

# ANALOG ELECTRONIC CIRCUITS

## LAB REPORT-6

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**Roll no:** 2023102032

## MOSFET: I-V and Voltage Transfer characteristics ( VTC )

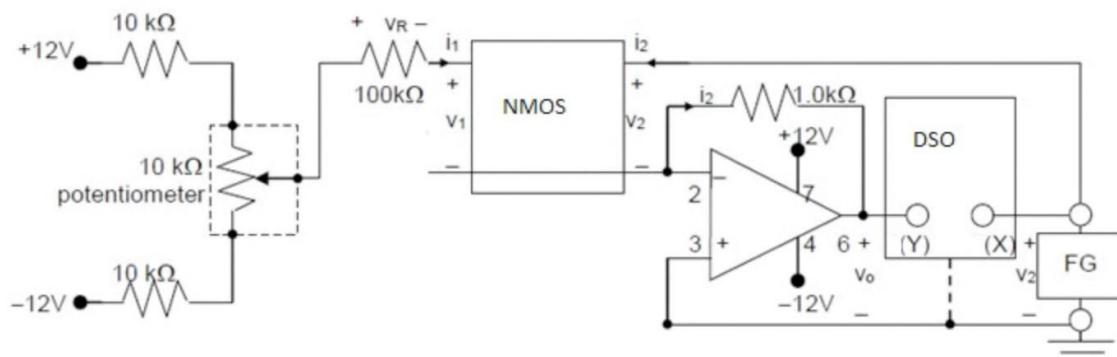
### 1) ID vs VDS Characteristics :

The MOSFET we are going to use is an n-channel device (NMOS), having its Gate, Source, and Drain terminals available at pins 3, 4 and 5 of the IC.

All NMOS devices in the IC have a common substrate (pin 7). In the below figure,  $V_2 = V_{DS}$  and  $V_0 = -I_D \times R_0 = -ID \times R_0$ , where  $R_0 = 1 \text{ k}\Omega$  (between node 2 and 6).

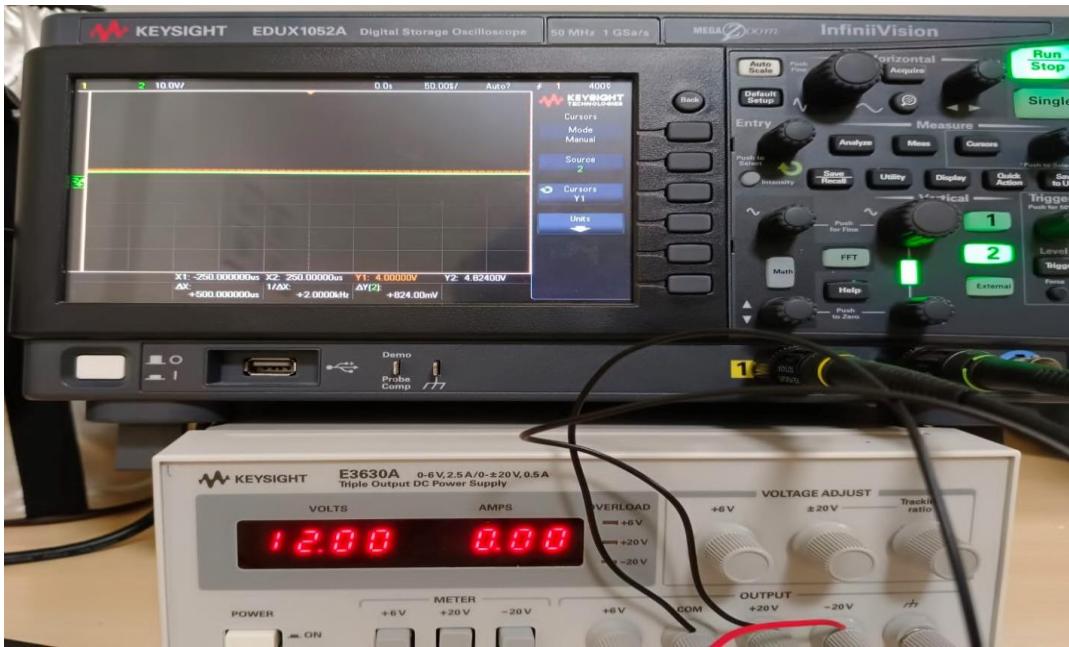
Therefore plot of  $ID$  will be proportional to  $V_0$ . We will sweep  $V_2 = V_{DS}$  using the function generator and plot  $V_0(\propto -ID)$ .

Potentiometer output verification:



**Figure 1:** Circuit for displaying the output i-v characteristics of MOSFET

Max value=+4



Min value=-4



VGS	VDS	Vo	Io
0.2	All	107.5mV	107.5uA
0.3	All	107.5mV	107.5uA
0.4	All	129mV	129uA
0.5	All	150.5mV	150.5uA
0.6	All	150.5mV	150.5uA
0.7	All	150.5mV	150.5uA
0.8	All	150.5mV	150.5uA

<b>1</b>	<b>All</b>	<b>150.5mV</b>	<b>150.5uA</b>
<b>1.2</b>	<b>All</b>	<b>150.5mV</b>	<b>150.5uA</b>
<b>1.4</b>	<b>All</b>	<b>150.5mV</b>	<b>150.5uA</b>
<b>1.6</b>	<b>All</b>	<b>150.5mV</b>	<b>150.5uA</b>
<b>1.8</b>	<b>All</b>	<b>330mV</b>	<b>330uA</b>
<b>2</b>	<b>500mV</b>	<b>333mV</b>	<b>333uA</b>
<b>2</b>	<b>4V</b>	<b>333mV</b>	<b>333uA</b>
<b>2</b>	<b>8V</b>	<b>333mV</b>	<b>333uA</b>
<b>2</b>	<b>12V</b>	<b>333mV</b>	<b>333uA</b>
<b>3</b>	<b>500mV</b>	<b>528mV</b>	<b>528uA</b>
<b>3</b>	<b>4V</b>	<b>627mV</b>	<b>627uA</b>
<b>3</b>	<b>8V</b>	<b>627mV</b>	<b>627uA</b>
<b>3</b>	<b>12V</b>	<b>627mV</b>	<b>627uA</b>
<b>4</b>	<b>500mV</b>	<b>1.1055V</b>	<b>1.1055mA</b>
<b>4</b>	<b>4V</b>	<b>1.716V</b>	<b>1.716mA</b>
<b>4</b>	<b>8V</b>	<b>1.764V</b>	<b>1.716mA</b>
<b>4</b>	<b>12V</b>	<b>1.764V</b>	<b>1.716mA</b>

For VGS values up to 1.8V, the observed output voltage (Vo) remains relatively constant for different VDS values.

