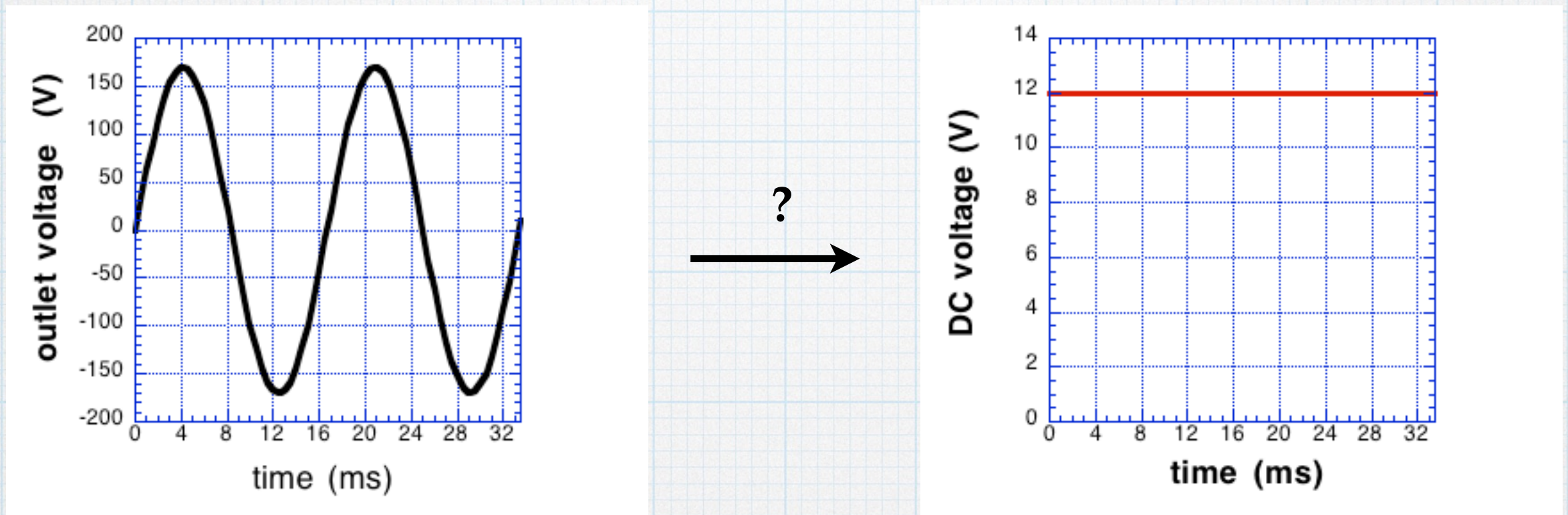


# Rectifier circuits & DC power supplies

Goal: Generate the DC voltages – needed for most electronics – starting with the AC power that comes through the power line.

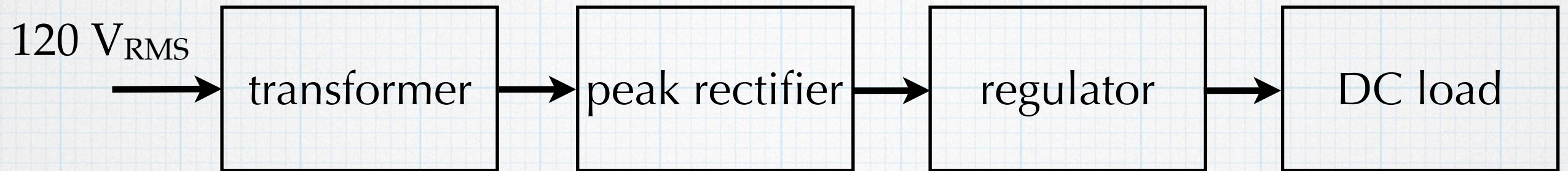


$$120 V_{\text{RMS}} \quad f = 60 \text{ Hz} \quad (T = 16.67 \text{ ms})$$

$$V_{ac} = (170\text{V}) \sin\left(\frac{2\pi}{T}t\right)$$

How to take time-varying voltage with an average value of 0 and turn it into a DC voltage?





transformer : reduces AC amplitude to something safe and manageable.

$V_{peak}$  from the transformer will be a few volts bigger than the desired DC voltage.

peak rectifier : breaks up the AC waveform and produces a  $V_{DC} \approx V_{peak}$ .

regulator : Refines the output of the rectifier. (optional)

Issues:

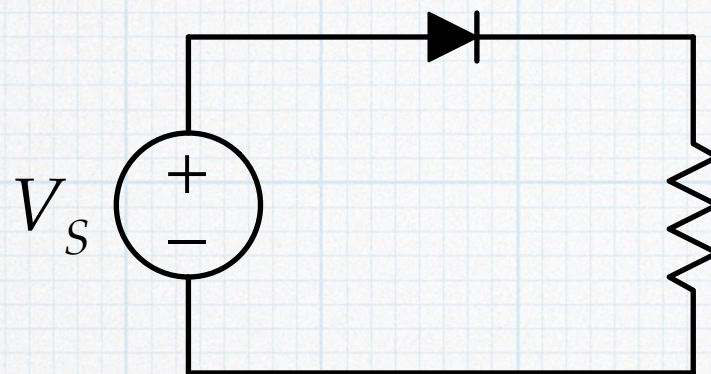
- Total power
- Efficiency
- Cost
- Load regulation (Does  $V_{DC}$  change as the load draws different amounts of current?)
- Line regulation (Does  $V_{DC}$  change if the input AC amplitude changes?)



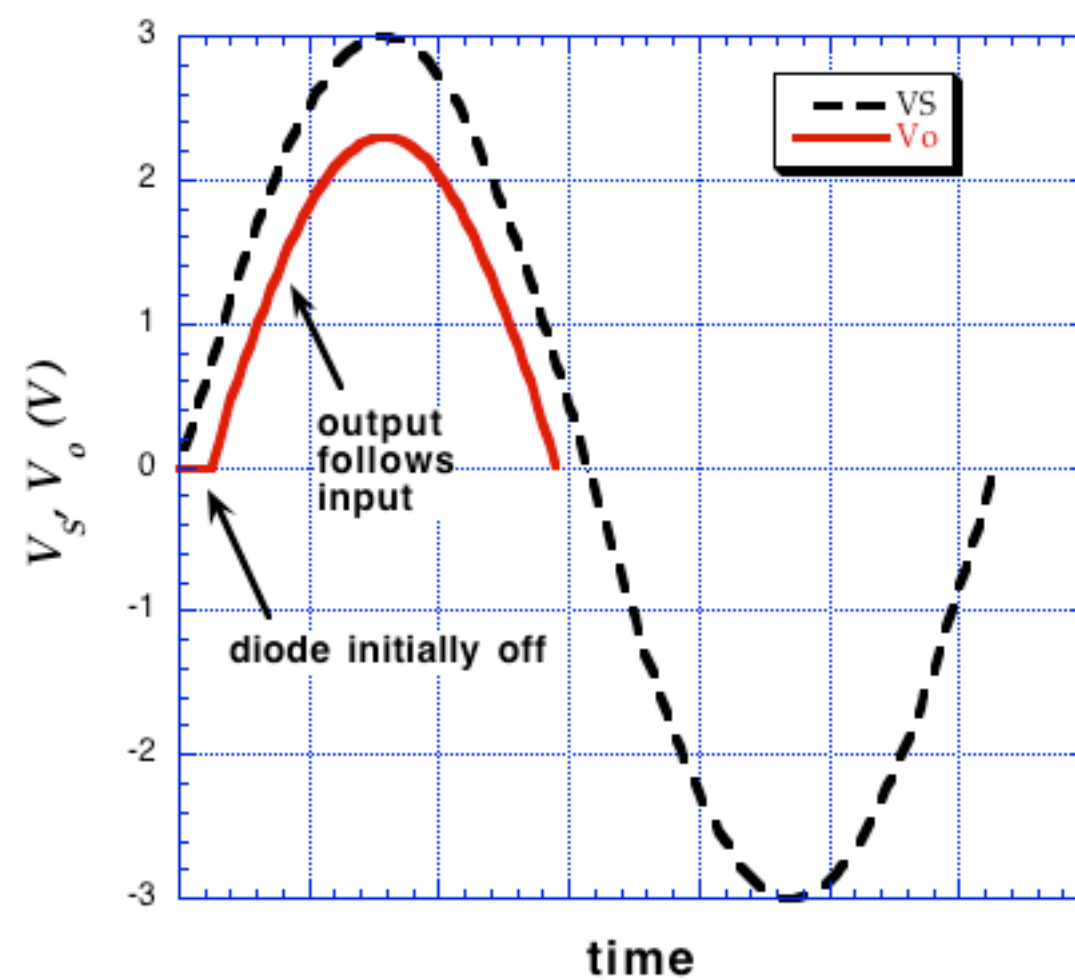
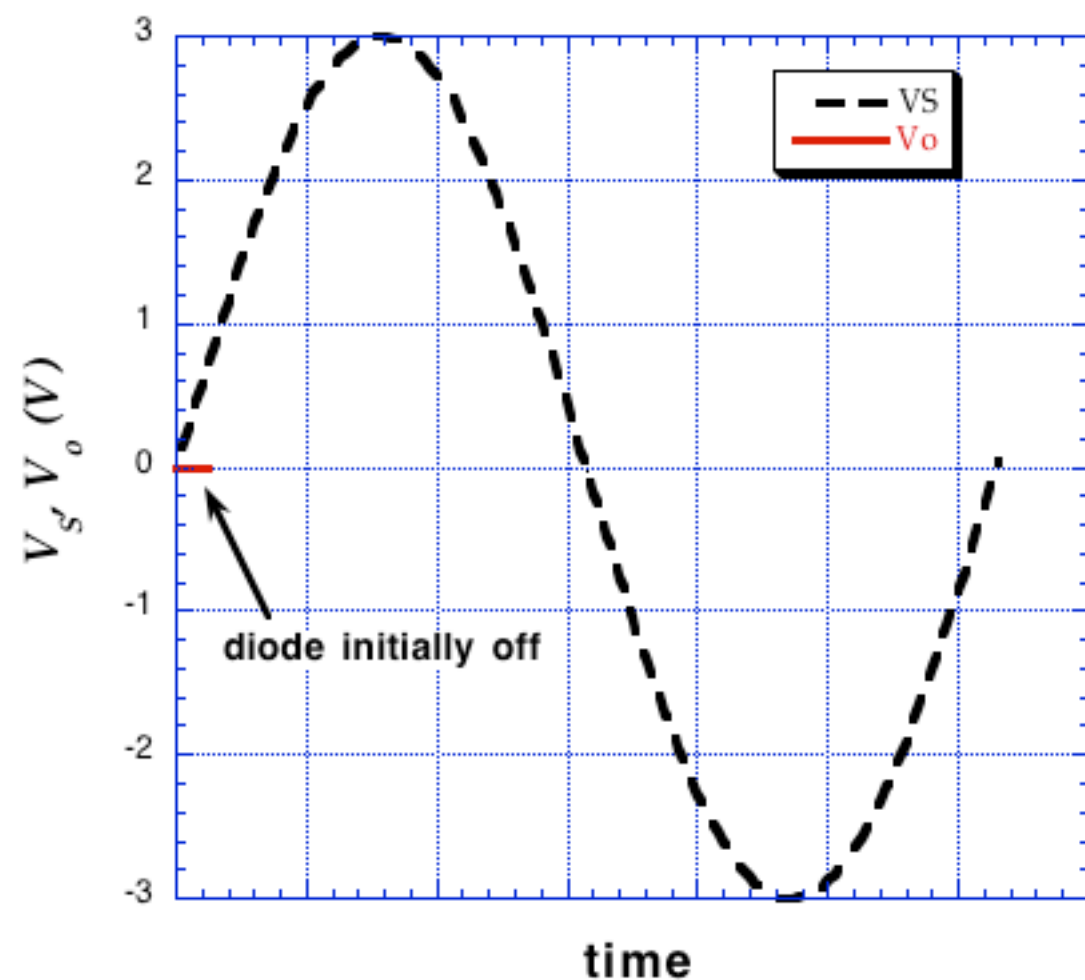
# Half-wave rectifier

