

Tutorial Problem Set
(Based on Magnetostatics)

Q. 1 A current I is uniformly distributed over a wire of circular cross-section, with radius R . Find the surface and volume current densities.

Sol. (i) Here, it is obvious that length \perp ar to the current flow is $2\pi R$ and therefore,

$$dl_{\perp} = 2\pi R$$

$$\text{and } K = I/dl_{\perp} = I/2\pi R$$

(ii) Here also area \perp ar to the current flow is πR^2 and therefore,

$$da_{\perp} = \pi R^2$$

$$\text{and } K = I/da_{\perp} = I/\pi R^2$$

Q. 2 (a) The volume current density in a wire of radius R is proportional to the distance from the axis is given by

$$\vec{J} = k\vec{r}$$

for some constant k . Find the total current in the wire.

(b) Find the total current if the volume current density is inversely proportional to the distance from the axis.

Sol. (a) We have,
$$I = \int_S \vec{J} \cdot d\vec{a} = \int_S (kr)(r dr d\phi) = k \left(\int_{r=0}^R r^2 dr \right) \left(\int_{\phi=0}^{2\pi} d\phi \right) = k \cdot \frac{R^3}{3} \cdot 2\pi = \frac{2\pi k R^3}{3}$$

(b) Here, $J = \frac{k}{r}$ so
$$I = \int_S \vec{J} \cdot d\vec{a} = \int_S \left(\frac{k}{r} \right) (r dr d\phi) = k \left(\int_{r=0}^R dr \right) \left(\int_{\phi=0}^{2\pi} d\phi \right) = k \cdot R \cdot (2\pi) = 2\pi k R$$

Q. 3 Suppose the magnetic field in some region has the form

$$\vec{B} = kz\hat{x} \quad (k \text{ is some constant})$$

Find the force on a square loop of side s , lying in the yz plane, centered at the origin, which carries a current I .

$$[Ika^2\hat{z}]$$

Sol. Let I flows in anti-clockwise direction.

The force on the left side (towards the left) cancels the force on the right side (towards the right).

The force on the top is $IsB = Isk(s/2) = Iks^2/2$, (pointing upwards), and

the force on the bottom is $IsB = -Iks^2/2$ (also points upwards).

\therefore the net force is $\vec{F} = (Iks^2/2 + Iks^2/2) = Iks^2\hat{z}$.

Q. 4 For a configuration of charges and currents confined within a volume V , show that

$$\int_V \vec{J} d\tau = \frac{d\vec{p}}{dt},$$

where \vec{p} is the total dipole moment. [Hint: Evaluate $\int_V \vec{\nabla} \cdot (x\vec{J}) d\tau$]

Sol. Here, $\frac{d\vec{p}}{dt} = \frac{d}{dt} \int_V \rho \vec{r} d\tau = \int_V \left(\frac{\partial \rho}{\partial t} \right) \vec{r} d\tau = - \int_V (\vec{\nabla} \cdot \vec{J}) \vec{r} d\tau \quad \dots (i)$

(using continuity equation)

Using the product rule,

$$\vec{\nabla} \cdot (x\vec{J}) = x(\vec{\nabla} \cdot \vec{J}) + \vec{J} \cdot (\vec{\nabla} x) = x(\vec{\nabla} \cdot \vec{J}) + J_x$$

Thus $\int_V (\vec{\nabla} \cdot \vec{J}) x d\tau = \int_V \vec{\nabla} \cdot (x\vec{J}) d\tau - \int_V J_x d\tau$

The first term $\int_V \vec{\nabla} \cdot (x\vec{J}) d\tau = \int_S x\vec{J} \cdot d\vec{a}$, by divergence theorem.

Since, \vec{J} is entirely inside V, it is zero on the surface S.

$$\therefore \int_V (\vec{\nabla} \cdot \vec{J}) x d\tau = - \int_V J_x d\tau \quad \dots (ii)$$

Similarly, $\int_V (\vec{\nabla} \cdot \vec{J}) y d\tau = - \int_V J_y d\tau \quad \dots (iii)$

