

2024/02/04 Assignment - 2 AEC

1)

(i.1) given npn BJT

$$I_B = 14.46 \mu A$$

$$I_E = 1.46 mA$$

$$V_{BE} = 0.7 V$$

as $V_{BE} = 0.7$ BJT is in forward active or saturation mode then,

$$I_E = I_B + I_C$$

$$1.46 mA = 14.46 \mu A + I_C$$

$$I_C \approx 1.445 mA$$

$$\beta = \frac{I_C}{I_B}, \alpha = \frac{I_C}{I_E}$$

$$\beta = \frac{1.445 \times 10^3}{14.46 \times 10^{-6}} = 99.99 \approx 100$$

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$$\alpha = \frac{1.445 mA}{1.46 mA} = 0.99 \approx 1$$

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$$I_S (e^{V_{BE}/V_T} - 1) = I_C$$

$$N_{BE} = 0.7 V, V_T = 26 mV \text{ at room Temp}$$

$$I_S = \frac{1.445 \times 10^{-5}}{(e^{0.7/0.026} - 1)} = 9.6 \times 10^{-6} \times 10^{-8} \times 10^{-3} = 9.6 \times 10^{-16} A$$

(1.2)

$$I_S = 10^{-16} A, \beta = 100$$

$$I_C = 1 \text{ mA}$$

$$I_C = I_S (e^{V_{BE}/V_T} - 1)$$

$$10^13 = e^{V_{BE}/V_T} \quad V_T = 26 \text{ mV} = 0.026 \text{ V}$$

$$V_{BE} = 0.77 \text{ V}$$

$$I_B = I_{SB} (e^{V_{BE}/V_T} - 1)$$

$$\frac{I_C}{\beta} (e^{V_{BE}/V_T} - 1) = I_{SB} (e^{V_{BE}/V_T} - 1)$$

$I_C \Rightarrow I_{SB} = \frac{I_S}{\beta} = 10^{-18} = \frac{10^{-16}}{100} = 10^{-18} \text{ A}$

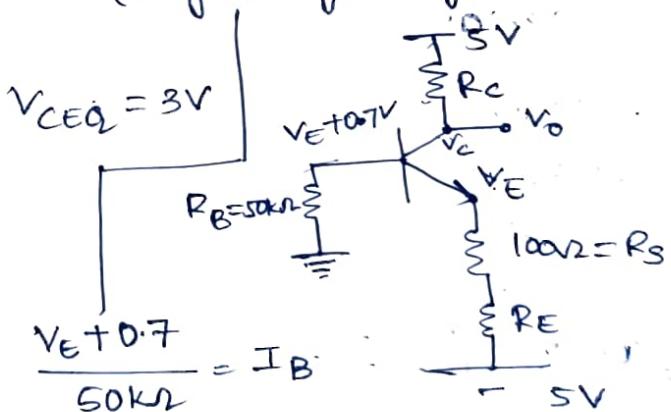
$$\Rightarrow I_{SE} = \frac{I_S}{\alpha} = \left(\frac{\beta+1}{\beta} \right) I_S = 1.01 \times 10^{-16} \text{ A}$$

(1.3) Given,

$$\beta = 100, \quad V_A = \infty$$

(neglecting early effect)

$$I_{CG} = 0.25 \text{ mA}$$



$$I_B = \frac{V_E + 0.7}{50 \text{ k}\Omega}$$

$$I_E = \frac{V_E + 5}{100 + R_E}$$

$$I_B = \frac{I_C}{\beta} = \frac{0 - (V_E + 0.7)}{50 \text{ k}\Omega} = \frac{0.25 \times 10^{-3}}{100}$$

$$-2V_E - 1.4 = 0.25$$

$$V_E = \frac{-1.65}{2} = -0.825 \Rightarrow V_B = -0.125$$

$$I_E = \left(\frac{\beta+1}{\beta}\right) I_C = \frac{101}{100} \times 0.25 \text{ mA}$$

$$I_E = 0.2525 \text{ mA}$$

$$(R_E + 100) I_E = V_{EE} + 5$$

$$R_E = 16.4 \text{ k}\Omega$$

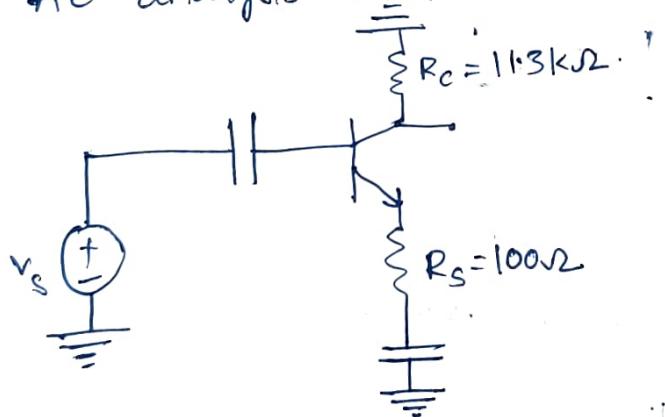
$$V_{CE} = 3V \Rightarrow V_C = 3V - 0.0875V$$

$$V_C = 2.175$$

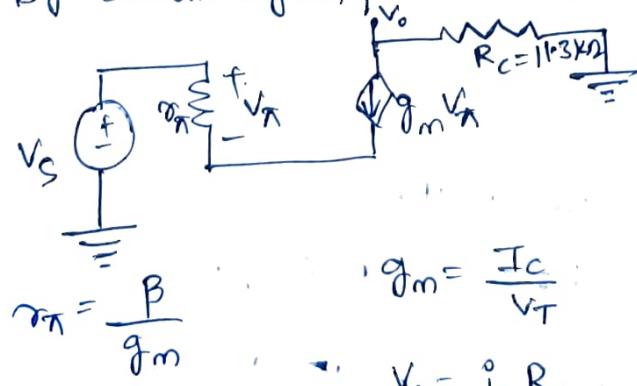
$$\frac{5 - 2.175}{R_C} = I_C = 0.25 \text{ mA}$$

$$R_C = 11.3 \text{ k}\Omega$$

AC analysis now,



By small signal AC model replacement



$$r_o = \frac{B}{g_m}$$

$$V_o = i_C R_C$$

$$I_C = 0.25 \text{ mA}$$

$$g_m V_o = i_C$$

$$V_s = i_b r_o + i_e R_s \quad V_o = i_e R_s$$

$$P_{AV} = \frac{V_o}{V_s} = \frac{i_C R_C}{V_s} = \frac{B R_C}{r_o + (B+1) R_S}$$

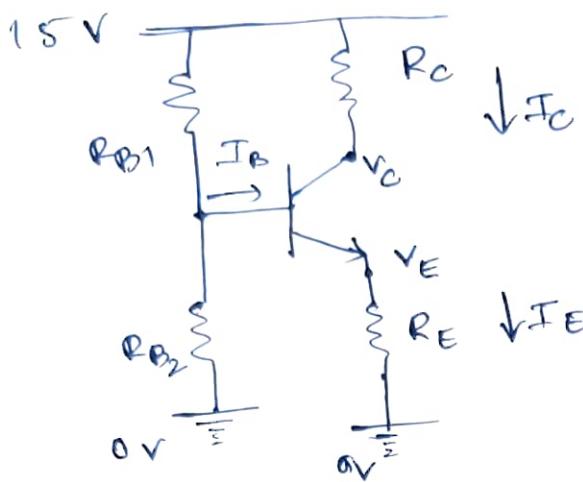
$$A_v = \frac{100 \times 11.3}{20.4} = 55.39$$

$$\text{input Resistance} = \frac{B}{g_m} + (B+1) R_S = 20.4 \text{ k}\Omega$$

$$g_m = 9.6 \text{ mS}$$

$$\therefore r_o = 10.9 \text{ k}\Omega$$

(2.1)



$$\beta = 100 \quad R_{B1} = 100\text{k}\Omega$$

~~$$R_{B2} = 50\text{k}\Omega$$~~

$$R_C = 5\text{k}\Omega$$

$$R_E = 3\text{k}\Omega$$

$$\frac{V_{CC} R_{B2}}{R_{B2} + R_{B1}} \approx V_B = \frac{15 \times 50}{150} = 5\text{V}$$

$$V_E = 4.3\text{V}$$

$$I_E = \frac{V_E}{R_E} = \frac{4.3\text{V}}{3\text{k}\Omega} = 1.43\text{mA}$$

$$I_C \approx I_E$$

$$\frac{15 - V_C}{R_C} = I_C$$

$$15 - V_C = 5 \times 10^3 \times 1.43 \times 10^{-3}$$

$$V_C \approx 7.85\text{V}$$

$$\frac{15 - V_B}{R_{B1}} = I_{B1} + \frac{V_B}{R_{B2}}$$

$$\frac{15 - 3V_B}{100\text{k}\Omega} = I_B$$

$$V_E = I_E \cdot R_E$$

$$V_B = 0.7 = (\beta + 1) I_B R_E$$

$$\frac{V_B - 0.7}{(\beta + 1) R_E} = \frac{15 - 3V_B}{100\text{k}\Omega} = \frac{V_B - 0.7}{303}$$

$$100(V_B - 0.7) = 303 \times 15 - 909V_B$$

$$V_B = 4.57\text{V}$$

$$V_E = 3.87\text{V}$$

$$\frac{15 - V_C}{R_C} = I_C$$

$$15 - V_C = (5\text{k}\Omega) \times 2.9\text{mA}$$

$$V_C = 8.55\text{V}$$

$$I_C = \beta I_B$$

$$I_B = 1.29 \mu A$$

$$I_E = I_B + I_C \approx 1.29 mA$$

$$I_C = 1.29 mA$$

2.2

$$\beta \rightarrow \beta/2$$

$$\beta_n = 50$$

$$\frac{V_B - 0.7}{(\beta_n + 1)R_E} = \frac{15 - 3V_B}{100 k\Omega} = I_B$$

$$\frac{V_B - 0.7}{153 k\Omega} = \frac{15 - 3V_B}{100 k\Omega}$$

$$100V_B - 70 = 15 \times 153 - (15)(3)V_B$$

$$559V_B = 2365$$

$$\frac{15 - V_C}{R_C} = I_C$$

$$-I_C R_C + 15 = V_C$$

$$V_C = 9.25$$

$$V_B = 4.23V$$

$$V_E = 3.55V$$

$$V_C = 9.25V$$

$$I_B = 23.1 \mu A$$

$$I_C = 1.15 mA$$

$$I_E \approx 1.15 mA$$

β	$I_C (\mu A)$	$I_B (\mu A)$	$I_E (\mu A)$	$V_C (V)$	$V_B (V)$	$V_E (V)$
100	1.29	12.9	1.29	8.55	4.57V	3.87
50	1.15	23.1	1.15	9.25	4.23V	3.55
0/0	10.85	99.06	10.85	8.18	7.4	8.78

(2.3) In both the cases the BJT is present in the forward active mode.

