Method

$$R_{trms} = \frac{\text{Voltmeter Indication}}{\text{Ammeter Indication}}$$

Long Thermistor Wires and Header pins may distort actual Thermistor Resistance value during measurements. 4-wires Measurement Method is recommended for the most accurate measurement results.



## Finding the most optimal TEC - Application Parameters Required



### Primary Set

1. Max Ambient Temperature
2. Ambient Conditions (gas, vacuum)
3. Total Heatload in Application
4. Max required  $dT$  from Ambient
5. Min required Cold Side
6. Max available space for Hot Side

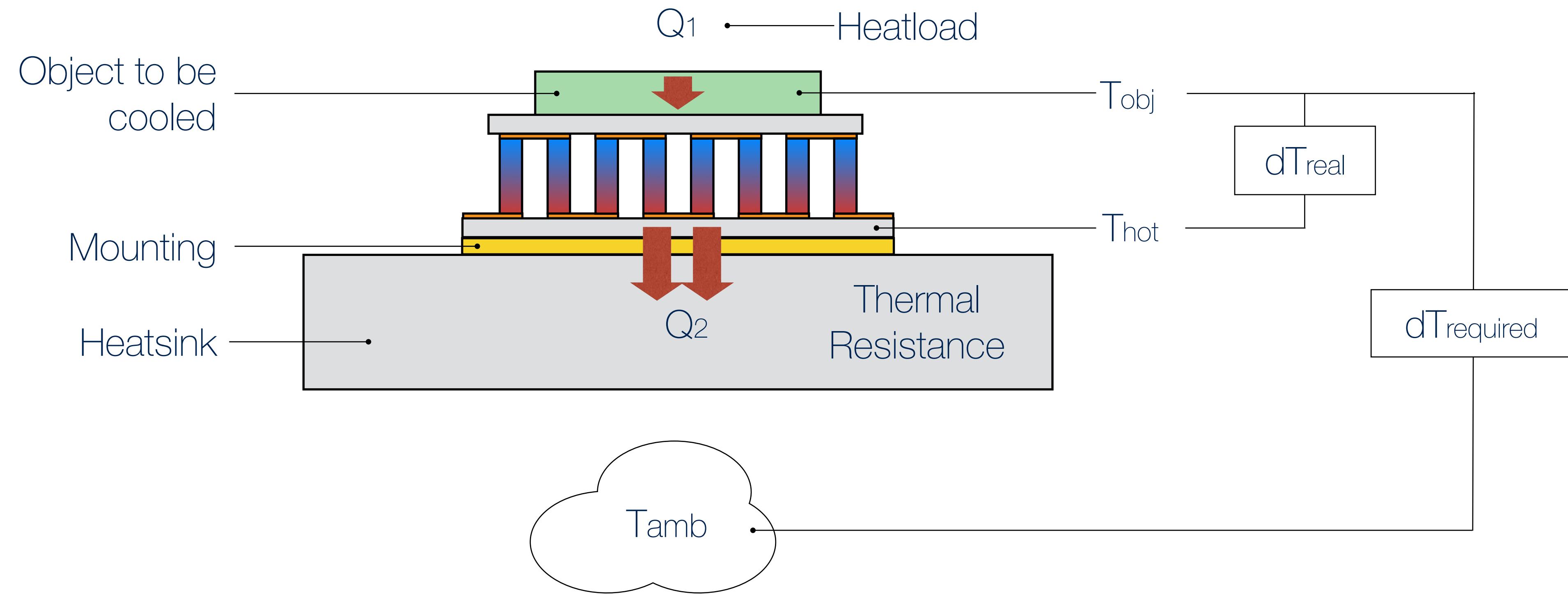
### Secondary Set

7. TE Cooler Height Limit
8. Electrical Power limits (if any)
9. Heatsink Thermal Resistance
10. Package Type and Materials

Items 1-6 are the minimum set of application parameters to start finding the most optimal TE Cooler



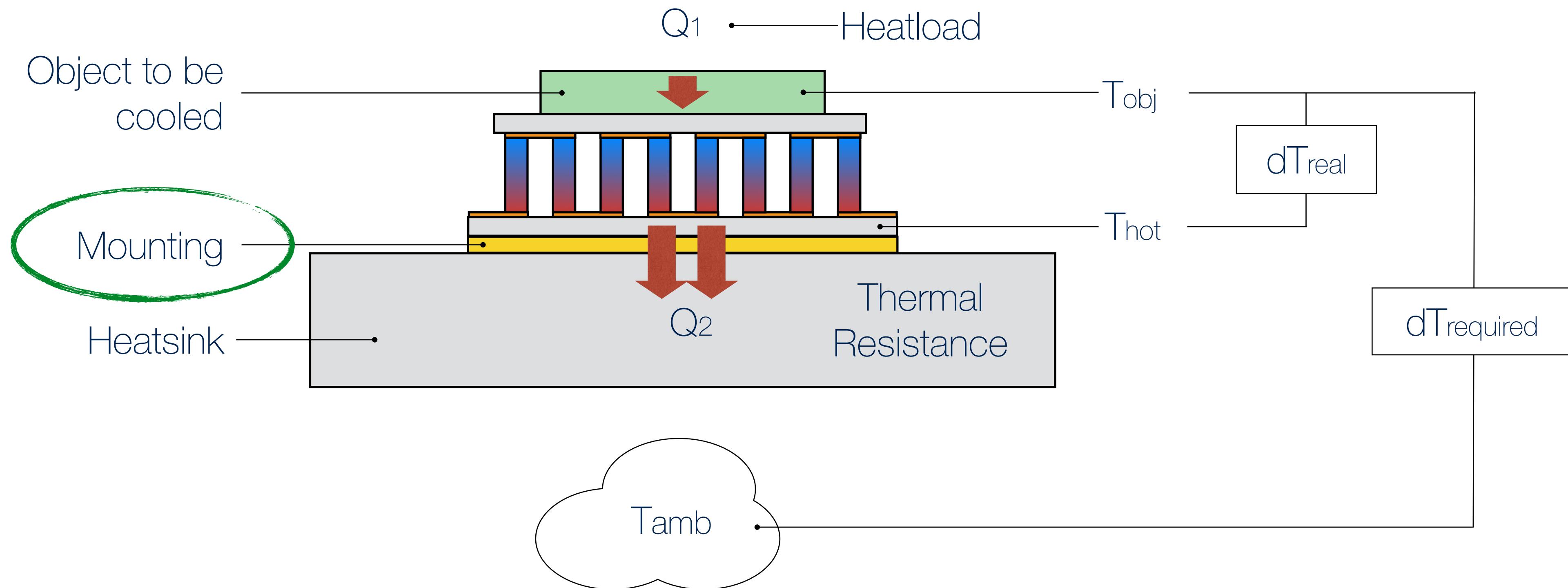
## Optimal and Real Application Conditions - Hot Side Overheating Issue



Heat  $Q_2$  from TEC Hot Side is  $Q_1 + \text{TEC } (I \times U)$ . Heatsink and Package have Thermal Resistances  
Thus in most cases:  $T_{hot} > T_{amb}$  and  $dT_{real} > dT_{required}$



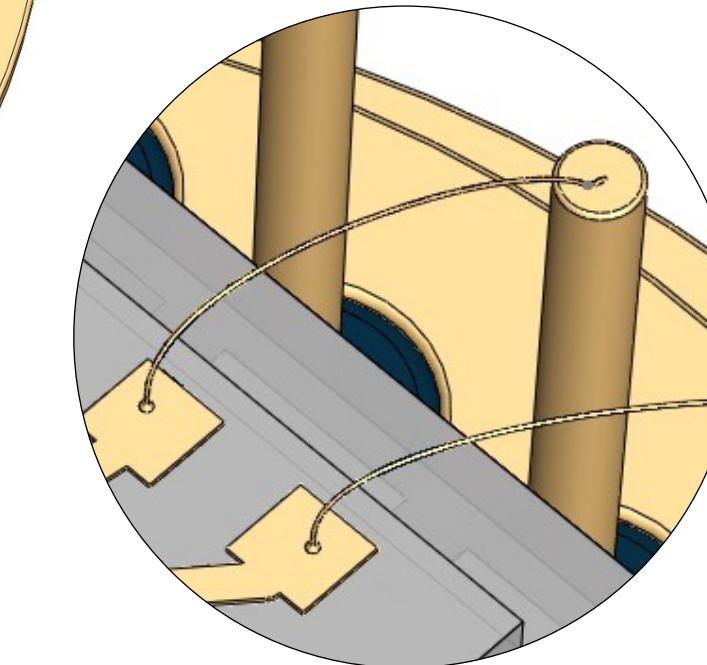
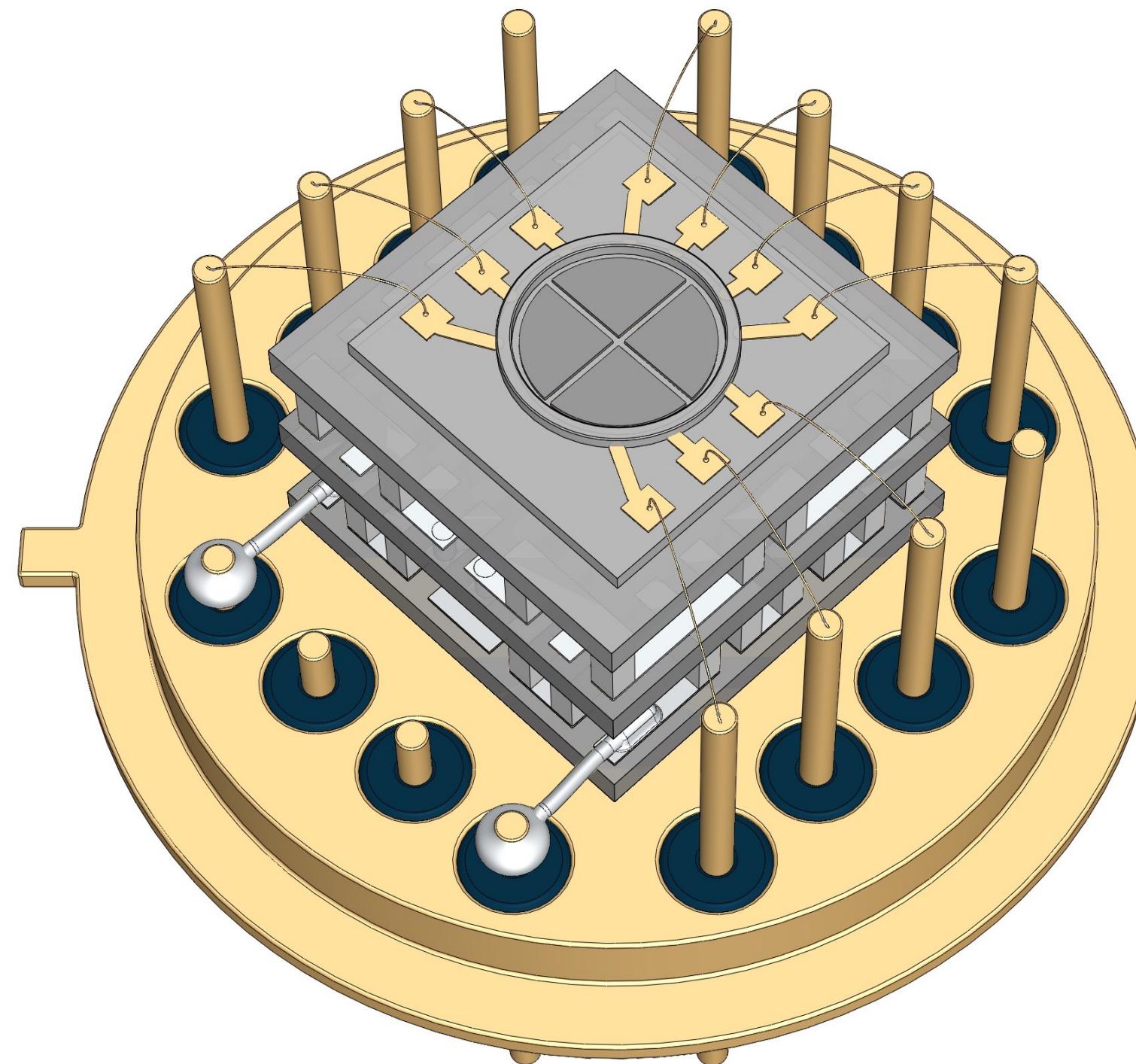
## Application Conditions Optimal and Real - Hot Side Overheating Issue



Mounting method and materials are important to avoid overheating and low performance issues. Soldering is usually the most optimal method by thermal conductivity and mechanical properties.



## Extra Heatload Coming by Wires on TEC Cold Side



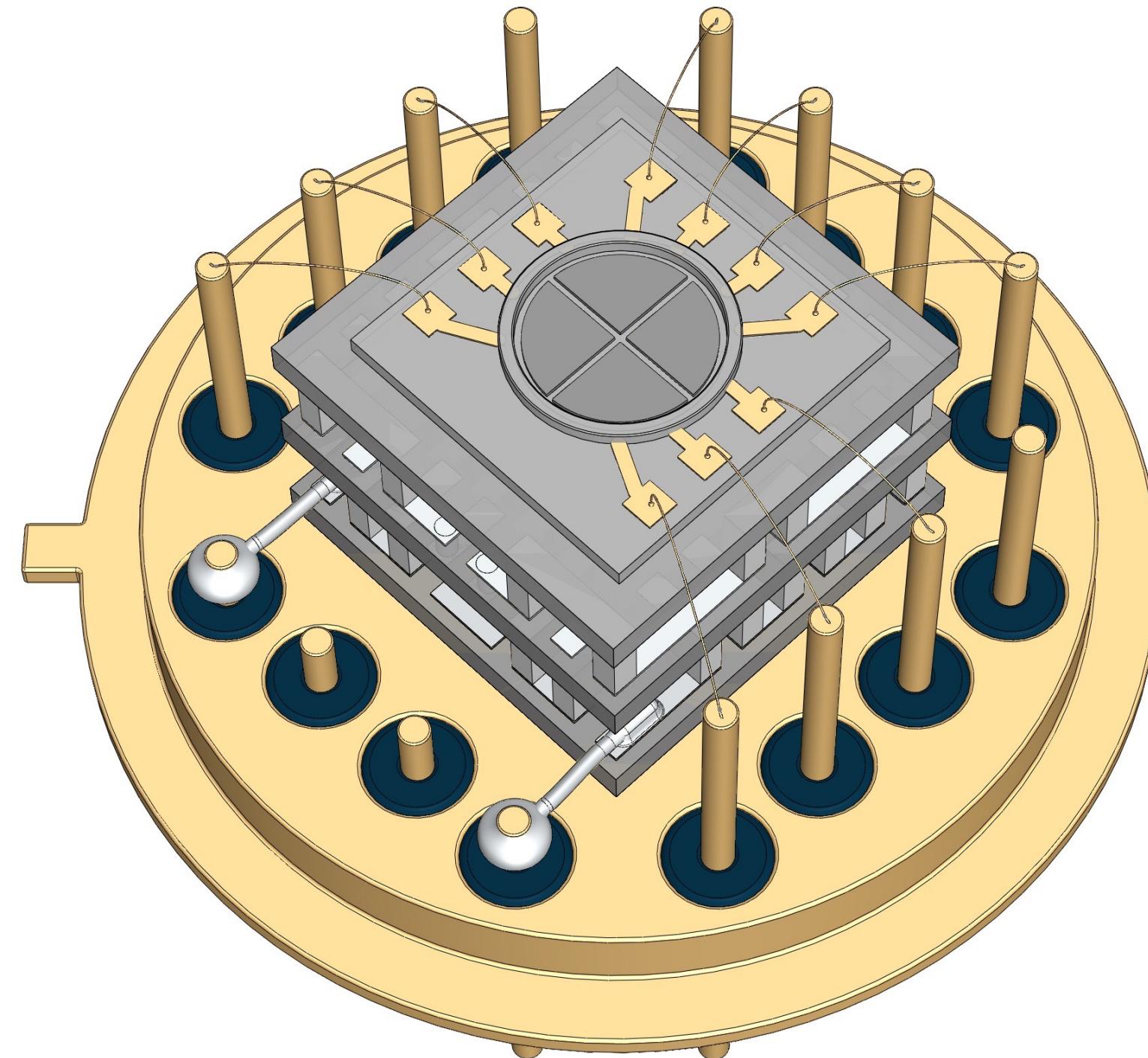
Heat coming by wires can be estimated by simplified formula

$$Q_{\text{wires}} = N \times K \times \frac{S}{L} \times dT$$

- N - Number of wires
- K - Wires Material Thermal Conductivity
- S - Wire Cross-section
- L - Wire Length
- dT - Temperature difference in application  
(between TEC cold side and header)

WB wires length, diameter and material are very important in minimizing passive heatload.  
Improper WB wire type choice may lead to unexpected and significant heatload in final application.

