

A - Information and Communication - 3

Q1)

$$x(t) = e^{-t/2} \cdot u(t) \quad \left| \begin{array}{l} \text{considering } u(t) \text{ as} \\ u(t) = \begin{cases} 1 & t \geq 0 \\ 0 & t < 0 \end{cases} \end{array} \right.$$

(a) $|X(\omega)|$

$$\text{w.r.t., } x(t) = e^{-t/2} \cdot u(t)$$

$$\text{and } X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

$$\Rightarrow X(\omega) = \int_0^{\infty} e^{-t/2 - j\omega t} \cdot u(t) dt$$

$$X(\omega) = \int_{-\infty}^0 e^{-t/2 - j\omega t} \cdot (0) dt + \int_0^{\infty} e^{-t/2 - j\omega t} dt$$

$$X(\omega) = \left[\frac{e^{-(1/2 + j\omega)t}}{-(1/2 + j\omega)} \right]_0^{\infty}$$

$$X(\omega) = \left[\frac{1}{-(1/2 + j\omega) \times \infty} \right] \xrightarrow{\text{bounded}} \frac{1}{1/2 + j\omega}$$

$$X(\omega) = \frac{2}{1 + 2j\omega}$$

$$X(\omega) = \frac{2}{1 + 2j\omega} \cdot \frac{(1 - 2j\omega)}{1 - 2j\omega}$$

$$X(\omega) = \frac{2 - 4j\omega}{1 + 4\omega^2}$$

$$X(\omega) = \frac{2}{1 + 4\omega^2} - j \frac{4\omega}{1 + 4\omega^2}$$

$$X(\omega) = \frac{Re\{X(\omega)\}}{2} + Im\{X(\omega)\}j$$

$$Re\{X(\omega)\} = \frac{2}{1 + 4\omega^2}, \quad Im\{X(\omega)\} = \frac{-4\omega}{1 + 4\omega^2}$$

$$|x(\omega)| = \sqrt{(\operatorname{Re}\{x(\omega)\})^2 + (\operatorname{Im}\{x(\omega)\})^2}$$

$$|x(\omega)| = \sqrt{\left(\frac{2}{1+4\omega^2}\right)^2 + \left(\frac{-4\omega}{1+4\omega^2}\right)^2}$$

$$|x(\omega)| = \sqrt{\frac{4 + 16\omega^2}{1 + 16\omega^2 + 8}} = \sqrt{\frac{4(1 + 4\omega^2)}{(1 + 4\omega^2)^2}}$$

$$|x(\omega)| = \frac{2}{\sqrt{1 + 4\omega^2}}$$

(b) $\angle x(\omega)$

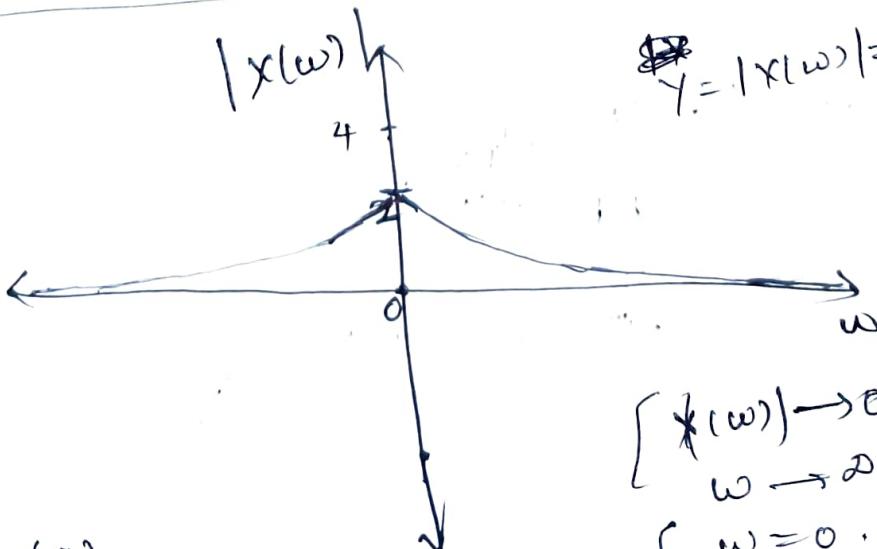
w.k.t,

$$\angle x(\omega) = \tan^{-1} \left(\frac{\operatorname{Im}\{x(\omega)\}}{\operatorname{Re}\{x(\omega)\}} \right) = \tan^{-1} \left(\frac{\frac{-4\omega}{1+4\omega^2}}{\frac{2}{1+4\omega^2}} \right)$$

$$\angle x(\omega) = \tan^{-1} \left(\frac{-4\omega}{2} \right) = \tan^{-1}(-2\omega)$$