We can show this through the calculations, as initially we started off with taking $V_{BE} = 0.7V$ and later arrived at the conclusion $V_{CE} > 0.2$ which proves our initial assumption that both are forward active is true.

* as from our calculations we can say V_{BE} or Base-emitter is forward biased and collector-base is reverse biased due to decrease in β have in this circuit there's been a drastic change in I_B .

(3.3)

* below 0.24 is deep saturation $I_C \approx 0$ goes to cutoff

* forward active ($0.65 - 0.71$) * ($0.25 - 0.26$) saturation to 0.30

S.No	V_{CE}	(I_{B1})	(I_{B2})	(I_{C1})	(I_{C2})	ΔI_C	ΔI_B	β
1	100mV	50mA	60mA	5.34mA	6.21mA	0.87mA	10mA	87
2	600mV	50mA	60mA	18.95	15.29	-3.66	2.34mA	234

β at saturation (100mV) 87

β at active (600mV) 234

(sat to active)

Incremental:

Difference observed b/w β at different V_{CE} because collector goes into reversed bias while V_{CE} going from saturation to active mode

$$V_{CE} \quad I_C(\text{mA}) \quad I_B(\text{mA}) \quad \beta = \frac{I_C}{I_B}$$

~~-178.68~~ 0 —

IV	2.8	10	280
IV	5.5	20	275
IV	8.1	30	270
IV	10.61	40	265
IV	13.04	50	260
IV	15.39	60	256
IV	17.68	70	252
IV	19.91	80	248
IV	22.09	90	245
IV	24.2	100	242

Then $I_B \downarrow$ and
thereby $\uparrow B = \frac{I_C}{I_B \downarrow}$
Hence, β increases

Yes, Early effect is observed (Base-Width modulation) causes β to increase as V_{CE} \uparrow as since higher V_{CE} reduces the base width, so, I_C increases in very small amount.

Let $I_B = 60 \text{ mA}$

Since slope is same

w.r.t. given

slope = $I_C / (V_A + V_{CE})$ equating slopes.

$$\text{at } 5V \Rightarrow \frac{13.88}{V_A + 5V} = \frac{14.94}{V_A + 10V} \text{ at } 10V$$

$$14.94V_A - 13.88V_A + 5 \times 14.94 = 10 \times 13.88$$

$$1.06V_A = 6.41$$

$$V_A = 60.47 \text{ approx (60)}$$

(3.2) from the graph.

V_{BE} decreases $-1.6 \text{ to } -2 \text{ mV per } {}^\circ\text{C}$ ~~is~~
almost linear.

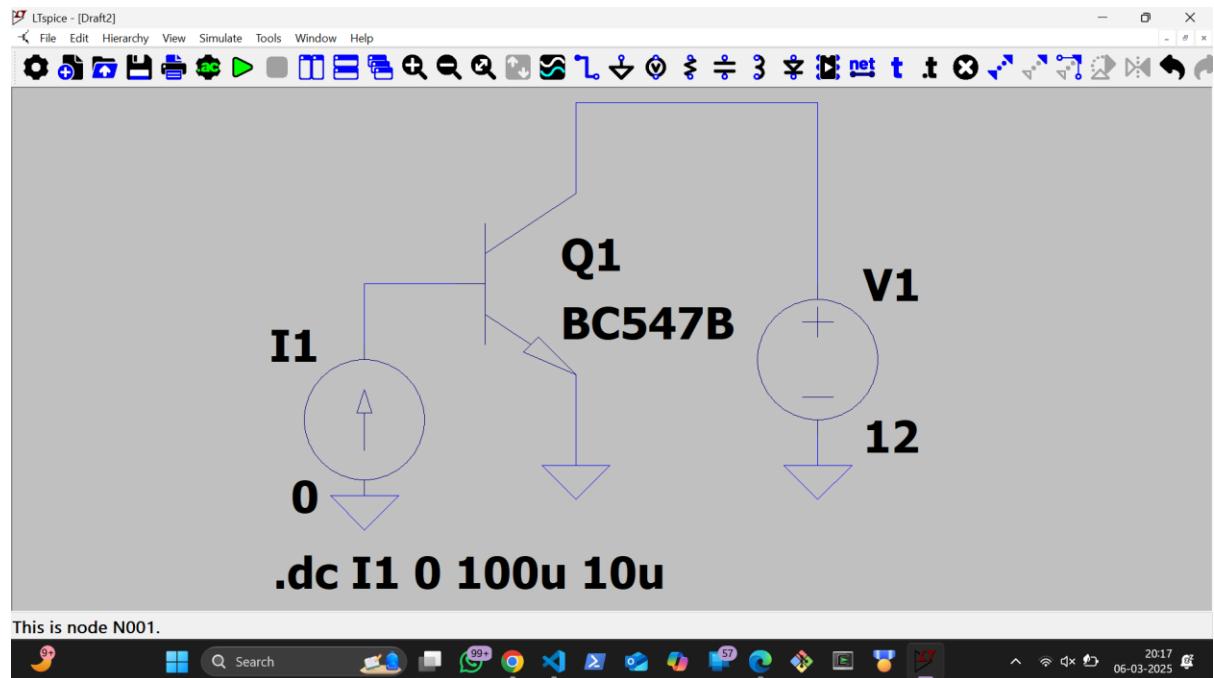
(3.1) from plot we get EBJ (Emitter base Jⁿ)

- voltage to be about $700-740 \text{ mV}$

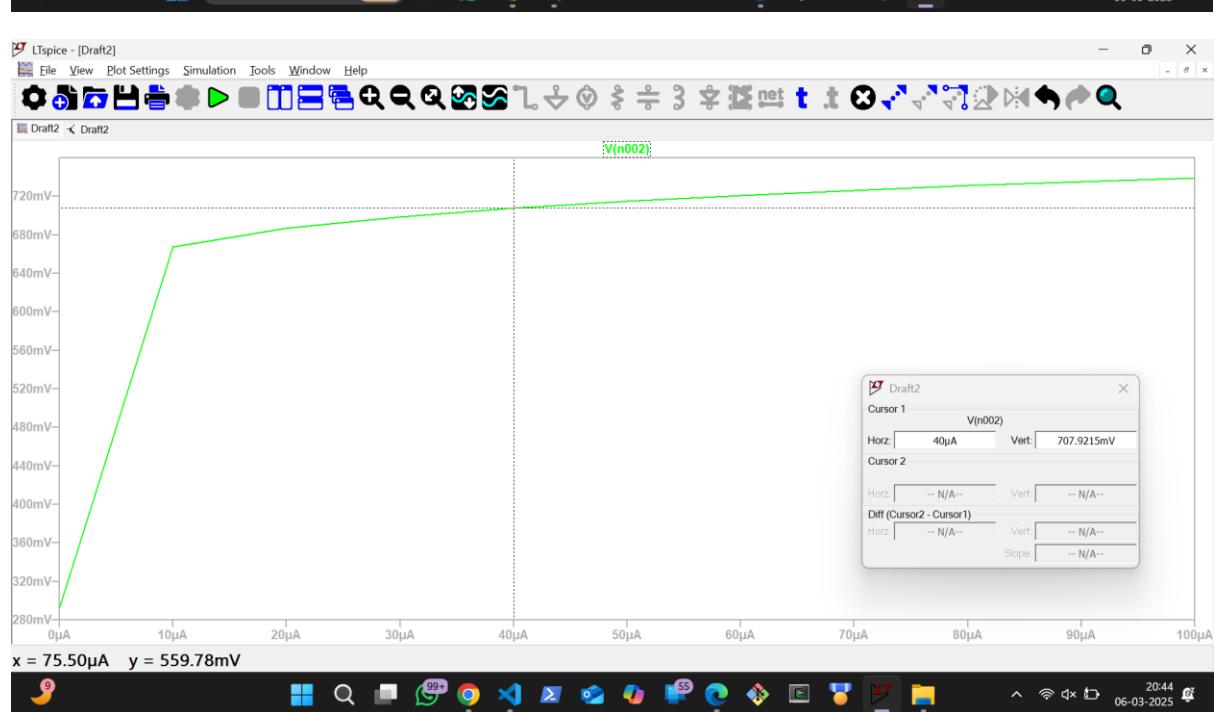
from above plots for BJT in active/saturation