## Extra Heatload Coming by Wires on TEC Cold Side, Example

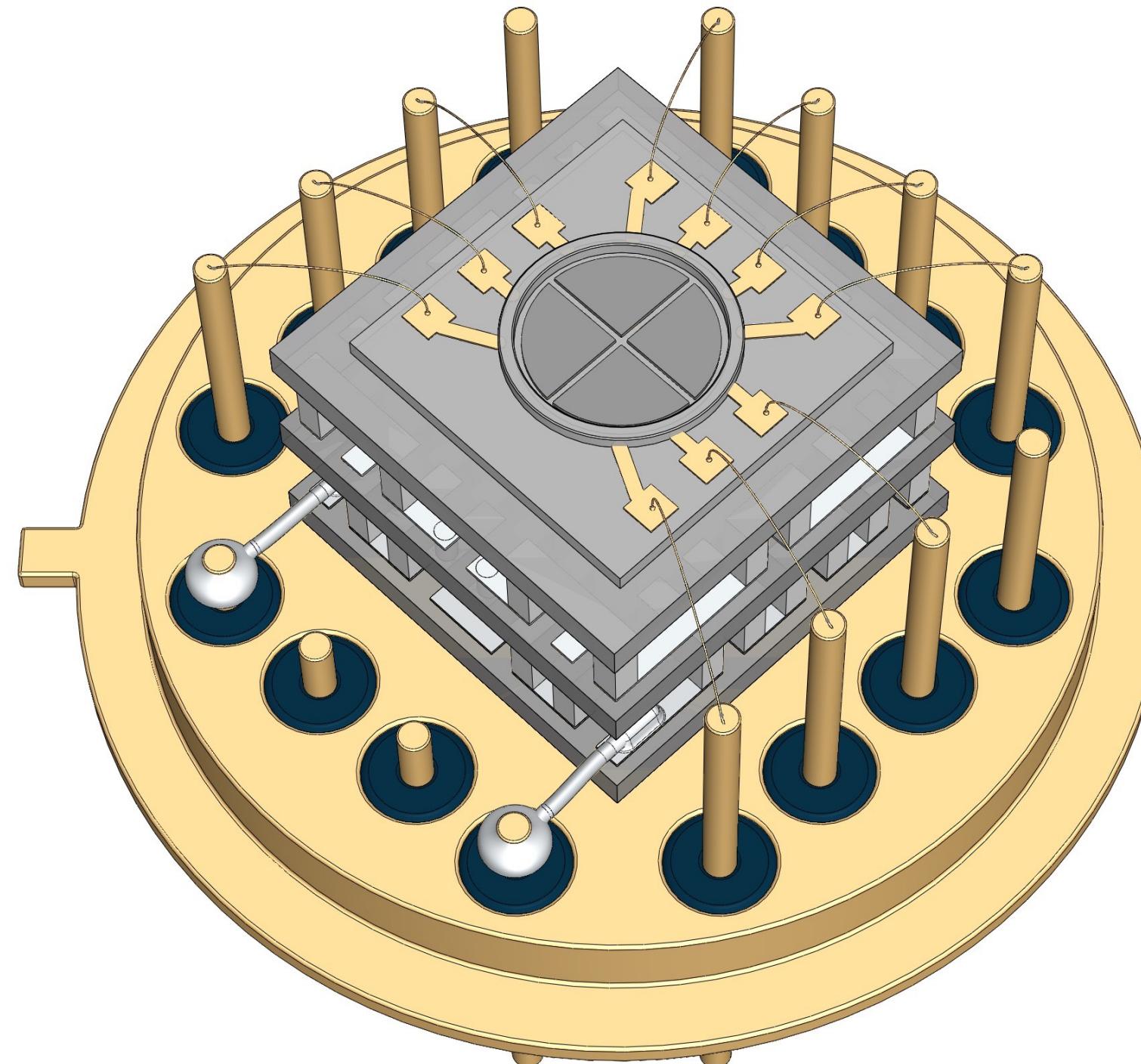


N = 10 (number of wires)  
D = 50um (diameter) = 0.05mm = 0.5E-4 m  
K = 317 W/mK (Gold wires)  
 $S = (\pi \times D^2)/4 = 0.196E-8 \text{ m}^2$   
L = 3.5mm = 0.0035m  
dT = 80K (between TEC cold side and header)

$$Q_{\text{wires}} = 10 \times 317 \times \frac{0.196E-8}{0.0035} \times 80 = 0.142W$$

WB wires length, diameter and material are very important in minimizing passive heatload.  
Improper WB wire type choice may lead to unexpected and significant heatload in final application.

## Extra Heatload Coming by Wires on TEC Cold Side, Materials Comparison



Example #1:  $dT=80K$ , 10 WB Wires, 50um dia, 3.5mm Length

Property	Units	Au	Al	Pt
Thermal Conductivity	W/(m x K)	317	237	72
Resulting Heatload	mW	142	106	32

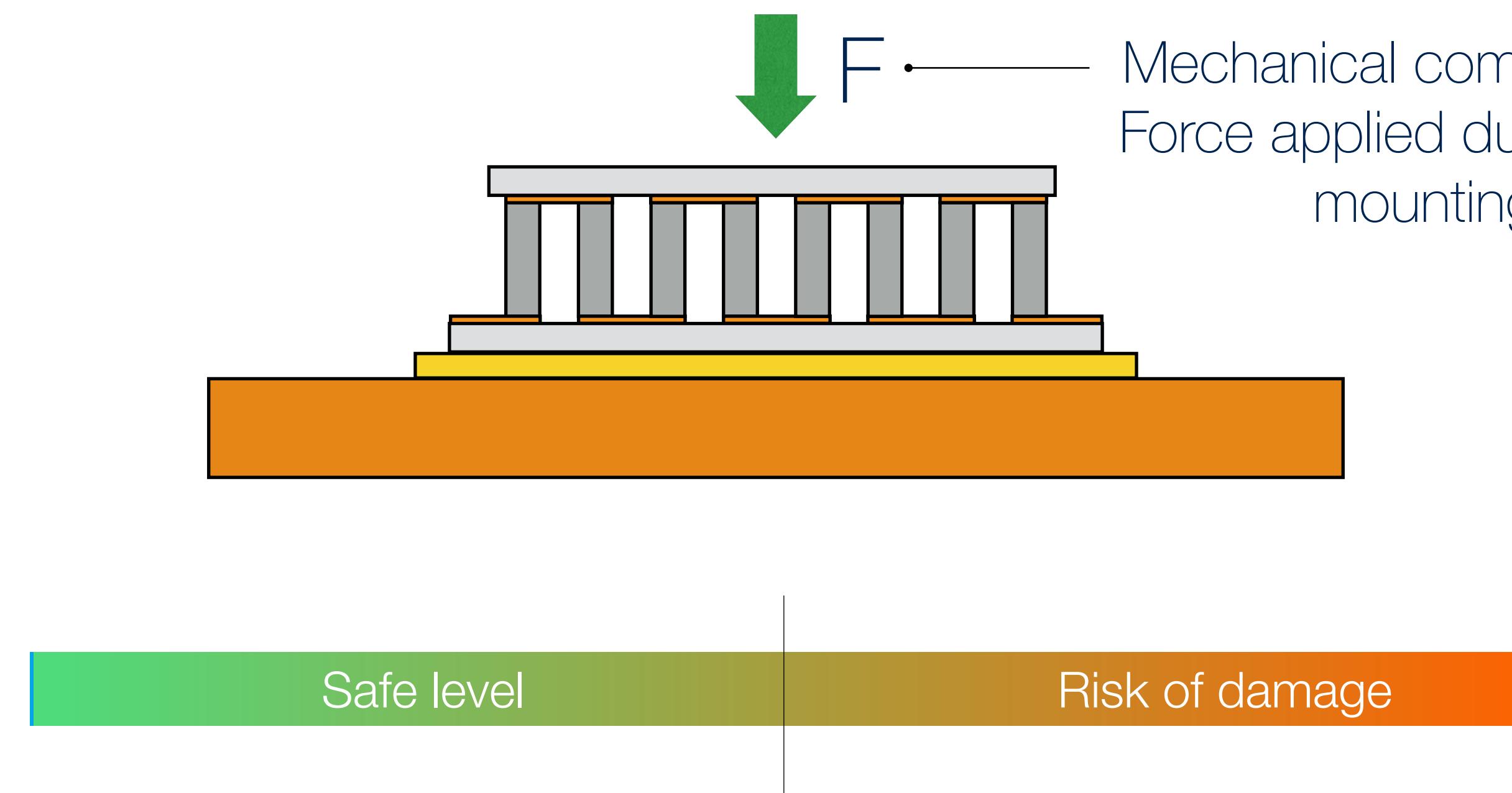
.. but if to apply **20um** dia wires (instead of 50um)

Resulting Heatload	mW	23	17	5
--------------------	----	----	----	---

WB wires length, diameter and material are very important in minimizing passive heatload.  
Improper WB wire type choice may lead to unexpected and significant heatload in final application.



## Max Compression Force during TEC mounting



Mechanical compression  
Force applied during TEC  
mounting

Example with TEC\*

1ML06-023-10

0.6x0.6mm<sup>2</sup>      23 pellet  
Pellets      Couples

$$F_{max} = 1 \text{ kg per mm}^2$$

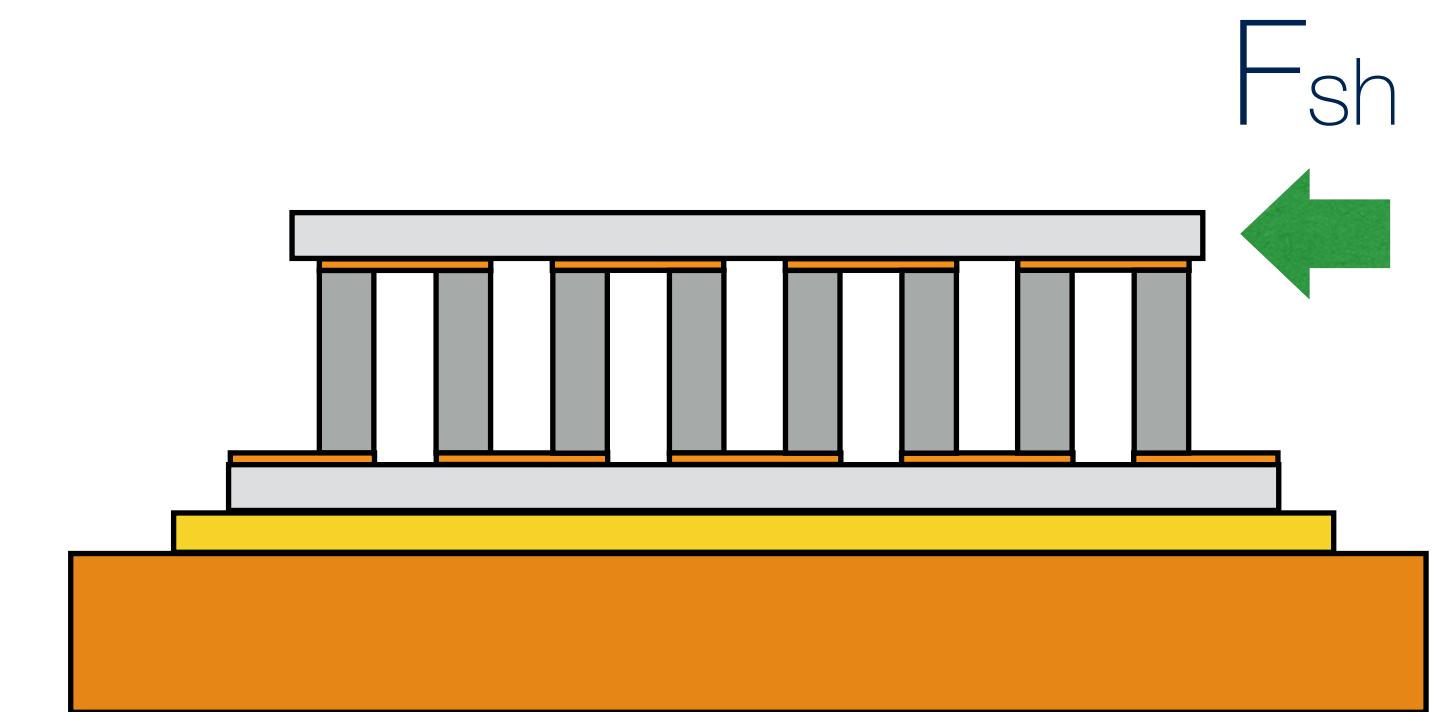
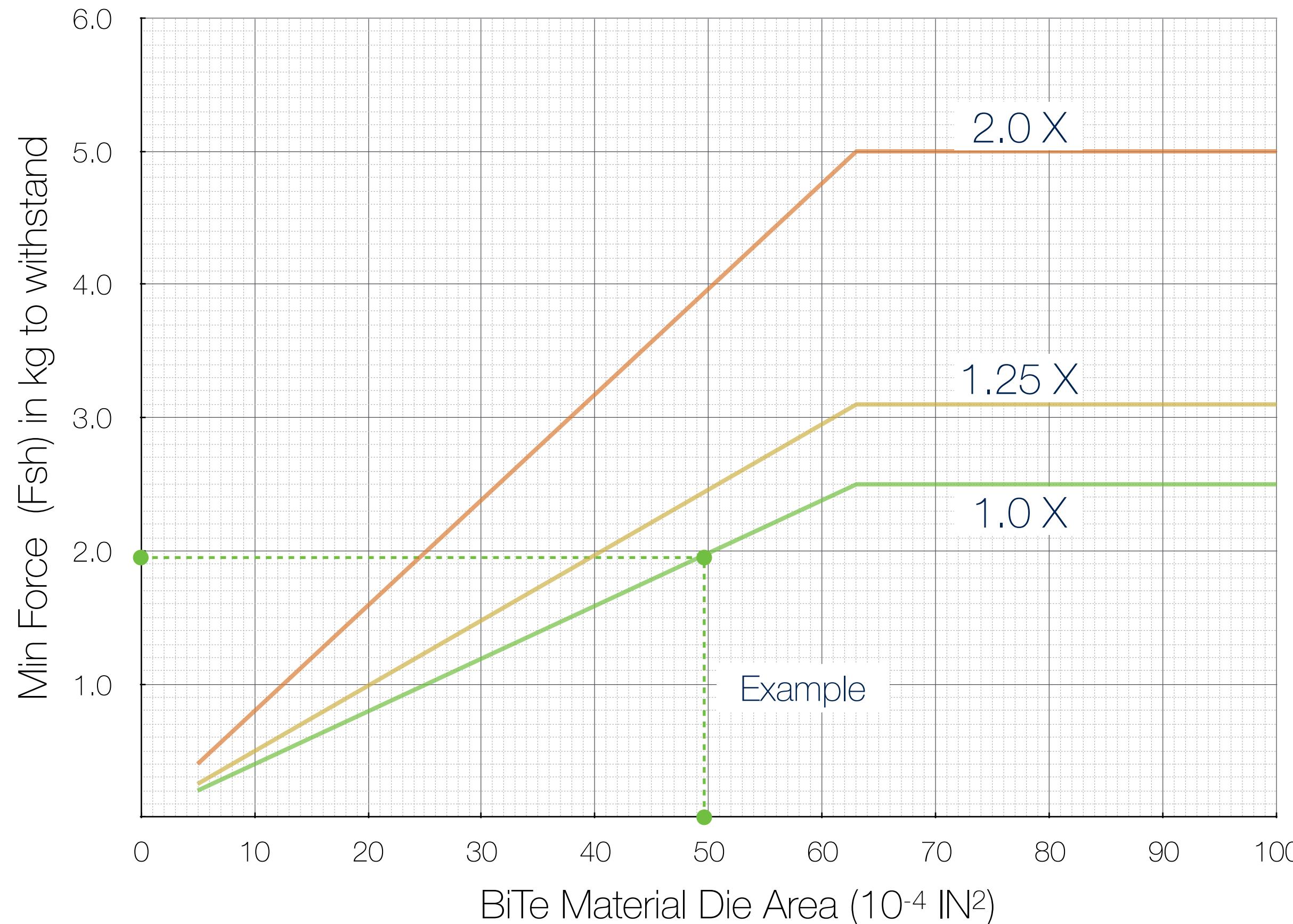
BiTe die area inside  
TEC

$$F_{max} = 0.6 \times 0.6 \times 23 \times 2 = 16.5 \text{ kg}$$

\* TEC Microsystems uses the patented nomenclature system, where TEC type name describes TEC internal construction



## TE Coolers and Shear Force



Example with TEC Microsystems TEC

1MC04-010-05

0.4x0.4mm<sup>2</sup>  
Pellets      10 pellet  
                Couples

BiTe Die Area =  $0.4 \times 0.4 \times 10 \times 2 = 3.2 \text{ mm}^2 = 49.6(10^{-4} \text{ IN}^2)$

