

POWER ELECTRONICS
B.E., VII Semester, Electronics & Communication Engineering
[As per Choice Based Credit System (CBCS) Scheme]
Course Code 17EC73 CIE Marks 40

Number of Lecture Hours/Week: 04	SEE Marks 60
Total Number of Lecture Hours: 50 (10 Hours / Module)	Exam Hours 03
	CREDITS – 04

RNS INSTITUTE OF TECHNOLOGY
DEPARTMENT OF ELECTRONICS AND COMMUNICATION
POWER ELECTRONICS NOTES:

MODULE-1

Course Objectives:

- understand the Construction and working of various power devices
- Study and analysis of thyristor circuits with different triggering Conditions
- Learn the applications of power devices in Controlled rectifiers, Converters and inverters.
- Study of power electronics circuits under various load conditions.

COURSE OUTCOMES

- Describe the characteristics of different power devices and identify the various applications associated with it.

- Illustrate the working of power circuit as DC-DC Converter

- Illustrate the operation of inverter

circuit and static switches.

- Determine the output response of a thyristor circuit with various triggering options

- Determine the response of controlled rectifier with resistive and inductive loads.

~~SEM 2~~

MODULE - 1

P-3

TOT: 10 Hrs.

SYLLABUS

SL NO.	HEADING	TEXT CH.	REMARKS
01.	INTRODUCTION: Applications of PE	T-1; 1.1	Theory Que.
02.	Power Semiconductor Devices	T-1 1.2	OLD syllab Unit-1
03.	Control Ch of Power Devices	T-1 1.3	
04.	Types of PE circuits	T-1 1.5	
05.	Peripheral effects	T-1 1.8	
06.	Power Transistor & Power BJT	T-1 4.1 4.2	UNI.
07.	Steady State ch.	T-1 4.2.1	Theory Derivati
08.	Power MOSFETs Device operation	T-1 4.3 T-1 4.3.1	prob. OLD syllab
09.	Switching Ch.	T-1 4.3.2	Unit-2
10.	IGBTs Device operation o/p & Transfer ch.	T-1 4.6	
11.	d/dt & dv/dt limitation	T-1 4.8	

Slipper

11

INTRODUCTION

Definition :

Power = Voltage * Current , in Watts

Energy = Power * Time : in Whrs.

Power Electronic :

The applications of Solid State electronics for the Control and Conversion of electric power.

Power deals with static & rotating power equipment for Generation ; Transmission and distribution.

Electronics deals with Solid State devices and Circuits for Signal processing to meet the desired control objectives.

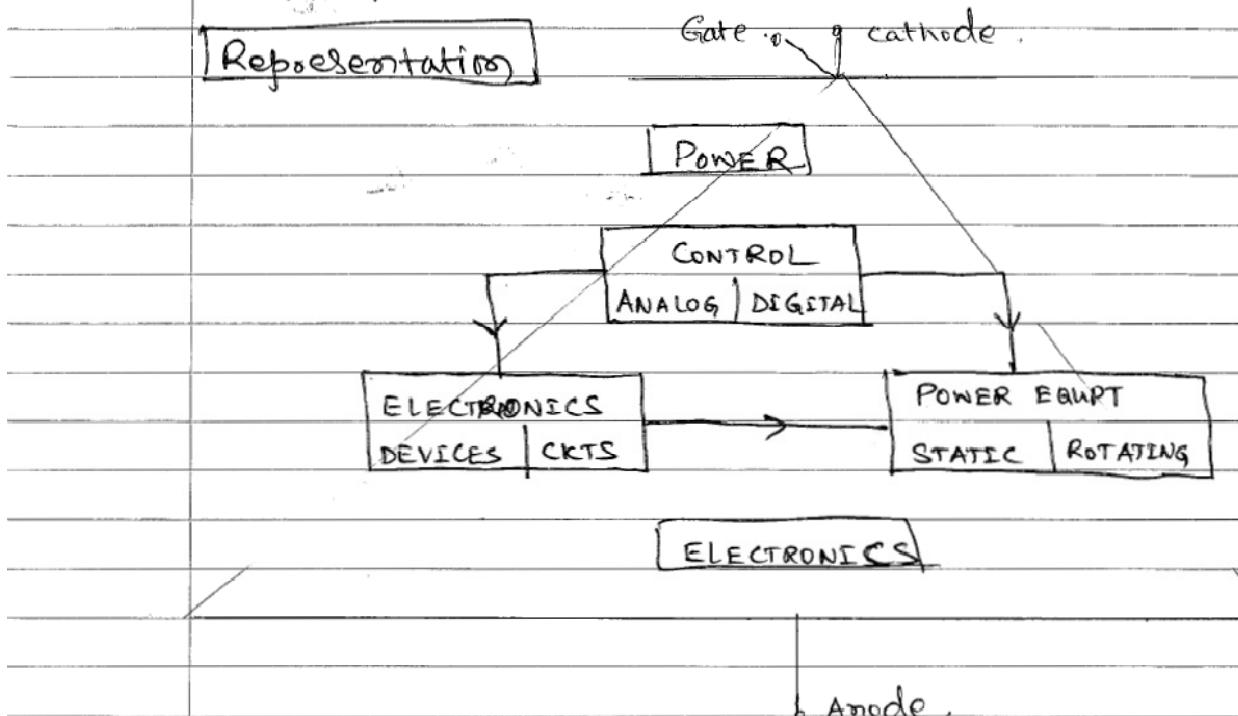
IEEE PE Society definition of Power Electronic

" Power electronic encompassed the use of electronic devices, the application of circuit theory and design techniques and the development of analytical tools towards efficient electronic conversion, control and conditioning of electric power.

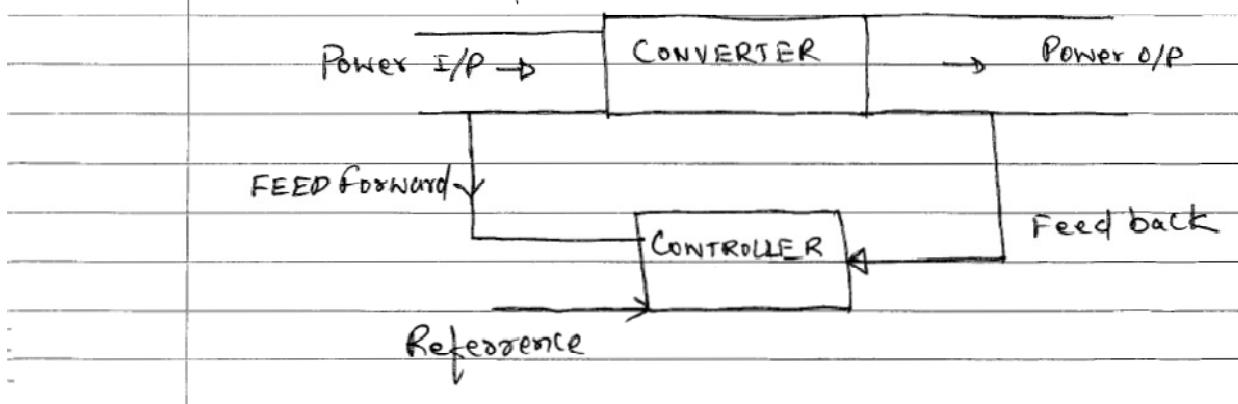
~~Block 3~~

Simpler definition:

"use of electronics for the control of large power" is known as Power Electronics



BLOCK DIAGRAM OF A POWER PROCESSOR :



APPLICATIONS OF PE.

COMMERCIAL

1. Air Con
2. Central refrigeration
3. UPS
4. Elevators
5. Emergency Lamp
6. Heating Sys

DOMESTIC

1. Cooking equipmt
2. Lighting/heating ckts
3. Air Con
4. Refrigerators
5. Freezer
6. P.C.S.

TELECOM

1. Battery Chargers
2. DC power Supply & UPS
3. Mobile Cell phone battery chargers.

TRANSPORTATION

1. Traction Control of electric vehicles.
2. Battery Chargers for electrical vehicle
3. Electric Locomotives
4. Street Cars and trolley buses.

UTILITY SYSTEMS

- * High voltage DC Transmission (HVDC)

~~Slab 2)~~

Pt 7

* Static VAR Compensation

* Fuel cell

* Energy storage systems

* Boilers feed systems.

POWER SEMICONDUCTOR DEVICES

* Power devices are of major two types. Silicon and Silicon Carbide devices.

In Silicon devices

Power Diodes

TRANSISTORS

THYRISTORS



1) BJTs

2) MOSFETs

3) IGBTs

4) SiTs

Note: 1) BJT → Power Bipolar Junction Transistor

2) Power MOSFETs → Power Metal Oxide Semiconductor field-effect transistors

3) Power IGBT : Power Insulated gate Bipolar Transistor

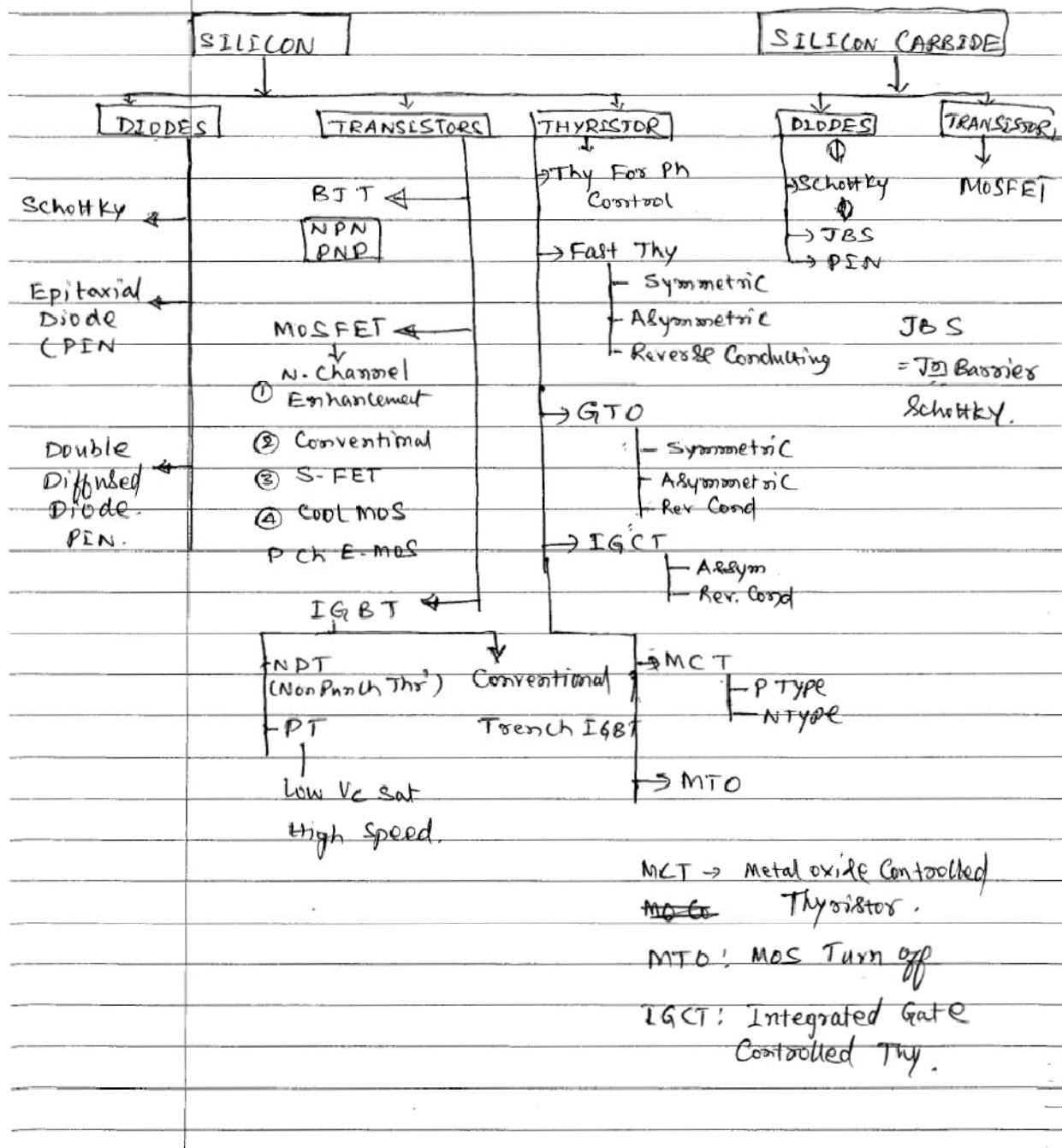
4) Power SiTs : Static Induction Transistor.