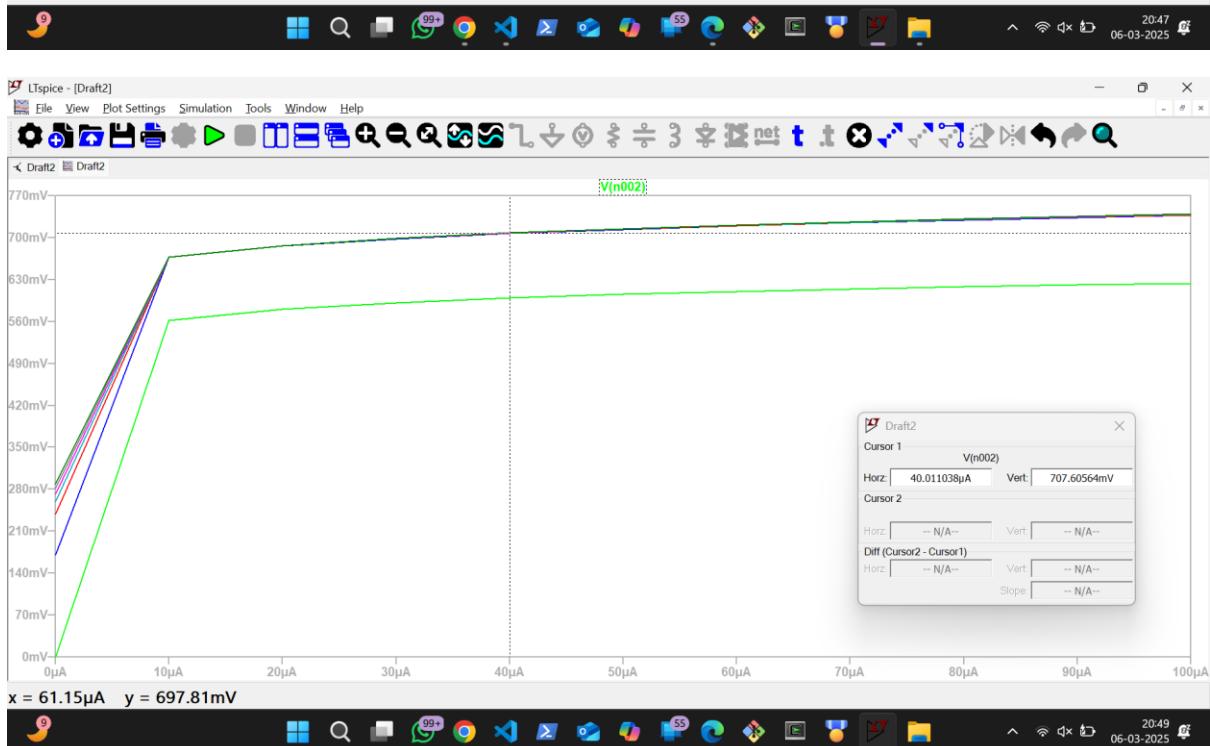
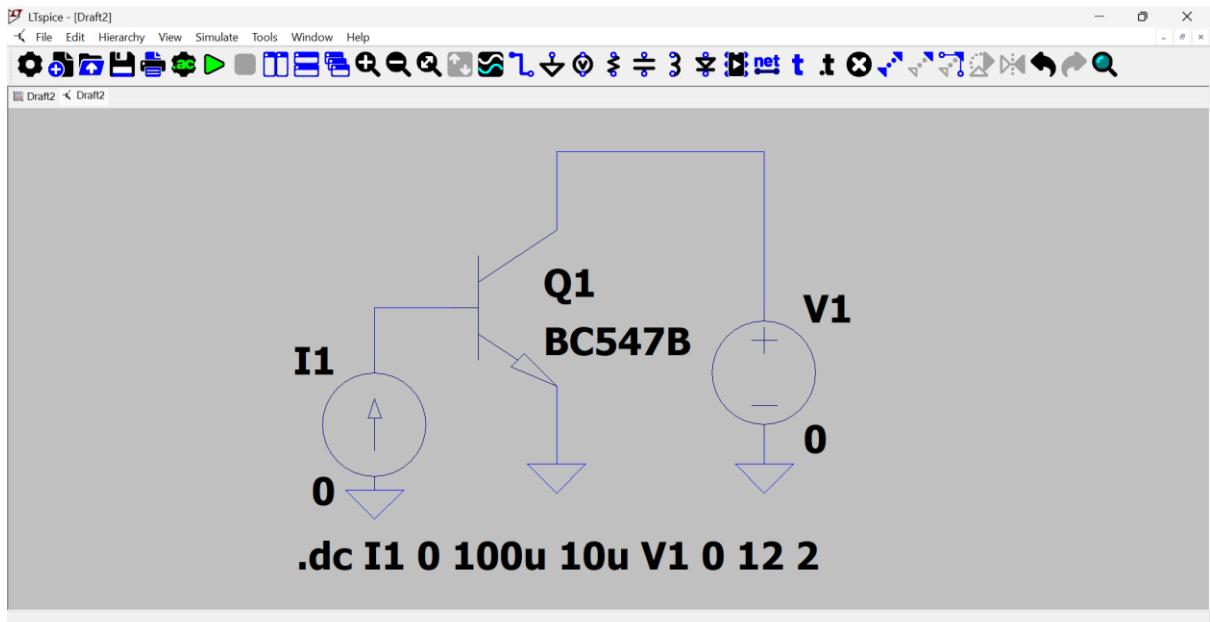
we need to have V_{BE} greater than the EBJ voltage

Q-3.1

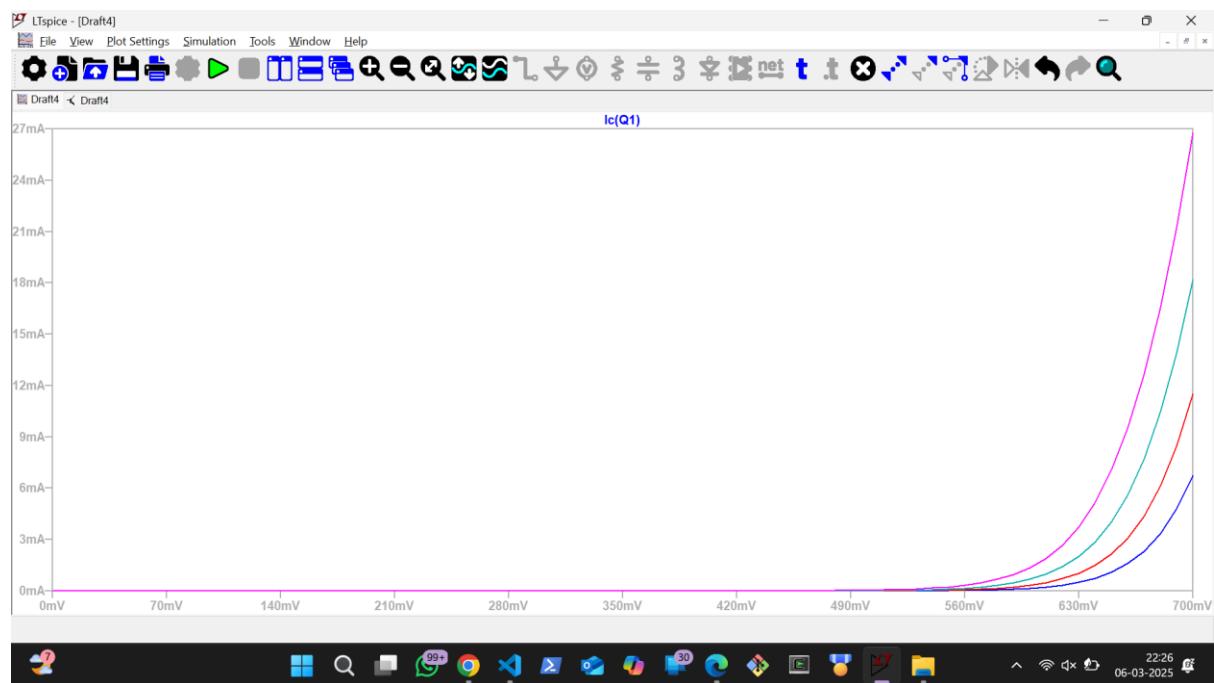
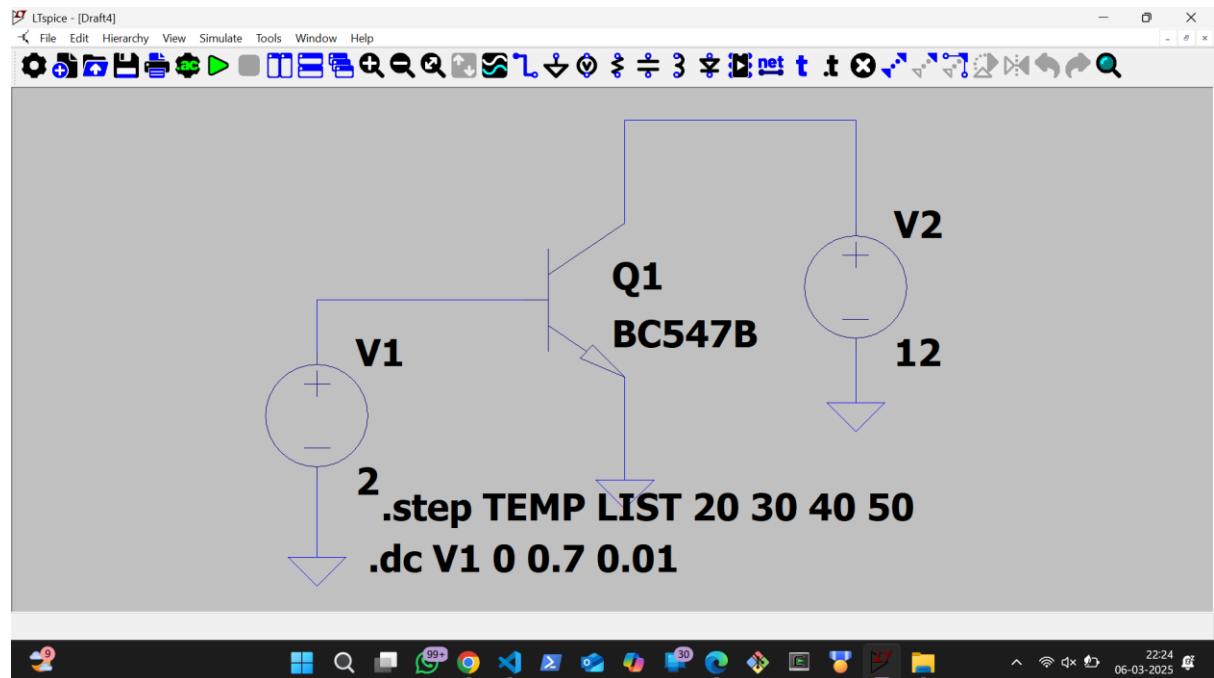


This is node N001.