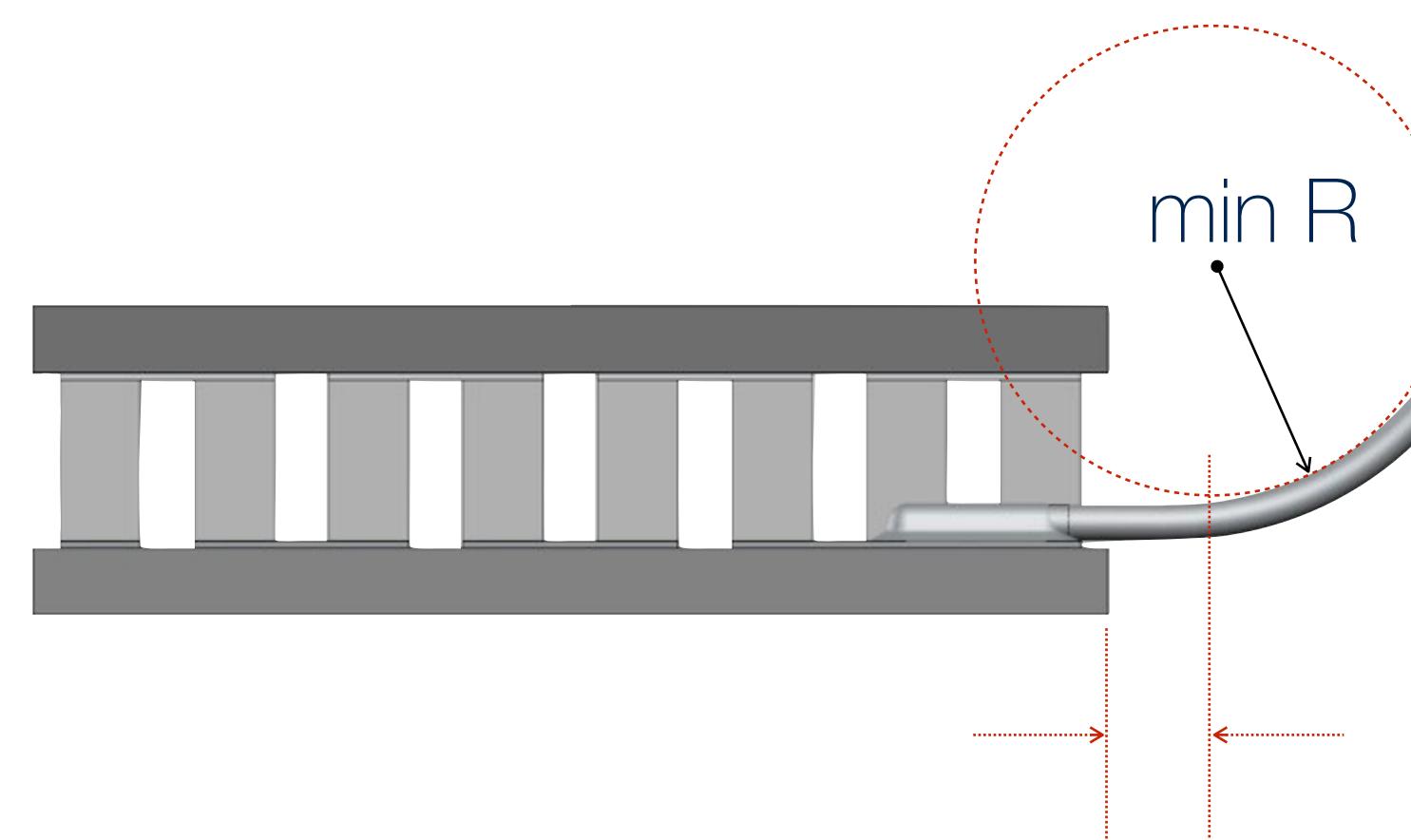
MIN force (1.0X) to withstand is 1.95kg (per chart)

By Telcordia GR-468 Standard (based on MIL-STD-883F, method 2019.7) TEC must endure, at least, the minimal given effort to shift (1.0X)



## Wire integrity and Bending

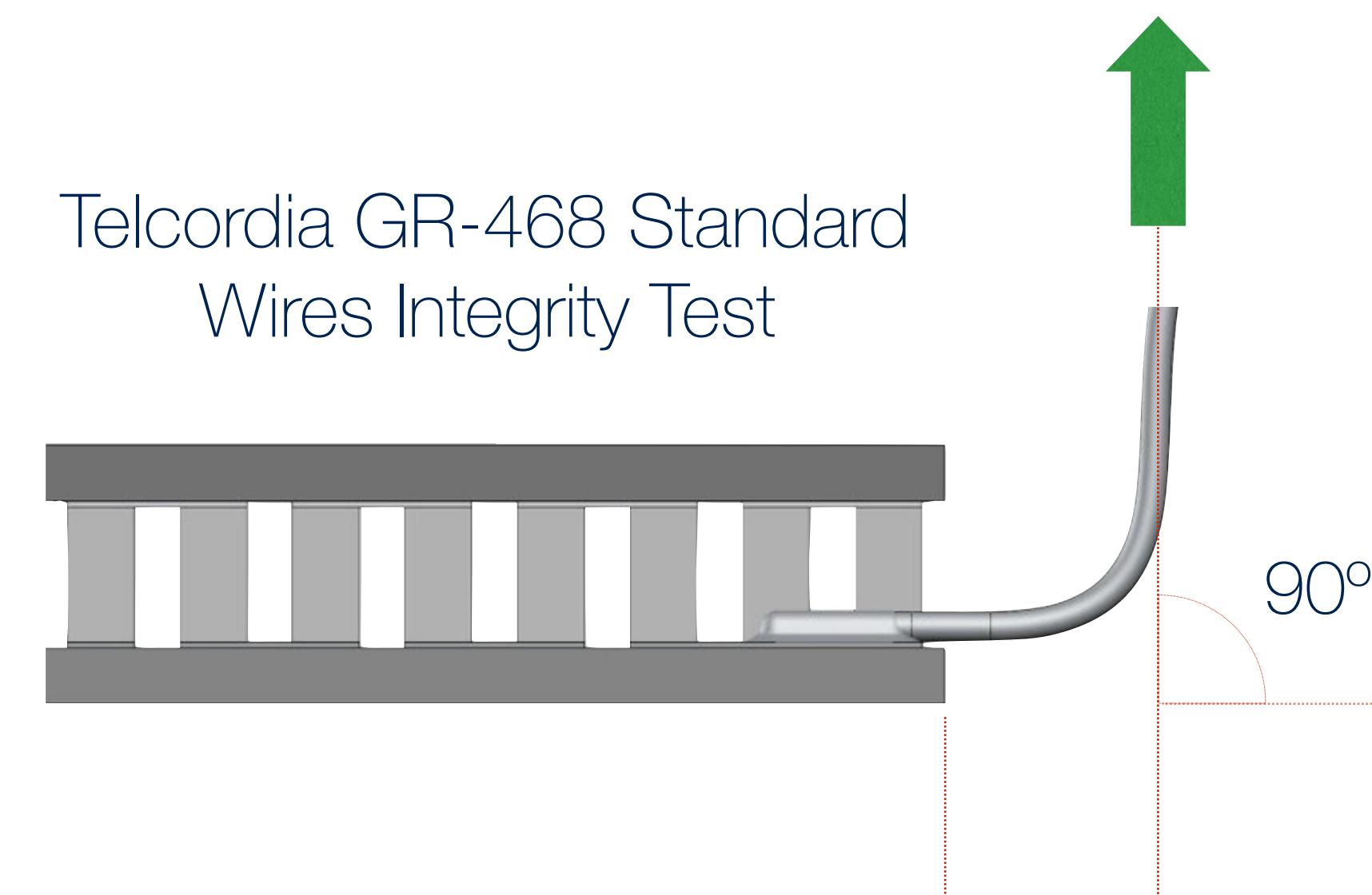
MIN bend Radius: 0.5mm  
Recommended: 4x Wire Dia



1.0 mm MIN  
Safe Area  
(do NOT bend closer)

Max Pull 8 oz  
(2.2N)

Telcordia GR-468 Standard  
Wires Integrity Test

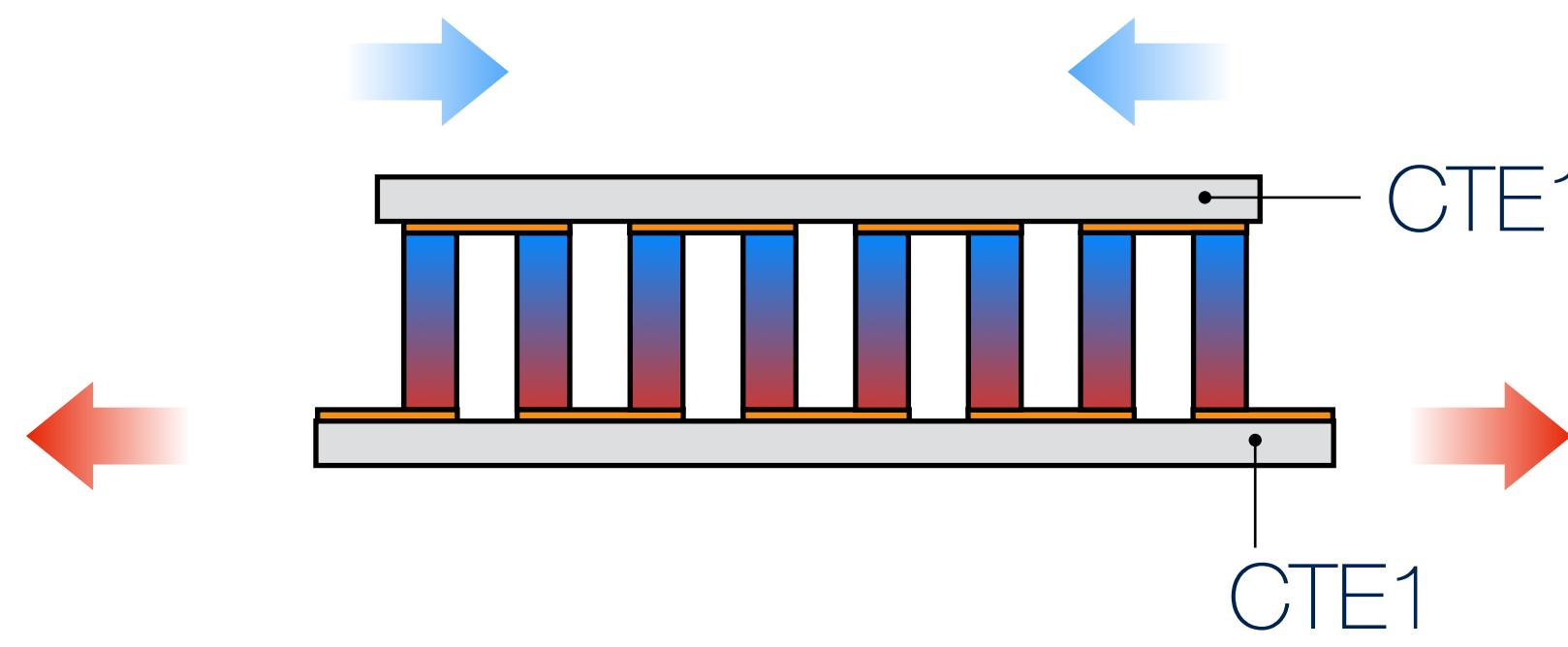


Control Force Level, MIN bending Radius and safe Distance to avoid wires damaging or detachment

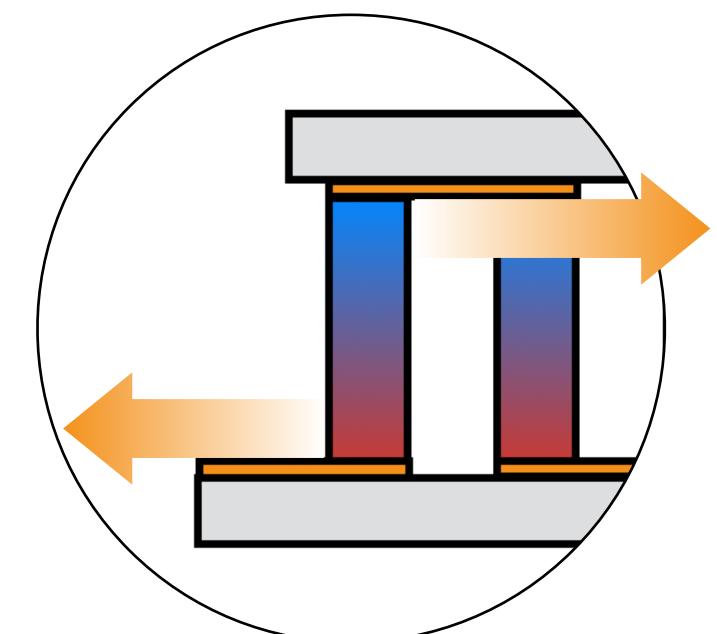


## Coefficient of Thermal Expansion (CTE) - Basics

During TEC operating  
Cold Side shrinks

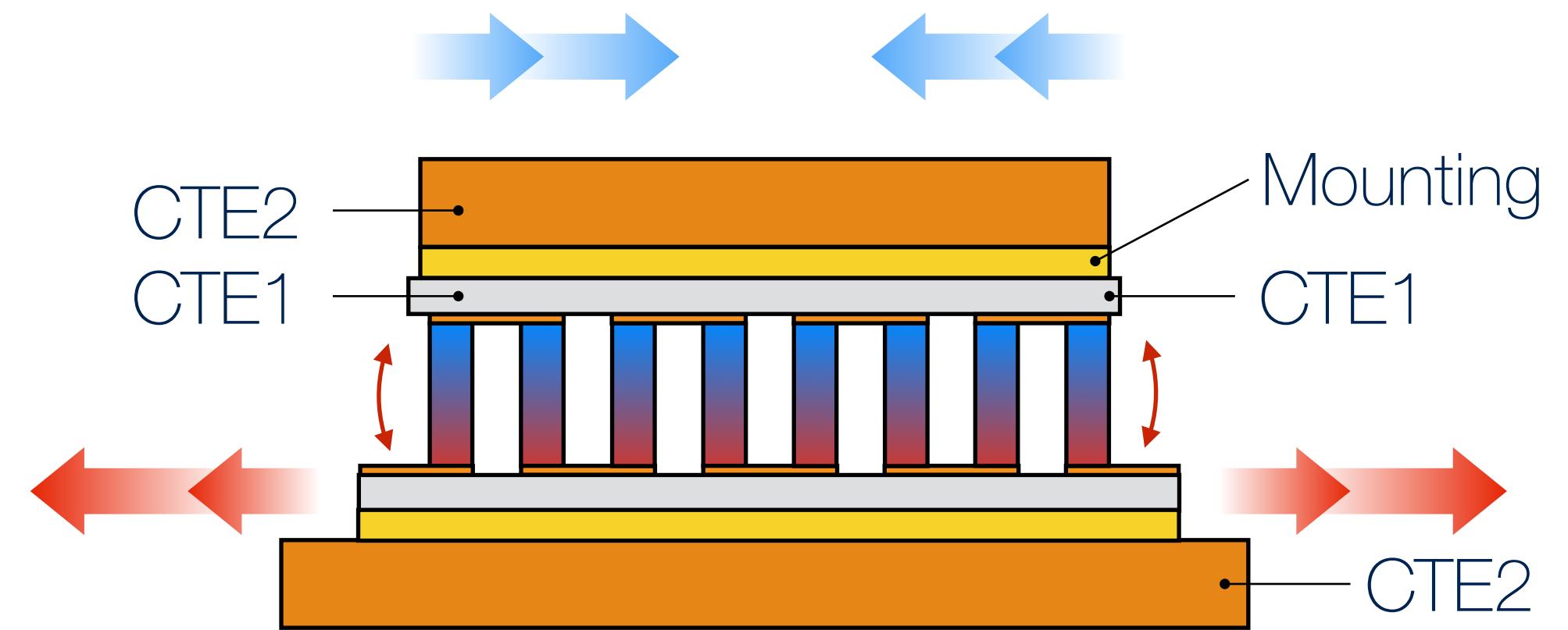


Hot Side expands



Mechanical Strains on Pellets  
Safe Level

$CTE_2 >> CTE_1$



Mechanical Strains on Pellets  
Pellet cracks



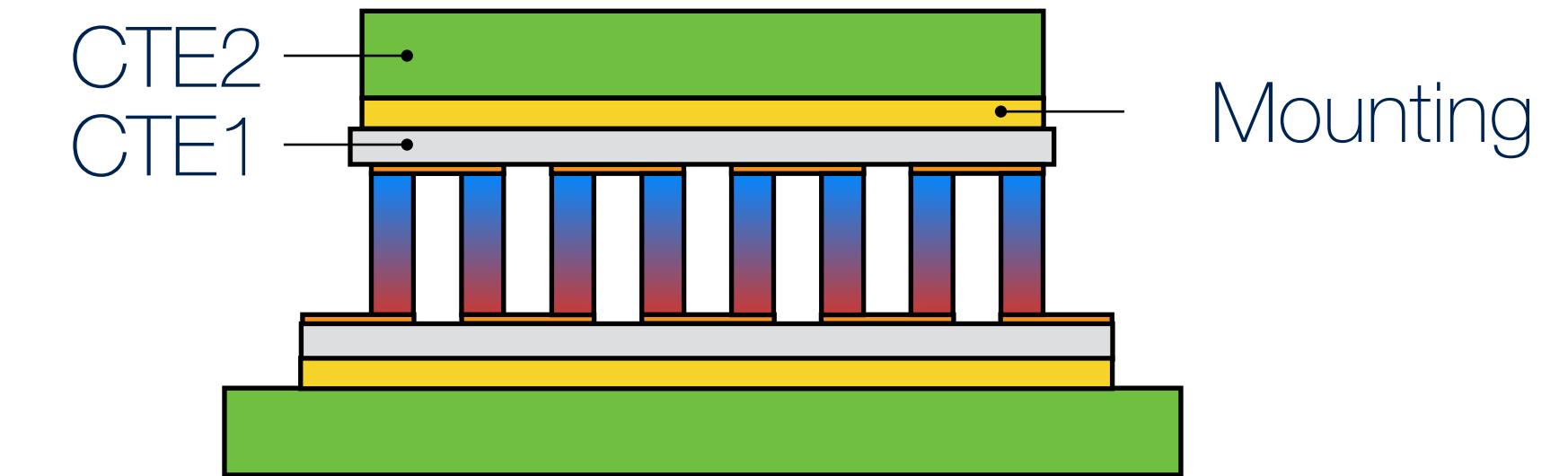
# Coefficient of Thermal Expansion (CTE) - Materials

Material	CTEx10-6, 1/K	Thermal Conductivity, W/mK	
Aluminium	22.5	237	risky
Bismuth Telluride	12.9	1.5	
Brass	18.0	110	risky
<b>Ceramics Al<sub>2</sub>O<sub>3</sub> - 100%</b>	<b>7.2</b>	30	friendly
<b>Ceramics Al<sub>2</sub>O<sub>3</sub> - 96%</b>	<b>7.0</b>	24	friendly
<b>Ceramics AlN</b>	<b>4.5</b>	170	friendly
Ceramics BeO	7.0	230	friendly
Cold-roll Steel (CRS)	11.5	50	friendly
Copper	16.7	400	risky
Copper-Molybdenum(15%-85%)	6.9	190	friendly
Copper-Molybdenum(25%-75%)	8.0	175	friendly
Copper-Wolfram(10%-90%)	6.7	180	friendly
Copper-Wolfram(20%-80%)	8.5	200	friendly
Gold	14.0	317	risky
Kovar	5.5	17	friendly
Nickel	13.4	90	risky
Platinum	9.0	72	friendly
Silicon	3.0	150	
Silver	18.9	429	risky
Stainless steel	17.1	14.5	risky

