

LAB REPORT 6: BJT AMPLIFIER ANALYSIS

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Lab: Analog Electronics and Circuits (AEC)

3rd question is after 4,5th questions

1. Objective

The objective of this experiment is to analyze a common emitter (CE) voltage amplifier circuit using BC547B transistor in LTSPICE. Theoretical calculations, simulations, and performance analysis will be conducted to verify various parameters.

2. Circuit Specifications

- Supply Voltage (VCC): 12 V
- R1 = 18.46 kΩ
- R2 = 2.24 kΩ
- RC = 30.3 kΩ
- RE = 2 kΩ
- RL = 1 kΩ
- CB = 10 μF
- CC = 10 μF
- CE = 100 μF
- **Input Signal:** $v_{in} = V_m \cdot \sin(2\pi f_0 t)$ V with $f_0 = 1$ kHz
- **Transistor:** BC547B (NXP)

DC Analysis

(a) Theoretical Calculations

For DC analysis, AC sources are removed, and capacitors act as open circuits. The values of VC, VB, VE, IC, and IB are determined using:

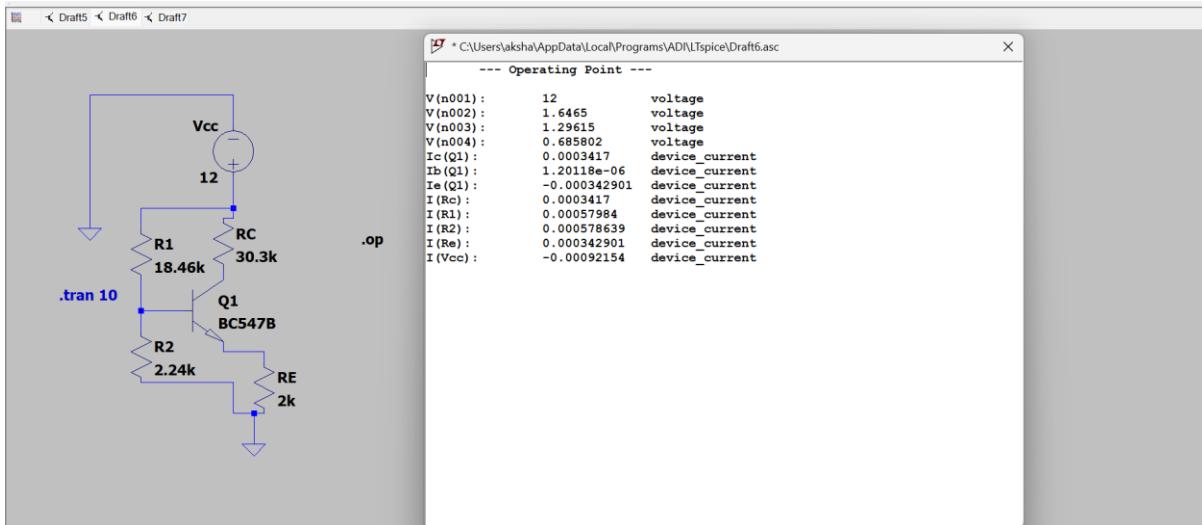
- $V_{BE} \approx 0.7$ V (for active mode)

- $IC = \beta * IB$ (β avg I_S taken as range of 260-280 according to V_{CC} and other factors in previous experiment)
- KVL and voltage divider rule to find node voltages.

The reason AC sources are replaced with its internal resistance and capacitors act as open During AC analysis is because,

As we are doing DC analysis after some time capacitors get fully charged and act as open circuits and do not conduct DC current , but responds to AC currents and voltages

By constructing an amplifier that stays stable with respect to its operating point hence the change in the operating point due to the AC is neglected and it is replaced with its internal resistance



The values of voltages and currents from the plots (.op) and the values obtained theoretically are approximately the same

Values tabulated for theoretical and simulation obtained as per asked in the manual in the below written sheet

05-03-2025

Lab-6

4
(a)

Part-2(c) BJT amplifier analysis and design

$$V_{CC} = 12V$$

$$R_1 = 18.46k\Omega$$

$$C_B = 100fF$$

$$R_2 = 2.24k\Omega$$

$$C_C = 100fF$$

$$R_E = 2k\Omega$$

$$C_E = 100fF$$

$$R_C = 30.3k\Omega$$

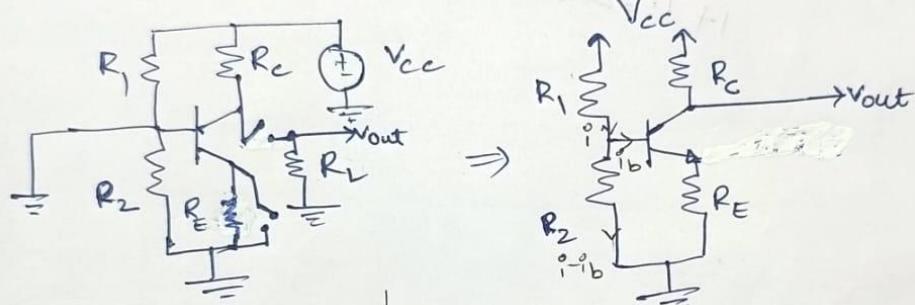
$$R_L = 1000\Omega$$

$$v_{in} = V_m \sin(2\pi f_o t) v$$

$$f_o = 1\text{kHz}$$

BC547B - NPN Transistor

(a) DC analysis circuit becomes



$$V_{BE} \text{ fixed } \approx 0.7V$$

β from previous experiment analysis.

$$I_C = \beta I_B$$

in forward active mode

In simulation LTSpice

$$v(6004) = V_E$$

$$v(6002) = V_C$$

$$v(6003) = V_B$$

$$v(6001) = V_{CC} = 12V$$

Practical Calculations
(# theoretical calculations)

$$(i - i_b)R_2 = V_B$$

$$\frac{V_{CC} + i_b R_2}{R_1 + R_2} = i$$

$$V_{CC} - V_B = (i)(R_1)$$

$$V_E = V_B - 0.7$$

$$I_E = \frac{V_B - 0.7}{R_E}$$

$$V_{CC} - (iR_2 - i_b R_2) = iR_1$$

$$(\beta + 1)i_b R_E = R_2 \left(\frac{V_{CC} - i_b R_1}{R_1 + R_2} \right) - 0.7$$

$$i_b = \left(\frac{V_{CC} R_2}{R_1 + R_2} - 0.7 \right) / (R_1 R_2)$$

$$i_b = 1.21mA$$

$$i_C = \beta i_b =$$

$$= 0.35mA$$

$$V_C = 1.9V$$

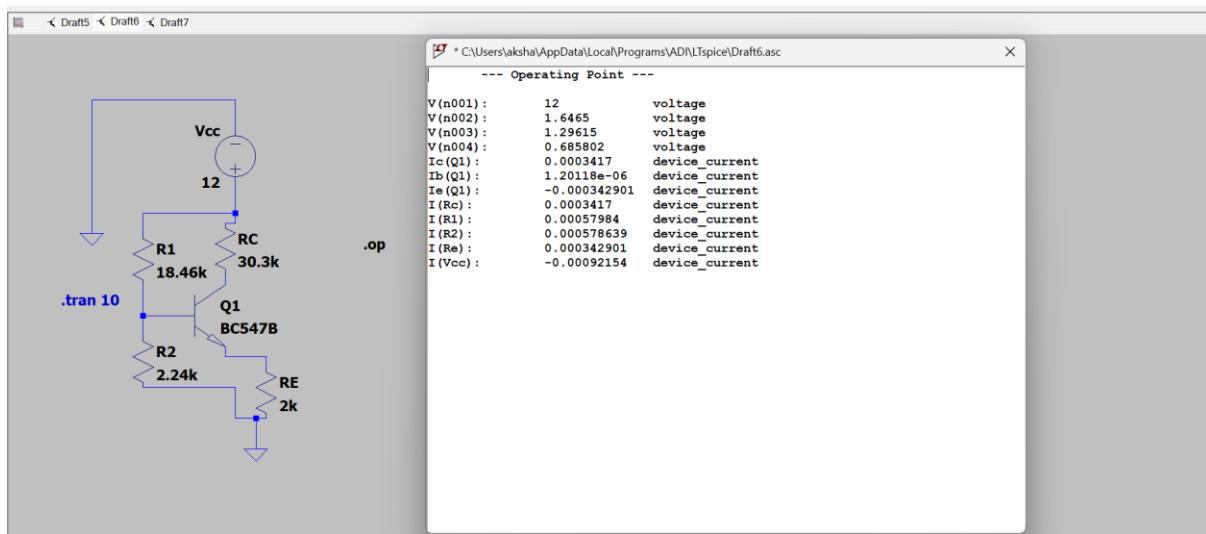
$$V_E = 0.599V$$

$$V_B = 1.294V$$

Mode of Operation: .

(b) Operating Point Simulation

- Run .op simulation in LTSPICE.



- Compare theoretical and simulated values in a table.

4. Small Signal and Transient Analysis

(c) Calculate Small Signal Parameters

- $gm = IC/VT = 13m/\text{ohm}$
- $r_{\pi} = \beta/gm = 21.8 \text{ kohm}$
- $r_0 = VA/IC = 181.4 \text{ kohm}$

(d) Small Signal Equivalent Circuit

- Replace capacitors with their impedance at $f_0 = 1 \text{ kHz}$.
- Draw the small signal equivalent model.

(e) Derivation of Voltage Gain Expression.

Use small signal model to derive $A_v = v_{out}/v_{in}$

- Use small signal model to derive $A_v = v_{out}/v_{in}$
- Calculated $A_v=12.23$ approximately

Simulated Values obtained in LTspice

experimental (LTspice)

Theoretical calculations

$$V_{CC} = 12V$$

$$V_C = 1.646V$$

$$V_B = 1.296V$$

$$V_E = 0.685V$$

$$I_C = 0.341mA$$

$$I_B = 1.2 \times 10^{-6} A = 1.2mA$$

$$I_E = 0.342mA$$

$$V_{CC} = 12V$$

$$V_C = 1.9V$$

$$V_B = 1.294V$$

$$V_E = 0.599mV$$

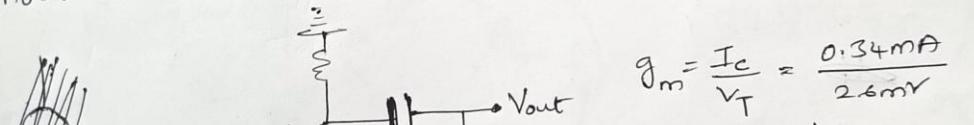
$$I_C = 0.34mA$$

$$I_B = 1.21mA$$

$$I_E \approx i_c = 0.342mA$$

* Capacitors act as open circuit for DC voltage after fully charged (charged immediately) allow AC to pass
 → Small Signal parameters

Shoot all the constant voltage sources

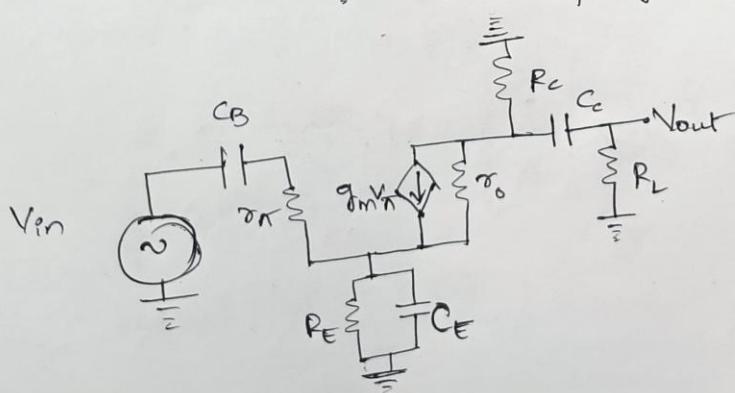


$$g_m = \frac{I_C}{V_T} = \frac{0.34mA}{2.6mV}$$

$$r_m = \frac{\beta}{g_m} = 21.8k\Omega$$

$$r_o = \frac{V_A}{I_C} = 181.4k\Omega$$

→ replacing with model.



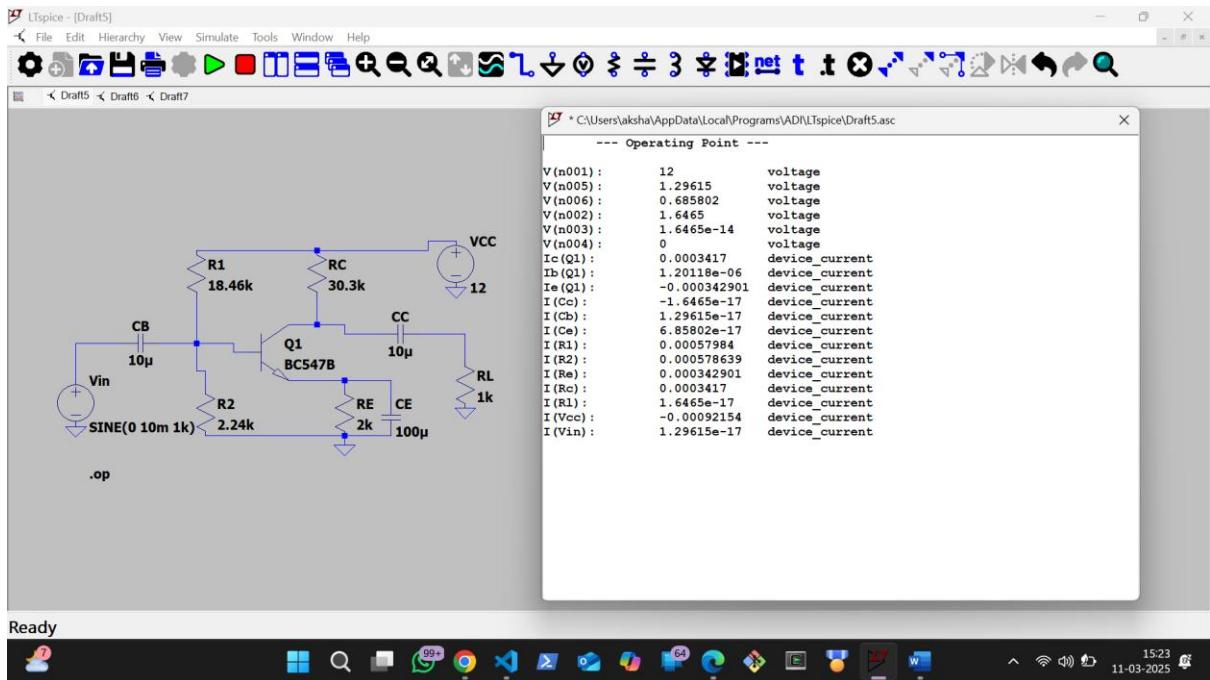
(f) Transient Simulation

- Run .tran 50m for Vm = 10 mV.
- Plot vin and vout.v

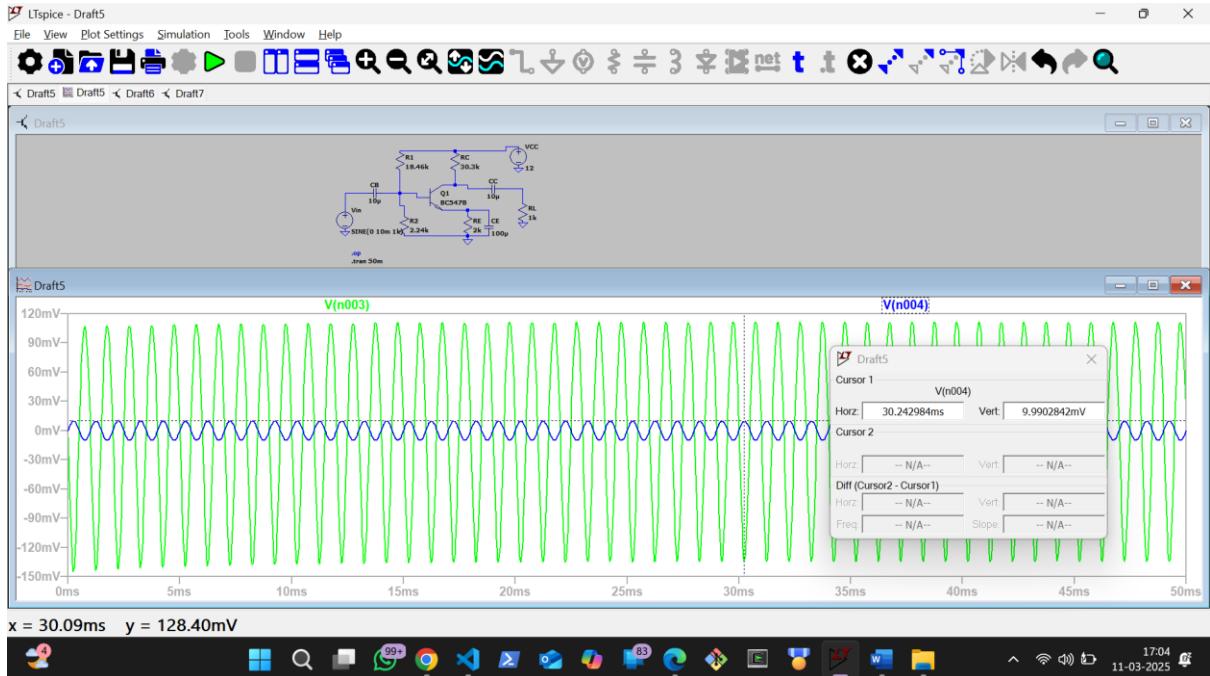
- Compare simulated gain with theoretical gain.
- In Ltspice simulation 11.15 and 13.89 for top-gain and bottom-gain of the signal respectively . images attached below
- i.e the range of gain is 11.15 to 13.90

