Problems: Passband Modulation

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1. Passband conversion in time-domain. Suppose that the complex baseband signal in time-domain is

$$u(t) = (a+bj)e^{-\alpha t}, \quad t \ge 0,$$

where a, b, α are real.

- (a) What at the I and Q components?
- (b) What is the real passband signal after upconversion with a carrier frequency f_c ?
- 2. Passband conversion in frequency domain. Let u(t) be a complex baseband signal with the real and imaginary parts of the spectrum (Fourier Transform) shown in Fig. 1. The constants are $f_0 = 5$ MHz, $f_1 = 10$ MHz, A = 8 and B = 10.

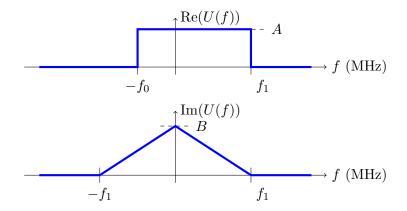


Figure 1: Real and imaginary parts of complex baseband signal U(f)

- (a) Suppose that we create a real passband signal $u_p(t) = \text{Re}(u(t)e^{2\pi i f_c t})$ for a carrier frequency $f_c = 800$ MHz. Draw the spectrum of $U_p(f)$. Show both the real and imaginary parts and show both the positive and negative frequencies.
- (b) Is u(t) an energy signal or power signal? What is its energy or power (in linear scale)? Leave your answer in terms of A, B, f_0 and f_1 . You do not need to convert to dB scale.
- (c) A receiver attempts to downcovert the signal with a two step process:

$$v(t) = 2u(t)e^{-2\pi i f_c t}, \quad \hat{u}(t) = h_{LPF}(t) * v(t),$$

where $h_{LPF}(t)$ has a frequency response,

$$H_{LPF}(f) = \begin{cases} C & \text{if } |f| < f_{LPF} \\ 0 & \text{if } |f| \ge f_{LPF}. \end{cases}$$

For what values of C and f_{LPF} is $\hat{u} = u(t)$?

- 3. Baseband equivalent filter. Consider a communication system with three steps:
 - A complex baseband signal u(t) is upconverted $u_p(t) = \text{Re}(u(t)e^{2\pi i f_c t})$ for some f_c .
 - The real passband channel is passed through a linear filter,

$$\frac{dy_p(t)}{dt} = bu_p(t) - ay_p(t),$$

with constants a and b > 0.

- The received signal is downconverted, $v(t) = 2y_p(t)e^{-2\pi i f_c t}$ and $y(t) = h_{LPF}(t) * v(t)$ where $h_{LPF}(t)$ is an ideal low-pass filter.
- (a) What is the real passband frequency response, $H_p(f) = \frac{Y_p(f)}{U_p(f)}$?
- (b) What is the effective baseband frequency response $H(f) = \frac{Y(f)}{U(f)}$?
- (c) Find a_1 and b_1 such that

$$\frac{dy(t)}{dt} = b_1 x(t) - a_1 y(t).$$

- (d) Suppose that $2\pi f_c \gg a$, what is the power gain of H(0) in dB?
- 4. PSD and RX filtering. Suppose that a real passband signal has two components:

$$x(t) = x_0(t) + x_1(t),$$

where $x_0(t)$ is a desired signal, and $x_1(t)$ is an interfering signal. They have PSD $S_i(f) = A_i \operatorname{Rect}((f - f_i)/W_i)$, i = 0, 1 with parameters:

- Desired signal: $f_0 = 2.50$ GHz, $W_0 = 20$ MHz, total receive power $P_0 = -100$ dBm.
- Interfering signal: $f_1 = 2.53$ GHz, $W_1 = 10$ MHz, total receive power $P_1 = -80$ dBm.
- (a) Find A_i from P_i using reasonable approximations. State the units of A_i .
- (b) Draw $S_0(f)$ and $S_1(f)$.
- (c) A signal is downconverted with mixing $v(t) = 2x(t)e^{2\pi i f_c t}$ and u(t) = h(t) * v(t). Find f_c and a filter magnitude response $|H(f)|^2$ such that:
 - The component from desired signal is centered at 0 and amplified to -60 dBm.
 - The component from interfering signal attenuated to below -110 dBm.

There is no single correct answer. Draw $|H(f)|^2$ and the PSD of u(t).

5. Circuit implementations. Fig. 2 shows the circuit schematic of the RF front-end a SiGe (silicon Germanium) bipolar transceiver presented in:

Floyd, Brian A., et al. "SiGe bipolar transceiver circuits operating at 60 GHz." *IEEE journal of solid-state circuits* 40.1 (2005): 156-167.

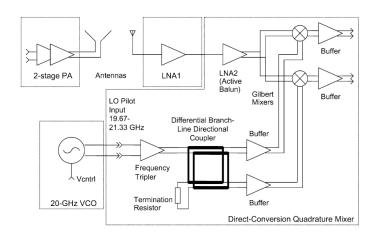


Figure 2: Schematic diagram of a SiGe RF front-end from Floyd, et. al, 2005.

Feel free to look up terms in the paper or any other source to answer the following questions:

- (a) Which block is the local oscillator?
- (b) What is the carrier frequency? Why?
- (c) What is the role of the "Differential branch line directional coupler"?
- (d) How is the frequency tuned?