$$(c) = \frac{2}{1 + 4\omega^2}$$

$$(d) = \bullet \frac{-4\omega}{1 + 4\omega^2}$$

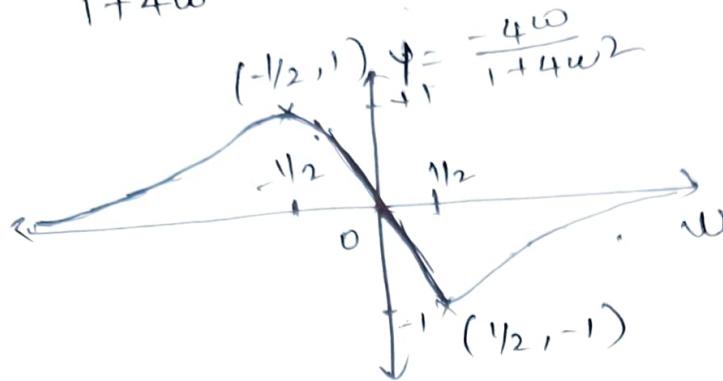


~~$$y = |x(\omega)| = \frac{2}{\sqrt{1 + 4\omega^2}}$$~~

$$\begin{aligned} & [x(\omega) \rightarrow 0] \\ & \omega \rightarrow \infty \\ \therefore & [x(\omega) = 0] \end{aligned}$$

(a)

$$(d) \frac{-4\omega}{1+4\omega^2} = y = T_m(x(\omega))$$



$$\frac{dy}{d\omega} = \frac{(1+4\omega^2)(-4) + (-4\omega)(8\omega)}{(1+4\omega^2)^2}$$

$$8\omega^2 = 1 + 4\omega^2$$

$$4\omega^2 = 1 \\ \omega^2 = \pm \frac{1}{2}$$

$$y = \frac{-4(1/2)}{1 + 4 \times \frac{1}{4}} \\ = \frac{-2}{2} = -1$$

$y = (+)$ minimum

after this

Then ~~decreases~~

Increases

$$\frac{2}{1 + 4 \times \frac{1}{4}} = \frac{2}{2} \\ y = 1$$

$y = +1$ (maximum)
after this

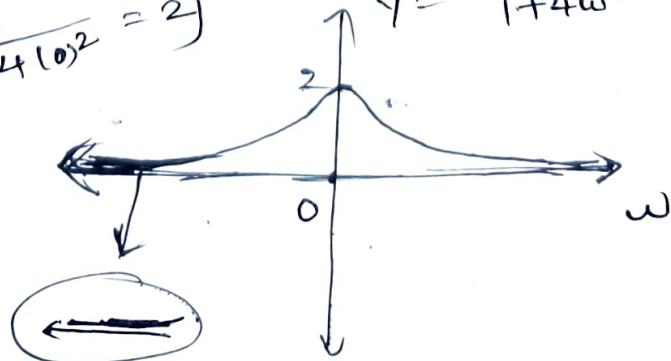
then decreases

$$(c) \operatorname{Re}(x(\omega))y < y = \frac{2}{1+4\omega^2}$$

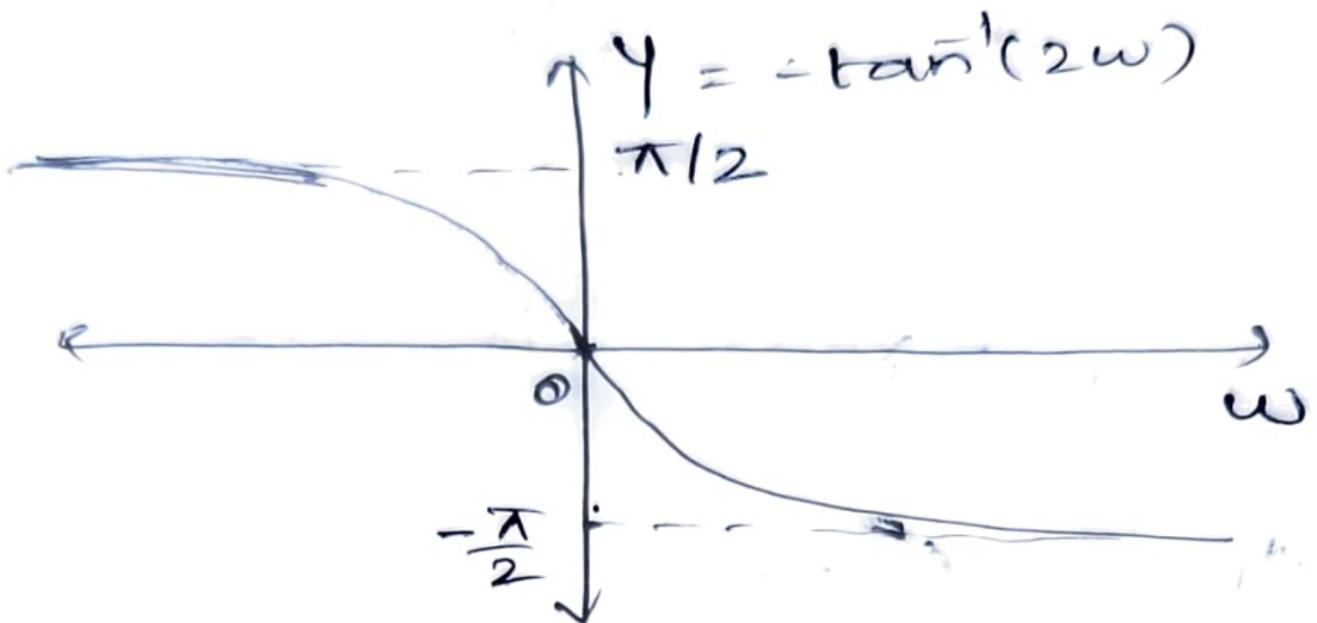
$$\left\{ \begin{array}{l} \omega=0 \Rightarrow y = \frac{2}{1+4(0)^2} = 2 \\ y=2 \end{array} \right.$$

