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[FAQ] How do I design a pulse width modulator (PWM) circuit using LMC555, TLC555, LM555, NA555, NE555, SA555, or SE555?



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Other Parts Discussed in Thread: [LM293](#)

1. How does the PWM example in the data sheet work?
2. What are the limitations of the data sheet PWM example?
3. Is there a way to improve linearity and duty cycle range?

[over 5 years ago](#)



[Ron Michallick](#) [over 5 years ago](#)

[TI_Guru****](#) 165376 points

This FAQ covers PWM circuits. Figure 1 below shows a pulse width modulator using the [LM555](#), [NA555](#), [NE555](#), [SA555](#) and [SE555](#) timers that are called LM, NA, NE, SA and SE respectively hereafter. As a group they are called bipolar timers due to their design. This FAQ also covers [LMC555](#) and [TLC555](#) timers that will be called LMC and TLC respectively hereafter. As a group they are called CMOS timers due to their design. This FAQ is applicable to the xx556, [TLC551](#), and [TLC552](#) timers as well. Supply voltage pins for the timers use different symbols, namely V_S , V_{CC} , and V_{DD} , that have the same function.

Data sheet example circuit

The data sheets show this setup to implement a PWM using a 555 timer:

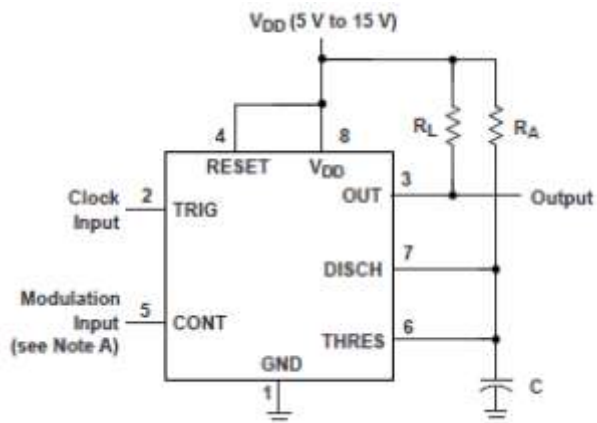


Figure 1. Data sheet example (pin 2 is input clock, F_I)

The circuit in Figure 1 is a mono-stable pulse generator that provides an output high time that is ideally $-R_A \cdot C \cdot \ln(1 - V_{CONT}/V_{DD})$. The output frequency will ideally match the clock input frequency, F_I . The resulting output duty cycle is $-R_A \cdot C \cdot \ln(1 - V_{CONT}/V_{DD})/F_I$. Therefore the output duty cycle varies with V_{CONT} in a non-linear fashion. The nonlinearity is a result of the timing capacitor ramp being an exponential curve. Duty cycle also varies with R_A , C and F_I .

The data sheet example uses values of $R_A = 3k\Omega$ and $C = 20nF$, which sets the RC time constant value, $R_A \cdot C$, to $60\mu s$. The example mentions that the $R_A \cdot C$ product is set to the clock period divided by four. In other words, the $240\mu s$ period is 4 times the $R_A \cdot C$ product. The control voltage to duty cycle transfer function for this setup can be seen in the $4RC = 1/F_I$ plot in figure 2. Clearly, the linearity is very poor. The results for $R_A \cdot C$ values that are closer to the input clock period, such as $RC = 1/F_I$ and $2RC = 1/F_I$, are more linear. Note that increasing the RC product also compresses the control voltage range. Figure 2 represents the ideal transfer function for different RC time constants relative to input clock period.