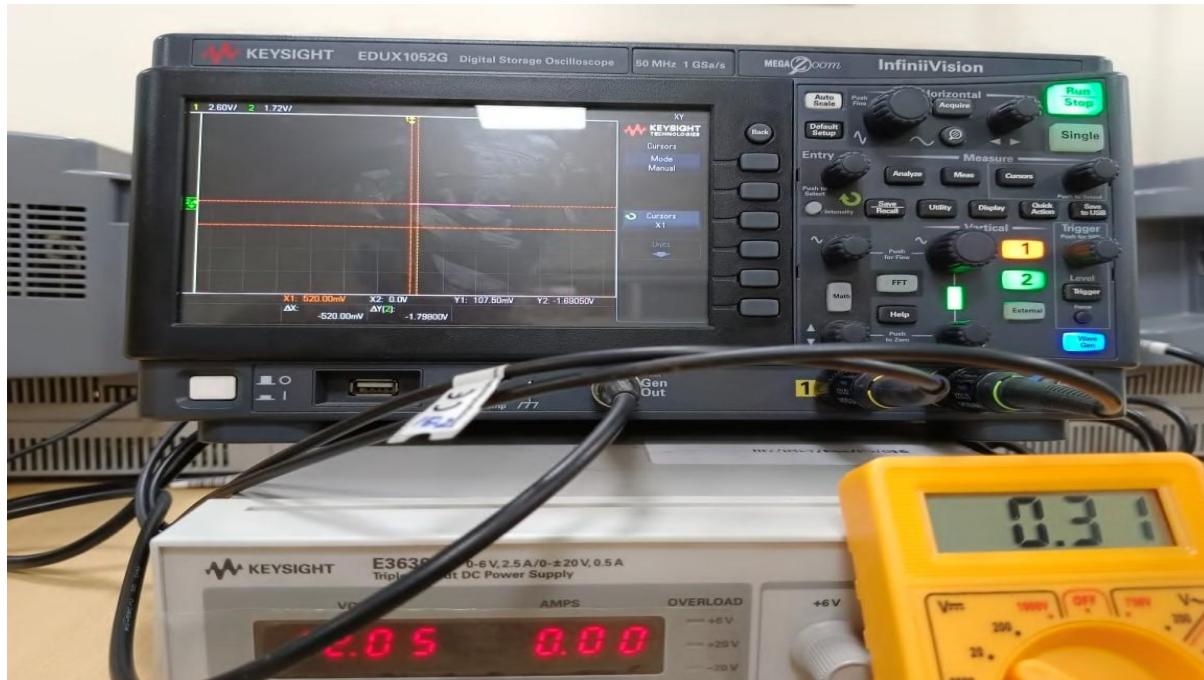
However, as VGS increases beyond 2V, the behavior of Vo starts to change. Specifically, between 2V and 4V of VGS, there is a noticeable variation in the value of Vo.

#### For VGS=0.2V



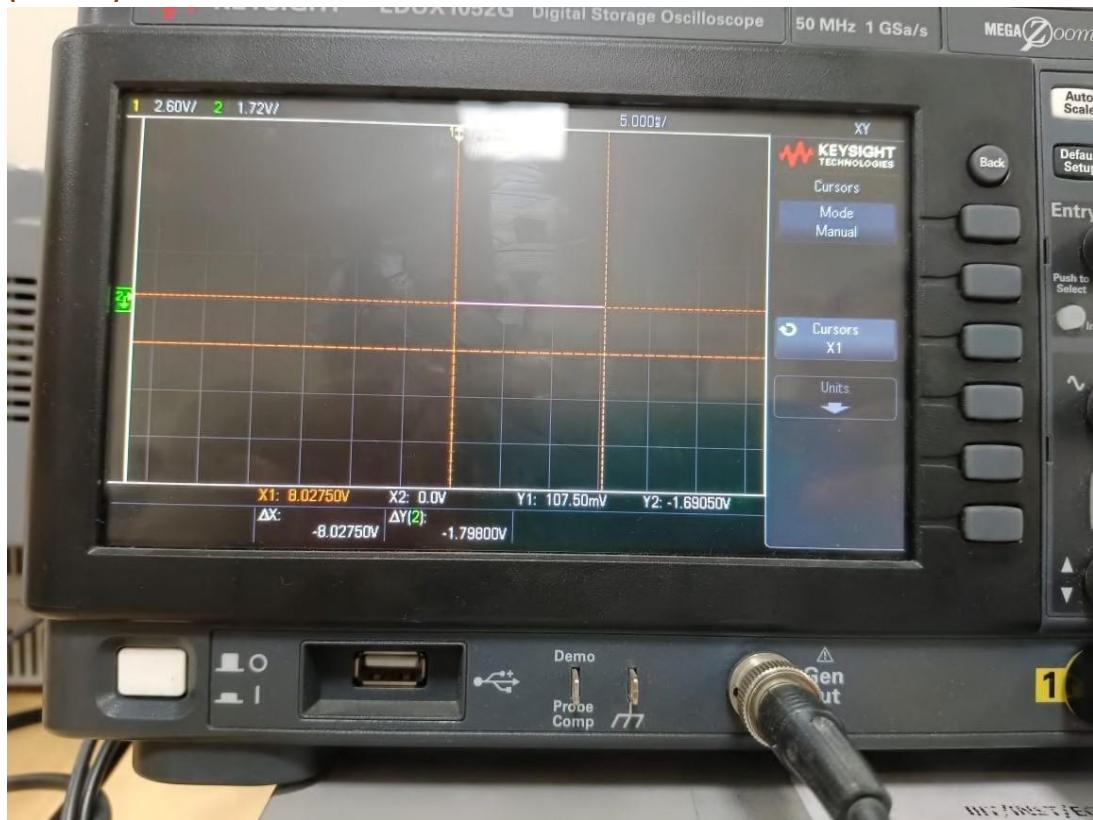
For VGS=0.3V

(VDS=500mV)



For VGS=0.4V

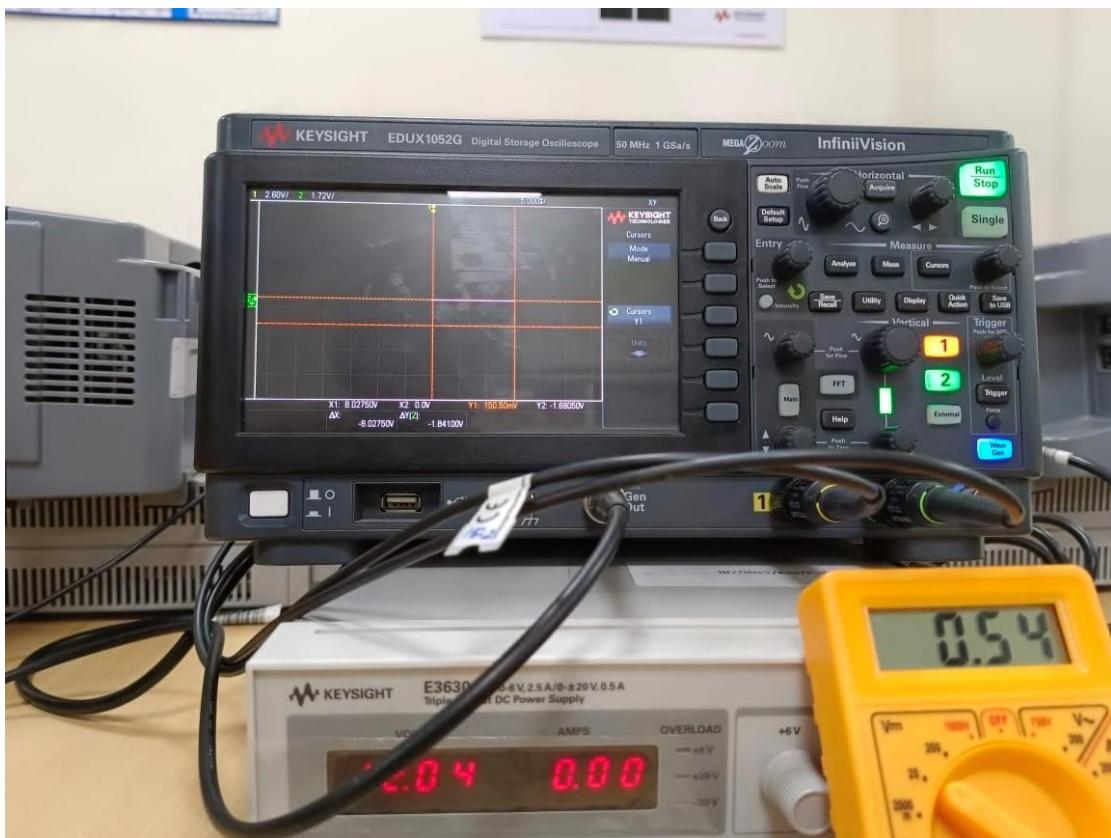
(VDS=4V)



