

ANALOG ELECTRONIC CIRCUITS

LAB REPORT-3

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Full Wave Rectifiers

1) TRANSFORMER CHARACTERISATION:

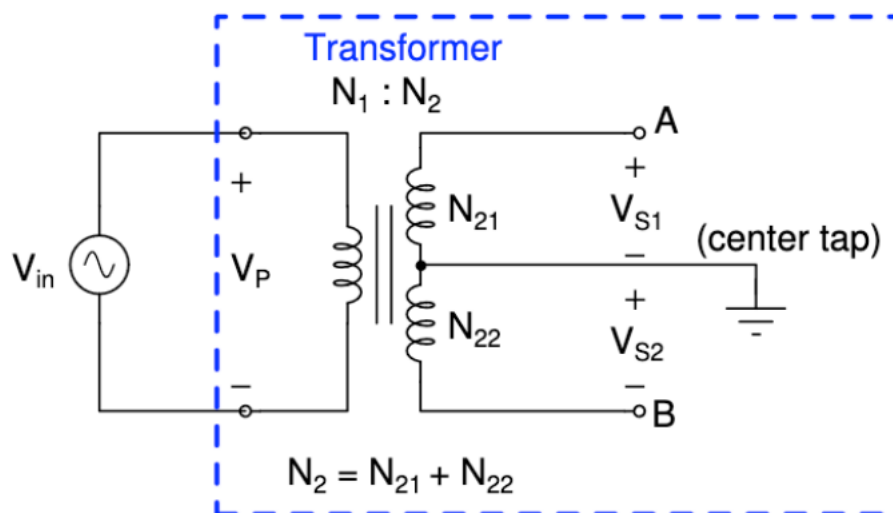


Figure 1: Bridge Rectifier

a)

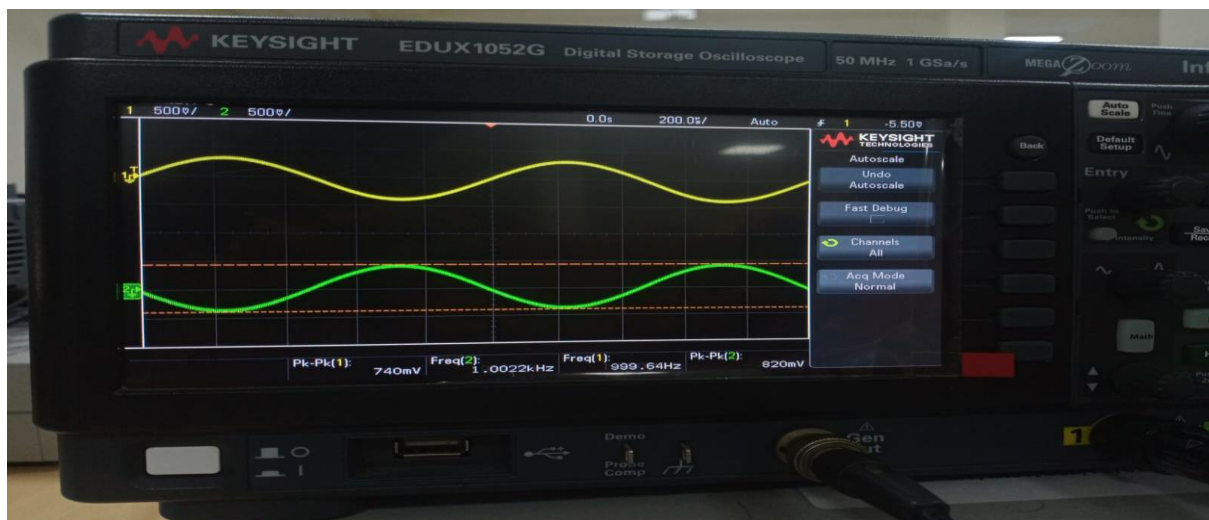
INPUT:

$V_{in} = 12V_{pp}$

Frequency = 1k Hz

OUTPUT:

We can conclude that from figure:



	Amplitude	Frequency	Phase
Va	460 mV	1k Hz	0 deg
Vb	420 mV	1k Hz	182.91 deg

b)

From the plot of VA and VB obtained:

Amplitude of VA : $(V_{pp})_2 = 830\text{mV} = V_{S1}$

Amplitude of VB : $(V_{pp})_1 = 830\text{mV} = V_{S2}$

Frequency of VA = Frequency of VB = 1000kHz

Phase Difference between VA and VB is 180 degrees.

Magnitude of Input $V_{in} = 12$ (Vpp)

Magnitude of final output $V_{out} = |V_A - V_B| = |V_{S1} + V_{S2}|$

$$= 830 + 830$$

$$= 1660\text{mV}$$

$$= 1.66\text{V}$$

The output voltage $V_{AB} = 1.6\text{V} \ll$ input Voltage $V_{in} = 12\text{Vpp}$ This drop in the output as compared to the input is because of the transformer with $N_1:N_2$ to be the transformed ratio.

$$N_1:N_2 = V_{in} : V_{AB}$$

$$= 12.4/1.66$$

$$= 7.469$$

$$= V_{\text{primary}} : V_{\text{secondary}}$$

Actually the input peak-peak voltage was set to be 12 Vpp but the observed output have $V_{pp} = 12.4$ due to some calibration error or non linearity in the output generated by the DSO.

So 12.4 output was considered while calculating the transformer ratio $N_1:N_2$.

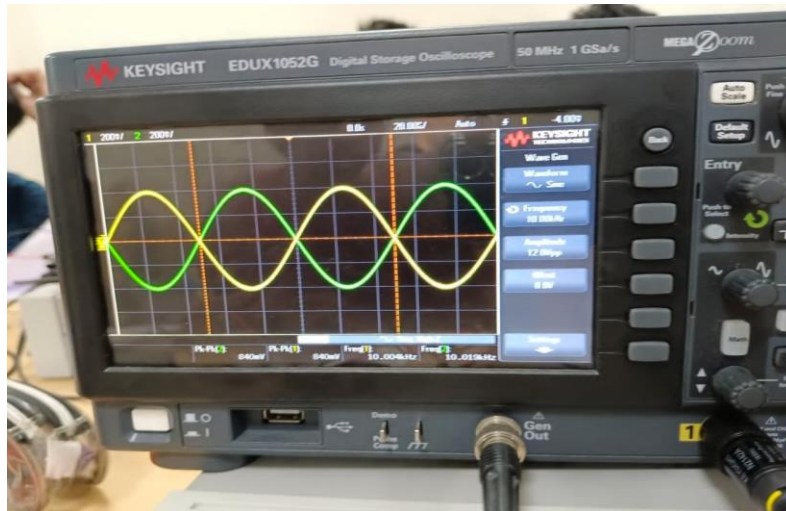
since $N_1:N_2 > 1$ so the given transformed is a STEP DOWN transformer.

c)

Variation in output as the input frequency changes:

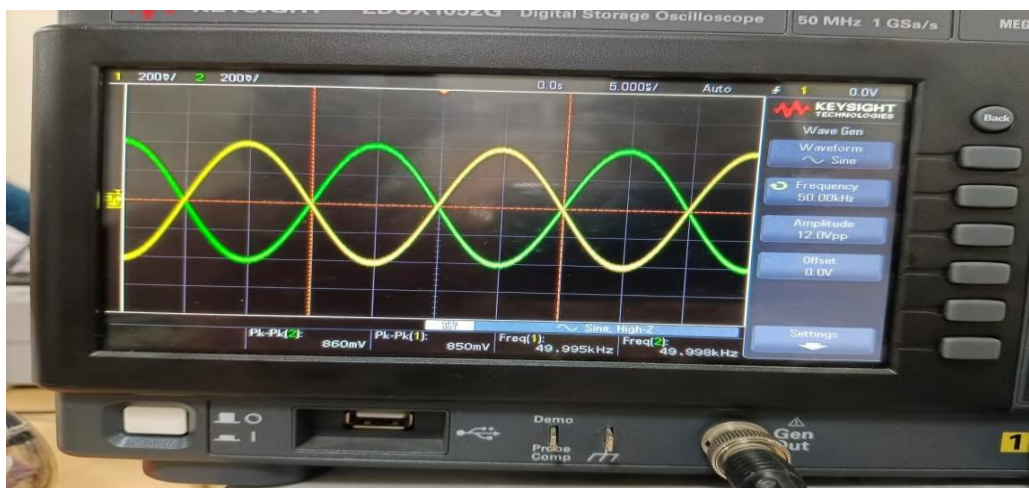
Case1: $f=10\text{ kHz}$

$V_A=840\text{ mV}$ and $V_B=840\text{mV}$ with the phase difference to be 180 degrees.



