

### Wave Impedance ( $Z_0$ )

$$\frac{E}{H} = \mu_0 c \quad \text{also} \quad \frac{E}{H} = \frac{1}{\epsilon_0 c}$$

The ratio of ~~E~~ magnitude of  $E$  to  $H$  is  $\text{F/m}$  called impedance ( $Z_0$ ). i.e.  $E_0 = 8.85 \times 10^{-12} \text{ C}^2/(\text{N}\cdot\text{m}^2)$   
 $\mu_0 = 4\pi \times 10^{-7} \text{ N/A}^2 = \text{Henry/m}$

$$Z_0 = \left| \frac{E}{H} \right| = \frac{E_0}{H_0} = \mu_0 c = \sqrt{\frac{\mu_0}{\epsilon_0}} \quad (\because c = \frac{1}{\sqrt{\mu_0 \epsilon_0}})$$

$$= \sqrt{\frac{4\pi \times 10^{-7}}{8.85 \times 10^{-12}}} = 376.6 \text{ ohm} \approx 377 \Omega \quad \text{✓ (see next page)}$$

Since the ratio  $Z_0 = \frac{E_0}{H_0}$  is real & positive this implies that field vectors  $\vec{E}$  &  $\vec{H}$  are in the same phase i.e. they have the same relative magnitude at all points at all times.

The Poynting Vector, which is <sup>the</sup> energy flow per unit area per unit time for a plane e.m. wave is given by

$$\vec{S} = \vec{E} \times \vec{H} = \vec{E} \times \frac{\hat{n} \times \vec{E}}{\mu_0 c} \quad [\text{using eqn. 9}]$$

$$= \frac{1}{\mu_0 c} \vec{E} \times (\hat{n} \times \vec{E}) = \frac{1}{\mu_0 c} [(\vec{E} \cdot \vec{E}) \hat{n} - (\vec{E} \cdot \hat{n}) \vec{E}]$$

Since  $\vec{E} \cdot \hat{n} = 0$  because both being perp.

$$\therefore \vec{S} = \frac{1}{\mu_0 c} \vec{E}^2 \hat{n} = \frac{\vec{E}^2}{Z_0} \hat{n} \quad [\because Z_0 = \mu_0 c]$$

For a plane e.m. w. of ang. freq  $\omega$ , the average value of  $S$  over a complete cycle is given by

$$\langle S \rangle = \frac{1}{Z_0} \langle E^2 \rangle \hat{n} = \frac{1}{Z_0} \langle (E_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)})^2 \rangle_{\text{real}} \hat{n}$$

$$= \frac{1}{Z_0} E_0^2 \langle \cos^2(\omega t - \vec{k} \cdot \vec{r}) \rangle \hat{n}$$

$$= \frac{1}{Z_0} \frac{E_0^2}{2} \hat{n} \quad [\because \langle \cos^2 \omega t - \vec{k} \cdot \vec{r} \rangle = \frac{1}{2}]$$

$$= \frac{1}{Z_0} E_{\text{rms}}^2 \hat{n} \quad \text{--- (1) Since } E_{\text{rms}} = \frac{E_0}{\sqrt{2}}.$$

## Plane e.m. waves in Conducting medium

In conducting medium

$$D = \epsilon E, \quad B = \mu H, \quad J = \underset{\substack{\downarrow \\ \text{conductivity}}}{\sigma} E; \quad \rho = 0 = \text{charge density.}$$

[ $\rho = 0$ ,  $\therefore$  there is no net charge within a conductor because the charge resides on the surface of the conductor]. Therefore

Maxwell's eqn. becomes

$$\vec{\nabla} \cdot \vec{D} = \nabla \cdot E = 0 \quad \text{--- (1)}$$

$$\vec{\nabla} \cdot \vec{B} = 0 \quad \text{--- (2)}$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial B}{\partial t} \quad \text{or} \quad \nabla \times E = -\mu \frac{\partial H}{\partial t} \quad \text{--- (3)}$$

$$\vec{\nabla} \times \vec{H} = J + \frac{\partial D}{\partial t} \quad \text{or} \quad \nabla \times H = \sigma E + \epsilon \frac{\partial E}{\partial t} \quad \text{--- (4)}$$

Taking curl of eqn (3) we get

$$\nabla \times (\nabla \times E) = -\mu \frac{\partial}{\partial t} (\nabla \times H)$$