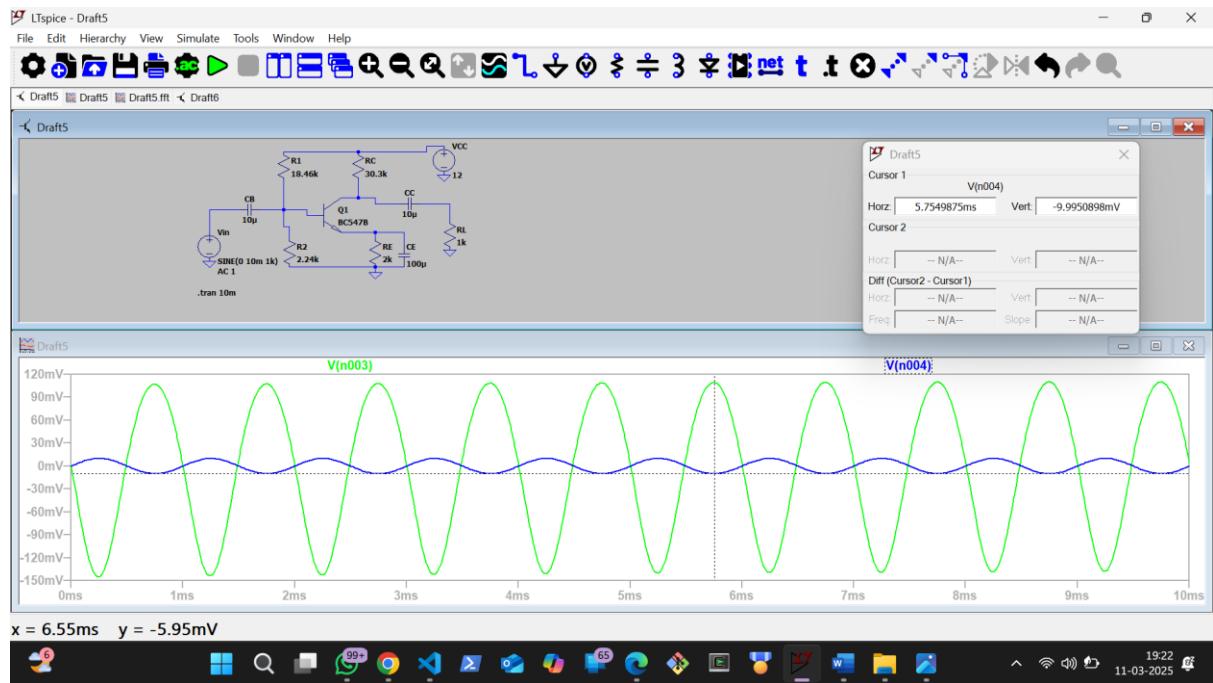
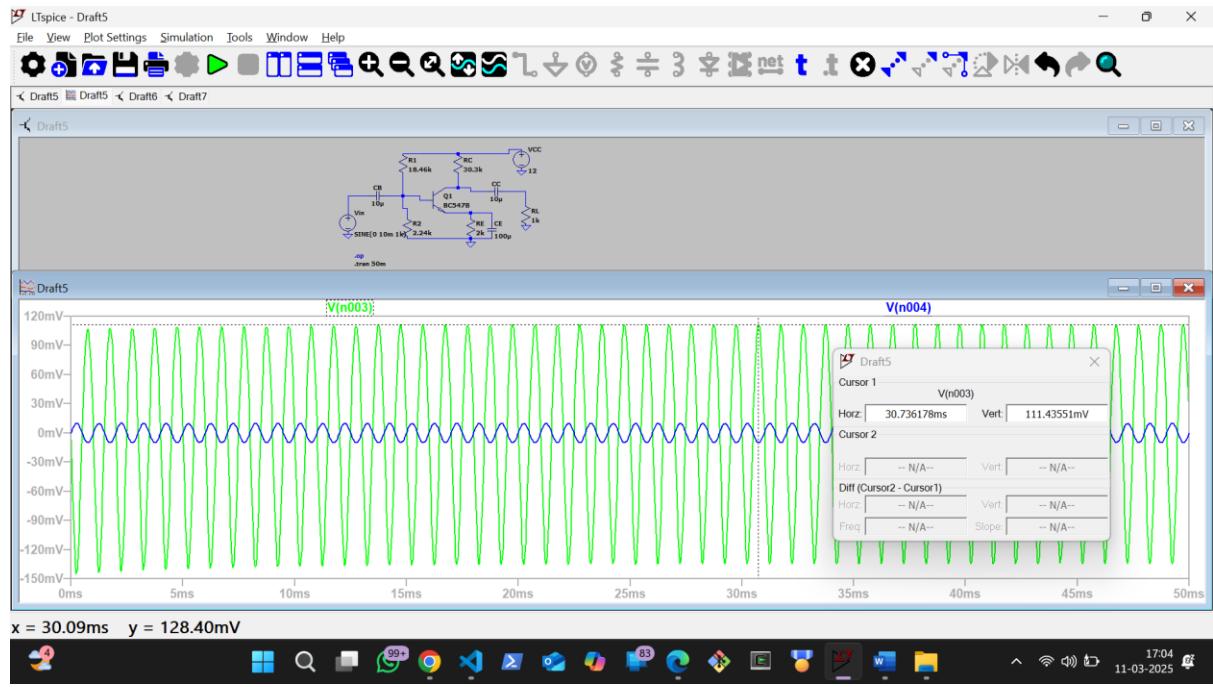
$A_v = \frac{-g_m \times (\text{collector load})}{1 + (g_m \times \text{emitter load})}$

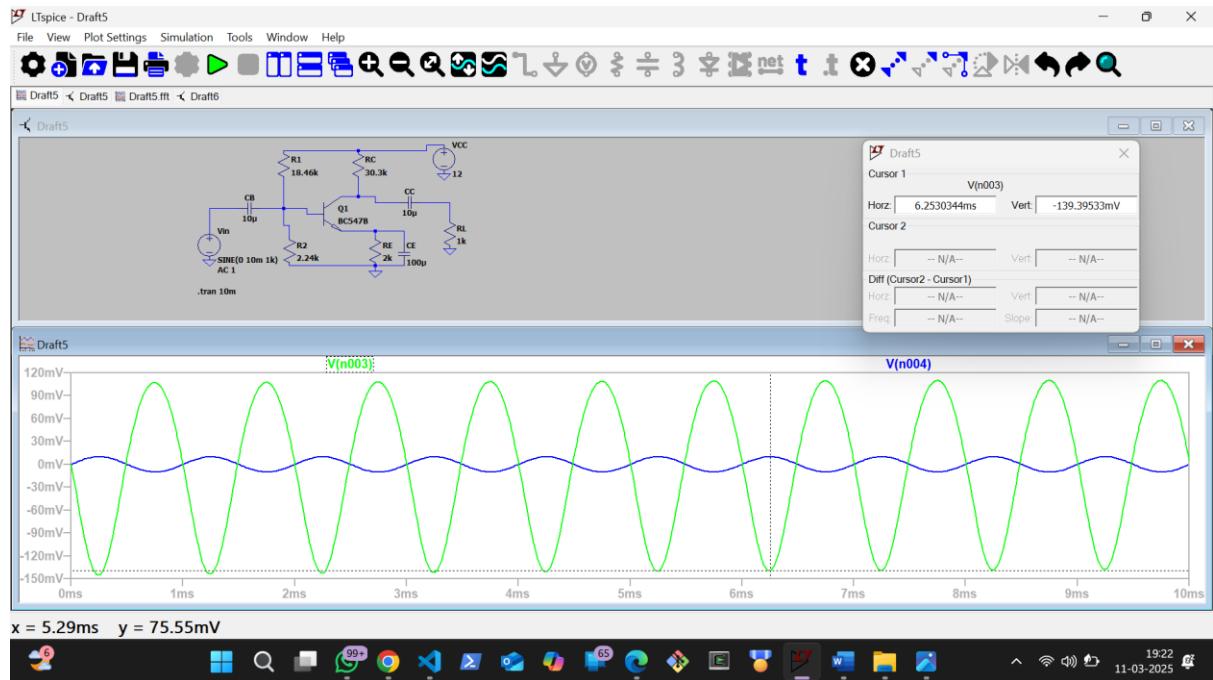
 $R_{C\text{eff}} = \left(\frac{1}{R_C} + \frac{1}{R_L + Z_{CE}} + \frac{1}{r_o} \right)^{-1} \approx 959 \Omega$
 $R_{E\text{eff}} = \left(\frac{1}{R_E} + \frac{1}{Z_{CE}} \right)^{-1} \approx 1.62 \Omega$
 $A_v = -13m\Omega^{-1} \times 959 \approx 12.23$
 $A_v = \frac{V_{out}}{V_{in}} = \frac{13.89}{9.99} = 1.387$
 $A_v = \frac{11.4}{9.99} = 11.15$



Ready



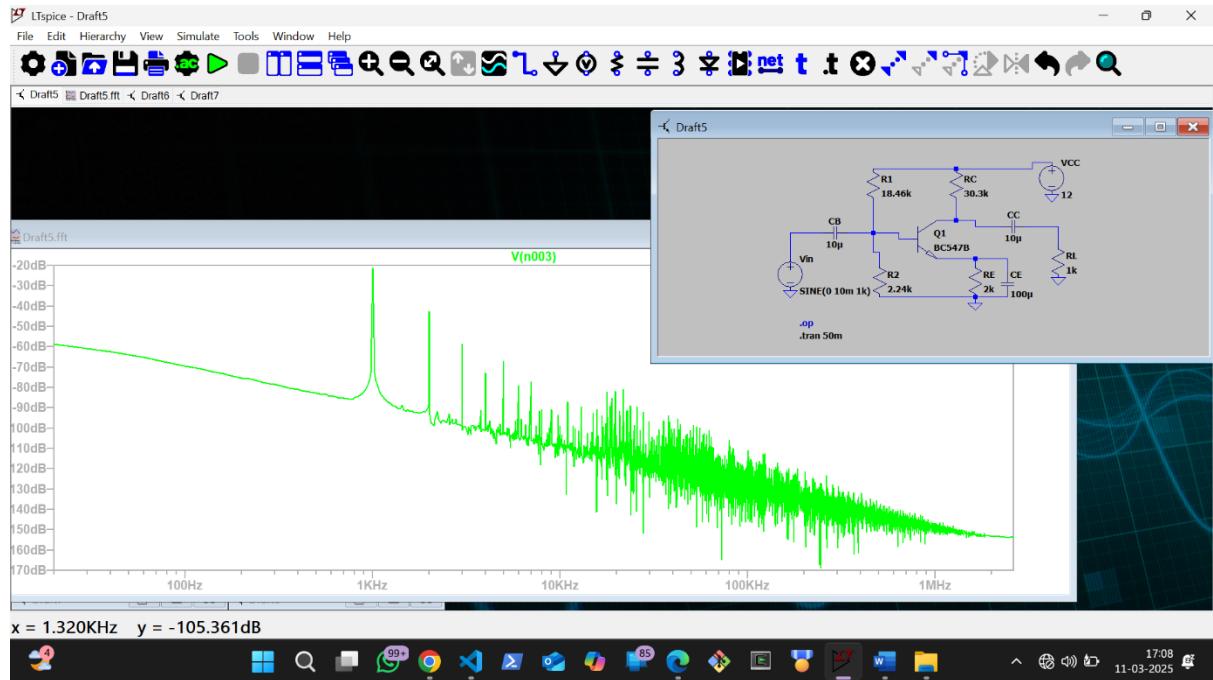




Frequency Analysis

Fast fourier transform

Fundamental FFT 1st Harmonic at 1kHz frequency

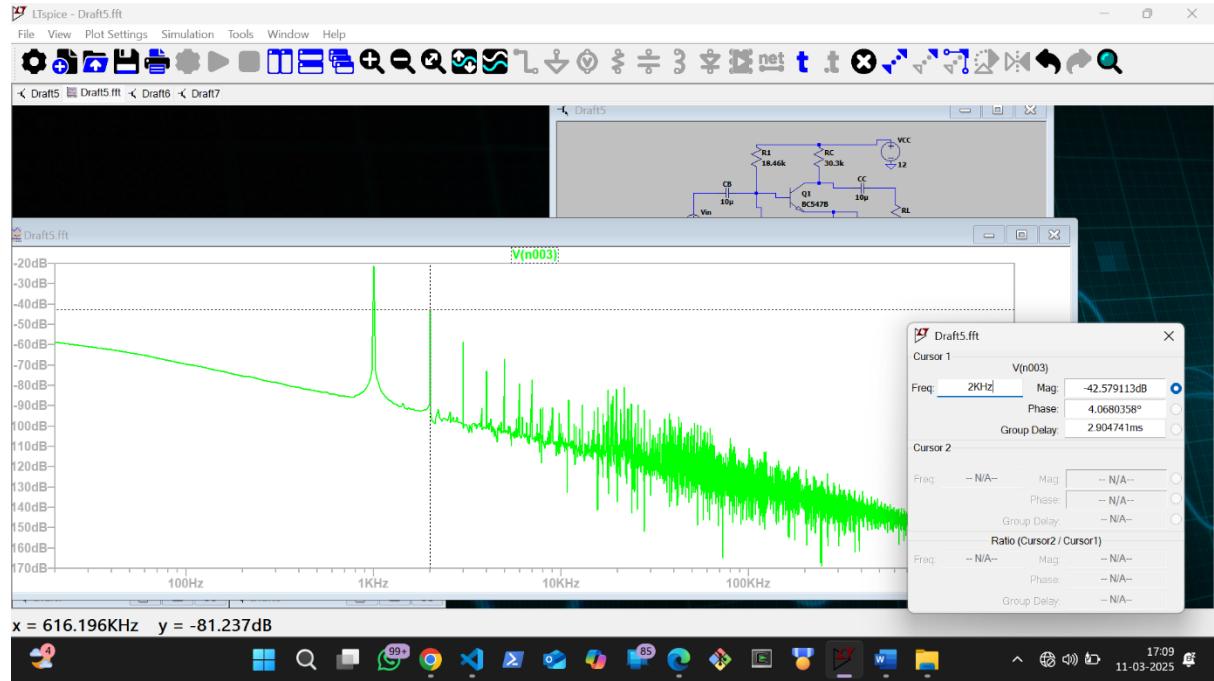


(g) FFT Analysis

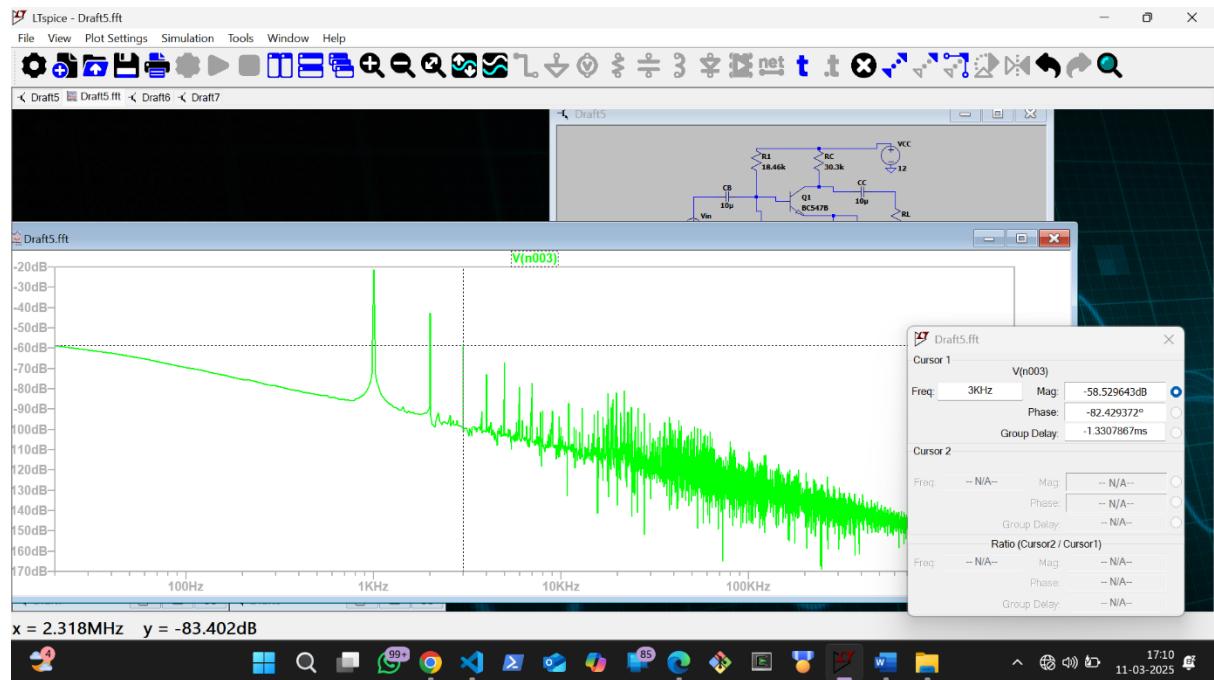
- Run FFT on vout.

- Compare 2nd, 3rd, and 4th harmonics with fundamental (1 kHz) component.