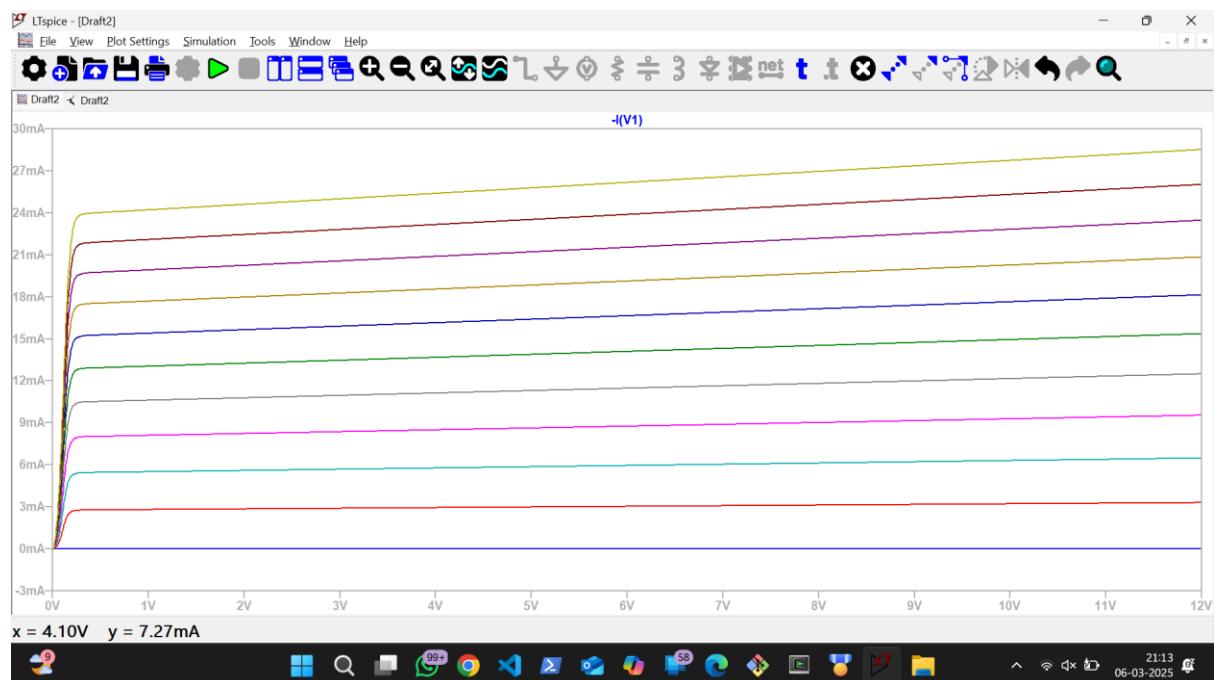
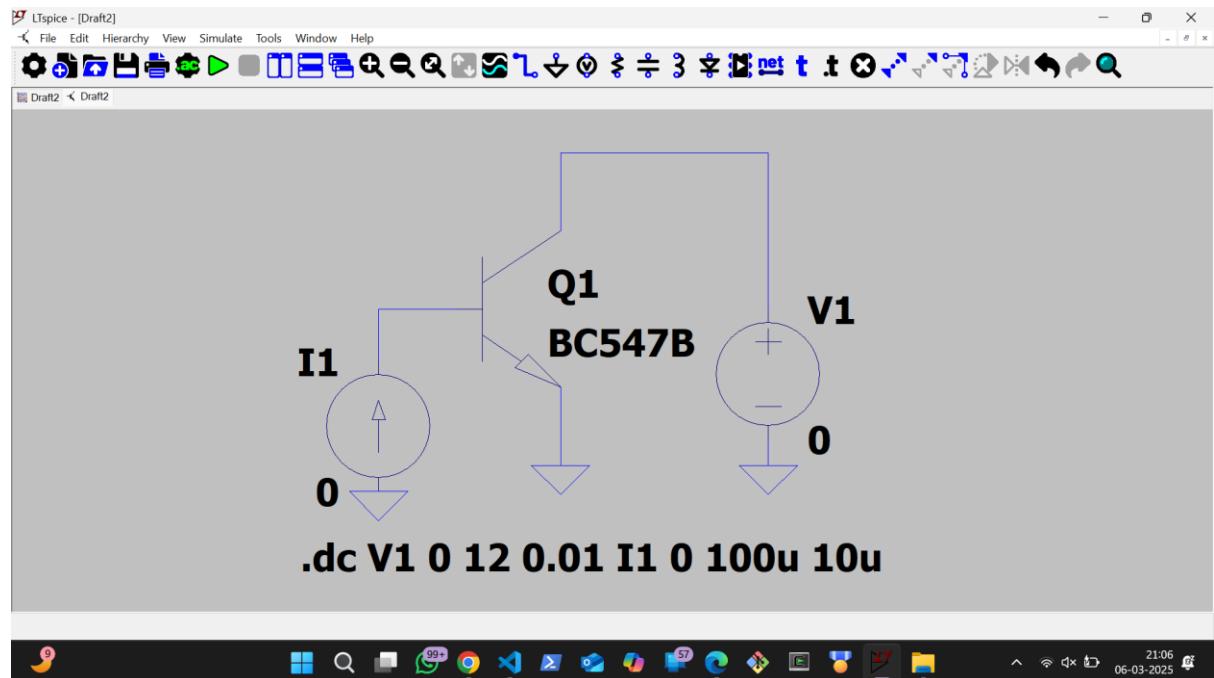




Q-3.2

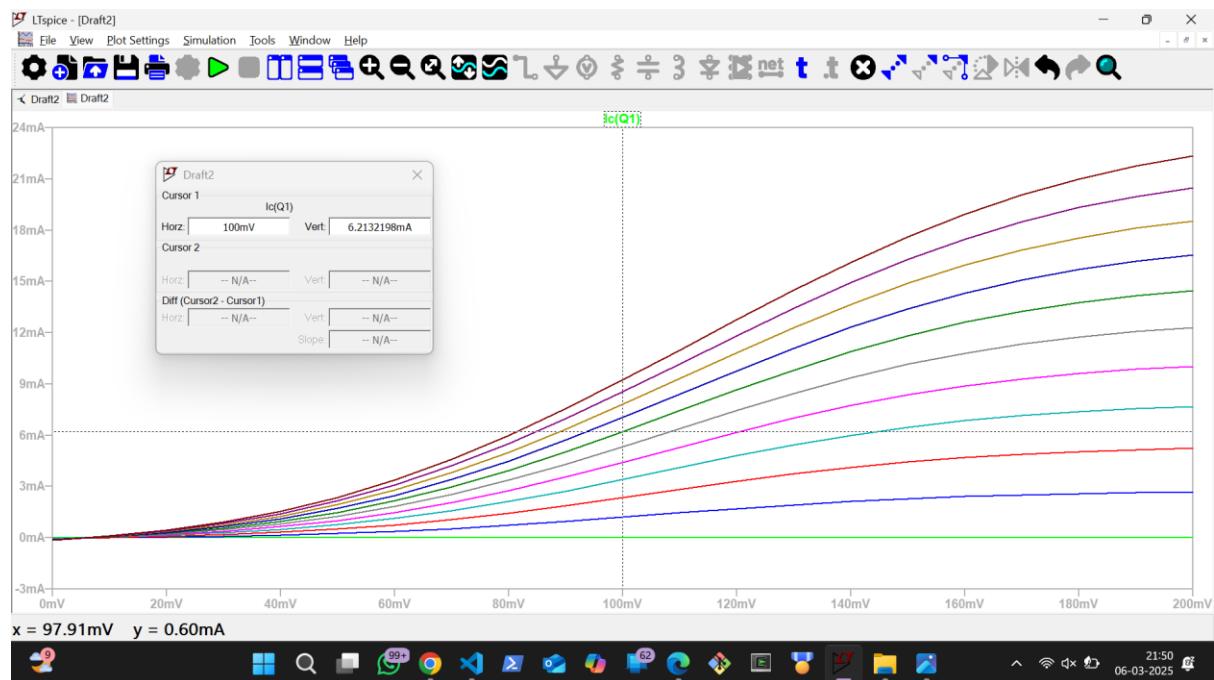
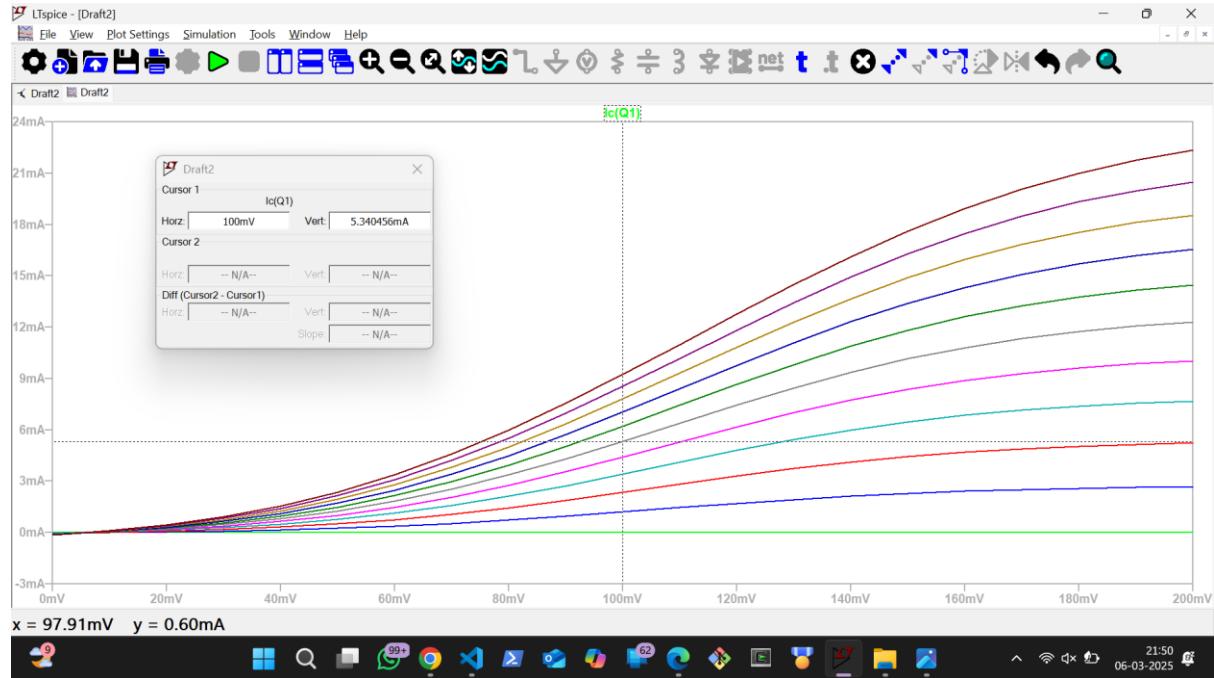