$$V_S(t) = V_p \sin\left(\frac{2\pi}{T}t\right)$$

$$V_p = 3 \text{ V.}$$



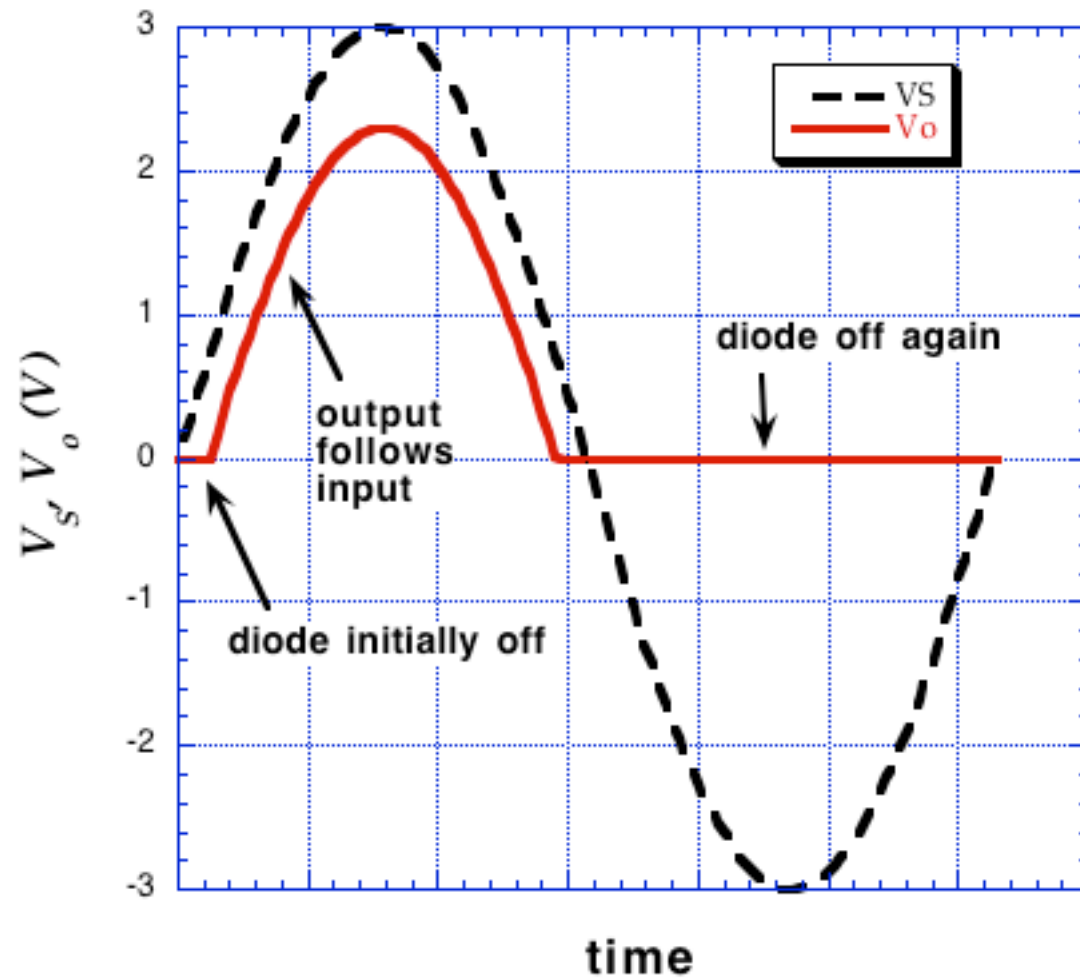
Resistor represent a load.  
We are trying to deliver DC power to the load.



Diode is off until  $V_S > 0.7 \text{ V.}$

Current flows when diode is in forward conduction. The output tracks the input during positive half cycle.





The diode turns off when  $V_S < 0.7$  V. It stays off during the negative half cycle of the sinusoid.

$$V_S > 0: \quad v_R(t) \approx V_p \sin\left(\frac{2\pi}{T}t\right) - 0.7V$$

$$V_S < 0: \quad v_R(t) = 0:$$

$$V_o(\text{avg}) \approx \frac{V_P}{\pi} - \frac{0.7V}{2} \neq 0!$$

To get the negative half of the cycle, turn the diode around.