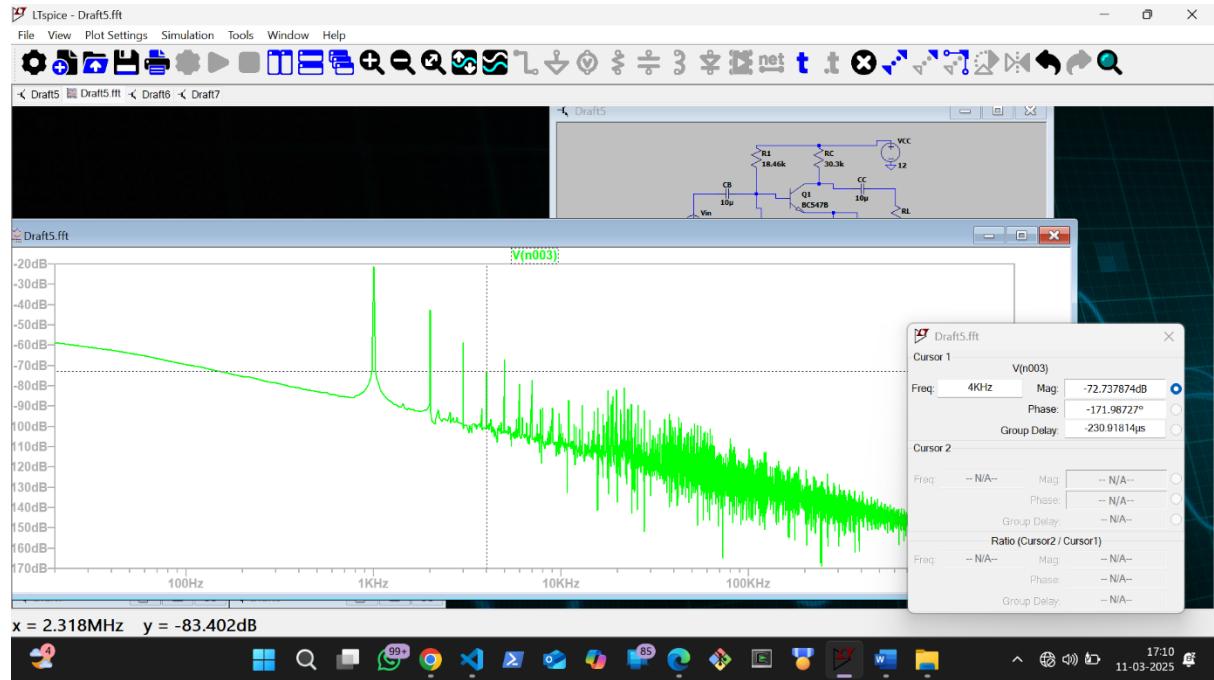
2nd Harmonic



3rd Harmonic



4th Harmonic



Differences for harmonic magnitudes

1KHz → -21.34 → 0.34V

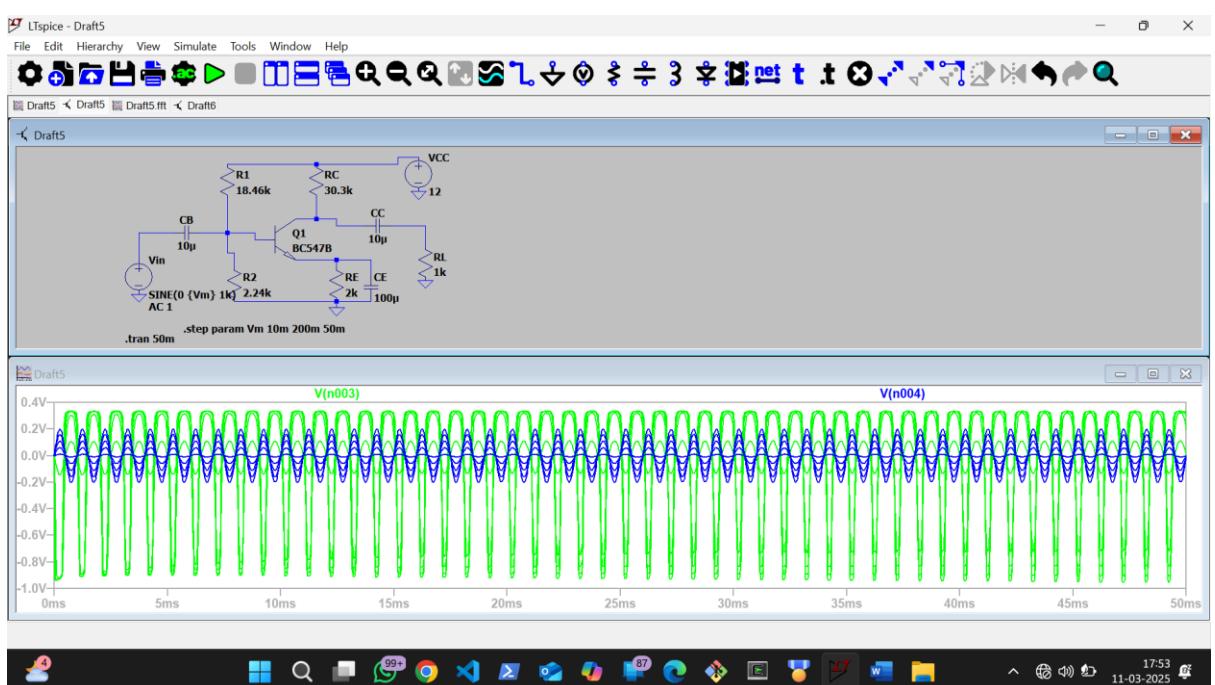
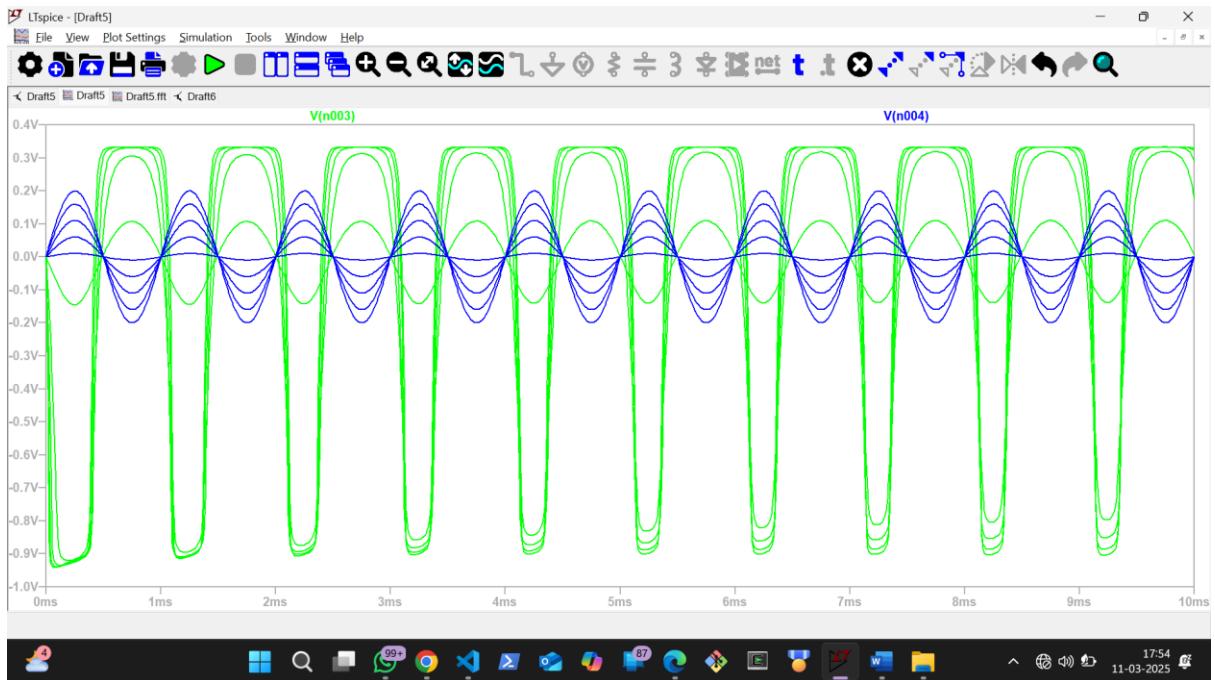
2KHz → -42.579 → 0.12V → 1st - 2nd harmonic = 0.22V

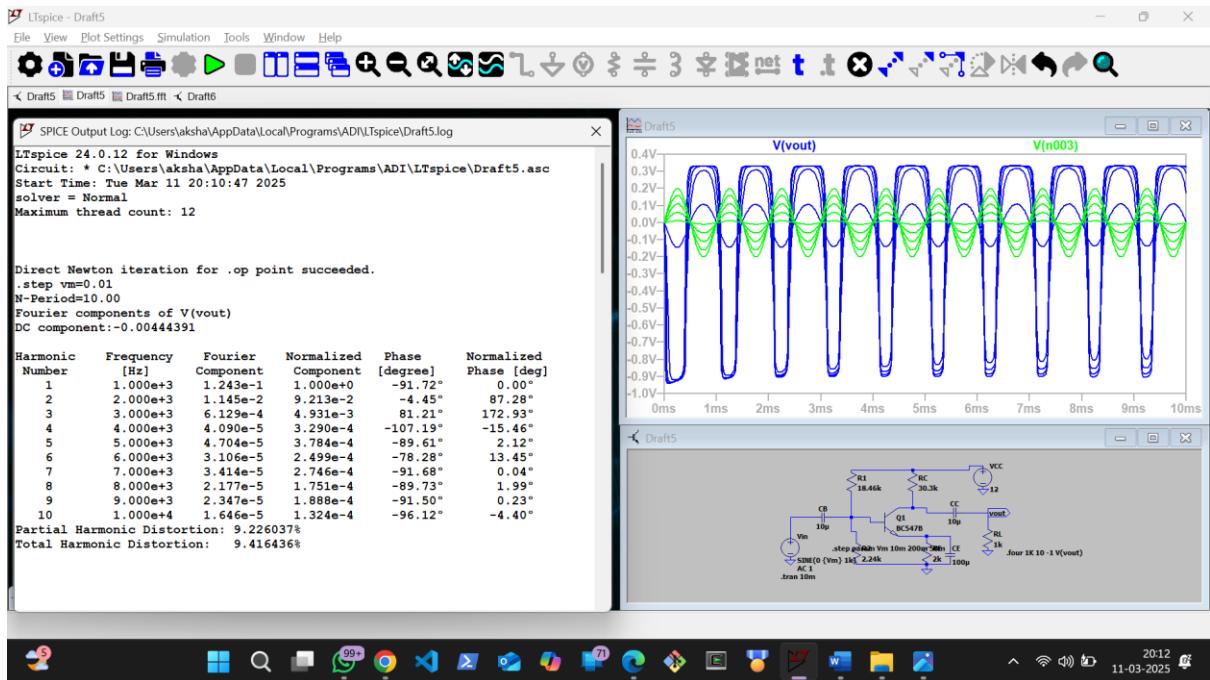
3KHz → -58.52 → 0.05V → 1st - 3rd harmonic = 0.29V

4KHz → -72.73 → 0.026V → 1st - 4th harmonic = 0.314V

(h & i) Total Harmonic Distortion (THD) Analysis and AC Analysis

- Use parametric sweep: **.step param Vm 10m 200m 50m.**
- Extract THD from SPICE error log.
- Analyze THD increase with V_m and justify using calculations.
- Run **.ac dec 10 1m 1G.**
- Plot magnitude and phase of A_v .
- Report DC gain (dB) and -3 dB bandwidth.





```
.step vm=0.06
N-Period=10.00
Fourier components of V(vout)
DC component:-0.097524
```

Harmonic Number	Frequency [Hz]	Fourier Component	Normalized Component	Phase [degree]	Normalized Phase [deg]
1	1.000e+3	5.993e-1	1.000e+0	-92.42°	0.00°
2	2.000e+3	2.192e-1	3.658e-1	-5.88°	86.54°
3	3.000e+3	1.295e-2	2.161e-2	69.09°	161.51°
4	4.000e+3	4.085e-2	6.817e-2	-10.36°	82.06°
5	5.000e+3	3.297e-2	5.501e-2	76.39°	168.81°
6	6.000e+3	1.604e-2	2.677e-2	167.88°	260.30°
7	7.000e+3	4.546e-3	7.586e-3	-96.95°	-4.53°
8	8.000e+3	1.896e-3	3.164e-3	164.40°	256.83°
9	9.000e+3	4.247e-3	7.088e-3	-109.39°	-16.96°
10	1.000e+4	3.289e-3	5.489e-3	-29.02°	63.40°

Partial Harmonic Distortion: 37.791268%
Total Harmonic Distortion: 40.993892%

```

.step vm=0.11
N-Period=10.00
Fourier components of V(vout)
DC component:-0.065071

Harmonic      Frequency      Fourier      Normalized      Phase      Normalized
Number        [Hz]          Component    Component     [degree]    Phase [deg]
1             1.000e+3     6.296e-1   1.000e+0   -93.17°     0.00°
2             2.000e+3     2.892e-1   4.593e-1   -6.45°      86.72°
3             3.000e+3     2.421e-2   3.845e-2   82.13°      175.30°
4             4.000e+3     7.350e-2   1.167e-1   -13.62°     79.55°
5             5.000e+3     6.177e-2   9.812e-2   76.50°      169.66°
6             6.000e+3     2.458e-2   3.905e-2   174.89°     268.06°
7             7.000e+3     3.392e-3   5.387e-3   -6.64°      86.52°
8             8.000e+3     1.105e-2   1.755e-2   167.59°     260.76°
9             9.000e+3     1.298e-2   2.061e-2   -98.29°     -5.13°
10            1.000e+4     8.463e-3   1.344e-2   -18.68°     74.49°

Partial Harmonic Distortion: 48.803404%
Total Harmonic Distortion: 53.855299%

```

```

.step vm=0.16
N-Period=10.00
Fourier components of V(vout)
DC component:-0.0343598

Harmonic      Frequency      Fourier      Normalized      Phase      Normalized
Number        [Hz]          Component    Component     [degree]    Phase [deg]
1             1.000e+3     6.101e-1   1.000e+0   -93.73°     0.00°
2             2.000e+3     3.317e-1   5.438e-1   -6.72°      87.00°
3             3.000e+3     7.422e-2   1.217e-1   85.07°      178.80°
4             4.000e+3     5.861e-2   9.607e-2   -18.56°     75.16°
5             5.000e+3     7.789e-2   1.277e-1   76.97°      170.70°
6             6.000e+3     4.926e-2   8.075e-2   173.86°     267.59°
7             7.000e+3     1.516e-2   2.485e-2   -87.83°     5.90°
8             8.000e+3     1.098e-2   1.800e-2   174.25°     267.97°
9             9.000e+3     2.212e-2   3.626e-2   -99.93°     -6.20°
10            1.000e+4     1.764e-2   2.892e-2   -22.55°     71.18°

Partial Harmonic Distortion: 58.788415%
Total Harmonic Distortion: 64.638172%

```

```

tnom = 27
temp = 27
method = modified trap
.step vm=0.2
N-Period=10.00
Fourier components of V(vout)
DC component:-0.0151986

```

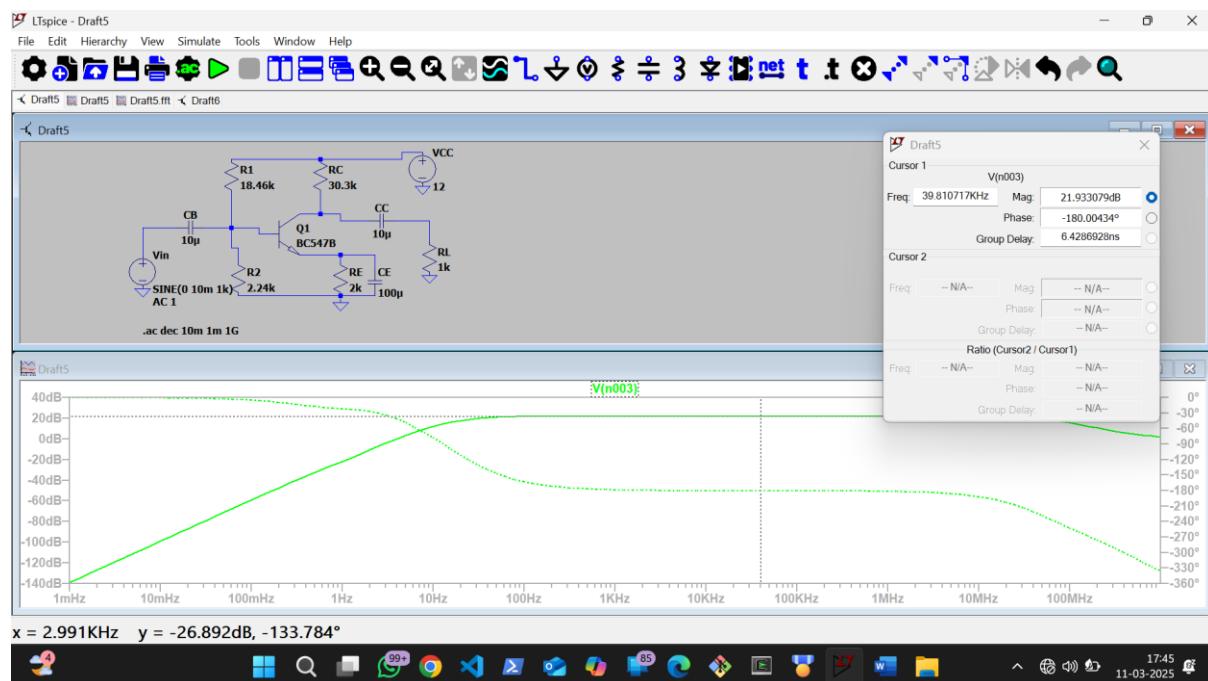
Harmonic Number	Frequency [Hz]	Fourier Component	Normalized Component	Phase [degree]	Normalized Phase [deg]
1	1.000e+3	5.910e-1	1.000e+0	-94.09°	0.00°
2	2.000e+3	3.498e-1	5.918e-1	-6.98°	87.11°
3	3.000e+3	1.096e-1	1.855e-1	85.03°	179.12°
4	4.000e+3	3.669e-2	6.209e-2	-27.98°	66.10°
5	5.000e+3	7.923e-2	1.341e-1	76.64°	170.72°
6	6.000e+3	6.654e-2	1.126e-1	172.86°	266.94°
7	7.000e+3	3.222e-2	5.452e-2	-96.21°	-2.12°
8	8.000e+3	4.434e-3	7.503e-3	-161.14°	-67.06°
9	9.000e+3	2.524e-2	4.271e-2	-100.48°	-6.40°
10	1.000e+4	2.497e-2	4.226e-2	-23.09°	70.99°