Q-3.3

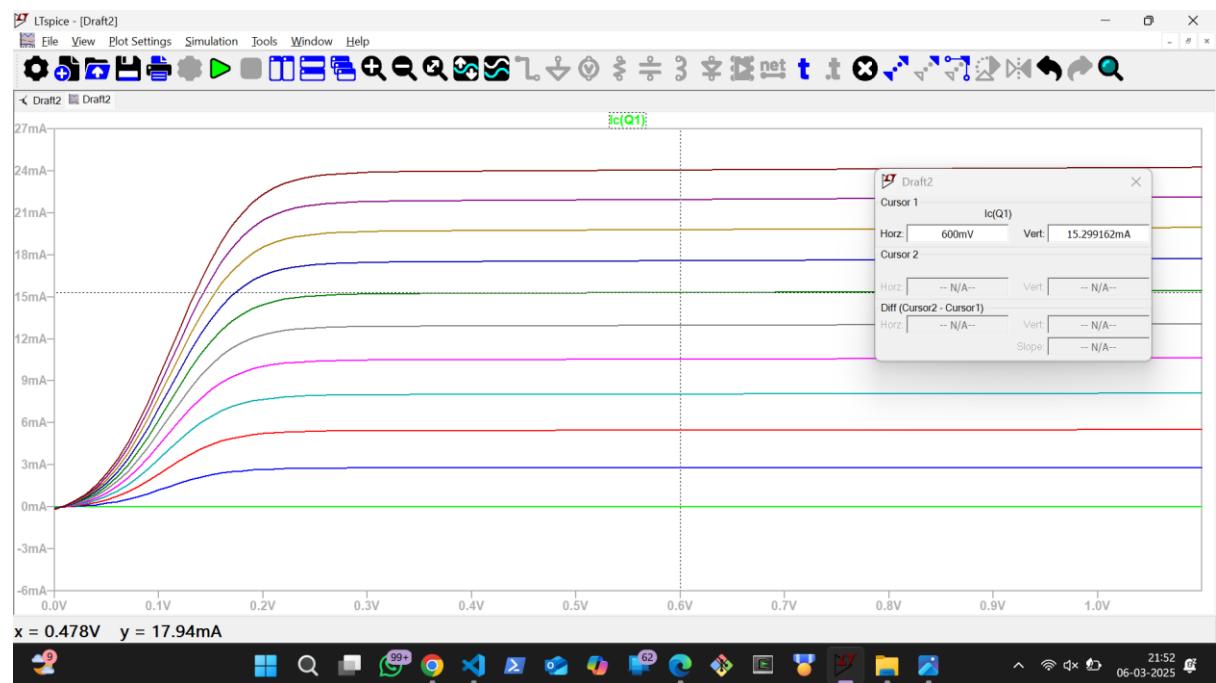
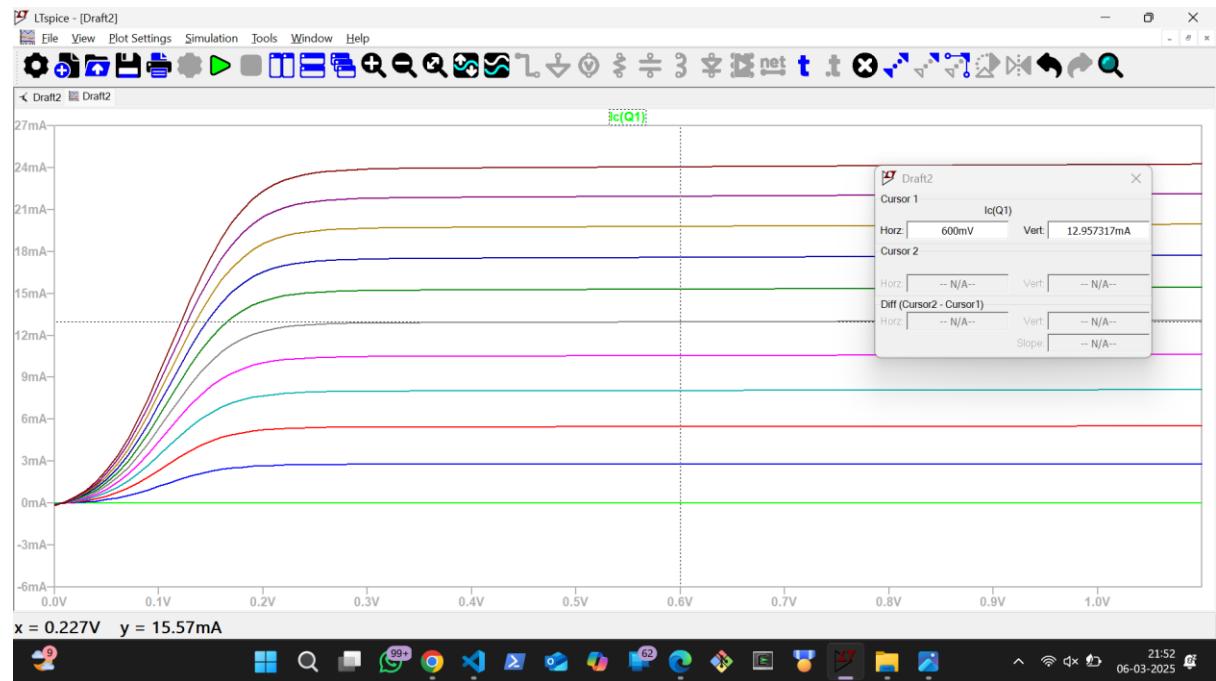