Putting the value of  $(\nabla \times H)$  from eqn. (4) we get-

$$\nabla \times (\nabla \times E) = -\mu \frac{\partial}{\partial t} \left( \sigma E + \epsilon \frac{\partial E}{\partial t} \right)$$

$$\text{or, } \nabla \times (\nabla \times E) = -\mu \sigma \frac{\partial E}{\partial t} - \mu \epsilon \frac{\partial^2 E}{\partial t^2} \quad \text{--- (5)}$$

$$\text{Now } \nabla \times (\nabla \times E) = \nabla (\nabla \cdot E) - \nabla^2 E$$

$$\text{But } \vec{\nabla} \cdot \vec{E} = 0 \text{ from eqn. (1)}$$

$\therefore$  Eqn. (5) becomes

$$\text{or, } \boxed{\nabla^2 E - \mu \sigma \frac{\partial E}{\partial t} - \mu \epsilon \frac{\partial^2 E}{\partial t^2} = 0} \quad \begin{array}{l} \text{--- (6a)} \\ \text{In one dimension.} \\ \text{--- (6b)} \end{array}$$

(12)

Similarly by taking curl of eqn. (4) & then using eqn (3) we get

$$\boxed{\nabla^2 H - \mu\sigma \frac{\partial H}{\partial t} - \mu\epsilon \frac{\partial^2 H}{\partial t^2} = 0} \quad \text{--- (7(a))}$$

or In one dimension

$$\boxed{\frac{\partial^2 H}{\partial x^2} - \mu\sigma \frac{\partial H}{\partial t} - \mu\epsilon \frac{\partial^2 H}{\partial t^2} = 0} \quad \text{--- (7(b))}$$

Eqn. (6) & (7) are plane e.m. wave eqns. in conducting medium. An e.m. wave is rapidly attenuated in a conducting medium. In fact in a good conductor the attenuation is so rapid that at high radio frequencies the wave penetrates the conductor to a very small depth.

### Plane-Wave

The plane waves are those waves which are travelling in one direction, i.e. <sup>say,</sup> in the  $\hat{z}$  direction, and have no  $x$  &  $y$  dependency and their amplitude is same at any point in a plane  $\perp$  to the direction of propagation.

### Plane e.m. wave in conducting medium:

The three dimensional wave eqn. for a conducting medium is given by

$$\nabla^2 E - \mu\epsilon \frac{\partial^2 E}{\partial t^2} - \mu\sigma \frac{\partial E}{\partial t} = 0 \quad \text{or, } \nabla^2 H - \mu\epsilon \frac{\partial^2 H}{\partial t^2} - \mu\sigma \frac{\partial H}{\partial t} = 0$$

$$\text{or, } \frac{\partial^2 E}{\partial x^2} + \frac{\partial^2 E}{\partial y^2} + \frac{\partial^2 E}{\partial z^2} - \mu\epsilon \frac{\partial^2 E}{\partial t^2} - \mu\sigma \frac{\partial E}{\partial t} = 0 \quad \text{--- (1)}$$

(P.T.O.)

In one dimension we have

$$\frac{\partial^2 E}{\partial x^2} - \mu\sigma \frac{\partial E}{\partial t} - \mu\epsilon \frac{\partial^2 E}{\partial t^2} = 0 \quad \text{--- (1a)}$$

$$\frac{\partial^2 H}{\partial x^2} - \mu\sigma \frac{\partial H}{\partial t} - \mu\epsilon \frac{\partial^2 H}{\partial t^2} = 0 \quad \text{--- (1b)}$$

Let us consider a plane e.m. wave propagating in  $z$  direction with  $\vec{E}$  in  $x$  direction & vector  $\vec{H}$  in  $y$  direction. Then

$$\frac{\partial(E_x \text{ or } H_y)}{\partial x} = \frac{\partial(E_x \text{ or } H_y)}{\partial y} = 0 \quad \& \quad E = E_x \hat{a}_x \quad \& \quad H = H_y \hat{a}_y$$

Therefore eqn(1) can be written as

$$\frac{\partial^2 E_x}{\partial z^2} = \mu\epsilon \frac{\partial^2 E_x}{\partial t^2} + \mu\sigma \frac{\partial E_x}{\partial t} \quad \text{--- (2)}$$