Summary

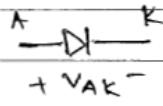
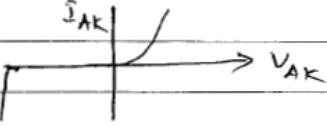
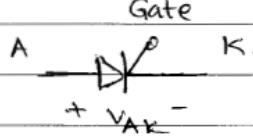
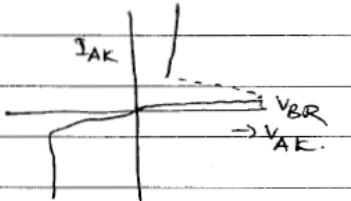
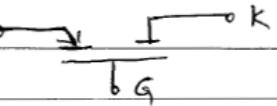
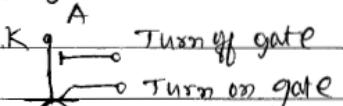
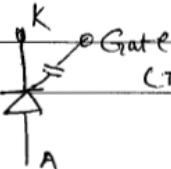
CLASSIFICATION OF POWER DEVICES

Based on material.

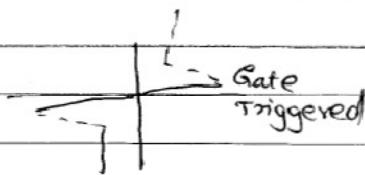
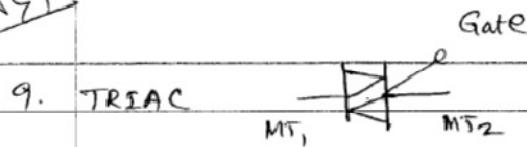
POWER SEMICONDUCTORS



CONTROL CHARACTERISTICS OF DEVICES

Device	Symbol	Characteristic
1. Diode		
2. Thyristor.		
3. SITH		-II-
4. GTO		-II-
5. MCT		-II-
6. MTO		-II-
7. ETO		(MOS-GTO hybrid) EMOSFET - GTO.
8. IG CT		-II-

~~8.10m SI~~

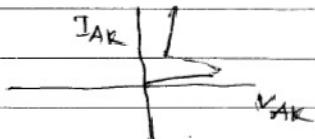
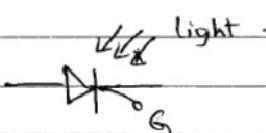


10. DIAC

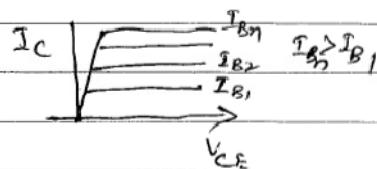
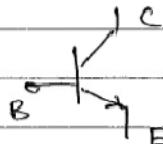


④

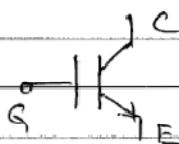
11. LASCR



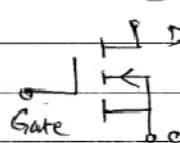
12. BJT
(NPN)



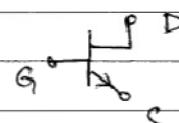
13. IGBT



14. MOSFET

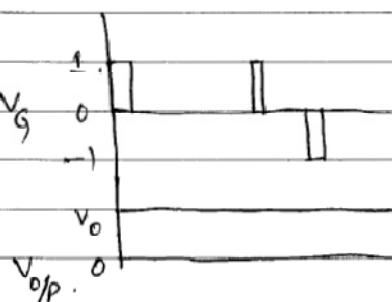
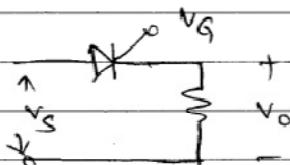


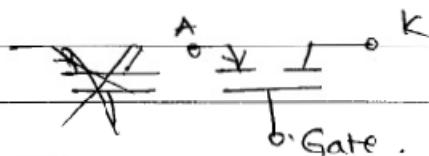
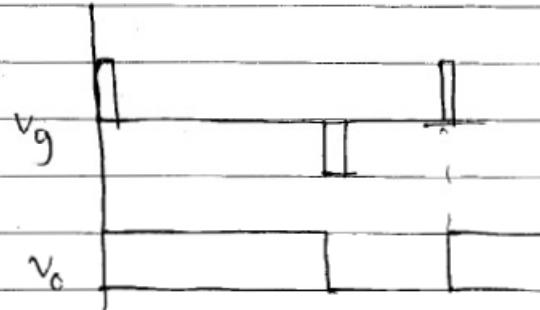
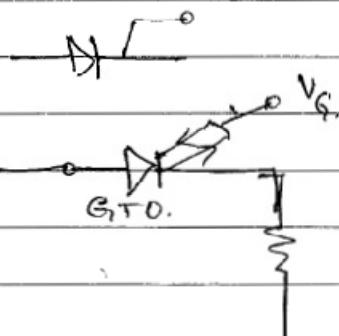
15. SIT



static Induction Transistor.

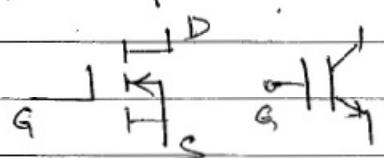
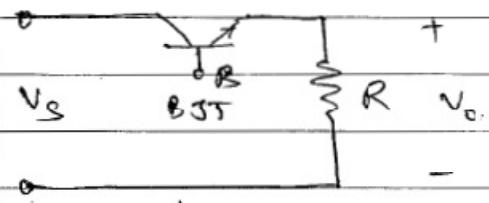
FOR CONTROL CH OF DEVICES
REFER PPT ALSO.





MCT

For all three devices.



MOSFET

IGBT



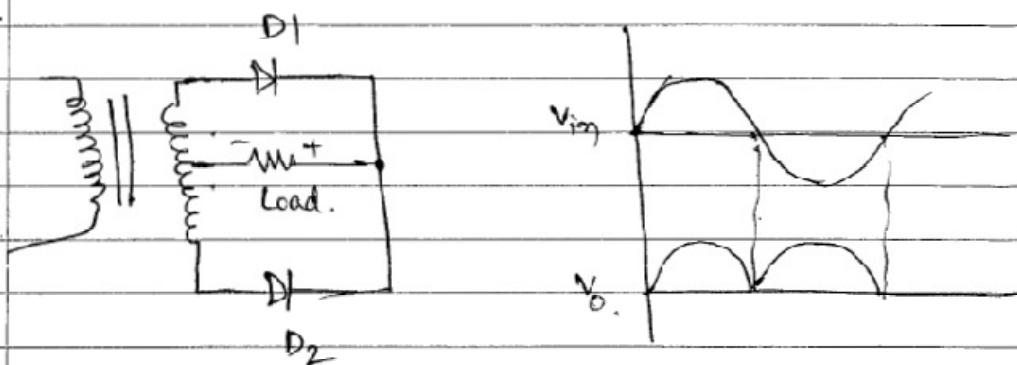
TYPES OF PE CIRCUITS

OR

TYPES OF POWER CONVERTERS

1. AC-DC Rectifiers Diode rectifiers
Controlled rectifiers
2. AC-AC Converters (AC VC)
3. DC-DC Converters (DC CHOPPERS)
4. DC - AC Converters (Inverters)
5. Static Switches.

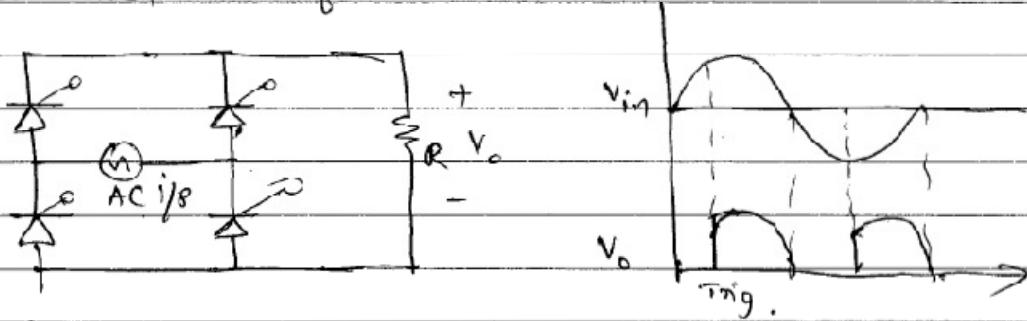
1.



Diode rectifiers.

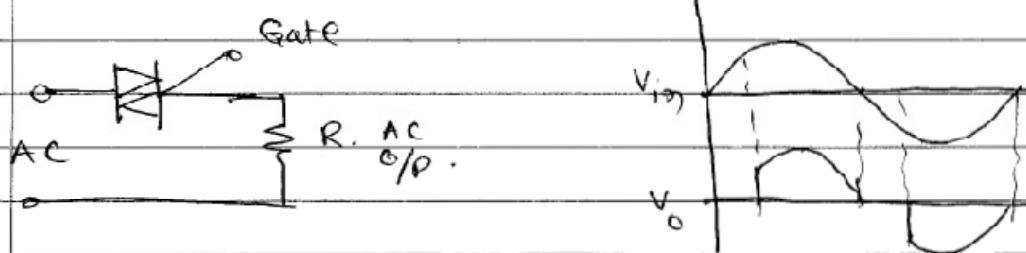
Explains the working. Converts AC i/p to fixed DC.

2. Controlled Rectifiers.



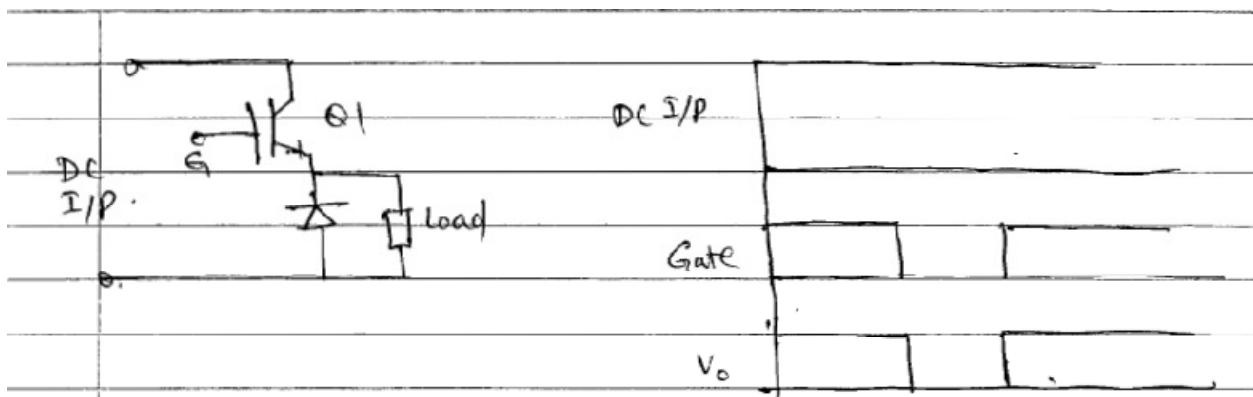
Converts Fixed AC TO Var DC.

3. AC TO AC Converter.



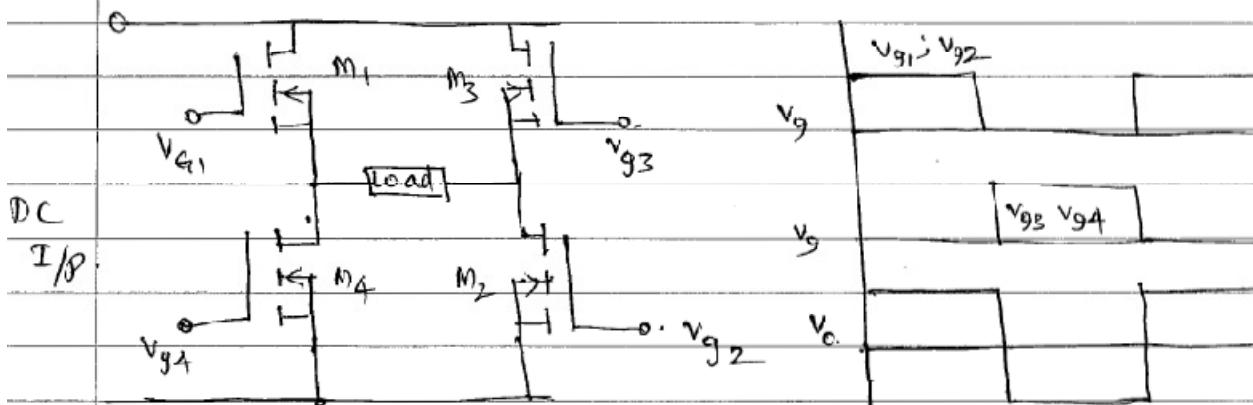
Converts Fix AC to Var AC.