Calculation of beta(β) by change in currents of I_C and I_B at 50uA and 60uA

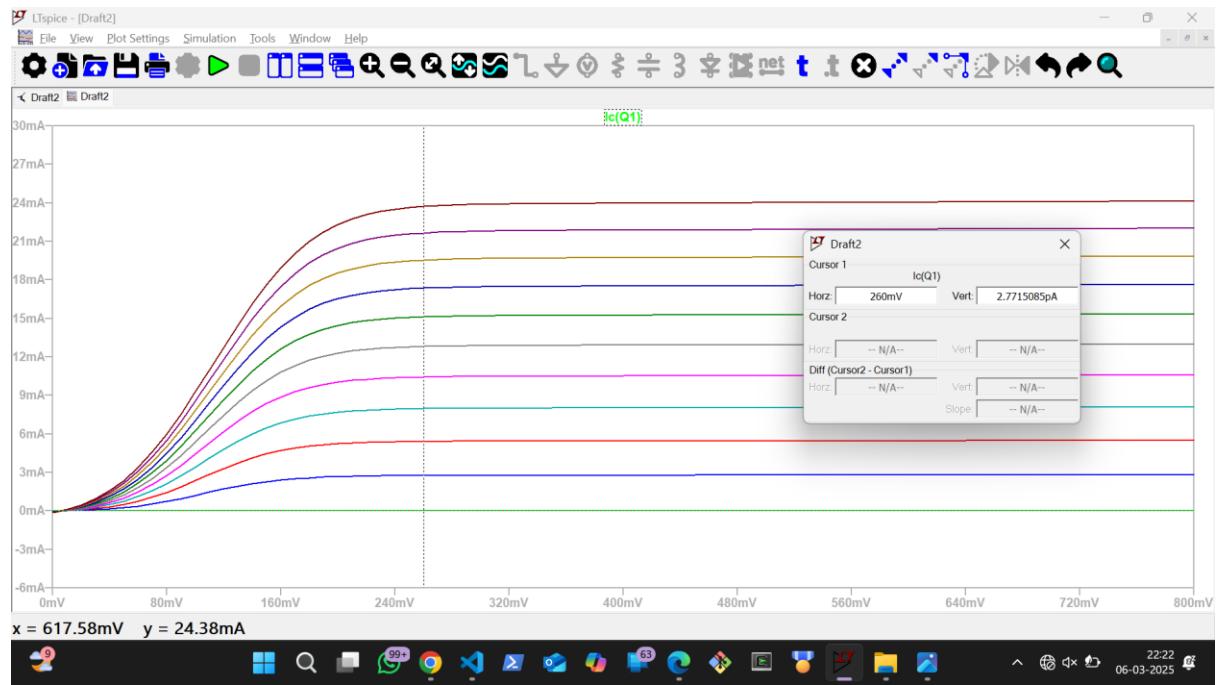
At 100mV



At 600mV



Saturation and Active mode mark

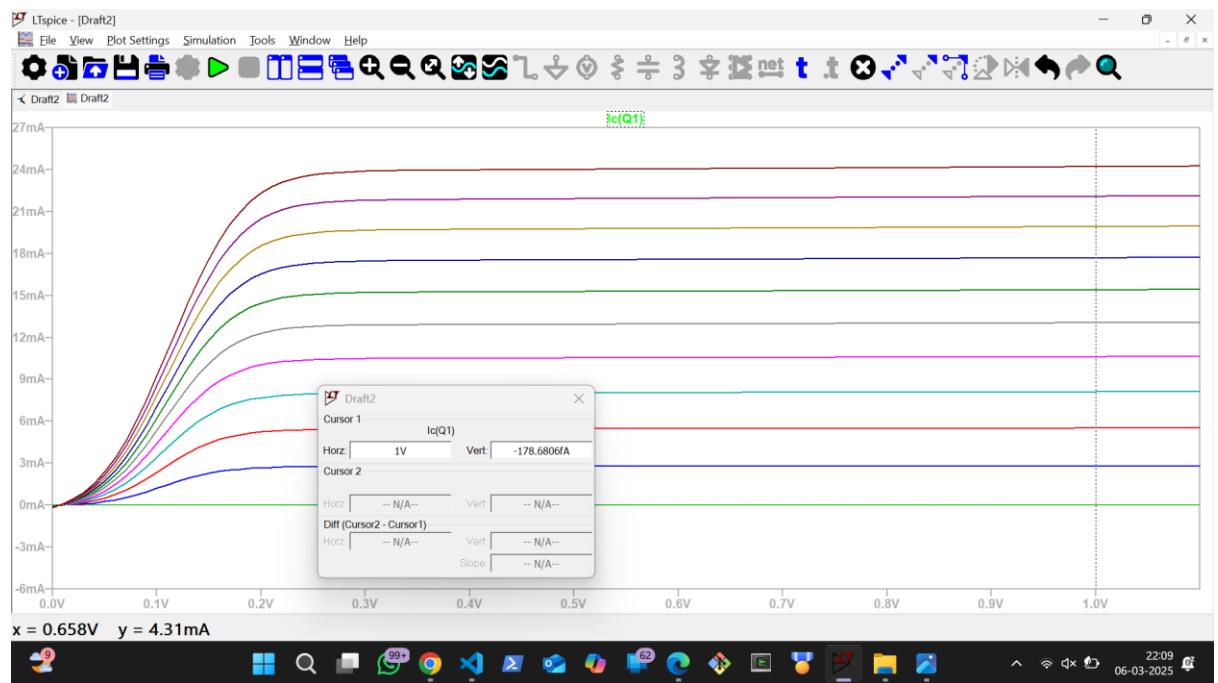


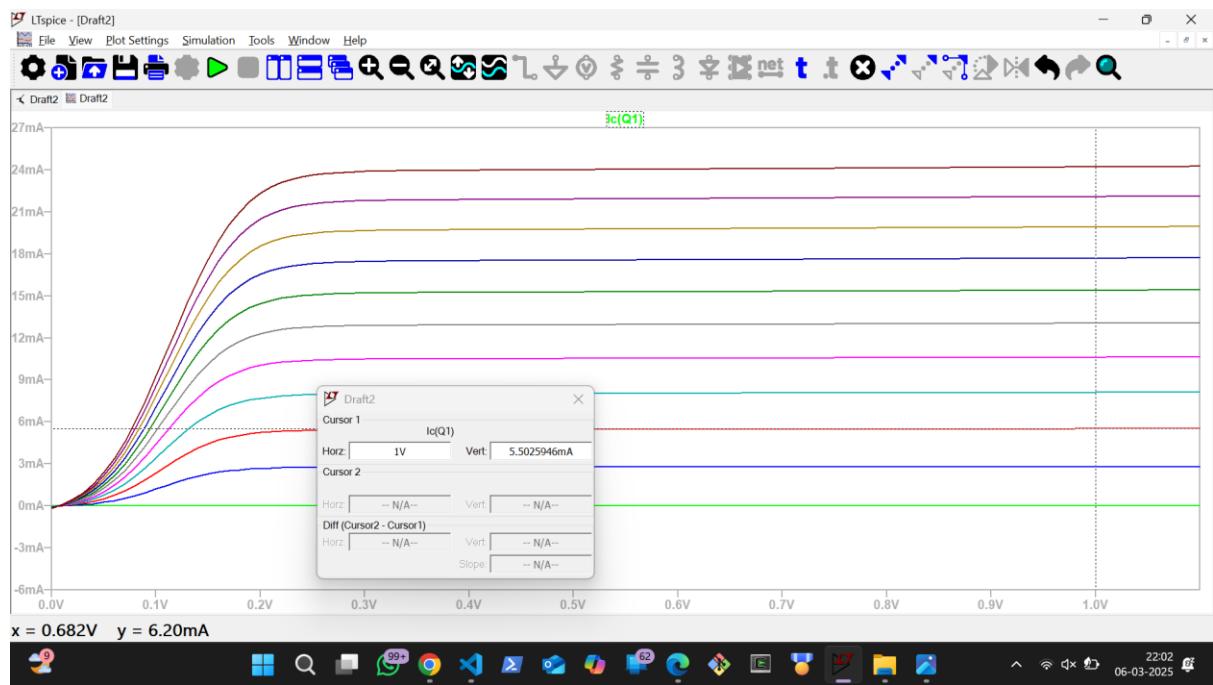
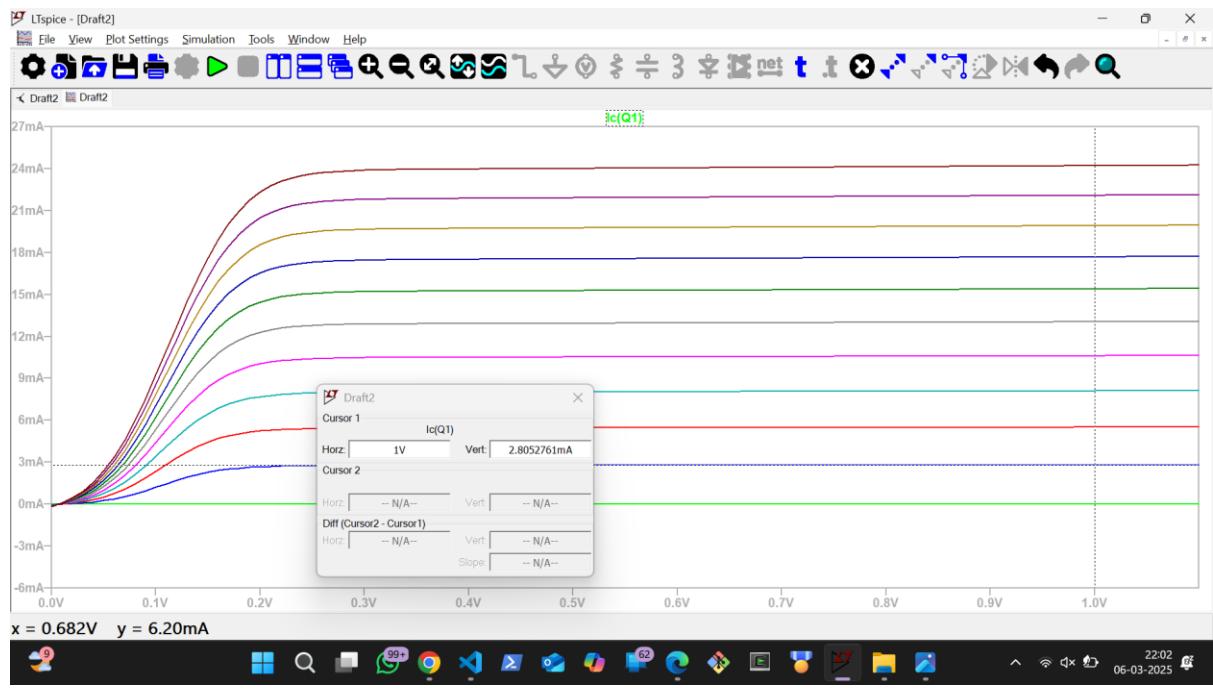
220mV-260mV-300mV saturation