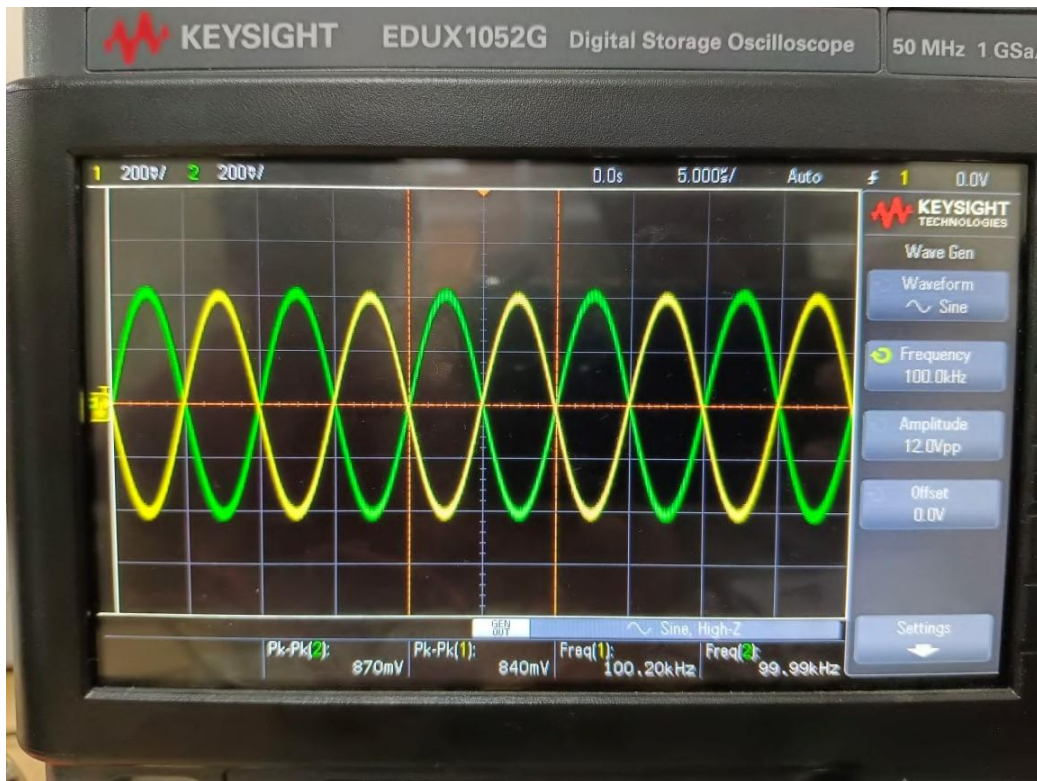
Case2: $f=50\text{ kHz}$

$V_A=860\text{ mV}$ and $V_B=850\text{mV}$, phase difference= 180 degree .



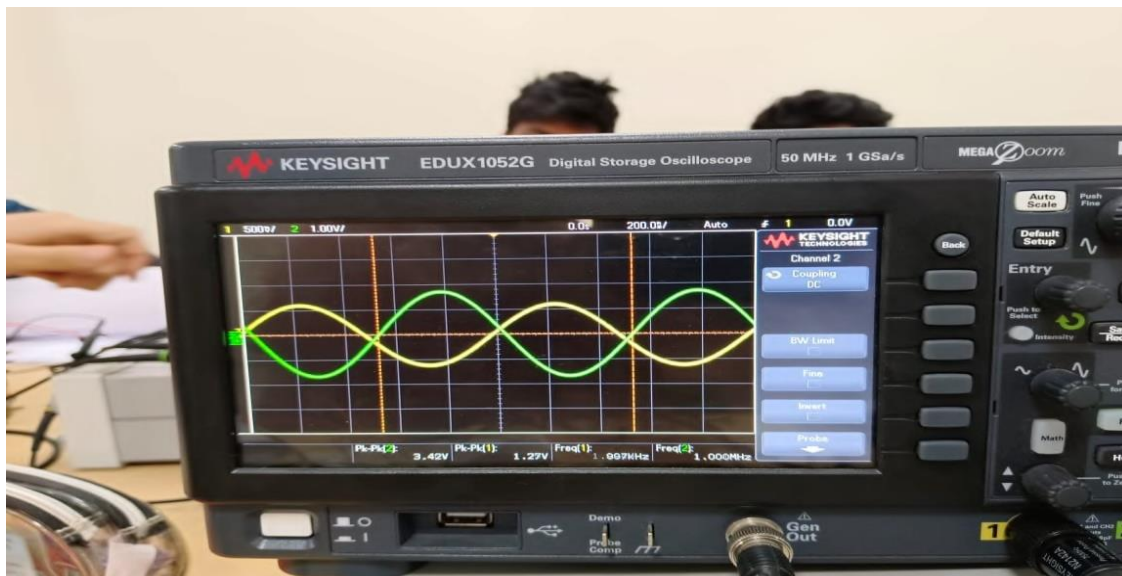
Case3: $f=100\text{ kHz}$

$V_A=870\text{ mV}$ and $V_B=850\text{mV}$, phase difference= 180 degree.



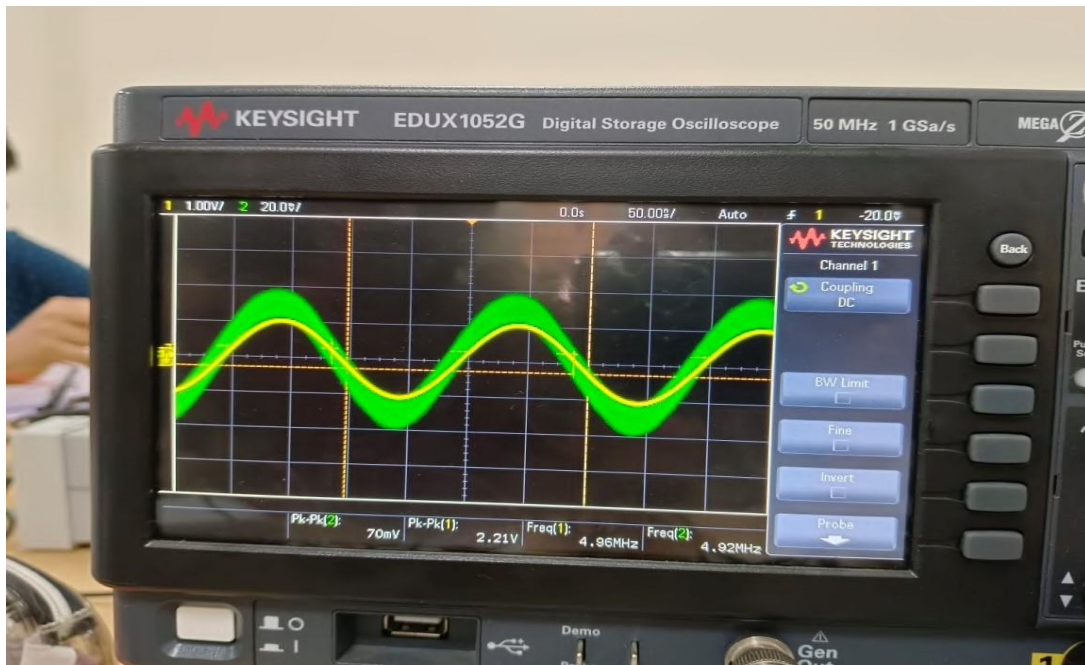
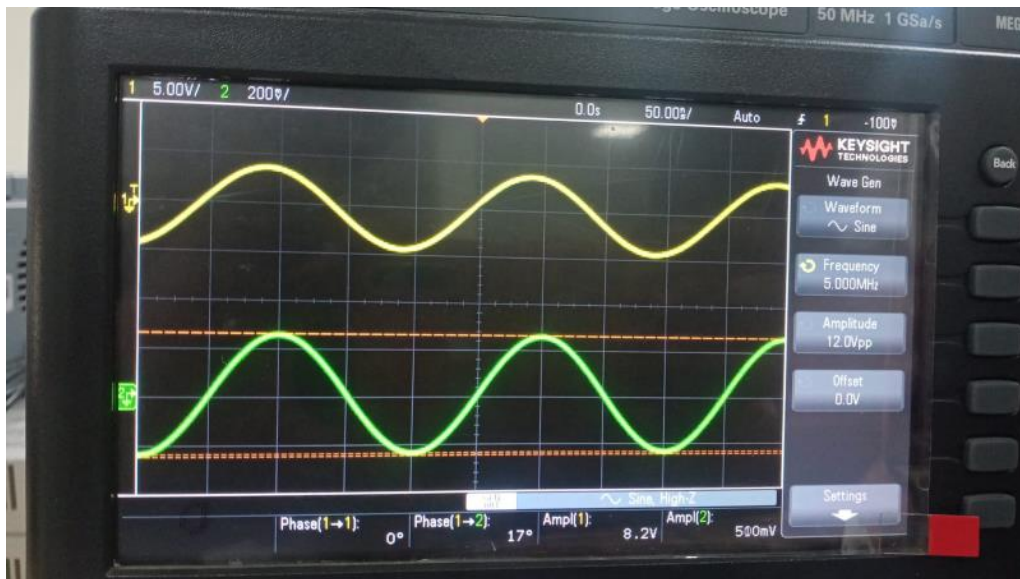
Case4: $f=1\text{MHz}$

$V_A=3.42\text{ V}$ and $V_B=1.27\text{ V}$, phase difference < 180 degree.



