

Analog Electronic Circuits Lab (EC2.103, Spring 2025)

Lab Report – 7: Common Source Amplifier

Name: Chanda Akshay Kumar

Roll No 2024102014

Team Member Name: S V Santhosh

Team Member Roll.No 2024102054

1. Objectives

1. To analyze the effect of body bias on the gain of a Common Source (CS) amplifier.
2. To study the impact of bias voltage (VBIAS) on the amplifier's gain.
3. To observe the effect of input signal swing on amplifier gain and clipping behavior.
4. To analyze the frequency response of a CS amplifier with external coupling.

2. Equipment Used

1. Breadboard
2. NMOS transistor (CD4007BE)
3. DC power supply
4. Function generator
5. Digital Multimeter (DMM)
6. Oscilloscope
7. Resistors: $RL=4.7\text{ k}\Omega$, $RBIAS=\text{few } 100\ \Omega$
8. Capacitors: $CC=10\ \mu\text{F}$, $CL=470\ \text{pF}$

3. Theory

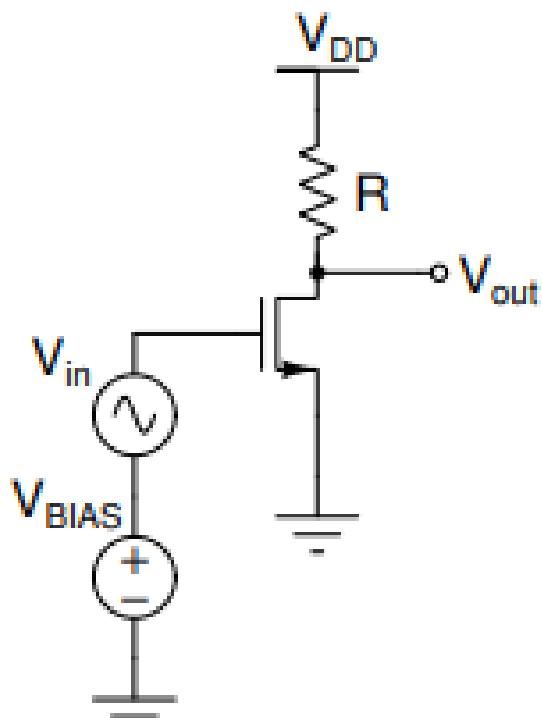
The Common Source (CS) amplifier is a fundamental MOSFET amplifier configuration. Key parameters include:

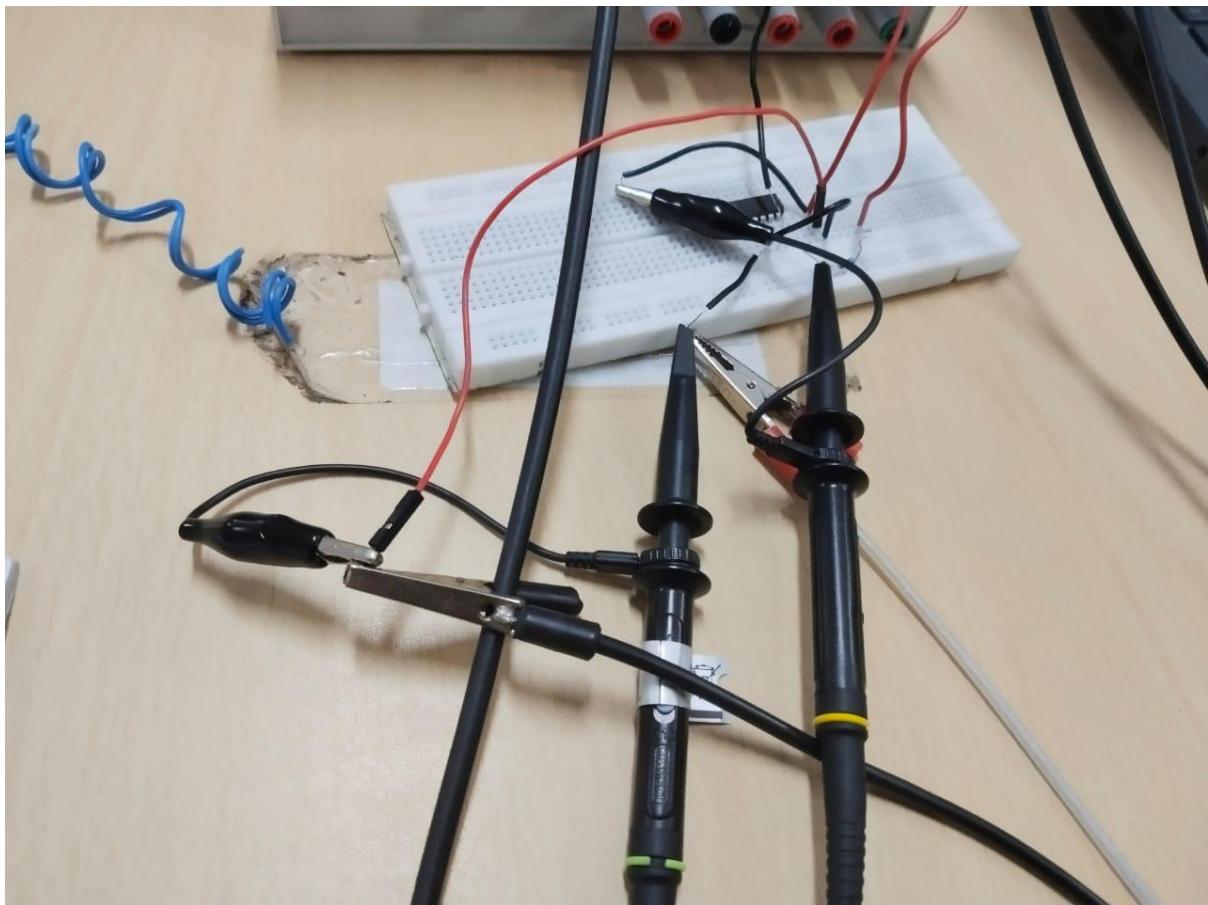
- **Voltage Gain (A_v):** $A_v=-gmRL$

- **Transconductance (gm):** $gm = \mu_n C_{ox} W L (V_{GS} - VT)$
- **Body Effect:** Changes in V_{SS} alter the threshold voltage (VT), affecting gm and gain.
- **Clipping:** Occurs when the output exceeds the linear range of the amplifier.
- **Frequency Response:** Determined by coupling and load capacitances.

4. Experimental Procedure & Observations

4.1 Effect of Body Effect on Gain





Circuit: CS amplifier with $VDD=5V$, $VBIAS=2.5V$, $RL=4.7\text{ k}\Omega$.

(a) DC Measurements

- Measured $VDS=3.5V$
- Calculated $IDS=(VDD-VDS)/RL=0.31\text{ mA}$
- Calculated $\mu nCoxWL=1.27\text{ A/V}^2$
- Calculated $gm= mS$

(b) AC Measurements

- Applied $vin=50\text{ mVpp}$, $f=1\text{ kHz}$
- Measured $vout=200\text{ mVpp}$
- Calculated Gain (Av) = $vout/vin=4$
- Calculated $gm(\text{effective})=0.91\text{ mS}$

LAB-7

(a) When we take V_{GS} as ~~20~~ V we

get $V_{DS} = 180 \text{ mV } \cancel{\text{approx}} \quad 1.55 \text{ V}$

~~V_{DD}~~ $V_{DD} = 5 \text{ V}$

$\Rightarrow 5 - (I_D)(4.7\text{k}) = \cancel{1.55} \quad 1.55 \text{ V}$

$= (I_D)(4.7\text{k}) = 3.45 \text{ V}$

$3.45 = I_D(4.7\text{k})$

$$I_D = \frac{3.45}{4.7} \times 10^{-3} \sim 0.734 \times 10^3 \text{ A}$$
$$= 0.7 \text{ mA}$$

$$g_m = \frac{m_n C_{ox} \omega}{2L} (V_{GS} - V_{TH})^2 \left[\text{let } k = \frac{m_n C_{ox} \omega}{2L} \right]$$

$$0.73 \times 10^{-3} = \frac{k}{2} (2 - 1.8)^2$$

$$= k(0.02) = 0.73 \times 10^{-3}$$

$$= k = \frac{0.73}{2} \times 10^{-1}$$

$$= 0.365 \times 10^{-1}$$

$$g_m = k (V_{GS} - V_{TH})$$

$$= 0.365 \times 10^{-1} (2 - 1.8)$$

$$= 0.73 \times 10^{-2}$$

(b) $A_v = g_m R_L$

$$= (0.73 \times 10^{-2}) (4.7 \text{ k}\Omega)$$

$$= 0.73 \times 10 \times 4.7$$

$$= 34.31$$

$$A_v = \frac{V_{out}}{V_{in}} = \frac{220mV}{50mV} = 4.4$$

$$A_v = g_m R_L$$

$$g_m = \frac{4.4}{4.7} \times 10^{-2} = 0.93 \times 10^{-3}$$

(c) Body Effect Analysis

VSS(V)	vout(Vpp)	Gain (Av)	gm(effective)(mS)
0	220m	4	0.91
0.4	280m	4.67	1.04
-0.4	80m	1.6	0.47

$$gm(\text{effective}) = gm + gmb$$

Observation:

- As |VSS| increases, the gain changes due to the body effect (gmb).
- The equation of the Vth according to the body voltage will be given as
- $Vth = Vth0 + (\sqrt{VSB + 2(\pi)} - \sqrt{2(\pi)})$
- Increasing the body voltage above zero raises the threshold voltage, which in turn lowers the output voltage.
- Decreasing the body voltage below zero reduces the threshold voltage, leading to a higher output voltage.
- gmb affected by bias voltage at body which changes VTH(threshold)

The initial bias voltage (Vbias) was set to 2.5V, but the MOSFET did not enter the saturation region as expected. This happened because Vds was too low, making it less than Vgs minus Vt. To fix this, the bias voltage was reduced to 2V, which increased Vds and ensured that the MOSFET operated in the saturation region. This adjustment was needed because Vgs was already less than Vt, preventing proper operation in the previous setup.