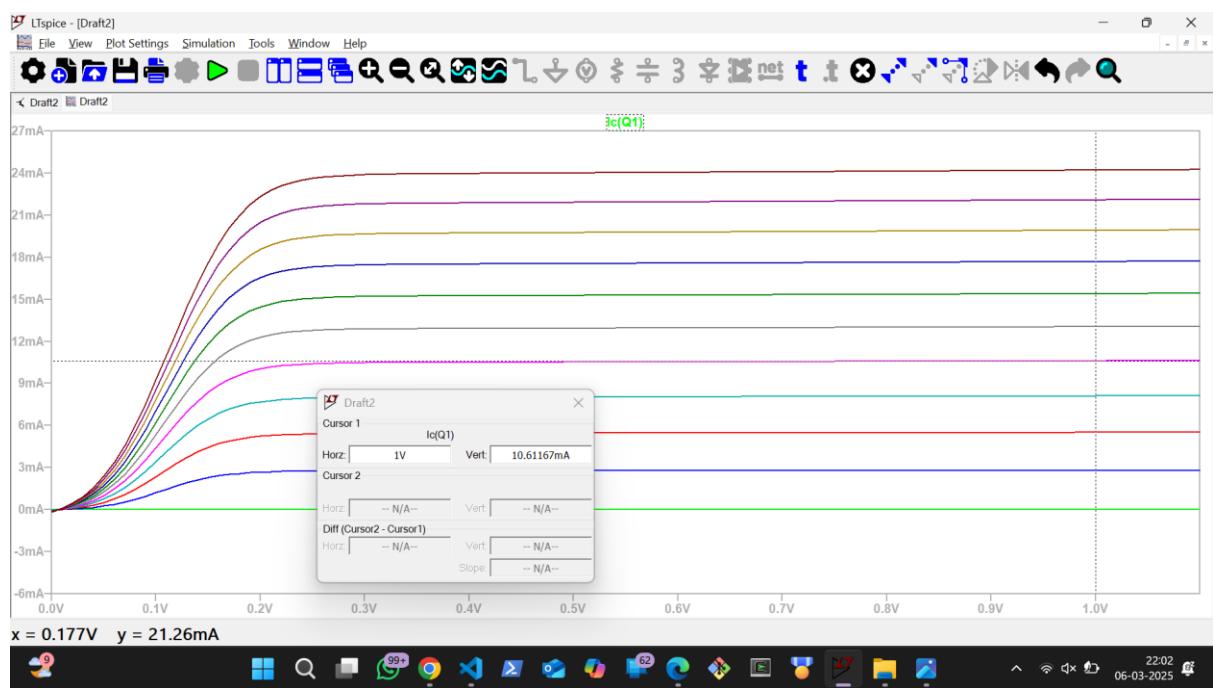
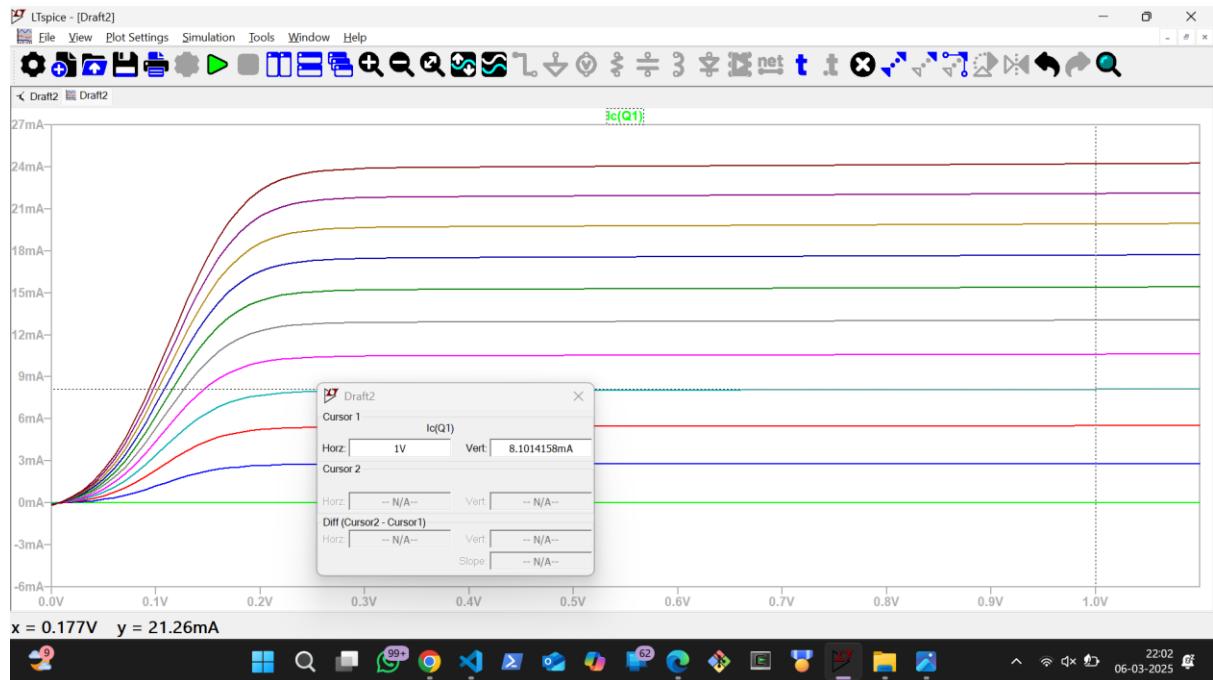
Above it is active mode

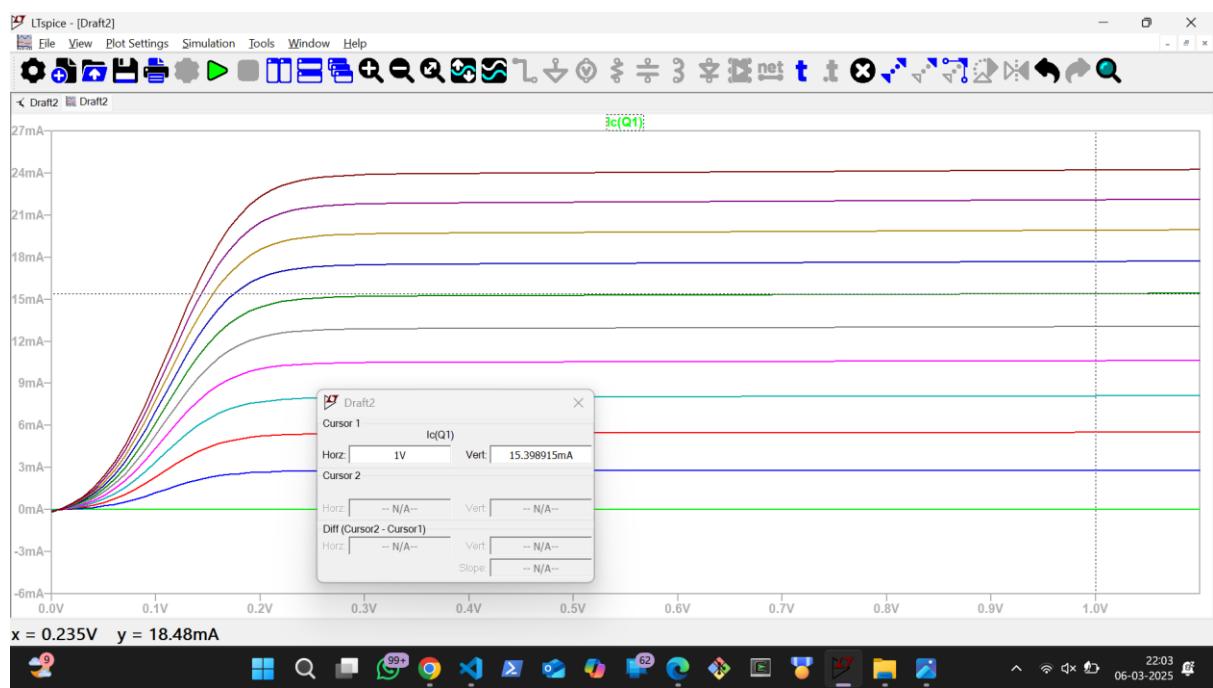
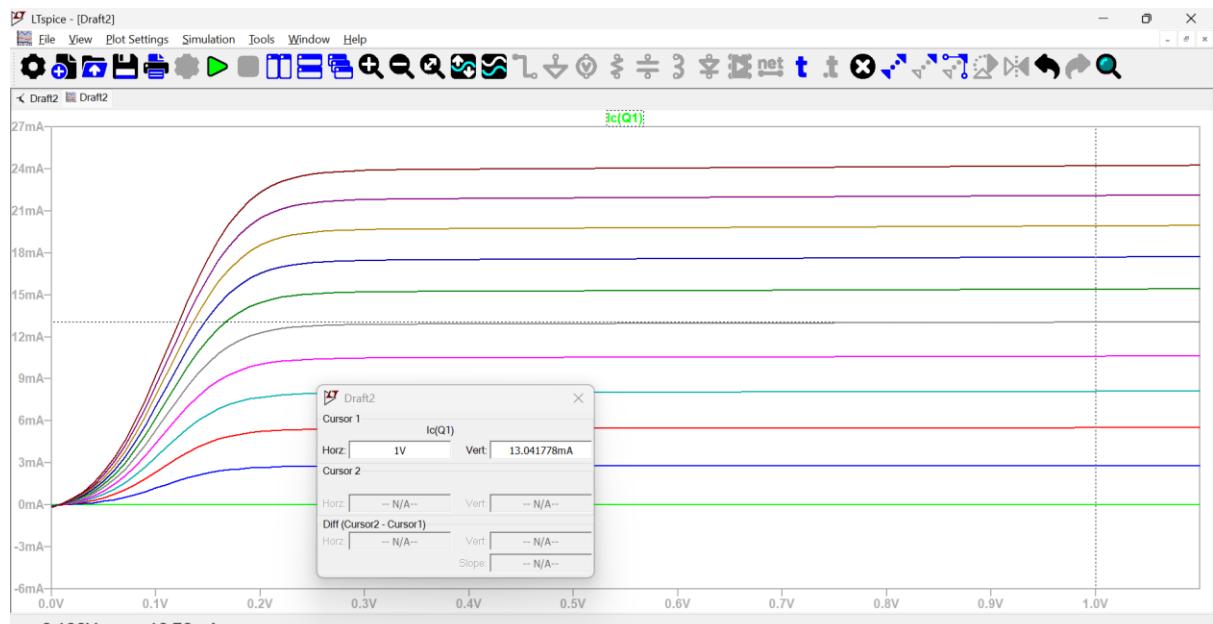
Below it is $I_c \sim 0$ and cutoff mode

