# Path Planning Challenge

Magicc Lab, Summer 2023

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#### Abstract

Convex optimization challenge for summer 2023.

### 1 Introduction

The convex optimization challenge will use the VTOL example from [1], which is describe below for convenience.

In this design study we will explore the control design for a simplified planar version of a quadrotor following a ground target. In particular, we will constrain the dynamics to be in two a dimensional plane. In Cartesian space, the position of the VTOL can be defined by a variable describing the vertical position, one describing the horizontal position, and one angular variable describing the orientation, as shown in 1. The planar vertical take-off and landing (VTOL) system is comprised of a center pod of mass  $m_c$  and inertia  $J_c$ , a right motor/rotor that is modeled as a point mass  $m_r$  that exerts a force  $f_r$  at a distance d from the center of mass, and a left motor/rotor that is modeled as a point mass  $m_{\ell}$  that exerts a force  $f_{\ell}$  at a distance -d from the center of mass. The position of the center of mass of the planar VTOL system is given by horizontal position  $z_v$ and altitude h. The airflow through the rotor creates a change in the direction of flow of air and causes what is called "momentum drag." Momentum drag can be modeled as a viscous drag force that is proportional to the horizontal velocity  $\dot{z}_v$ . In other words, the drag force is  $F_{\rm drag} = -\mu \dot{z}_v$ . The target on the ground will be modeled as an object with position  $z_t$  and altitude h=0. We will not explicitly model the dynamics of the target.

Use the following physical parameters:  $m_c = 1$  kg,  $J_c = 0.0042$  kg m<sup>2</sup>,  $m_r = 0.25$  kg,  $m_\ell = 0.25$  kg, d = 0.3 m,  $\mu = 0.1$  kg/s, g = 9.81 m/s<sup>2</sup>.

## 2 Dynamics

The dynamics are given by

$$\begin{pmatrix} m_c + 2m_r & 0 & 0 \\ 0 & m_c + 2m_r & 0 \\ 0 & 0 & J_c + 2m_r d^2 \end{pmatrix} \begin{pmatrix} \ddot{z} \\ \ddot{h} \\ \ddot{\theta} \end{pmatrix} = \begin{pmatrix} -(f_r + f_\ell)\sin\theta - \mu\dot{z} \\ -(m_c + 2m_r)g + (f_r + f_\ell)\cos\theta \\ d(f_r - f_\ell) \end{pmatrix}.$$
(1)

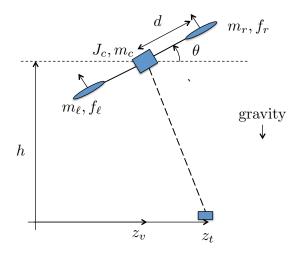


Figure 1: Planar vertical take-off and landing (VTOL)

We will assume that the right and left rotor forces are constrained as follows

$$0 \le f_r, f_\ell \le 0.75(m_c + 2m_r)g. \tag{2}$$

If the thrust was limited to  $0.5(m_c + 2m_r)g$ , then at full throttle, the VTOL could just hover. Therefore, the limit allows some additional control authority, but is somewhat constraining.

# 3 Trajectory Following

We will assume that a state-space controller with integrator is designed for the system as described in Chapter 12 of [1], and that a disturbance observer is used to estimate the states as described in Chapter 14 of [1]. The input to the system is the desired forward position  $z^r(t)$  and the desired altitude  $h^r(t)$ .

## References

 R. W. Beard, T. W. McLain, C. Peterson, and M. Killpack, Introduction to Feedback Control Using Design Studies. Amazon, 2016.