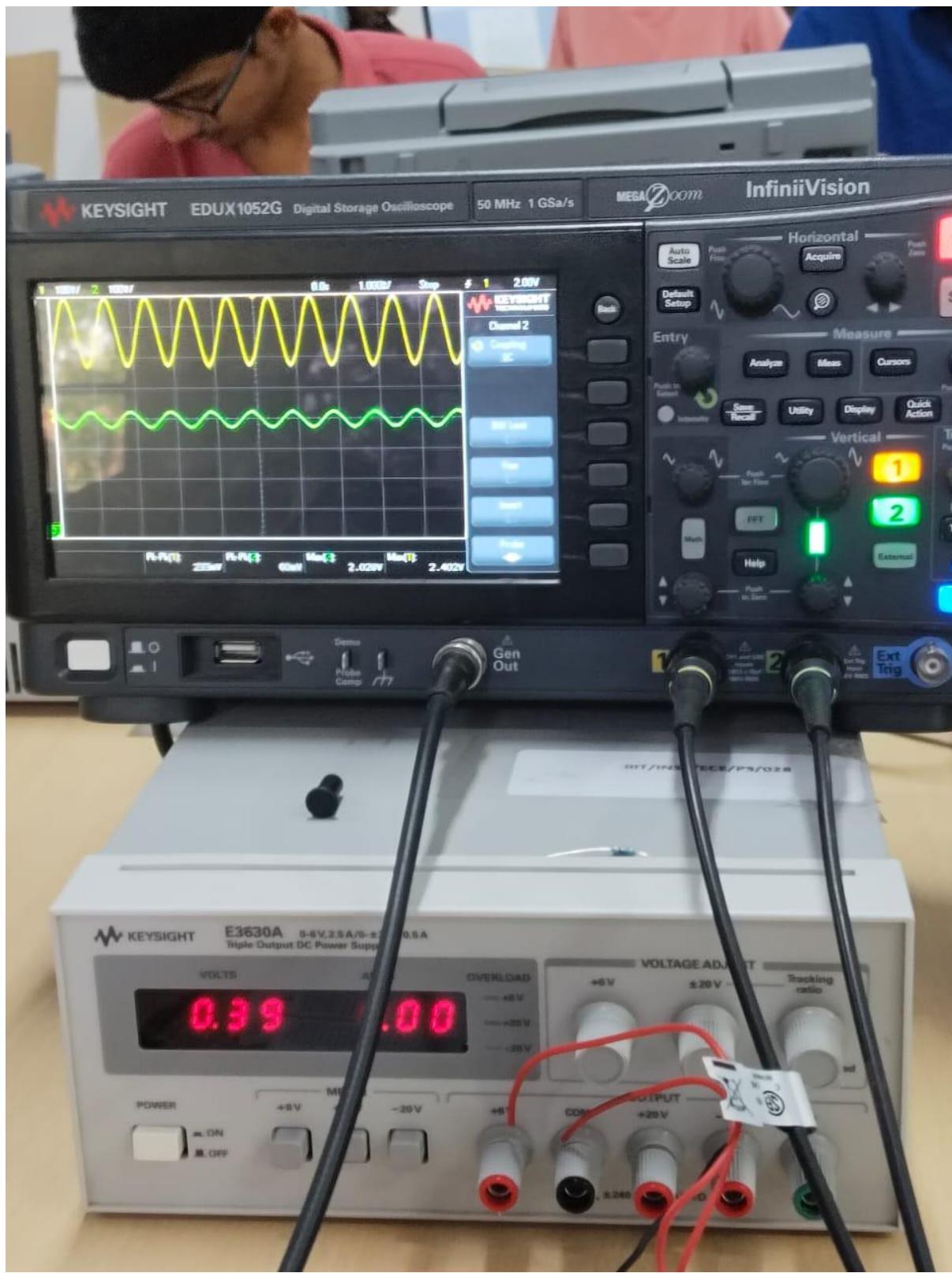
$$Vbias = 2V$$



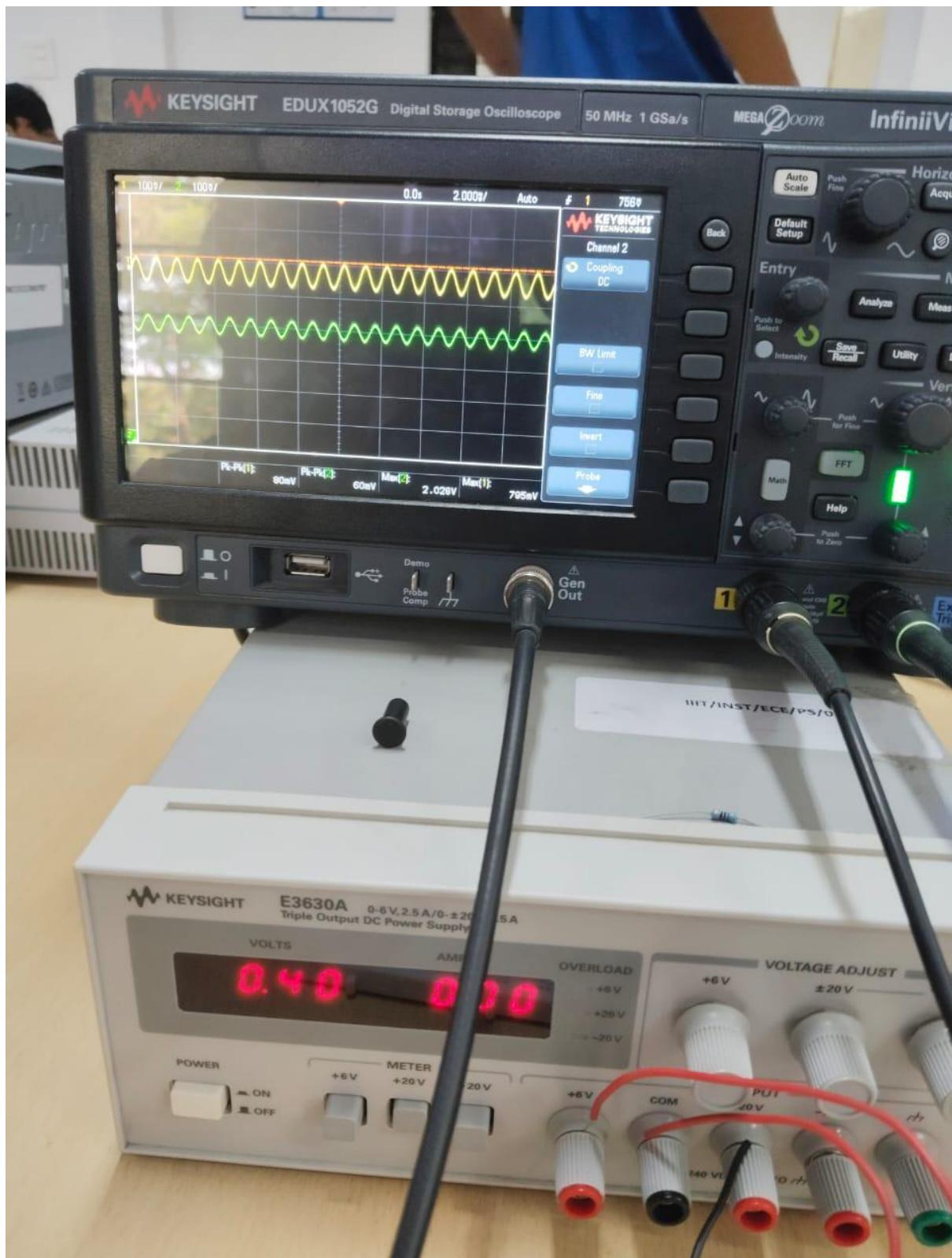
Vbias=2.5V



VBS=-0.4



VBS=+0.4



4.2 Effect of Bias Voltage on Gain

By changing v_{bias} we need to observe what changes has occurred on the parameters v_{out} , gain, gm etc.,,