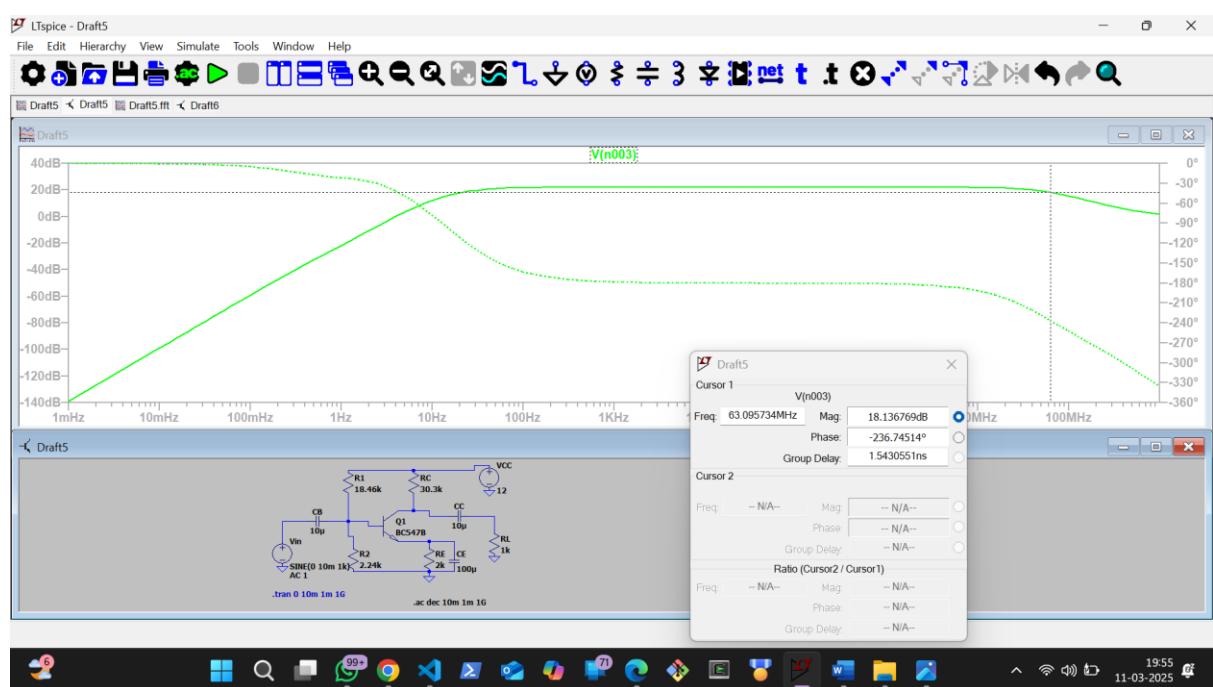
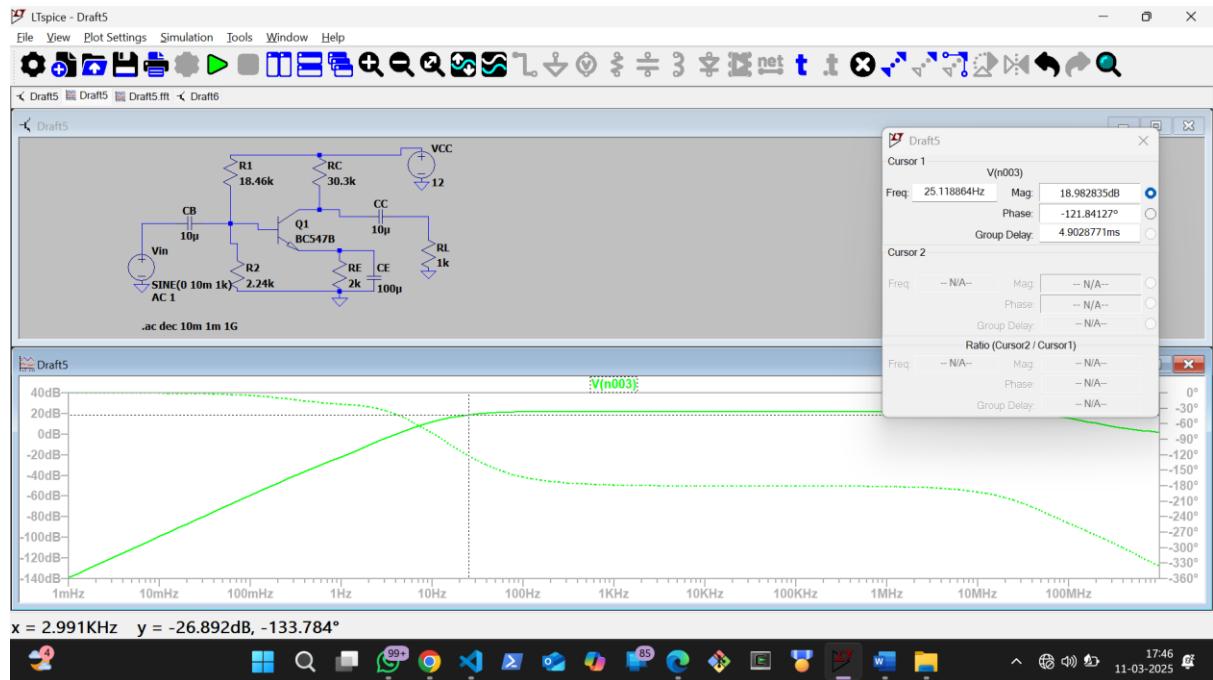
Partial Harmonic Distortion: 65.256930%

Total Harmonic Distortion: 71.503067%

Total elapsed time: 0.551 seconds.

THD increases with increasing input voltage because the BJT operates more nonlinearly at higher signal amplitudes, introducing harmonic distortion through gain variation, clipping, capacitance effects, and intermodulation.





Lower cutoff frequency is 25.11 Hz

Higher cutoff frequency is 63.09 MHz

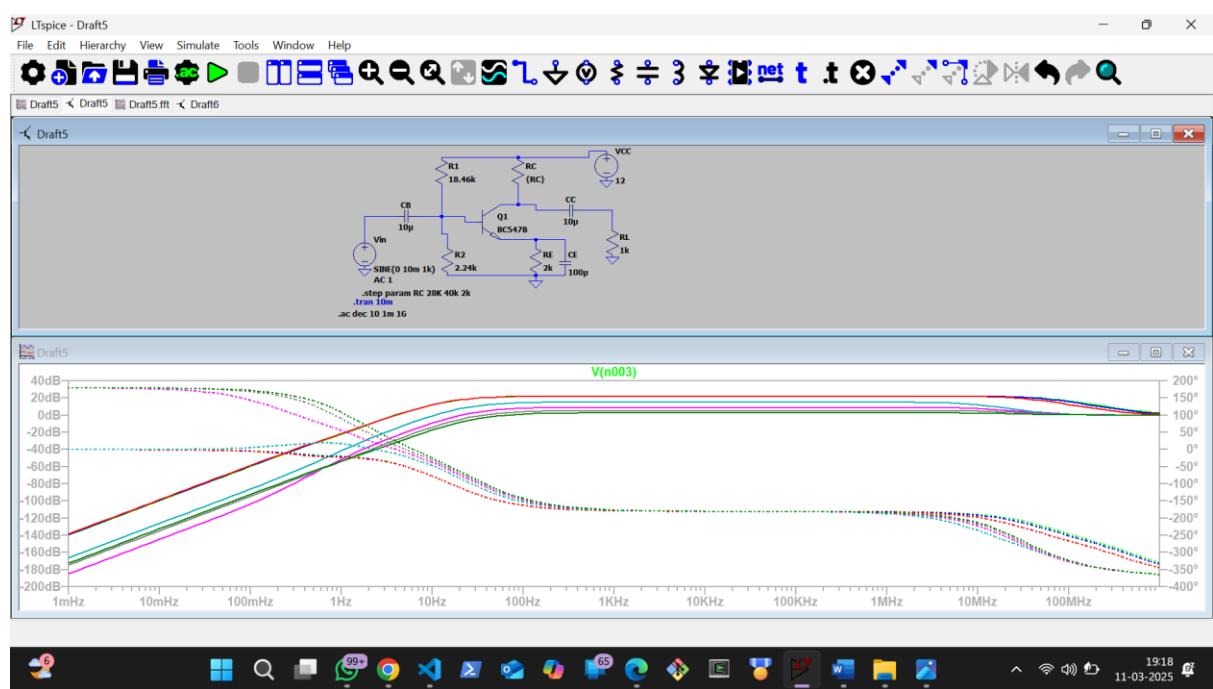
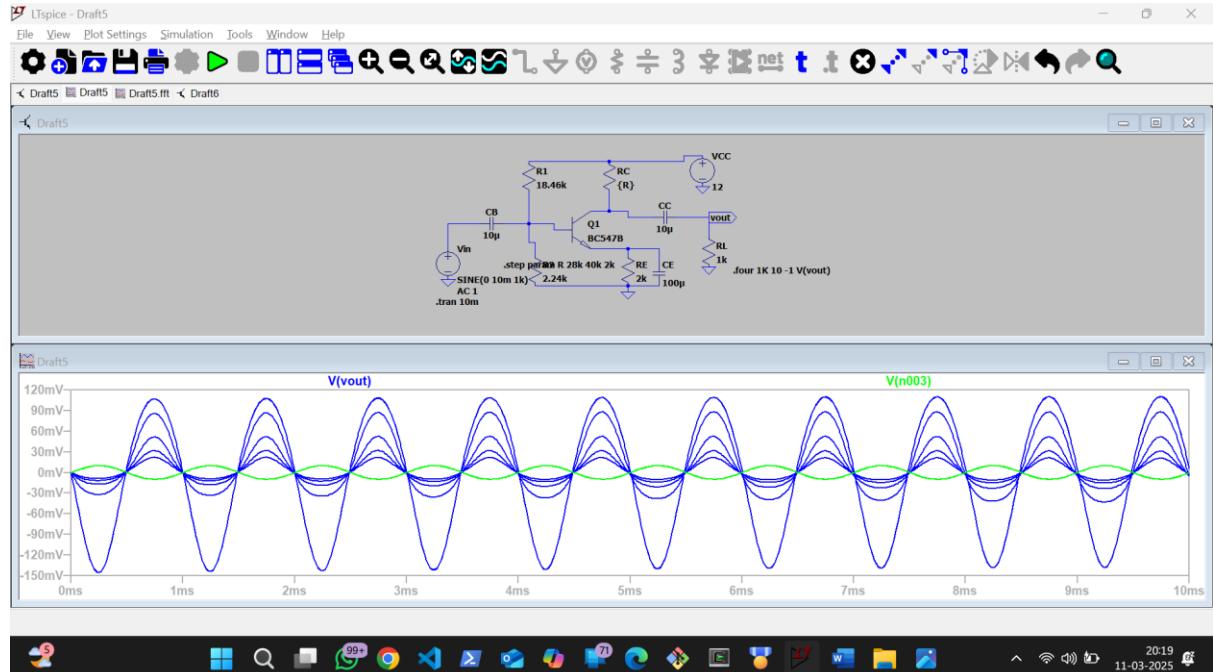
Band width is approx 63.09MHz

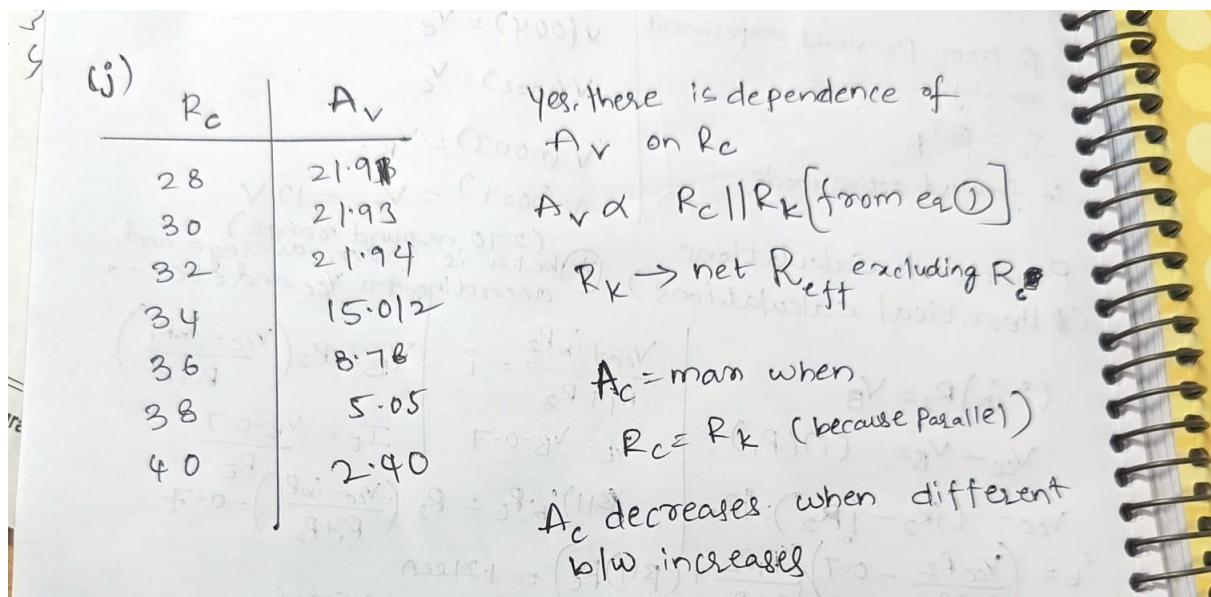
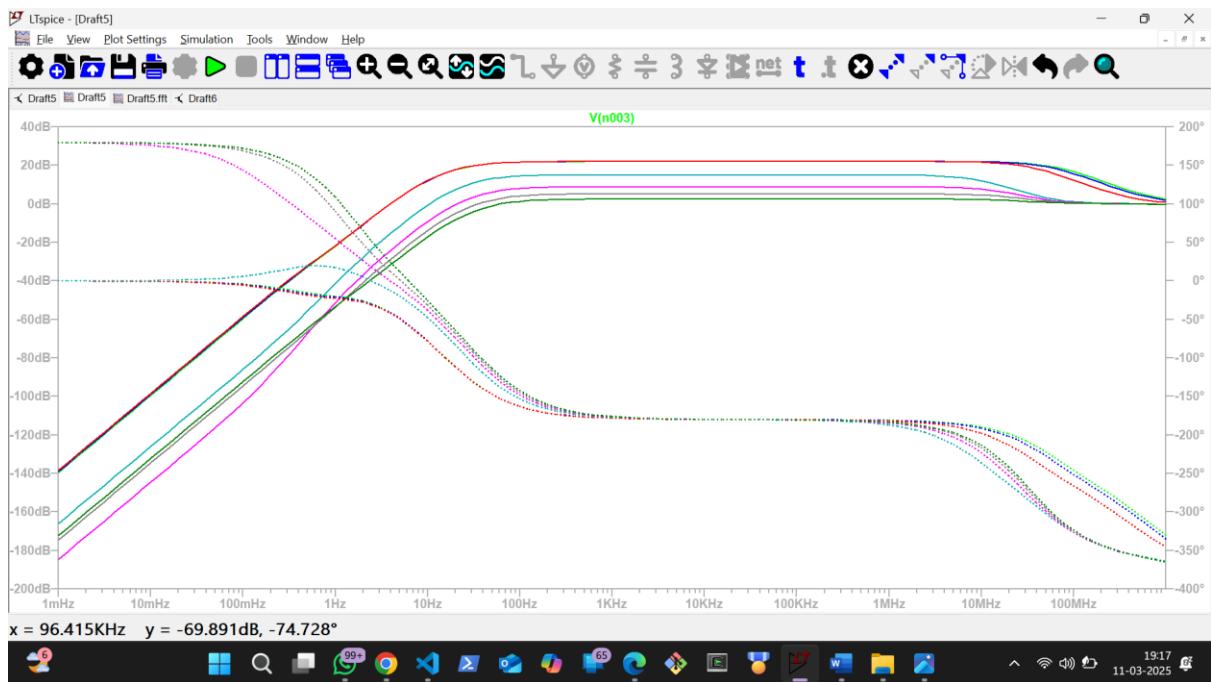
The max DC gain is 21.933 dB

6. Change in gain by RC

(j) Effect of RC on Gain

- Parametrize RC from **28 kΩ** to **40 kΩ** in steps of **2 kΩ**.
- Run **.ac** simulation and plot Av.
- Compare DC gain for different RC values.
- Justify gain variation quantitatively for $RC = 30 \text{ k}\Omega$ and $RC = 40 \text{ k}\Omega$.





5)

5) We require same bandwidth and same gain
but V_{cc} changes from 12 V_{cc} to 5 V_{cc}

by prev calculations

$$V_C = 0.16V, I_C = 0.34mA \text{ at } V_{cc} = 5V$$

$$\text{if and only if } R_C = 10k\Omega$$

Similarly

$$V_{cc}R_2 = 1.3(R_1 + R_2)$$

by Trial & error and some other calculations and theory

$$\text{let, } R_1 = 30k\Omega \quad R_2 = 10.45k\Omega$$

by considering these values such that V_B and i_b
do not change as previous gain should be same

there's very little change in the bandwidth which
can be adjusted by changing frequency dependent
impedances slightly but not by huge value.