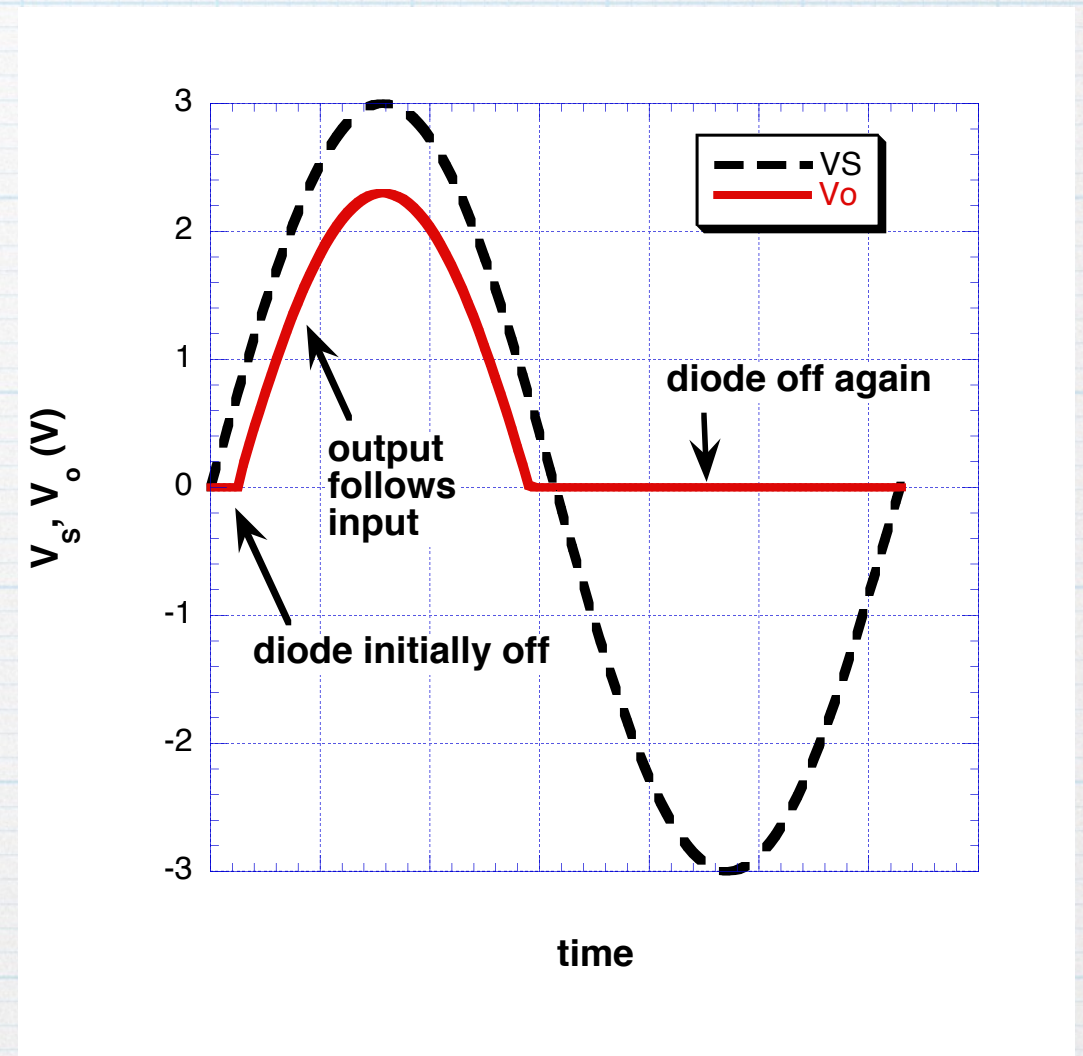
# Time delay

Note that since the diode will not turn on until the sinusoid goes above  $\approx 0.7\text{ V}$ , there is time delay before the rectifier “turns on”. It is a simple matter to determine the delay time, using the “on-off” diode model:

$$0.7\text{V} = V_p \sin\left(\frac{2\pi}{T}t'\right)$$

$$t' = \frac{T}{2\pi} \arcsin\left(\frac{0.7\text{V}}{V_p}\right)$$

If  $f = 60\text{ Hz}$  ( $T = 16.67\text{ ms}$ )  
and  $V_p = 3\text{ V}$ ,  $t' = 0.62\text{ ms}$ .



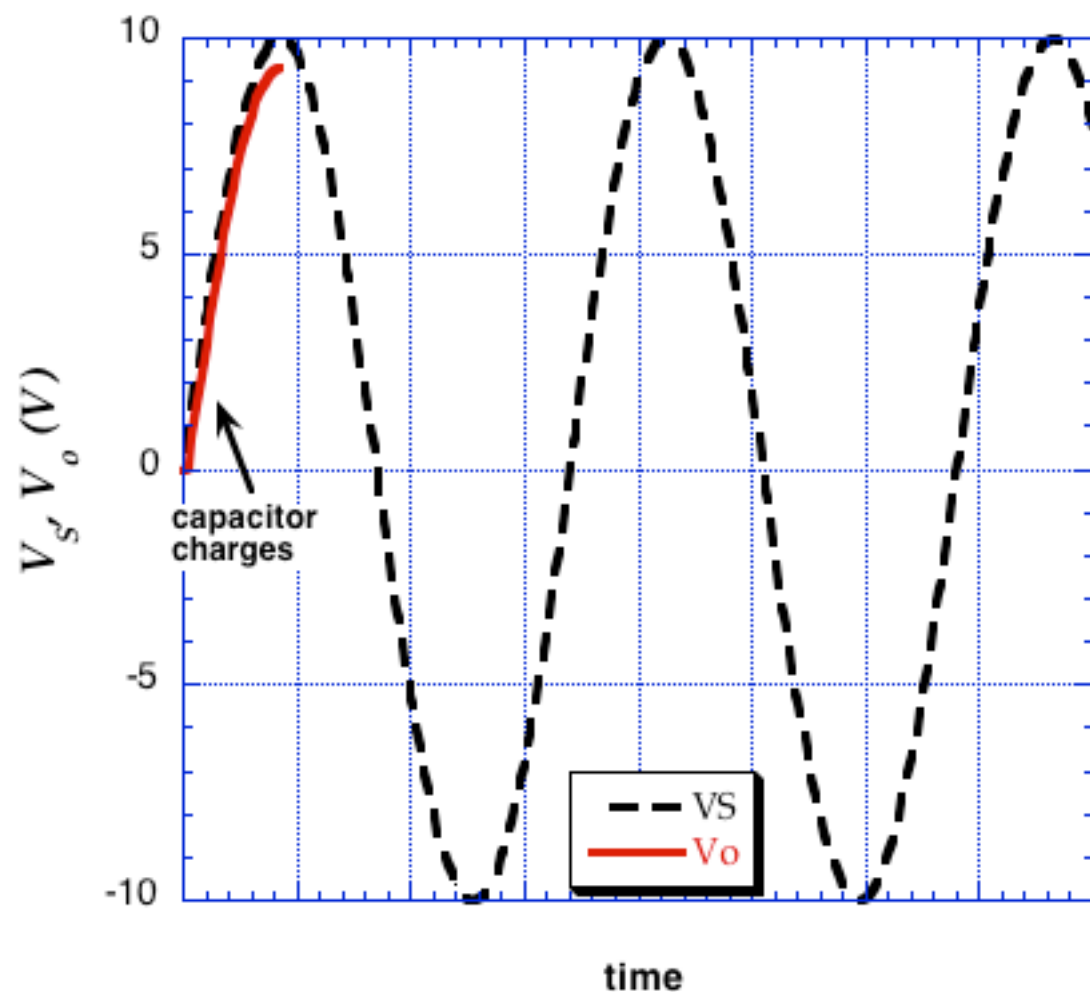
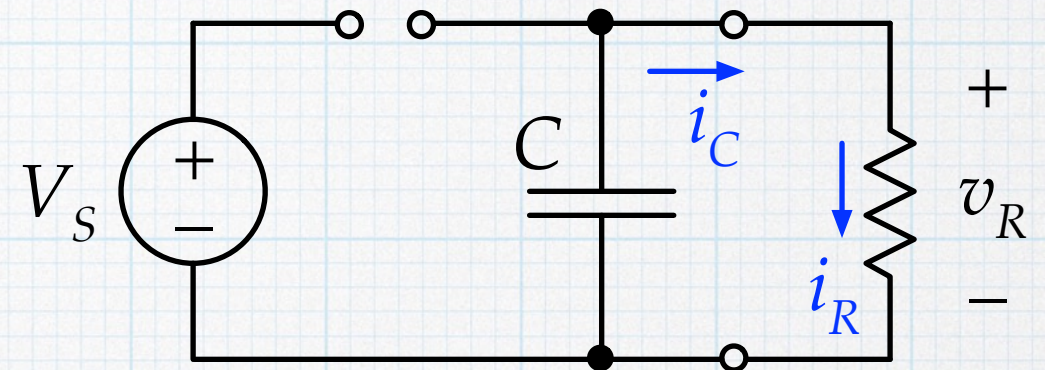
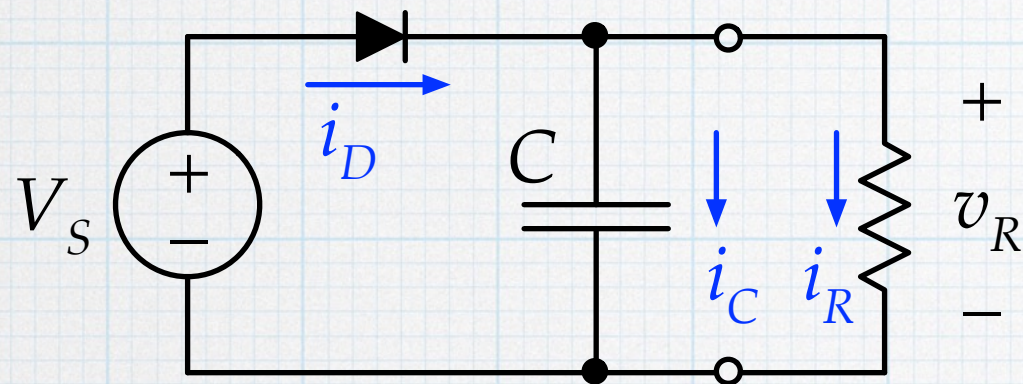
There is a similar time offset at the other end of the positive half cycle.

The effect of the time offset become negligible if  $V_p \gg 0.7\text{ V}$ .