Case5: $f=5\text{MHz}$

$V_A=70\text{mV}$ and $V_B=2.21\text{ V}$, phase difference close to 0 degree.



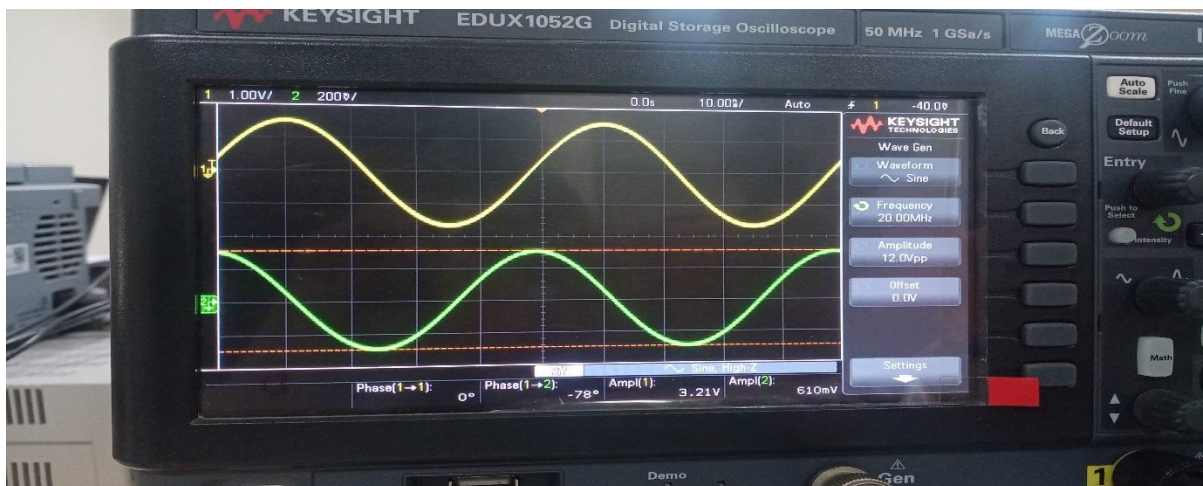
Case6: $f=10\text{MHz}$

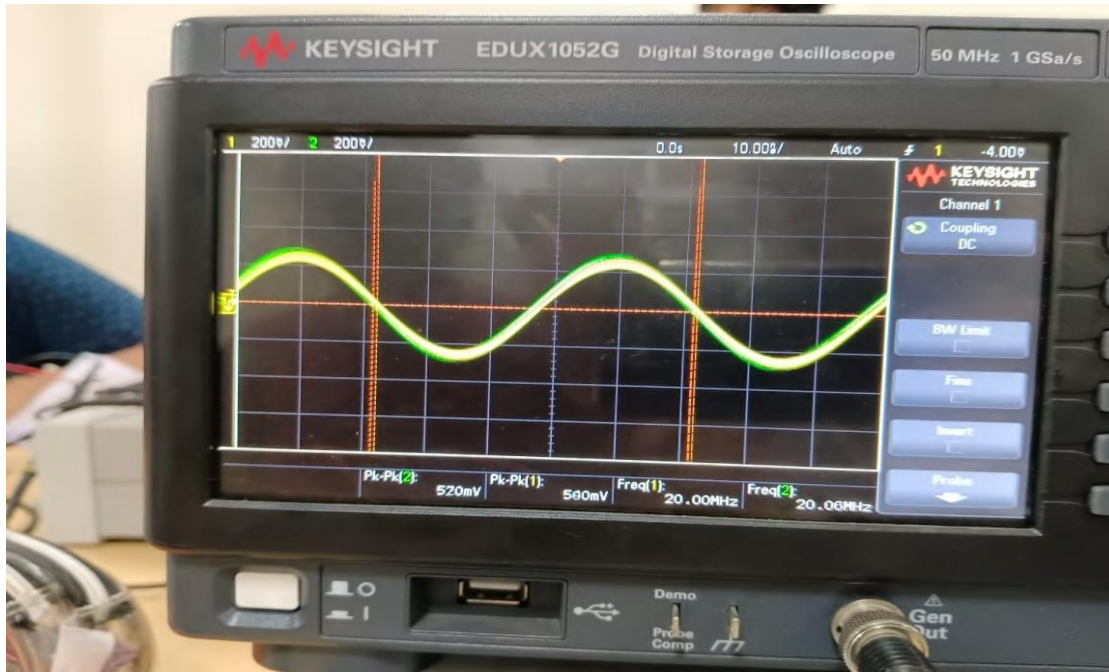
$V_A=680\text{mV}$ and $V_B=410\text{mV}$, phase difference close to 180 degree.



Case7: $f=20\text{M Hz}$

$V_A=520\text{mV}$ and $V_B=510\text{mV}$, phase difference close to 0 degree.





Tabular column containing the following values:

V in (frequency)	Va (Vpp)	Vb(vpp)
10k Hz	840 mV	840 mV
50k Hz	860 mV	850 mV
100k Hz	870 mV	850 mV
1M Hz	3.42 V	1.27 V
5M Hz	70 mV	2.21 V
10M Hz	680 mV	410 mV
20M Hz	520 mV	510 mV

d)

As we observed from above table, we can conclude that:

The magnitude of V_a increased first and we observe sudden drop in V_a and then slight Increase.

The probe wire could be acting like a low pass filter only allowing low frequency inputs to pass through it and attenuating the high frequency inputs.

Every cable has a specific impedance, which is the resistance to the flow of alternating current.

At higher frequencies, the impedance of the cable rises, resulting in signal attenuation or reduction in the signal amplitude.

The limited bandwidth of the input cable could also contribute to the reduction in amplitude with an increase in frequency.

The bandwidth of a cable is the range of frequencies that can pass through the cable with minimal attenuation.

If the input cable's bandwidth is limited, it can cause attenuation at higher frequencies, leading to a reduction in amplitude.

Repeating the experiment by plotting VA in channel 1 and Vp(V input) in channel 2 :

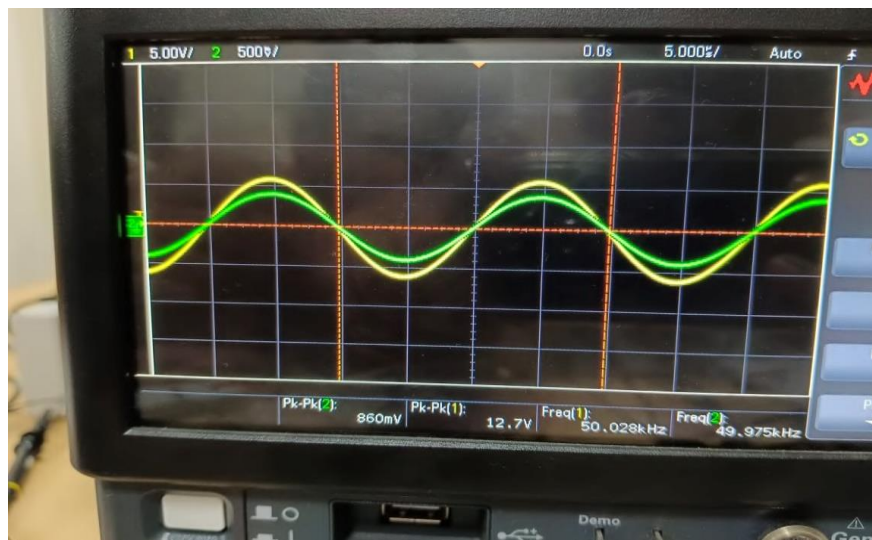
Case1: $f=10\text{kHz}$

$V_A=840\text{ mV}$ and $V_p=12.3\text{V}$ with the phase difference to be 0 degrees.