In conclusion,

$$R_1 = 30k\Omega$$

$$R_2 = 10.45k\Omega$$

$$R_C = 10k\Omega$$

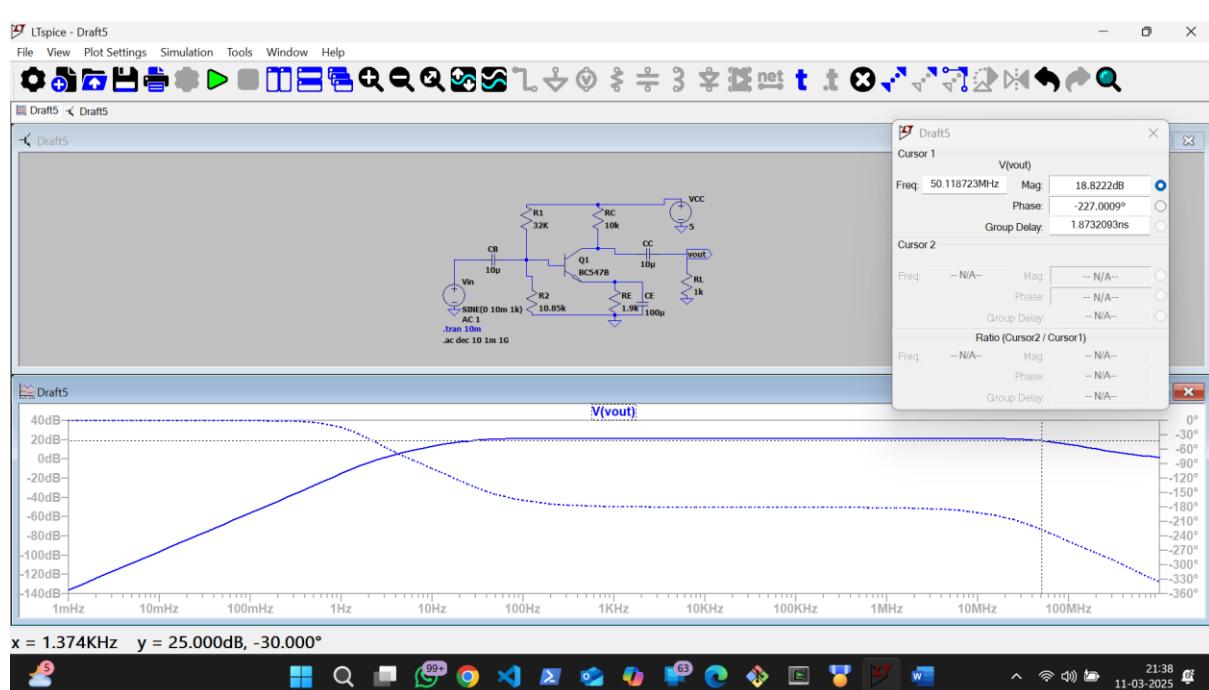
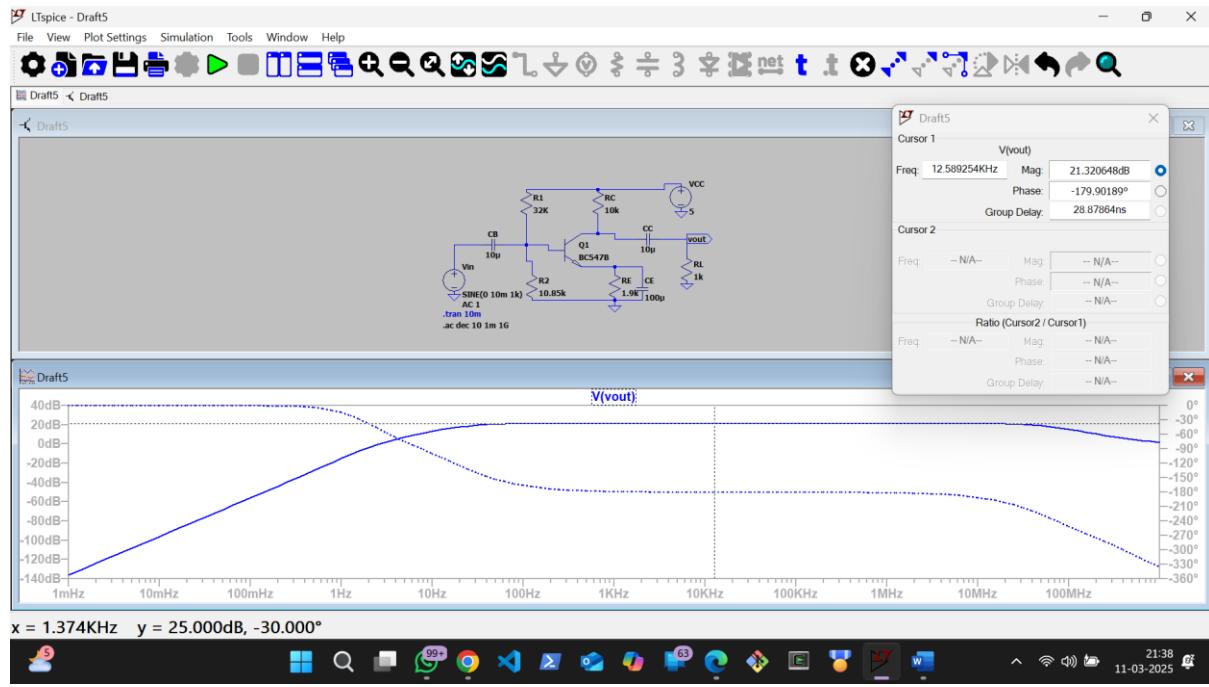
$$R_L = 1k\Omega$$

$$R_E = 2k\Omega$$

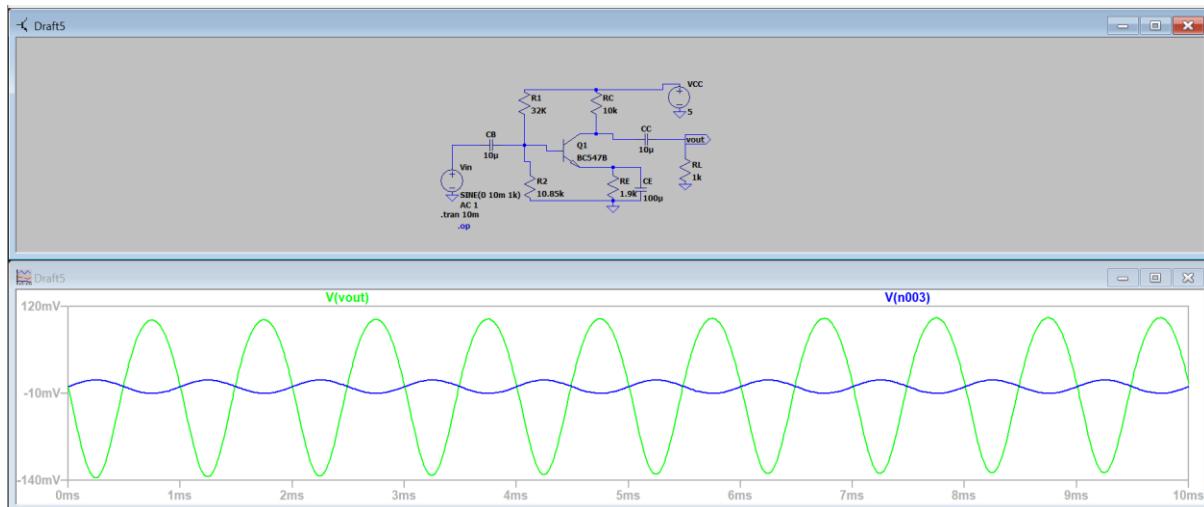
$$C_E = 100\text{pF}$$

$$C_B = 10\text{pF}$$

$$C_C = 10\text{pF}$$



V(n001) :	5	voltage
V(n004) :	1.25639	voltage
V(n005) :	0.646256	voltage
V(n002) :	1.61057	voltage
V(vout) :	1.61057e-14	voltage
V(n003) :	0	voltage
Ic(Q1) :	0.000338943	device_current
Ib(Q1) :	1.19143e-06	device_current
Ie(Q1) :	-0.000340135	device_current
I(Cc) :	-1.61057e-17	device_current
I(Cb) :	1.25639e-17	device_current
I(Ce) :	6.46256e-17	device_current
I(R1) :	0.000116988	device_current
I(R2) :	0.000115796	device_current
I(Re) :	0.000340135	device_current
I(Rc) :	0.000338943	device_current
I(Rl) :	1.61057e-17	device_current
I(Vcc) :	-0.000455931	device_current
I(Vin) :	1.25639e-17	device_current



The DC power of the amplifier is

$$\text{For } VCC = 5V \quad P_{DC} = Vcc * (Ic + (Vcc - Vb) * R1) = 2.31\text{mW}$$

$$\text{For } VCC=12V \quad P_{DC} = Vcc * (Ic + (Vcc - Vb) * R1) = 11\text{mW}$$

The net effective current is taken from (.op) I(VCC): in both the pictures.

at
Let $I_B = 60 \mu A$

Since slope is same

w.r.t. given

slope = $I_C / (V_A + V_{CE})$ equating slopes.

$$\text{at } 5V \Rightarrow \frac{13.88}{V_A + 5V} = \frac{14.94}{V_A + 10V} \text{ at } 10V$$

$$14.94V_A - 13.88V_A + 5 \times 14.94 = 10 \times 13.88$$

$$1.06V_A = 64.1$$

$$\therefore V_A = 60.47 \text{ approx (60)}$$

(3.2) from the graph.

V_{BE} decreases -1.6 to $-2 mV$ per $^{\circ}\text{C}$ is ~~is~~
almost linear.

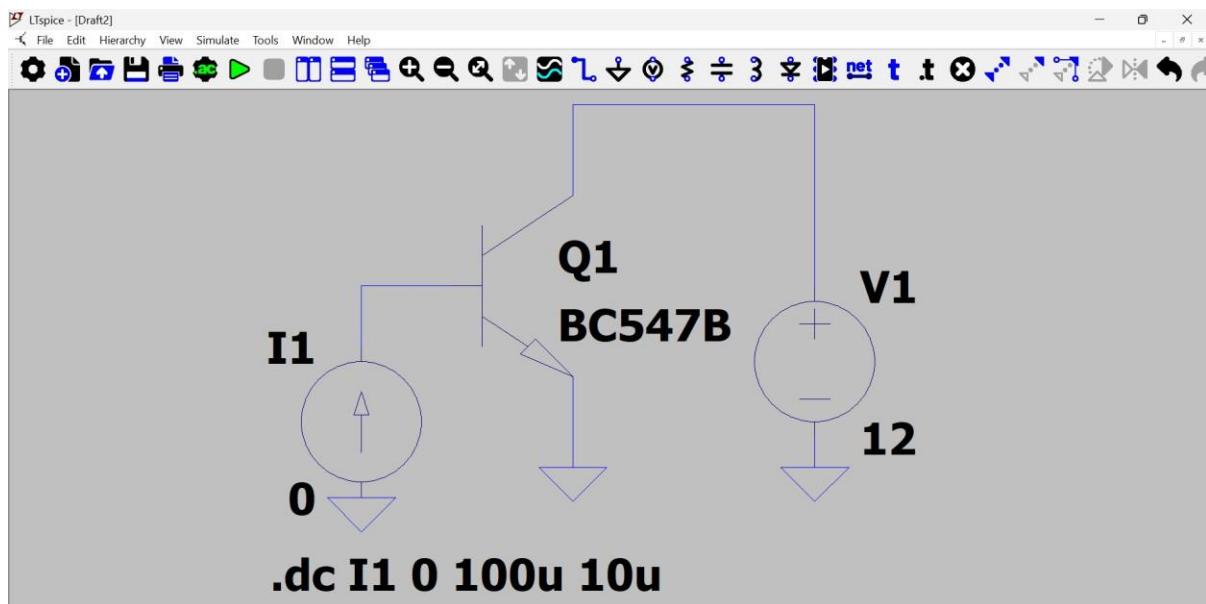
(3.1) from plot we get EBJ (Emitter base junction)

- voltage to be about 700 to $740 mV$

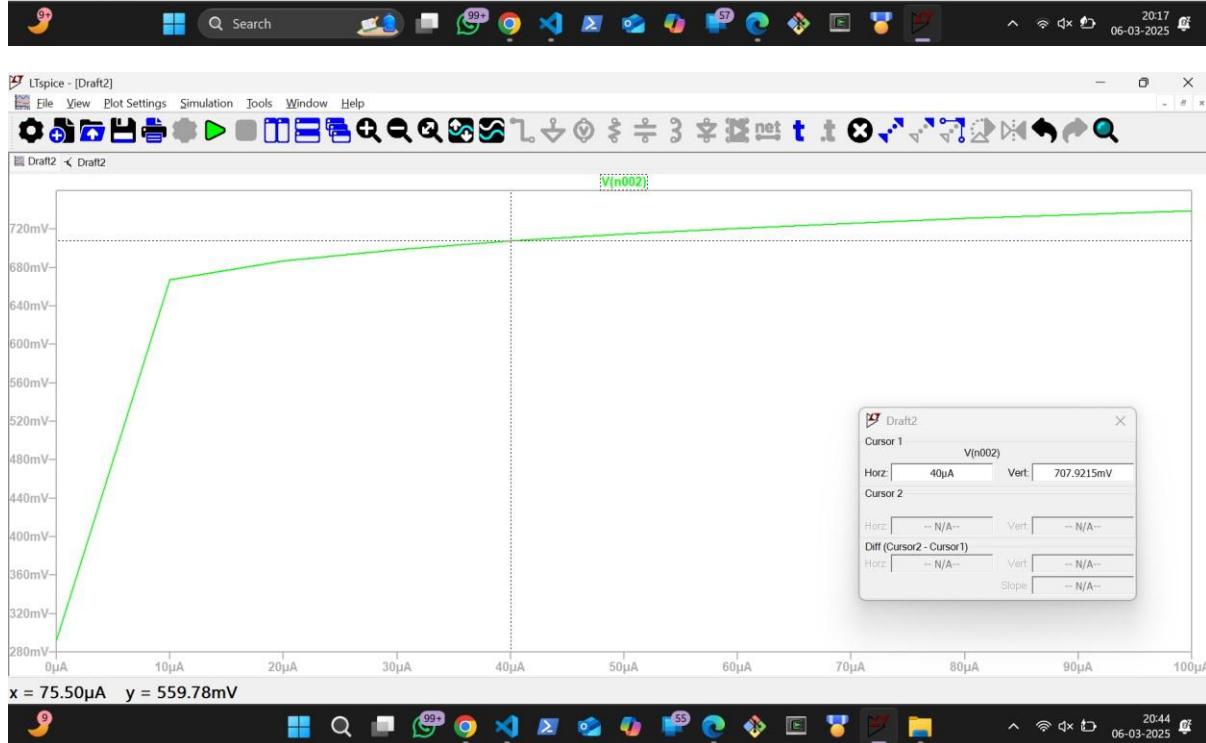
from above plots for BJT in active/saturation

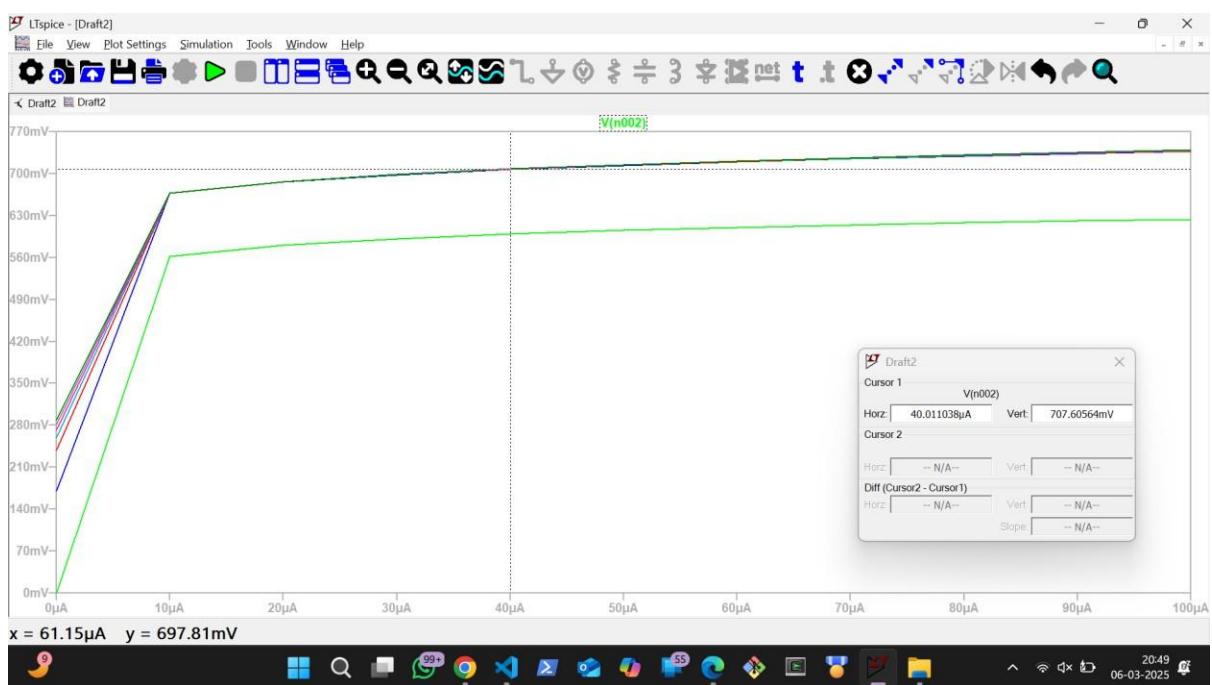
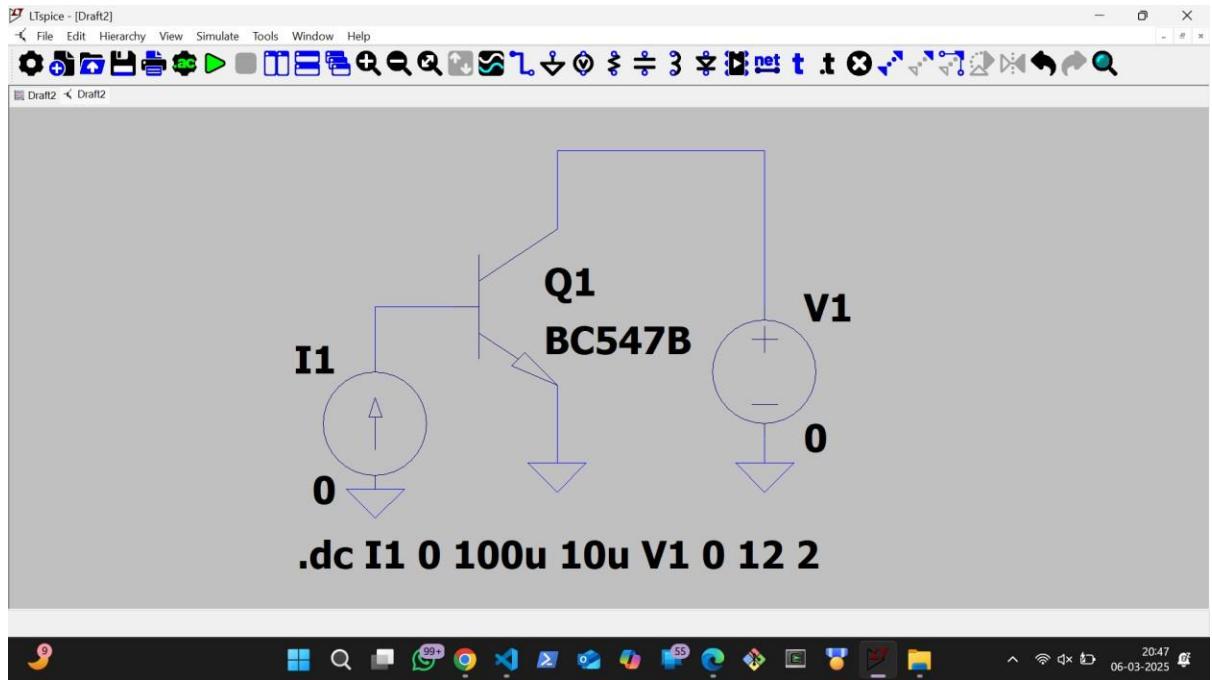
we need to have V_{BE} greater than the EBJ voltage

