

## Ultrasonic Sensors / Numericals on Sensors.

Q.1  $f = 20 \text{ kHz}$ ,  $\gamma = 11.6 \times 10^{10} \text{ N/m}^2$ ;  $\rho = 7.23 \times 10^3 \text{ kg/m}^3$

$$f = \frac{1}{2L} \sqrt{\frac{\gamma}{\rho}} \Rightarrow L = \frac{1}{2f} \sqrt{\frac{\gamma}{\rho}}$$

$$L = \frac{1}{2 \times 20 \times 10^3} \sqrt{\frac{11.6 \times 10^{10}}{7230}}$$

$$= 0.1 \text{ m} = 10 \text{ cm.}$$

Q.2.  $L = 40 \text{ mm}$ ;  $\rho = 7.25 \times 10^3 \text{ kg/m}^3$ ;  $\gamma = 11.5 \times 10^{10} \text{ N/m}^2$

$$f = \frac{1}{2L} \sqrt{\frac{\gamma}{\rho}} = \frac{1}{2 \times 40 \times 10^{-3}} \sqrt{\frac{11.5 \times 10^{10}}{7250}}$$

$$= 49.78 \text{ kHz.}$$

Yes, US waves can be produced by the magnetostiction oscillator as the frequency obtained here is 49.78 kHz which is more than 20 kHz.

Q.3.  $t_1 = 1.8 \text{ mm}$ ;  $\gamma = 8 \times 10^{10} \text{ N/m}^2$ ;  $\rho = 2650 \text{ kg/m}^3$

a)  $f_1 = \frac{1}{2t_1} \sqrt{\frac{\gamma}{\rho}} = \frac{1}{2 \times 1.8 \times 10^{-3}} \sqrt{\frac{8 \times 10^{10}}{2650}}$

$$= 1.37 \text{ MHz.}$$

b)  $f_2 = \frac{1}{2t_2} \sqrt{\frac{\gamma}{\rho}} \Rightarrow t_2 = \frac{1}{2f_2} \sqrt{\frac{\gamma}{\rho}}$

$$t_2 = \frac{1}{2 \times 2 \times 10^6} \sqrt{\frac{8 \times 10^{10}}{2650}}$$

∴ The required change in the thickness  
 $\Rightarrow t_2 - t_1 \Rightarrow 1.8 - 0.915 = 1.085 \text{ mm}$

∴ Required change is 1.085 mm

Q.4.  $t_1 = 4 \text{ mm}$  ;  $f_1 = 400 \text{ KHz}$

$t_2 = ?$  ;  $f_2 = 500 \text{ KHz}$

$$f_1 = \frac{1}{2t_1} \sqrt{\frac{Y}{\rho}} ; f_2 = \frac{1}{2t_2} \sqrt{\frac{Y}{\rho}}$$

$$\frac{f_1}{f_2} = \frac{\frac{1}{2t_1} \sqrt{Y/\rho}}{\frac{1}{2t_2} \sqrt{Y/\rho}} = \frac{t_2}{t_1}$$

$$t_2 = \frac{f_1 \times t_1}{f_2} = \frac{400 \times 10^3 \times 4 \times 10^{-3}}{500 \times 10^3}$$

$$t_2 = 3.2 \text{ mm}$$

Q.5.  $T_N = 285^\circ \text{C}$  ;  $T_c = 0^\circ \text{C}$

$T_i = ?$  if  $T_c = -30^\circ \text{C}$

$$T_N = \frac{T_c + T_i}{2}$$

$$2T_N = T_c + T_i$$

$$T_i = 2T_N - T_c$$

$$= 2 \times 285 - (-30)$$

$$T_i = 600^\circ \text{C}$$

Q.6.  $a_{\text{Sb-Au}} = a_{\text{Sb-Pb}} - a_{\text{Au-Pb}}$

$$= 32.68 \mu\text{V}/^\circ\text{C}$$

$$b_{\text{Sb-Au}} = b_{\text{Sb-Pb}} - b_{\text{Au-Pb}} = 0.137 \mu\text{V}/^\circ\text{C}$$



$$e = at + \frac{1}{2}bt^2$$

$$= 32.68 \times 100 + \frac{1}{2}(0.137) \times 10^4$$

$$= 3268 + 685$$

$$= 3953 \mu V$$

Q.7: Thermo emf  $e = 2160 \mu V$  at  $t_1 = 0^\circ C$   
 $t_2 = 250^\circ C$

$$t_n = 330^\circ C$$

The thermoemf is given by  $e = at + \frac{1}{2}bt^2$

$$2160 \times 10^{-6} = a(250) + \frac{1}{2}b(250)^2$$

$$2160 \times 10^{-6} = 250a + 31250b$$

$$\text{As } t_n = -a/b$$

$$a = -330b$$

Substituting  $a$  in the above eq<sup>n</sup>

$$2160 \times 10^{-6} = 250(-330b) + 31250b$$

$$\therefore b = -0.04214 \mu V/^\circ C^2$$

$$a = -330(-0.04214) = 13.906 \mu V/^\circ C$$

Q.8: If  $a_1, b_1$  are the coefficients for Fe-Pb thermocouple; while  $a_2, b_2$  are the <sup>coeff. for Cd-Pb</sup> thermocouple. coeff. of Cd-Pb thermocouple.

$$\text{As emf } e = at + \frac{1}{2}bt^2$$

$$P = \frac{de}{dt} = a + bt$$

∴ for Fe-Pb thermocouple

$$P_1 = a_1 + b_1 t \quad \text{--- (1)}$$

and for Cd-Pb is  $P_2 = a_2 + b_2 t \quad \text{--- (2)}$

∴ For Fe-Pb

$$17.5 = a_1 + b_1 \cdot 0$$

$$\therefore a_1 = 17.5 \mu\text{V}/^\circ\text{C} \quad \text{at } t = 0^\circ\text{C}$$

Also  $5 = a_1 + b_1 \times 125$

$$\Rightarrow 5 = 17.5 + 125 b_1$$

$$\Rightarrow b_1 = \frac{5 - 17.5}{125} = -0.1 \mu\text{V}/^\circ\text{C}^2$$

For Cd-Pb

$$3 = a_2 + b_2 \cdot 0 \Rightarrow a_2 = 3 \mu\text{V}/^\circ\text{C}^2$$

$$15 = a_2 + b_2 \times 150 \Rightarrow 15 = 3 + b_2 \times 150$$

$$\therefore b_2 = \frac{15 - 3}{150} = 0.08 \mu\text{V}/^\circ\text{C}^2$$

∴ For Fe-cd thermocouple, we have the coefficients as

$$a = a_1 - a_2$$

$$a = 17.5 - 3 = 14.5 \mu\text{V}/^\circ\text{C}$$

$$b = b_1 - b_2 = -0.1 - 0.08 = -0.18 \mu\text{V}/^\circ\text{C}^2$$

∴ The neutral temperature for Fe-cd is

$$t_n = -a/b = \frac{-14.5}{-0.18}$$

$$t_n = 80.55^\circ\text{C}$$