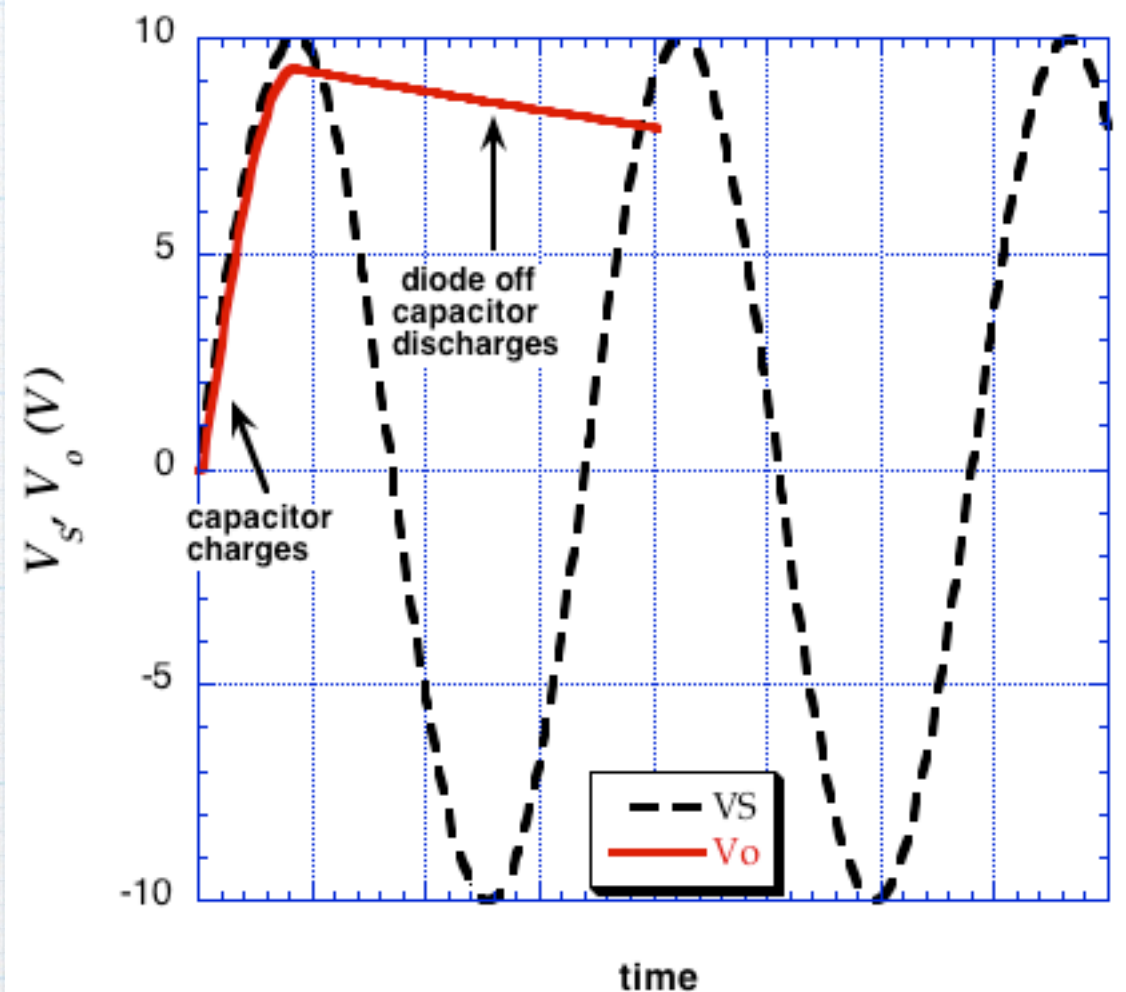


# Peak rectifier

Add a largish capacitor after the diode, in parallel with the load.

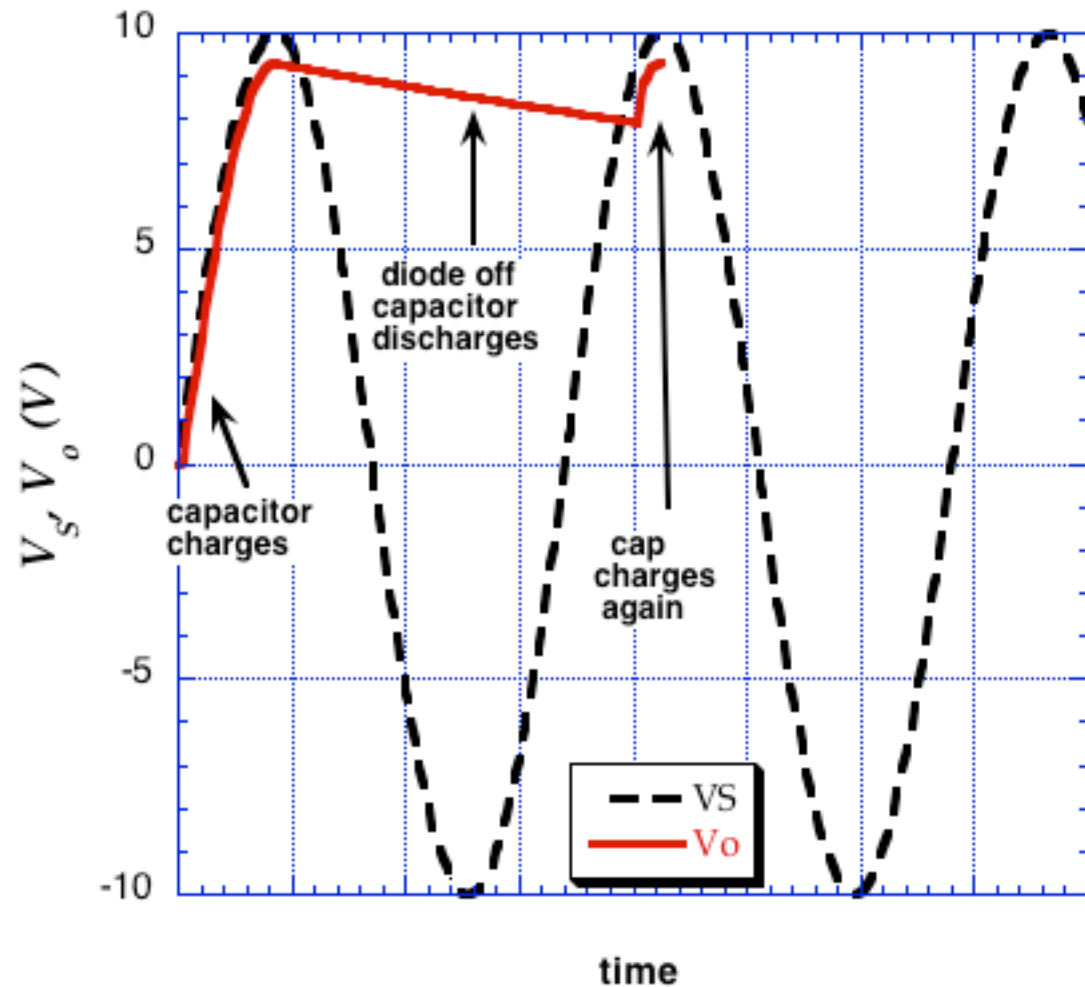
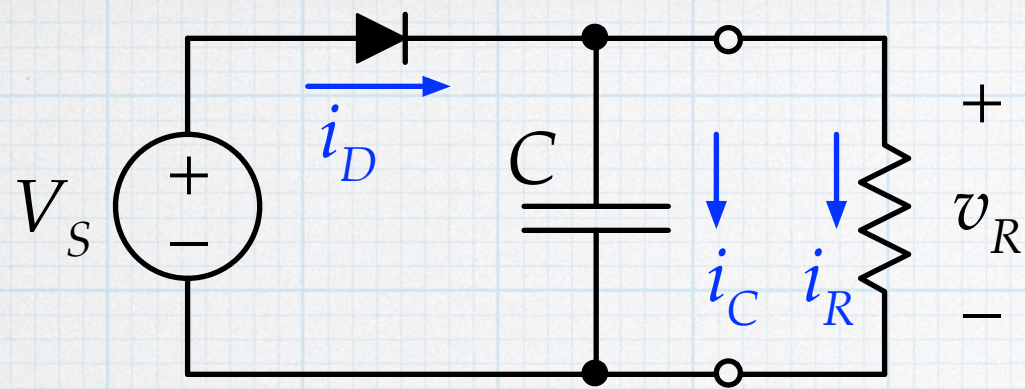


Initially, diode is on & cap charges to  $V_P - 0.7 \text{ V}$ .