With Fixed $v_{in}=100 \text{ mVpp}$, $f=1 \text{ kHz}$

And also we need to plot gm vs $VGS(\text{bias})$ in notebook

Wkt,

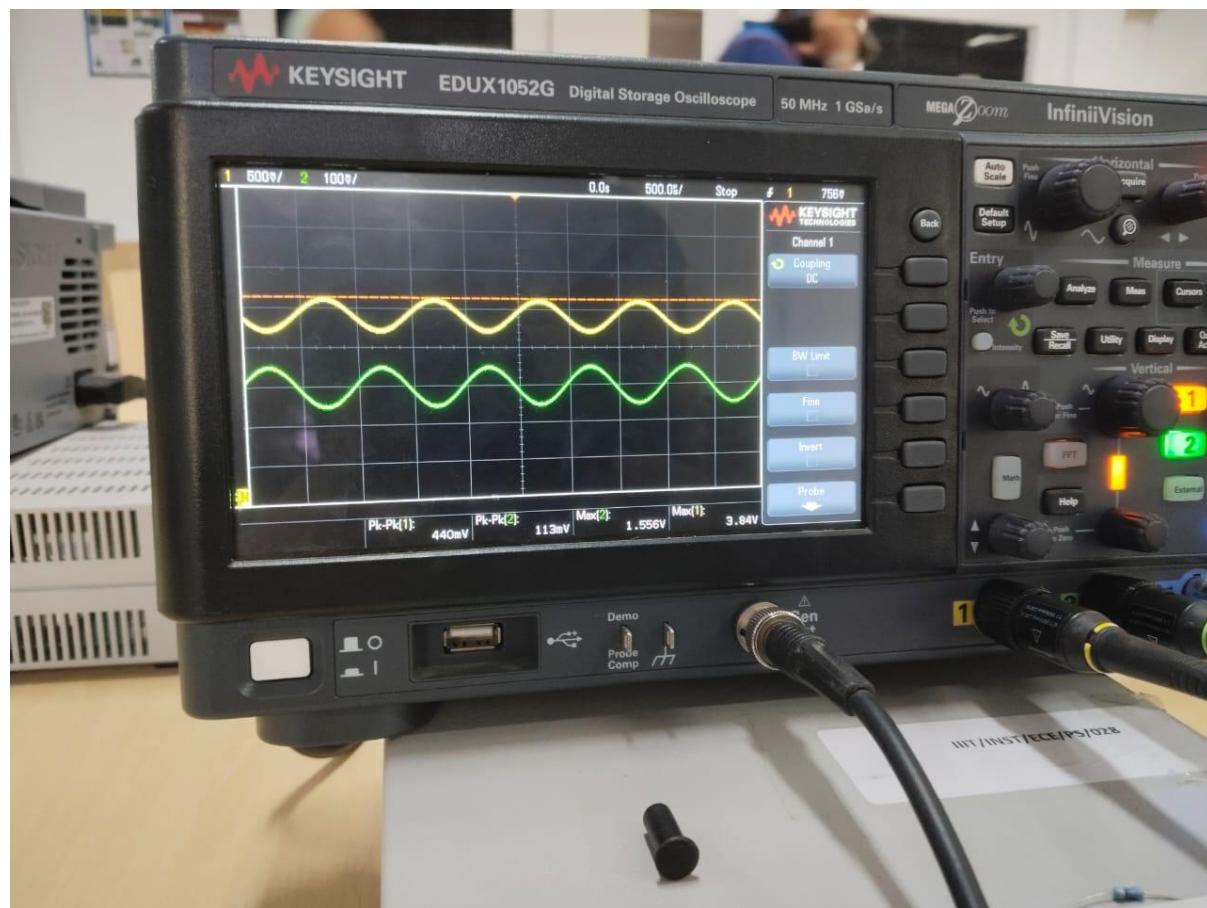
$$Av = V_{out}/v_{in}$$

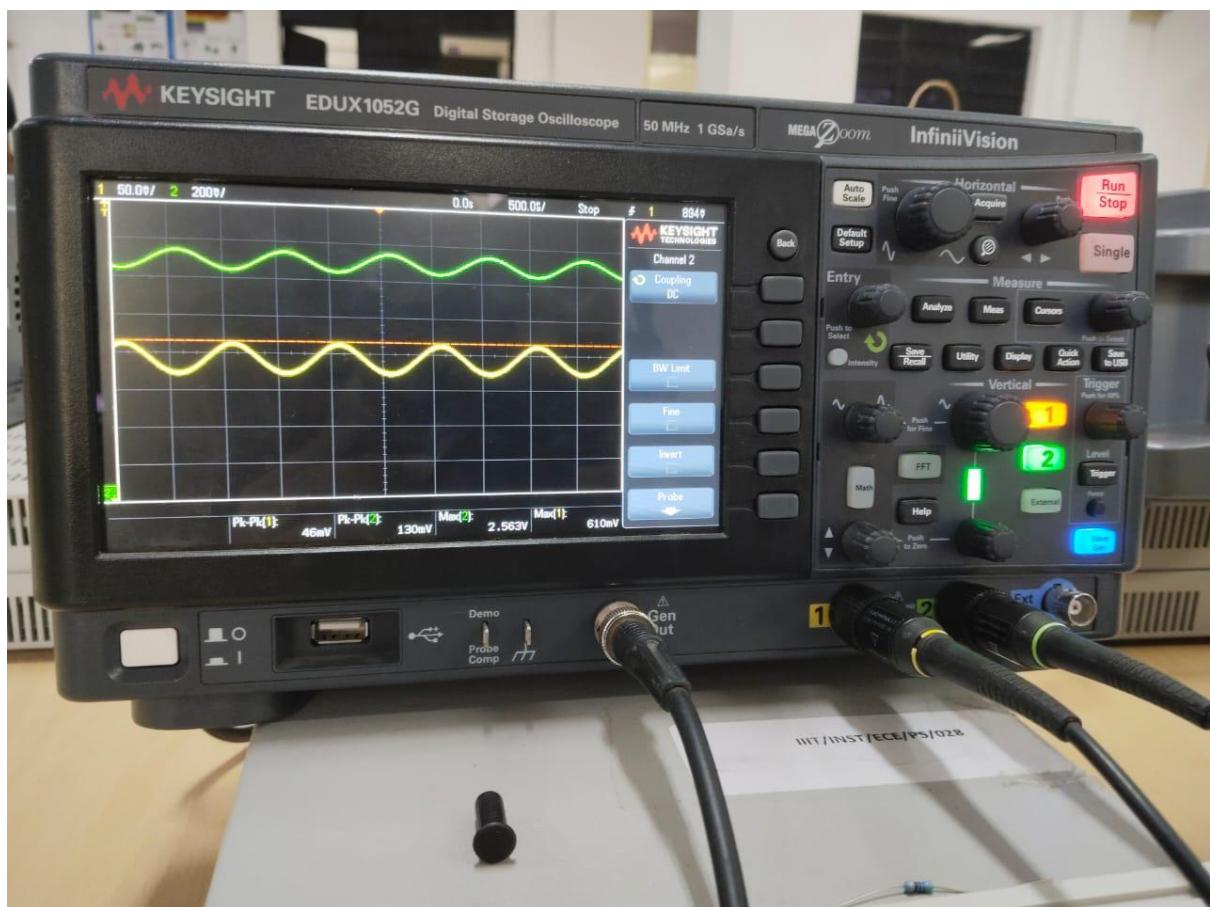
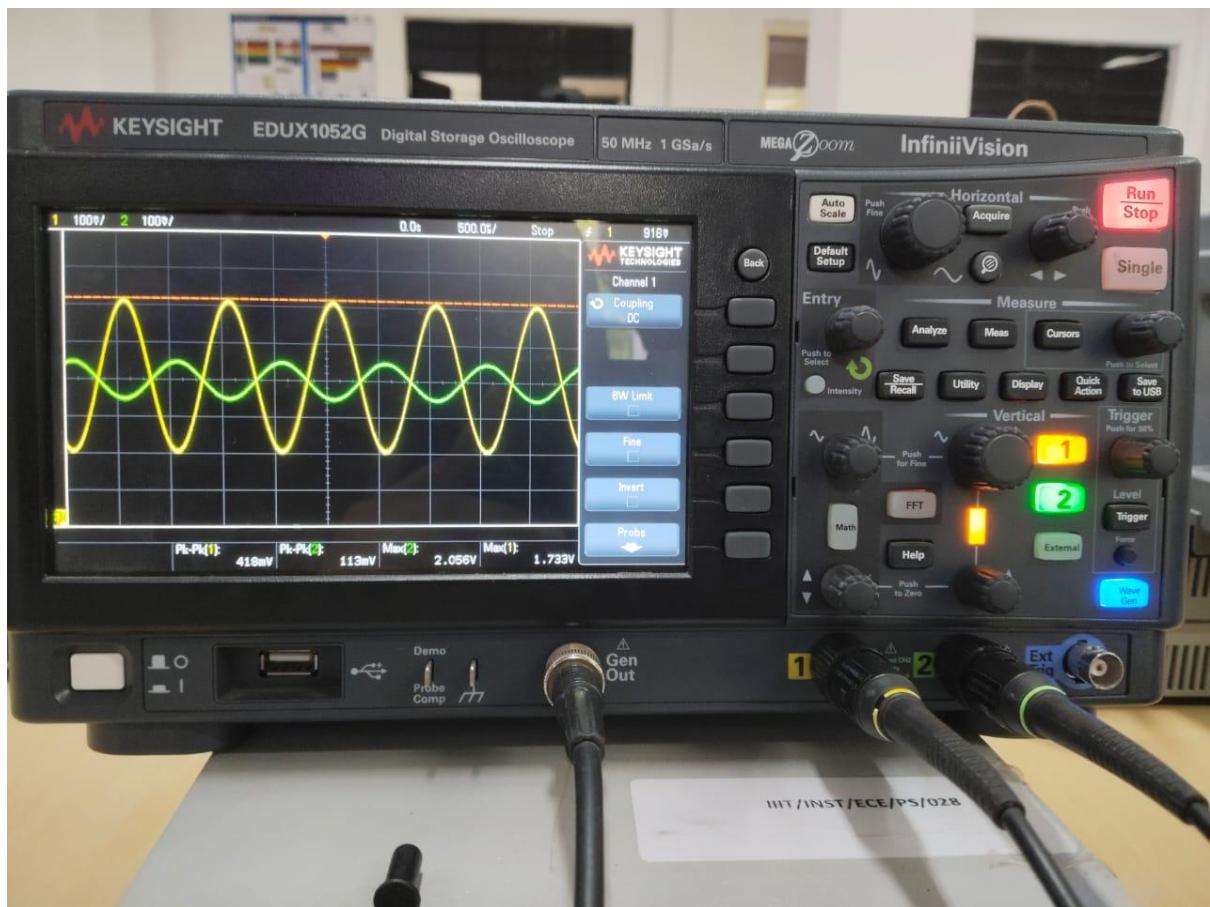
$$Av = (gm * RL * v_{in}) / (v_{in})$$

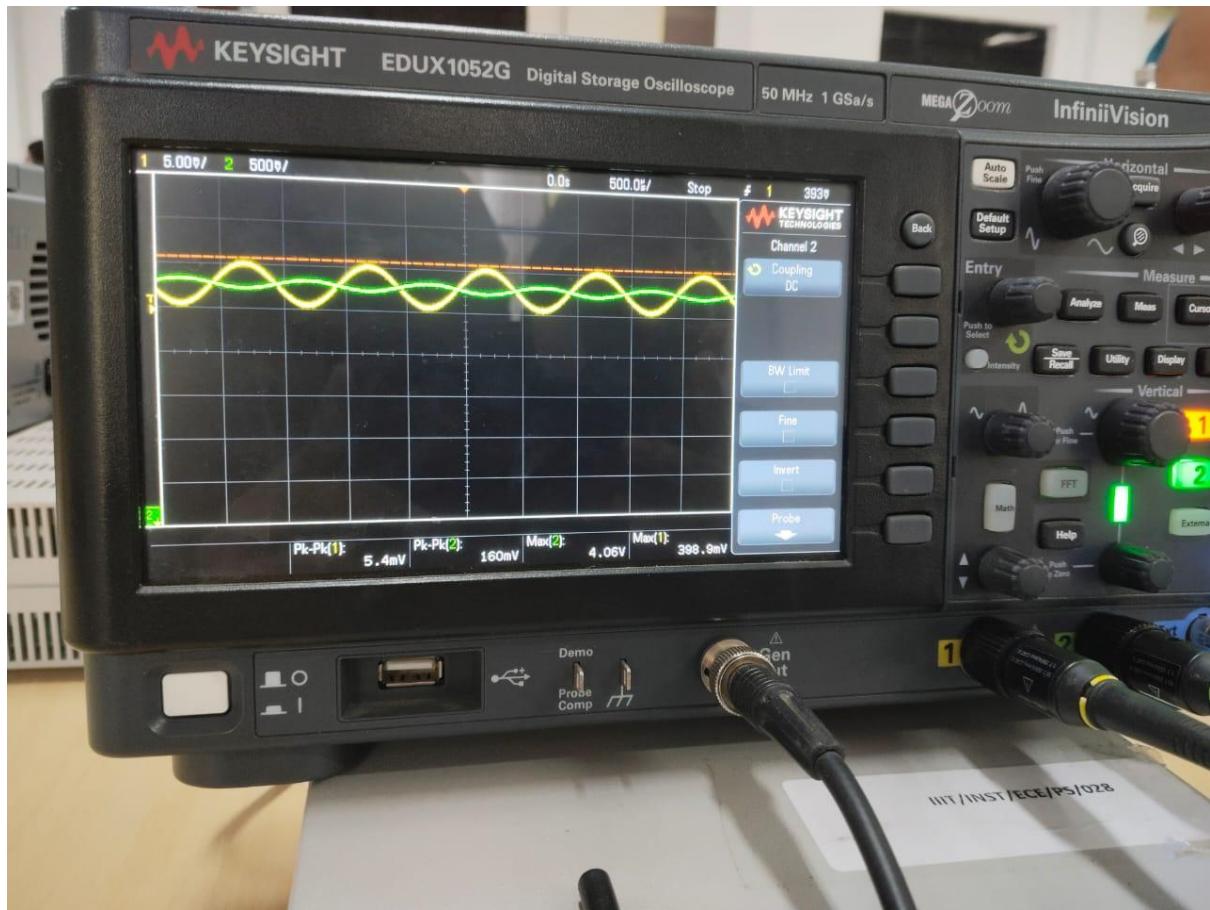
[$v_{out} = V_{in} * (\text{output impedance})$]

$$Av = -gm * RL$$

VBIAS(V)	Vout(Vpp) mV	Gain (Av)	gm(mS)
1.5	400	4	0.85
1.8	410	4	0.85
2.5	46	0.5	0.106
4.0	5.4	0.08	0.017