TEC  
ceramics

CTE2 ~ CTE1

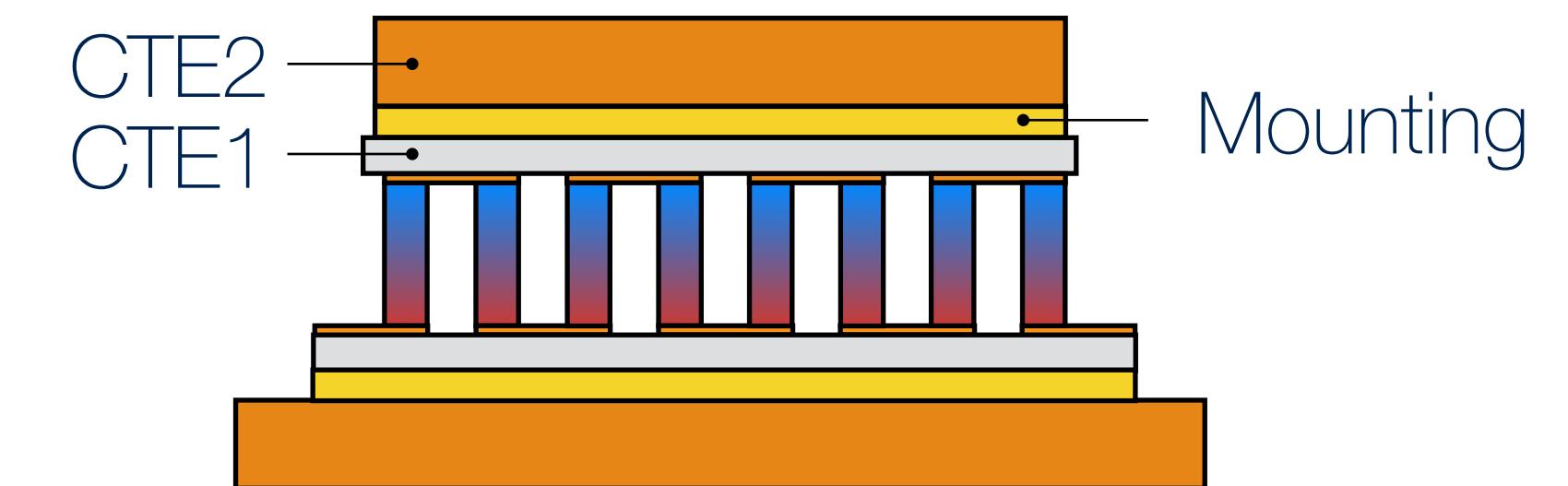
CTE friendly



Mounting

CTE2 >> CTE1

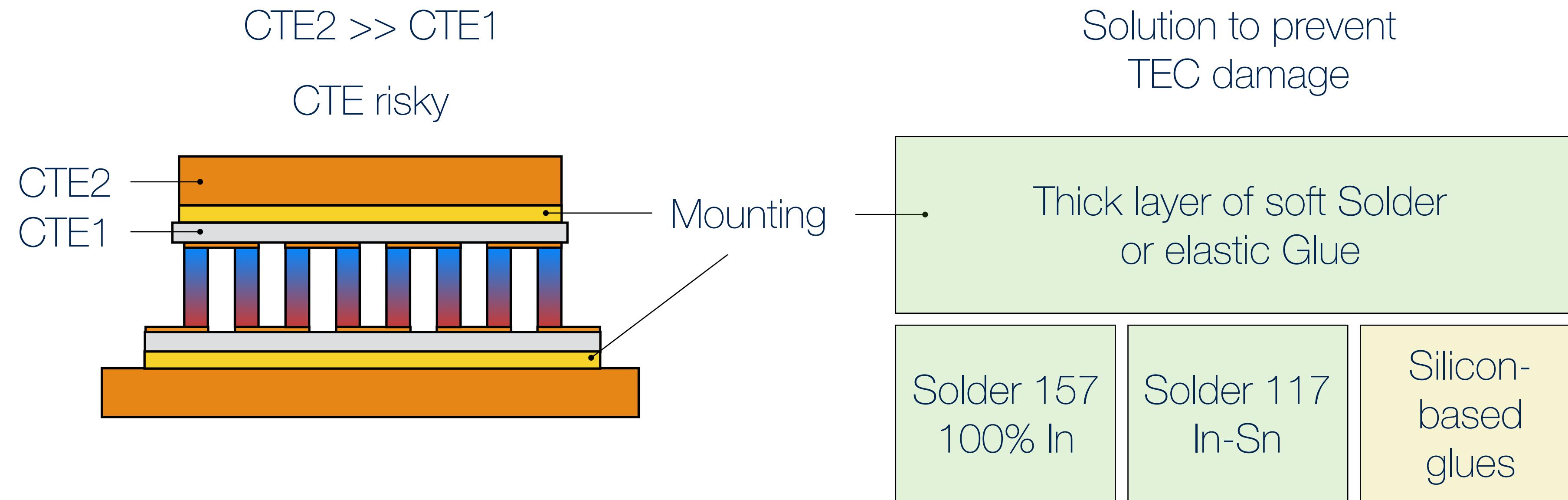
CTE risky



Mounting



## CTE Mismatch Issues - Solution #1 (recommended)

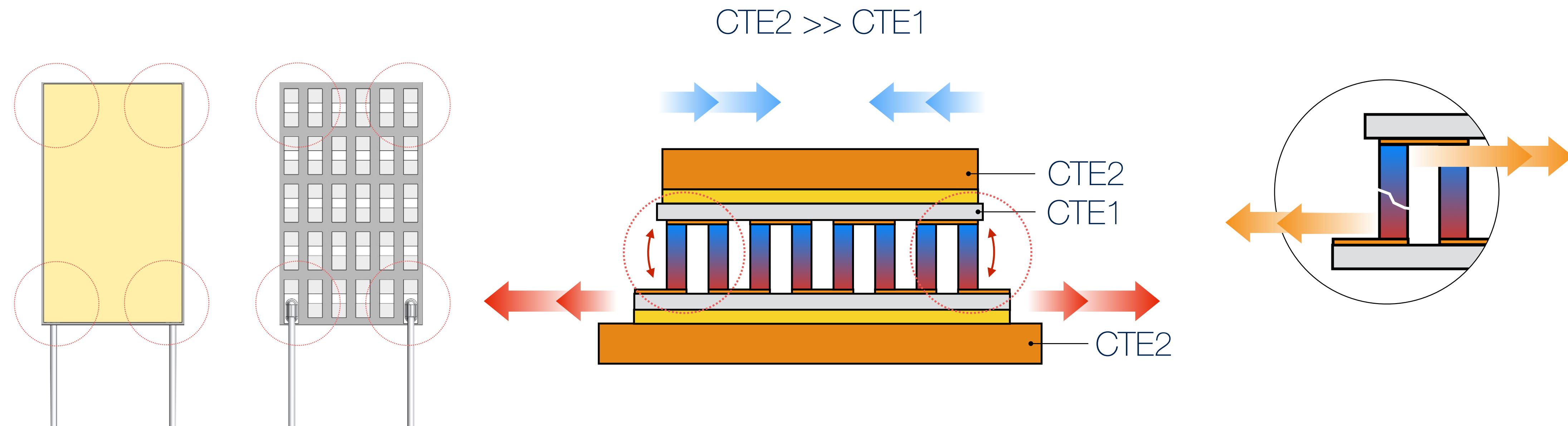


If it's not possible to avoid CTE risky materials, there is a solution to apply mounting with elastic materials - soft solders or silicon-based elastic glues



## CTE Mismatch Issues - Solution #2 “Flying Corners” (page1)

The most critical areas affected by thermomechanical strains due to CTE mismatch are located in corners inside TEC

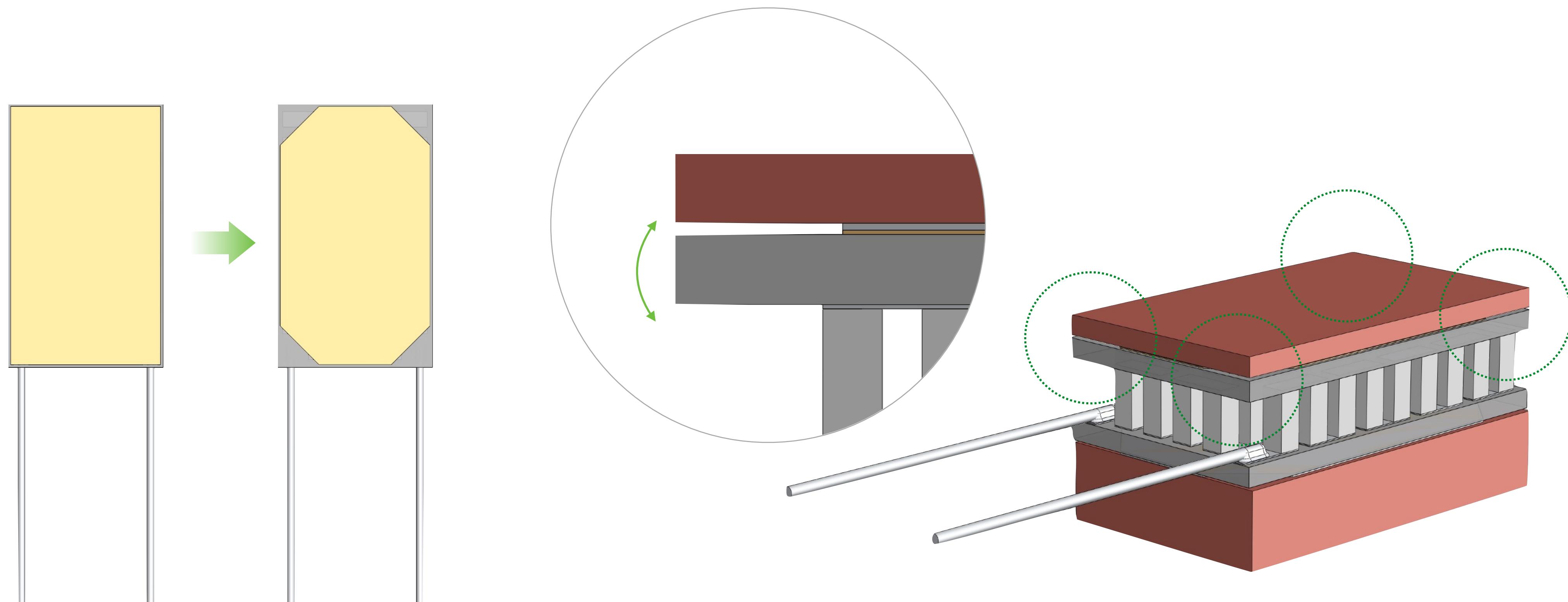


During thermomechanical stress caused by CTE mismatch in most cases pellets are damaged in TEC corner areas, where strain force affect reaches the maximum



## CTE Mismatch Issues - Solution #2 “Flying Corners” (page2)

“Flying corners” solution keeps TEC corner areas without Direct Contact to objects. TEC gets certain elasticity in corner areas, reducing strain affect on internal pellets.

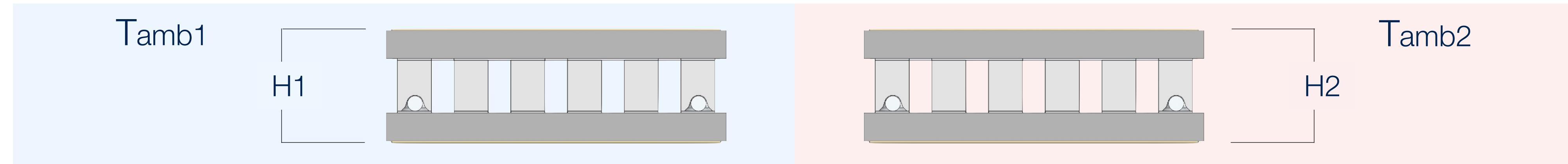


Up to ~15% contact area can be used for “flying-corners” w/o TEC performance reduction.  
The solution is recommended for soldering mounting with CTE risky materials only.



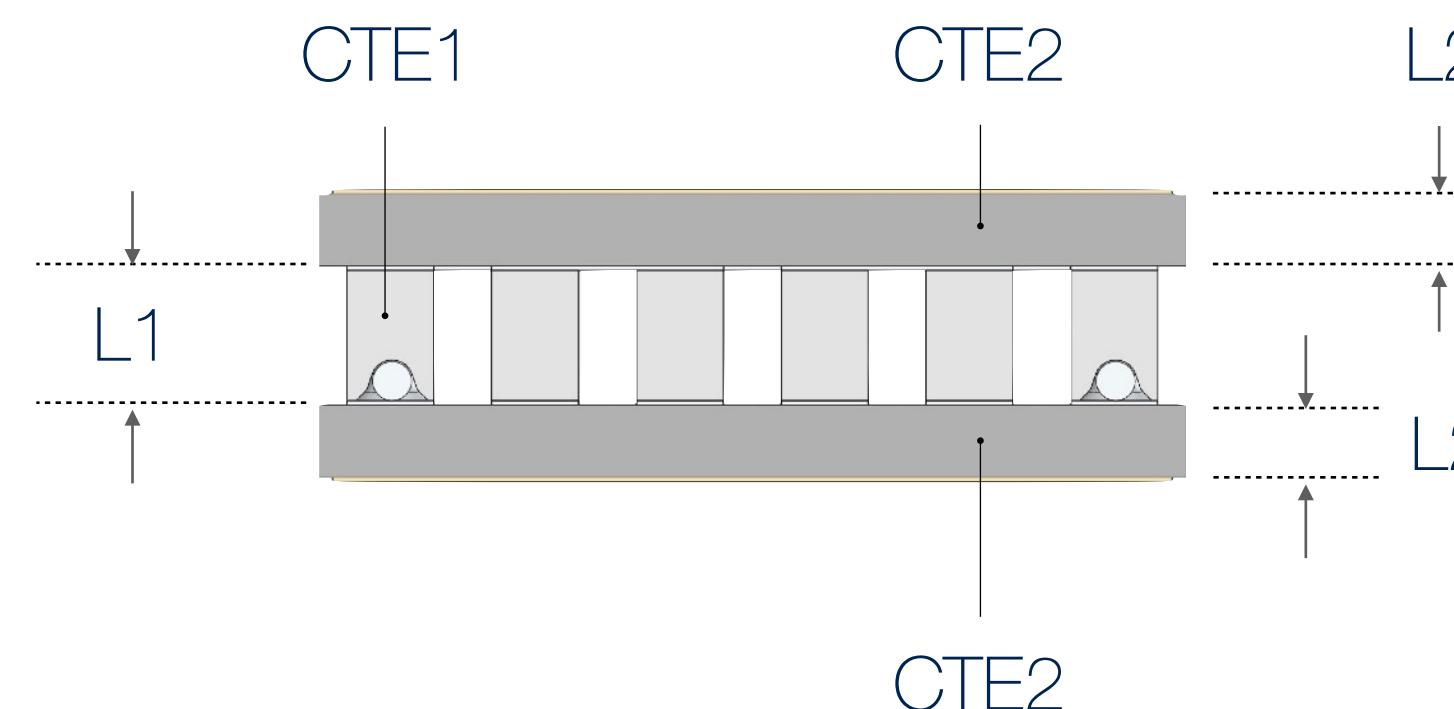
## Optical Axis alignments - TEC Height changes depending on Ambient Temperature

$$dT_{amb} = T_{amb2} - T_{amb1}$$



$$dH = H2 - H1$$

$$dH = (N \times L1 \times CTE1 + M \times L2 \times CTE2) * dT_{amb}$$



N - number of TEC stages

M - number of Ceramics plates

$L1$  - BiTe pellets Height

$L2$  - Ceramics thickness

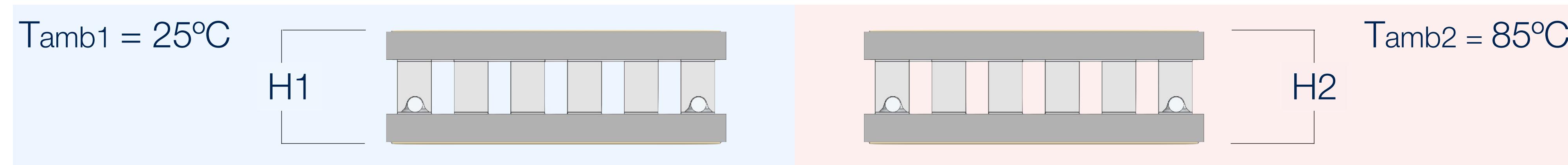
$CTE1$  - BiTe Coefficient of Thermal Expansion