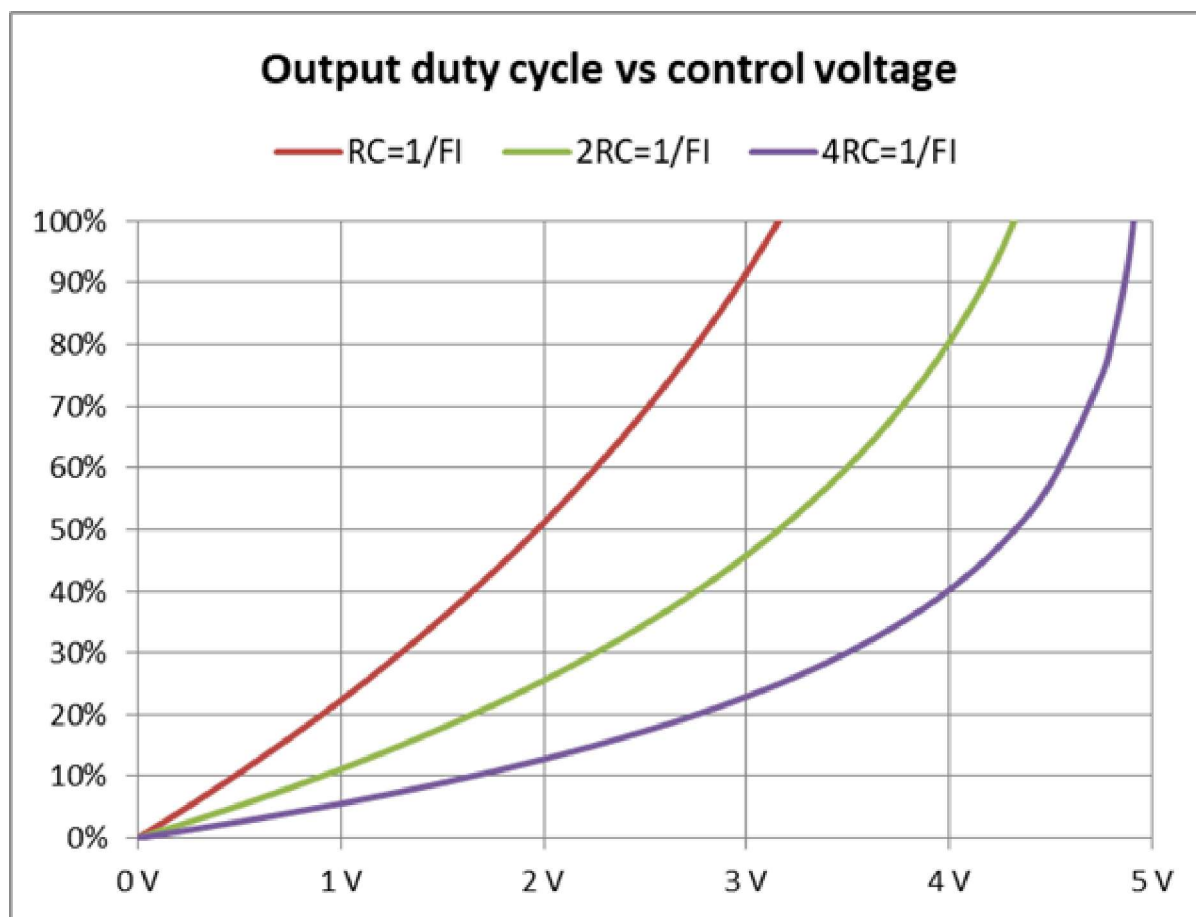


Figure 2. Duty cycle vs control voltage for various $R \cdot C$ products per timing period, $1/F_I$. $V_{DD} = 5V$

When designing a PWM signal with a 555 timer, there are additional limiting factors to consider. For example, the external clock driving the trigger input must have a low negative duty cycle, output low time percentage, because the PWM output minimum high time cannot be less than the input clock low time. The external clock can be generated with another 555 timer in an [a-stable](#) setup. Operation below 10% or near 100% duty cycle can cause extra or missing output pulses. In the latter case, duty cycle and output frequency drops in half. The minimum useful control voltage for LMC is 0.4V and the TLC minimum is 0.5V. Operation at lower control voltages will result in a duty cycle that is fixed or may cause an inconsistent pulse stream.