4. DC - DC (static S/W) Also.



- ① Converts Fixed DC to var DC
- ② Q1 acts as Static E/W.

④ INVERTER



Converts DC to var AC.

PERIPHERAL EFFECTS

* Power Converters ~~operate~~ mainly operate by switching of Power devices.

④ Hence Converters introduce Current and

Voltage harmonics into the Supply System

* Problems because of this are:

- Distortion in o/p voltage,
- Harmonic generation into Supply system
- Interference with Communication or Signalling equipment (EMI)

Solution to the problem :

Introduce i/p and o/p filters in the Converter.

Important measuring factors are.

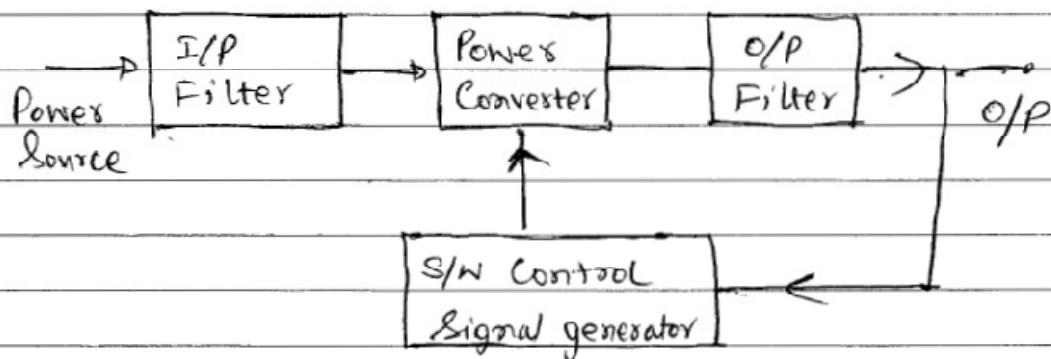
THD : Total Harmonic Distortion

DF : Displacement factor

IPF : I/P Power factor.

Further EMI can cause erroneous signals generated by gating circuits.

EMI can be reduced by grounded shielding.



Power modules :

Power devices are available as a single module or unit.

Power Converters require 2 or 4 or 6 devices depending on application.

Utilizing power modules offer lower on state losses, high voltage and current switchings at higher speed than that of conventional devices.

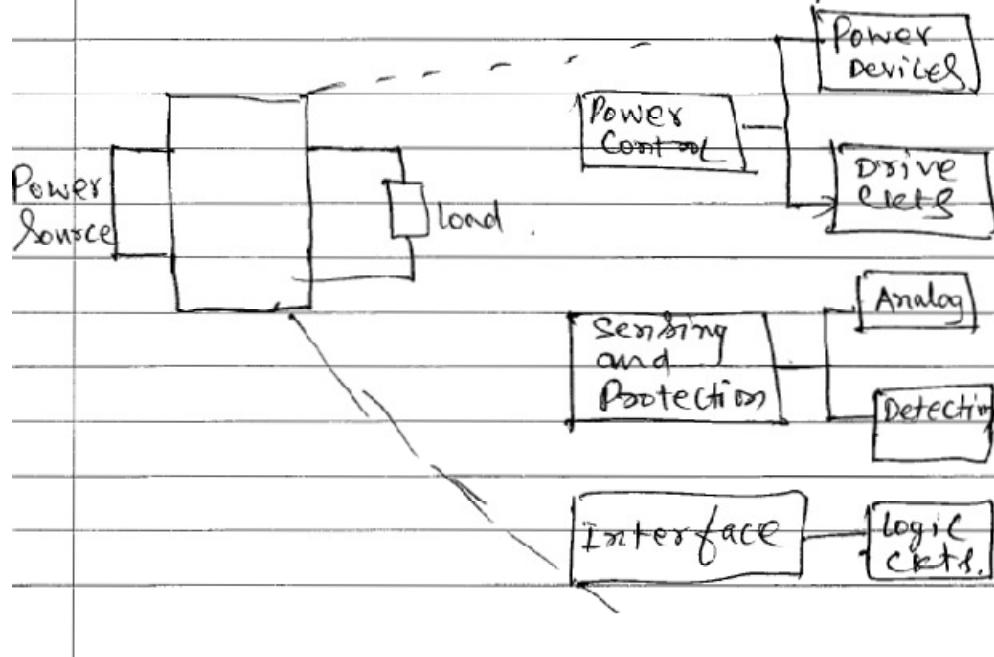
Some modules include transient protection and drive circuitry.

INTELLIGENT MODULES

These integrate the power module and the peripheral ~~unit~~ circuit.

Peripheral Ckt consists of i/p or o/p isolation, interface with signal & high voltage system, a drive Ckt, protection and diagnostic Ckt.

This is also known as Smart power technology.



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(P-17)

MODULE - 1

PART - 2

POWER TRANSISTORS

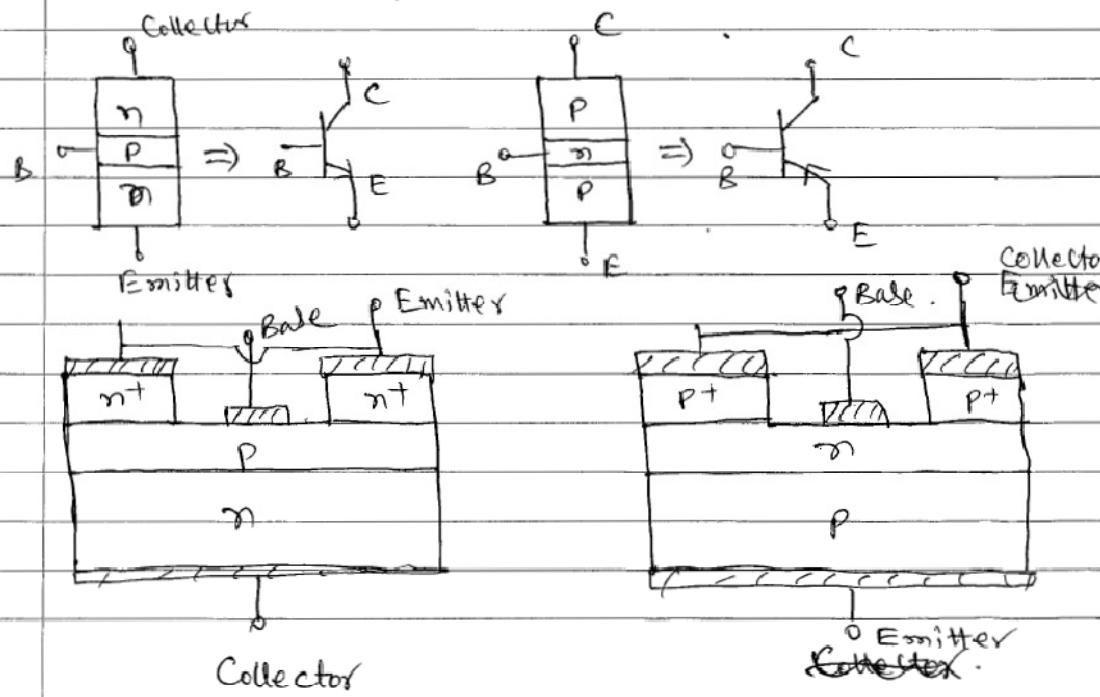
Power BJT :

- A switching device operated in Saturation and Cut off regions to reduce on-time power loss
- Faster than SCR but power rating is lower than SCR.

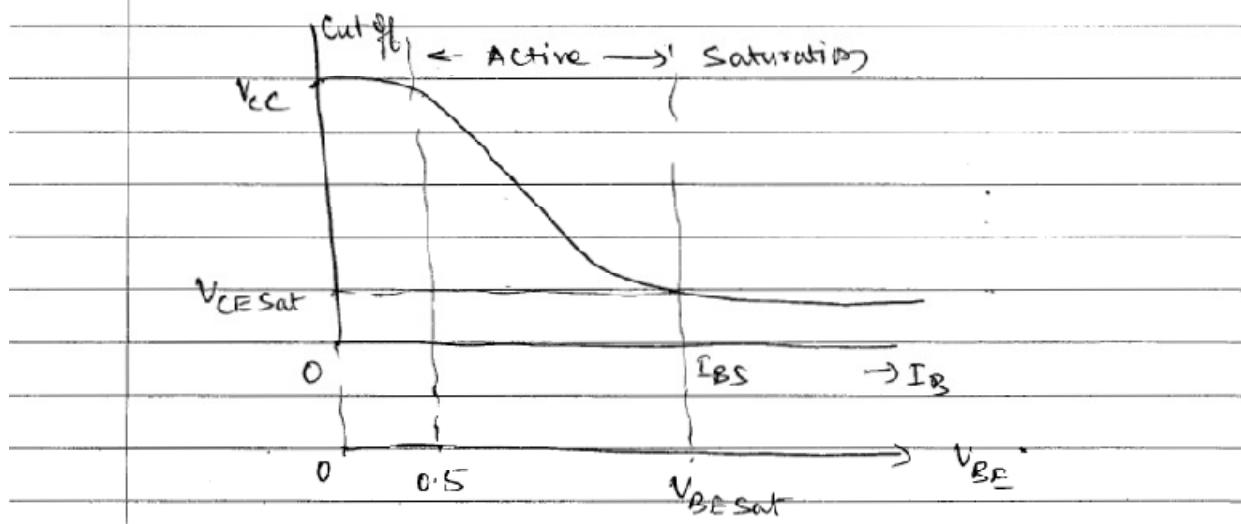
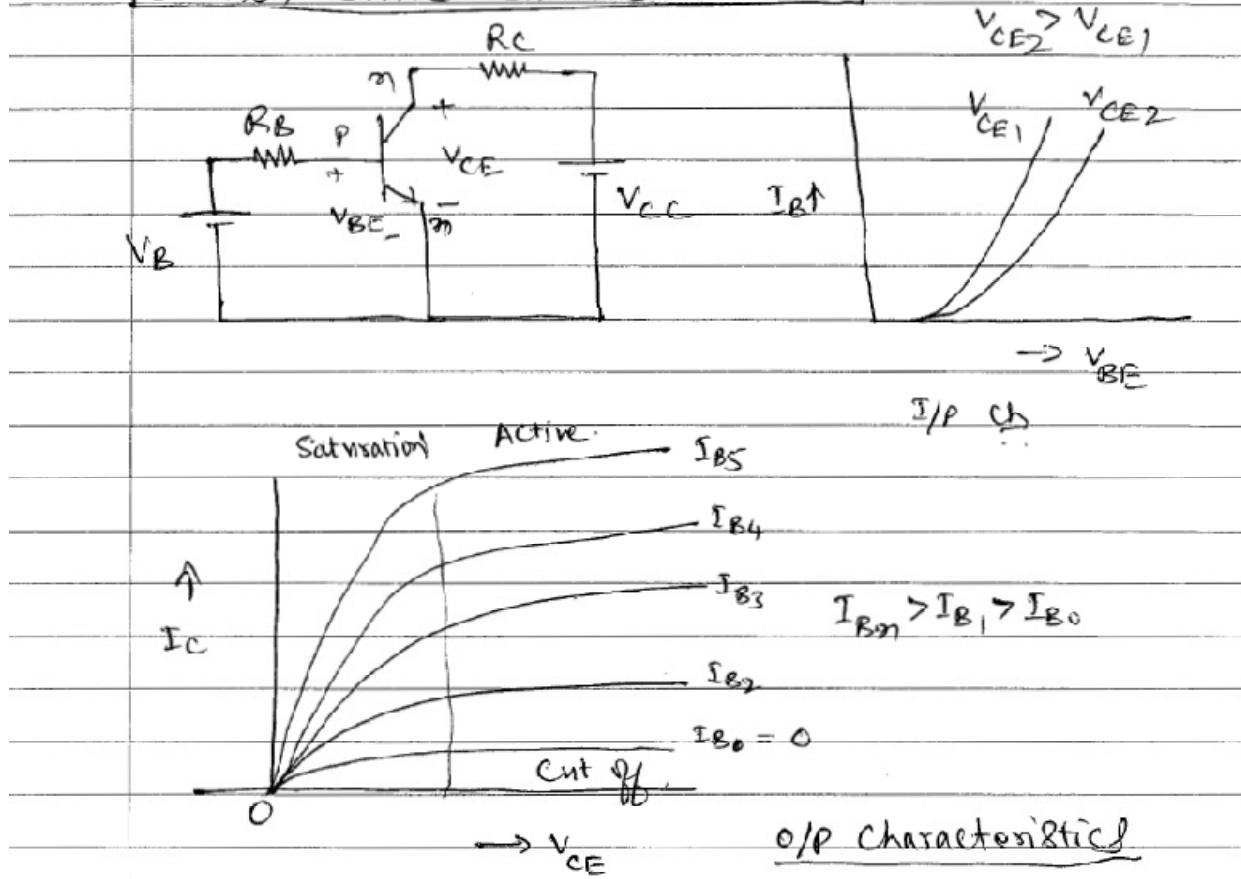
Classification :