$CTE2$  - Ceramics Coefficient of Thermal Expansion



## Optical Axis alignments - TEC Height changes, Example

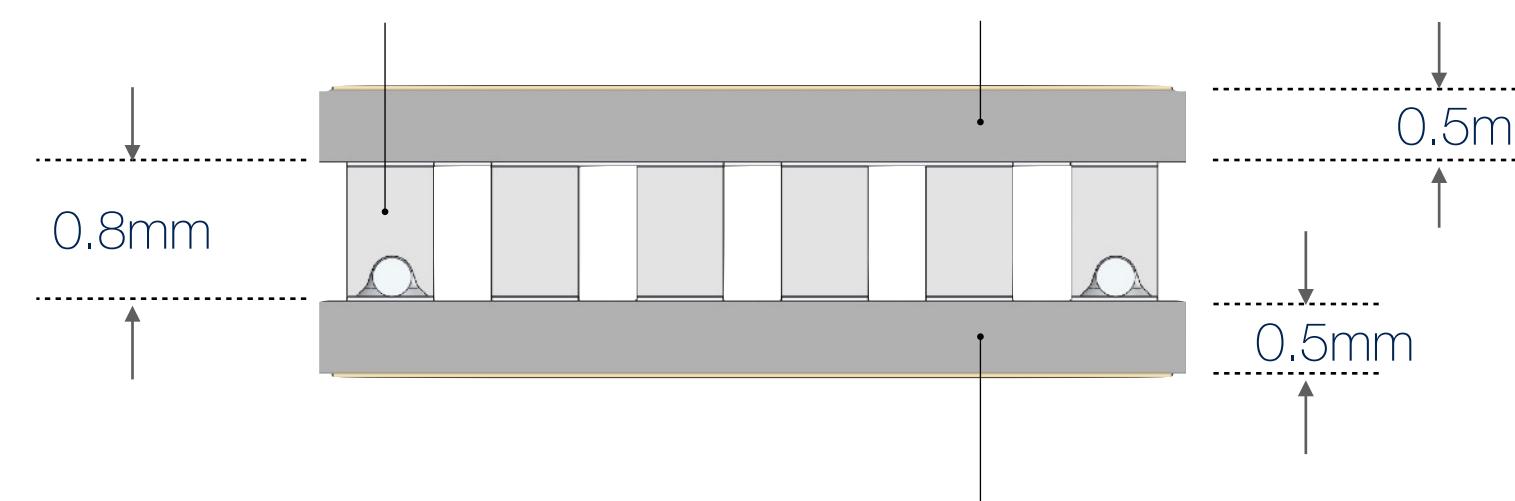
$$dT_{amb} = T_{amb2} - T_{amb1} = 60^{\circ}C$$



$$dH = H_2 - H_1$$

$$dH = (1 \times 0.8 \times 12.9 \times 10^{-6} + 2 \times 0.5 \times 7.2 \times 10^{-6}) \times 60 = 0.00105mm = 1.05\mu m$$

$$BiTe CTE1 = 12.9 \times 10^{-6} 1/K$$



$$Al_2O_3 CTE = 7.2 \times 10^{-6} 1/K$$

N=1- number of TEC stages

M=2- number of Ceramics plates

L1=0.8mm - BiTe pellets Height

L2=0.5mm- Ceramics thickness

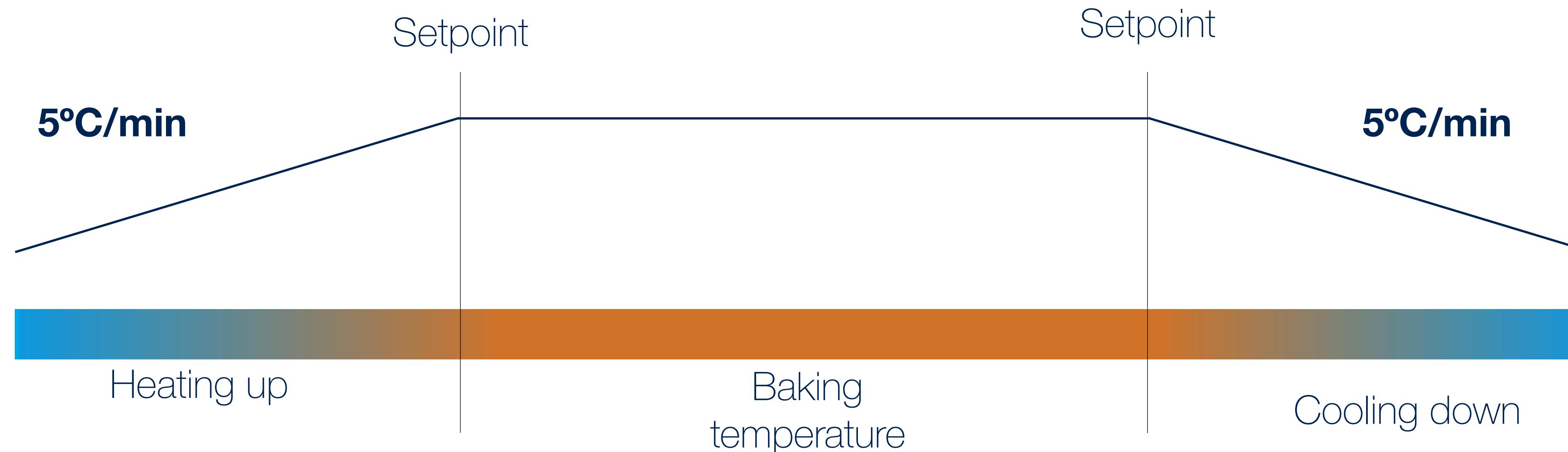
CTE1 - BiTe Coefficient of Thermal Expansion

CTE2 - Al<sub>2</sub>O<sub>3</sub> Coefficient of Thermal Expansion



## TE Coolers Baking process in case of Epoxy Gluing

1. Silver Epoxy and similar solutions are very common for TECs mounting.
2. Epoxy mounting method usually requires curing at high temperature.
3. Typical curing process can be made at +125°C...+150°C for several hours

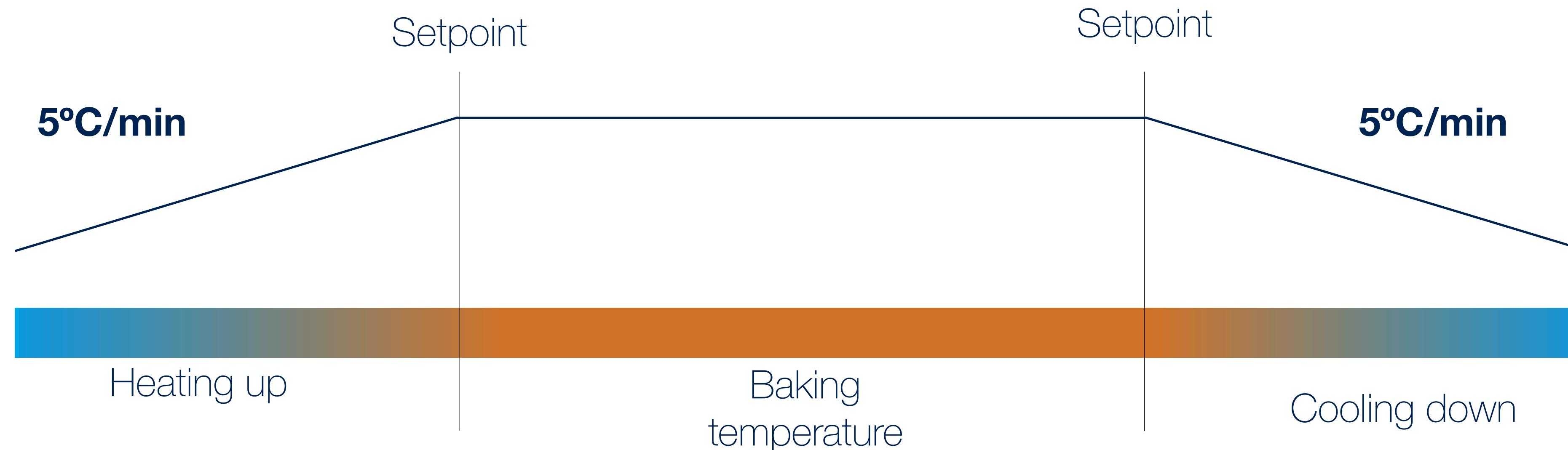


**Important:** Curing process to be with temperature ramping at heating up and cooling down stages to avoid thermal shock. The recommended rate is 5°C per minute during heating up and cooling down.



## TE Coolers in UHV applications

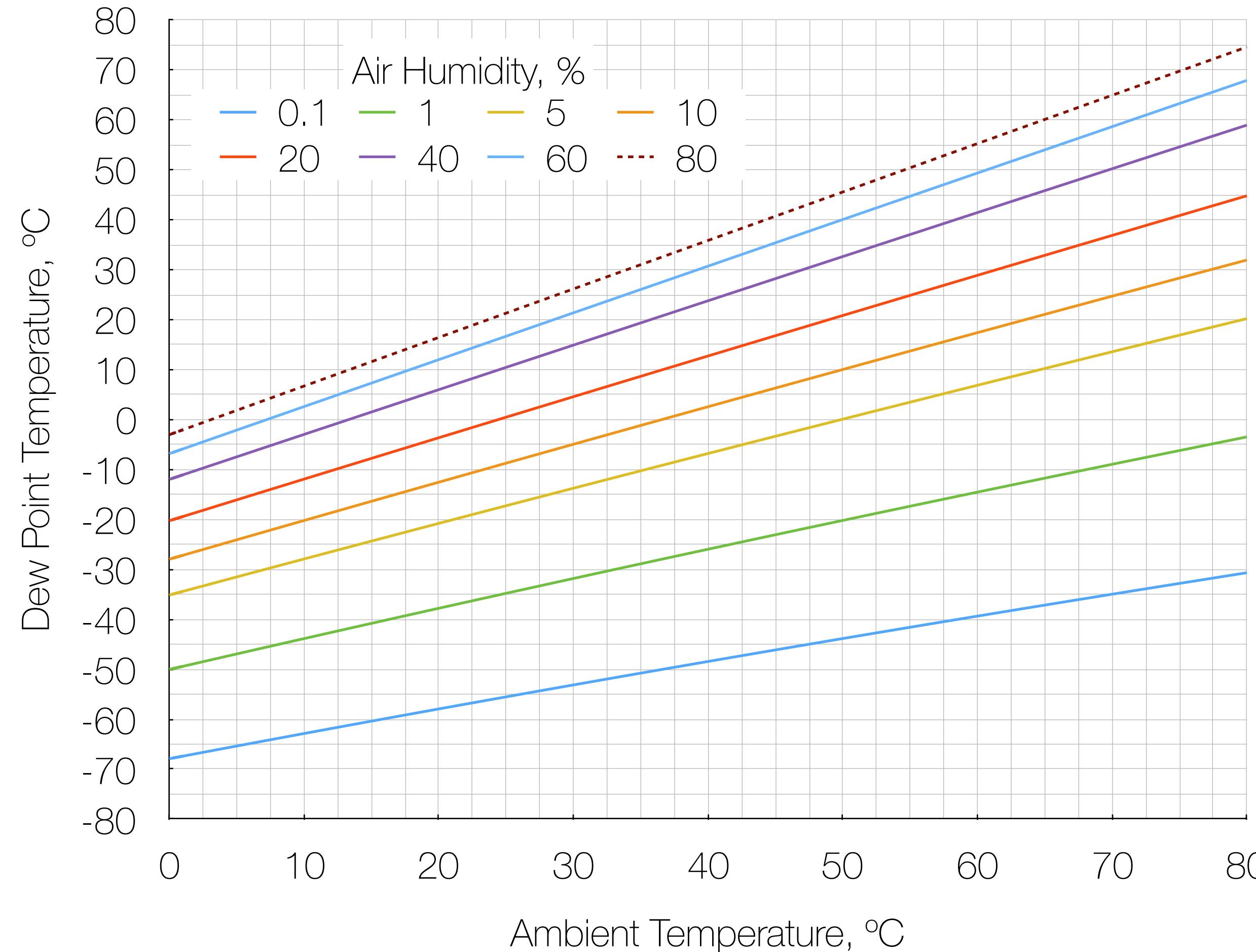
1. All TEC Microsystems TECs are Flux-Free and suitable for vacuum and UHV applications.
2. TE Coolers require baking (annealing) before final assembly in vacuum application.
3. Typical baking process is made at +125°C...+150°C for several hours



**Important:** Baking (annealing) process must be applied with temperature ramping to avoid thermal shock. The recommended temperature change rate is max 5°C per minute during heating up and cooling down.



## Ambience Humidity and Dew Point Risks



Dew Point  $T_d$  at relative humidity RH and the actual temperature  $T$  of Air is estimated as:

$$T_d = \frac{237.7 \times Y(T, RH)}{17.27 - Y(T, RH)}$$

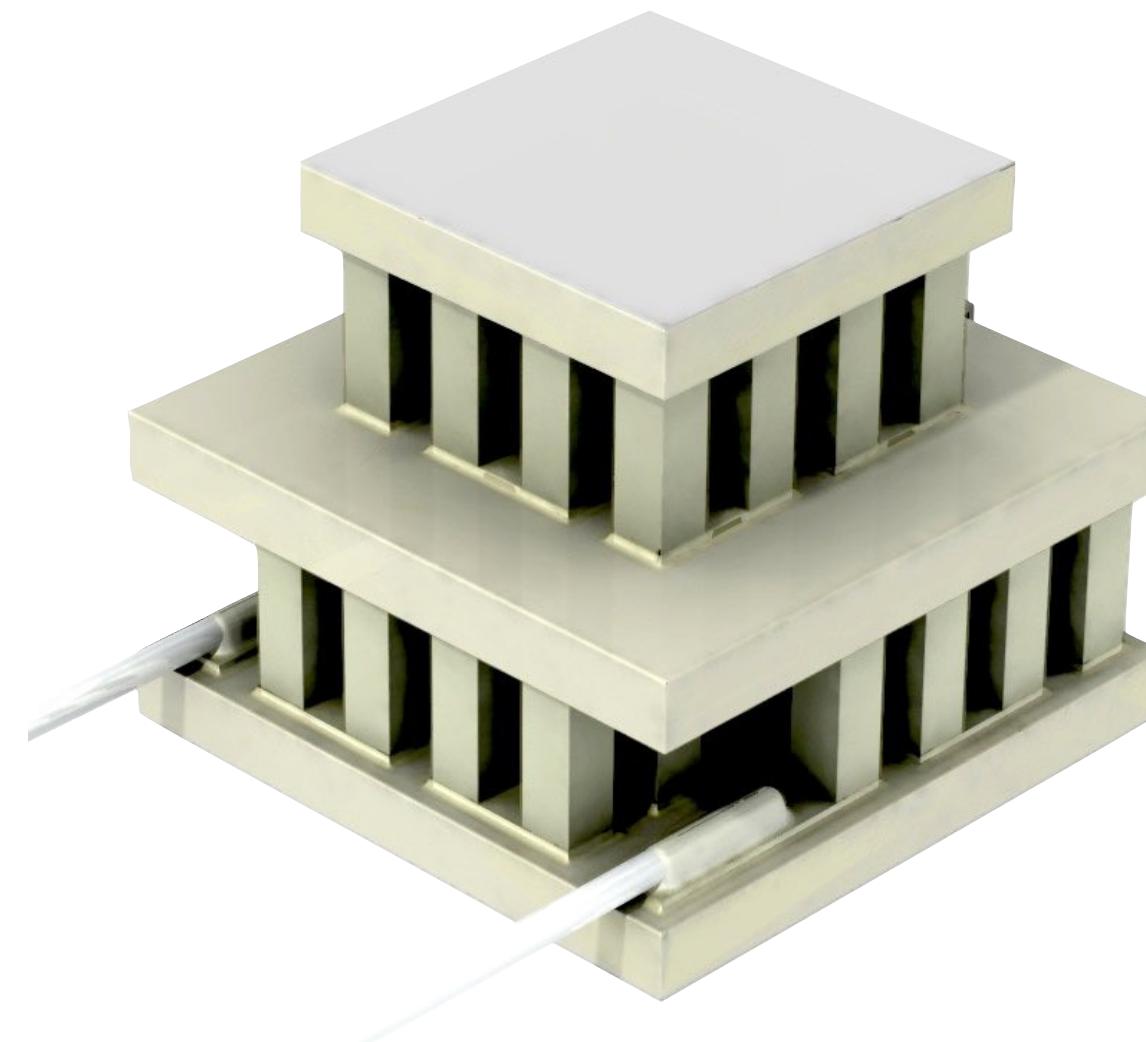
$$Y(T, RH) = \frac{17.27 \times T}{237.7 + T} + \ln \left( \frac{RH}{100} \right)$$

**Important:** Water condensation creates significant risks for TEC normal operating. To prevent water condensation filling gas must be dry and have Dew Point lower than required cooling temperature.