The bipolar timers have a storage delay of about 16 μ s which can limit the minimum duty cycle. The maximum duty cycle for these devices is limited to about 97%. Adjusting the control voltage to attempt a higher duty cycle will create an output that has frequency division. In such cases, the frequency is divided because there are missing output low pulses, resulting in a duty cycle near 50%. The bipolar timers also have increased threshold current when input voltage is close to V_{DD} . This input bias current can limit the high duty cycle maximum. Adding R_L can improve the V_{OH} level for the bipolar timers, but it is not required for any of them.

Using the data sheet example of $R_A = 3k$ and $C = 20nF$ with clock periods of 60 μ s, 120 μ s, 240 μ s results in the minimum duty cycles in table 1 and maximum duty cycles in table 2.

Period	NA	SE	LM	LMC	TLC
60 μ s	26 %	25 %	24 %	12 %	16 %
120 μ s	13 %	14 %	12 %	6 %	8 %
240 μ s	7 %	7 %	6 %	3 %	4 %
Limiter	16us	16us	15us	0.4V	0.5V

Table 1: Minimum duty cycle $R_A=3k$, $C=20nF$

The minimum duty cycle is limited by the 16 μ s delay of the bipolar timers and the control voltage minimum of the CMOS timers.

Period	NA	SE	LM	LMC	TLC
60 μ s	97 %	95 %	98 %	98 %	98 %
120 μ s	98 %	98 %	98 %	98 %	98 %
240 μ s	98 %	85 %	95 %	97 %	98 %

Table 2: Maximum duty cycle $R_A=3k$, $C=20nF$

The maximum duty cycle is limited by the occurrence of pulse skipping and also input current on the bipolar timers.

In summary, the data sheet pulse width modulator example is good for applications that are resistant to poor linearity and do not need to operate near 0% or 100% duty cycles.

Improved example circuit

Figure 3 is a much improved, but still imperfect, PWM generator. It uses a 50 percent fixed duty cycle 555 timer oscillator and a comparator. The [a-stable oscillator FAQ](#) describes how to make the 50% duty cycle oscillator. Alternatively use these formulas to choose components. $R_B * C = 0.481 / F$, $R_A = R_B / 2$, $R_D = 0.15 * R_A$, where F is the oscillator frequency. The comparator performs the DC input voltage to output PWM duty cycle conversion. The timing capacitor's charges and discharges are exponential ramps. However, both the rising and falling ramps are used for the conversion. Therefore, much of the non-linearity is removed. This circuit is useful down to 0% and up to 100% with the condition that the output frequency may be divided. But, the duty cycle will be correct, not 50% as will happen with the figure 1 schematic. R_1 , R_2 and R_3 scale the input voltage to between 1/3 to 2/3 V_{DD} to match the timing ramp

voltage range. The LM293 needs a VDD of at least 6V to keep the ramp voltage within the input common mode range.

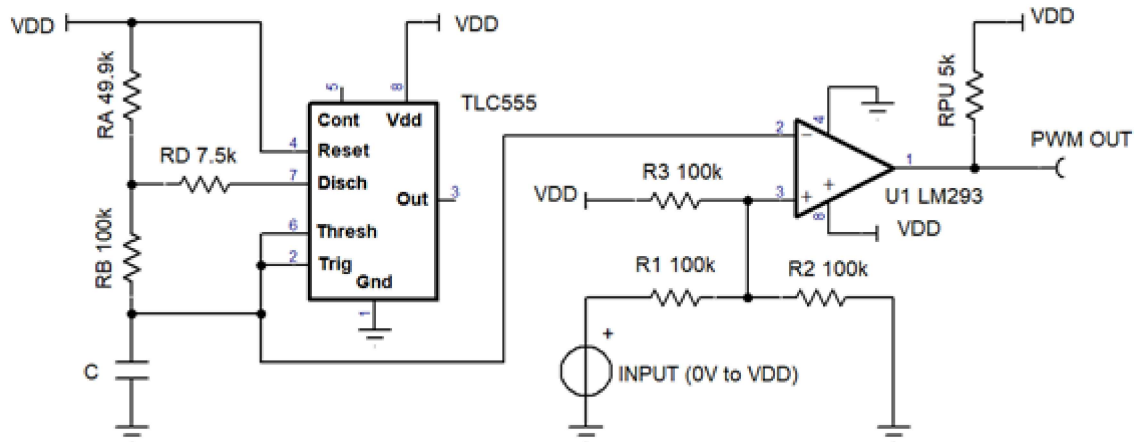


Figure 3. Improved linearity PWM circuit

Sample lab results for the figure 3 schematic are presented in figure 4. The dotted line represents an ideal linear transfer function. As can be seen, the output duty cycle of this circuit is more linear than the results from the circuit in figure 1.