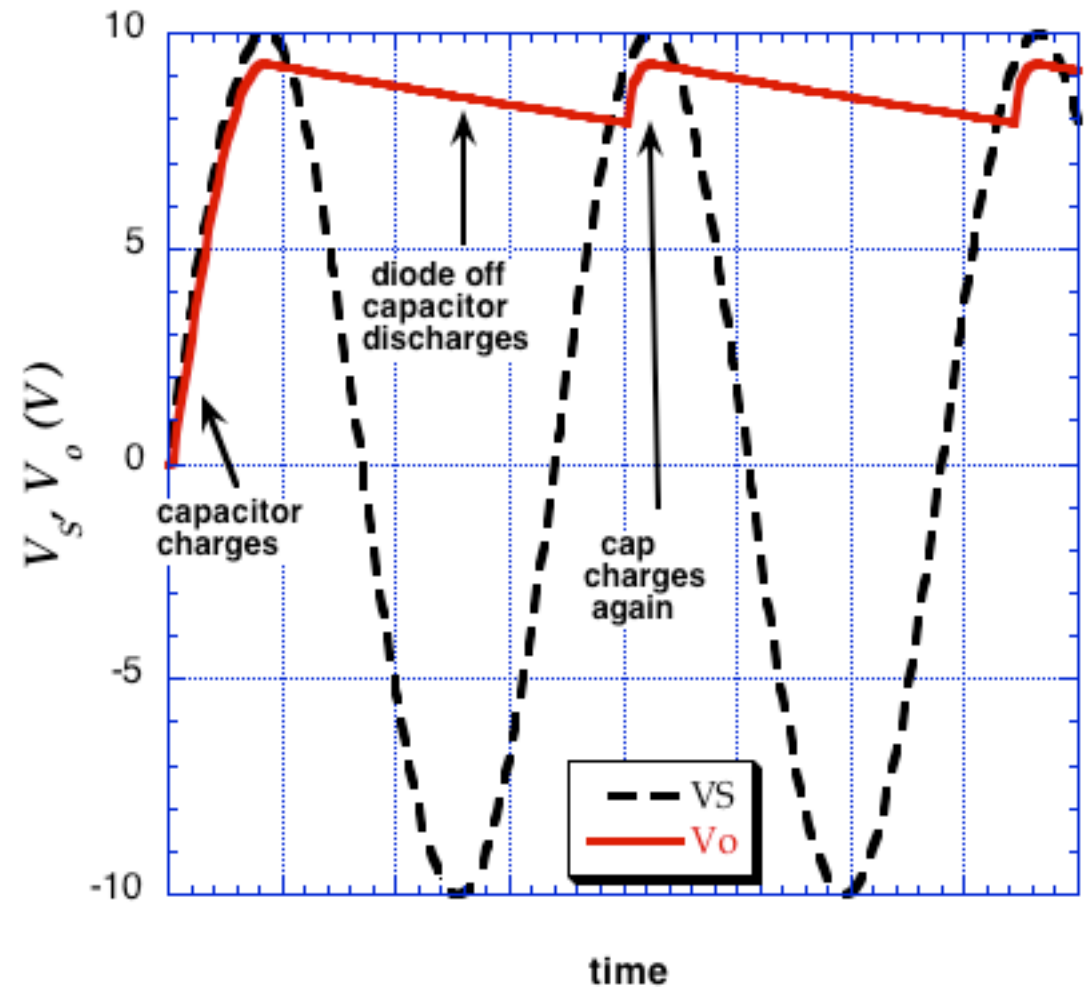


While  $V_S < v_C$ , diode is off!  
Cap discharges through load.



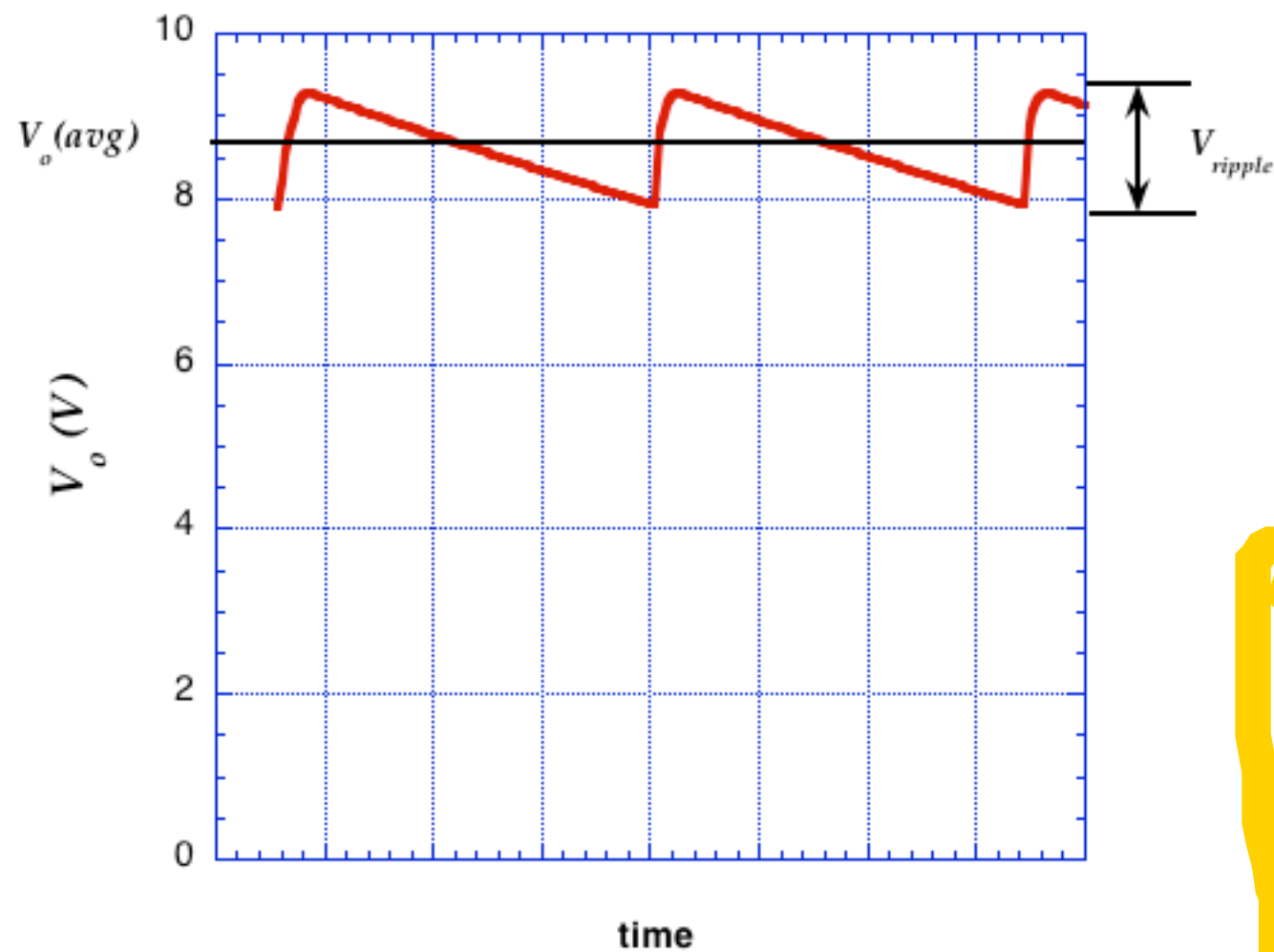


Diode stay off until  $V_S$  comes back around and becomes bigger than  $v_C$ . Then diode comes on again and re-charges the capacitor.



When  $V_S$  falls to less than  $v_C$ , the diode turn off again, and the cycle continues.





Not a perfect DC voltage at output. There is some variation (ripple) around an average value.

$$V_o(max) = V_P - 0.7V$$

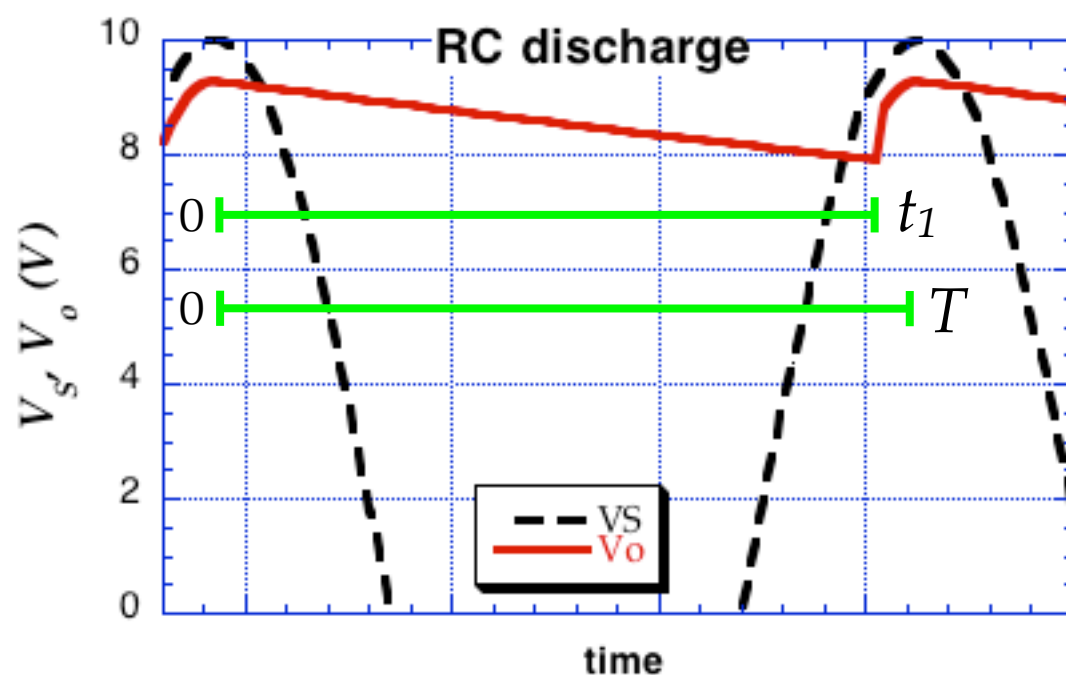
$$V_o(min) = [V_P - 0.7V] \exp\left(-\frac{t_1}{RC}\right)$$

$$\approx [V_P - 0.7V] \exp\left(-\frac{T}{RC}\right)$$

$$V_{ripple} = V_o(max) - V_o(min)$$

$$= [V_P - 0.7V] \left[1 - \exp\left(-\frac{T}{RC}\right)\right]$$

$$V_o(avg) \approx V_o(max) - \frac{V_{ripple}}{2}$$



$t_1$  = time when diode conducts again.