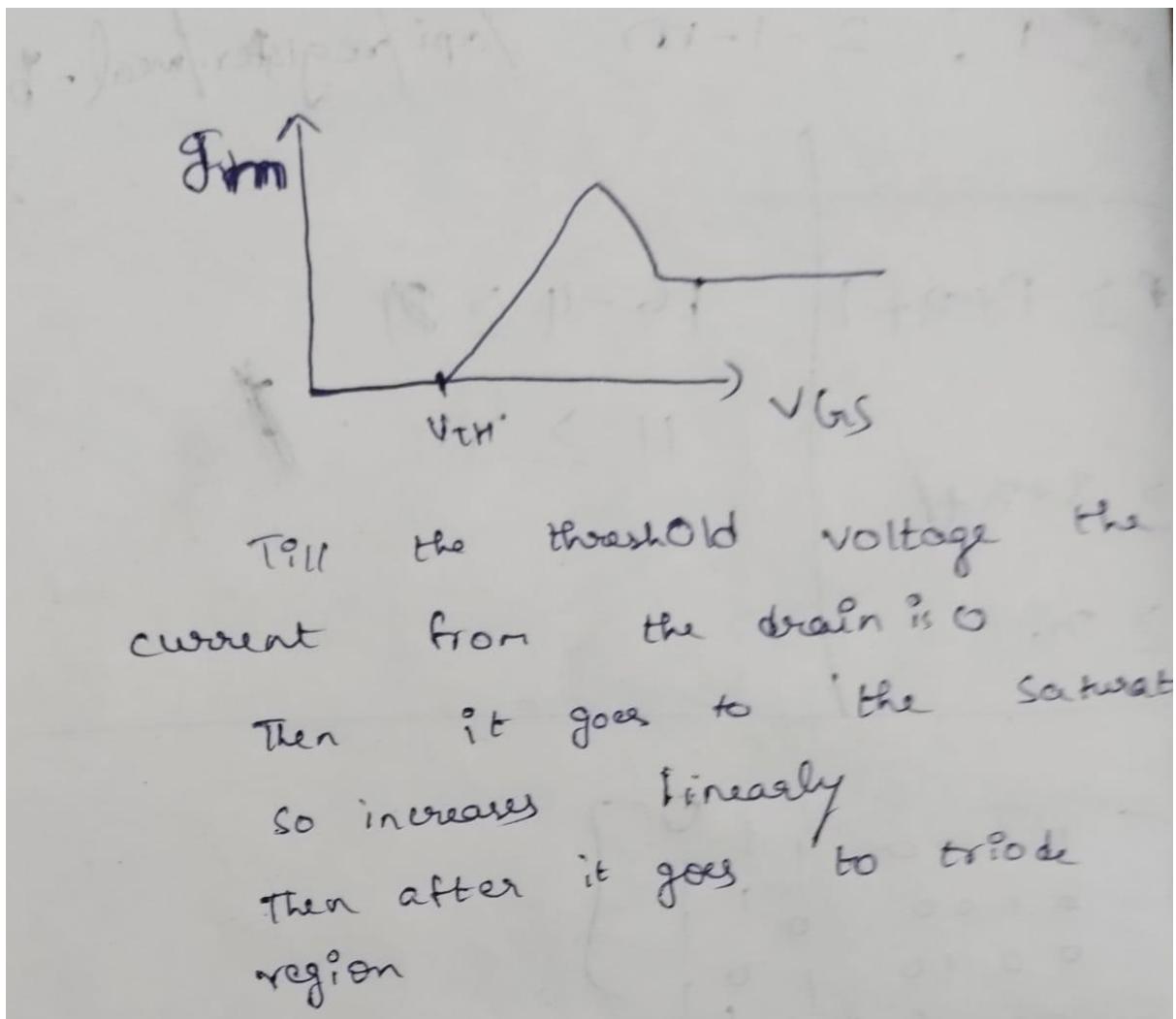






Observation:

- Gain increases with VBIAS until saturation.
- After saturation slight increase with large increase in vbias because of channel length modulation
- Plot of gm vs Vgs



4.3 Effect of Input Swing on Gain

Fixed VBIAS=2.5V, f=1 kHz

vin(mVpp)	vout(Vpp) mV	Gain (Av)	gm(mA/V)
100	400	4	0.85
200	960	4.2	0.98
300	1.23	5	1.06
400	1.56	5	1.06
500	1.89	4.8	1.02
600	2.21	3.4	0.72
700	2.45	3.2	0.68

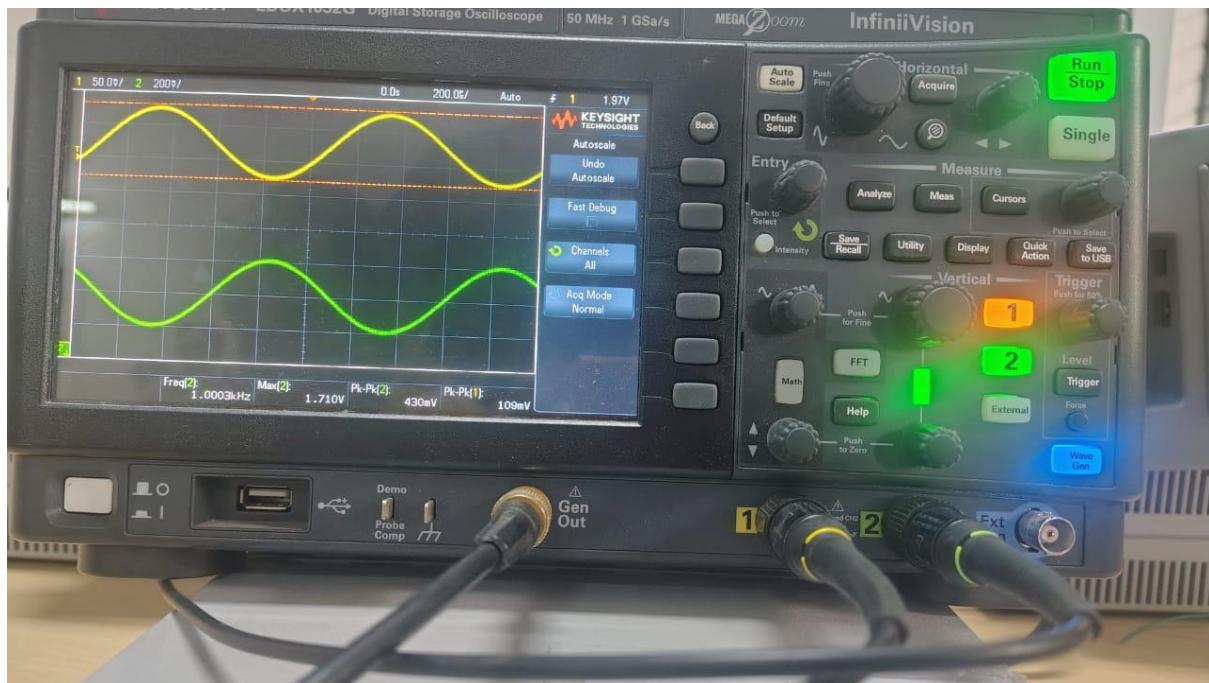
From above mentioned stat bias voltage is still 2V

Clipping observed after 700mv for v bias 2v

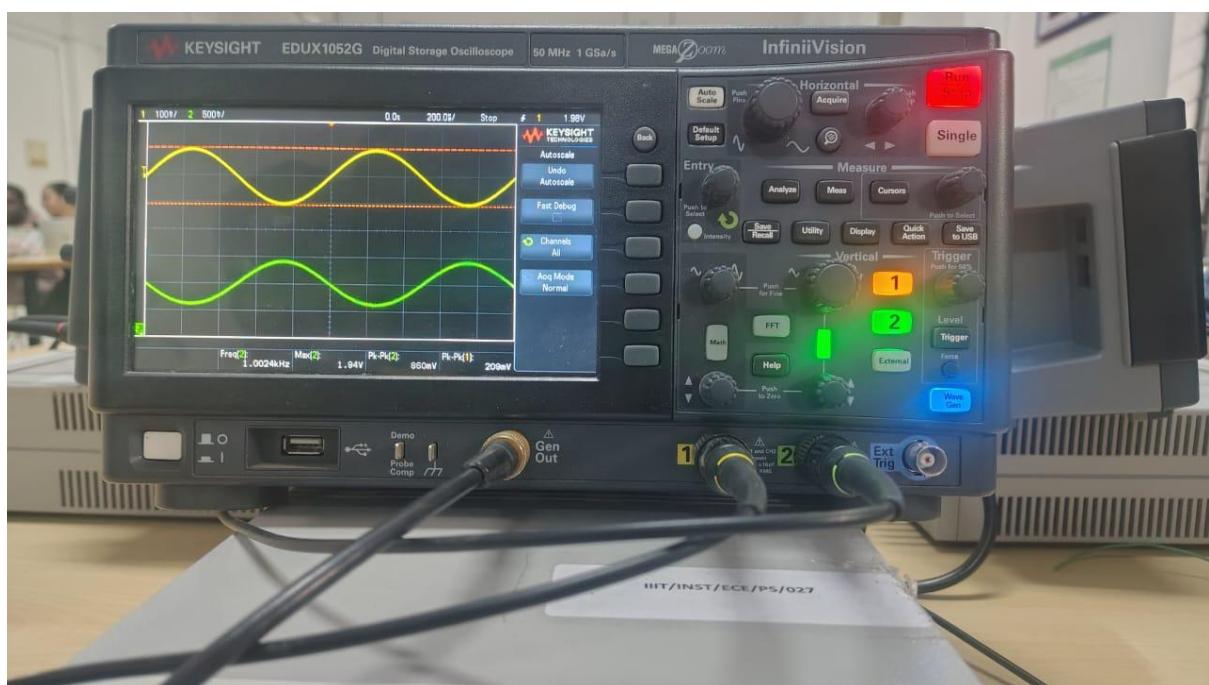
Observation:

- Clipping occurs when vin exceeds the linear range.

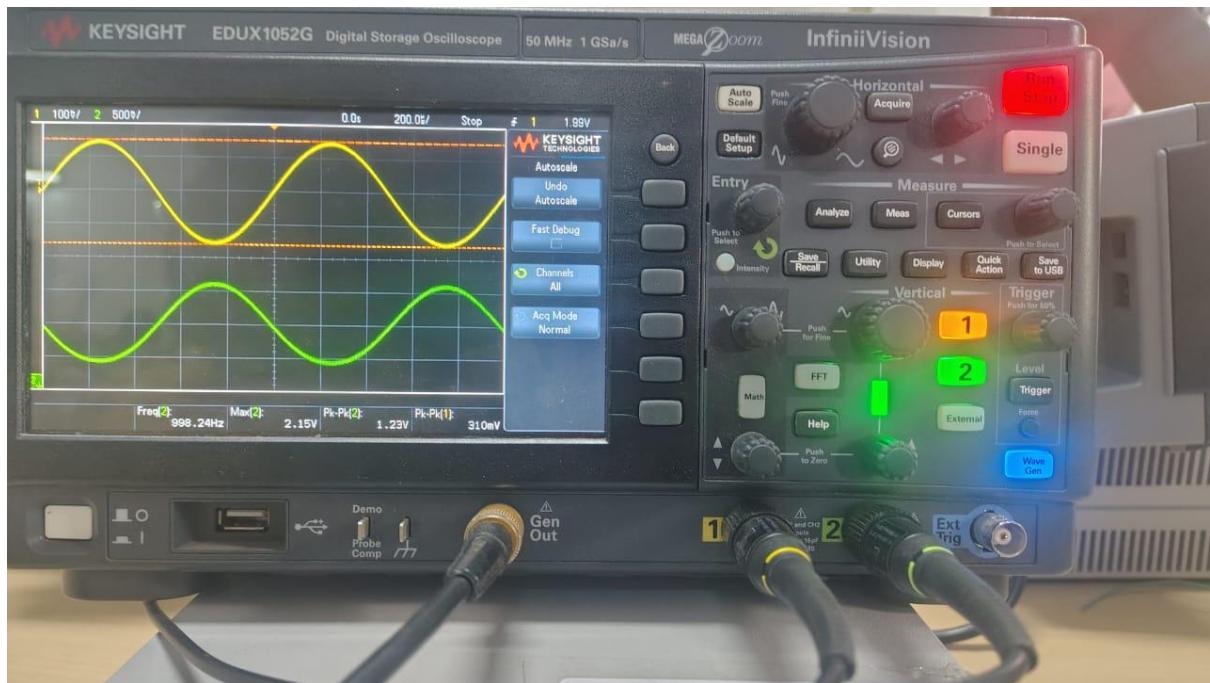
When the input voltage is 100mV(amplitude peak to peak)