The solution of eqn(2) may be expressed as

$$E = E_0 e^{i(K \cdot z - \omega t)} \quad \text{or} \quad H = H_0 e^{i(K \cdot z - \omega t)} \quad \text{--- (3)}$$

where  $K = \text{propagation vector} = \frac{2\pi}{\lambda} \hat{n}$ ;  $\hat{n} = \text{unit vector along propagation (z) direction.}$

$$\text{Now, } \frac{\partial E}{\partial z} = iK E \quad \& \quad \frac{\partial^2 E}{\partial z^2} = (iK)^2 E = -K^2 E$$

$$\frac{\partial E}{\partial t} = -i\omega E \quad \& \quad \frac{\partial^2 E}{\partial t^2} = -\omega^2 E$$

Putting these values in eqn (2) we get

$$(-K^2 + \mu\epsilon\omega^2 + i\mu\sigma\omega) E = 0$$

Since  $E$  is arbitrary so,

$$(-K^2 + \mu\epsilon\omega^2 + i\mu\sigma\omega) = 0;$$

See page 12(i)  
first



(12ii)

$$\frac{\partial^2 E_x}{\partial z^2} = -K^2 E_x \quad (1*)$$

$$\& \frac{\partial^2 E_x}{\partial z^2} = \mu \epsilon (-\omega^2 E) + \mu \sigma (-i\omega E_x)$$

$$\Rightarrow \frac{\partial^2 E_x}{\partial z^2} = -[\mu \epsilon \omega^2 + i\mu \sigma \omega] E_x \quad (2*)$$

Comparing eqns (1\*) & (2\*) we get where

$$K^2 = \mu \epsilon \omega^2 + i\mu \sigma \omega. \quad (3*)$$

$$\text{Let } K = \alpha + i\beta \quad (4*)$$

$$\because K^2 = \alpha^2 - \beta^2 + 2i\alpha\beta$$

On solving above eqns we get expressions of  $\alpha$  &  $\beta$ .

$\therefore$  The required solution is

$$E = E_0 e^{i(\alpha + i\beta)\hat{n} \cdot \vec{z} - i\omega t}$$

$$\text{or, } E = E_0 e^{-\beta \hat{n} \cdot \vec{z}} e^{i(\alpha \hat{n} \cdot \vec{z} - \omega t)} \quad (5*)$$

From eqn (5\*), it is obvious that field amplitudes are attenuated due to the presence of the term  $e^{-\beta \hat{n} \cdot \vec{z}}$ . The quantity  $\beta$  is a measure of attenuation & is known as absorption co-efficient. Greater the value of  $\beta$  greater is the attenuation. The term  $1/\beta$ , measures the depth at which electric field of wave entering a conductor is damped to  $[e=2.718]$   $1/e = 0.367$  times of its initial amplitude at the surface. This depth is called skin depth or penetration depth denoted by  $\delta$ .

$$\delta = \frac{1}{\beta} = \sqrt{\frac{2}{\mu \sigma \omega}} \quad \text{for good conductor. For perfect}$$

conductor  $\sigma = \infty$  &  $\delta = 0$ .

(P.T.O.)

If  $\delta$  be the penetration depth or skin depth

$$\Rightarrow E_0 e^{-\beta z} = \frac{E_0}{e}$$

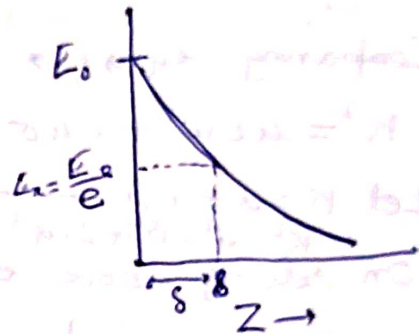
$$\Rightarrow e^{-\beta z} = e^{-1} \Rightarrow \beta z = 1 \quad \alpha, \quad z = \frac{1}{\beta} \quad \alpha, \quad \beta = \frac{1}{z} = \frac{1}{\delta}$$

$$\boxed{\beta = \frac{1}{z} = \frac{1}{\delta}}$$

For good conductor  $\alpha = \beta$

$$\alpha = \beta = \sqrt{\frac{\mu \sigma \omega}{2}}$$

$$\therefore \boxed{\delta = \frac{1}{\beta} = \sqrt{\frac{2}{\mu \sigma \omega}}}$$



∴ The required solution is

$$\left. \begin{aligned} E &= E_0 e^{i(\alpha + i\beta)\hat{n}\cdot\vec{z} - i\omega t} \\ H &= H_0 e^{i(\alpha + i\beta)\hat{n}\cdot\vec{z} - i\omega t} \end{aligned} \right\} \text{ or } \left. \begin{aligned} E &= E_0 e^{-\beta\hat{n}\cdot\vec{z}} e^{i(\alpha\hat{n}\cdot\vec{z} - \omega t)} \\ H &= H_0 e^{-\beta\hat{n}\cdot\vec{z}} e^{i(\alpha\hat{n}\cdot\vec{z} - \omega t)} \end{aligned} \right\}$$

From eqn(7), it is obvious that field amplitudes (7) are attenuated due to the presence of the term  $e^{-\beta\hat{n}\cdot\vec{z}}$ . The quantity  $\beta$  is a measure of attenuation & is known as absorption co-efficient.