Q-3.1

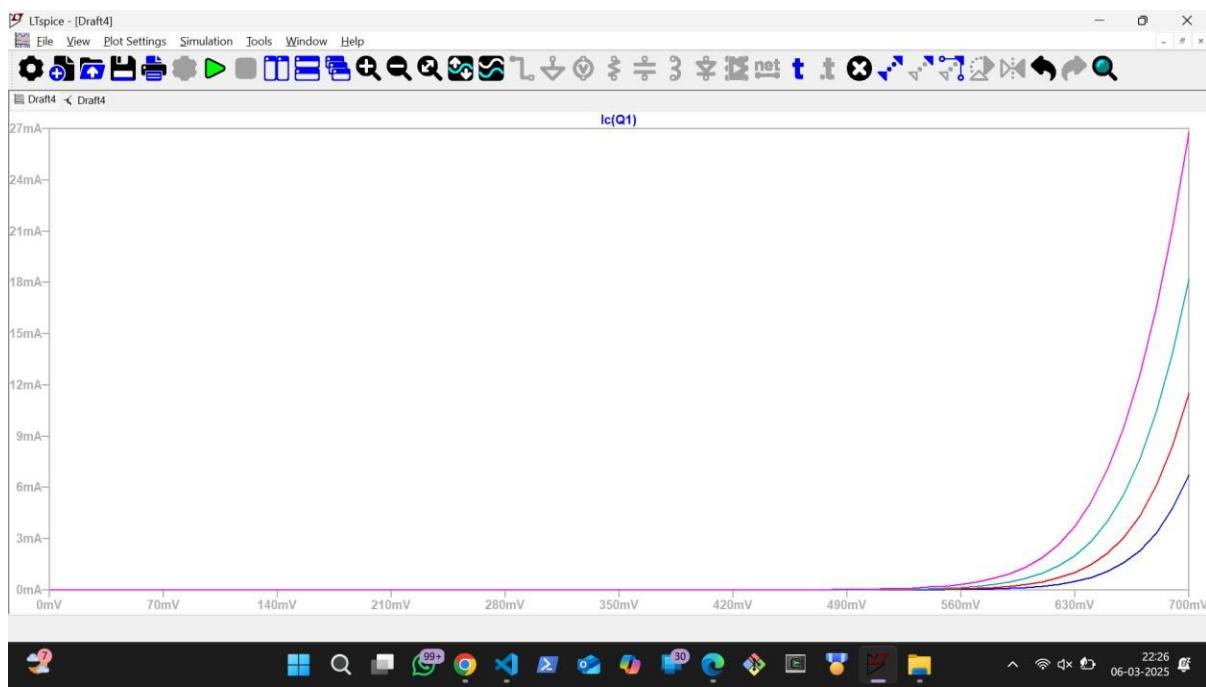
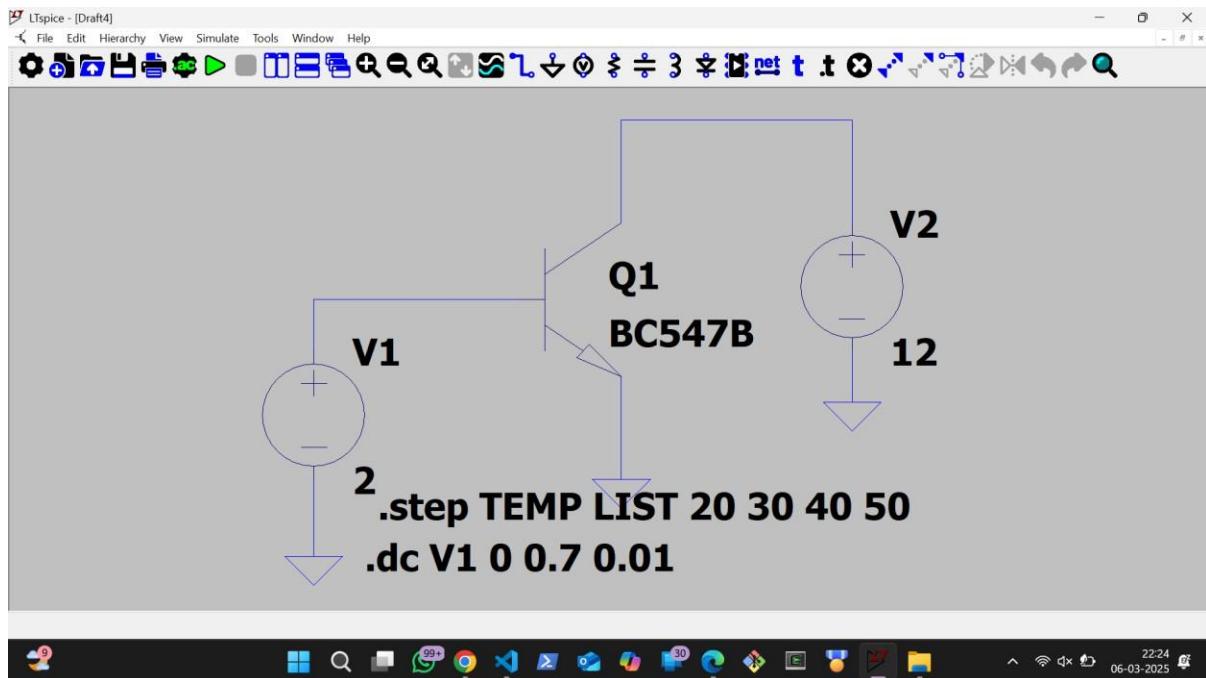


This is node N001.





Q-3.2



- (3.3) * below 0.24 is deep saturation $I_C \approx 0$ goes to cutoff
 * forward active ($0.65 - 0.71$) * ($0.25 - 0.26$) saturation
 to 0.30

S.No	V_{CE}	$(I_B)_1$	$(I_B)_2$	$(I_c)_1$	$(I_c)_2$	ΔI_c	$\Delta I_B \beta$
1	100mV	50mA	60mA	5.34mA	6.21mA	0.87mA	10mA 87
2	600mV	50mA	60mA	18.95	15.29	2.34mA	10mA 234

β at saturation (100mV) 87

β at active (600mV) 234 (sat to active)

Incremental: Difference observed b/w β at different V_{CE}

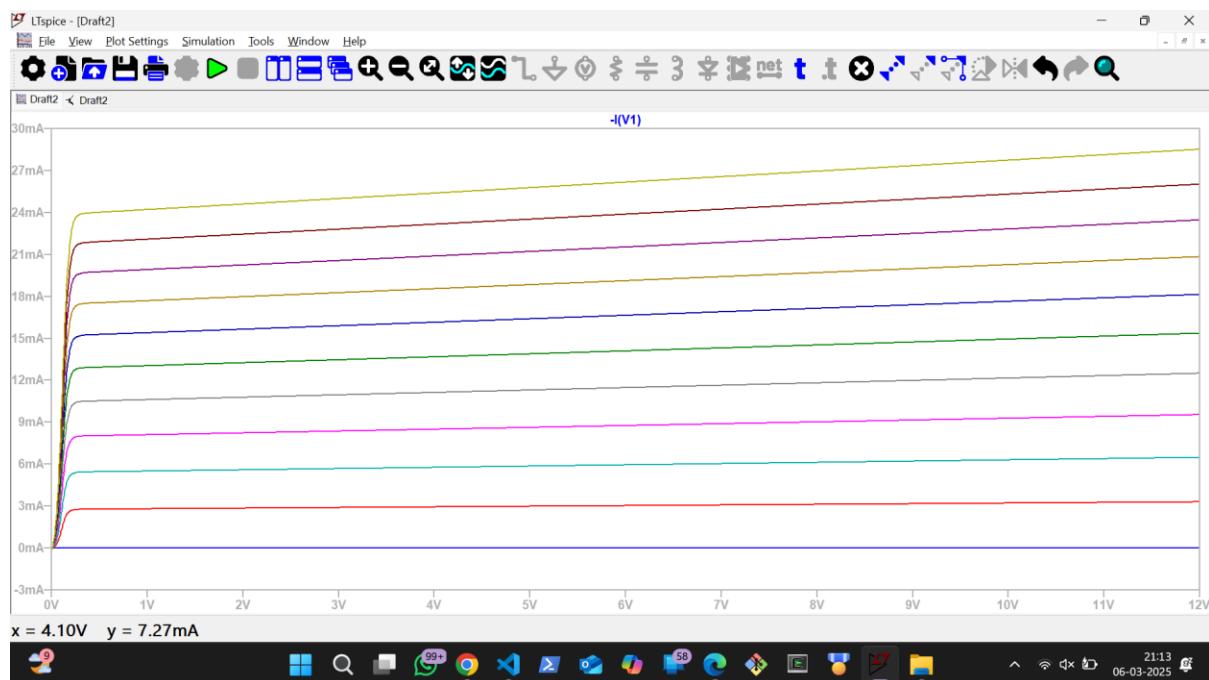
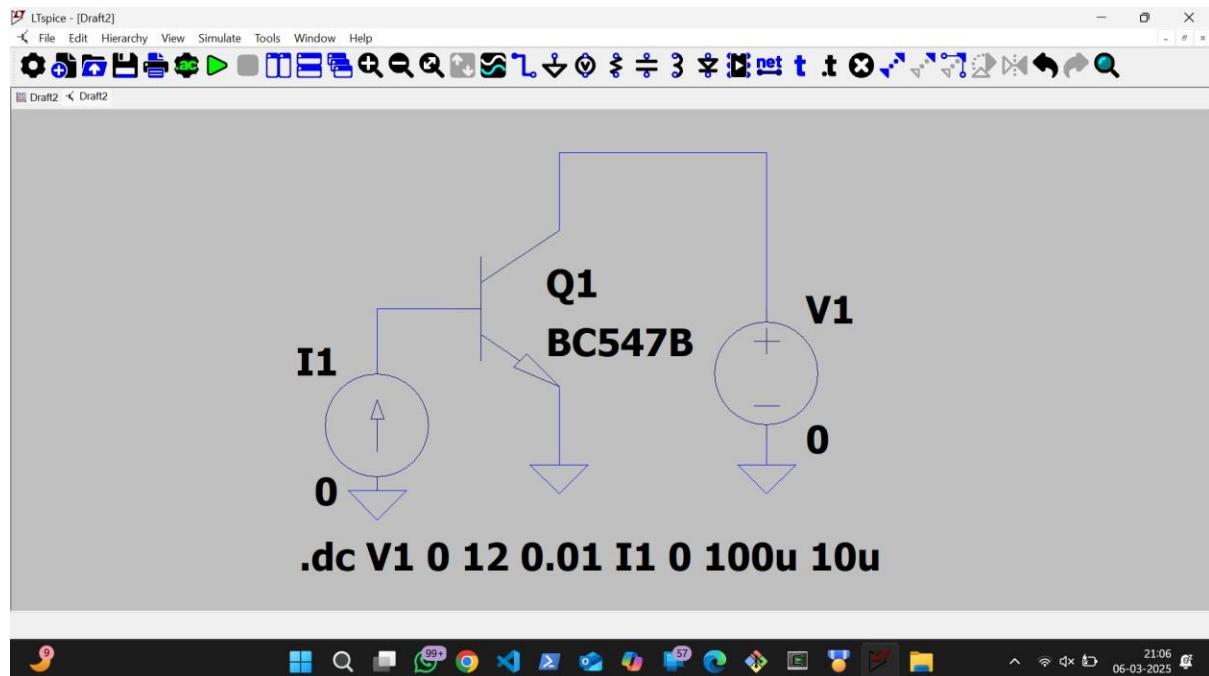
because collector goes into reverse bias while V_{CE} going from saturation to active mode

V_{CE}	$I_C(mA)$	$I_B(mA)$	$\beta = \frac{I_C}{I_B}$
IV	-17.68	0	-
IV	2.8	10	280
IV	5.5	20	275
IV	8.1	30	270
IV	10.61	40	265
IV	13.09	50	260
IV	15.39	60	256
IV	17.68	70	252
IV	19.91	80	248
IV	22.09	90	245
IV	24.2	100	242

Then $I_B \downarrow$ and
thereby $\uparrow \beta = \frac{I_C}{I_B}$
Hence, β increases

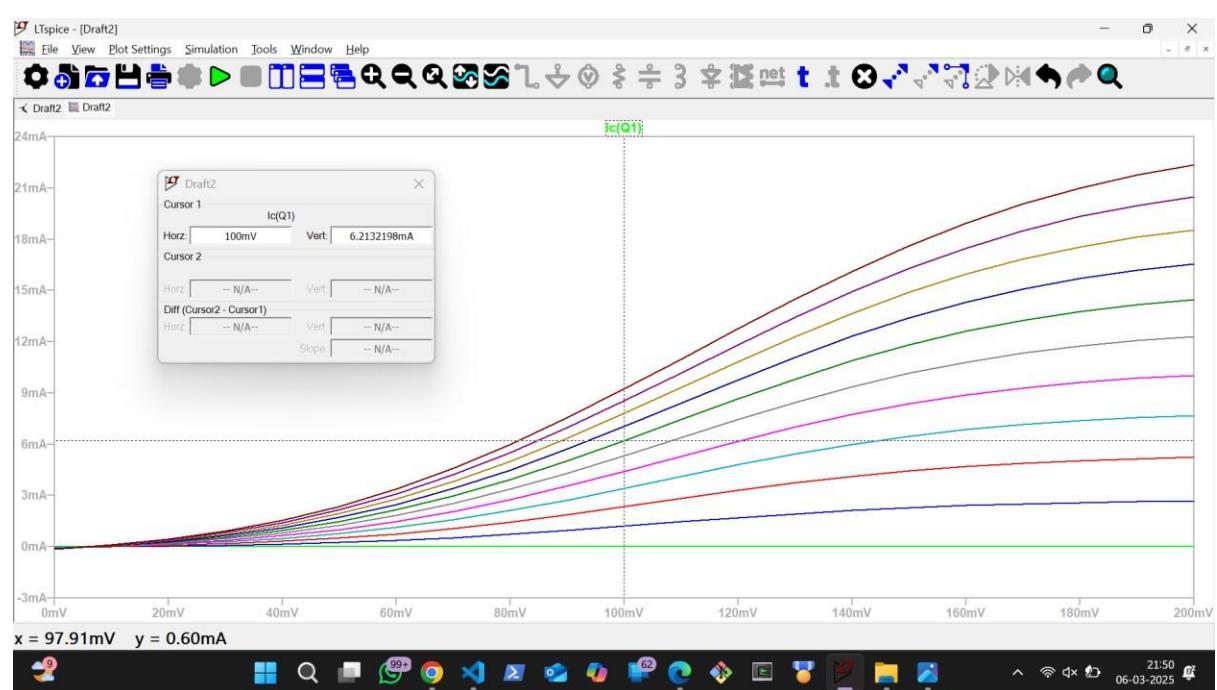
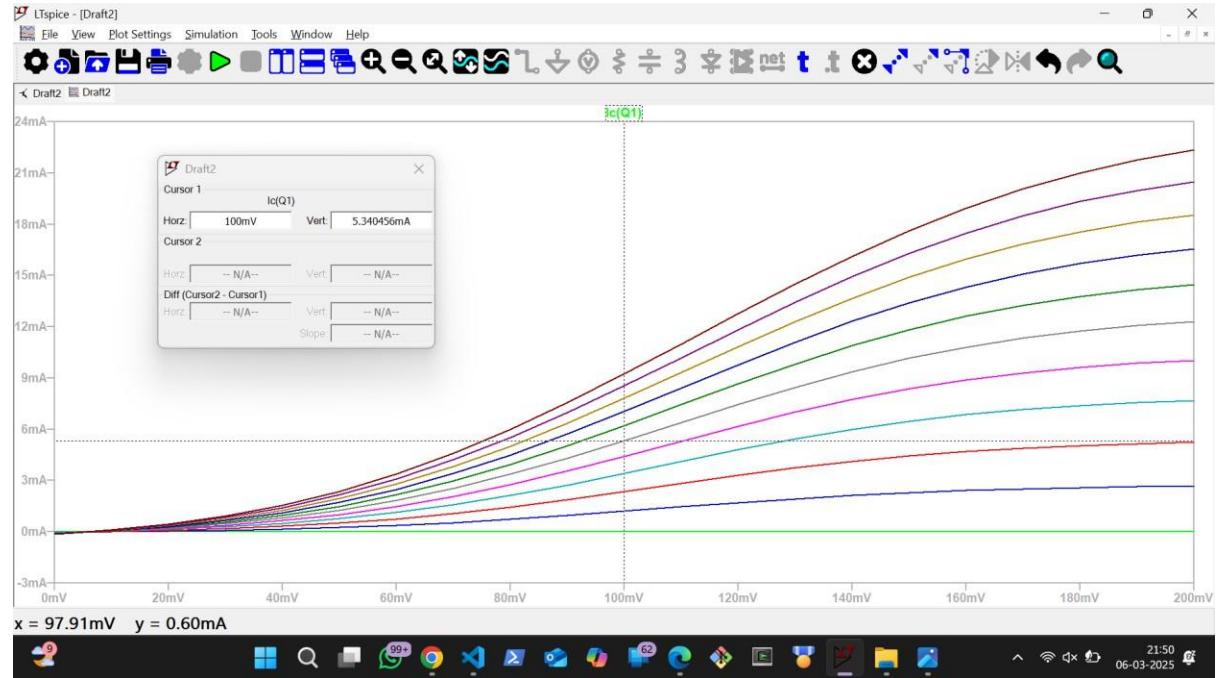
Yes, Early effect is observed (Base-Width modulation) causes β to increase as V_{CE} \uparrow as since higher V_{CE} reduces the base width, so, I_C increases in very small amount.