When the input voltage is 200mV



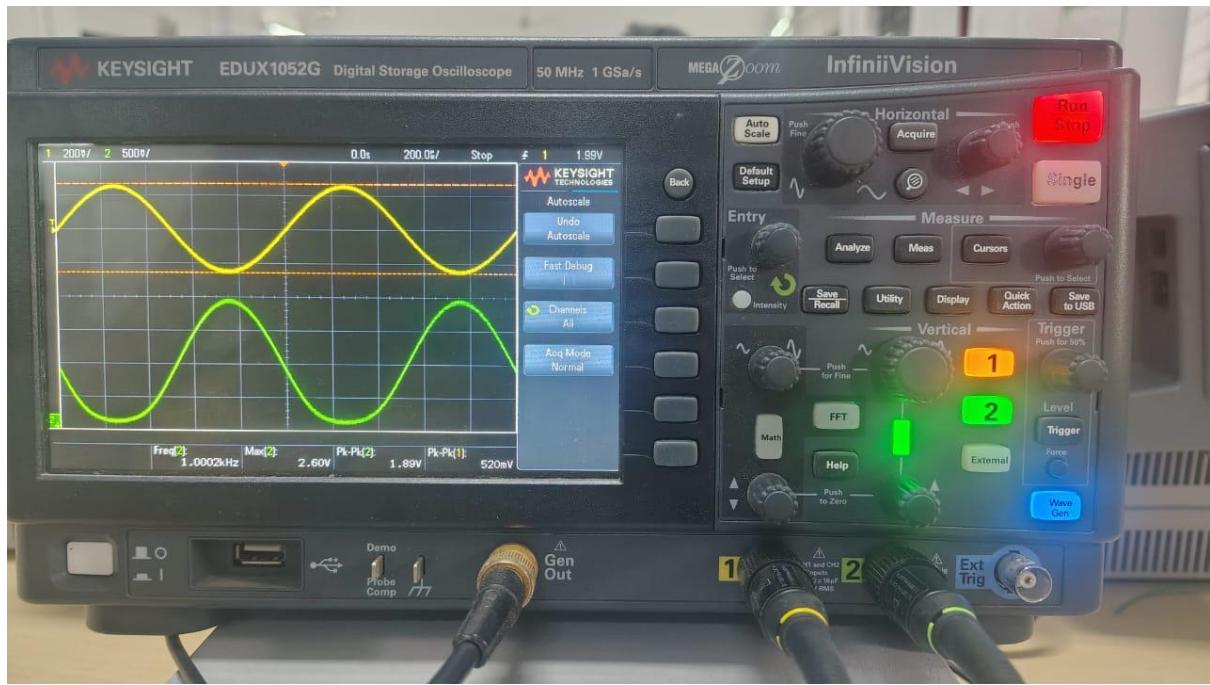
When the input voltage is 300mV



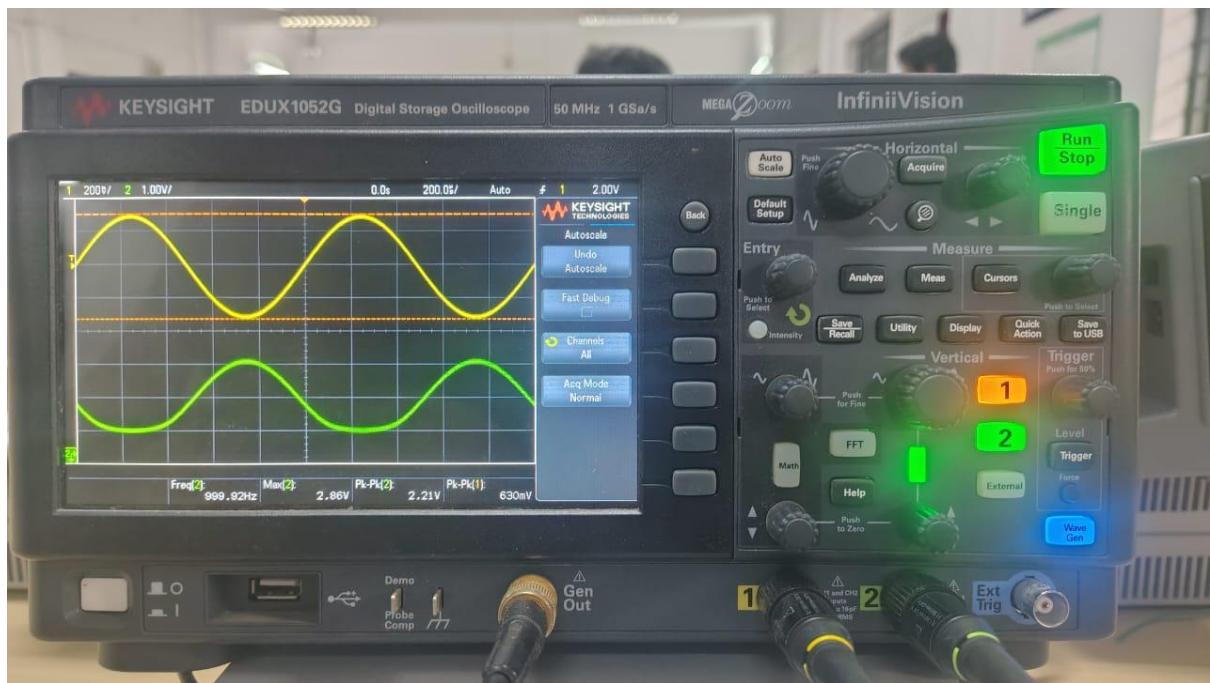
Input voltage is 400mV



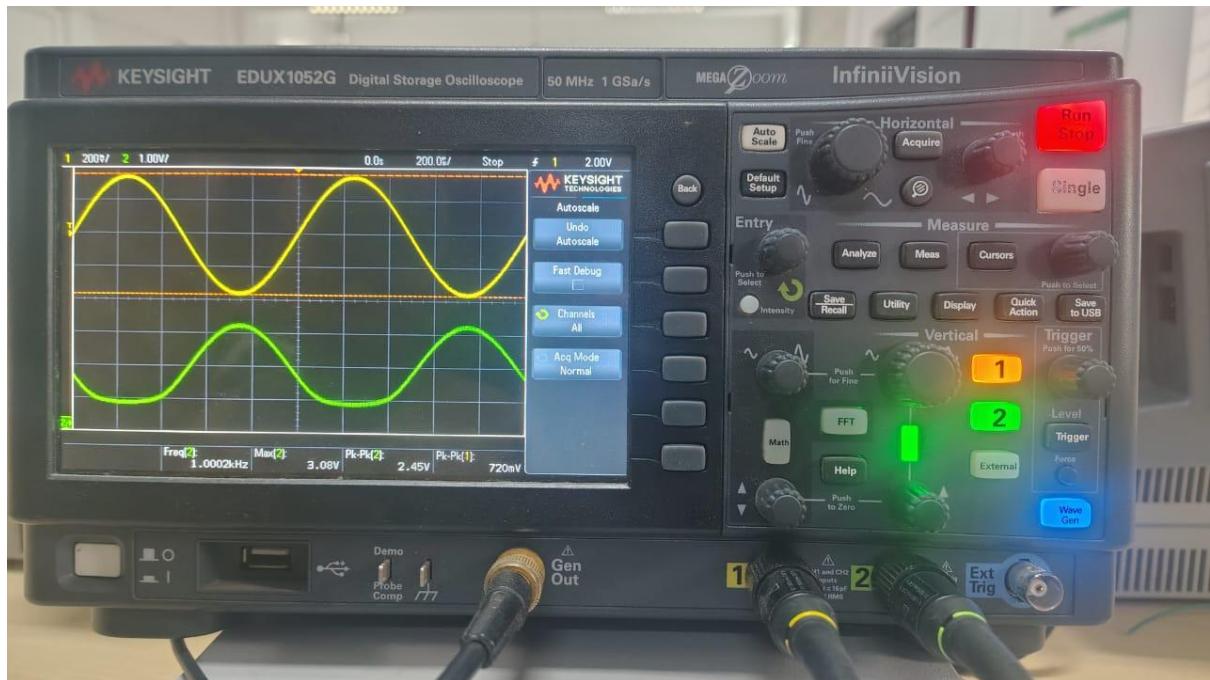
Input voltage is 500mV



Input voltage is 600mV



Input voltage is 700mV



- The output clips when the input amplitude exceeds 700 mV, as the peak V_{gs} becomes 2.35V ($2V + 700mV/2$). This pushes the MOSFET into the triode region since increasing V_{gs} increases I_d .
- Since $V_{ds} = V_{dd} - I_d \cdot R$, as I_d increases, V_{ds} decreases. When V_{ds} becomes less than $V_{gs} - V_{th}$, the MOSFET exits saturation and enters the triode region.
- Further increase in amplitude causes clipping on both sides of the sine wave, as the MOSFET moves into the subthreshold region.
- When the input amplitude reaches 1Vpp, V_{gs} at some points drops below V_{th} , reducing conduction and leading to clipping.

We can observe the clipping started due to v_{in} exceeds the linear range that means mosfet is in triode region

4.4 CS Amplifier with External Coupling

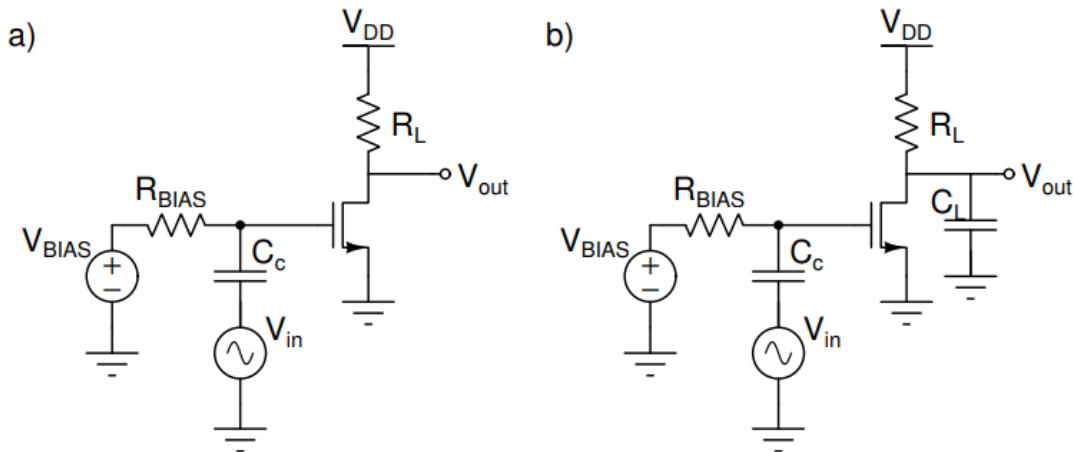


Figure 22: CS amplifier with external coupling capacitance and resistor

- **Gain with coupling:** $A_v=6$
- **Input V_{in} = 50mV Vpp**
- **Rbias=100ohm**
- **$g_m=6/RL=1.27mA/V$**

$$\begin{aligned}
 & 500 & 1.89V \\
 & 600 & 2.81 \\
 & 700 & 2.45V. \\
 \textcircled{4} \quad \text{gain} &= \frac{V_{out}}{V_{in}} = \frac{300}{50} = 6 \\
 \text{gain} &= A_v + g_m R_L \\
 g_m &= \frac{6}{R_L} \\
 &= \frac{6}{4.7} \times 10^{-3} \\
 &\approx 1.27 \times 10^{-3}
 \end{aligned}$$

- **Measured $V_{DS}=300mV$**
- **Calculated $IDS=((5-0.3)/4.7)*10^{-3}mA=1mA$**

$$g_m = 1.27 \times 10^{-3}$$

$$I_D = \frac{1}{2} (g_m) (V_{GS} - V_{TH})$$

$$\Rightarrow g_m = \left(\frac{\mu C_{ox} W}{L} \right) (V_{GS} - V_{TH})$$

$$g_m = \frac{\mu C_{ox} W}{L} (2 - 1.8)$$

$$= 1.27 \times 10^{-3} = \frac{\mu C_{ox} W}{L} (0.2)$$

$$\Rightarrow \boxed{\frac{\mu C_{ox} W}{L} = \frac{1.27}{2} \times 10^{-2} = 6.35 \times 10^{-3}}$$

- By above calculations $\mu C_{ox} W/L = 6.35 \times 0.01$ is calculated using VDS come IDS
- **Vbias=2.5V**
- Connected a load capacitor (C_L) of 470 pF to check the frequency response.
- Set start frequency to 100 Hz and stop frequency to 20 MHz.
- Input amplitude is 10 mV, output load is High-Z, and 50 points are taken.
- Selected the gain channel and moved the marker to get the 3-dB bandwidth.
- Compared the measured bandwidth with the estimated pole of the transfer function $V_{out}/V_{in}(s)$.
- Used the frequency response analysis chart in the DSO for plotting.
- **Frequency Response:**