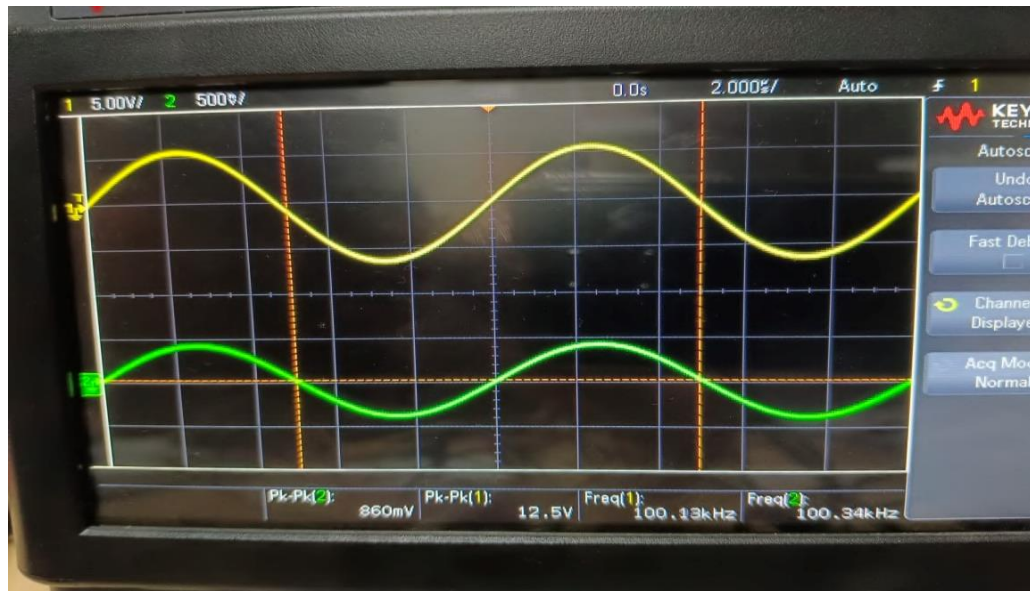
Case2: $f=50\text{kHz}$

$V_A=860\text{ mV}$ and $V_p=12.7\text{V}$ with the phase difference to be 0 degrees.



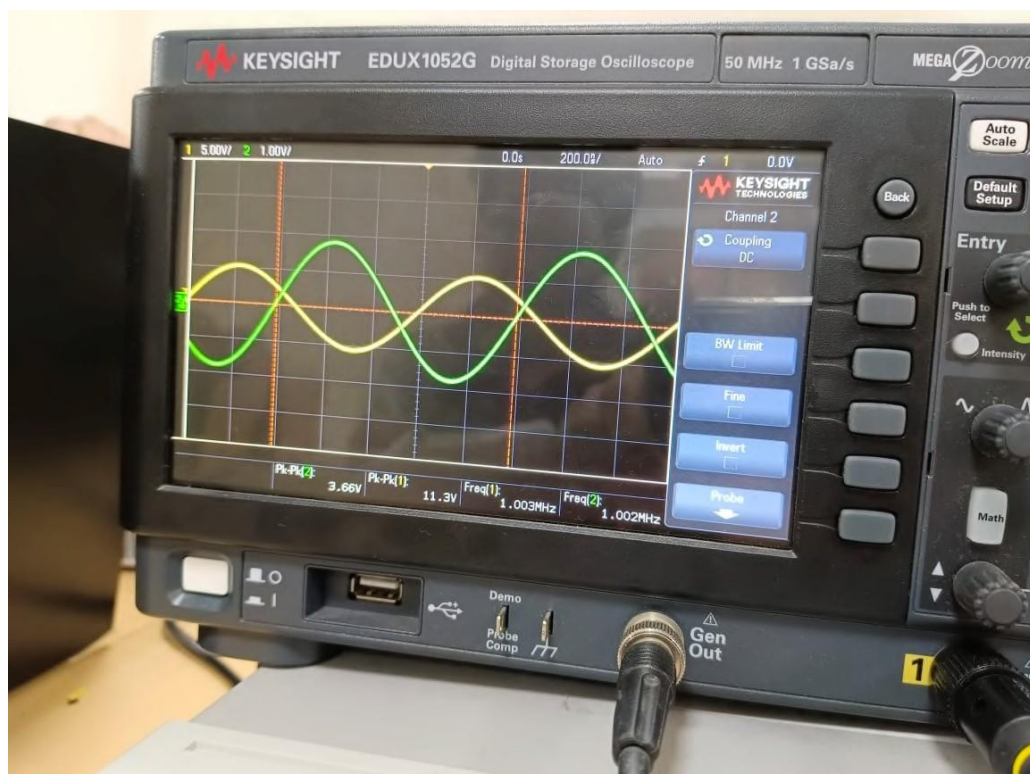
Case3: $f=100\text{kHz}$

$V_A=860\text{ mV}$ and $V_p=12.5\text{V}$ with the phase difference to be 0 degrees.