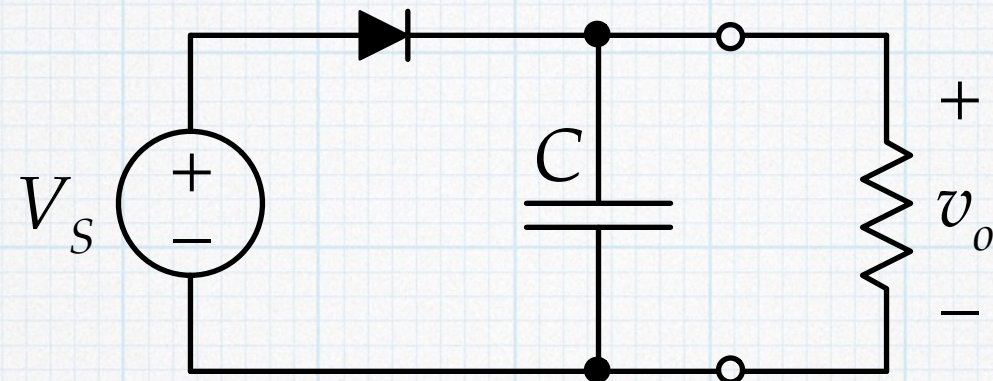
$$t_1 \approx T$$



# Example 1

$$V_s = (15V) \sin\left(\frac{2\pi}{T}t\right)$$

$$T = 16.67 \text{ ms}$$



$$C = 100 \mu\text{F}$$

$$R = 5000 \Omega$$

Find the average value of  $v_o$  and the ripple voltage. Repeat for  $R = 1000 \Omega$  and  $200 \Omega$ .

$$V_{\text{ripple}} = [V_P - 0.7V] \left[ 1 - \exp\left(-\frac{T}{RC}\right) \right]$$

$$= [15V - 0.7V] \left[ 1 - \exp\left(-\frac{16.67\text{ms}}{(5000\Omega)(100\mu\text{F})}\right) \right]$$

$$= 0.47 \text{ V}$$

$$V_o(\text{avg}) = V_o(\text{max}) - \frac{V_{\text{ripple}}}{2} = 14.3V - \frac{0.47V}{2} = 14.1V$$

$$R = 1 \text{ k}\Omega$$

$$V_{\text{ripple}} = 2.19 \text{ V}$$

$$V_o(\text{avg}) = 13.2 \text{ V}$$

$$R = 200 \Omega$$

$$V_{\text{ripple}} = 8.09 \text{ V}$$

$$V_o(\text{avg}) = 10.2 \text{ V}$$

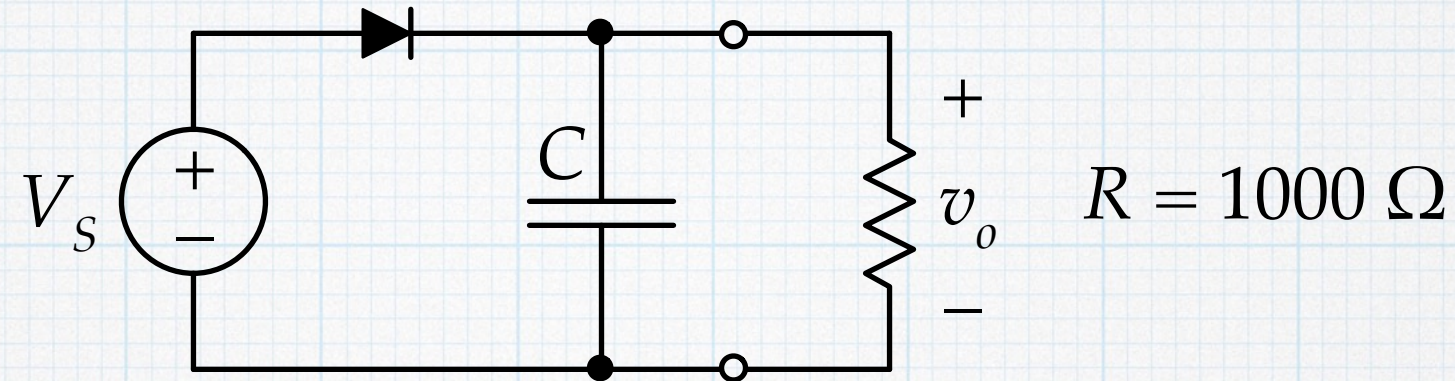
Drawing more current causes the ripple to increase and  $V_{DC}$  to droop. Can fight this with more capacitance.



## Example 2

$$V_S = (25\text{V}) \sin\left(\frac{2\pi}{T}t\right)$$

$$T = 16.67 \text{ ms}$$



Find the capacitance so that the ripple will be no bigger than 1 V.

What is the DC voltage?

$$V_{\text{ripple}} = [V_P - 0.7\text{V}] \left[ 1 - \exp\left(-\frac{T}{RC}\right) \right]$$

$$C = -\frac{T}{R} \left[ \ln\left(1 - \frac{V_{\text{ripple}}}{V_P - 0.7\text{V}}\right) \right]^{-1} = -\frac{16.67\text{ms}}{1000\Omega} \left[ \ln\left(1 - \frac{1\text{V}}{24.3\text{V}}\right) \right]^{-1} = 397 \mu\text{F}$$

$$V_o(\text{avg}) = V_o(\text{max}) - \frac{V_{\text{ripple}}}{2} = 24.3\text{V} - \frac{1\text{V}}{2} = 23.8\text{V}$$

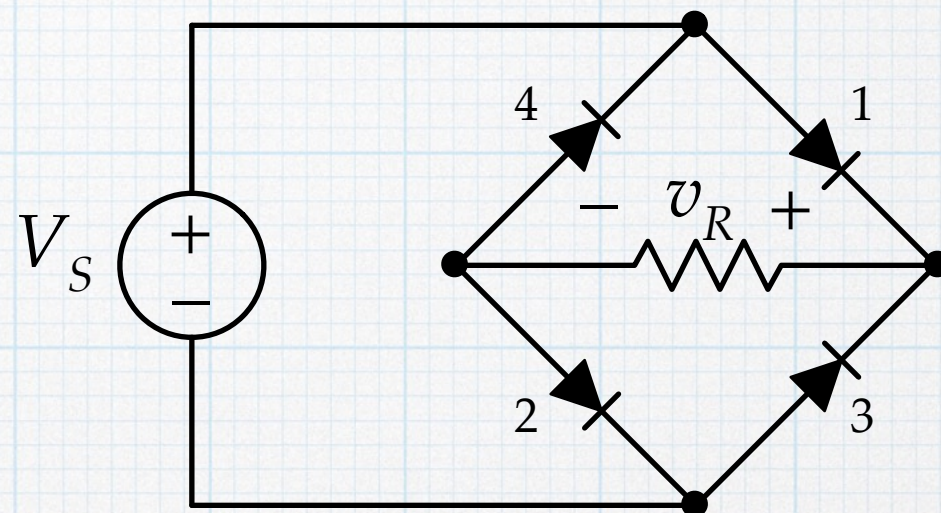
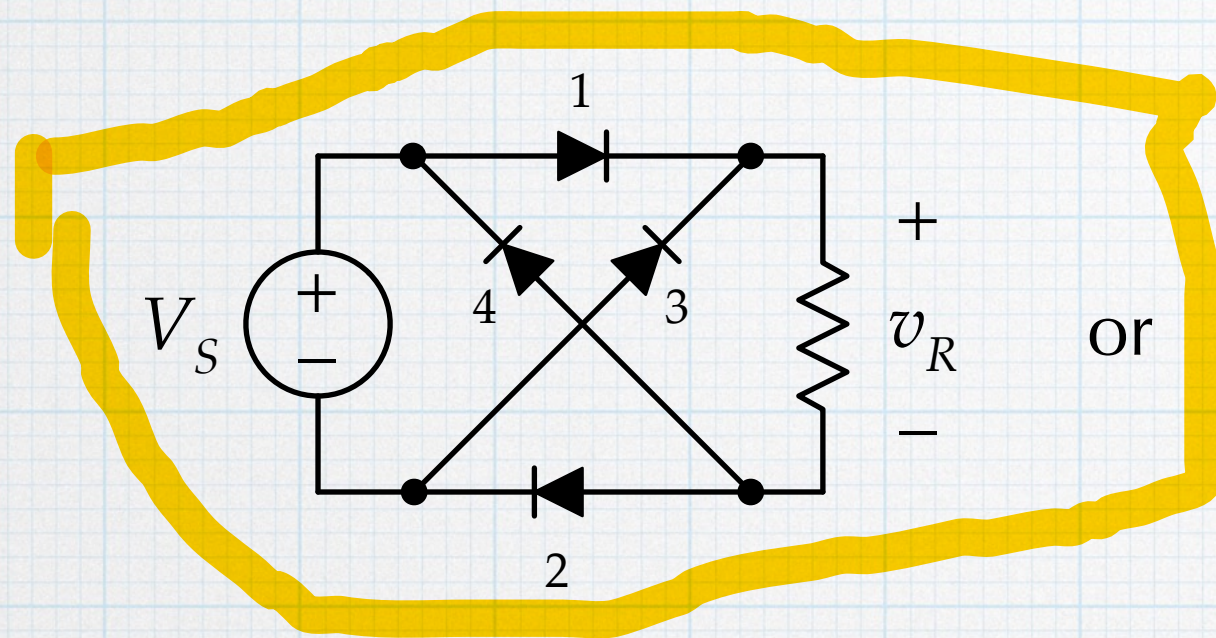
What capacitance is needed to limit the ripple to 0.1 V?

$$C = 4000 \mu\text{F} \quad !!!$$



# Full-wave rectifier

With a few more diodes, we can rectify the entire sinusoidal input.