- o 3-dB Bandwidth frequency responses are

$$f_L = 300\text{Hz}, f_H = 80\text{kHz}$$

then
so increases linearly
Then after it goes to triode
region

Calculation of gain poles

$$H_1(s) = \frac{V_{gate}}{V_{in}} = \frac{R_{Bias}}{R_{Bias} + 2C} = \frac{sC_R_{Bias}}{1 + sC_R_{Bias}}$$

$$H_2(s) = \frac{V_{out}}{V_{gate}} = \frac{R_{Bias}}{R_{Bias} + 2C} = \frac{sC_R_{Bias}}{1 + sC_R_{Bias}}$$

$$H_3(s) = Z_{load} = \frac{R_C \frac{1}{sC_C}}{R_C + \frac{1}{sC_C}}$$

$$V_{out} = -\bar{I}_d R_C \frac{1}{1 + sR_C C_C}$$

$$i_d = g_m v_{gate}$$

$$V_{out} = \frac{+g_m v_{gate} R_C}{1 + s R_L C_L}$$

$$\frac{V_{out}}{v_{gate}} = -\frac{g_m R_L v_{gate}}{1 + s R_L C_L}$$

$$\frac{V_{out}}{v_{gate}} = -\frac{g_m R_L}{1 + s R_L C_L} = H_2(s)$$

$$H(s) = H_1(s) + H_2(s)$$

$$H(s) = \frac{(-g_m R_L)}{1 + s R_L C_L} \cdot \frac{(s C_L R_{bias})}{1 + s R_{bias} C_L}$$

$H(s)$ poles

$$s = \frac{-1}{R_L C_L}, \frac{-1}{R_{bias} C_L}$$

$$2\pi f = \frac{-1}{R_L C_L}, \frac{-1}{R_{bias} C_L}$$

$$2\pi f = -\frac{1}{R_L C_L}, -\frac{1}{R_{bias} C_L}$$

$$f = \frac{1}{2\pi R_L C_L}, \frac{1}{2\pi R_{bias} C_L}$$

$$f_L = \frac{1}{(2\pi)(50)(10^{-5})}$$

$$= \frac{10^4}{10\pi}$$

$$= \frac{1000}{\pi}$$

$$\approx 318.47$$

$$f_R = \frac{1}{(2\pi)(4.7 \times 10^3)(4.7 \times 10^{-10})}$$

$$\approx \frac{10^7}{(2\pi)(4.7)(4.7)}$$

$$\approx 72 \text{ kHz}$$



5. Results & Discussion

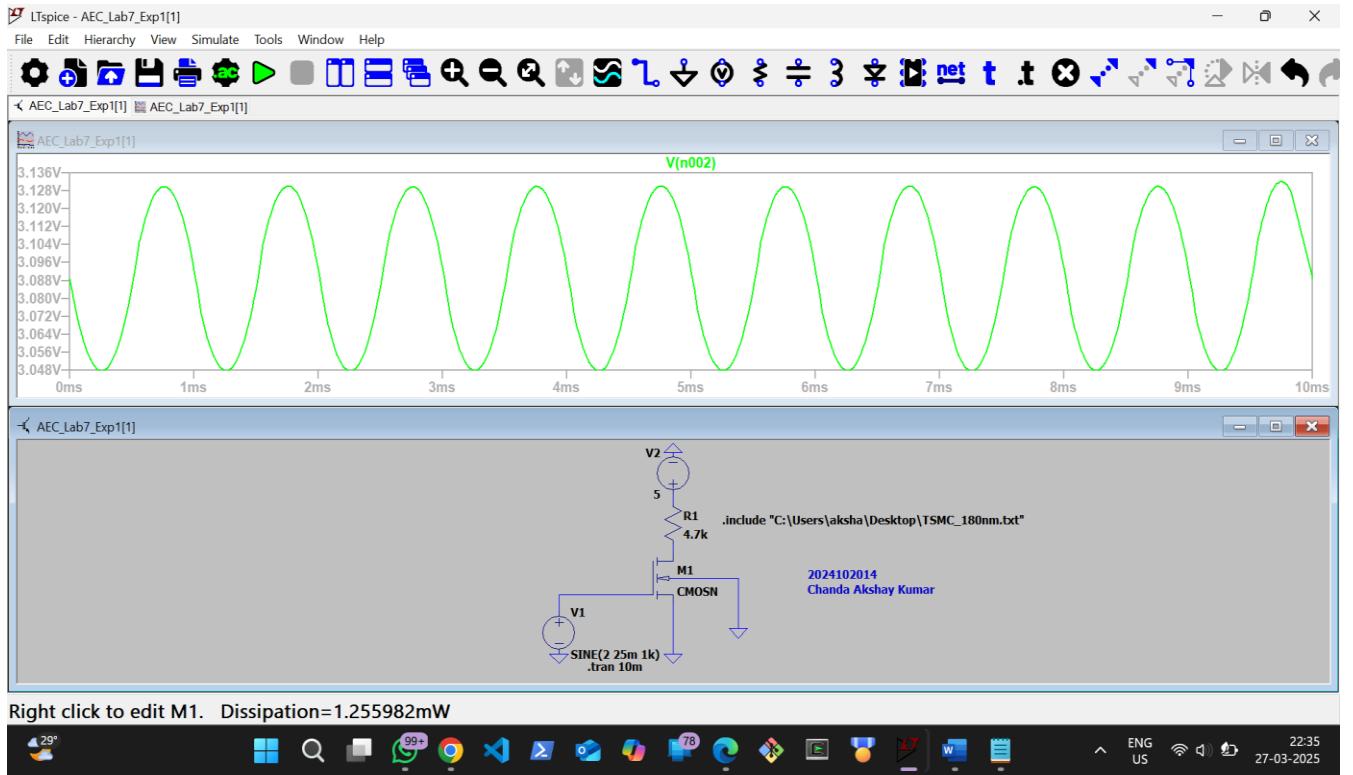
- Body Effect:** Changes in VSS alter gm and gain.
- Bias Voltage:** Higher VBIAS increases gain until saturation.
- Clipping:** Occurs due to MOSFET entering cutoff or triode region.
- Coupling Capacitor:** Blocks DC but allows AC signal, improving stability.

6. Conclusion

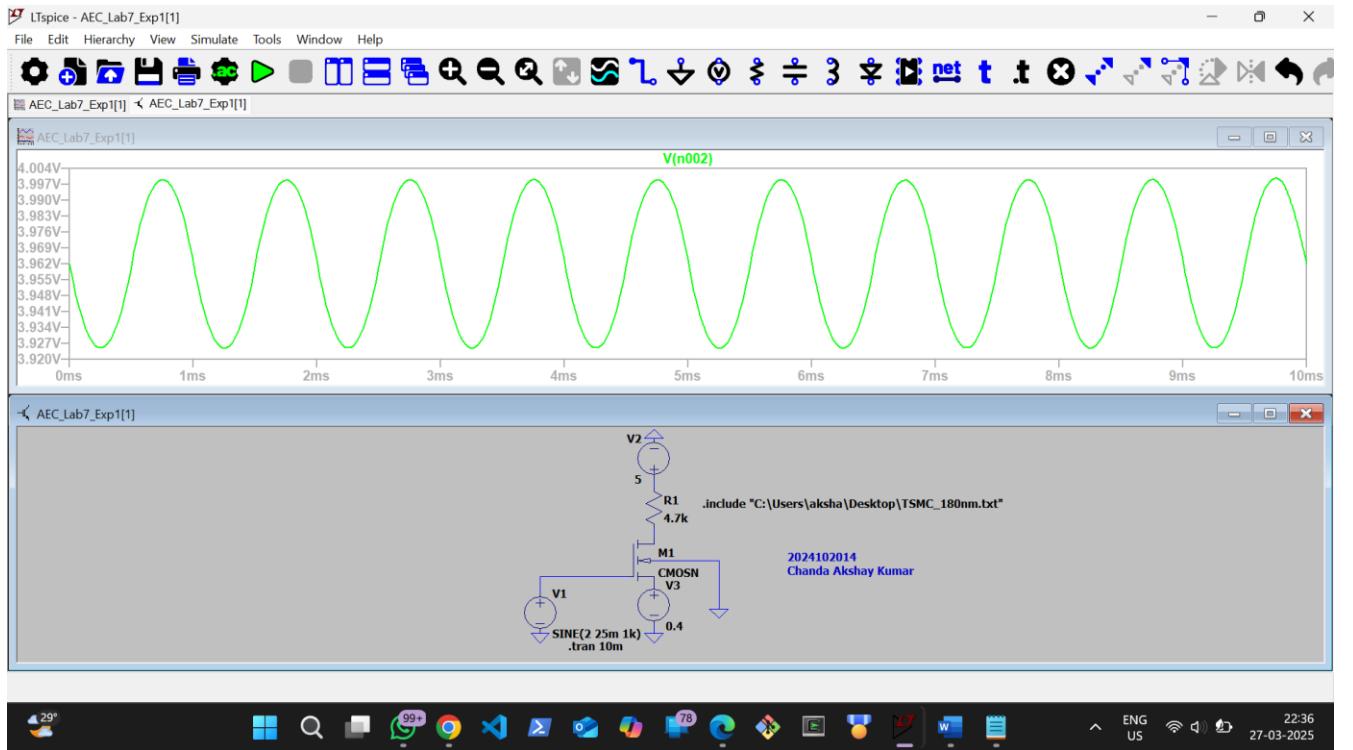
- The experiment showed the main features of a CS amplifier, like how body bias, bias voltage, and input signal swing affect gain.
- The frequency response confirmed bandwidth limits caused by capacitive effects.