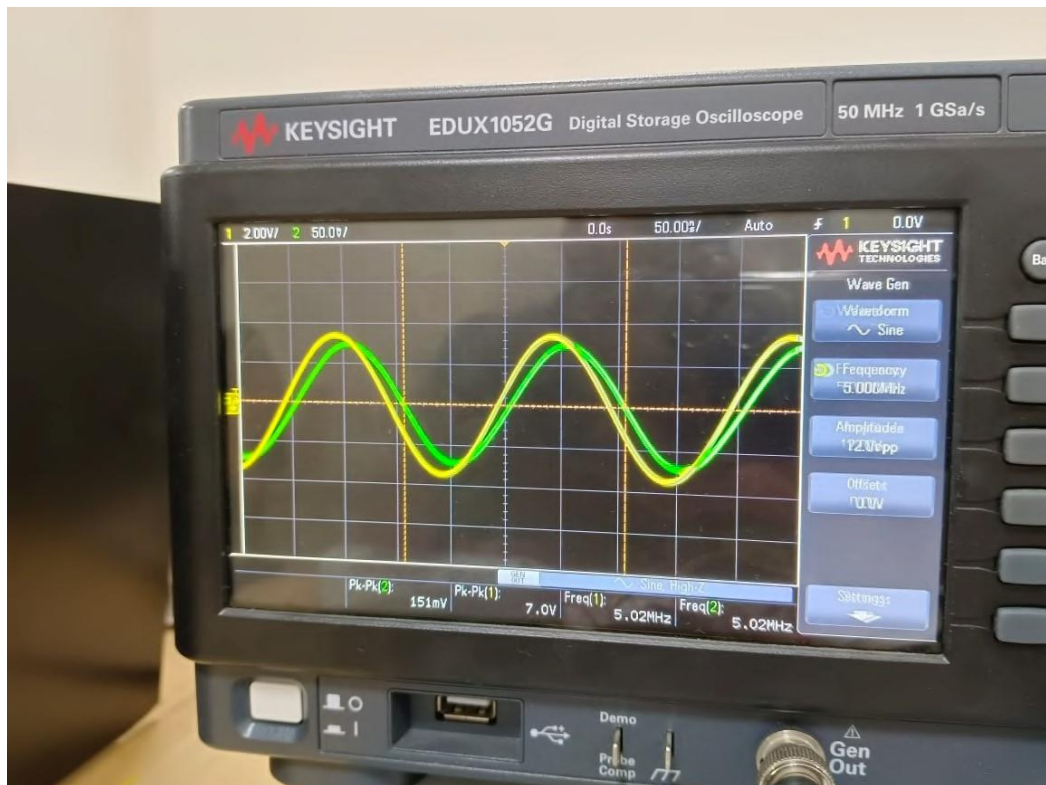
Case4: $f=1\text{MHz}$

$V_A=3.66\text{V}$ and $V_p=11.3\text{V}$ with V_A lagging than V_p



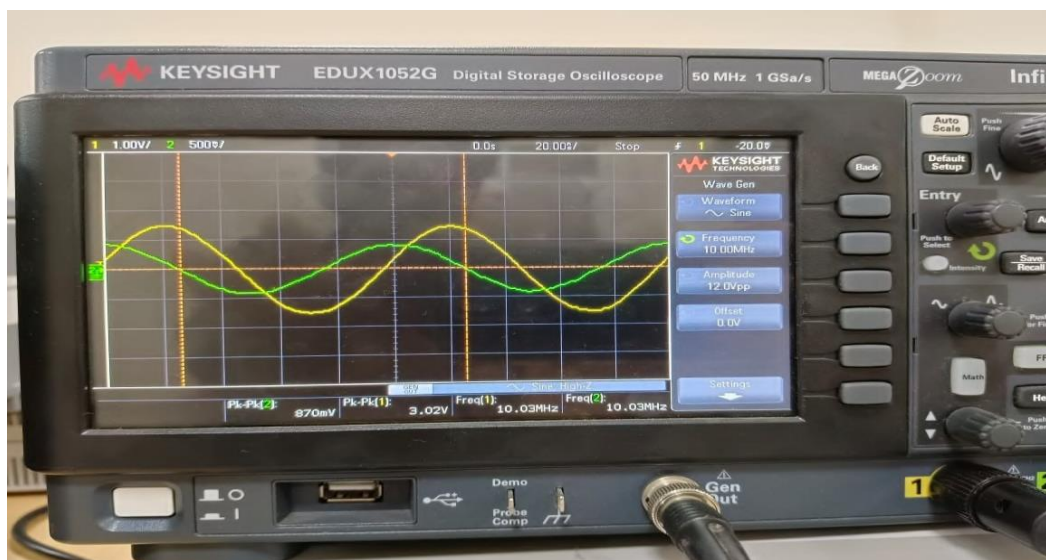
Case5: $f=5\text{MHz}$

$V_A=151\text{mV}$ and $V_p=7\text{V}$ with V_A slightly leading than V_p



Case6: $f=10\text{MHz}$

$V_A=870\text{mV}$ and $V_p=3.02\text{V}$ with V_A lagging than V_p



Case7: $f=20\text{MHz}$

$V_A=550\text{mV}$ and $V_p=2.48\text{V}$ with V_A slightly leading V_p



V in (frequency)	$V_A(V_{pp})$	$V_p(V_{pp})$
10 k Hz	840 mV	12.3 V
50 k Hz	860 mV	12.7 V
100 k Hz	860 mV	12.5 mV
1MHz	3.66 V	11.3 V
5MHz	151 mV	7 V
10MHz	870 mV	3.02 V
20MHz	550 mV	2.48 mV

From above table we can conclude that:

As frequency of input voltage kept increasing there was a gradual decrease in V_p and we can observe sudden Drop in between.

There are several reasons why the output of a step-down transformer may be less than expected when a high-frequency signal is input.

Impedance Mismatch: The signal may be returned back to the source when there is a mismatch in impedance between the transformer and the load. The amplitude of the signal may decrease.

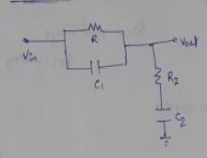
Core Saturation: The transformer core may become saturated by a high-frequency signal, which will lessen its capacity to step down the voltage. The output voltage may decrease as a result of this saturation.

Resonance: The transformer may resonate at a particular frequency, causing a reduction in the output voltage at that frequency.

PART D and E calculation:

LAB BOOK

(1) (c)

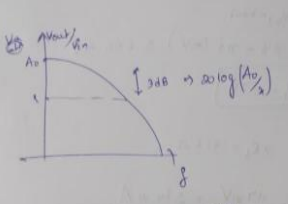


Team Mate: Radheshyam (discussed)

∴ In probe circuit, R_1 & C_1 are connected in parallel to each other which are in series with input (V_{in}).
At low frequencies,
The impedance $X_{C_1} = \frac{1}{j\omega C_1}$ is very large (as $f \downarrow$ ω is less)
∴ More value of V_{in} drops across resistor R_1 .
We know that,
As f increases, the impedance across X_{C_1} decreases and allow voltage to drop across gradually.
The combⁿ of R_1 & C_1 in parallel makes it Low PASS FILTER.
We can observe that,
 R_2 & C_2 are in series to each other which are connected to V_{out} .
∴ At low frequencies,
 X_{C_2} is very high
then the capacitor circuit behaves like open-circuit.
∴ $V_{out} \approx 0$.
As frequency increases, the impedance X_{C_2} decreases and allow voltage to drop across capacitor C_2 .
∴ V_{out} increased.

∴ This combination acts as High pass FILTER.
From both combinations we can conclude that
Probe circuit behaves as voltage divider depending on frequency.
Acts as BAND PASS FILTER. → allow range of freq to pass

(e)



TA explained in LAB

∴ $20 \log A_0 - 20 \log x = 3 \text{ dB}$
 $\Rightarrow 20 \log \left(\frac{A_0}{x} \right) = 3$
 $A_0 = x \cdot 10^{3/20}$
 $\therefore A_0 = x \sqrt{2}$

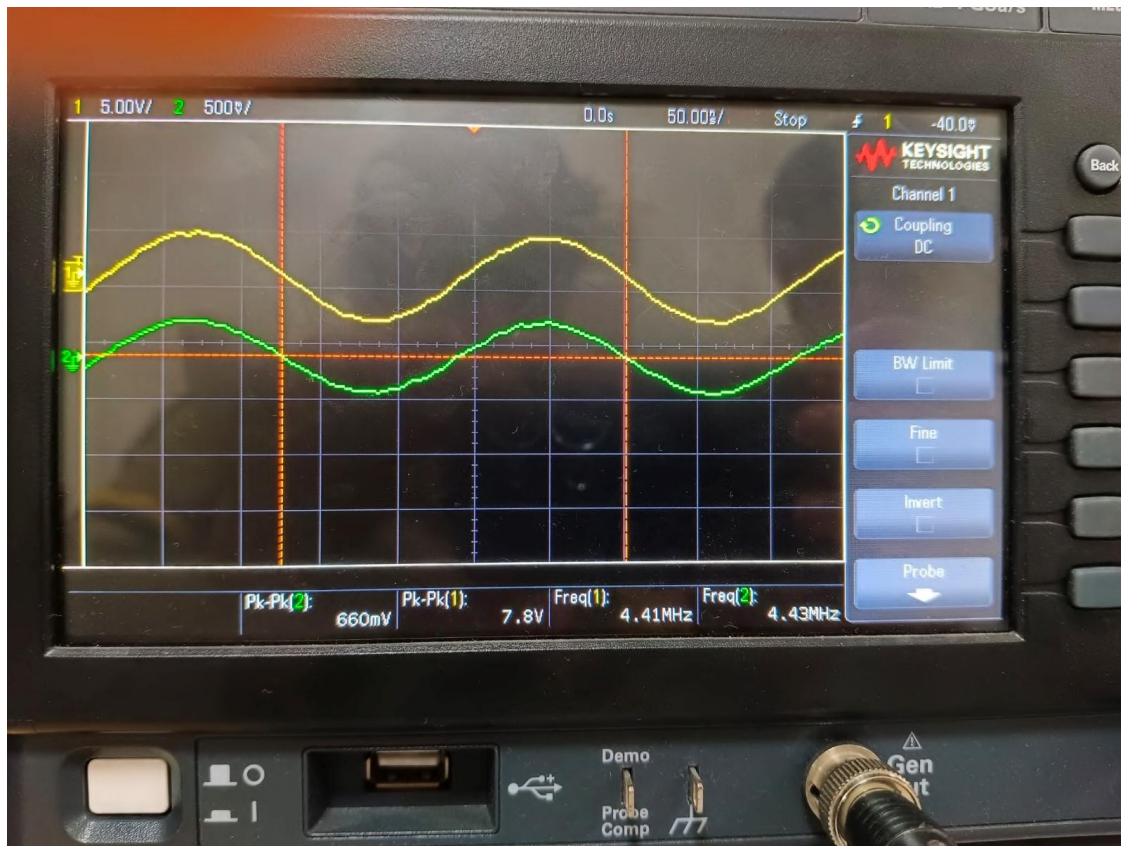
$x = \frac{A_0}{\sqrt{2}} = \frac{1}{\sqrt{2}}$

$\Rightarrow -3 \text{ dB}$ observed at where amplitude goes to $\frac{1}{\sqrt{2}}$ times
 of amplitude $\Rightarrow \frac{1}{\sqrt{2}} \approx 0.707$

$A_0 = 1$
 as it passes all values
 $10^{3/20} \approx \sqrt{2}$ (approx)