$$\left[\begin{array}{l} \omega \rightarrow \infty \\ y \rightarrow 0 \end{array} \right. \therefore$$

$$y = \frac{2}{1+4\omega^2}$$

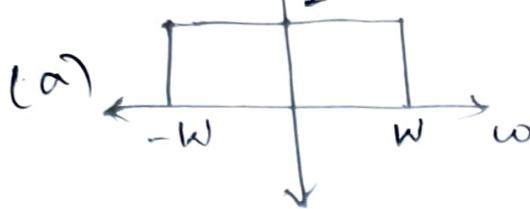


$$(b) \angle x(\omega) = y = \tan^{-1}(-2\omega) \doteq -\tan^{-1}(2\omega)$$

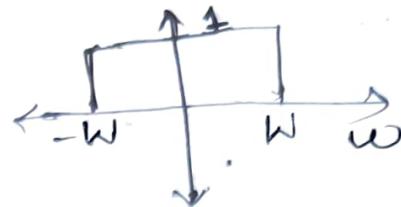


Given, $\operatorname{Re}\{x(\omega)\}$

2)



$\operatorname{Im}\{x(\omega)\}$



$$\operatorname{Re}\{x(\omega)\} = \begin{cases} 1 & -w < \omega < w \\ 0 & \text{other} \end{cases}$$

$$\operatorname{Im}\{x(\omega)\} = \begin{cases} 1 & -w < \omega < w \\ 0 & \text{other} \end{cases}$$

$$x(\omega) = \boxed{\text{?}} \quad \begin{cases} 1 + j\frac{1}{\omega} & -w < \omega < w \\ 0 & \text{other} \end{cases}$$

$$x(\omega) = \operatorname{Re}\{x(\omega)\} + j\operatorname{Im}\{x(\omega)\} \Rightarrow |x(\omega)| = \sqrt{\operatorname{Re}\{x(\omega)\}^2 + \operatorname{Im}\{x(\omega)\}^2}$$

$$|x(\omega)| = \sqrt{0^2 + 1^2} = \sqrt{\operatorname{Re}\{x(\omega)\}^2 + \operatorname{Im}\{x(\omega)\}^2}$$

$$|x(\omega)| = \begin{cases} \sqrt{2} & -w < \omega < w \\ 0 & \text{other} \end{cases}$$

$$\angle x(\omega) = \tan^{-1} \left(\frac{\operatorname{Im}\{x(\omega)\}}{\operatorname{Re}\{x(\omega)\}} \right)$$

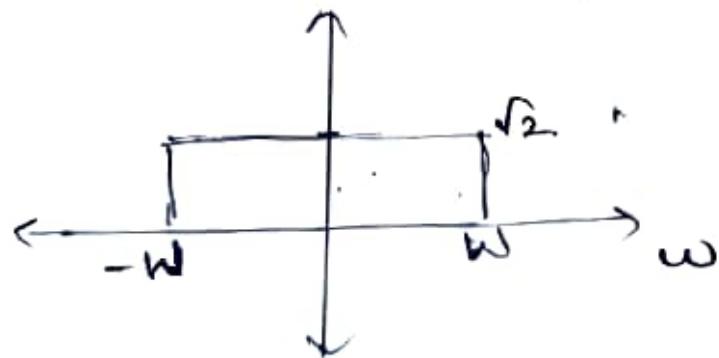
$$\angle x(\omega) = \tan^{-1} \left(\frac{1}{1} \right) = 45^\circ = \frac{\pi}{4}$$