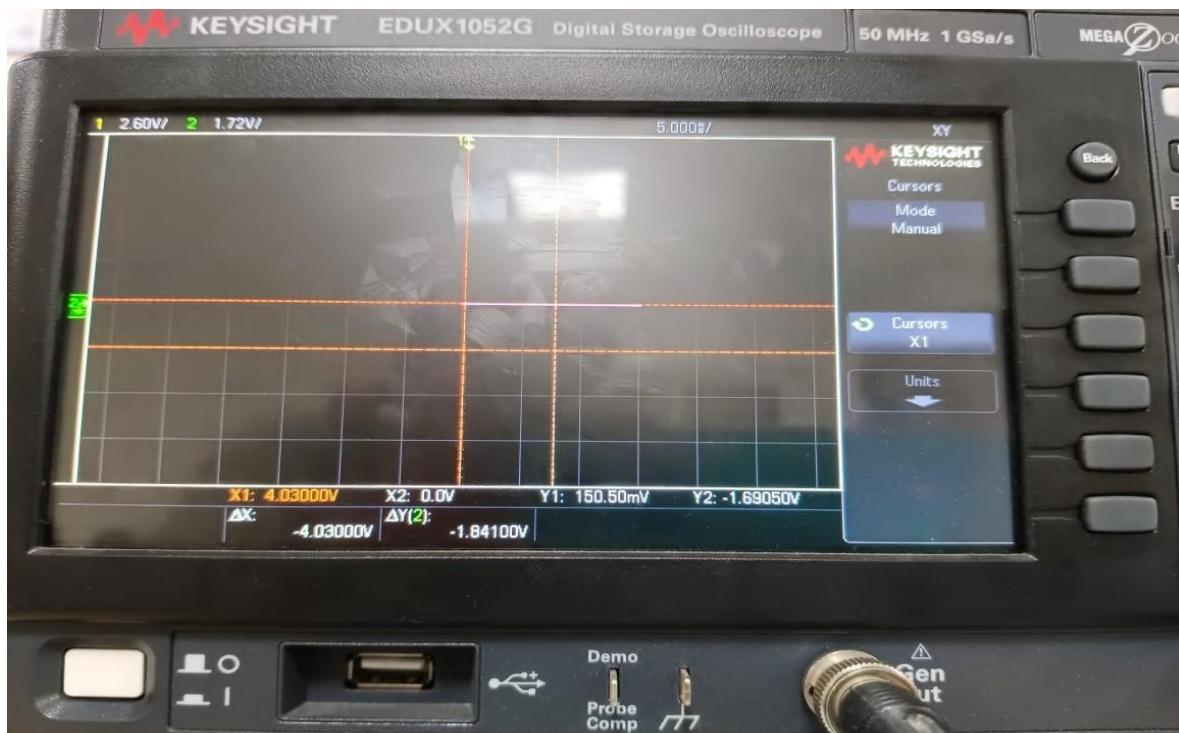


For  $V_{GS}=0.5V$

( $V_{DS}=8V$ )

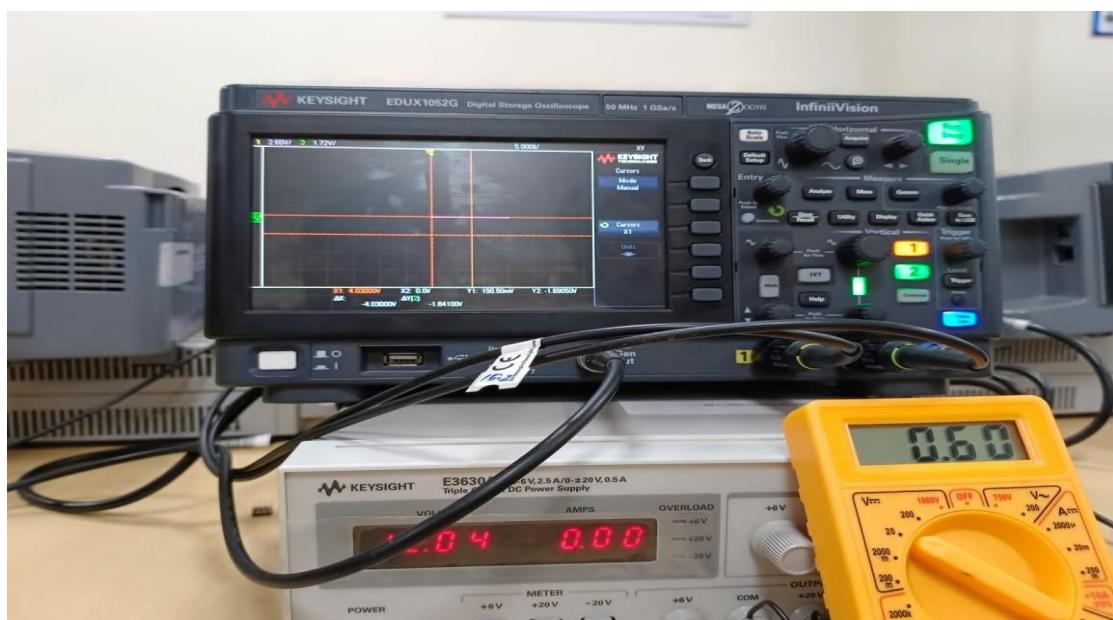


(VDS=4V)