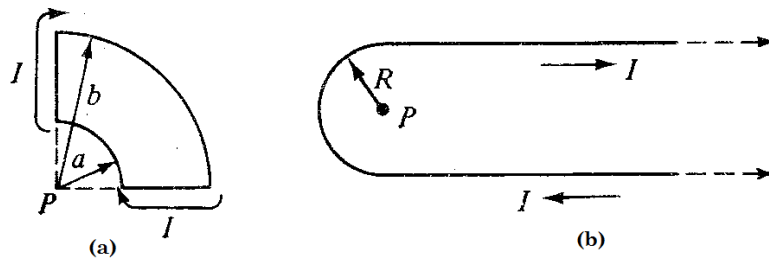
and $\int_V (\vec{\nabla} \cdot \vec{J}) z d\tau = - \int_V J_z d\tau \quad \dots (iv)$

Combining (ii), (iii) and (iv), we get

$$\int_V (\vec{\nabla} \cdot \vec{J}) \vec{r} d\tau = - \int_V \vec{J} d\tau \quad \dots (v)$$

From (i) and (v), $\frac{d\vec{p}}{dt} = \int_V \vec{J} d\tau$

Q. 5 Find the magnetic field at point P for each of the steady current



configurations shown in Fig.

Sol. (a) The straight line segments produce no field at P. The two quarter-circles give

$$\vec{B} = \frac{\mu_0 I}{8} \left(\frac{1}{a} - \frac{1}{b} \right)$$

out of the page.

(b) The two half-lines are the same as one infinite line which has magnetic field as

$$B = \frac{\mu_0 I}{2\pi R}$$

and the half-circle contribution is

$$B_{half} = \frac{\mu_o I}{8R}$$

so $B = \frac{\mu_o I}{4R} \left(1 + \frac{2}{\pi}\right)$ directed into the page perpendicular to it.

Q. 6 A steady current I flows down a long cylindrical wire of radius R . Find the magnetic field, both inside and outside the wire, if

(a) The current is uniformly distributed over the outside surface of the wire;

(b) The current is distributed in such a way that J is proportional to r , the distance from the axis.

$$\text{Sol. (a)} \quad \oint \vec{B} \cdot d\vec{l} = B(2\pi r) = \mu_o I_{enc} \quad \Rightarrow \vec{B} = \begin{cases} 0, & \text{for } r < R; \\ \frac{\mu_o I}{2\pi r} \hat{\phi} & \text{for } r > R. \end{cases}$$

$$\text{(b)} \quad J = kr; \quad I = \int_0^R J da = \int_0^R kr(2\pi r) dr = \frac{2\pi k R^3}{3} \quad \Rightarrow k = \frac{3I}{2\pi R^3}$$

$$\text{Now, } I_{enc} = \int_0^r J da = \int_0^r kr'(2\pi r') dr' = \frac{2\pi k r^3}{3} = I \frac{r^3}{R^3}, \text{ for } r < R; I_{enc} = I, \text{ for } r > R$$

$$\text{So} \quad \vec{B} = \begin{cases} \frac{\mu_o I r^2}{2\pi R^3} \hat{\phi}, & \text{for } r < R; \\ \frac{\mu_o I}{2\pi r} \hat{\phi} & \text{for } r > R. \end{cases}$$

Q. 7 What current density would produce a constant azimuthal potential, $A_\phi = k$, in cylindrical co-ordinates?

Sol.

$$A_\phi = k \Rightarrow \vec{B} = \nabla \times \vec{A} = \frac{1}{s} \frac{\partial}{\partial s} (sk) \hat{z} = \frac{k}{s} \hat{z}; \quad \vec{J} = \frac{1}{\mu_o} (\nabla \times \vec{B}) = \frac{1}{\mu_o} \left[-\frac{\partial}{\partial s} \left(\frac{k}{s} \right) \right] \hat{\phi} = \boxed{\frac{k}{\mu_o s^2} \hat{\phi}}.$$

Q. 8 If \vec{B} is uniform, show that $\vec{A} = -\frac{1}{2}(\vec{r} \times \vec{B})$, where \vec{r} is a vector from the origin to the point in question. That is, check that $\vec{\nabla} \cdot \vec{A} = 0$ and $\vec{\nabla} \times \vec{A} = \vec{B}$.
Sol.

$$\vec{\nabla} \cdot \vec{A} = -\frac{1}{2} \vec{\nabla} \cdot (\vec{r} \times \vec{B}) = -\frac{1}{2} [\vec{B} \cdot (\vec{\nabla} \times \vec{r}) - \vec{r} \cdot (\vec{\nabla} \times \vec{B})] = 0,$$

since $\vec{\nabla} \times \vec{B} = 0$ (\vec{B} is uniform) and $\vec{\nabla} \times \vec{r} = 0$

$$\vec{\nabla} \times \vec{A} = -\frac{1}{2} \vec{\nabla} \times (\vec{r} \times \vec{B}) = -\frac{1}{2} [(\vec{B} \cdot \vec{\nabla})\vec{r} - (\vec{r} \cdot \vec{\nabla})\vec{B} + \vec{r}(\vec{\nabla} \cdot \vec{B}) - \vec{B}(\vec{\nabla} \cdot \vec{r})].$$