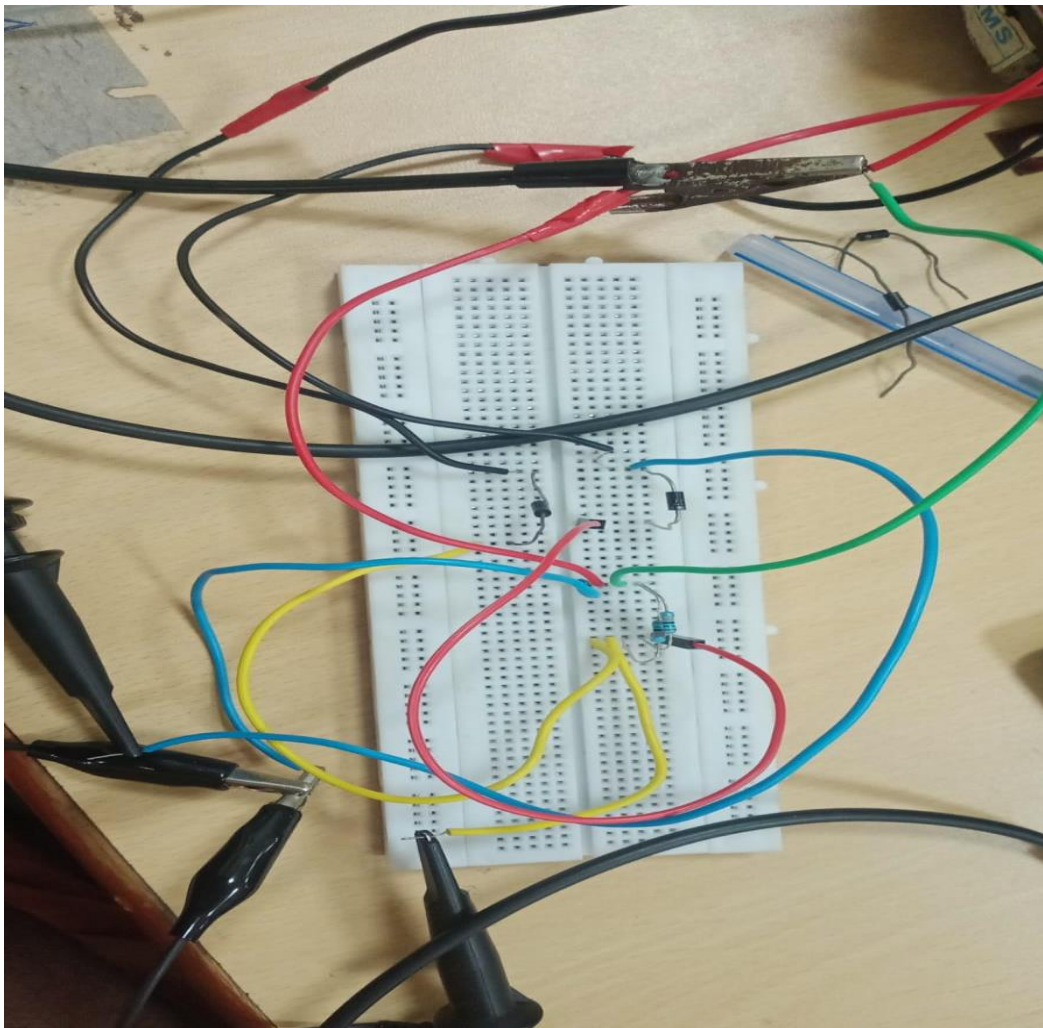
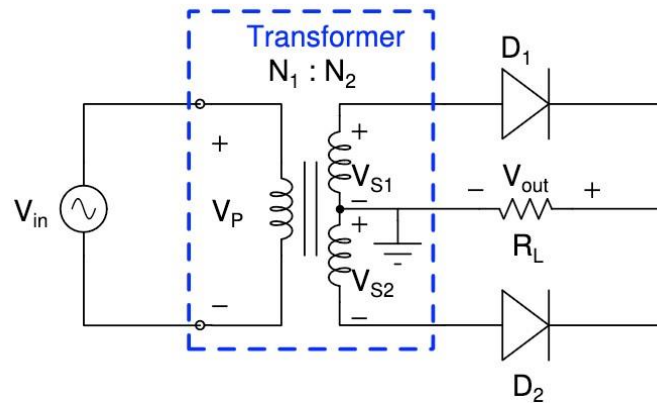
e) -3dB bandwidth can be obtained by the point when the output input voltage drops to 63% of its original Value.

Time constant = RC in the RC .At t=time constant, the Voltage drops in by 63% forming -3dB frequency bandwidth. $V_{in}(\text{max } V_{pp}) = 12\text{V}$, 63% of $V_{in} \sim 7.6 \text{ V}$.



The output voltages V_{in} shown lowers more than 7.6V at a frequency of 4.4MHz in the input. Thus, the probe wire's -3dB band width is 4.4MHz.

2) Full wave rectifier using centre tapped transformer and two diodes:



a)

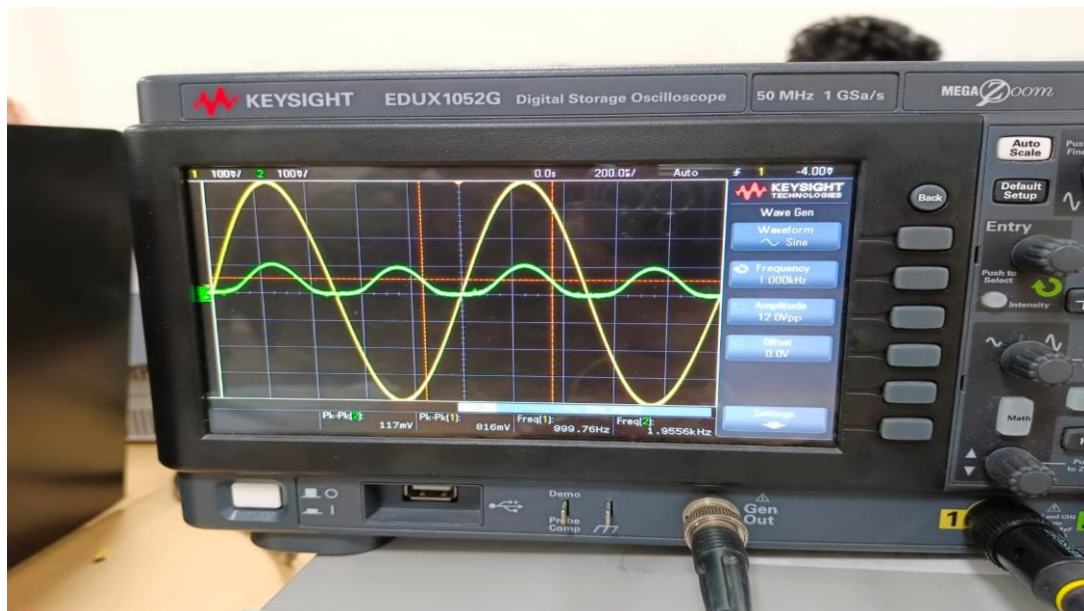
INPUT:

$V_{in}(V_{pp}) = 12\text{ V}$

Frequency = 1k Hz

$R = 50\text{ k ohm}$

b) Plot of V_{S1} and V_{out} :



->Full wave rectification observed

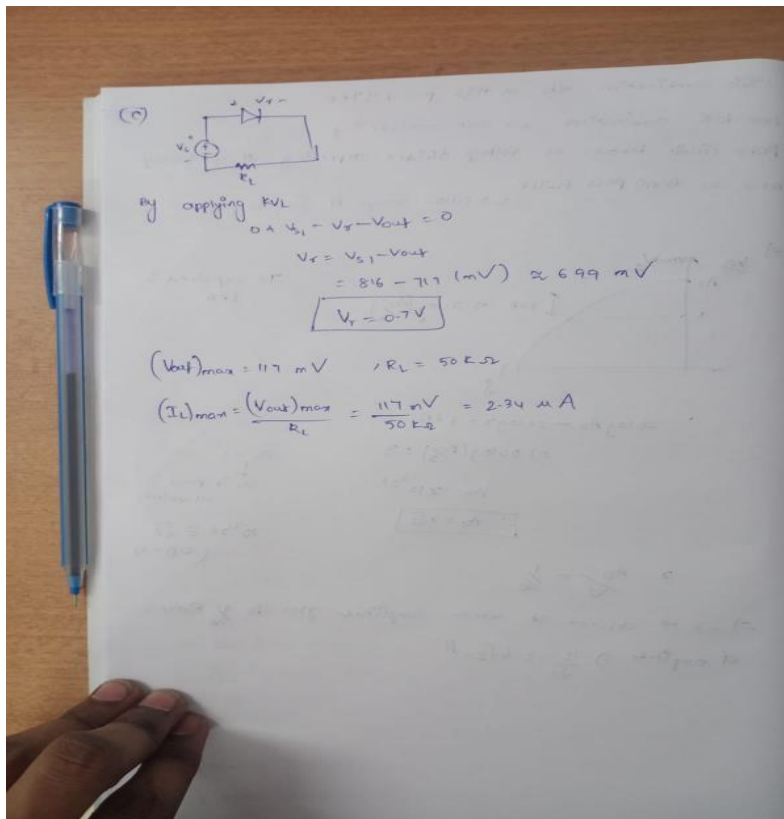
V_{out} plotted on channel 2 and V_{S1} plotted on channel 1.