$$\angle x(\omega) = \frac{\pi}{4} \quad (-w < \omega < w)$$

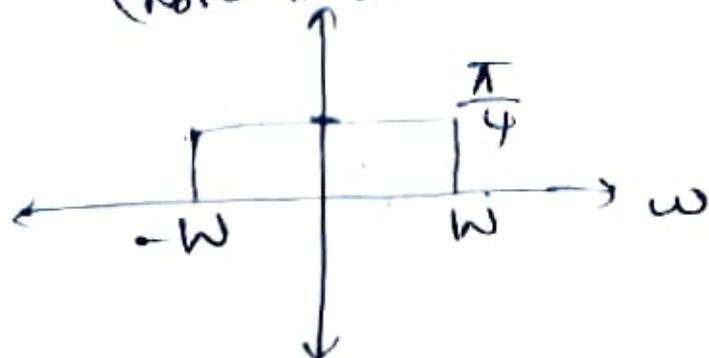
$$\angle x(\omega) = \boxed{\text{?}} \text{ undefined. (other } \omega \text{)}$$

Plots

$$y = |x(\omega)| = \begin{cases} \sqrt{2} & -\omega < \omega < \omega \\ 0 & \text{otherwise} \end{cases}$$



$$y = \angle x(\omega) = \begin{cases} \frac{\pi}{4} & -\omega < \omega < \omega \\ \text{Not defined} & \text{otherwise} \end{cases}$$



(b) By property of Fourier transform

For a real signal $x(t)$

It Fourier Transform must satisfy

$$X(-\omega) = X^*(\omega)$$

$$X(-\omega) = \begin{cases} 1 & -\pi < \omega < \pi \\ 0 & \text{Otherwise} \end{cases}$$

$$x^*(\omega) = \begin{cases} 1 & -W < \omega < W \\ 0 & \text{otherwise} \end{cases}$$

So,

No, $x(\omega)$ is not real, because

$$x^*(\omega) \neq x^*(-\omega)$$

④

$\mathcal{C}(n, k)$

(a)

let $c \in \mathcal{C}(n, k)$

If in general if $c \in \mathcal{C}(n, k)$

$$cH^T = 0.$$

but The received vector v may contain (include) error so,

received vector ' γ ' can be written as

$$\gamma = c + e$$

where c is codeword and e is the error pattern.

So, we might get some other (output) value instead of 0 for γH^T

$$\text{let, } s = \gamma H^T = (c + e) H^T = e H^T + 0$$

So, Instead of all 2^n codewords an $(n-k) \times n$ matrix is enough called H

The estimated code word for γ is

$$\gamma = c + e$$

$$\gamma + e = c + e + e$$

$$\hat{c} = \gamma + e = c \quad (\text{or}) \quad \hat{e} = \gamma - e = c$$

$$\gamma = c + e$$

$$\begin{aligned} \gamma H^T &= c H^T + e H^T \\ S &= \gamma H^T = e H^T + o \end{aligned} \quad \left. \begin{array}{l} \\ \end{array} \right\} \text{as written in} \\ &\quad \text{before page}$$

So, we can get e by multiplying γ with H^T . because we have equivalent table for $e, e H^T$

by this from the given table There's a corresponding ~~error~~ for errors occurred

So, The corresponding e for $e H^T$ is our required error.

Here we can save space because in standard array we need to store $(2^k) \cdot 2^{n-k} = 2^n$ elements but here 2^k is enough. here $k < n$ (k is no. of message bits and n is no. of message bits + parity)

(b) given $\gamma = [0, 0, 1, 1, 0, 1, 1]$

$$\gamma \cdot H^T = (c + e) H^T = e H^T$$

$$\Rightarrow [0, 0, 1, 1, 0, 1, 1] \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 1 & 1 & 1 \\ 1 & 0 & 1 & 1 \\ 1 & 1 & 0 & 1 \end{bmatrix}$$

$$\gamma \cdot H^T = [1, 1, 1, 1, 1]$$

$$xH^T = eH^T = [0101] \quad \begin{matrix} \text{given} \\ \text{from the table} \end{matrix}$$

The corresponding e will be $e = [0101000]$

So, The actual code word is

$$x = c + e$$

$$x + e = c + e + e \quad (\text{modulo 2 addition})$$

$$x + e = c$$

$$c = [0011011] + [0101000]$$

$$c = [0110011].$$

5(a) B-PSK Binary phase shift Keying.