7. LTSPICE

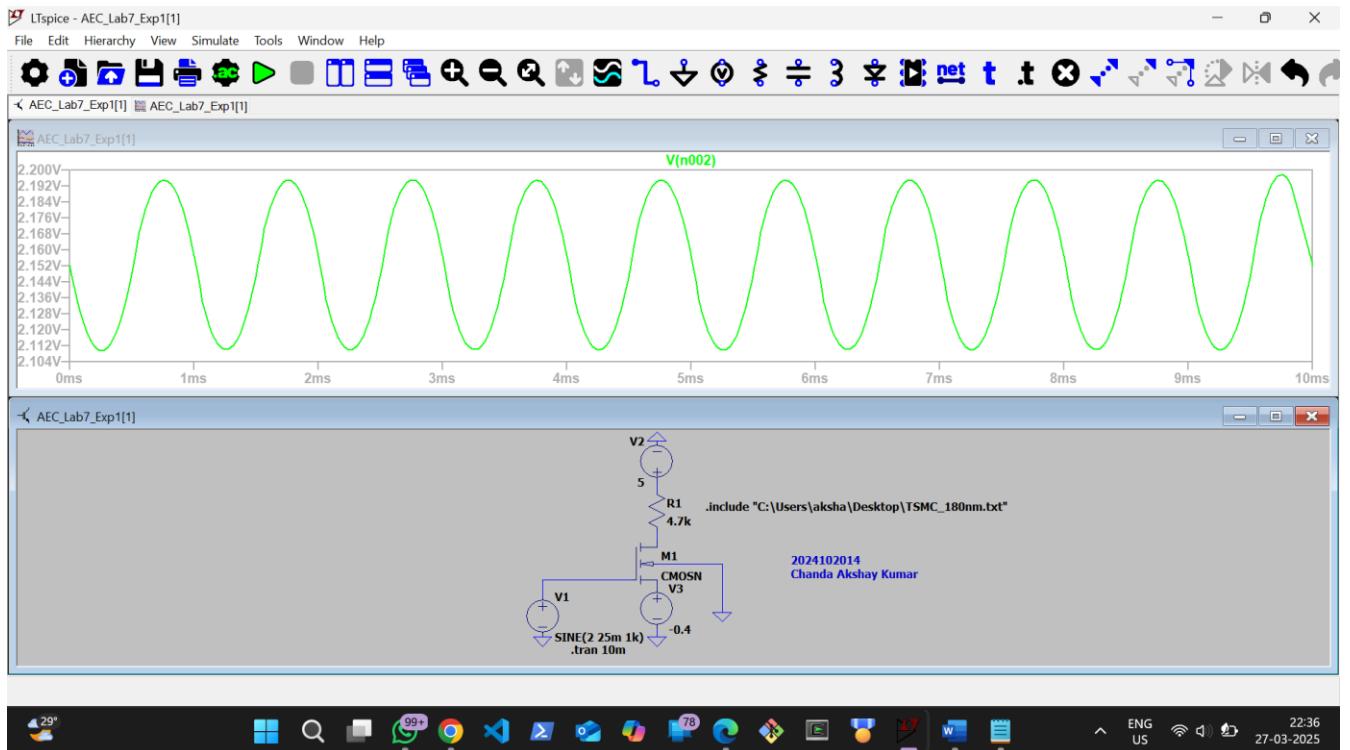
at vbody 0 V



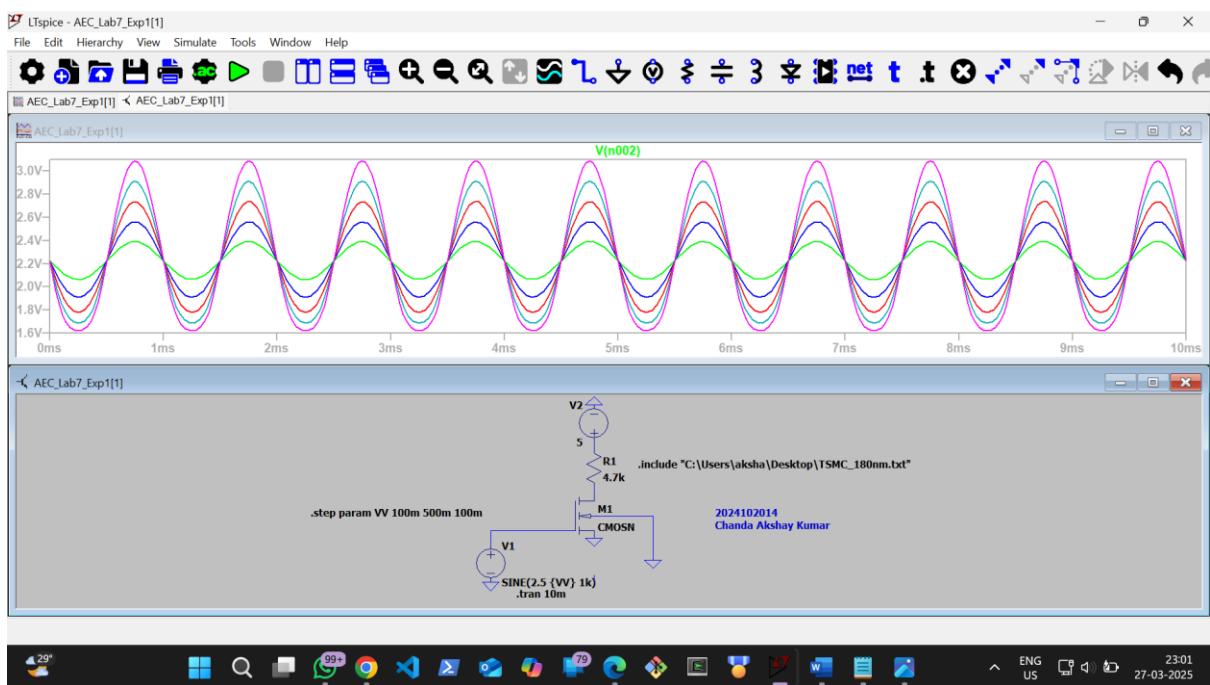
at vbody 0.4 V

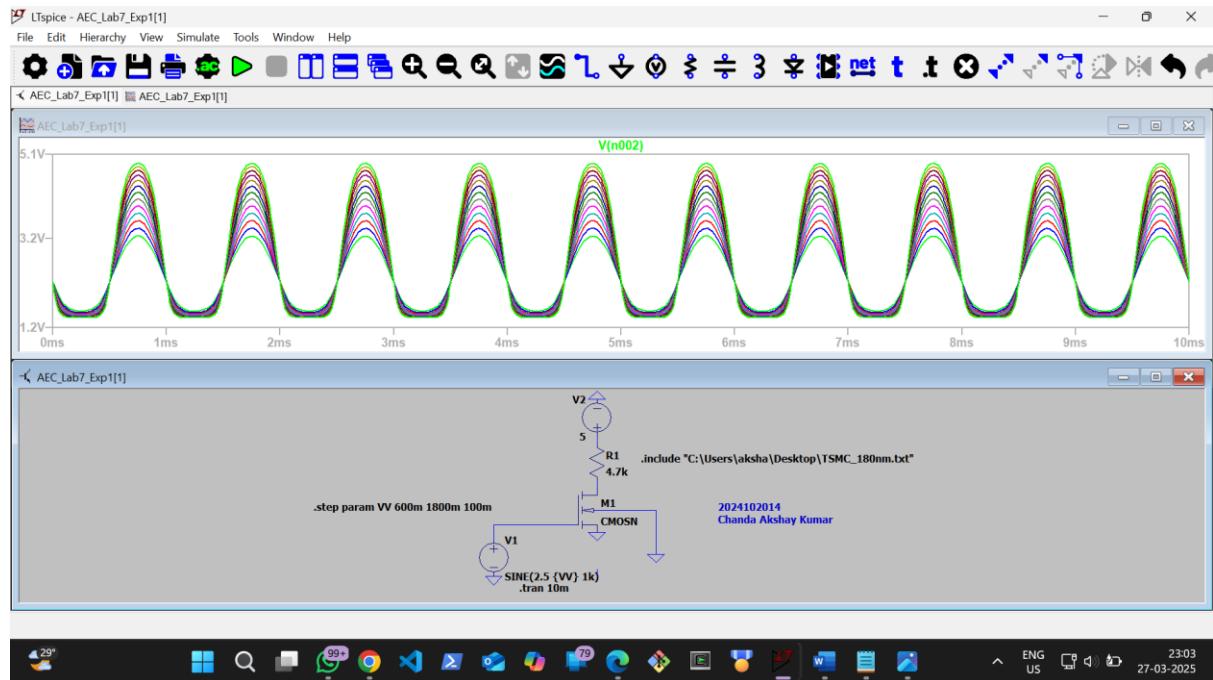


at vbody -0.4 V

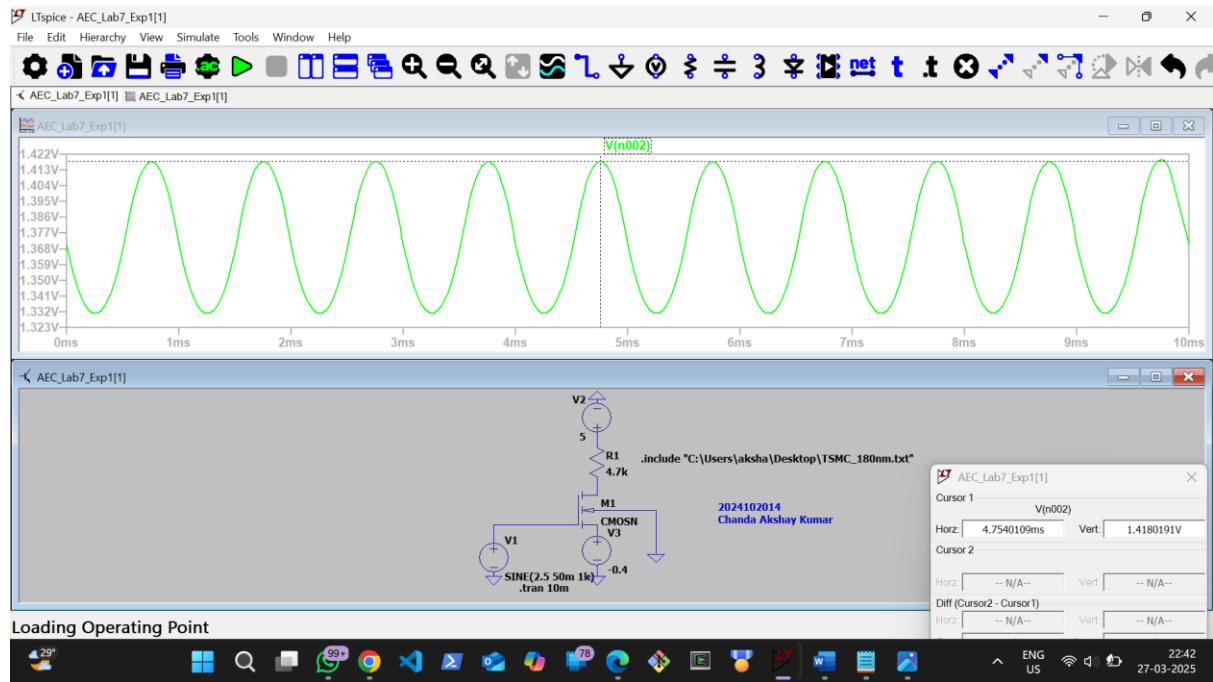