1. BJT (NPN & PNP)
2. Metal oxide Semiconductor field effect Transistor (MOSFETs)
3. Static Induction Transistor (SITs)
4. Insulated Gate Bipolar transistors (IGBT)
5. COOLMOS

1. BJT

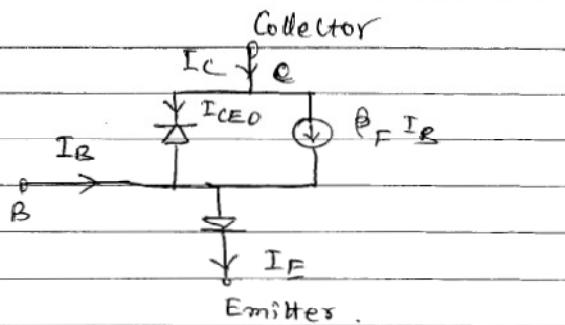


STEADY STATE CHARACTERISTICS



~~8 Jan 21~~

Transistor model:



$$I_C = \beta_F I_B + I_{CEO}$$

$$I_E = I_C + I_B = I_B(1 + \beta_F) + I_{CEO}$$

$$I_B = \frac{V_B - V_{BE}}{R_B} \quad \text{--- (1)} \quad I_{BS} = \frac{V_B - V_{BES}}{R_B}$$

$$I_{CS} = I_{CM} = \frac{V_{CC} - V_{CES}}{R_C} \quad \text{--- (2)}$$

$$I_{BC} = \frac{I_{CS}}{\beta}$$

$$I_B > I_{BS} \therefore \beta_{Forced} < \beta \text{ ---}$$

$$\boxed{\beta_{Forced} = \frac{I_{CS}}{I_B}}$$

Over drive factor $ODF = \frac{I_B}{I_{BS}}$

$$\boxed{\text{Power loss } P_J = V_{BES} I_B + V_{CES} I_{CS}}$$

Prob ① : In the BJT circuit shown above transistor has $\beta_F = 8$ to 40. The load resistance is $R_L = 11\sqrt{2}$. The dc supply $V_{CC} = 200V$ and input voltage to the base circuit is $V_B = 10V$. If $V_{CEsat} = 1.0V$

$V_{BES} = 1.5V$ find (a) value of R_B that results in saturation with an ODF of 5 (b) Forced β (c) Power loss.

If ODF = 10 Compare power loss.

$$\text{Ans: } I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{200 - 1}{11} = [18.1 \text{ A}]$$

$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{18.1}{8} = [2.2625 \text{ A}]$$

$$\text{ODF} = \frac{I_B}{I_{BS}} \therefore I_B = \text{ODF} * I_{BS}$$

$$= 5 * 2.2625$$

$$[I_B = 11.3125 \text{ A.}]$$

$$\therefore R_B = \frac{V_{BB} - V_{BES}}{I_B} = \frac{10 - 1.5}{11.3125} = [0.7514 \Omega]$$

$$\text{(ii) Forced } \beta = \frac{I_{CS}}{I_B} = \frac{18.1}{11.3125} = [1.6]$$

$$\text{(iv) Power loss} = P_T = V_{BES} I_B + V_{CES} I_{CS}$$

$$= 1.5 * 11.3125 + 1 * 18.1 = [35.07 \text{ W}]$$

$$\text{(v) If ODF} = 10 \quad [I_B = 22.625 \text{ A}]$$

$$\therefore P_T = 1.5 * 22.625 + 1 * 18.1 = [51.5 \text{ W}]$$

Note: Increasing ODF will not give any benefit

in I_{CS} and also power loss increased to double
Transistor is likely to burn.

Further reducing ODF more than 5 is likely
to make transistor to go to active region and
power loss will be more.

It is Compromise betⁿ S/N Speed, Saturation
and Power loss.

Prob 2: The β of BJT varies from 10 to 60. The load
(4.1) resistance is $R_L = 5\Omega$. The DC supply voltage
is 100V and i/p voltage $V_B = 8V$. If $V_{CESat} = 2.5V$
and $V_{BES} = 1.75V$ find (a) R_B which will result
in saturation with ODF of 20 (ii) Forced β
and Power loss for transistor.

[Ans]! $I_{CS} = \frac{V_{CC} - V_{CES}}{R_L} = \frac{100 - 2.5}{5} = 19.5A$.

$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{19.5}{10} = [1.95A]$$

$$I_B = ODF * I_{BS} = 20 * 1.95 = 39A$$

$$R_B = \frac{V_B - V_{BES}}{I_B} = \frac{8 - 1.75}{39} = [0.160\Omega]$$

$$(ii) \text{ Forced } \beta = \frac{I_{CS}}{I_B} = \frac{19.5}{39} = [0.5]$$

$$(iii) P_T = V_{BES} I_B + I_{CS} * V_{CES} = 1.75 * 39 + 19.5 * 2.5 \\ = [117W]$$

Prob ③: The β of BJT varies from 12 to 75.

The load resistance is $R_C = 1.5 \Omega$. The DC supply voltage is $V_{CC} = 40V$ and input voltage to the base circuit is $V_B = 6V$. If $V_{CES} = 1.2V$, $V_{BES} = 1.6V$ and $R_B = 0.7 \Omega$. Find ODF, Forced θ and Power loss P_T .

$$[Ans] I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{40 - 1.2}{1.5} = [25.87 A]$$

$$I_{BS} = \frac{I_{CS}}{\theta_{min}} = \frac{25.87}{12} = [2.16 A]$$

$$\text{ODF} \quad I_B = \frac{V_B - V_{BES}}{R_B} = \frac{6 - 1.6}{0.7}$$
$$= [6.28 A]$$

$$\text{ODF} = \frac{I_B}{I_{BS}} = \frac{6.28}{2.16} = [2.91] \approx [3].$$

$$\text{Forced } \theta = \frac{I_{CS}}{I_B} = \frac{25.87}{6.28} = [4.12].$$

$$P_T = V_{BES} I_B + V_{CES} I_{CS} = 1.6 * 6.28 + 1.2 * 25.87$$
$$= [41.09 W]$$

— o —

Prob ④: For the BJT Circuit if $V_{BES} = 1.5V$, $V_{CES} = 1.2V$, $\theta = 25$, $V_{CC} = 100V$, $R_C = 10 \Omega$ and $R_B = 20 \Omega$. Find (a) The min value of V_{BZ} required to ensure saturation.

(b) On state power loss of the transistor.

[Ans]

$$I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{100 - 1.2}{10} = [9.88 \text{ A}]$$

$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{9.88}{25} = [0.395 \text{ A}]$$

$I_{BS} = I_B$ with ODF = 1 as it is not given.

$$V_{BB} = I_{BS} R_B + V_{BEsat} = (0.395 * 20) + 1.5 = [9.4 \text{ V}]$$

(b) Power loss $P_T = V_{CES} I_{CS} + V_{BE} * I_B$ Note $I_B = I_{BS}$

$$= 1.2 * 9.88 + 1.5 * 0.395$$

$$[P_T = 12.44 \text{ W}]$$

Prob ⑤: The power BJT connected as a switch has

$V_{CES} = 1.2 \text{ V}$ and β in the range of 8 to 20

If $V_{CC} = 200 \text{ V}$, ODF = 5, $R_C = 15 \Omega$ compute

(a) value of the base cur required to move the transistor into saturation

~~for~~

[Ans]

$$I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{200 - 1.2}{15} = [13.25 \text{ A}]$$

$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{13.25}{8} = [1.66 \text{ A}]$$

$$I_B = ODF * I_{BS} = 5 * 1.66 = [8.30 \text{ A}]$$

$$\text{Forced } \beta = \frac{I_{CS}}{I_B} = \frac{13.25}{8.3} = [1.596]$$

Prob ⑥: In the above prob if $V_{BB} = 10 \text{ V}$ and $V_{BE} = 1.5 \text{ V}$

Compute R_B .

$$\text{Ans: } R_B = \frac{V_{BB} - V_{BES}}{I_B} = \frac{10 - 1.5}{8.3} = 1.024 \Omega$$

Prob ⑦: A Power BJT used as switch has β range of 10 to 25. If $V_{CC} = 230V$, $R_C = 12\Omega$, $V_{BB} = 15V$, $V_{CES} = 1.2V$ and $V_{BES} = 1.8V$

Find: (a) value of R_B required to move the transistor into saturation with ODF of 6.

(b) Forced θ

(c) Power dissipated in the transistor.

$$\text{Ans: } I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{230 - 1.2}{12} = 19.067A$$

$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{19.067}{10} = 1.9067A$$

$$I_B = \text{ODF} * I_{BS} = 6 * 1.9067 = 11.44A$$

$$R_B = \frac{V_{BB} - V_{BES}}{I_B} = \frac{15 - 1.8}{11.44} = 1.154 \Omega$$

$$(b) \text{Forced } \theta = \frac{I_{CS}}{I_B} = \frac{19.067}{11.44} = 1.667$$

$$(c) P_T = V_{CES} I_{CS} + V_{BES} I_B \\ = 1.2 * 19.067 + 1.8 * 11.44 = 43.47W$$

Prob(8): A Power BJT used at a S/W for the circuit
 has $V_{CE(SAT)} = 1.8V$ $V_{BE} = 1.2V$ $\theta_{min} = 12^\circ$.
 Given $R_C = 12\Omega$ and $R_B = 6\Omega$ and $V_{CC} = 220V$

calculate: (i) Min value of V_{BB} required to drive
 max cur thr' R_C . Also find power
 dissipated in transistor in this
 Condition.

(ii) If V_{BB} is reduce to 75% of the
 value calculated in part (i)
 Find power dissipated in transistor

Comment on the result.

$$(\text{Ans}) I_{CM} = I_{CS} = \frac{V_{CC} - V_{CE(S)}}{R_C} = \frac{220 - 1.8}{12} = [18.18A]$$

$$I_{BS} = \frac{I_{CS}}{\theta_{min}} = \frac{18.18}{12} = [1.515A]$$

With ODF = 1 as not given

$$V_{BB} = I_{BS} R_B + V_{BE(S)} = 1.515 * 6 + 1.2 \\ = [10.29V]$$

$$P_{TON} = I_{CS} V_{CE(S)} + V_{BE(S)} I_B \quad \text{Note } I_B = I_{BS} \\ = 1/2 18.18 * 1.8 + 1.2 * 1.515 = [34.54W]$$

$$\text{Part (2)}: V_{BB\text{NEW}} = V_{BB} * 0.75 = 0.75 * 10.29 \\ = [7.72V]$$

$$I_B = \frac{V_{BB} - V_{BE}}{R_B} = \frac{7.72 - 1.2}{6} = [1.087A]$$

$$I_C = \beta_{\text{min}} I_B = 12 * 1.087 = [13.044 \text{ A}]$$

New

$$V_{CE} = V_{CC} - I_C R_C = 220 - 13.044 * 12$$

$$[V_{CE} = 63.472 \text{ V.}]$$

$$P_T = V_{BE} * I_B + V_{CE} I_C$$

$$= 1.2 * 1.087 + 63.472 * 13.044$$

$$[P_T_{\text{New}} = 829.21 \text{ W.}]$$

Note: As V_{BE} is reduced I_B is reduced and transistor comes to active region. Hence power loss increased extensively which may damage transistor.

This is one of the reasons of ODF, which will avoid this scenario.