Peak to peak amplitude voltages of V_{out} and V_{S1} :

$V_{out} = 117\text{mV}$

$V_{S1} = 816\text{mV}$

c)



So, peak current through the resistor is (I_L) is $2.34 \text{ }\mu\text{A}$.

d)

Reasons for decrement in V_{out} amplitude: The significant reduction in output voltage amplitude in a full wave rectifier with center tapped transformer could be due to the fact that the diodes are not able to completely turn on and forward current is too less.

-> This could happen because the diodes have a threshold voltage that must be reached before they start conducting.

-> If the voltage across the diode is not high enough, the diode will not conduct properly.

EXPLANATION of Reason:

->we need to measure the forward bias current through the diode.

->It can be done using a multimeter (in ammeter mode), by connecting the diode in series with the multimeter and a power supply.

->The voltage across the diode should be equal to the forward voltage drop of the diode, which can be found in its datasheet.

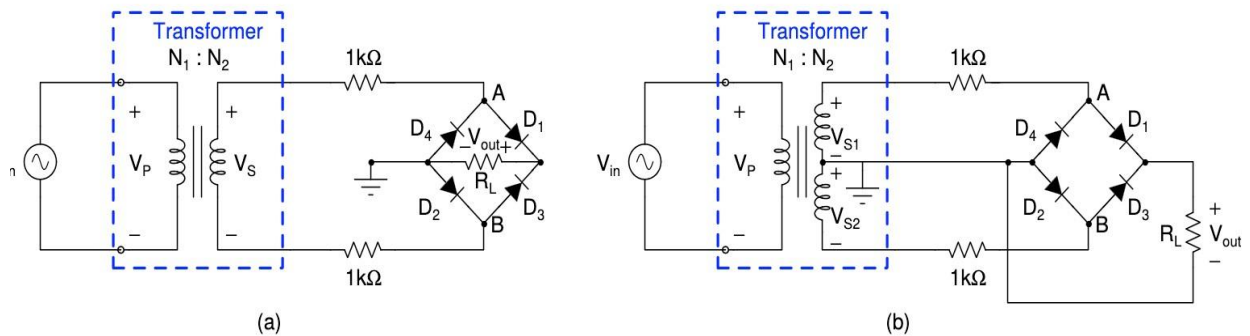
-> If the measured forward bias current is indeed too low, then we can conclude that the diodes are not able to completely turn on and conduct properly.

->In this case, we can try using different diodes with a lower threshold voltage or higher current rating.

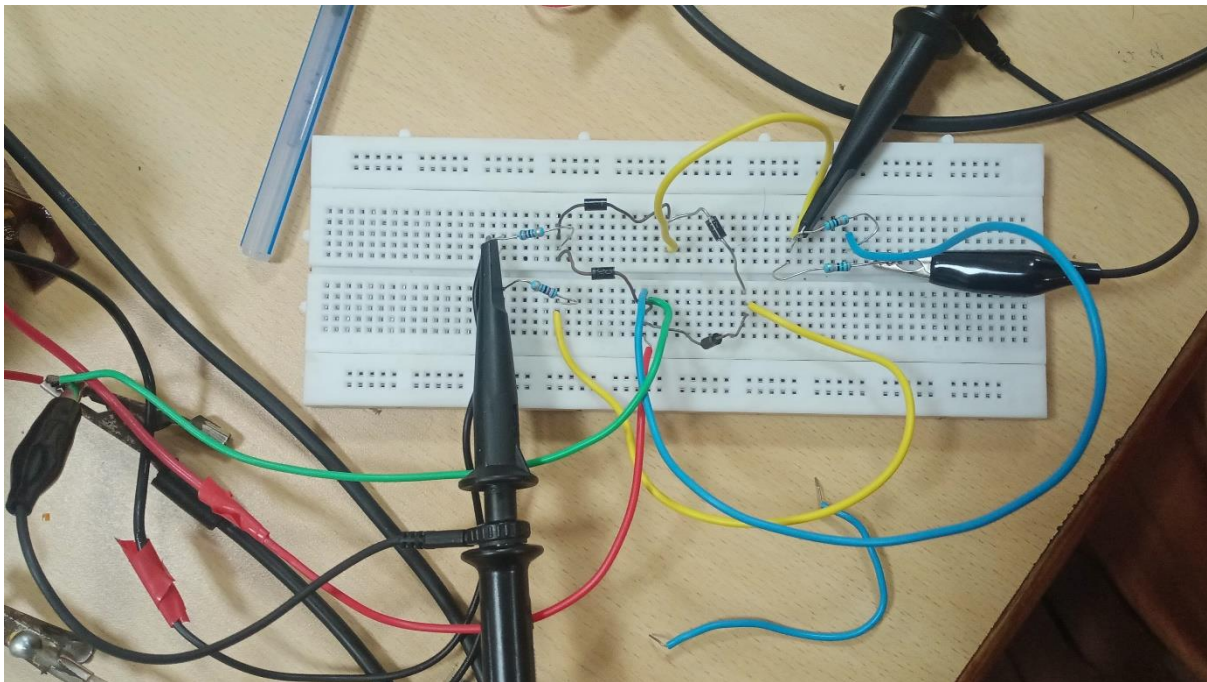
From the diode properties, we calculated the voltage across the diode and found that it was 699 mV, which is close to the diode's V_{cut} in (1N4007).

It says that the diode's complete inability to switch on was the reason for the decreased value of the input to the rectifier circuit (the output from the transformer) following rectification. We can observe that the V_{diode} was nearly 7V based on the observed values, which was not expected.

3) Bridge rectifier for full wave rectification:



a) BUILDING OF CIRCUIT:



b)

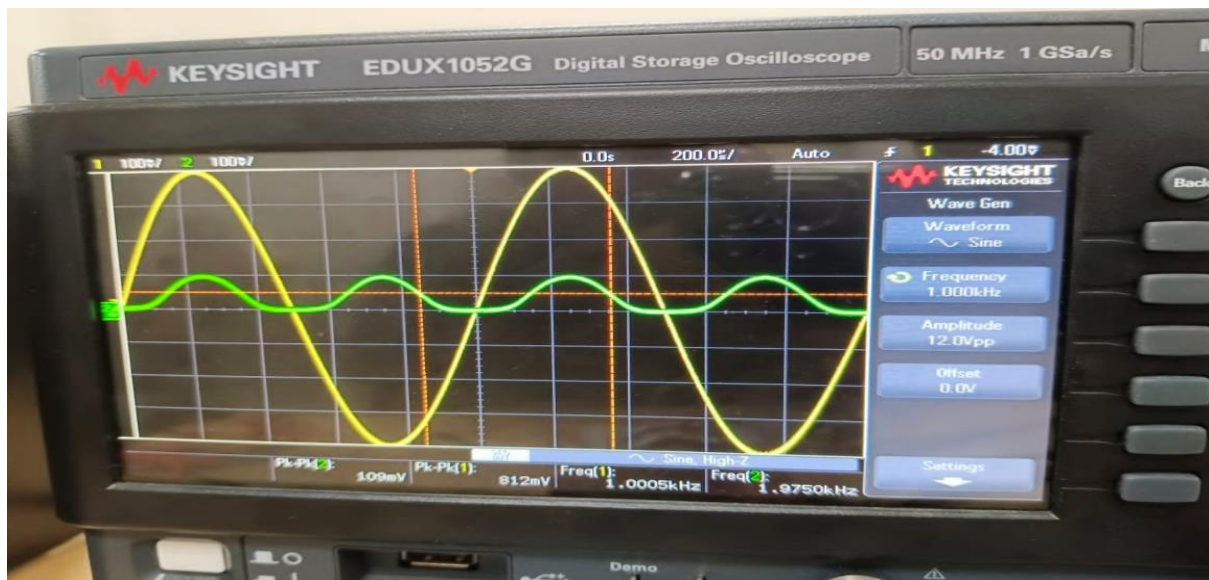
V_{in} (sinusoidal) :-----

$V_{input}(V_{pp})=12\text{ V}$

Frequency=1 k Hz

R=50 k ohm

b) Plot of VS1 and Vout :



Vout plotted on channel 2 and Vs1 plotted on channel 1.