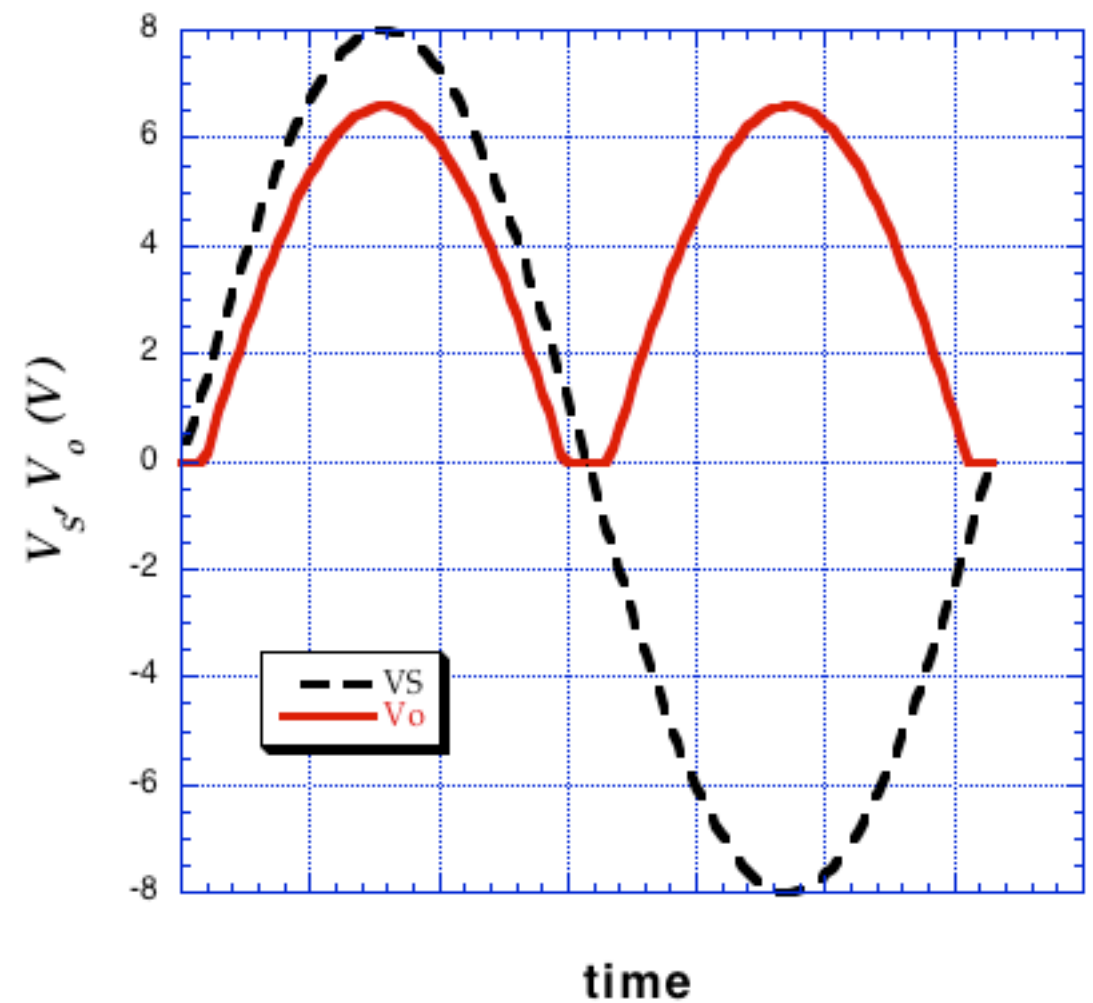
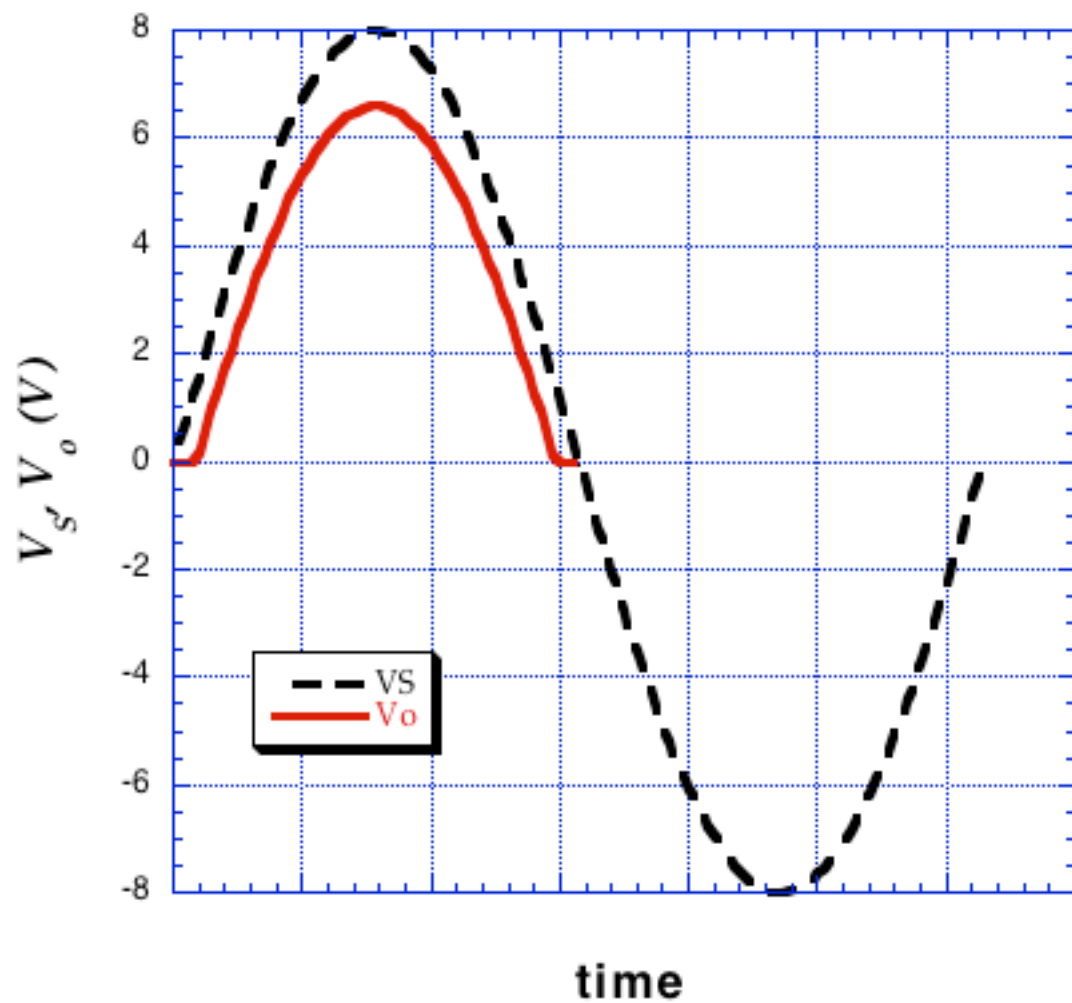
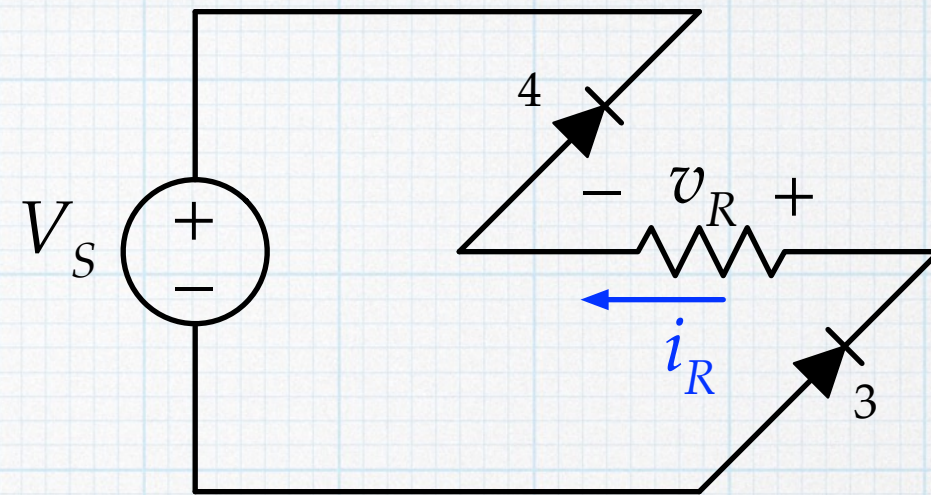
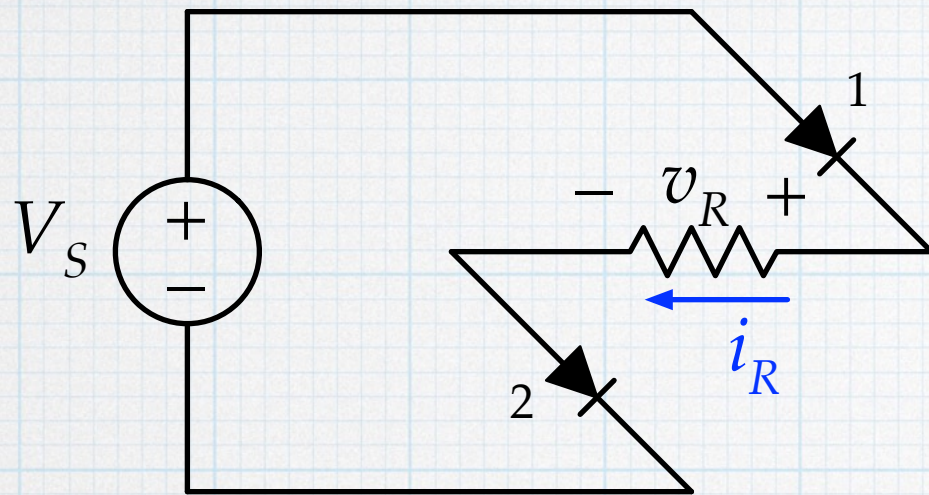


The diodes are in a bridge configuration.