→ C →

Q9: Jul Aug 2006 Vtu 7 mks

A power BJT is connected as a switch with following data:

R_E that will result in saturation with ODF 20

$V_{CC} = 100 \text{ V}$, $V_B = 8 \text{ V}$, $V_{CES} = 2.5 \text{ V}$, $V_{BES} = 1.75 \text{ V}$

$\beta = 10 \text{ to } 60$, $R_C = 10 \Omega$

$$I_{CS} = \frac{V_{CC} - V_{CES}}{R_C} = \frac{100 - 2.5}{10} = 9.75 \text{ A}$$

$$I_{BS} = \frac{I_{CS}}{\beta_{\text{min}}} = \frac{9.75}{10} = [0.975 \text{ A}]$$

$$I_B = ODF * I_{Bsat} = 20 * 0.975 = [19.5 \text{ A}]$$

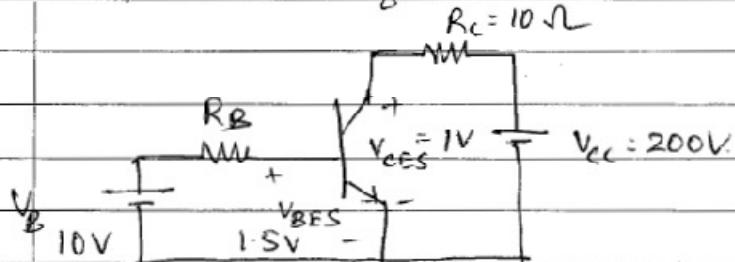
$$R_B = \frac{V_B - V_{BE}}{I_B} = \frac{8 - 1.75}{19.5} = [0.325 \Omega]$$

$$\text{Forced } \theta = \frac{I_{CS}}{I_B} = \frac{9.75}{19.5} = [0.5]$$

$$\begin{aligned} \text{Power loss } P_T &= V_{BE} I_B + I_{CS} V_{CE} \\ &= 1.75 * 19.5 + 2.5 * 9.75 \\ &[P_T = 58.5 \text{ W}] \end{aligned}$$

P_{QD} ⑩ Jan Feb 2007, 8 Mar 2008 7mks vtu.

A transistor S/W has θ in the range of 8 to 10
find value of R_B that results in saturation
with an ODF of 5



$$\text{Ans: (i) } I_{CS} = \frac{V_{CC} - V_{CEC}}{R_C} = \frac{200 - 1}{10} = [19.9 \text{ A}]$$

$$\text{(ii) } I_{BS} = \frac{I_{CS}}{\theta_{min}} = \frac{19.9}{8} = [2.4875 \text{ A}]$$

$$\text{(iii) } I_B = ODF * I_{BS} = [12.4375 \text{ A}]$$

$$R_B = \frac{V_B - V_{BE}}{I_B} = \frac{10 - 1.5}{12.4375} = 0.68348 \Omega$$

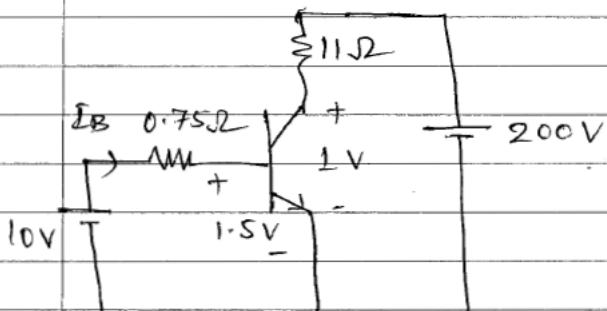
$$\beta_f = \frac{I_{CS}}{I_B} = \frac{19.9}{12.4375} = 1.6$$

$$P_T = V_{BE} I_B + V_{CE} I_{CS}$$

$$= 1.5 * 12.4375 + 1 * 19.9 = 38.55 \text{ W}$$

Prob(11): Aug 04, DEC10, 2009, 2017 8 Mks.

Calculate force Θ , if manufacturer specified β is in range of 8 to 40. Calculate min ODF obtain powerloss of transistor.



$$\text{Ans: } I_{CS} = \frac{V_{CC} - V_{CE}}{R_C} = \frac{200 - 1}{11} = 18.09 \text{ A}$$

$$V_B = I_B R_B + V_{BE} =$$

$$I_B = \frac{V_B - V_{BE}}{R_B} = \frac{10 - 1.5}{0.75} = 11.33 \text{ A}$$

$$\text{Forced } \theta = \frac{I_{CS}}{I_B} = \frac{18.09}{11.33} = 1.596$$

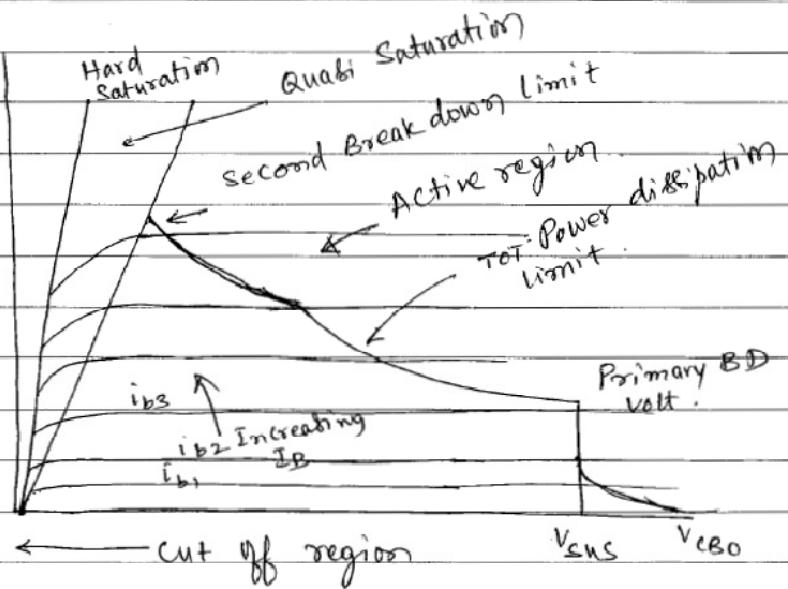
$$I_{BS} = \frac{I_{CS}}{\beta_{min}} = \frac{18.9}{8} = 2.261 \text{ A}$$

$$ODF = \frac{I_B}{I_{BS}} = \frac{11.33}{2.261} = 5$$

$$P_T = V_{BES} I_B + V_{CES} I_{CS}$$

$$= 1.5 * 11.33 + 1 * 18.09 = 35 \text{ W}$$

DIFFERENT OPERATING REGIONS OF BJT.



Regions of opⁿ:

1. Cut off region 2. Active region

3. Saturation (Hard Saturation & Quasi Saturation)

Second Break down: As the BJT is in hard saturation, V_{ce} is high but takes time to spread in junction. This creates high current intensity at small areas of operation. This forms hot spots and likely to burn the transistor.

Total power dissipation: The power to be dissipated by transistor based on area of the junction.

Primary break down: Avalanche break down of reverse biased CB junction.

FBSOA: Forward bias Safe operating area.

IMPORTANT FEATURES OF POWER BJT

1. Power BJTs are high power versions of normal BJT

2. Both NPN & PNP are available

3. NPN are relatively of higher rating typically 1200V 800A, with max switching speed of 10 KHz.

4 Compared to SCR they are faster and fully controlled that on and off both are controlled

5. For medium power applications of $< 500V$ MOSFETs are preferred

6. IGBT and MCT have replaced BJT in higher power applications also.

Types of BJT devices.

- Power BJT
- MOSFET
- IGBT
- SIT

MERITS OF BJT

1. Small turn on and turn off time, hence higher switching frequencies.
2. Small turn on losses
3. Base drive has full control on operation of BJT
4. BJTs do not require commutation circuits.
5. BJT is a Bipolar device.
6. Less expensive.

DEMERITS/ DISADV OF BJT

1. The DC current gain h_{FE} is as low as 20 or 10 and varies with collector current and temperature.
2. Increase in h_{FE} by multiple stages is not possible due to reduction in switching speed.

1. Device can be damaged due to secondary breakdown.
5. BJT require complex expensive base drive circuits and isolation circuits.
6. BJT parallel Configuration is difficult due to -ve temperature coefficient.

APPLICATIONS OF BJT

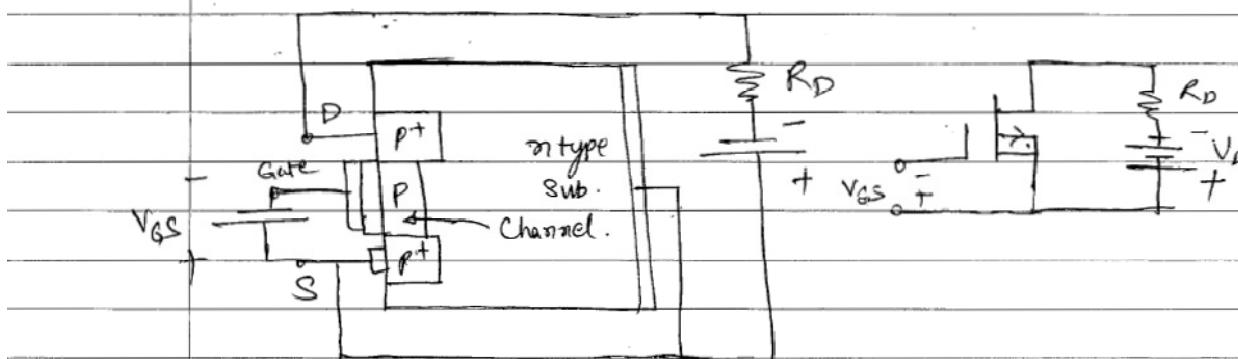
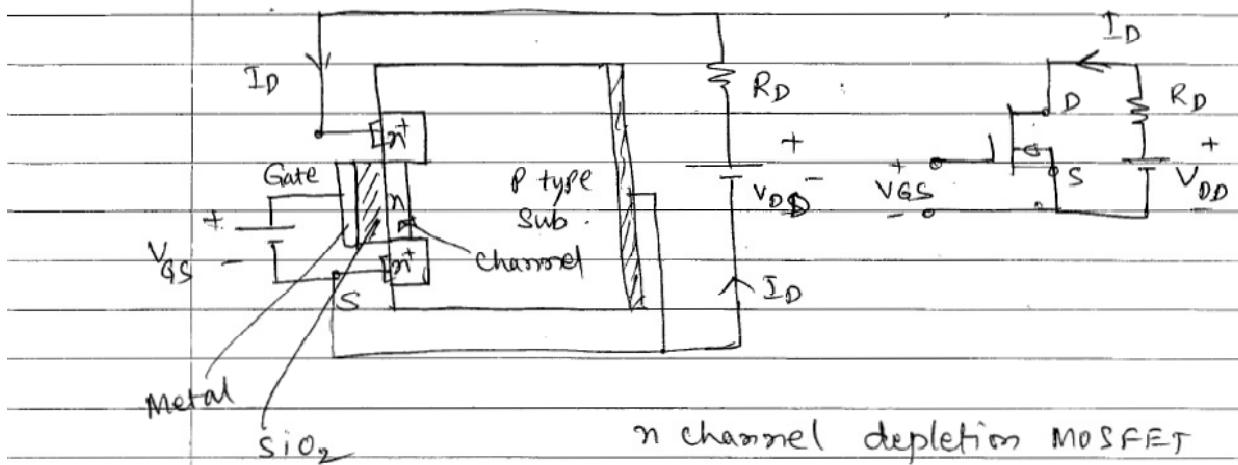
1. As main switching device in Inverter & chopper
2. In SMPS
3. In the linear power supplies as a series pass transistor.
4. In UPS and AC Motor applications.

Stomper:

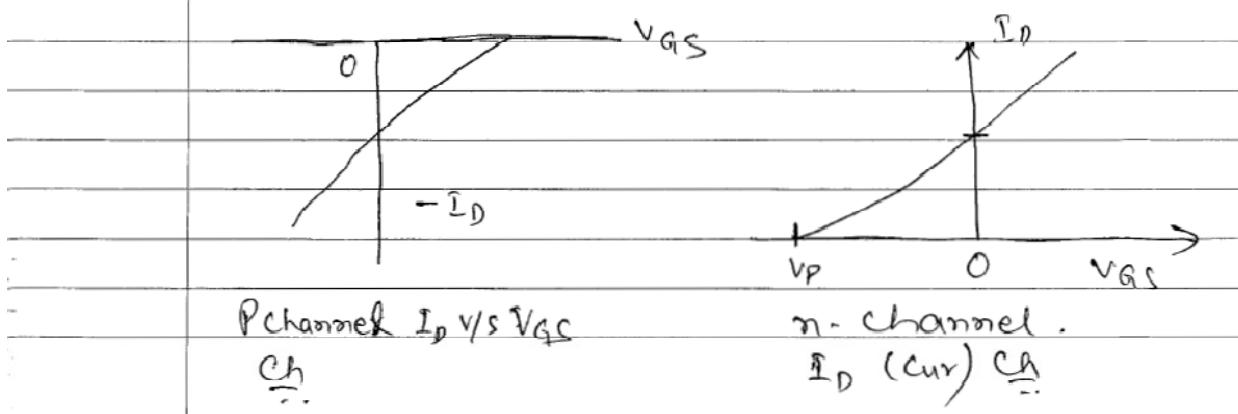
P-33

POWER MOSFETS

Construction :