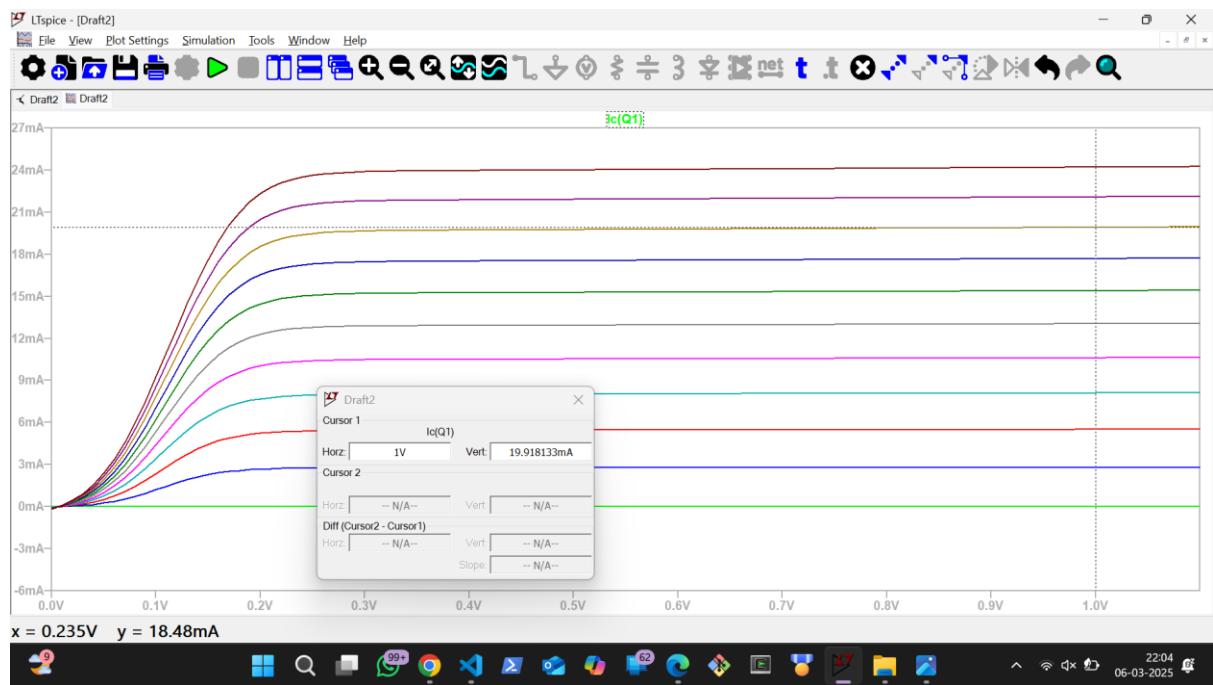
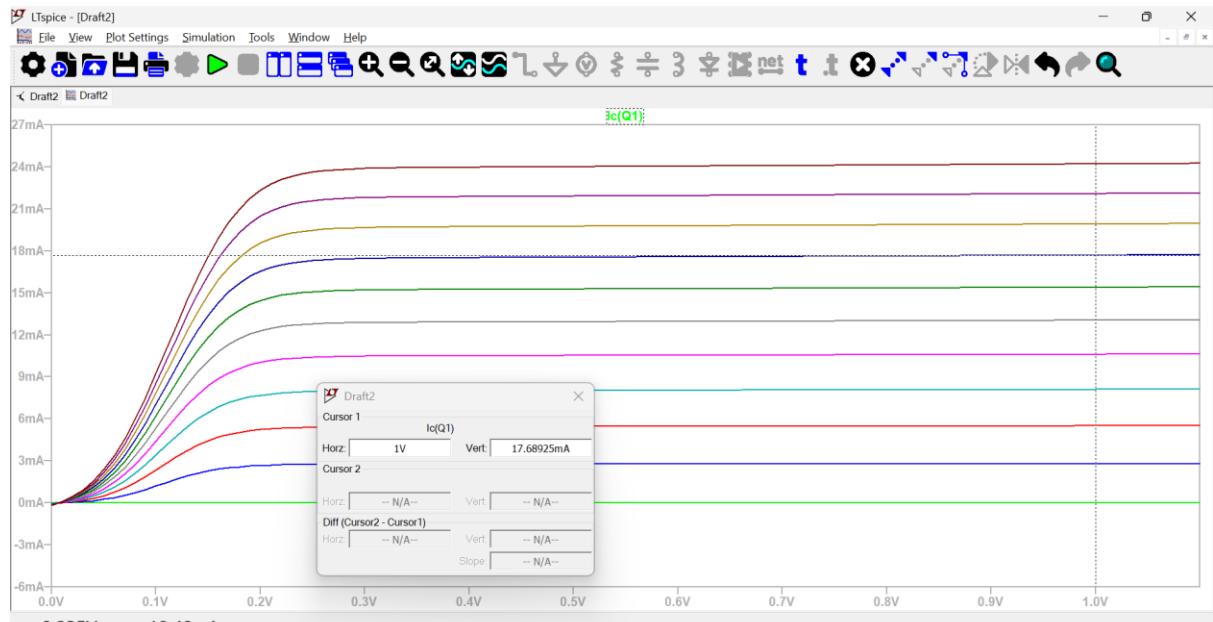
Tabulating β at 1V by I_c and I_b

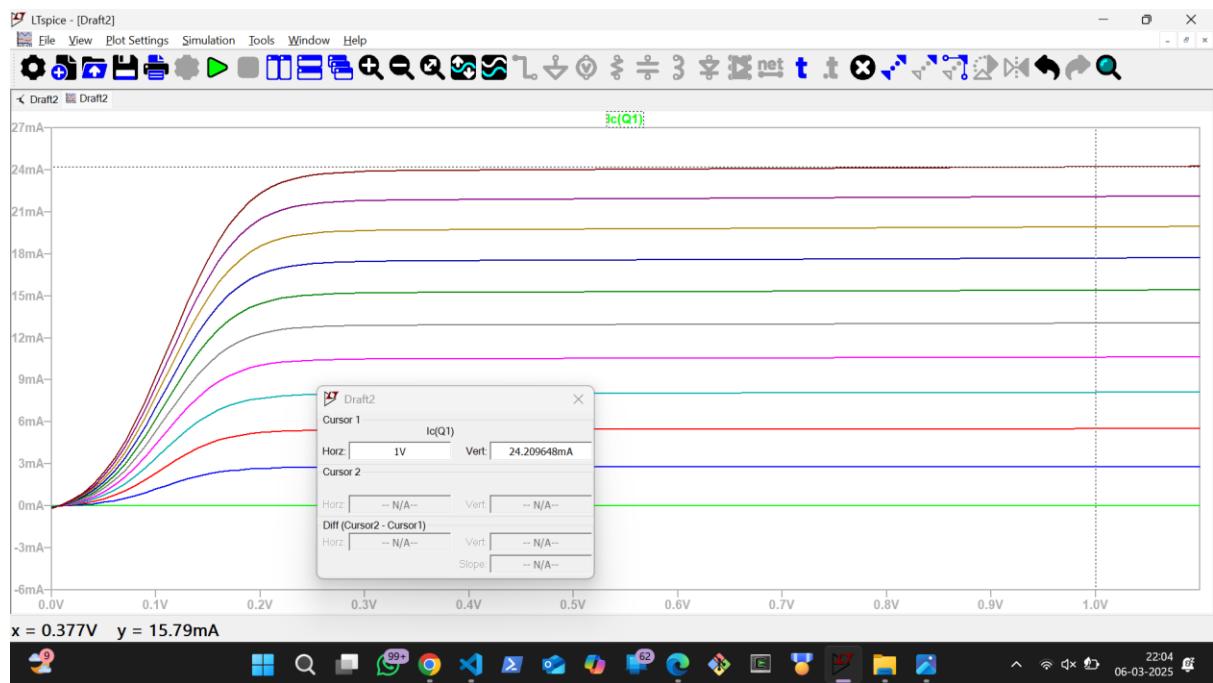
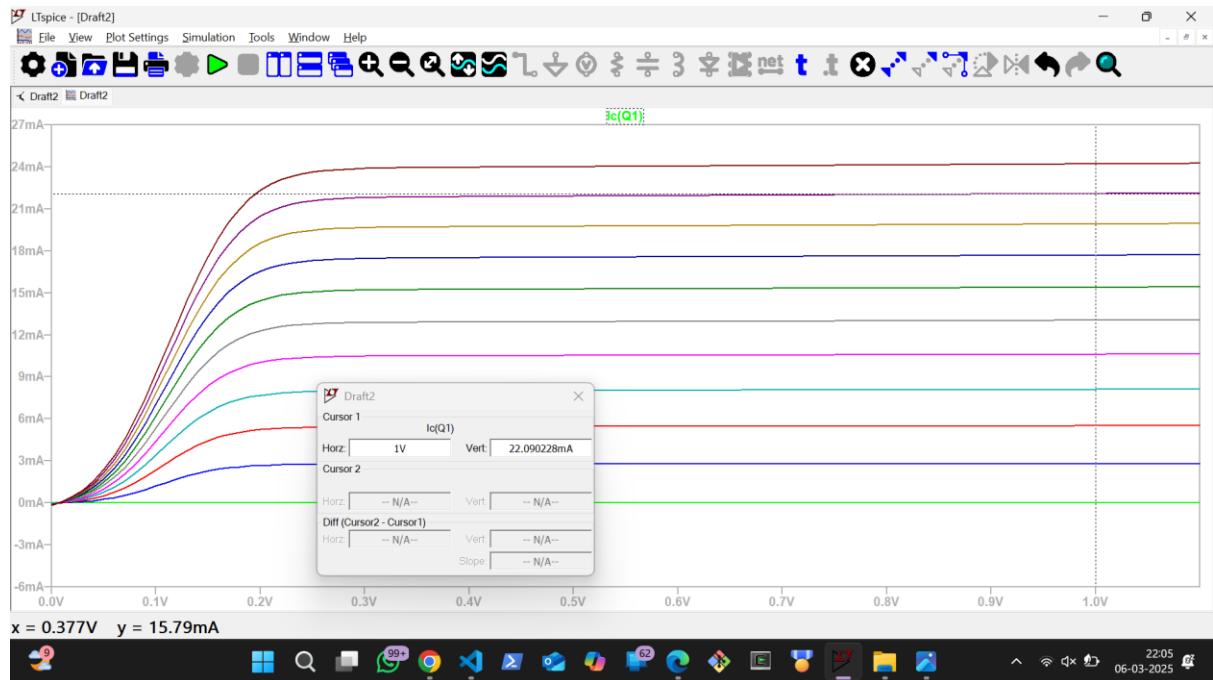












By these 11 values tabulated and calculated β

Early Voltage VA

VA is 60.47V