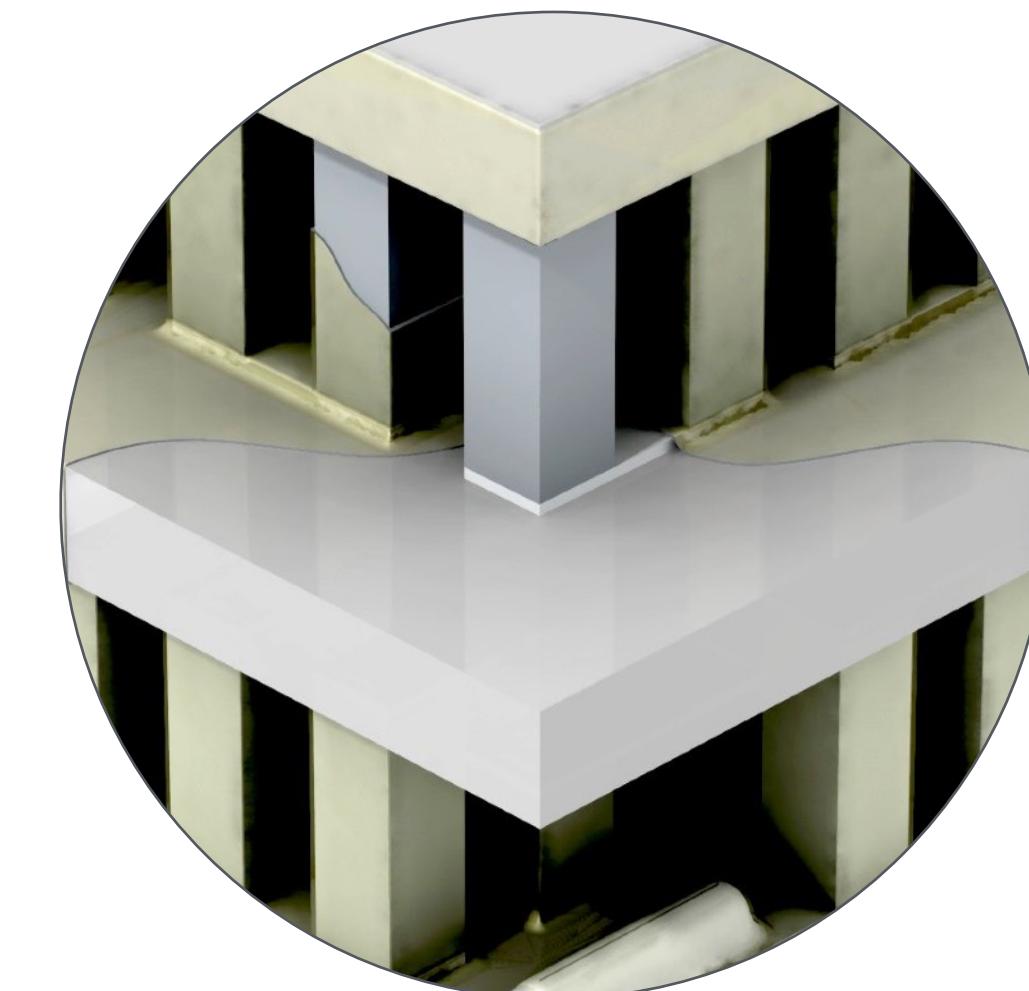
## TEC Advanced 3M™ Protective Coating against wet Ambience

TEC Protective Coating



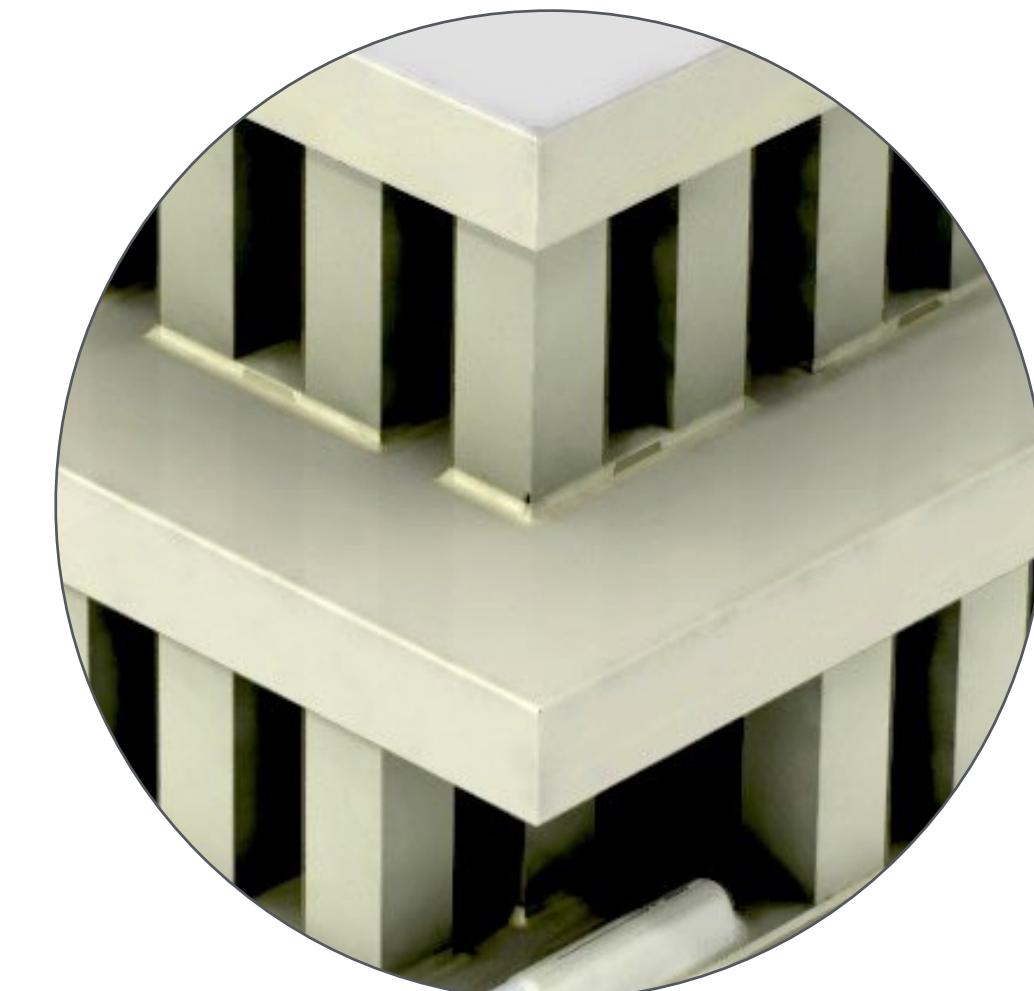
Withstand up to 200°C during  
mounting (short time)

Ultra-thin 3-5um Layer



Doesn't affect TEC  
Performance

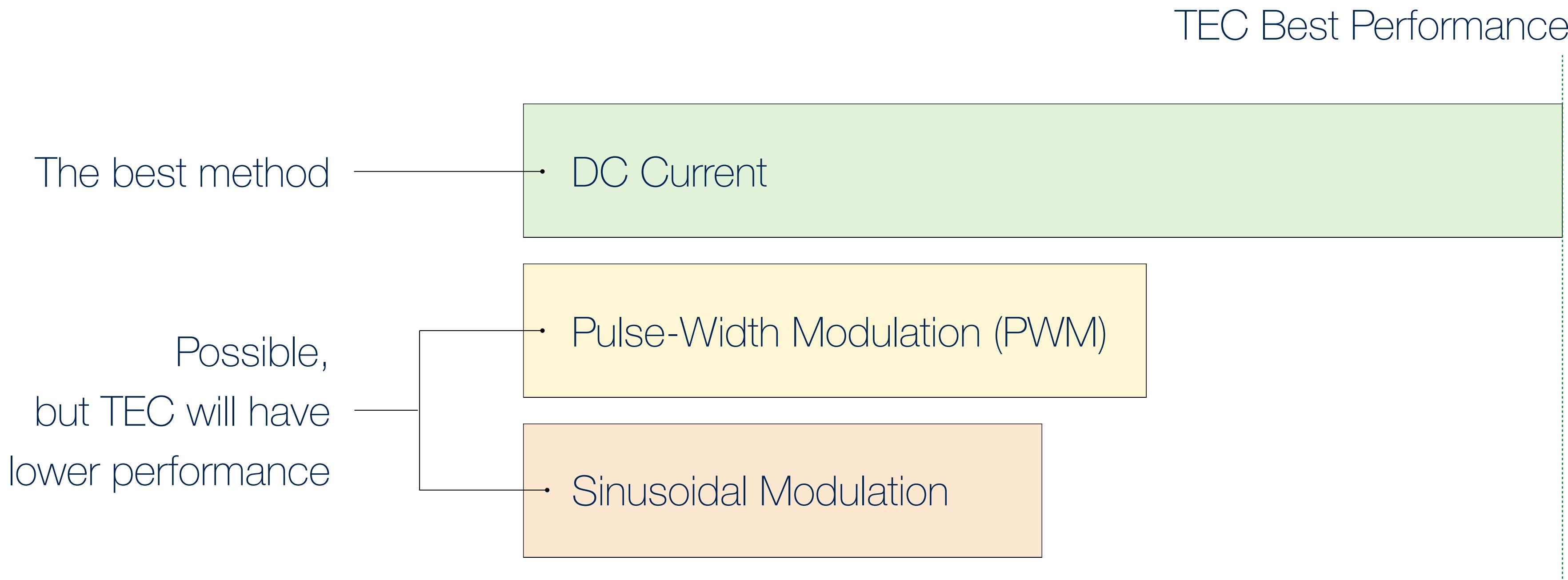
Covers all TEC inner surfaces



Protects TEC even being  
submerged in water



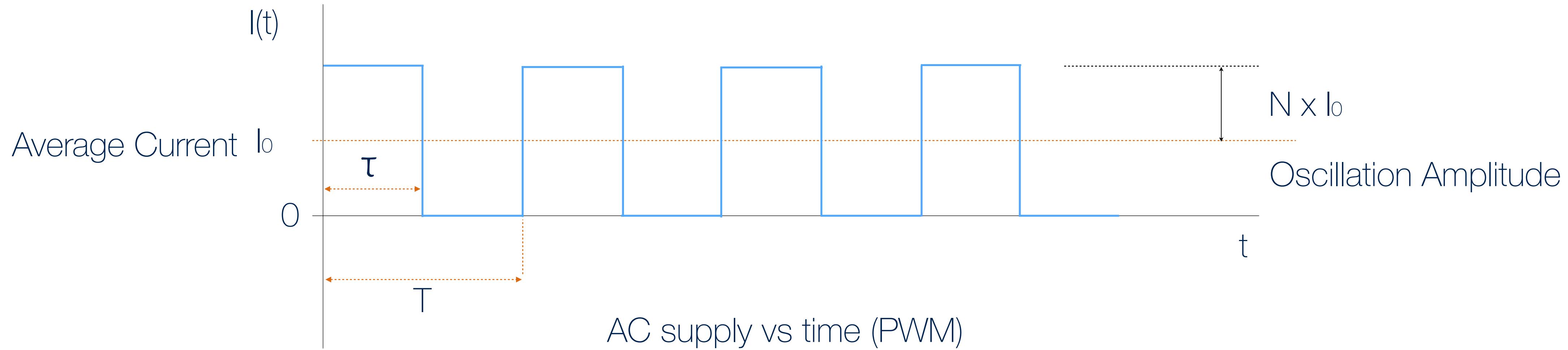
## TE Coolers Power Supply



TEC is DC regulated device. The best TEC performance is achieved with DC power supply.  
It's possible to use Sinusoidal modulation or PWM, but it will decrease TEC performance and efficiency.



## TEC Power Supply - Pulse-Width Modulation (PWM)



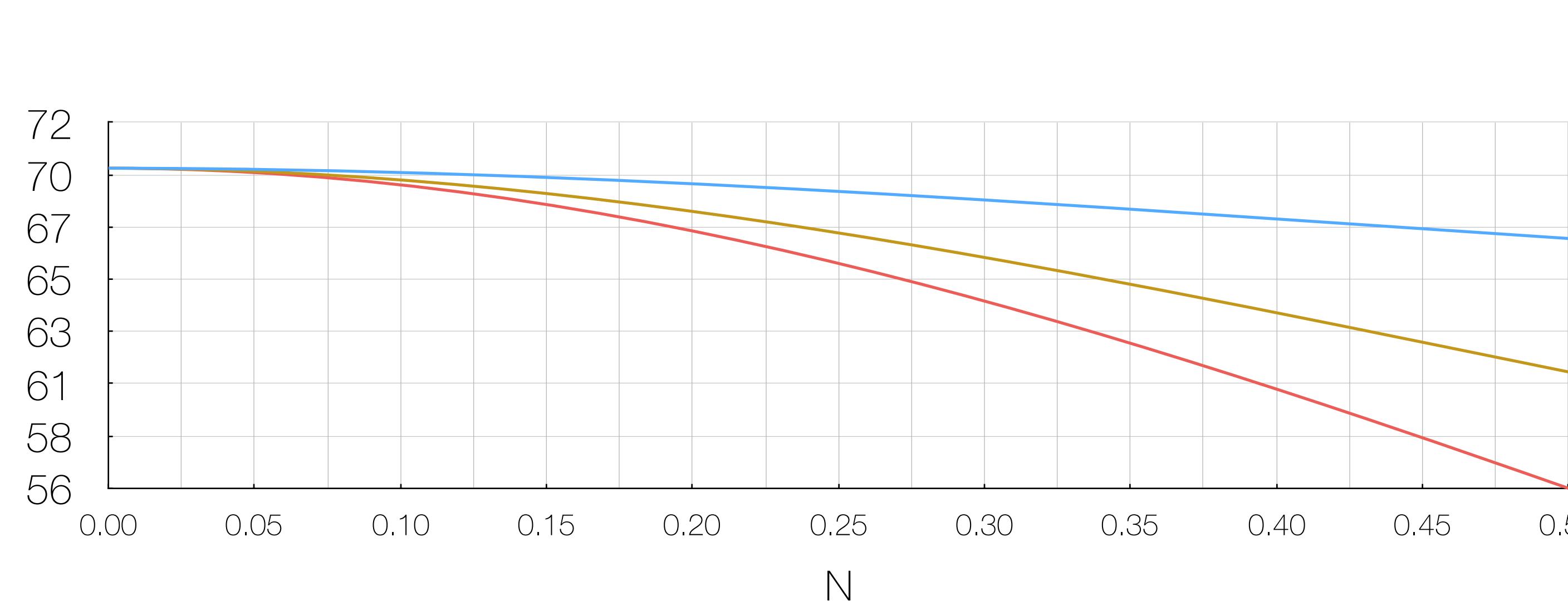
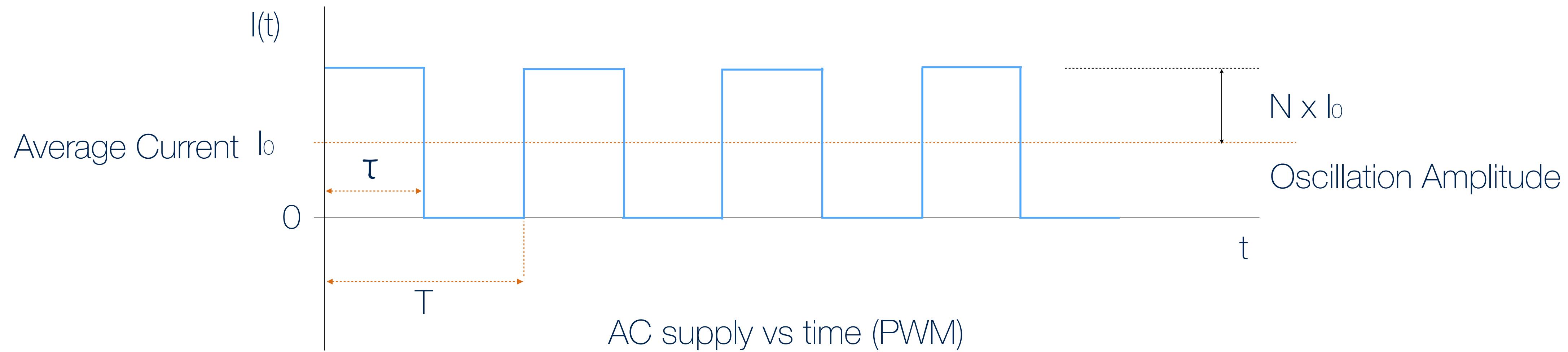
$$\text{Duty Cycle } Q = \frac{\tau}{T}$$

$$\frac{dT_{\max}(\text{PWM})}{dT_{\max}(\text{DC})} = \frac{(1 + N \times (2Q-1))^2}{1 + 2N \times (2Q-1) + N^2}$$

TEC is a DC current device. PWM reduces TE module efficiency. The reduction of  $dT_{\max}$  can be estimated by the formulas specified.



## Example - dTmax reduction at Pulse-Width Modulation (PWM)



$$Q = \frac{\tau}{T}$$

—  $Q=0.9$

—  $Q=0.7$

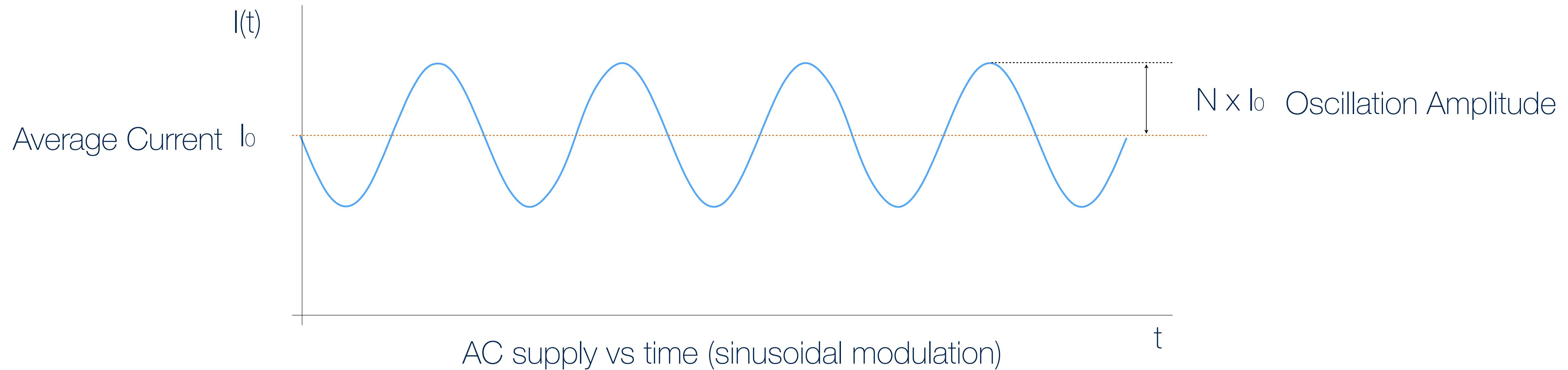
—  $Q=0.5$

Single-stage TEC  $dT_{max}$  reduction at PWM

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## TEC Power Supply - Sinusoidal Modulation

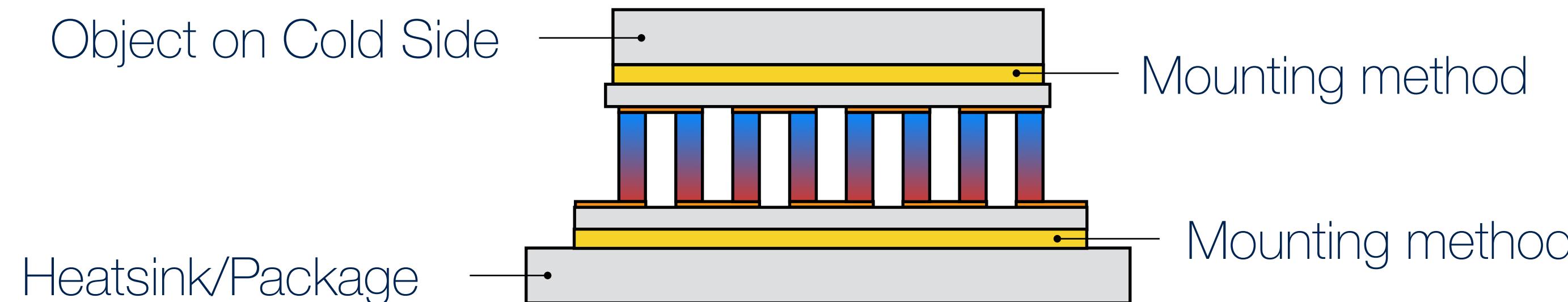


$$\frac{dT_{\max}(\text{DC})}{dT_{\max}(\text{AC})} = \frac{1}{1 + \frac{N^2}{2}}$$

TEC is a DC current device. AC current of any nature reduces TE module efficiency. The reduction of  $dT_{\max}$  can be estimated by the formula specified.