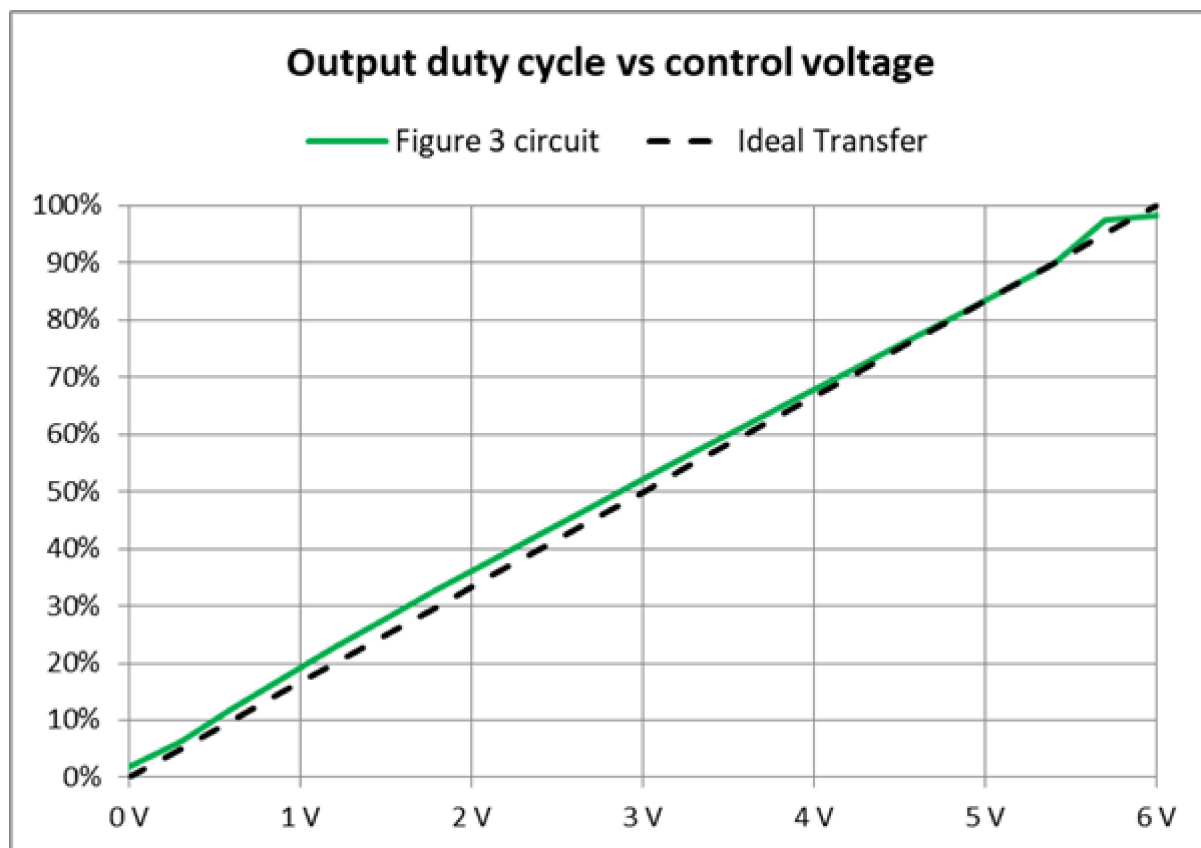


Figure 4. PWM duty cycle vs. control voltage using circuit figure 3, VDD = 6V, C = 1nf.

The transfer function result is similar to the ideal transfer function curve.