Q-PSK Quadrature phase shift keying

(i)

Bpsk

QPSK

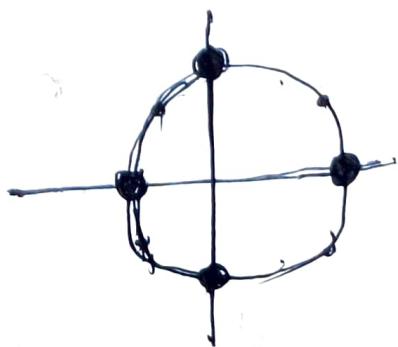
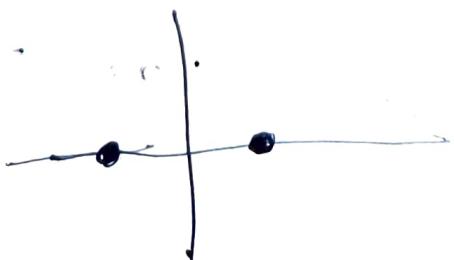
~~No of symbols~~ 2 bits per symbol

No of bits per symbol

1 bit per symbol

$$\Rightarrow 1 \Rightarrow \log_2^2$$

graph more info



$$\Rightarrow 2 \Rightarrow \log_2^4$$

$$\frac{360}{2} = 180^\circ, (\cancel{180^\circ})$$

$$\frac{360}{4} = 90^\circ, 180^\circ, 270^\circ, 360^\circ$$

(ii) 0° and 180°

(0) (1)

$$\Delta\phi = \frac{2\pi}{2} = 180^\circ$$

$$\Delta\phi = \frac{2\pi}{n}$$

$$\Delta\phi = \frac{2\pi}{4} = 90^\circ$$

→ $\Delta\phi$ is phase shift between neighbouring points. (in constellation)

(iii) Bandwidth efficiency.

as we know

BPSK transmits 1 bit per symbol

QPSK transmits 2 bits per symbol

For n -bit message transmission QPSK need only $\frac{n}{2}$ symbols whereas BPSK needs n symbols.

So, In QPSK more information is packed into the same time interval compared to BPSK.
 → higher symbol rate → more rapid changes → wider bandwidth
 each symbol change in time creates a change in the waveform → these changes determine frequency content of the signal.

here QPSK has [more bit rate / less symbol rate] compared to BPSK
 → lower symbol rate narrower band width.

and also

Bandwidth efficiency $\eta = \frac{\text{bits per symbol}}{\text{Symbol duration}}$

$$\eta_{BPSK} = \frac{1}{2} \cdot \eta_{QPSK}$$

because, QPSK is more bandwidth efficient than BPSK because, QPSK uses half the bandwidth of BPSK

- 5(a)
- (iv) Susceptibility to noise and 5(b)
generally as we know
- Bpsk uses only 2 points on constellation
(0° and 180°)
- These are far apart in phase
- So even if noise disturbs a single bit
it's unlikely to be confused for the
wrong bit
- Bpsk is like a Yes/No signal with a
large gap - very easy to distinguish
and worst case corrupted (by high noise)
only 1 bit is corrupted
- but in Qpsk 2 bits could be corrupted
instead of 1 and also more likely
to corrupted and unlike to distinguish
where the (noise) error is ^{when} compared to Bpsk.
- Let's see how
- Qpsk uses 4 points each representing
2 bits, ^{also} placed very closer (90° apart)
since these points are closer in phase
a small amount of noise might push
the signal to the wrong symbol.

The symbol Error rate for QPSK is slightly more ~~more~~.

QPSK is slightly more ^(susceptible) vulnerable to noise. Compare to BPSK.

The larger distance b/w the points, the less susceptible the system is to noise.

In QPSK the small amount of noise could cause the received symbol to shift into the wrong quadrant, leading to higher probability error (closer spacing of constellation points).

5 (b) If both modulation schemes are operating under the same bandwidth and power conditions.

Some theory already written in Susceptibility to noise that also follow this.

Similarly BPSK uses only 2 phases minimum distance is $2A$

$$\text{for QPSK } d_{\min} = A\sqrt{2}$$

QPSK is more vulnerable to noise. hence more BER error rate compared to BPSK at same power and bandwidth. The QPSK may have higher efficiency of bandwidth because it can pack more bits per symbol and BPSK is more noise resistant due to large symbol spacing.

So, under same power and bandwidth BPSK has a lower BER because its effective signal to noise ratio (SNR) per bit is higher.