Q-3.3

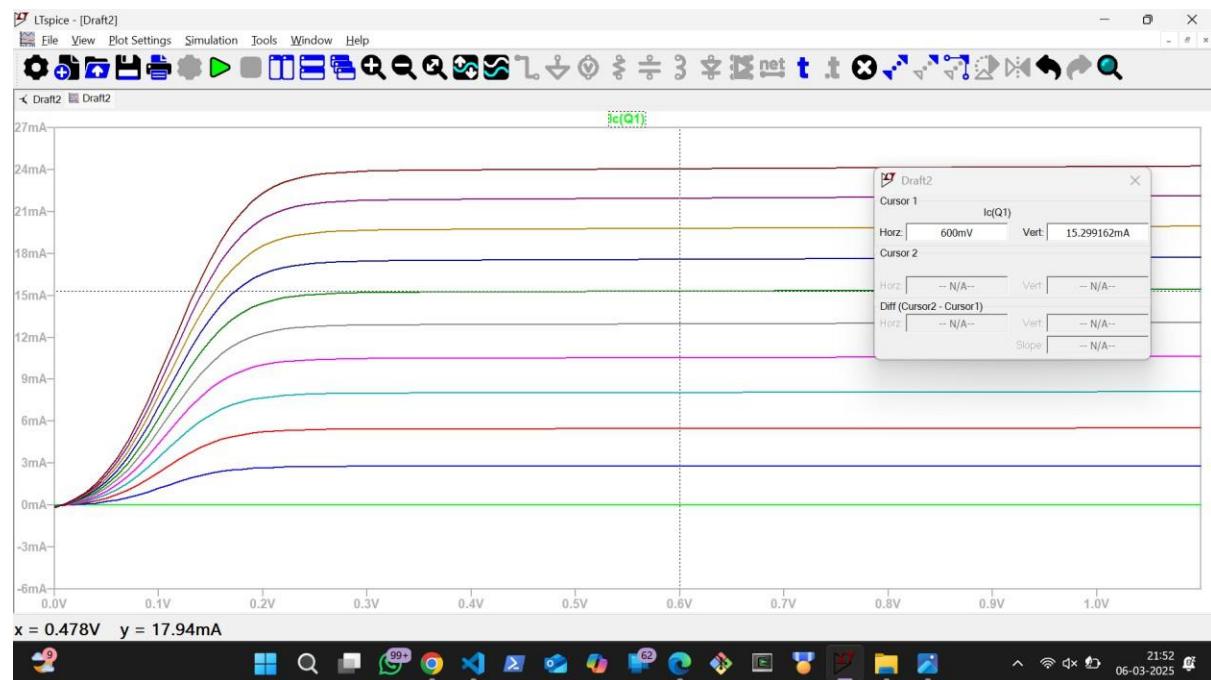
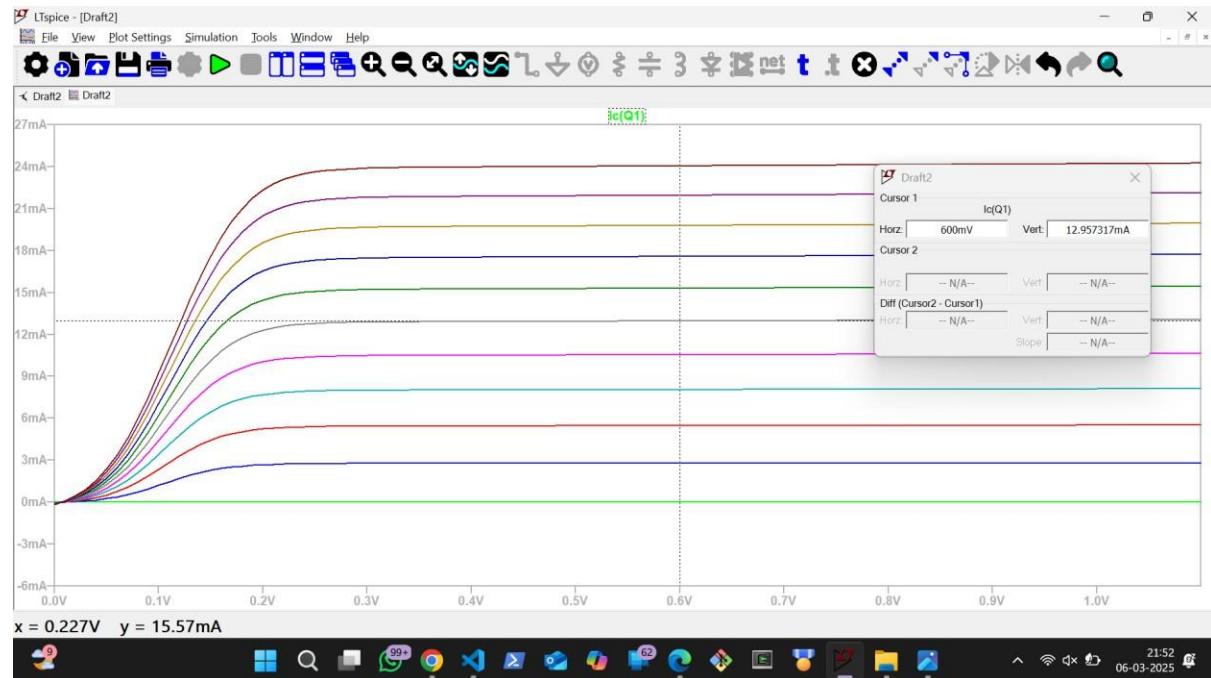


Calculation of beta (β) by change in currents of I_C and I_B at 50uA and 60uA

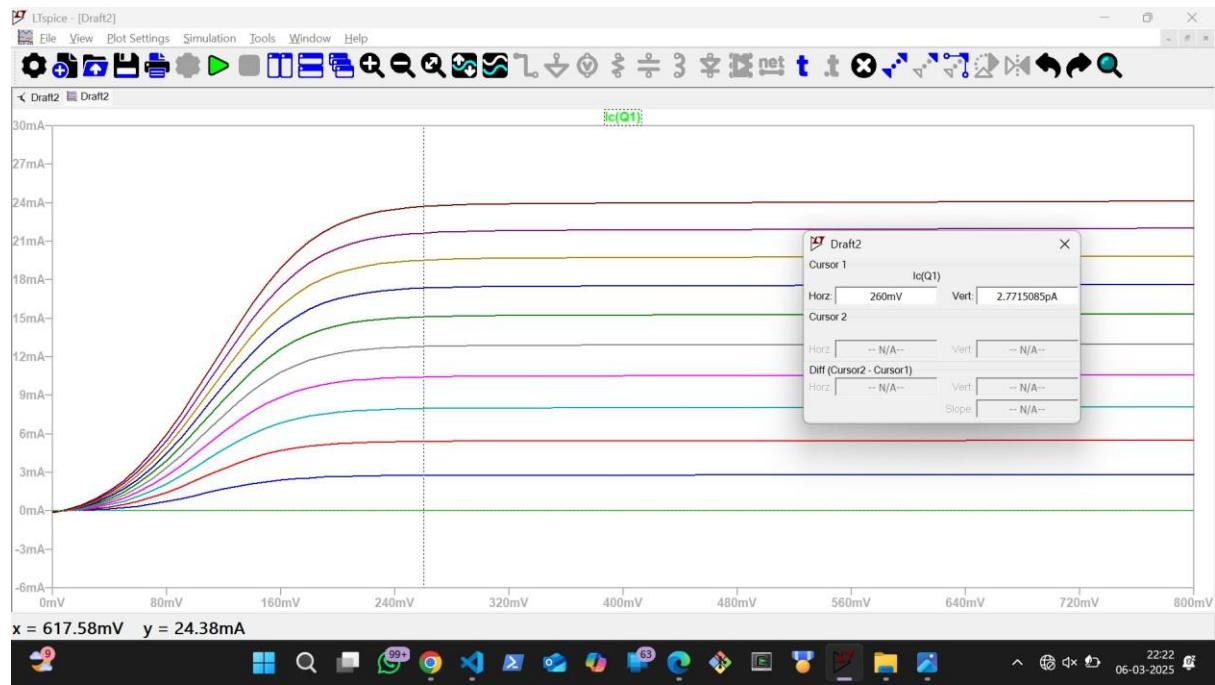
At 100mV



At 600mV



Saturation and Active mode mark

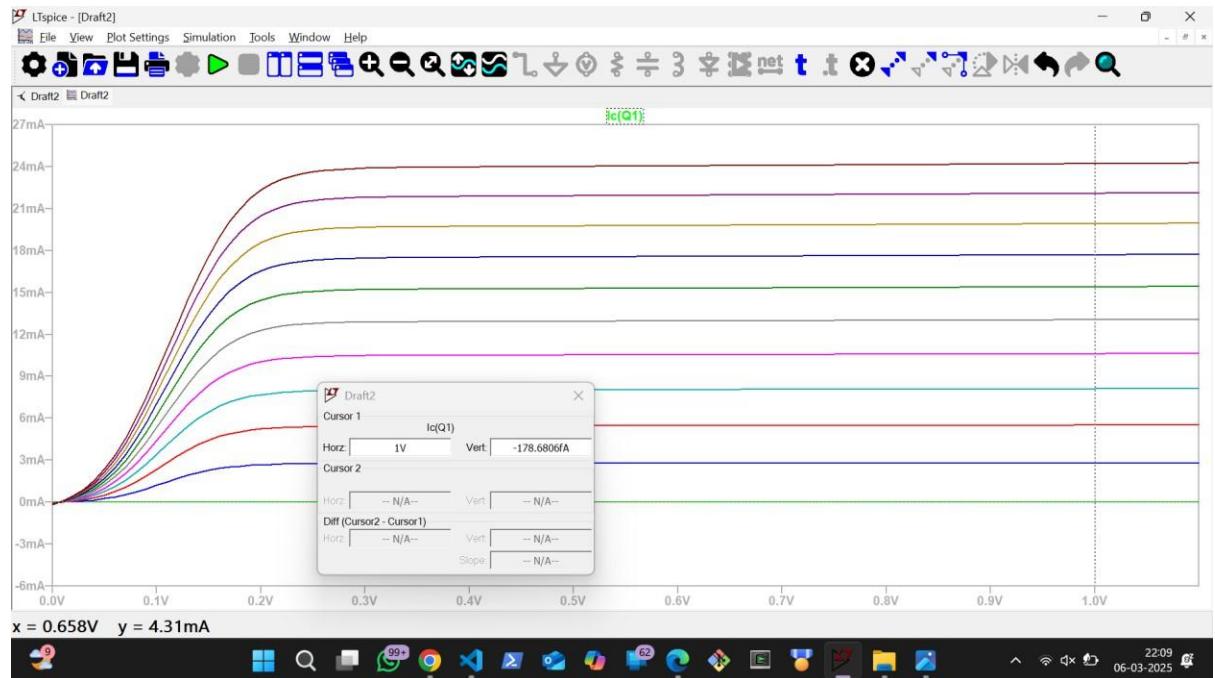


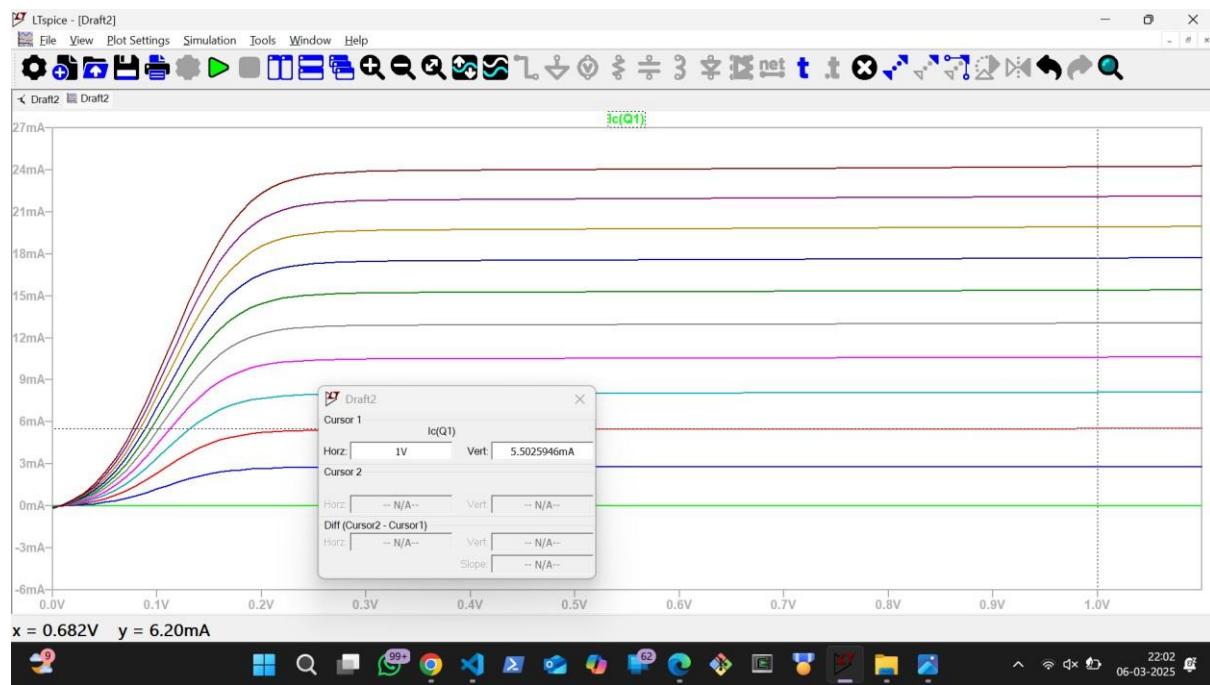
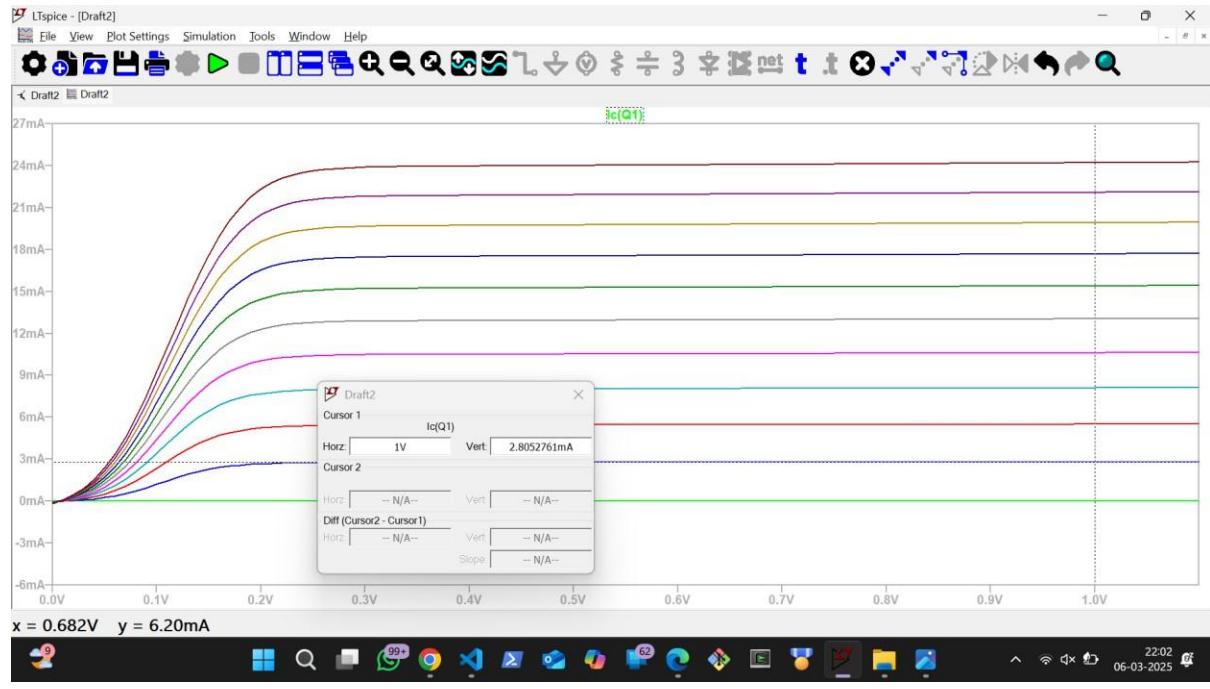
220mV-260mV-300mV saturation

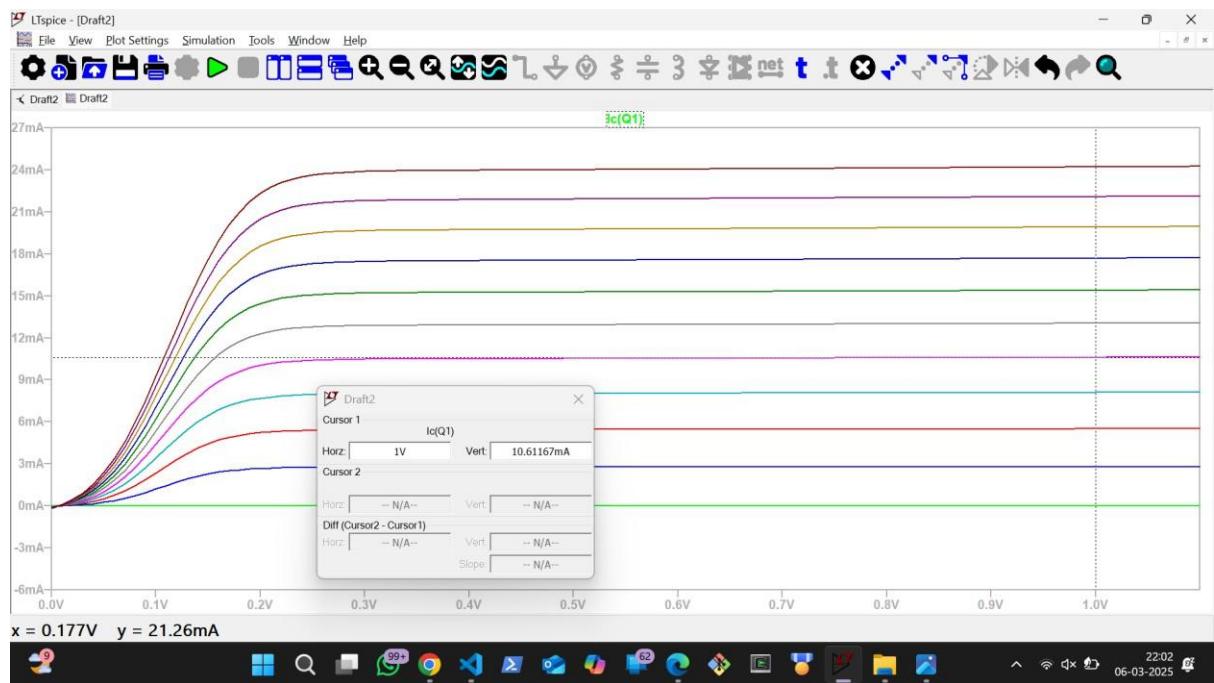
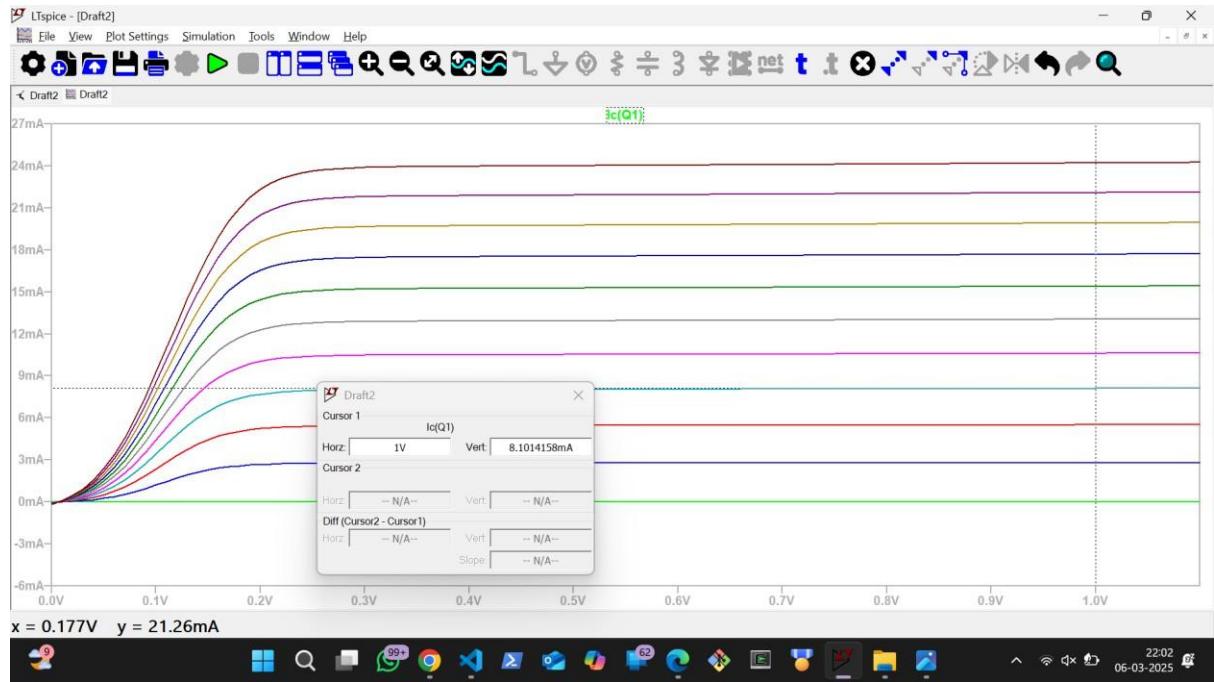
Above it is active mode