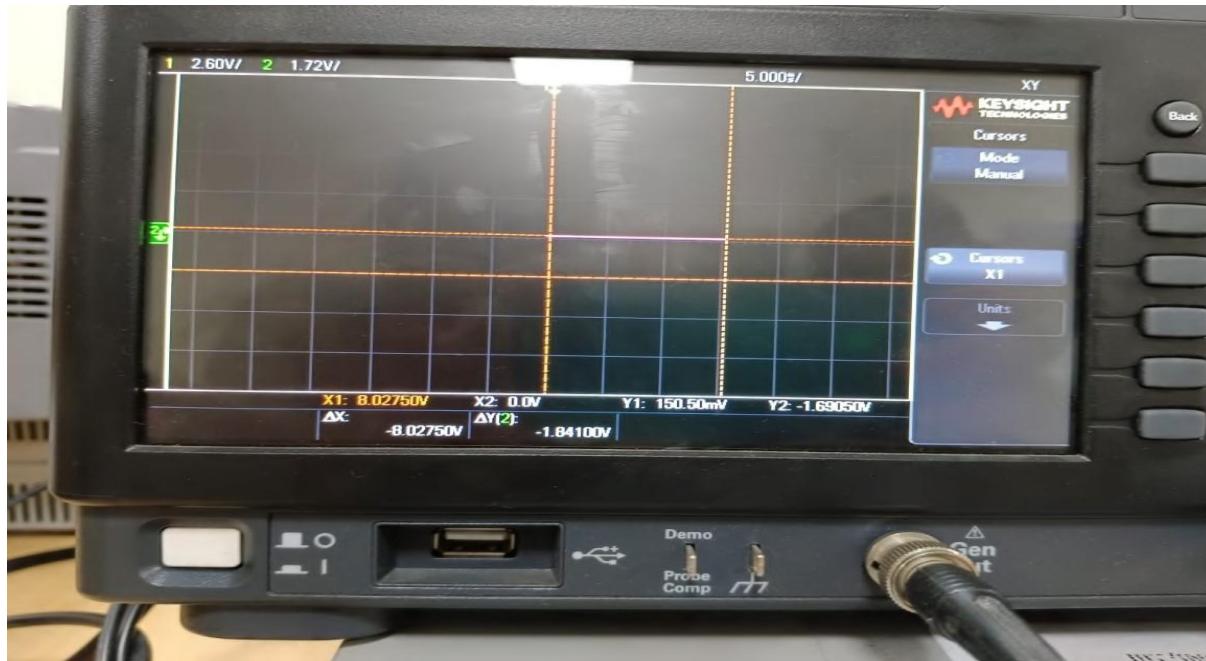


For VGS=0.6V

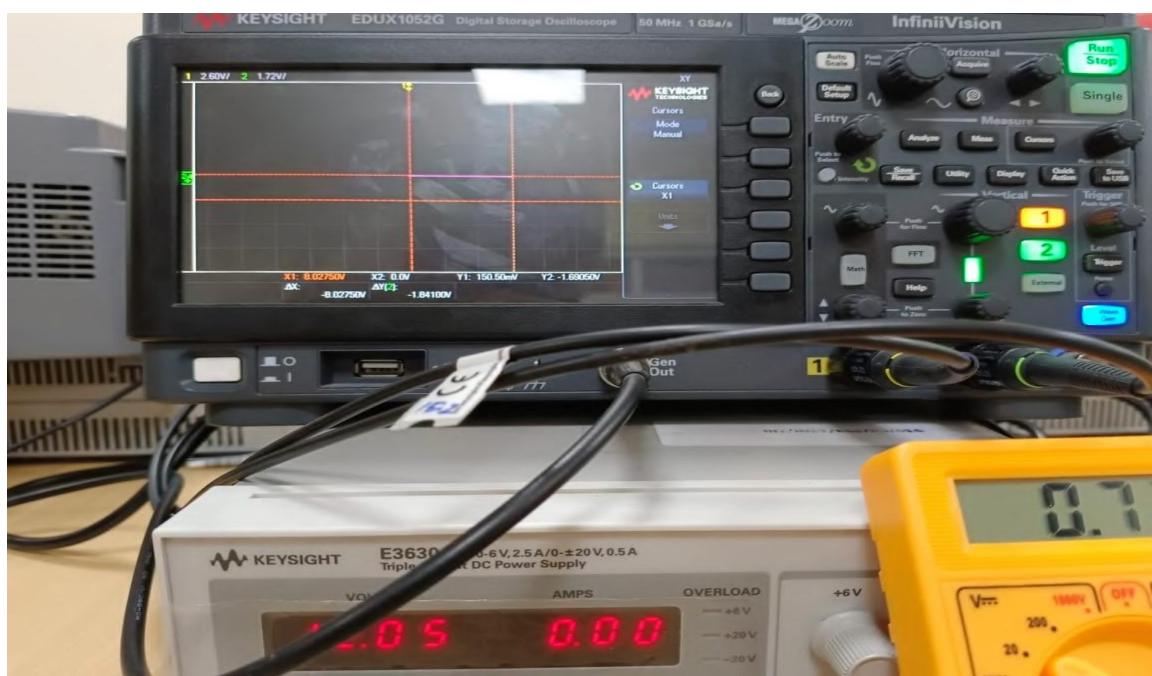
(VDS=4 V)



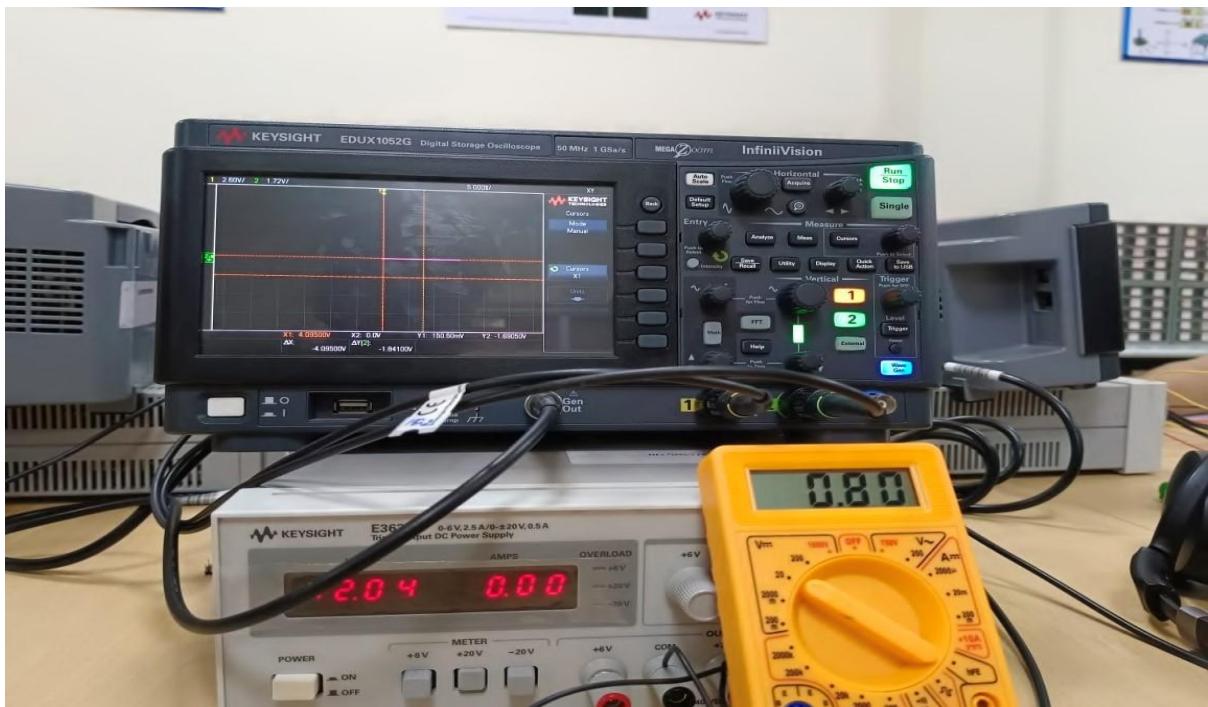
(VDS=8 V)