For poor conductor  $\frac{\sigma}{\omega\epsilon} \ll 1$  & for good conductor  $\frac{\sigma}{\omega\epsilon} \gg 1$

∴ For good conductor

$$\alpha = \beta = \omega \sqrt{\frac{\mu\epsilon}{2}} \left[ \frac{\sigma}{\omega\epsilon} \right]^{1/2} = \sqrt{\frac{\omega\mu\sigma}{2}}$$

Greater the value of  $\beta$ , greater is the attenuation. The term  $\frac{1}{\beta}$ , measures the depth at which electric field of wave entering a conductor is damped to  $1/e = 0.367$  times of its initial amplitude at the surface. This depth is called skin depth or penetration depth denoted by  $\delta$  [e=2.718]

$$\boxed{\delta = \frac{1}{\beta} = \sqrt{\frac{2}{\omega\mu\sigma}}} \text{ for good conductor. For perfect conductor } \sigma = \infty \text{ (infinity) } \& \delta = 0$$

For poor conductor or good di-electrics

$$\frac{\sigma}{\omega\epsilon} \ll 1, \text{ Now } \beta = \omega \sqrt{\frac{\mu\epsilon}{2}} \left[ \left( 1 + \frac{\sigma^2}{\omega^2\epsilon^2} \right)^{1/2} - 1 \right]^{1/2} \quad (8)$$

As  $\frac{\sigma}{\omega\epsilon} \ll 1$ , ∴ By Binomial expansion we have

$$\left( 1 + \frac{\sigma^2}{\omega^2\epsilon^2} \right)^{1/2} = 1 + \frac{\sigma^2}{2\omega^2\epsilon^2} + \dots$$

∴ Eqn (8) becomes

$$\beta = \omega \sqrt{\frac{\mu\epsilon}{2}} \left[ 1 + \frac{\sigma^2}{2\omega^2\epsilon^2} + \dots - 1 \right]^{1/2} = \omega \sqrt{\frac{\mu\epsilon}{2}} \left( \frac{\sigma}{\omega\epsilon} \right)$$

$$\therefore \boxed{\beta = \frac{\sigma}{2} \sqrt{\frac{\mu}{\epsilon}}} \quad \therefore \boxed{\delta = \frac{1}{\beta} = \frac{2}{\sigma} \sqrt{\frac{\epsilon}{\mu}}} \rightarrow \text{Skin depth}$$

depth is independent of frequency. For di-electric, the skin



## Poynting Vector ( $\vec{S}$ )

Poynting vector ( $\vec{S}$ ) is the energy flow per unit area per unit time for a plane e.m. wave, & is given by  $\vec{S} = \vec{E} \times \vec{H}$ , its unit is Watts/m<sup>2</sup>.

### Poynting Theorem Vector

At any point in electromagnetic field, the product of electric field intensity  $\vec{E}$  & mag. field intensity  $\vec{H}$  is a measure of rate of energy flow at that point. Mathematically,  $\vec{S} = \vec{E} \times \vec{H}$ , the direction of energy flow is perpendicular to  $\vec{E}$  &  $\vec{H}$  i.e. along the direction of propagation of e.m. wave.

Proof: By Maxwell's 3<sup>rd</sup> & 4<sup>th</sup> eqn. we have

$$\vec{\nabla} \times \vec{E} = -\mu \frac{\partial \vec{H}}{\partial t} \quad \text{--- (1)}$$

$$\vec{\nabla} \times \vec{H} = \vec{J} + \epsilon \frac{\partial \vec{E}}{\partial t} \quad \text{--- (2)}$$

by taking dot product with  $\vec{H}$  on both sides of eqn(1)  
& " " " " "  $\vec{E}$  " " " " eqn(2), we get

$$\vec{H} \cdot (\vec{\nabla} \times \vec{E}) = -\mu \vec{H} \cdot \frac{\partial \vec{H}}{\partial t} \quad \text{--- (3)}$$

$$\vec{E} \cdot (\vec{\nabla} \times \vec{H}) = \vec{E} \cdot \vec{J} + \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} \quad \text{--- (4)}$$