Peak to peak amplitude voltages of Vout and Vs1:

Vout=109mV

Vs1=812mV

RL =50KHz

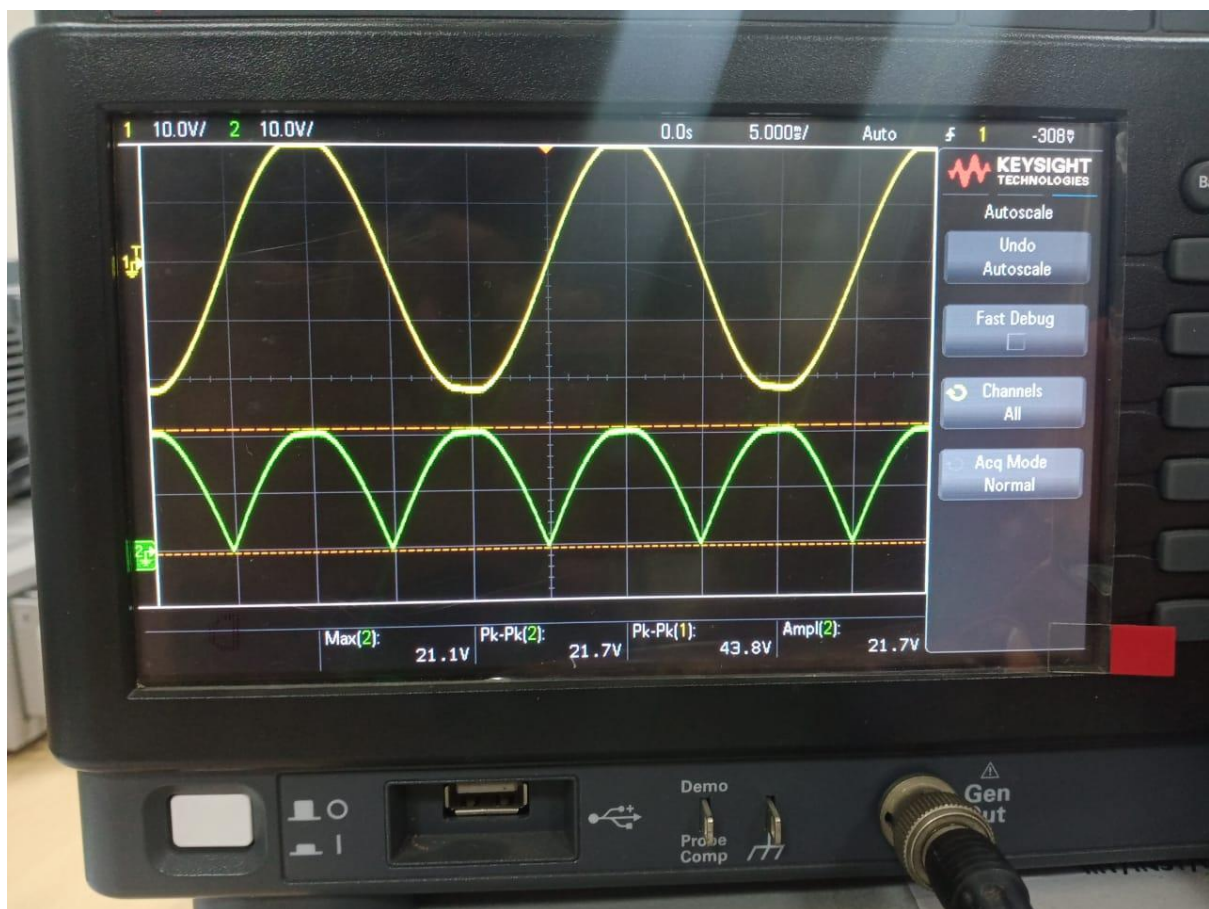
$I_L (\text{max}) = (V_{\text{out}})_{\text{max}} / R_L = 109\text{mV} / 50\text{kHz} = 2.18 \mu\text{A}_{\text{SEP}}$

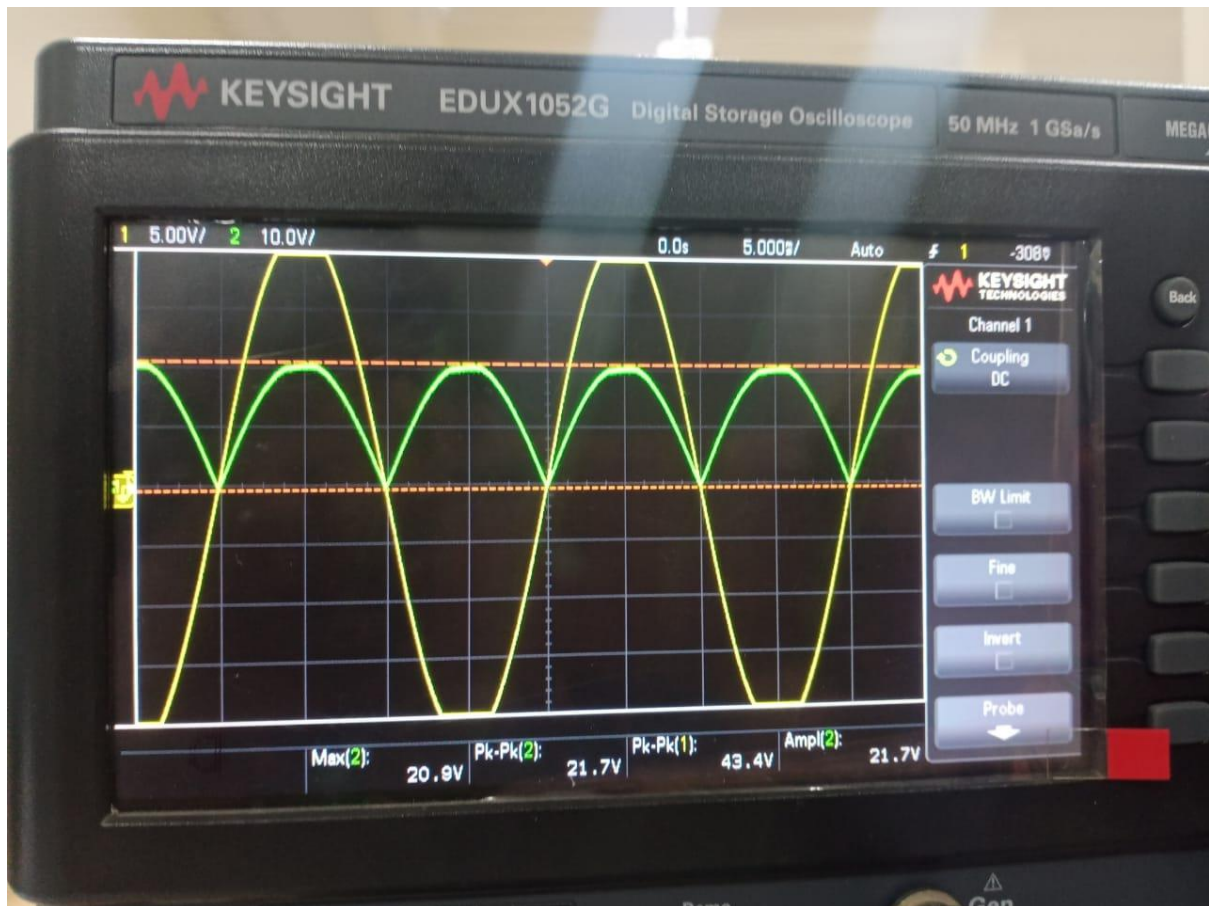
So the peak current through the resistor is 2.18uA.

c) Replacing V_{in} ($V_{pp}=12V$) to V_{in} ($V=220V$), the wall supply using the transformer plug pins.

$V_{in} \sim 220V$, frequency $f=50Hz$

Plot of V_{S1} and V_{out} :





d) As compared to the before situation, the output from the wall supply is less attenuated than the equivalent output from the DSO wave generator input. The forward bias voltage across the diode rises in concert with the input voltage, increasing the diode current value. For the same resistance value, this leads to a higher output voltage. For this reason, the output is less turned off.

CONCLUSION:

When the input voltage increases, the forward bias voltage across the diode also increases, causing a higher current to flow through the diode. This results in a larger output voltage

for the same resistance value. As a result, the output is less attenuated in this case