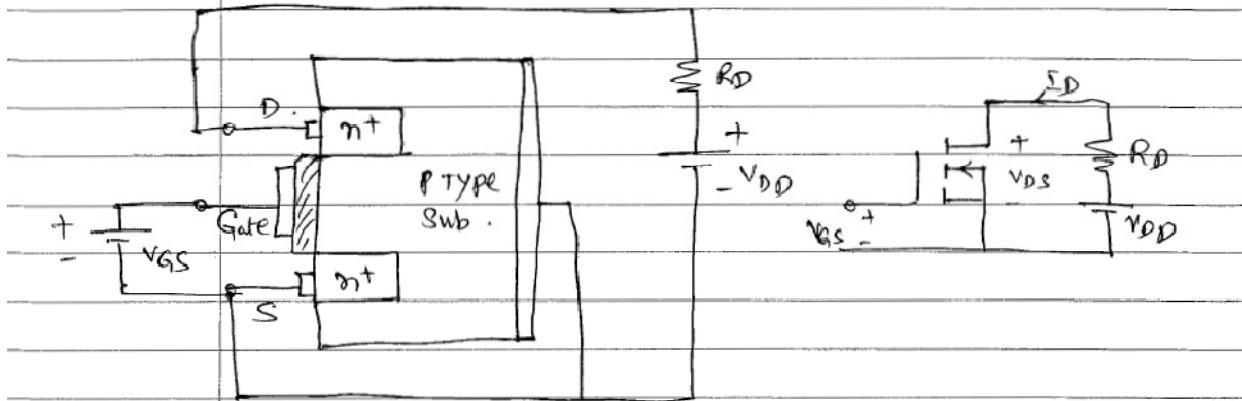


p Channel depletion MOSFET

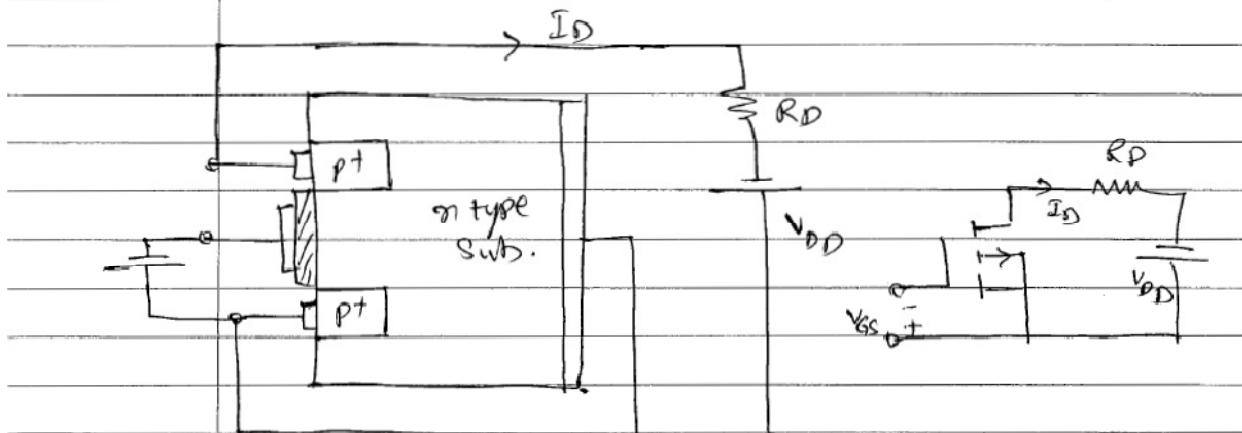


~~Slower~~

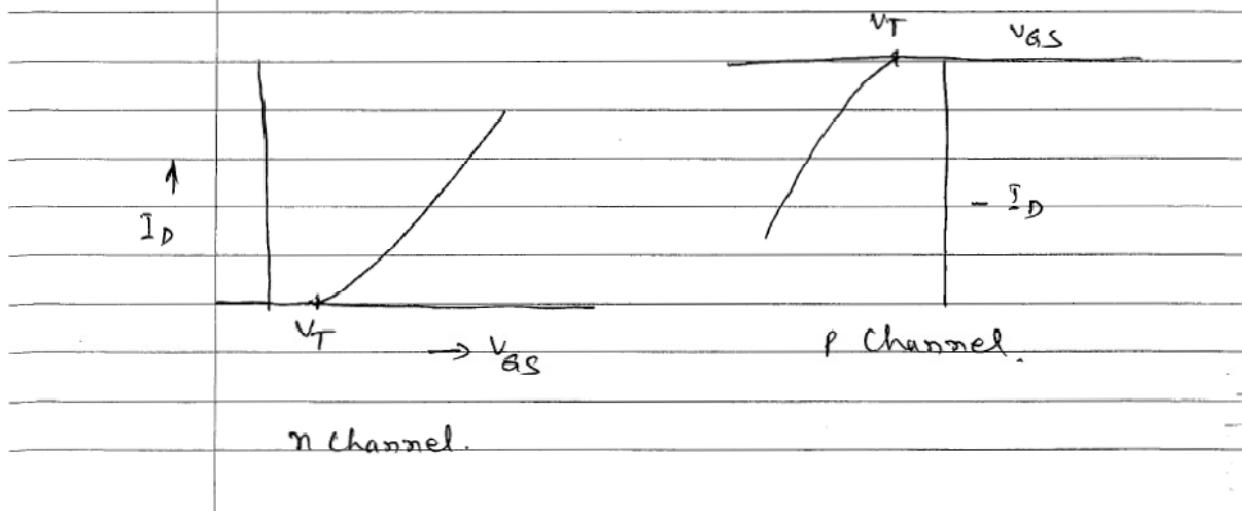
Enhancement MOSFET . (E-MOSFET)



n-channel E-MOSFET



P-channel E-MOSFET .



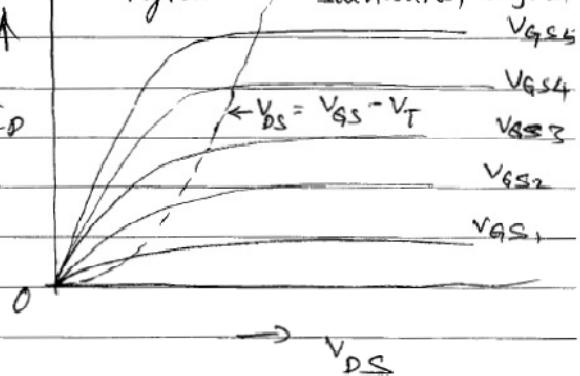
STEADY STATE CHARACTERISTICS

$$V_{GS4} > V_{GS3} > V_{GS2} > V_{GS1} > V_T$$

I_D

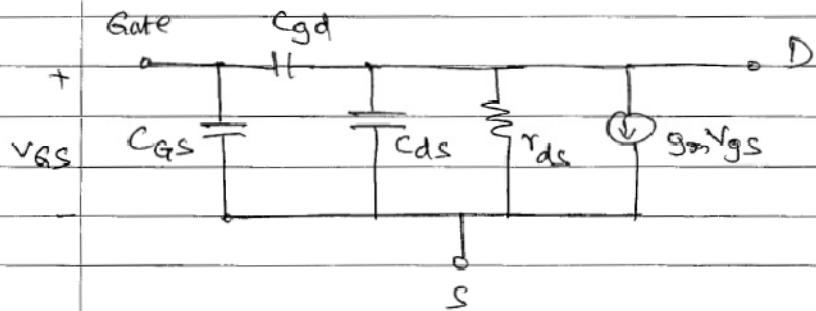
Linear \rightarrow Pinch off or
region Saturation region

V_{GS5}

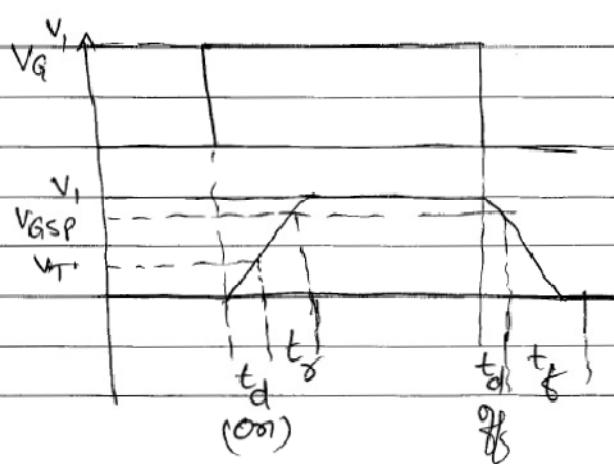


$$R_{DS} = \frac{\Delta V_{DS}}{\Delta I_D}$$

SWITCHING CHARACTERISTICS



Switching model.



$$t_{ON} = t_{d_{ON}} + t_r$$

$$t_{OFF} = t_{d_{OFF}} + t_f$$

t_d = delay time t_r = rise time t_f = fall time.

$t_{d_{ON}}$ = time taken to charge input Capacitor to threshold voltage.

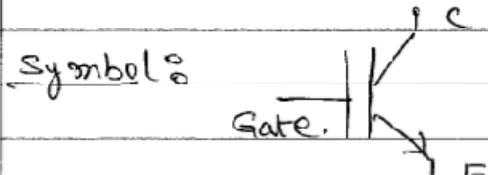
t_r = rise time is the time taken to take O/B voltage to full gate voltage.

$t_{d_{OFF}}$ = time taken to discharge i/b capacitor.

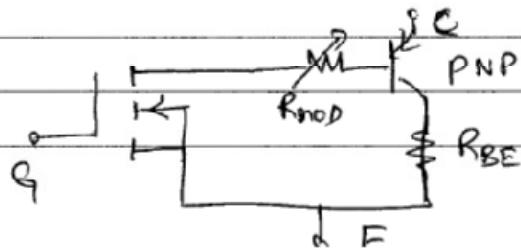
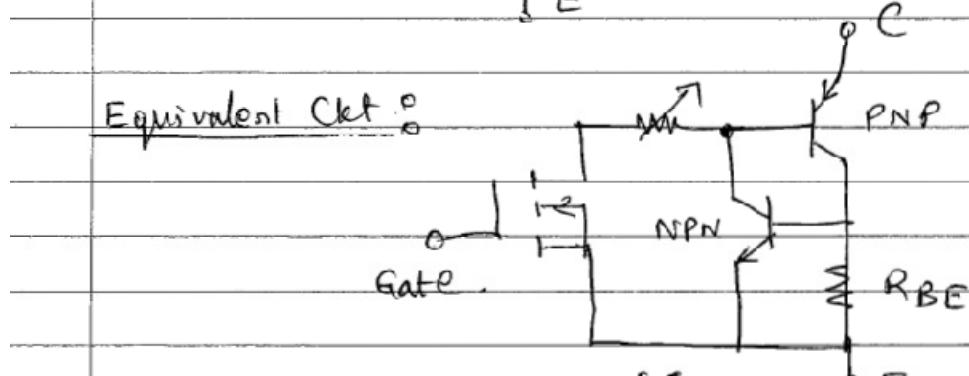
INSULATED GATE BIPOLAR TRANSISTOR.

[IGBT]

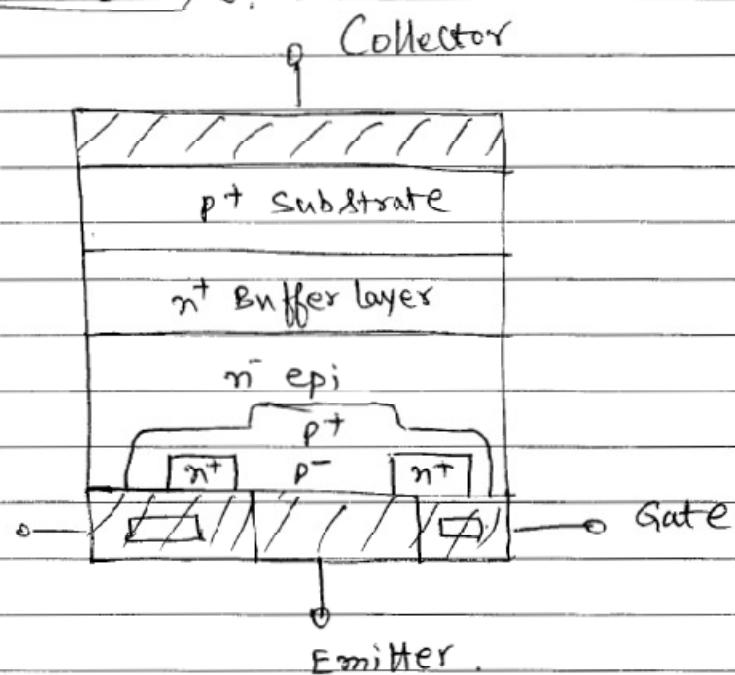
Symbols



Equivalent Circ. :



Construction :



[FEATURES]

- Low on state voltage drop
- Low on state Power loss
- Higher Switching Speed as Compared to BJT
- High input impedance because of isolation of gate by SiO_2
- Combined Adv of BJT & MOSFET
- BJT has lower on state power loss but slower switching speed
- MOSFET has higher on state power loss but higher switching speed.
- IGBT combines both advantages.
- Other names for IGBT : COMFET
(Conductivity modulated MOSFET)

IGT : Insulated gate Transistor

Bipolar MOS Transistor.