6)

$$b(t) \in \{0, 1\}$$

$$\text{carrier wave} = \cos(2\pi f_c t)$$

f_c is the carrier frequency

For bpsk

let

$$b(t)=0$$

phase diff
should be there

$$\text{Phase shift } \phi(b(t))=0$$

$$b(t)=1$$

$$\text{Phase shift } \phi(b(t))=\pi$$

Let

$$x(t) = A \cdot \cos(2\pi f_c t + \phi(b(t)))$$

Let $A=1$, since carrier wave has ~~amplitude~~

$$A=1,$$

$$x(t) = A \cdot \cos(2\pi f_c t + \pi \cdot b(t))$$

so, when $b(t)=0$ $x(t) = A \cdot \cos(2\pi f_c t \cdot \pi \cdot 0)$

$$x(t) = A \cdot \cos(2\pi f_c t)$$

$$x(t) = \cos(2\pi f_c t)$$

$$\underline{b(t)=1}$$

$$x(t) = A \cdot \cos(2\pi f_c t + \pi)$$

$$= -A \cos(2\pi f_c t)$$

$$x(t) = -\cos(2\pi f_c t)$$

This is how BPSK modulates.

given binary sequence [1, 0, 1, 1, 0]

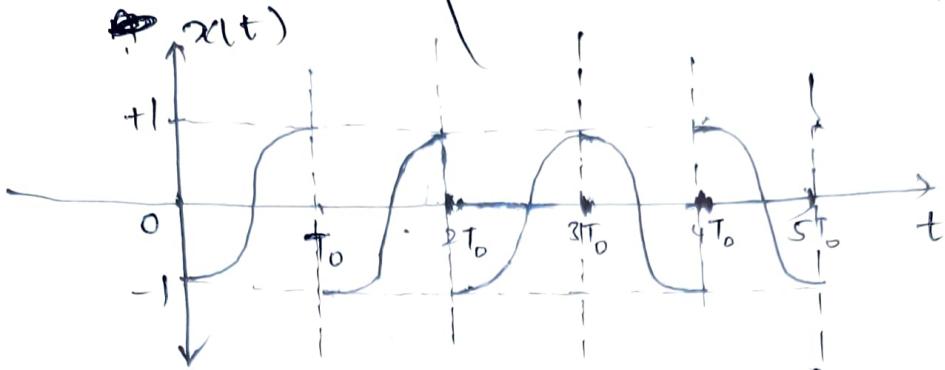
x-axis divided into 5-equal intervals $T_b = \Delta t$

y-axis ranging (-1, 0, +1)

at $t=0$ to T_b (taking complete coswave)

$x(t)$ \searrow considering 1st bit

taking $x(t) = \{ \cos(2\pi f_c t + \pi(bct)) \}$



Phase change $180^\circ \rightarrow 0^\circ \rightarrow 180^\circ \rightarrow 180^\circ \rightarrow 0^\circ$

$$b(t) = (1), (0), (1), (1), (0)$$

7. given $m(t) = 5 \cos(2\pi \cdot 1000t)$

$c(t) = 10 \cos(2\pi \cdot 100000t)$

$f_m = 1000 \text{ Hz}$ The message modulates in I-component of signal

modulated signal $= x(t) = m(t) \cdot c(t)$ $\boxed{\cos A \cos B = \cos(A+B) + \cos(A-B)}$

$$x(t) = 5 \cos(2\pi \cdot 1000t) \cdot 10 \cos(2\pi \cdot 100000t)$$

$$v_{PSB}(t) = x(t) = \frac{50}{2} \times 2 \cos(2\pi \cdot 1000t) \cos(2\pi \cdot 100000t)$$

$$r_a(t) = 25 \times (\cos(2\pi \cdot t(101000)) + \cos(2\pi \cdot t(99000)))$$

$$m(t) = 25 [\cos(2\pi \cdot 101000t) + \cos(2\pi \cdot 99000t)]$$

In DSBSC modulation the modulated signal has 2 sidebands.

upper sideband (USB): centered at $f_c + f_m$

lower side band (LSB): centered at $f_c - f_m$

(b)

(B) Bandwidth $= 2f_m = 2 B_{\text{message}}$

$$BW = 2000 \text{ Hz}$$

f_m is the highest frequency component msg signal.