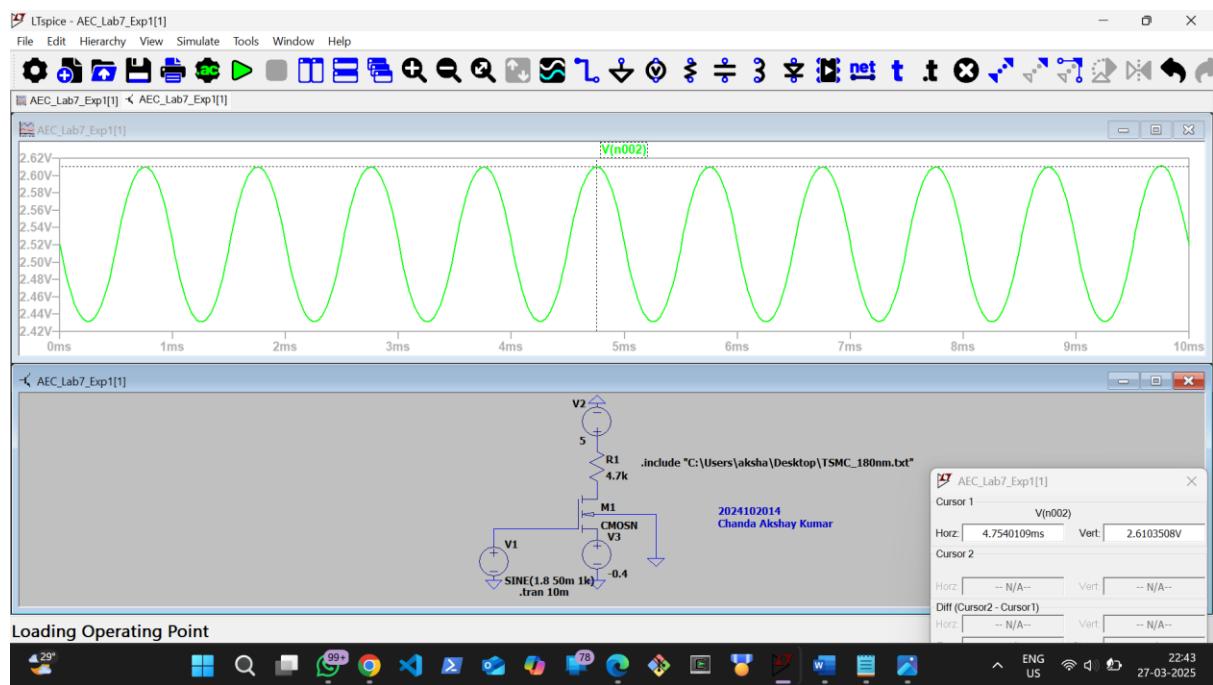
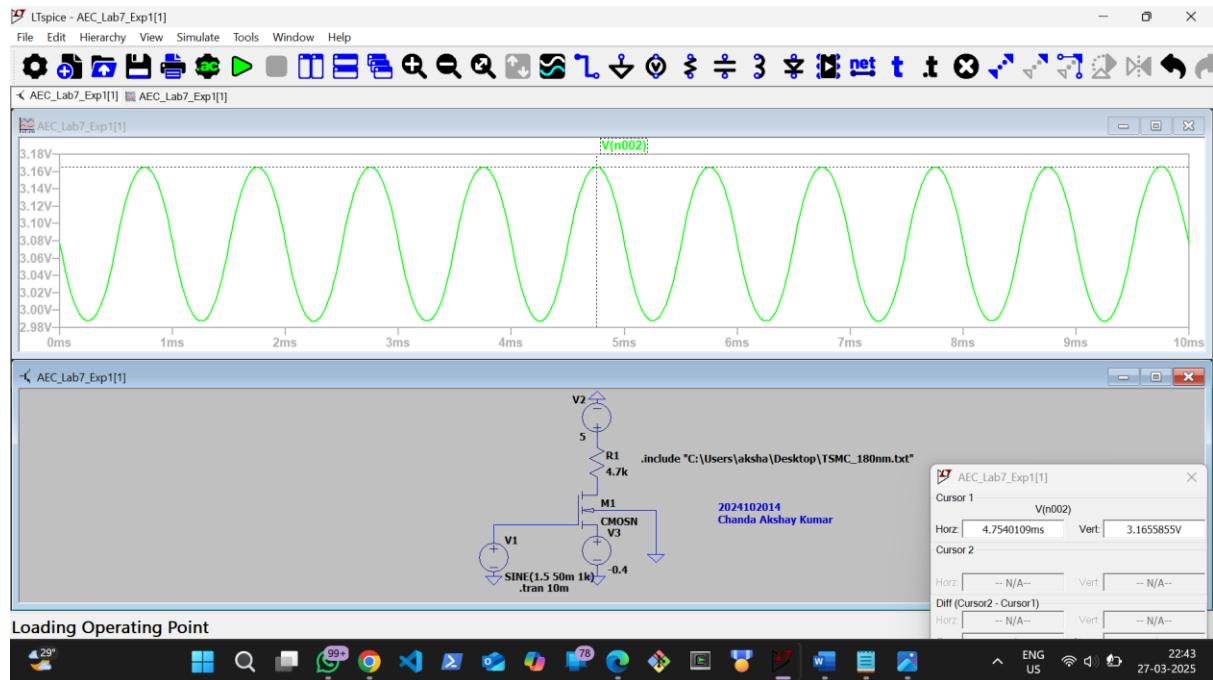
3rd exp

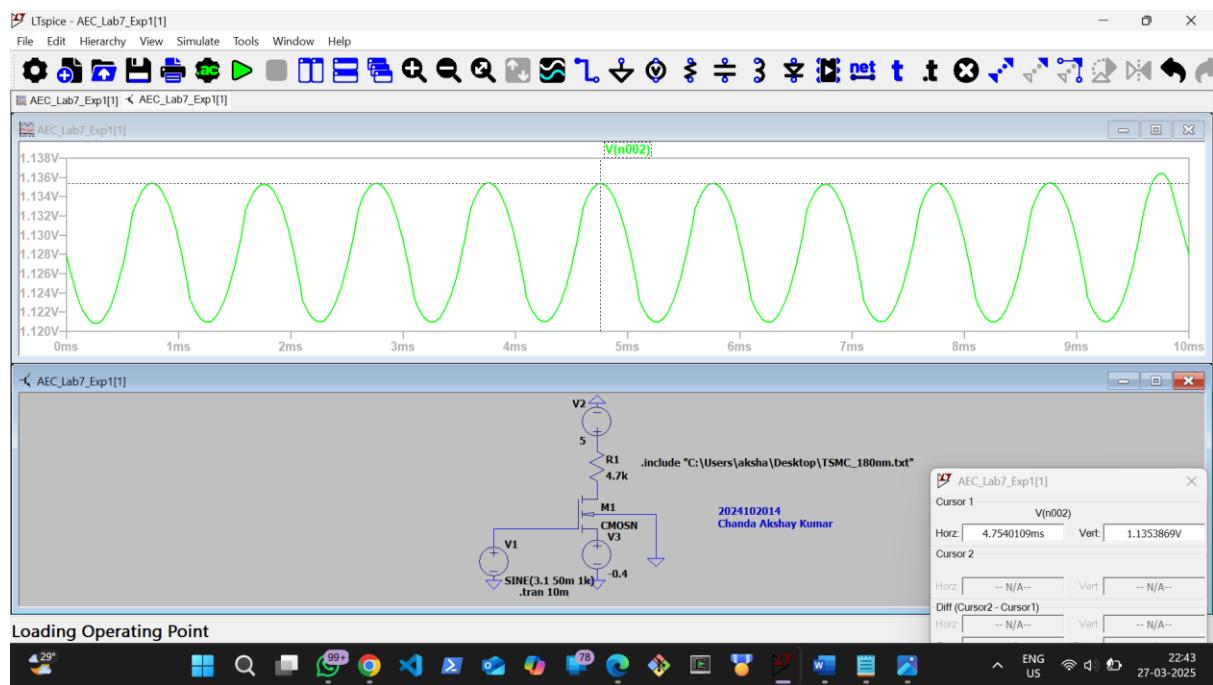
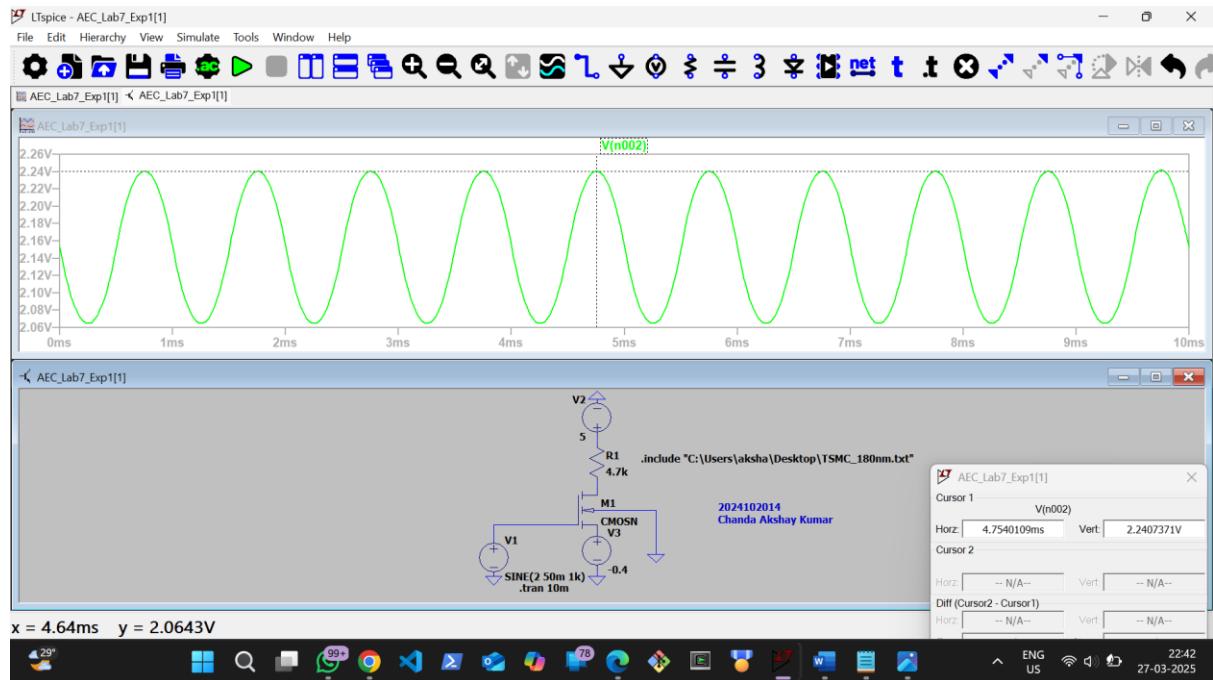


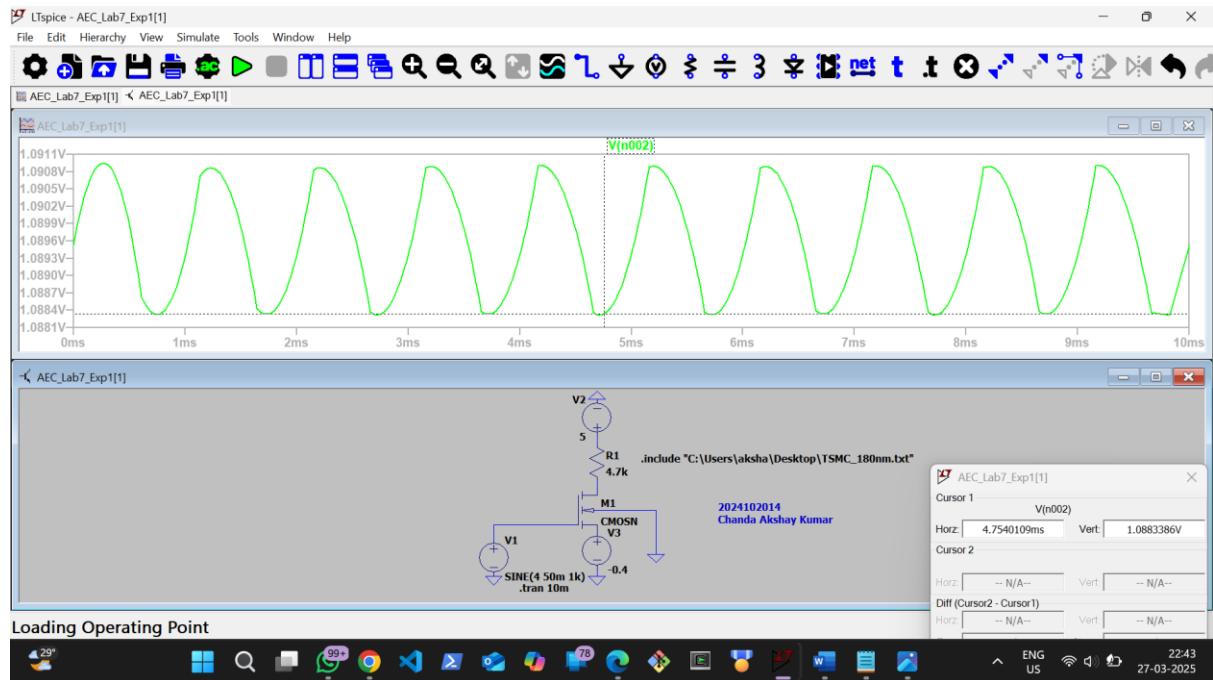


2nd exp









4th exp