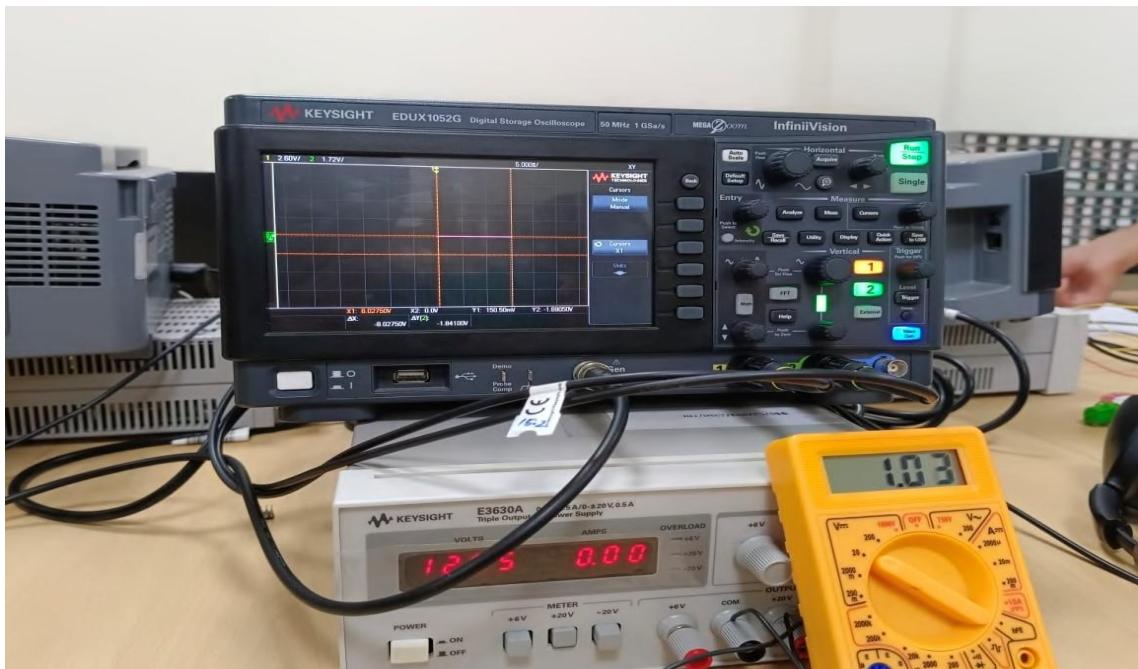
For VGS=0.7 V



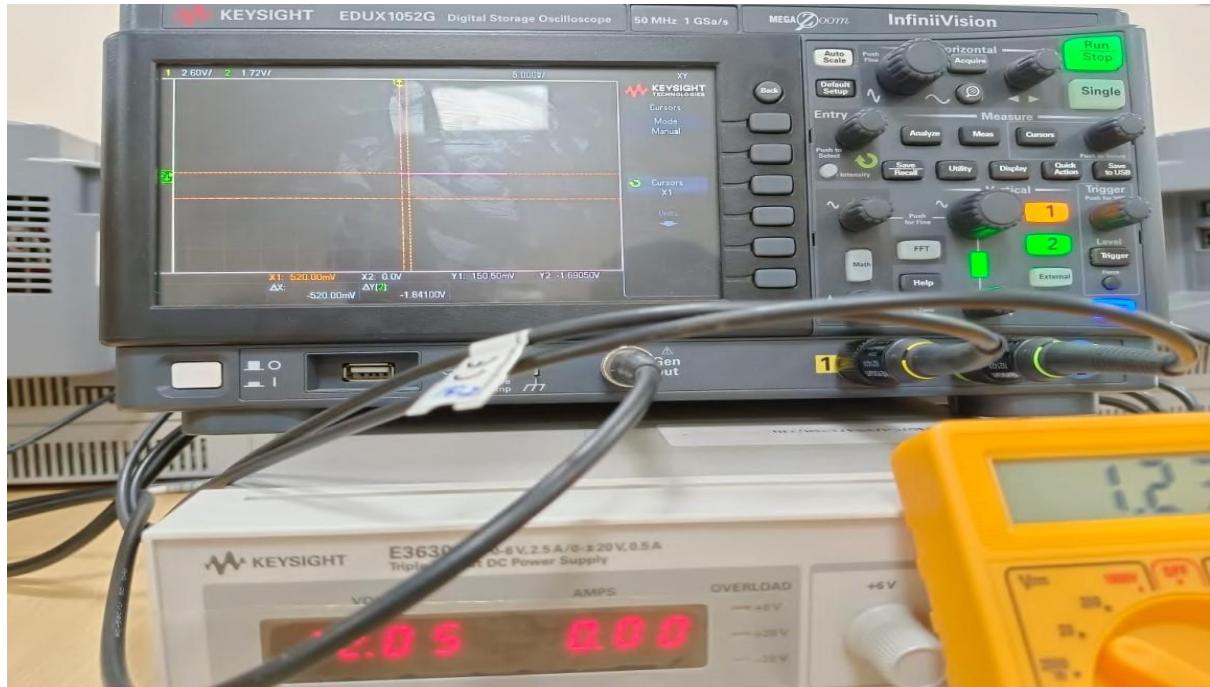
For VGS=0.8 V



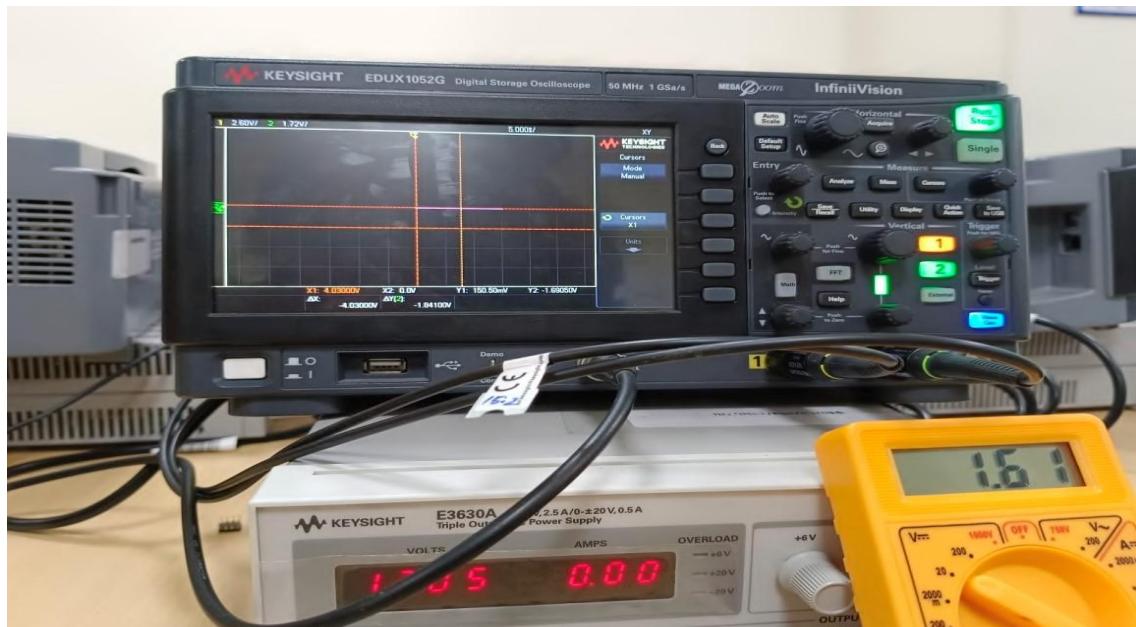
For VGS=1 V



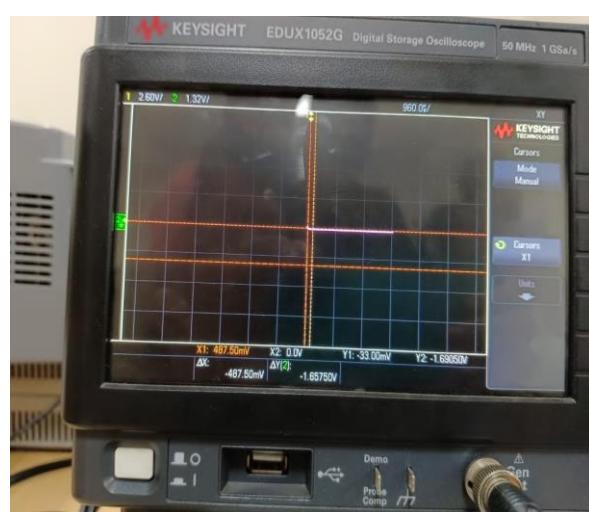
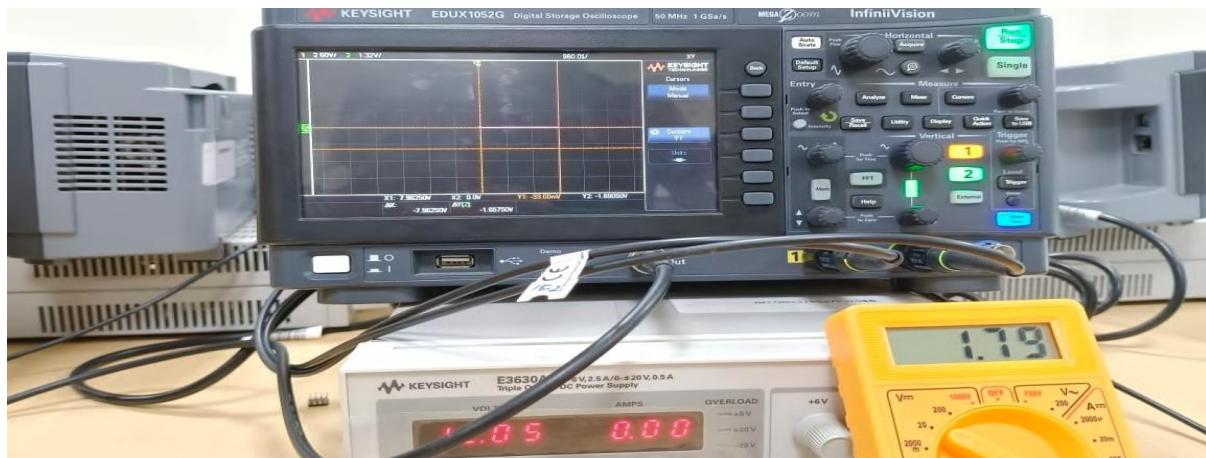
For VGS=1.2 V