(c) The frequency spectrum of modulated signal is

- There are 2nd cos signals in $v_{DSB}(t)$
each cos signal gives 2 frequencies give & -ve in Fourier transform S(term)
- The fourier transform of them
- each term(cosine) represents single frequency in spectrum

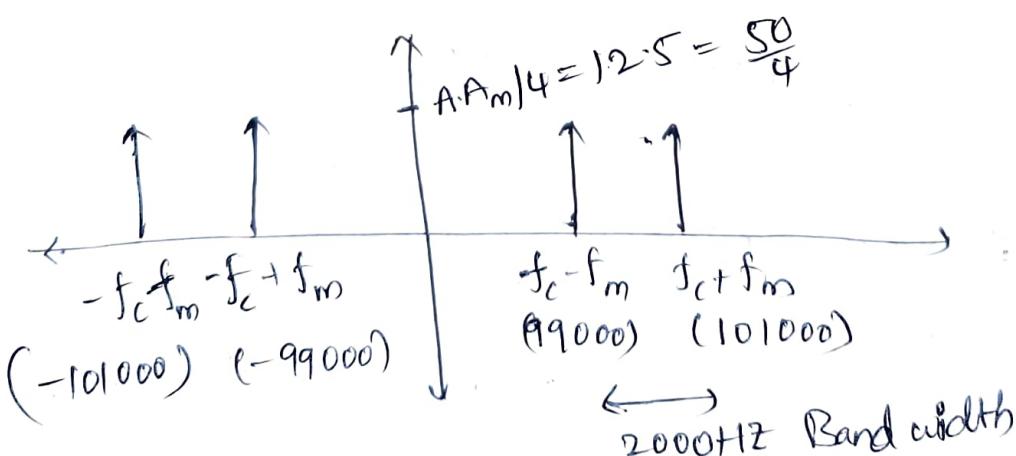
$$v_{DSB}(f) = \int_{-\infty}^{\infty} v_{DSB}(t) dt$$

$$v_{DSB}(f) = \int_{-\infty}^{\infty} 25 \left(e^{+2\pi 101000t - st} + \frac{e^{-2\pi 101000t + st}}{2} \right) dt$$

$$+ \int_{-\infty}^{\infty} \frac{25}{2} \left[e^{2\pi 99000t - st} + e^{-2\pi 99000t + st} \right] dt$$

$$v_{DSB}(f) = 12.5 \left[\delta(f - 101,000) + \delta(f + 101,000) \right]$$

$$+ 12.5 \left[\delta(f - 99,000) + \delta(f + 99,000) \right]$$



- The frequency Spectrum of $v_{DSB}(t)$ is a plot of amplitude vs frequencies
- real signal spectrum is symmetric about f_c
- The carrier frequency at $f_c = 100\text{kHz}$ is suppressed

→ no component at f_c , which is characteristic of DSB-SC

8) $s(t) = 4 \cos(2\pi \cdot 10^6 t) \cdot \cos(2\pi \cdot 10^3 t)$

(a)

WKT, $2\cos A \cos B = \cos(A+B) + \cos(A-B)$

$$s(t) = 2 \left[\cos 2\pi(10^6 + 10^3)t + \cos 2\pi(10^6 - 10^3)t \right]$$

$$s(t) = 2 \left[\cos 2\pi(1001000)t + \cos 2\pi(999000)t \right]$$

$$f_c + f_m = 1001000 \text{ Hz}$$

$$f_c - f_m = 999000 \text{ Hz}$$

by this $f_c = 10^6 \text{ Hz} = 1 \text{ MHz}$

$$f_m = 10^3 = 1 \text{ kHz}$$

(b)

$$(BW) \text{ Bandwidth} = 2 \cdot f_m = 2 \cdot B_{\text{message}}$$

$$= 2 \cdot 10^3$$

$$BW = 2 \text{ kHz}$$

f_m is highest freq component in msg signal.

③ wKT, In modulation
(a)

The modulation property

$$x(t) \cdot \cos(\omega_0 t) \xrightarrow{\mathcal{F}} \frac{1}{2} [X(\omega + \omega_0) + X(\omega - \omega_0)]$$

$X(f)$ ps Fourier transform of $x(t)$

~~1~~ $\mathcal{F} \{ x(t) \cdot \cos(2\pi f_0 t) \}$

$$x(t) \left(\frac{e^{2\pi j f_0 t} + e^{-2\pi j f_0 t}}{2} \right)$$

$$\frac{x(t) \cdot e^{2\pi j f_0 t}}{2} + \frac{x(t) e^{-2\pi j f_0 t}}{2}$$

$$x(t) \xrightarrow{\mathcal{F}} X(f)$$

\therefore Similarly, $x(t) \cdot e^{j2\pi f_0 t} \xrightarrow{\mathcal{F}} X(f - f_0)$
 $x(t) \cdot e^{j2\pi f_0 t} \xrightarrow{\mathcal{F}} X(f + f_0)$

$$\Rightarrow \frac{x(f-f_0)}{2} + \frac{x(f+f_0)}{2}$$

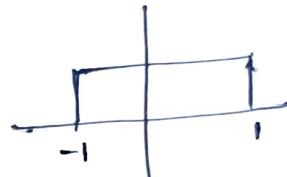
Fourier transform of the given signal

→ The modulation has made a baseband to passband signal.