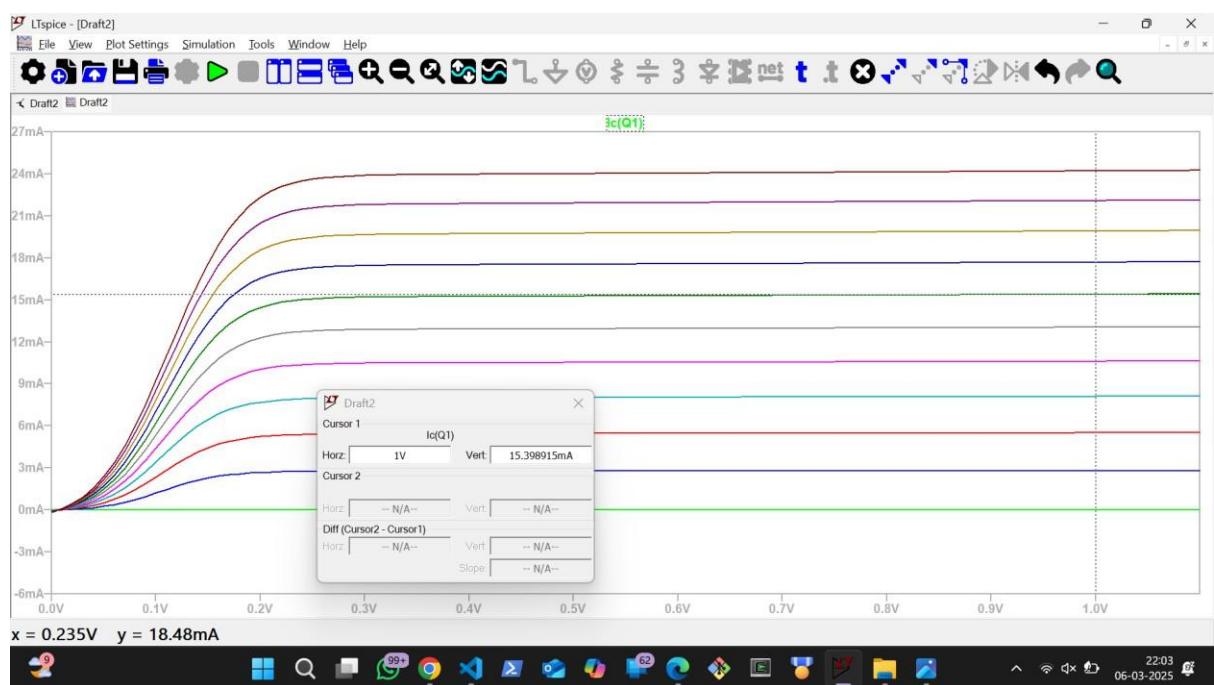
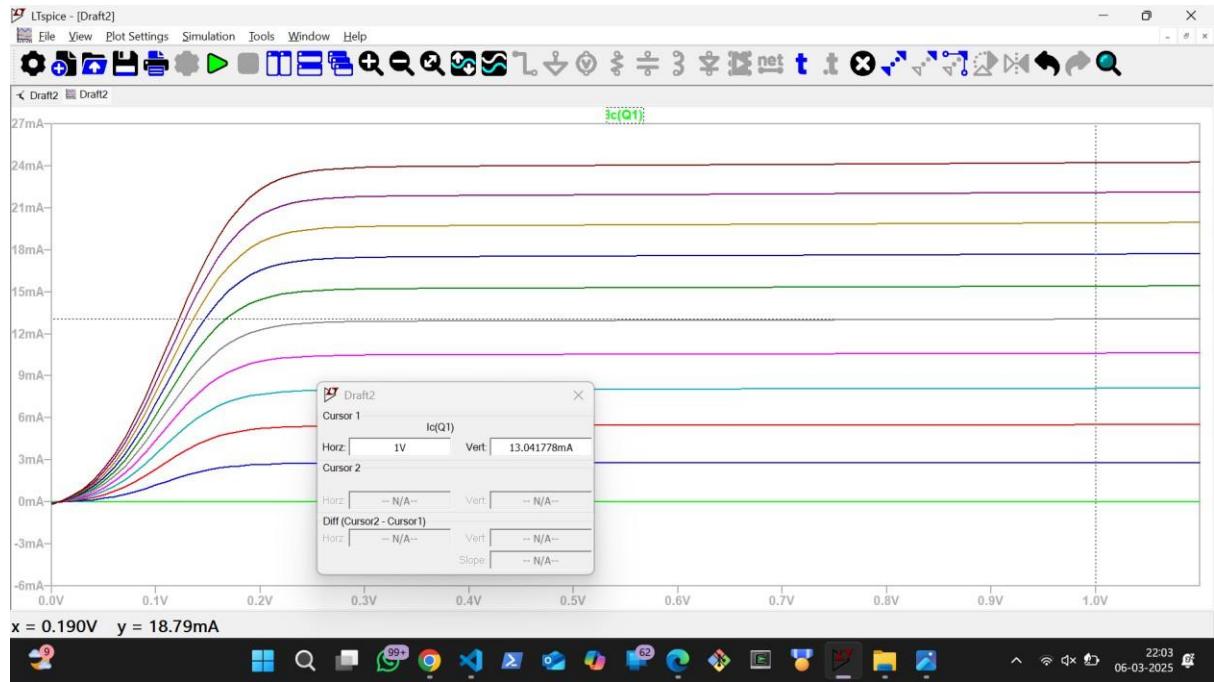
Below it is $I_C \sim 0$ and cutoff mode

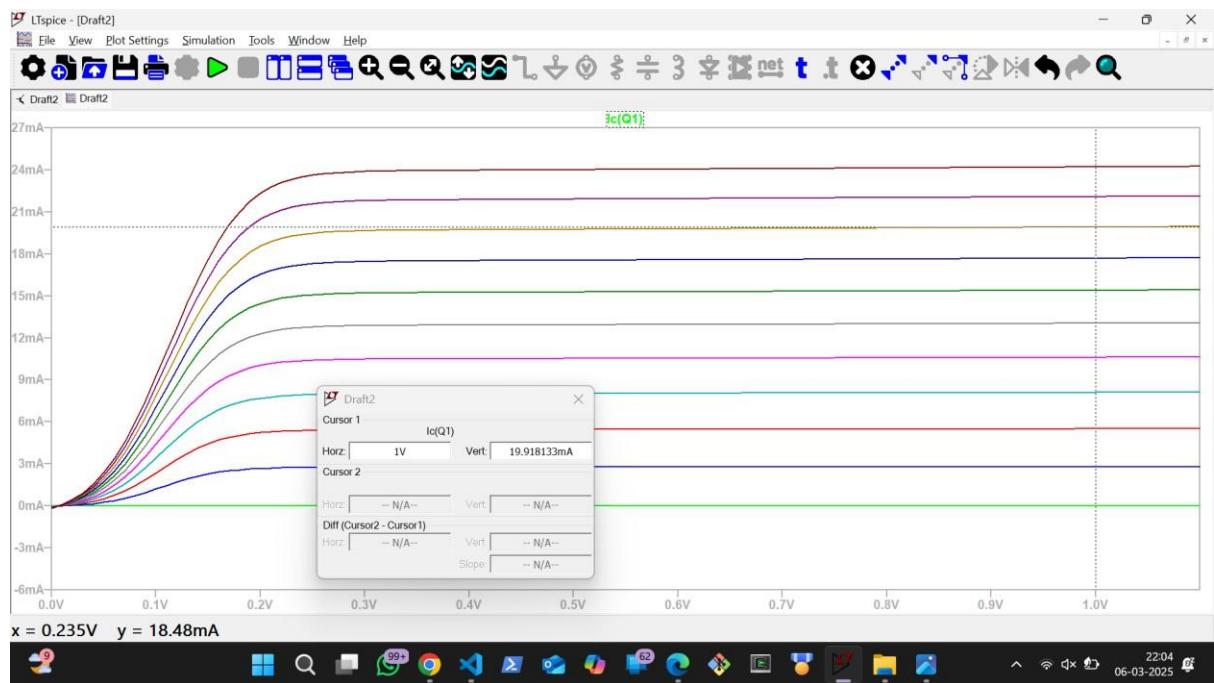
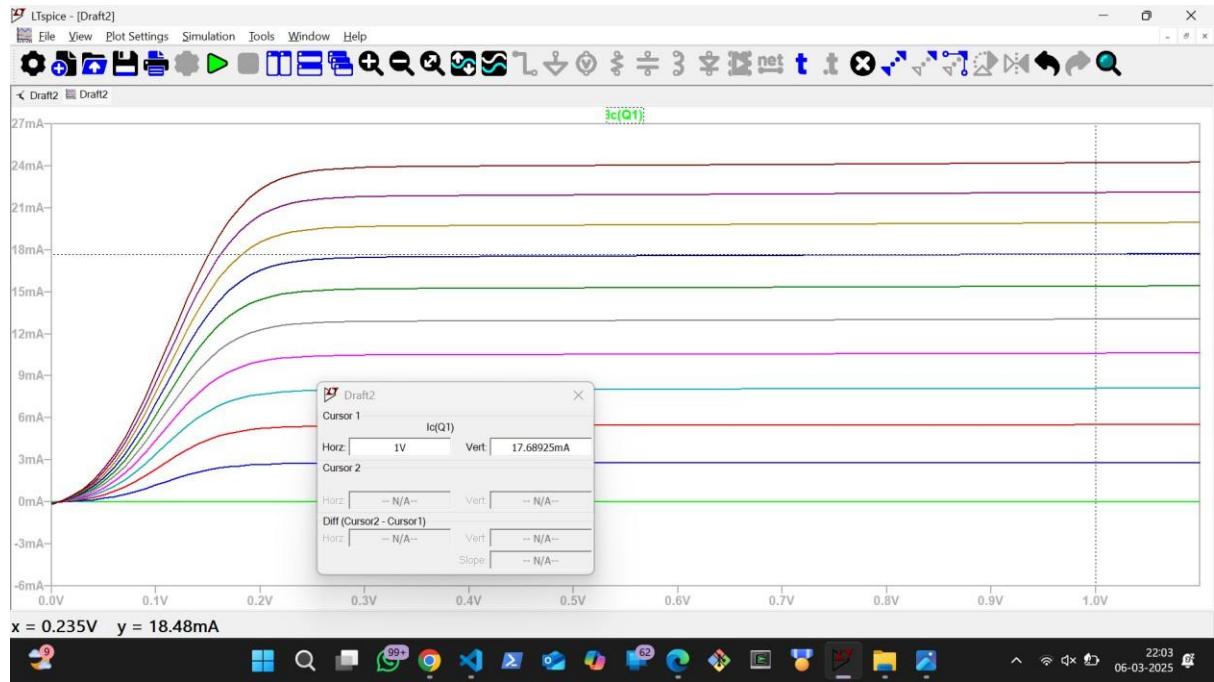
Tabulating β at 1V by I_C and I_B

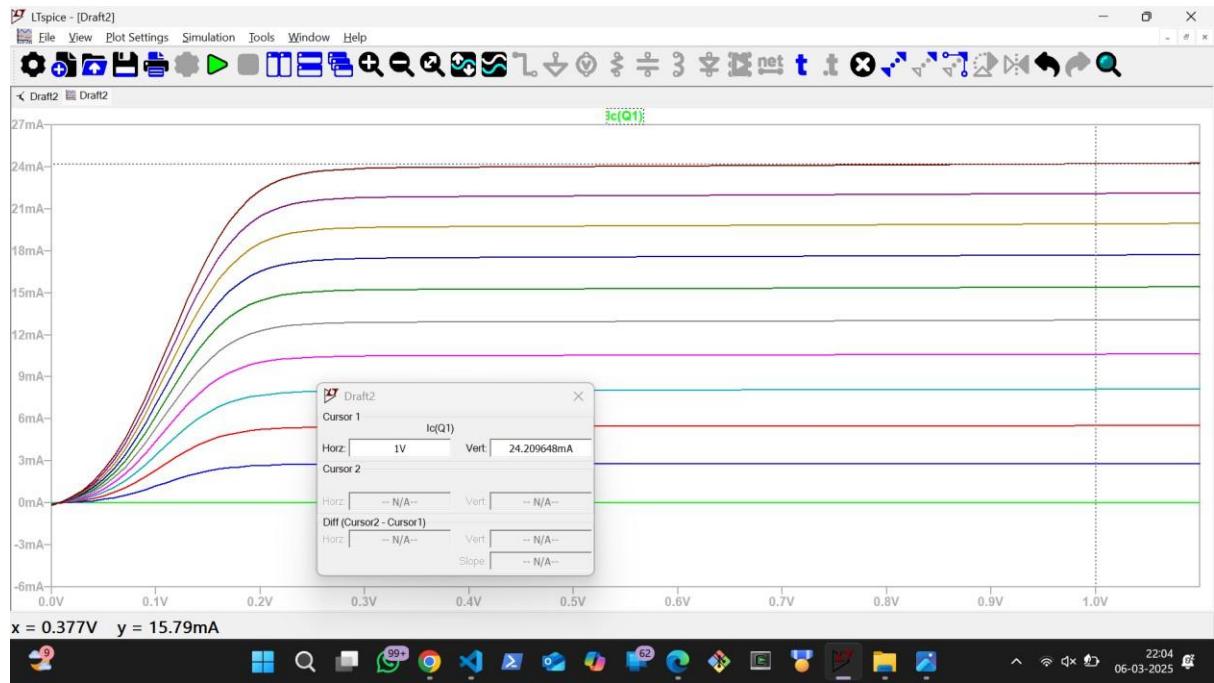
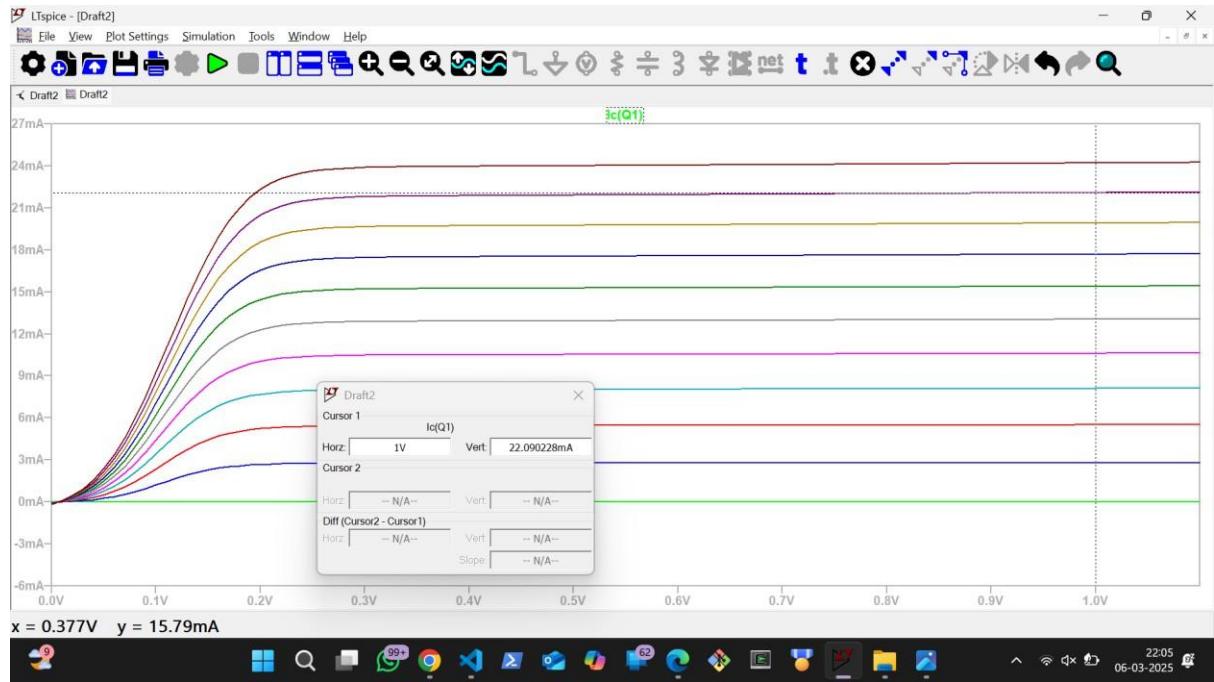












By these 11 values tabulated and calculated β

Early Voltage VA

VA is 60.47V