## Mounting Methods related to miniature TE Coolers



### Soldering

- Mechanical durability
- Thermal Conductivity
- No outgassing
- Requires technological skills and equipment
- Optimal for vacuum apps

### Gluing

- Easy to implement
- Requires annealing process
- May have thermal conductivity issues
- Requires an appropriate glue for application

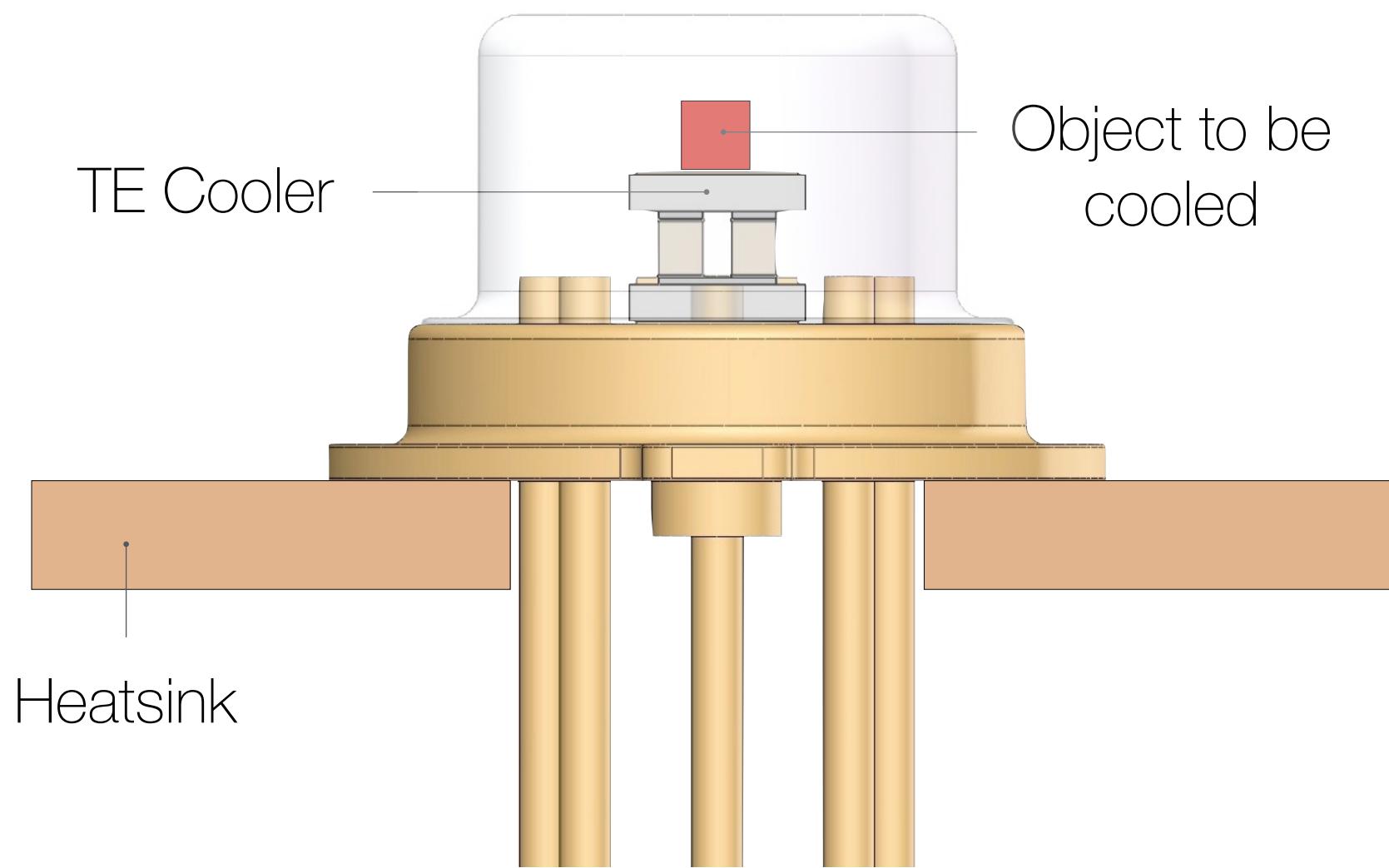
### Mechanical mounting

- Used usually for large TE Coolers mounting
- Requires thermal grease for best results
- Not suitable for very small TE Coolers



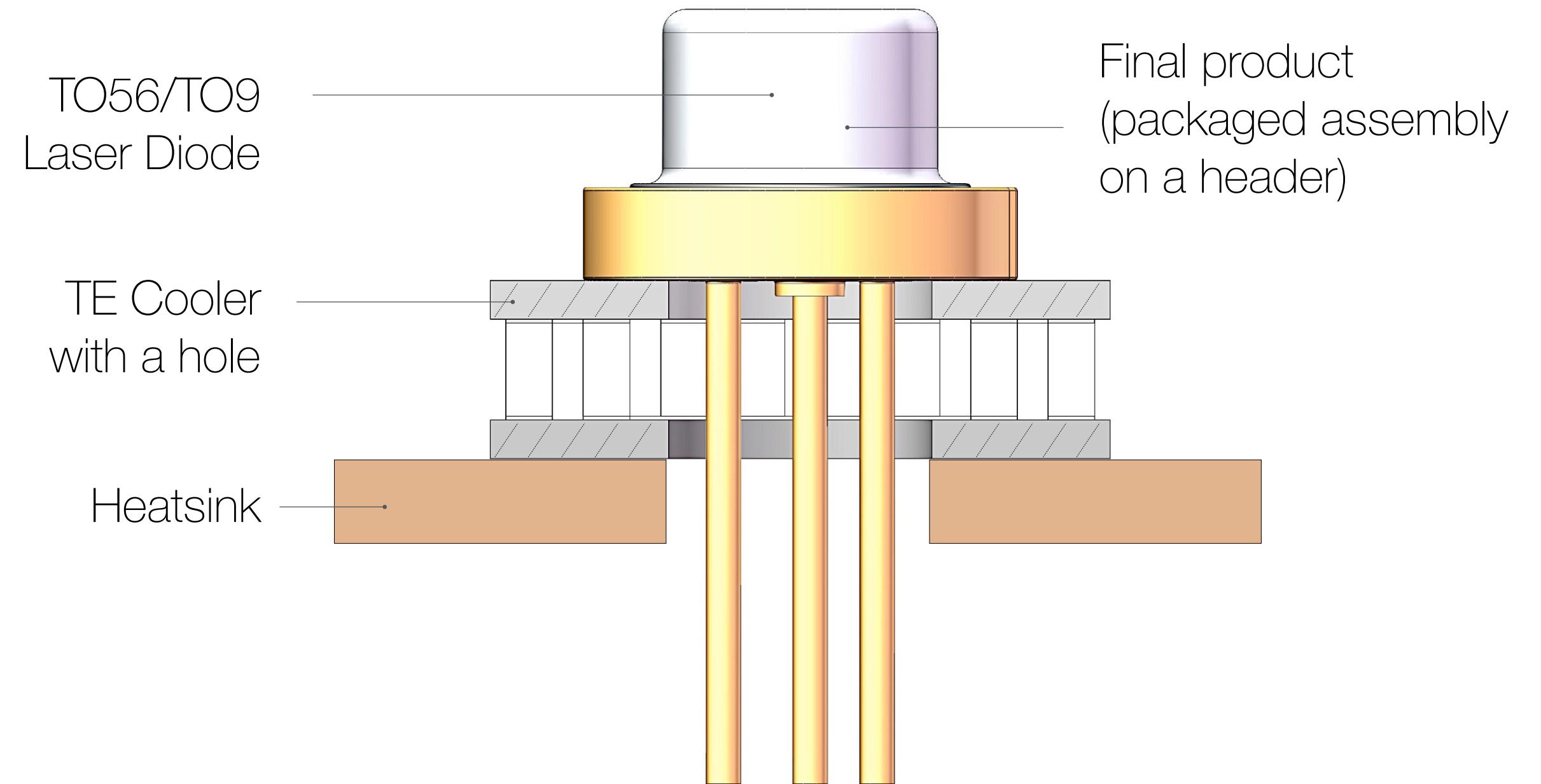
## “External” and “Internal” Cooling Methods with TECs

“Internal” Cooling



TEC directly controls the temperature of the object to be cooled

“External” Cooling

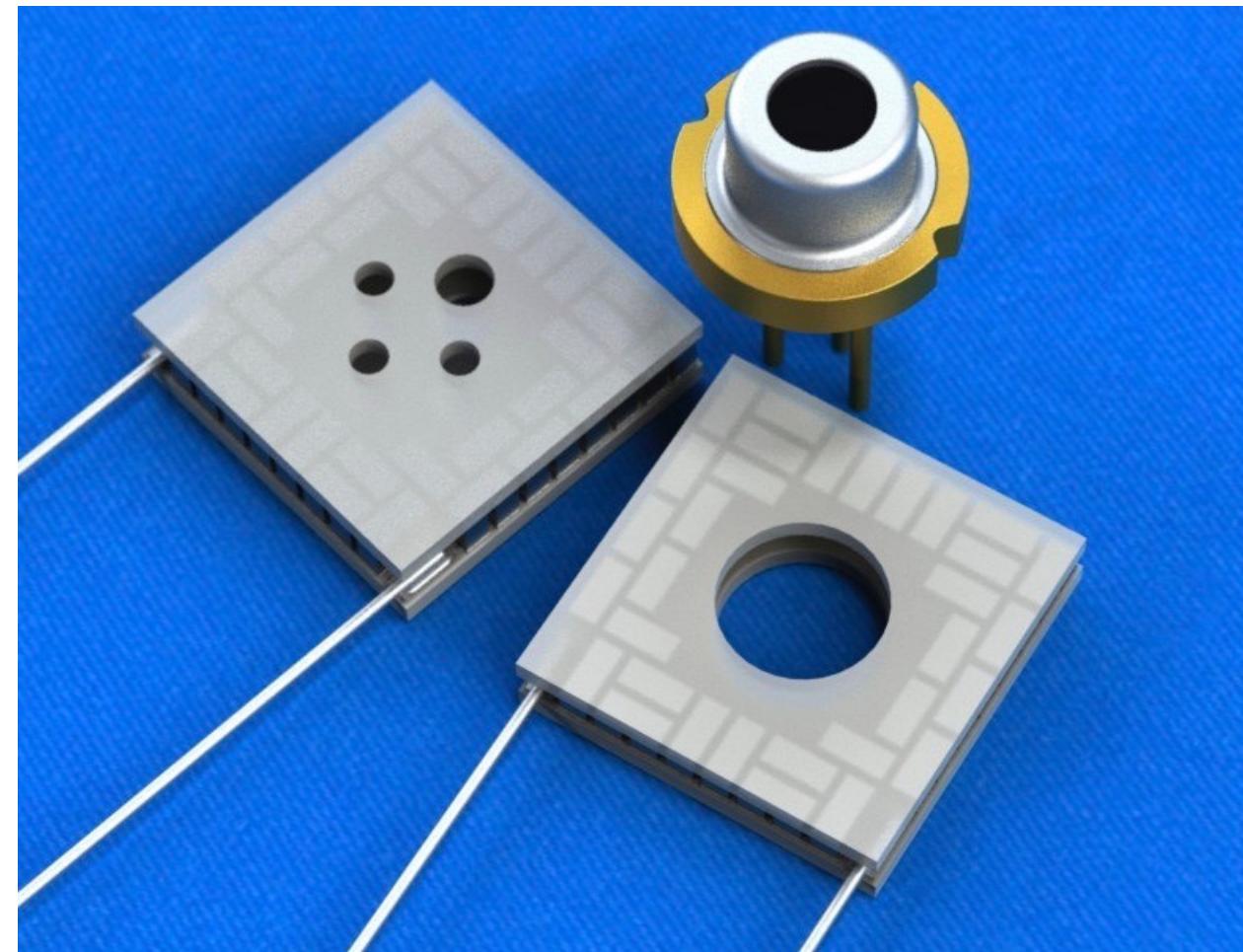


TEC controls the temperature of an assembly with the object to be cooled

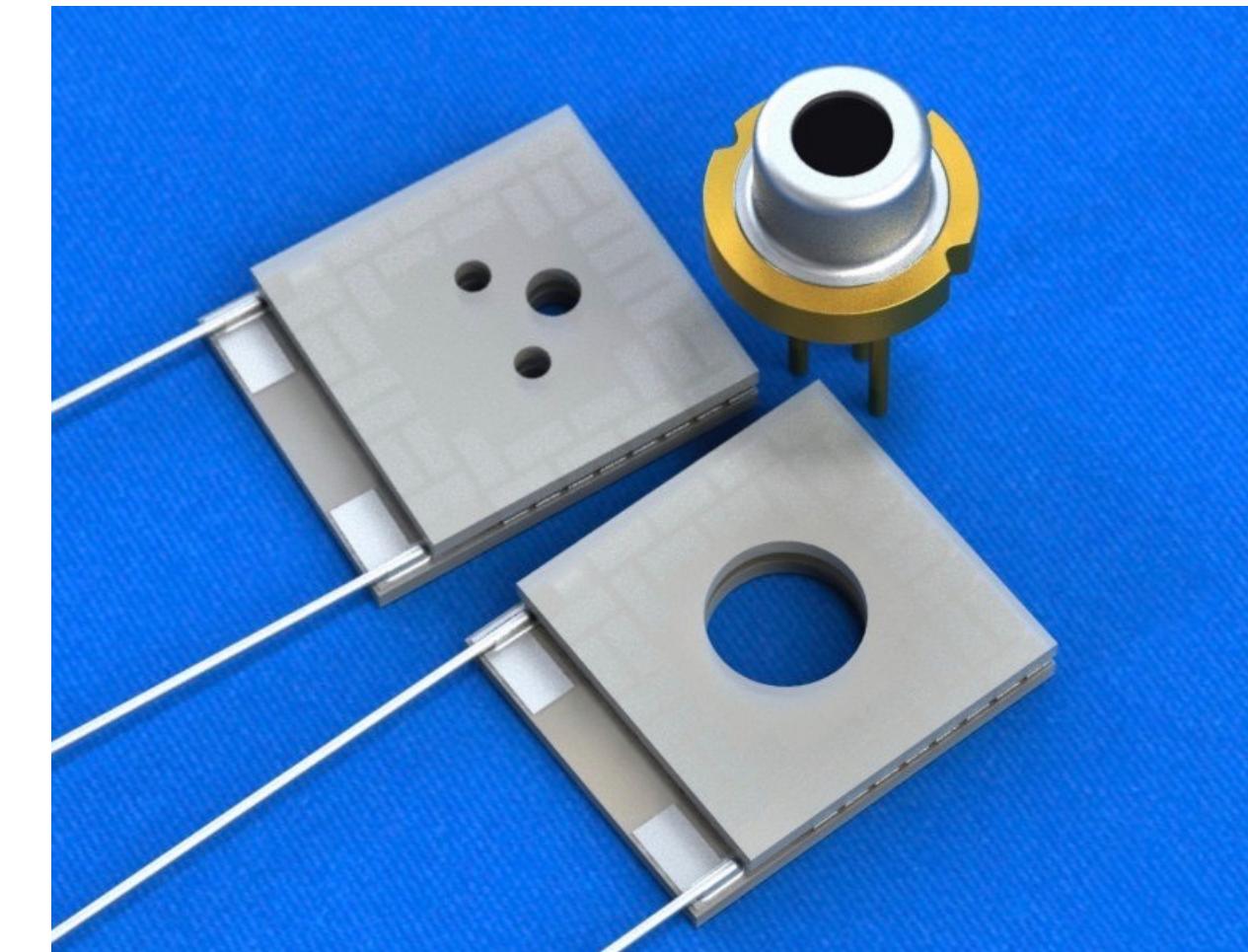
“External” cooling method can be applied, if there is no space (or possibility) to integrate TEC in assembly