without changing the bandwidth

→ made copies of the original signal i.e. at both $+f_0$ and $-f_0$ frequencies

$$(b) x(t) = \text{rect}(t/2)$$

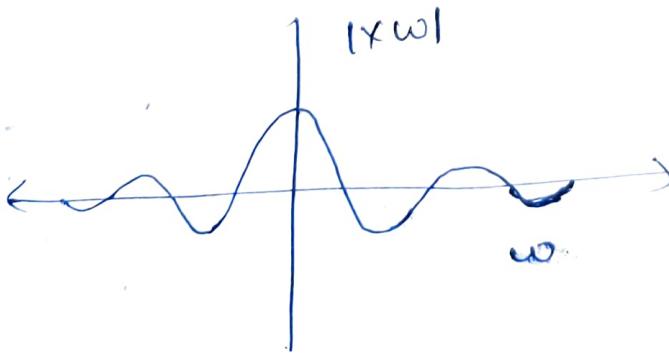


$$X(\omega) = \int_{-\infty}^{\infty} x(t) e^{-j\omega t} dt$$

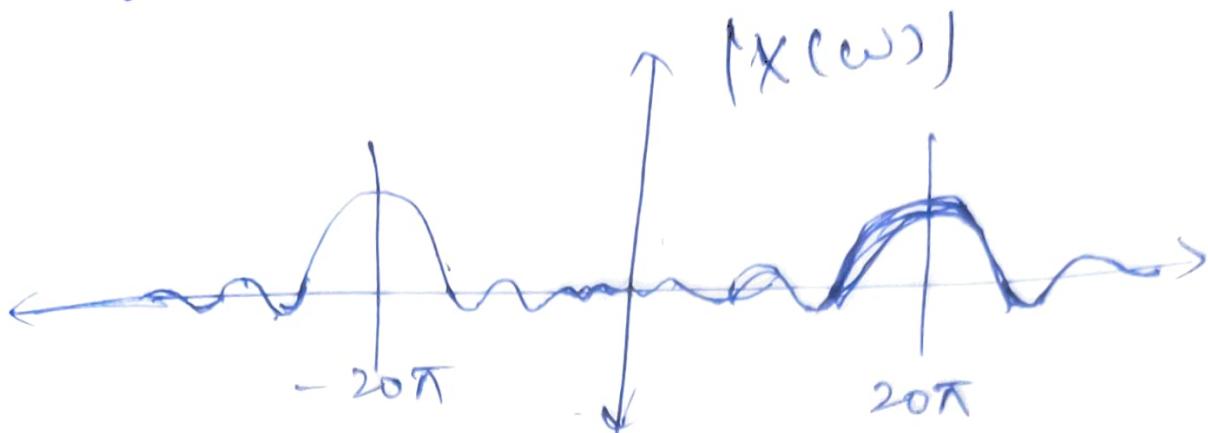
$$= \int_{-1}^{1} e^{-j\omega_0 t} dt$$

$$X(\omega) = \left[\frac{e^{-j\omega_0 t}}{-j\omega_0} \right]_{-1}^{1} = \frac{e^{-j\omega_0} - e^{j\omega_0}}{-j\omega_0}$$

$$X(\omega) = \frac{2j \sin \omega}{j\omega} = \frac{2 \sin \omega}{\omega}$$



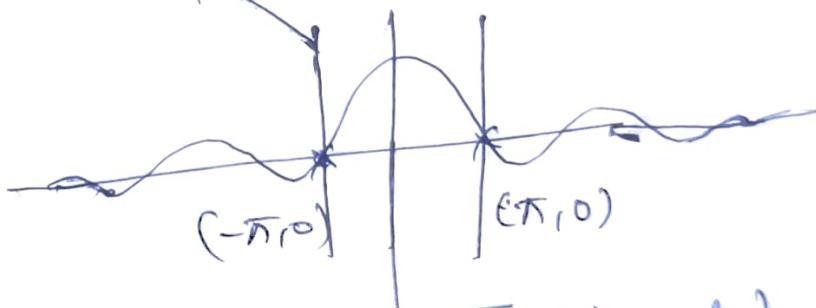
By (a) Part fft of $x(t)\cos(20\pi t)$ is



$$\frac{\sin(20\pi - \omega)}{20\pi - \omega} + \frac{-\sin(20\pi + \omega)}{20\pi + \omega}$$

The signal is never 0 it only decays its fft bandwidth is infinite

The maximum energy concentration is in $(-\pi, \pi)$ region taking π as bandwidth



Taking this as bandwidth π (input)

Now, band width of signal $x(t)\cos(20\pi t)$ becomes twice hence 2π .