Subtracting eqn.(4) from eqn(3) we get:

$$\vec{H} \cdot (\vec{\nabla} \times \vec{E}) - \vec{E} \cdot (\vec{\nabla} \times \vec{H}) = -\mu \vec{H} \cdot \frac{\partial \vec{H}}{\partial t} - \vec{E} \cdot \vec{J} - \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} \quad \text{--- (5)}$$

By Vector identity we know that.

$$\vec{H} \cdot (\vec{\nabla} \times \vec{E}) - \vec{E} \cdot (\vec{\nabla} \times \vec{H}) = \vec{\nabla} \cdot (\vec{E} \times \vec{H}).$$

$\therefore$  Eqn.(5) becomes

$$\vec{\nabla} \cdot (\vec{E} \times \vec{H}) = -\vec{E} \cdot \vec{J} - \mu \vec{H} \cdot \frac{\partial \vec{H}}{\partial t} - \epsilon \vec{E} \cdot \frac{\partial \vec{E}}{\partial t} \quad \text{--- (6)}$$

P.T.O.



By Calculus we know that

$$\nabla \cdot \frac{\partial \mathbf{H}}{\partial t} = \frac{1}{2} \frac{\partial}{\partial t} (\mathbf{H} \cdot \mathbf{H}) = \frac{\partial}{\partial t} \left( \frac{1}{2} \mathbf{H}^2 \right), \therefore \nabla \cdot (\mathbf{H} \times \frac{\partial \mathbf{H}}{\partial t}) = \frac{\partial}{\partial t} \left( \frac{1}{2} \mathbf{H}^2 \right)$$

Similarly  $\nabla \cdot (\mathbf{E} \times \frac{\partial \mathbf{E}}{\partial t}) = \frac{\partial}{\partial t} \left( \frac{1}{2} \mathbf{E}^2 \right)$

$\therefore$  Eqn (6) becomes

$$\nabla \cdot (\mathbf{E} \times \mathbf{H}) = -\mathbf{E} \cdot \mathbf{J} - \frac{\partial}{\partial t} \left( \frac{1}{2} \mathbf{E}^2 + \frac{1}{2} \mathbf{H}^2 \right) \quad \text{--- (7)}$$

By taking volume integral of both sides we get

$$\oint_V \nabla \cdot (\mathbf{E} \times \mathbf{H}) dV = - \oint_V \mathbf{E} \cdot \mathbf{J} dV - \frac{\partial}{\partial t} \oint_V \left( \frac{1}{2} \mathbf{E}^2 + \frac{1}{2} \mathbf{H}^2 \right) dV \quad \text{--- (8)}$$

Using Divergence theorem on L.H.S. of eqn (8) we have

$$\oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} + \oint_V \mathbf{E} \cdot \mathbf{J} dV = - \frac{\partial}{\partial t} \oint_V \left( \frac{1}{2} \mathbf{E}^2 + \frac{1}{2} \mathbf{H}^2 \right) dV \quad \text{--- (9)}$$

Let us discuss each terms

- (i) The term  $\oint_V (\mathbf{E} \cdot \mathbf{J}) dV$  represent instantaneous power dissipated in volume  $V$  [  $E = \frac{\text{Voltage}}{\text{Distance}} = \frac{V}{d}$  &  $J = \frac{I}{A}$    
  $\therefore \mathbf{E} \cdot \mathbf{J} = \frac{VI}{Ad} = \text{power loss in unit volume} = I^2 R$  ]

- (ii)  $-\frac{\partial}{\partial t} \oint_V \left( \frac{1}{2} \mathbf{E}^2 + \frac{1}{2} \mathbf{H}^2 \right) dV$  = The rate of decrease of total stored energy in volume  $V$ .  
Electric energy density      Mag. energy density

- (iii)  $\oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S}$ , gives the rate of flow of energy outward through the surface.

The product  $\mathbf{E} \times \mathbf{H} = \vec{S}$ , is a measure of rate of energy flow per unit area.  $\vec{S}$  is called Poynting vector. Thus the integral of  $\vec{S}$  over a closed surface represent the rate at which electromagnetic energy crosses the closed surface.

Poynting theorem states that: The work done on the charge by an electromagnetic force is equal to the decrease in energy stored in the field & work done less than the energy which flowed out the surface. It is also called conservation law in electrodynamics.