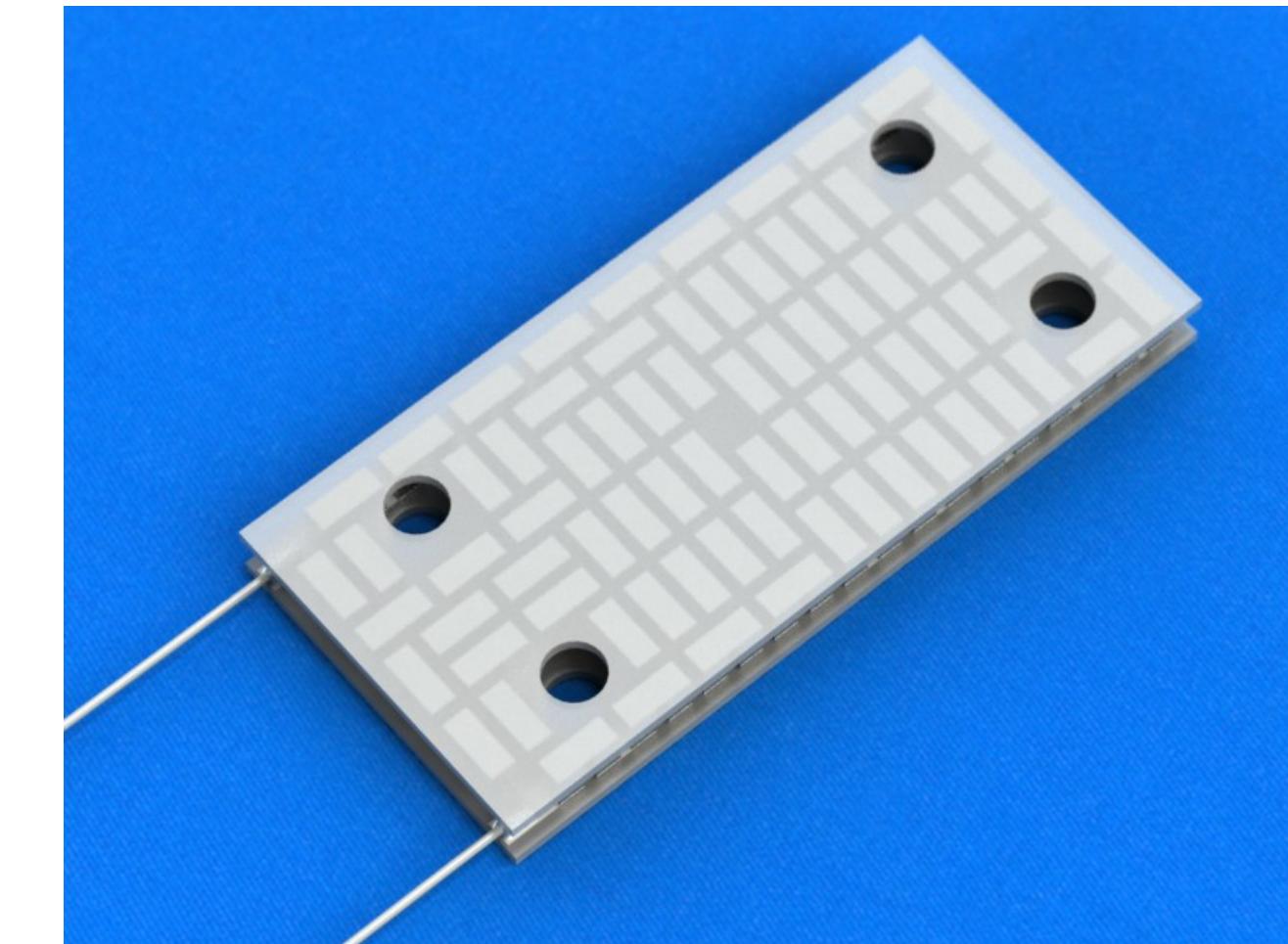
## Thermoelectric Coolers with Holes for “External” Cooling



Single- and Multi-Hole layouts  
for standard TO-56 and TO-9  
LD types



Low-height, High-Power  
TE Cooling solutions

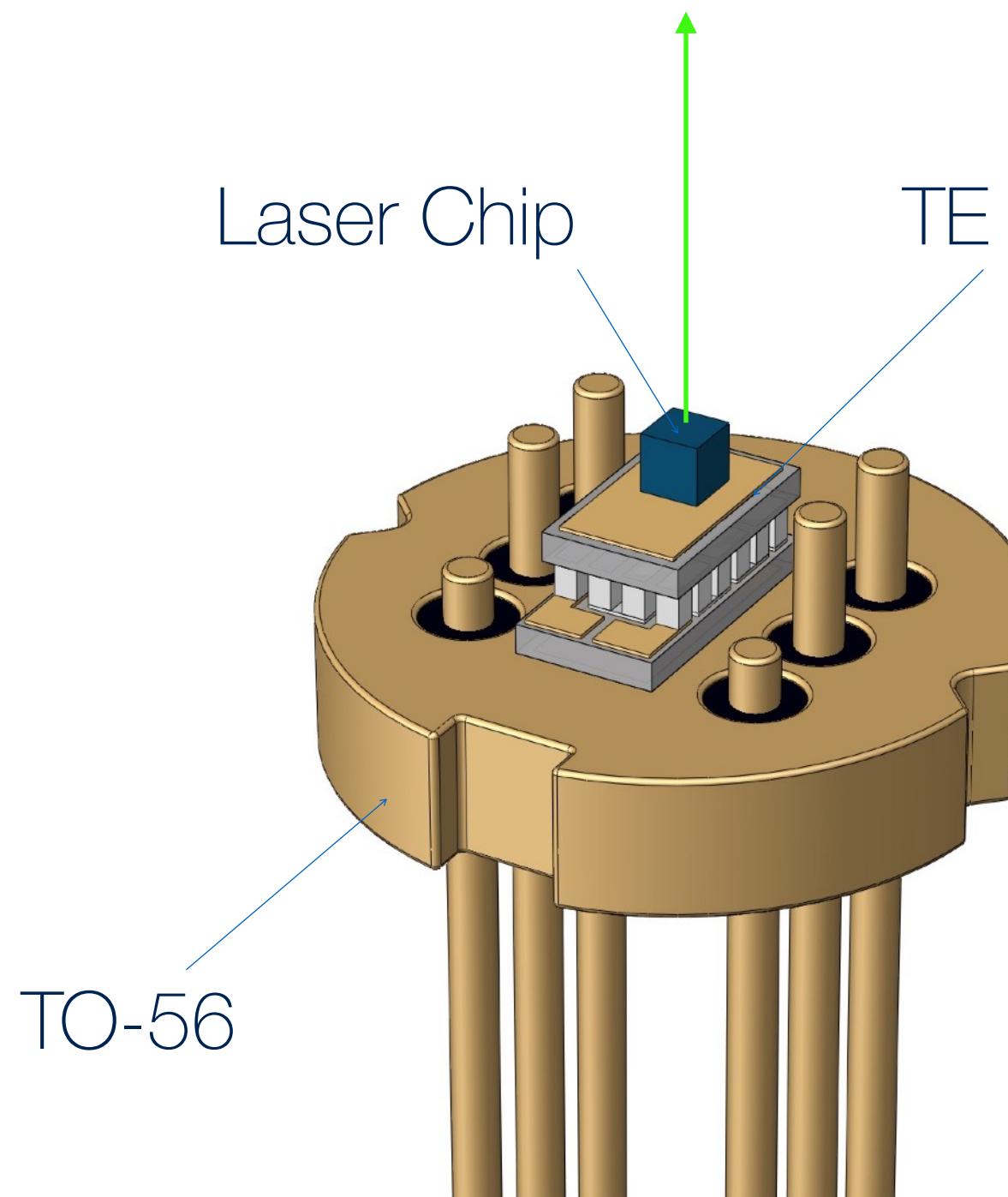


Development of customized  
TEC types

TEC Microsystems provides a wide range of TE Coolers with holes for external cooling.

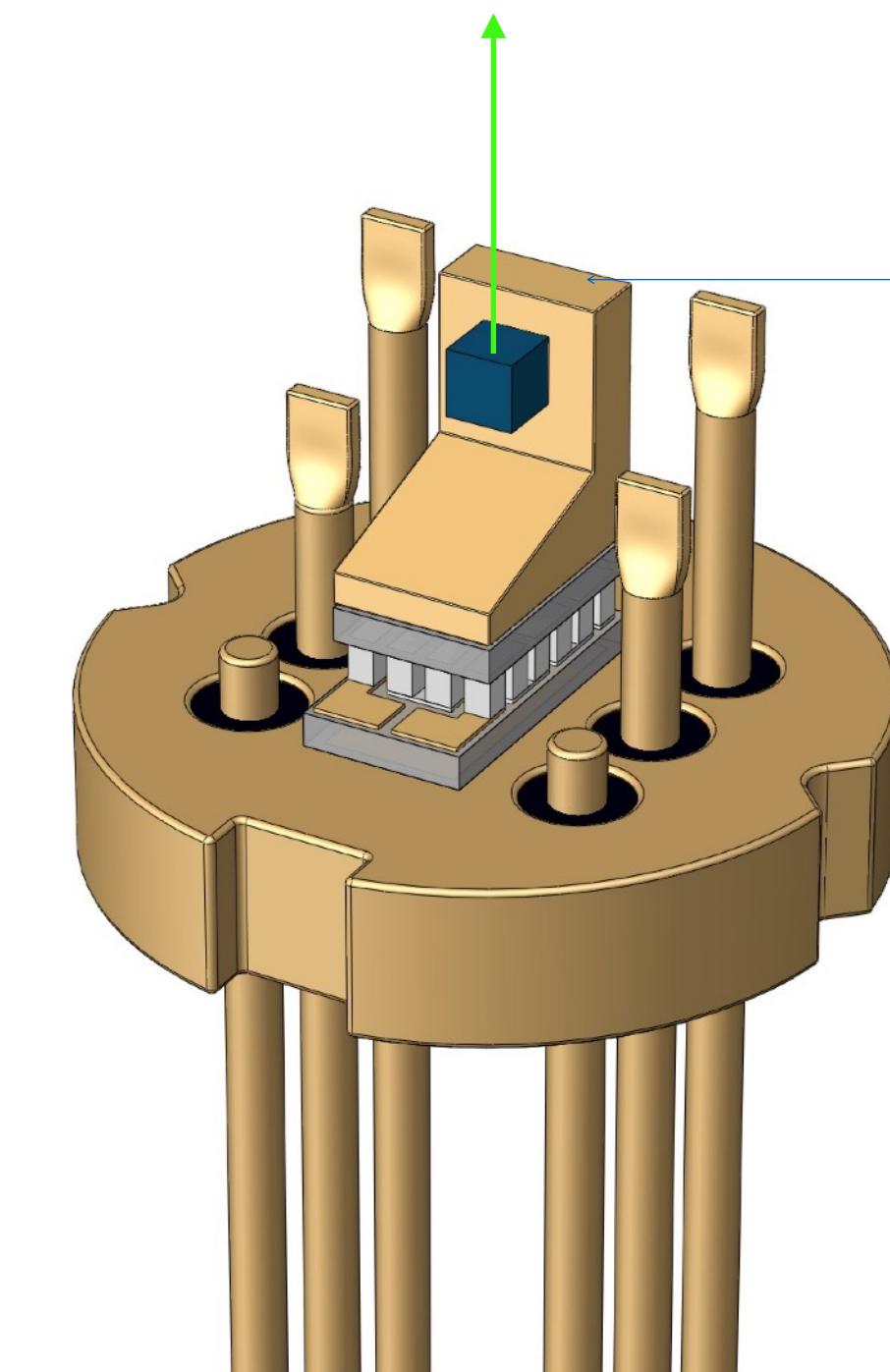


## Miniature TEC Integrating on TO-56 and similar Headers



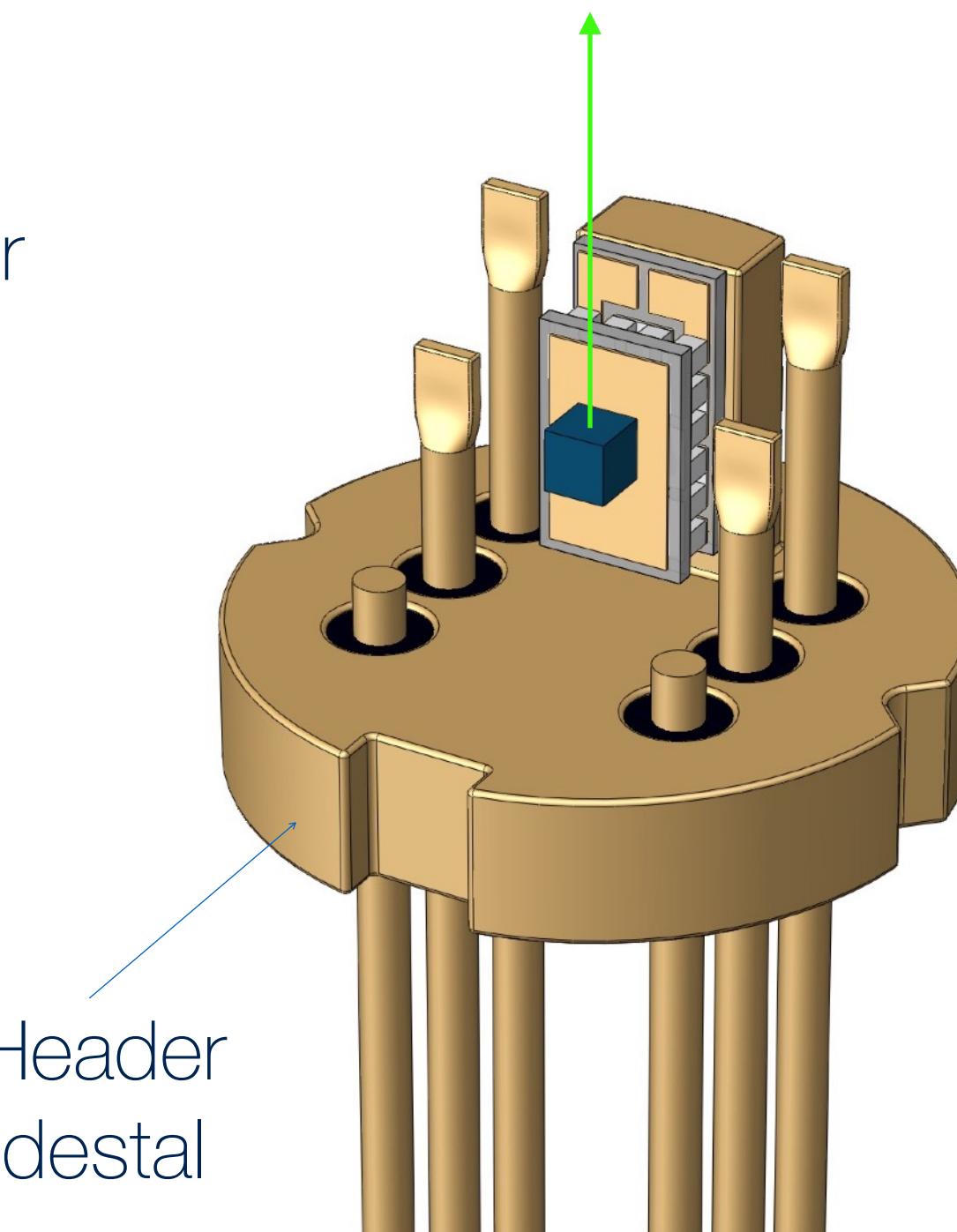
TO-56

“Horizontal TEC integration”  
for top-emitting LD



LD Holder

“Horizontal TEC integration” with  
holder on cold side for  
edge-emitting LD



TO-56 Header  
with Pedestal

“Vertical TEC integration”  
on Header optimized  
for edge-emitting LD

TEC Microsystems provides ultra-small TECs and value-added services for integration in cooled LD TO-can applications



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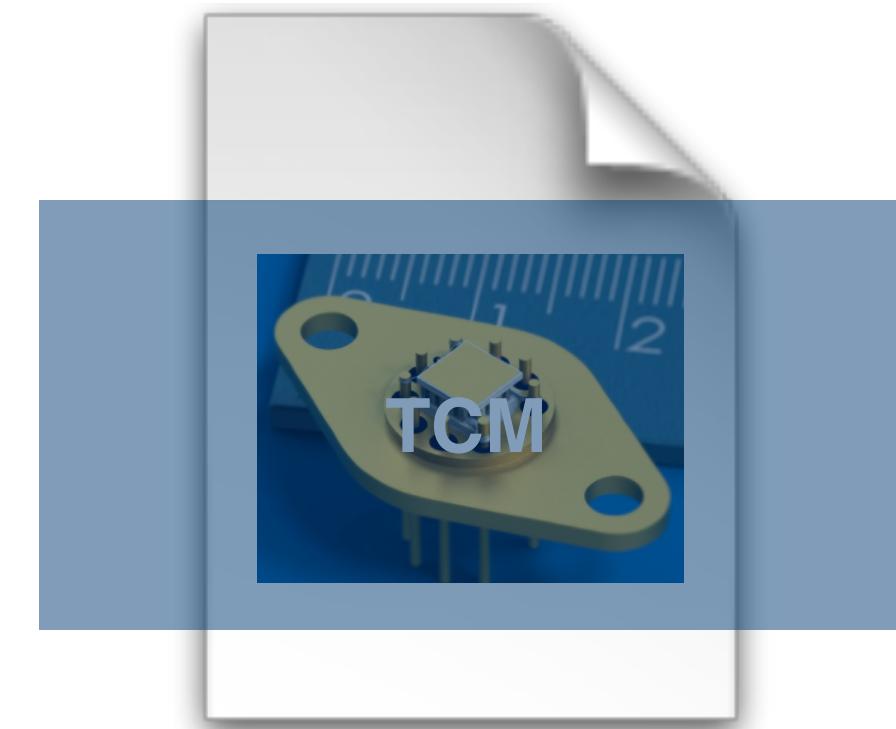
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