But $(\vec{r} \cdot \vec{\nabla})\vec{B} = 0$ and $\vec{\nabla} \cdot \vec{B} = 0$ (since \vec{B} is uniform), and

$$\nabla \cdot \mathbf{r} = \frac{\partial x}{\partial x} + \frac{\partial y}{\partial y} + \frac{\partial z}{\partial z} = 1 + 1 + 1 = 3.$$

$$\text{Finally, } (\mathbf{B} \cdot \nabla) \mathbf{r} = \left(B_x \frac{\partial}{\partial x} + B_y \frac{\partial}{\partial y} + B_z \frac{\partial}{\partial z} \right) (x \hat{\mathbf{x}} + y \hat{\mathbf{y}} + z \hat{\mathbf{z}}) = B_x \hat{\mathbf{x}} + B_y \hat{\mathbf{y}} + B_z \hat{\mathbf{z}} = \mathbf{B}.$$

$$\text{So } \nabla \times \mathbf{A} = -\frac{1}{2}(\mathbf{B} - 3\mathbf{B}) = \mathbf{B}.$$

Q. 9 Find the vector potential above and below an infinite plane surface current $\vec{K} = K\hat{i}$ covering the xy plane.

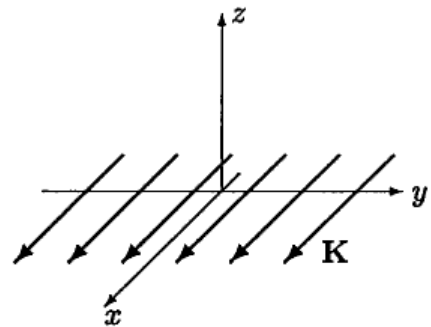
Sol.

$$\mathbf{K} = K \hat{\mathbf{x}} \Rightarrow \mathbf{B} = \pm \frac{\mu_0 K}{2} \hat{\mathbf{y}} \text{ (plus for } z < 0, \text{ minus for } z > 0).$$

\mathbf{A} is parallel to \mathbf{K} , and depends only on z , so $\mathbf{A} = A(z) \hat{\mathbf{x}}$.

$$\mathbf{B} = \nabla \times \mathbf{A} = \begin{vmatrix} \hat{\mathbf{x}} & \hat{\mathbf{y}} & \hat{\mathbf{z}} \\ \partial/\partial x & \partial/\partial y & \partial/\partial z \\ A(z) & 0 & 0 \end{vmatrix} = \frac{\partial A}{\partial z} \hat{\mathbf{y}} = \pm \frac{\mu_0 K}{2} \hat{\mathbf{y}}.$$

$$\boxed{\mathbf{A} = -\frac{\mu_0 K}{2} |z| \hat{\mathbf{x}}}$$



Q. 10 The magnetic vector potential at any point due to a dipole of magnetic moment \vec{m} pointing in the z -direction is given by

$$\vec{A}_{dip} = \frac{\mu_0}{4\pi} \frac{m \sin \theta}{r^2} \hat{\phi}$$

Calculate the magnetic field \vec{B}_{dip} at that point.

Sol. We have $\text{Curl } \vec{A} =$

$$\frac{1}{r \sin \theta} \left(\frac{\partial}{\partial \theta} (A_\phi \sin \theta) - \frac{\partial A_\theta}{\partial \phi} \right) \hat{\mathbf{r}} + \frac{1}{r} \left(\frac{1}{\sin \theta} \frac{\partial A_r}{\partial \phi} - \frac{\partial}{\partial r} (r A_\phi) \right) \hat{\theta} + \frac{1}{r} \left(\frac{\partial}{\partial r} (r A_\theta) - \frac{\partial A_r}{\partial \theta} \right) \hat{\phi}$$

Here, $A_\phi = \frac{\mu_0}{4\pi} \frac{m \sin \theta}{r^2}$, which on putting in above equation gives

$$\vec{B} = \frac{\mu_0 m}{4\pi r^3} (2 \cos \theta \hat{\mathbf{r}} + \sin \theta \hat{\theta})$$