Types of IGBT

NON - PUNCH THROUGH IGBT

n^+ Buffer layer is absent, causing symmetrical blocking i.e. Both $+V_{CE}$ & $-V_{CE}$ are blocked equally.

$+ve$ or $-ve$ V_{CE} blocked equally.

PUNCH THROUGH IGBT

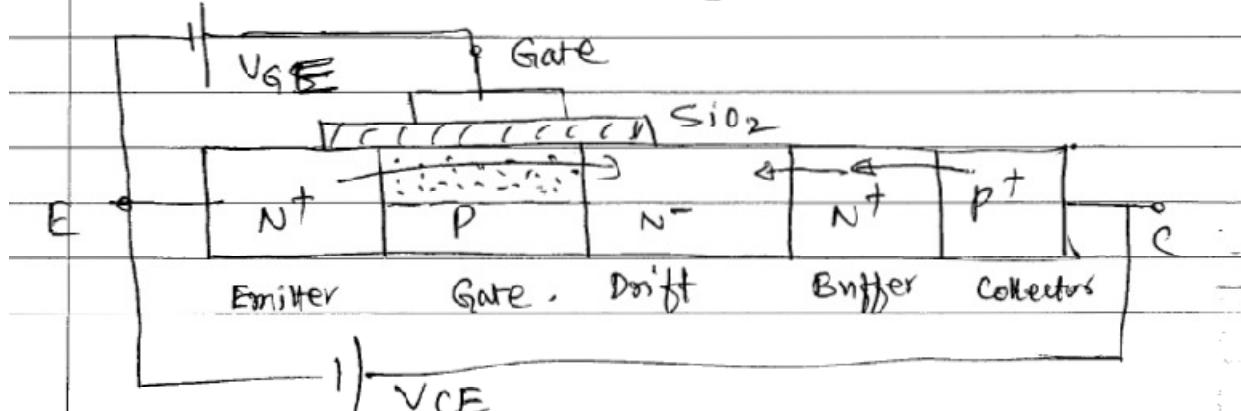
n^+ Layer or buffer present.

This has Asymmetrical blocking

$+V_{CE}$ blocked successfully but

not $-V_{CE}$.

OPERATION OF IGBT



1. Formation of Inversion Layer}:

Forward biasing of Gate to Source V_{GE} will attract minority carriers from P region to form a conduction path.

Minimum V_{GE} to formulate this electron layer is called as Threshold voltage which is similar to MOSFET.

2. CONDUCTIVITY MODULATION }:

Holes from P+ region are pushed towards drift region due to V_{CE} .

Electrons are pushed from N+ region through inversion layer.

A small amount of recombination takes place but most of charge carriers both electrons and holes travel in opposite direction.

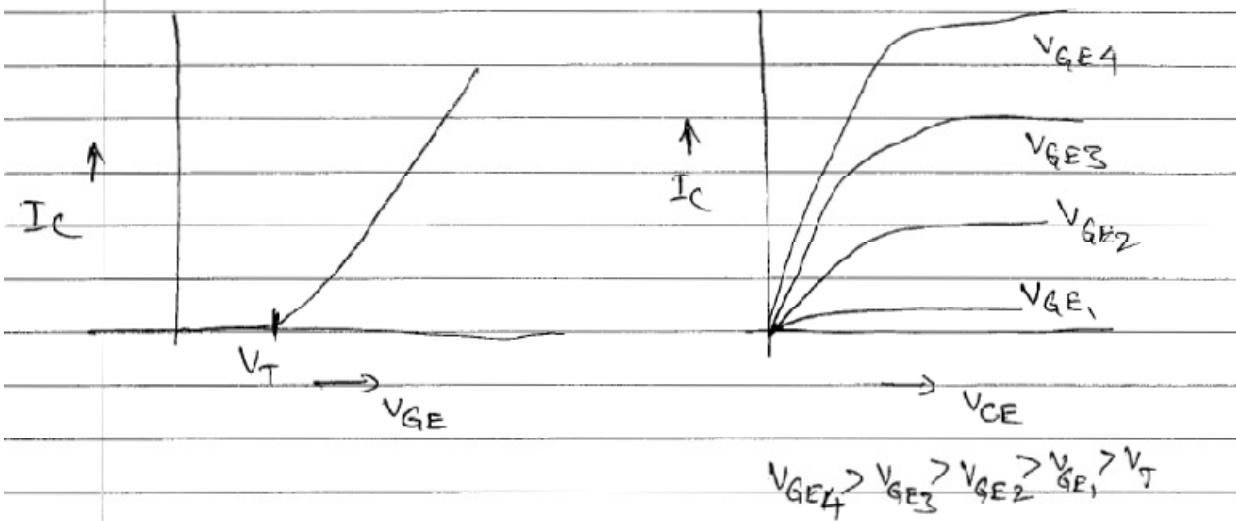
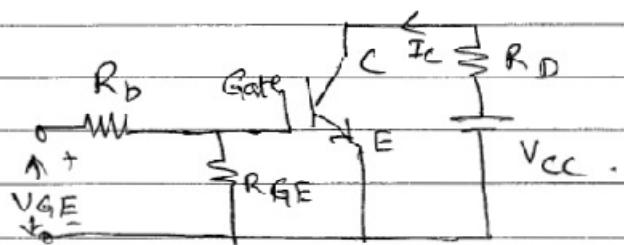
The Collector current is due to both carrier movement that is holes and electrons.

This process is called as Conductivity modulation which is not there in MOSFET.

In MOSFET Current is due to one type of charge carrier only.

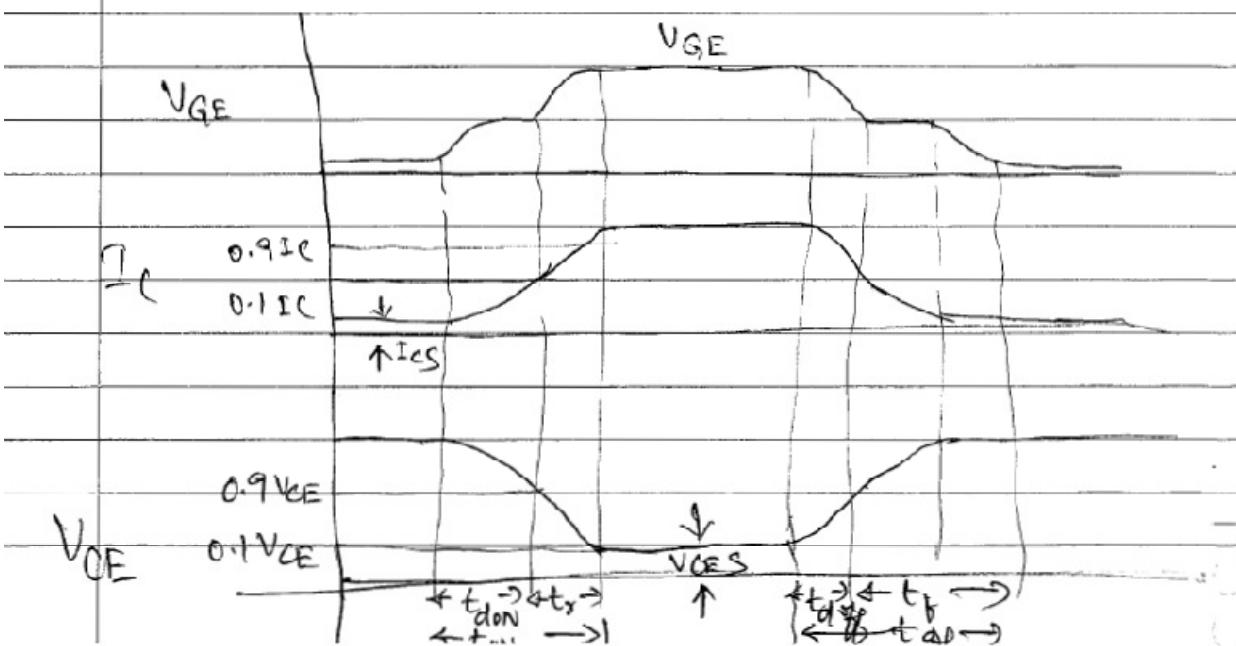
This results in higher C_{DS} in IGBT hence lower ON state resistance.

STATIC CHARACTERISTICS



Explain Ch in to MOSFET .

SWITCHING CHARACTERISTICS



$$t_{on} = t_{d_{on}} + t_{r} \quad \text{delay time + rise time.}$$

$$t_{off} = t_{d_{off}} + t_{f} \quad \text{delay time + fall time.}$$

ADVANTAGES OF IGBT .

1. Combines advantages of BJT and MOSFET
2. High input impedance like MOSFET
3. Voltage controlled device like MOSFET
4. Simple gate drive and lower switching loss
5. Low on state conduction power loss like BJT
6. Higher current capability and higher switching speed than BJT.

DISADVANTAGE OF IGBT .

1. Asymmetric blocking
2. Switching frequency lesser than MOSFET
3. Problem of latch up.
4. Power dissipation during turn off due to current tail in switching characteristic

APPLICATIONS OF IGBT .

1. AC & DC motor control
2. General purpose inverters
3. UPS
4. Welding equipment

~~Shameel~~

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5. Numerical Control Cutting tools

6. Robotics and Induction heating

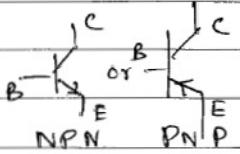
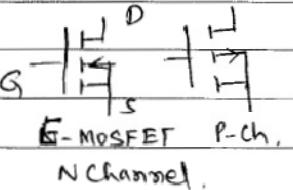
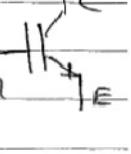
COMPARE SCR AND BJT }

SL No.	SCR	BJT
1.	Four layer device	Three layer device
2.	Turns on by regeneration	No regeneration
3.	Gate loses control after S/W off	Gate or base has full control.
4.	Commutation or circuit for S/W off required	No external circuit for switching off.
5.	Switching freq are low	S/W freq, high.
6.	$\frac{dv}{dt}$ protection required to avoid false switching	BJT will be damaged due to excessive $\frac{dv}{dt}$
7.	Used in Controlled rectifiers, AC regulators, DC drives.	Used in inverters, UPS, AC drives, SMPS

~~Slam 21~~

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COMPARISON OF POWER DEVICES

SL No.	Parameter	Power BJT	MOSFET	IGBT
1. Symbol				
2. Type of device	Minority Carrier device	Majority Carrier device	Majority Carrier Device	
3. Temp° Coefft	-ve	+ve	Flat.	
4. Volt Blocking	Asymmetric	Asymmetric	Asymmetric to Symmetric	
5. operating freq	10 KHz	100 KHz	10 KHz	
6. Trigger Circuit	Circuit Controlled Needs Continuous base drive	Volt Controlled Needs Continuous base drive	Volt Control - Need cont. Cont. base drive	
7. on State volt drop	< 2V	4-5V	3V	
8. Snubbers	Required	May be eliminated	May be eliminated	
9. VI rating	2kV/1KA	600V/200A	1500V/400A	
10. App	UPS, SMPS Static VAR Sys AC Motor Control	AC motor control SMPS	SMPS BLDC drives AC motor inverter	