For VGS=1.6 V



For VGS=1.8 V



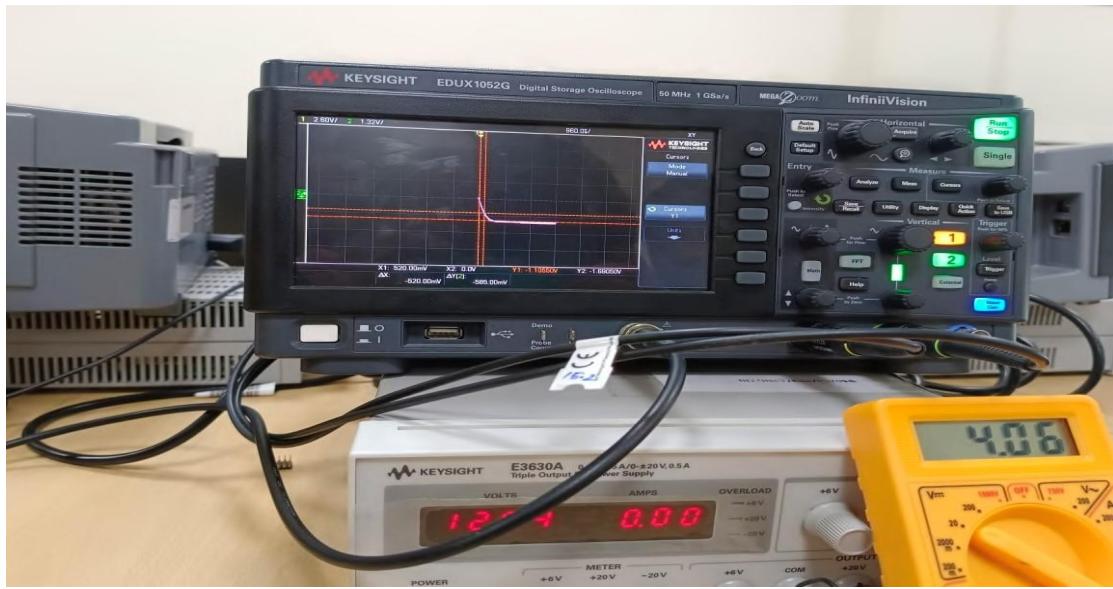
For VGS=2 V

(VDS=4V)

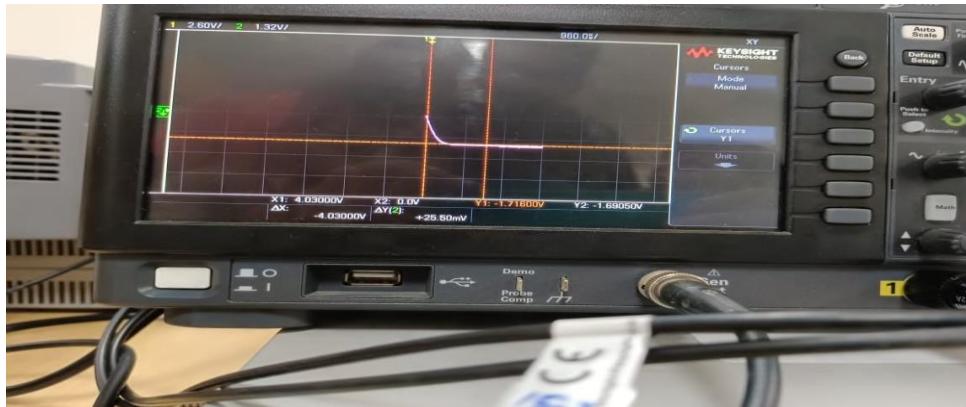


For VGS=4 V

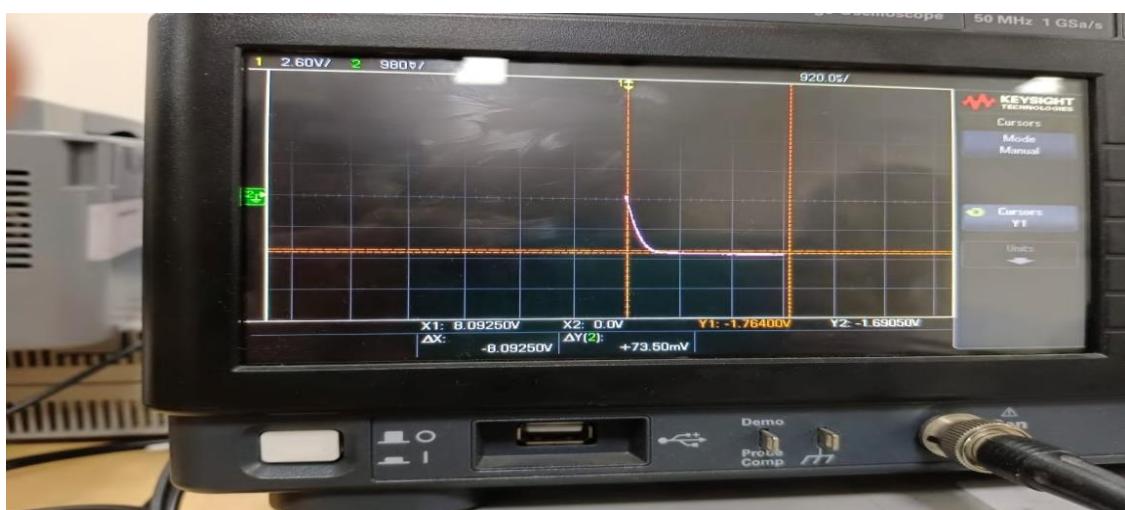
(VDS=500mV)



(VDS=4V)