During the positive half cycle of the input, diodes 1 and 2 will be forward biased. Current will flow from the positive source through those diodes and the resistor to generate a positive voltage across the resistor.

During the negative half cycle of the input, diodes 3 and 4 will be forward biased. Current will flow from the negative source through those diodes and the resistor to generate a positive voltage across the resistor, again.





Note that there are no two diode drops in the conduction path(s).  
Also, the frequency is effectively doubled.

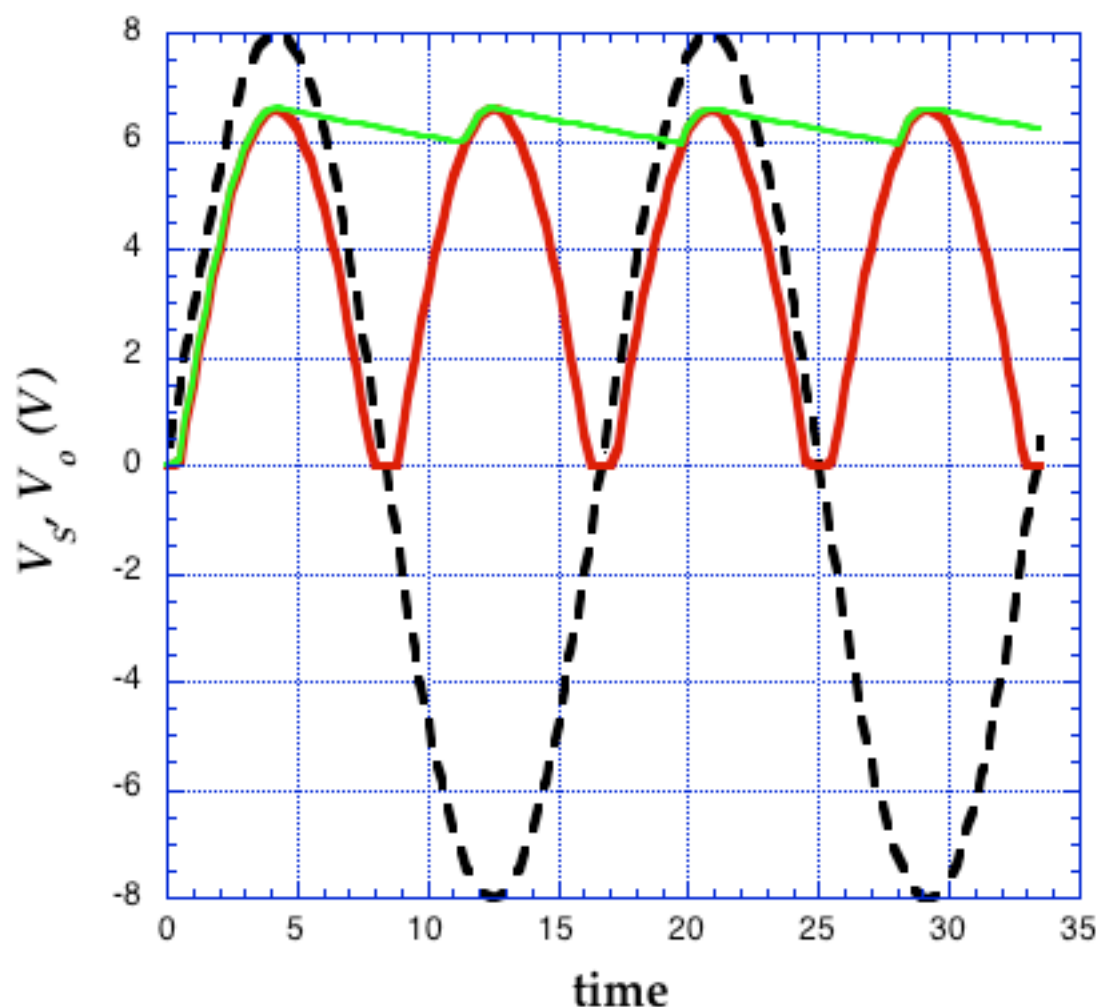
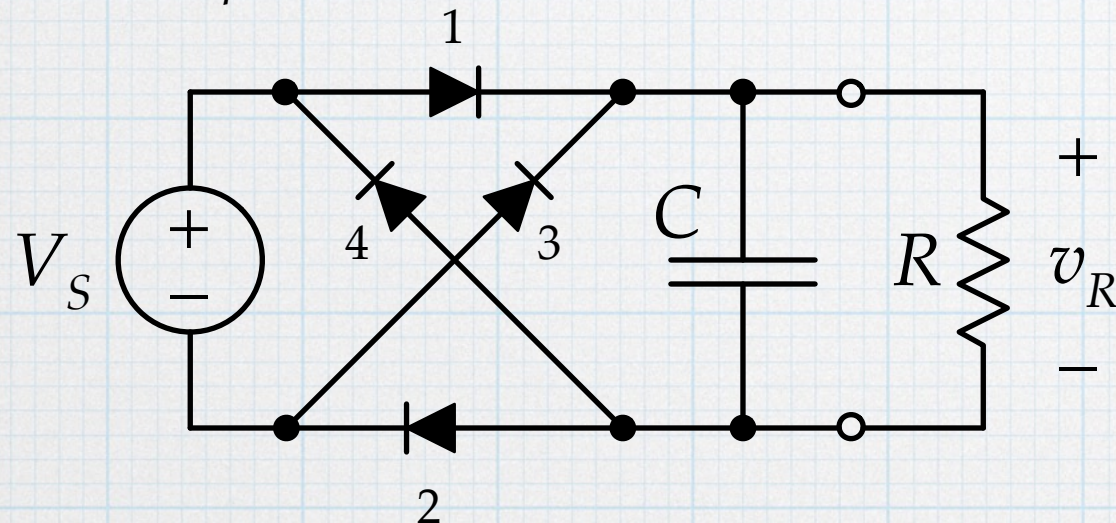


# Full-wave peak rectifier

Placing a capacitor in parallel with the load, turns the circuit into a full-wave peak rectifier. It behaves essentially the same as the half-wave peak rectifier except with twice the frequency (half the period).

$$V_S(t) = V_p \sin\left(\frac{2\pi}{T}t\right)$$

$$V_p = 8 \text{ V.}$$



The ripple voltage is calculated in exactly the same way, except that the period is cut in half (frequency doubled).

$$V_{\text{ripple}} = [V_P - 1.4\text{V}] \left[ 1 - \exp\left(-\frac{T}{2RC}\right) \right]$$

Same as doubling capacitance!



## Example 3

You want to use a wall transformer that produces 10- $V_{RMS}$  at the secondary to generate a DC voltage. The desired voltage DC should be greater than 12 V and it should be able to supply at least 50 mA while keeping the voltage ripple to less than 5%. Design the rectifier to meet these goals. (Note:  $f = 60$  Hz.)

$$10 V_{RMS} \rightarrow 14.1 V \text{ amplitude}$$

$$\text{effective } R_L \approx V_o / I_o = 12.0 V / (50 \text{ mA}) = 240 \Omega$$

Note: This would be the minimum value of effective resistance. If we choose  $C$  to meet the ripple requirement, then we will still be safe if we use a slightly higher  $V_o$ .

Two options: half-wave or full-wave rectifier. Try both.

Half-wave:

$$V_o(\text{max}) = V_p - 0.7 V = 13.4 V \rightarrow V_{\text{ripple}} \leq 0.67 V.$$

$$C = -\frac{T}{R} \left[ \ln \left( 1 - \frac{V_{\text{ripple}}}{V_p - 0.7V} \right) \right]^{-1} = 1350 \mu F$$

$$V_o(\text{avg}) = V_o(\text{max}) - V_{\text{ripple}} / 2 = 13.06 V.$$



Full-wave:

$$V_o(\text{max}) = V_p - 2(0.7 \text{ V}) = 12.74 \text{ V} \rightarrow V_{\text{ripple}} \leq 0.64 \text{ V}.$$

$$C = -\frac{T}{2R} \left[ \ln \left( 1 - \frac{V_{\text{ripple}}}{V_o(\text{max})} \right) \right]^{-1} = 673 \mu\text{F}$$

$$V_o(\text{avg}) = V_o(\text{max}) - V_{\text{ripple}} / 2 = 12.42 \text{ V}.$$

Either approach will work and meet the requirements. The full-wave version uses extra diodes, but only half the capacitance. Since diodes are nearly free (pennies per piece), but big capacitors are relatively expensive, the full-wave circuit will actually cost less than the half-wave.

This is why full-wave rectifiers are used more commonly than half-wave rectifiers.

Component manufactures supply full-wave bridge rectifiers packaged as single unit with the transformer sinusoid as input the rectified waveform as the output.