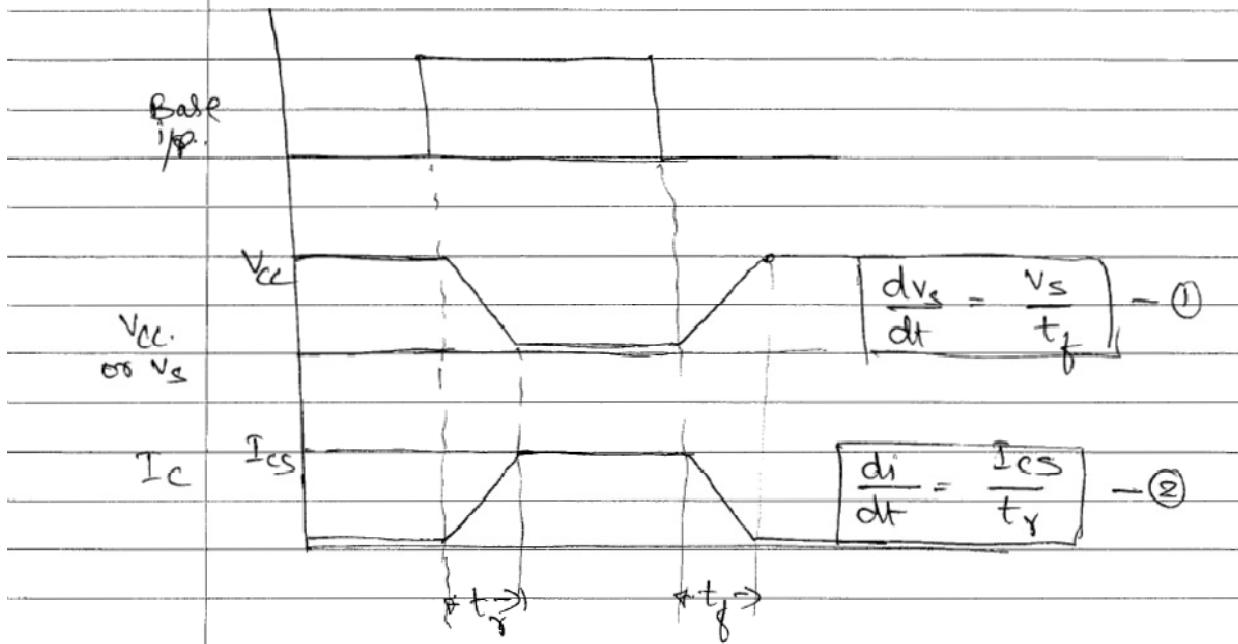
Stamp 2)

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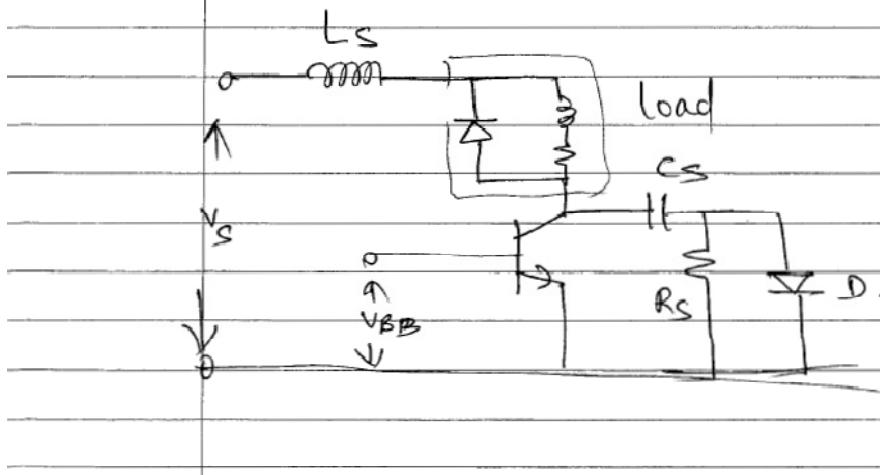
$\frac{di}{dt}$ and $\frac{dv}{dt}$ Protection OR

SNUBBER Ckt Design.

- Consider S/W Characteristic of BJT.
- Assume delay time t_d is very small.



SNUBBER Ckt.



~~Slowly~~

while Switching on $L_s \frac{di}{dt} = V_s$

As Complex voltage comes across L_s and slowly current increased.

$$\therefore \frac{di}{dt} = \frac{V_s}{L_s} = \frac{I_{cs}}{t_r} \quad \therefore L_s = \frac{V_s t_r}{I_{cs}}$$

From ② - ③

while S/n of

$$C_s \frac{dv_s}{dt} = I_{cs} \quad \therefore \frac{dv}{dt} = \frac{I_{cs}}{C_s} = \frac{V_s}{t_f}$$

$$\therefore C_s = \frac{I_{cs}}{V_s} t_f \quad - ④$$

Design $\Rightarrow R_s$.

Baled on resonant circuit and damping ratio

In a Series RLC network.

$$\frac{V_o(s)}{V_i(s)} = \frac{\frac{1}{L_s C_s s + \frac{R_s}{2}}}{s^2 + \frac{R_s}{L_s C_s} s + \frac{1}{L_s C_s}}$$

$$\therefore \text{In Ch eqn } \omega_m^2 = \frac{1}{L_s C_s} \quad \text{or} \quad \omega_m = \frac{1}{\sqrt{L_s C_s}}$$

$$2 \xi \omega_m = \frac{R_s}{L_s} \quad \text{or} \quad \xi = \frac{R_s}{L_s} \times \frac{1}{2 \omega_m}$$

$$\therefore \zeta = \frac{R_s}{2} \sqrt{\frac{C_s}{L_s}}$$

For Critically damped Case $\zeta = 1$.

$$\text{or } R_s = 2 \sqrt{\frac{L_s}{C_s}} \quad - (5)$$

i Case : Based on freq of operation.

$$\text{Time Constant } R_s C_s = \frac{T_s}{3}$$

$$\text{or } R_s = \frac{1}{3 f_{op} C_s} \quad - (6)$$

ii Case Based on Discharge Cur.

$$I_{\text{discharge}} = \frac{V_s}{R_s}$$

Power dissipated by Snubber neglecting Inductor loss.

$$\frac{1}{2} C_s V_s^2 f_s$$

Prob ①

A bipolar transistor is operated as a chopper switch at a freq of $f_S = 10 \text{ KHz}$. The DC voltage of chopper is $V_S = 220V$ and the load cur $I_L = 100A$ $V_{CES} = 0V$. The switching times are $t_d = 0$, $t_r = 3 \mu\text{s}$, $t_f = 1.2 \mu\text{s}$

Find L_S , C_S , R_S for critically damped case
 R_S for discharge time to be limited $\frac{1}{3}$ of switching period. R_S if the peak curr discharge curr limited 10% of load curr.
Power loss in RC ladder neglecting L_S

$$\text{Ans: } L_S = \frac{V_S t_r}{I_L} = \frac{220 * 3 * 10^{-6}}{100} = [6.6 \mu\text{H}]$$

$$C_S = \frac{I_L t_f}{V_S} = \frac{100 * 1.2 * 10^{-6}}{220} = [0.55 \mu\text{F}]$$

$$R_S = 2 \sqrt{\frac{L_S}{C_S}} = [6.98 \Omega]$$

Critically damped

$$R_S = \frac{1}{3 f_S C_S} = \frac{1}{3 * 10 * 10^3 * 0.55 * 10^{-6}} = [60.6 \Omega]$$

$$R_S = \frac{V_S}{I_{\text{Disch}}} = \frac{V_S}{0.1 * I_L} = \frac{220}{0.1 * 100} = [22 \Omega]$$

$$P_S = \frac{1}{2} C_S V_S^2 f_S = [133.1 \text{ W}]$$

Prob ②: A BJT operated as a chopper switch at a freq $f_s = 20 \text{ kHz}$. The DC input voltage is $V_s = 400\text{V}$, load curr $I_L = 100\text{A}$

The switching time $t_s = 1\mu\text{s}$ $t_f = 3\mu\text{s}$

Find L_s , C_s and R_s for Critically damped case, for $\frac{1}{3}$ of S/N period and if discharge curr limited to 5% of load curr.

Power loss due to capacitor.

Ans:

$$L_s = \frac{V_s}{I_L} t_s = \frac{400}{100} * 1 * 10^{-6} = [4 \text{ mH}]$$

$$C_s = \frac{I_L}{V_s} t_f = \frac{100}{400} * 3 * 10^{-6} = [0.75 \mu\text{F}]$$

$$R_s = 2 \sqrt{\frac{L_s}{C_s}} = 2 \sqrt{\frac{4}{0.75}} = [4.62 \Omega]$$

$$R_s = \frac{1}{3 C_s f_s} = \frac{1}{3 * 0.75 * 10^{-6} * 20 * 10^3} \\ = [22.2 \Omega]$$

$$R_s = \frac{V_s}{0.05 I_L} = \frac{400}{0.05 * 100} = [80 \Omega]$$

$$P_s = \frac{1}{2} C_s V_s^2 f_s = \frac{1}{2} * 0.75 * 10^{-6} * 400^2 * 20 * 10^3 \\ = [1200 \text{ W}]$$

~~Stamps~~:

Jan Feb 2006 7 mks

Prob ③: A MOSFET is operated as a Chopper switch at a frequency of $f_s = 50 \text{ kHz}$. The DC input voltage is 30V, and the load current $I_L = 40 \text{ A}$. The switching times $t_g = 60 \text{ ns}$, $t_f = 25 \text{ ns}$. Find the snubber parameters including power loss. $I_{\text{switch}} = 5 \text{ A}$.

$$\text{Ans: } L_s = \frac{V_s}{I_L} t_g = \frac{30}{40} * 60 * 10^{-9} = 45 \text{ nH.}$$

$$C_s = \frac{I_L}{V_s} t_f = \frac{40}{30} * 25 * 10^{-9} = 33.33 \text{ nF.}$$

$$R_s = 2 \sqrt{\frac{L_s}{C_s}} = 2.32 \Omega$$

$$R_s = \frac{1}{3 C_s f_s} = \frac{1}{3 * 33.33 * 10^{-9} * 50 * 10^3} = 200 \Omega$$

$$R_s = \frac{V_s}{0.05 * 40} = 15 \Omega$$

$$P_s = \frac{1}{2} C_s V_s^2 f_s = \frac{1}{2} * 33.33 * 10^{-9} * 30^2 * 50 * 10^3 = 0.75 \text{ W.}$$

~~Stamp~~

[Jul Aug 2005] VTN 6mk8

Prob(4): In the circuit shown the BJT is acting as a chopper switch at a freq \Rightarrow 15KHz $E_{DC} = 240V$, load cur is 100A

The switching times are $t_r = 1.5\mu s$

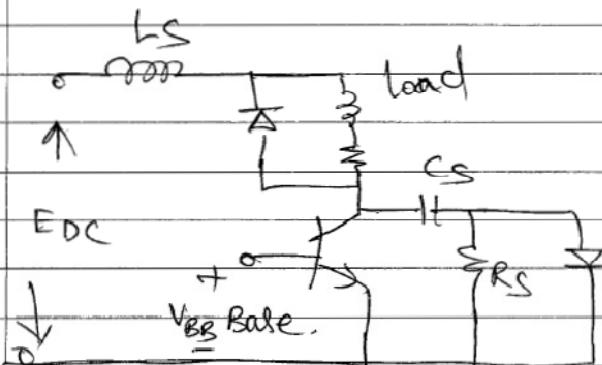
$t_f = 0.7\mu s$ Calculate & number values

Also R_s for ~~at~~ \approx d/c load cur of 5% of load cur.

Find Power loss neglecting inductor loss

Take $V_{CES} = 0$.

Ans:



Ans: $L_C = \frac{V_L}{I_L} t_r = [3.6 \text{ mH}]$

$C_S = \frac{I_L}{V_S} t_f = [0.29 \mu F]$

P-51

~~8pm 21:~~

$$R_s = 2 \sqrt{\frac{L_s}{C_s}} = [7 \Omega]$$

Critically
damped

$$R_s = \frac{1}{3 C_s f_s} = \frac{1}{3 \times 0.29 \times 10^{-6} \times 15 \times 10^3} \\ = [76.66 \Omega]$$

$$R_s = \frac{V_s}{0.05 I_L} = \frac{240}{0.05 \times 100} = [48 \Omega]$$

$$\text{Power loss } P_s = 0.5 C_s V_s^2 f_s = [125.28 \text{ W}]$$

Prob ⑤: A BJT is used as chopper switch at a freq of $f = 12 \text{ kHz}$ in the circuit shown in fig. The DC input voltage to the ckt is 230V, load cur $I_L = 100 \text{ A}$, The transistor switching times are $t_d = 0$, $t_r = 2.5 \mu\text{s}$, $t_f = 1 \mu\text{s}$ compute the values of snubber circuit chose discharge cur to be limited to 10%. If I_L Assume $V_{ces} = 0$

$$\text{Ans: } L_s = \frac{V}{I_L} t_r = 5.75 \mu\text{H}$$

$$C_s = \frac{I_L}{V} t_f = 0.435 \mu\text{F}$$

$$R_s = 2 \sqrt{\frac{L_s}{C_s}} = 7.27 \Omega$$

Critically
damped

$$R_s = \frac{1}{3f C_s} = 63.86 \Omega$$

$$R_s = \frac{V}{T_{dissn}} = \frac{230}{0.1 * 100} = \boxed{23 \Omega}$$

Power dissipated $P_s = \frac{1}{2} C_s V^2 f_s$
 $= \boxed{138.07 \text{ W}}$

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