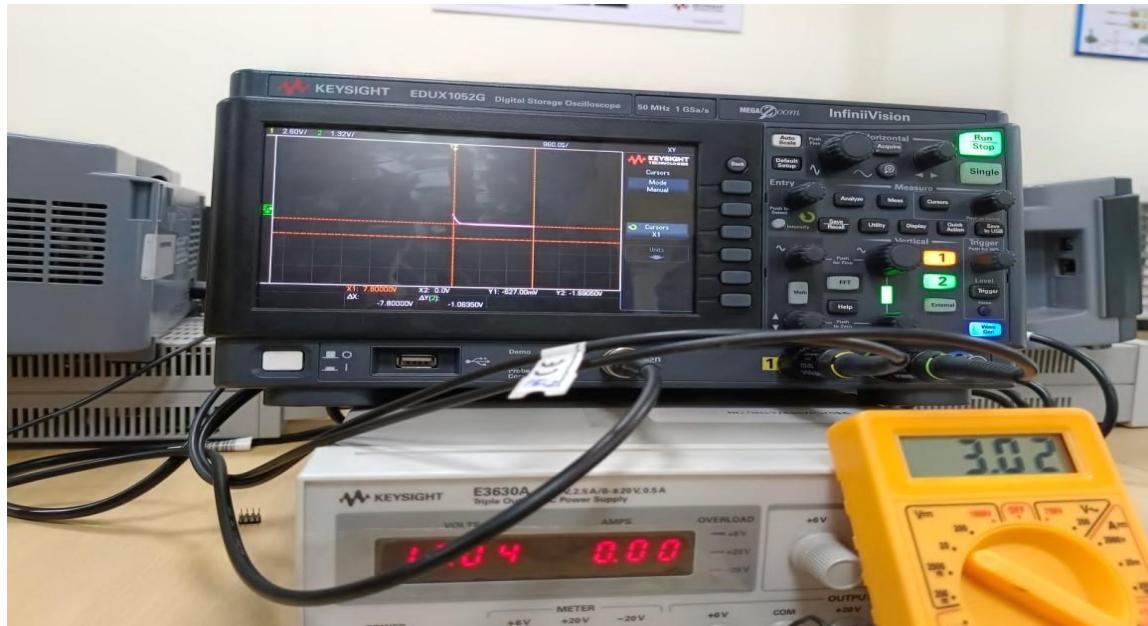


(VDS=8 V)



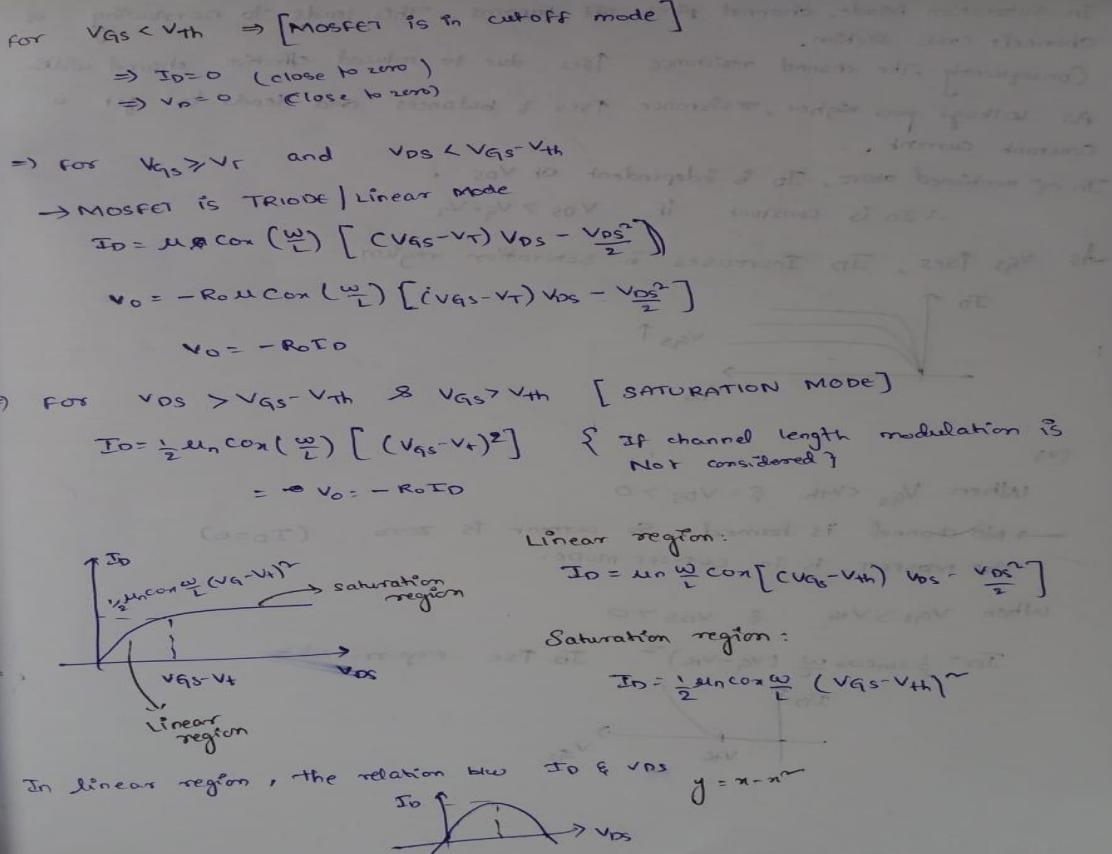
For VGS=8 V

(VDS=4V)



(VDS=8V)





In Saturation Mode, channel pinch off happens, This leads to narrowing of Channel's cross section.

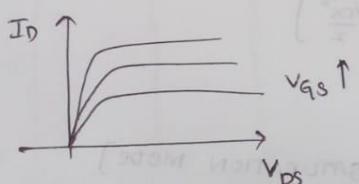
Consequently, The channel resistance increases due to reduced effective channel width

As Voltage goes higher, resistance increases & balances and leads to get a constant current.

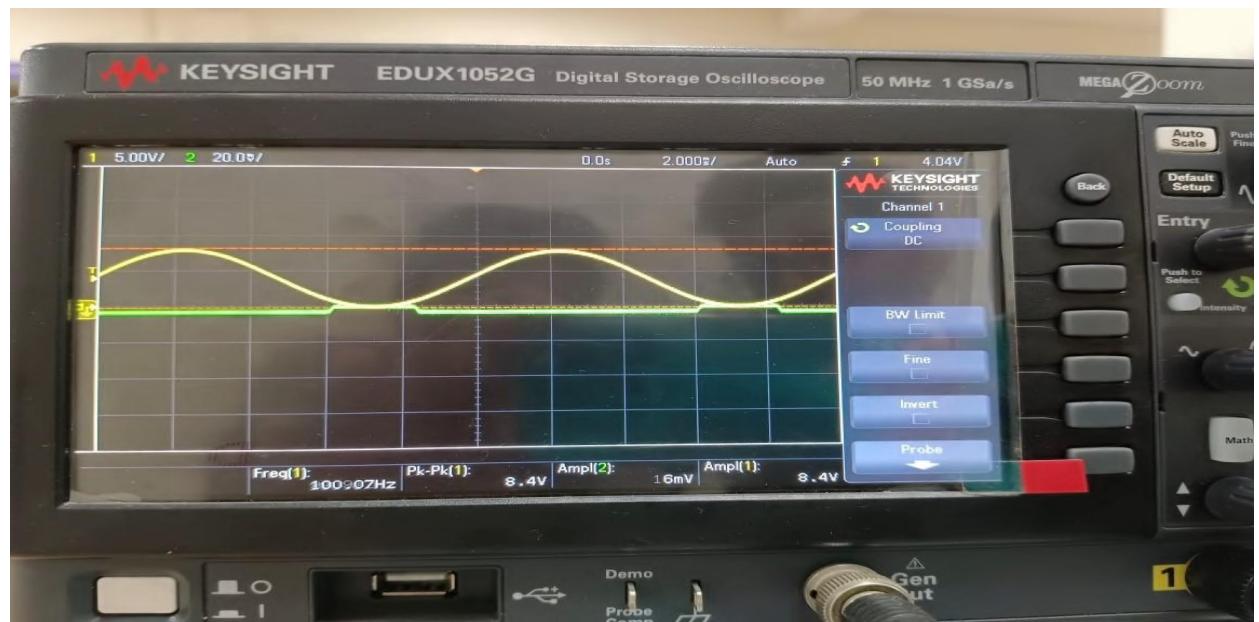
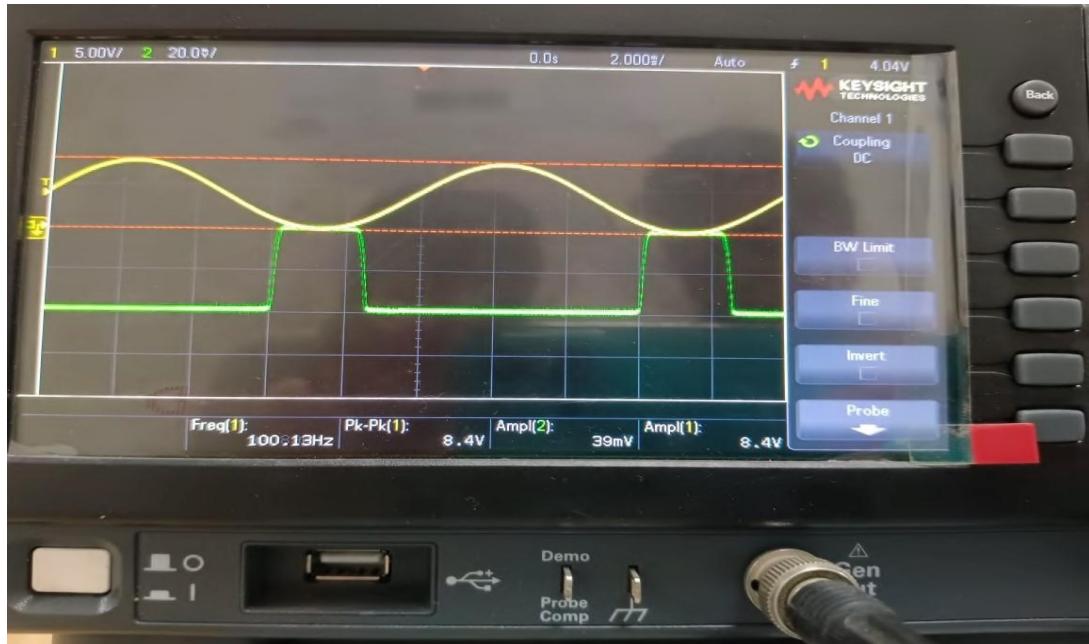
In eqn mentioned above,  $I_D$  is independent of  $V_{DS}$  !

$\therefore I_D$  is constant if  $V_{DS} > V_G - V_T$

As  $V_{GS}$  increases,  $I_D$  Increases in saturation region

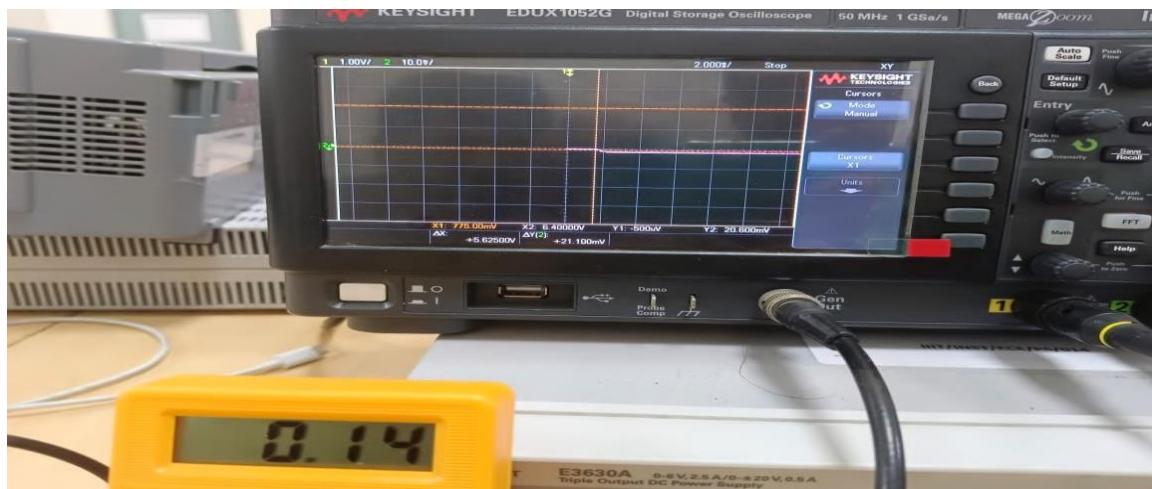


## 2) ID vs VGS Characteristics and Parameter Extraction:



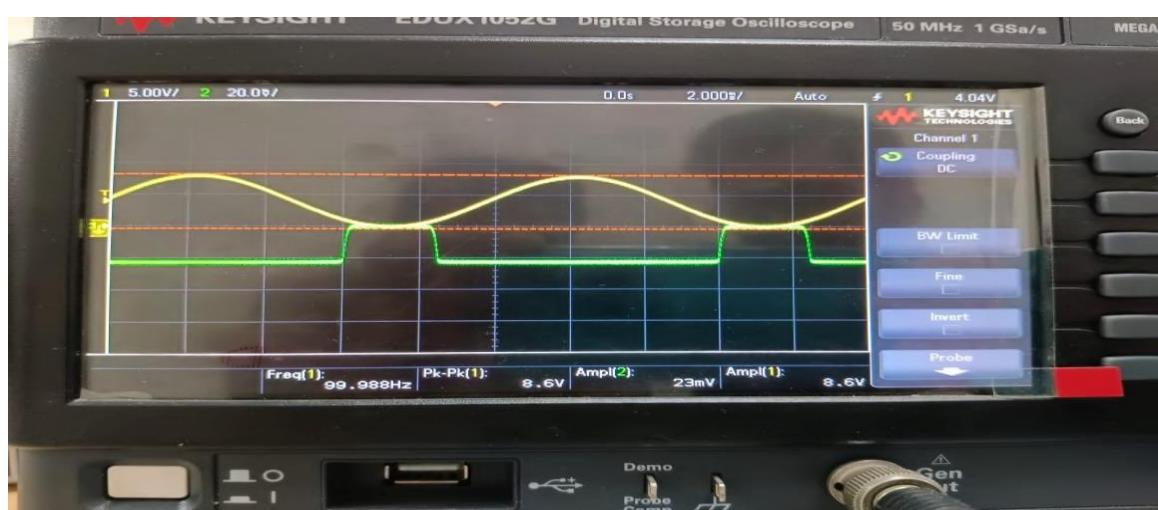
For VDS=0.1 V:

(VGS=775mV)



For VDS=0.2V:

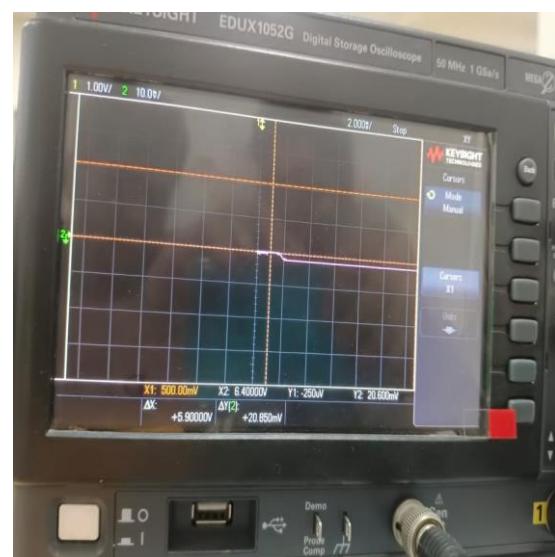
(VGS=675mV)



(VGS=2 V)

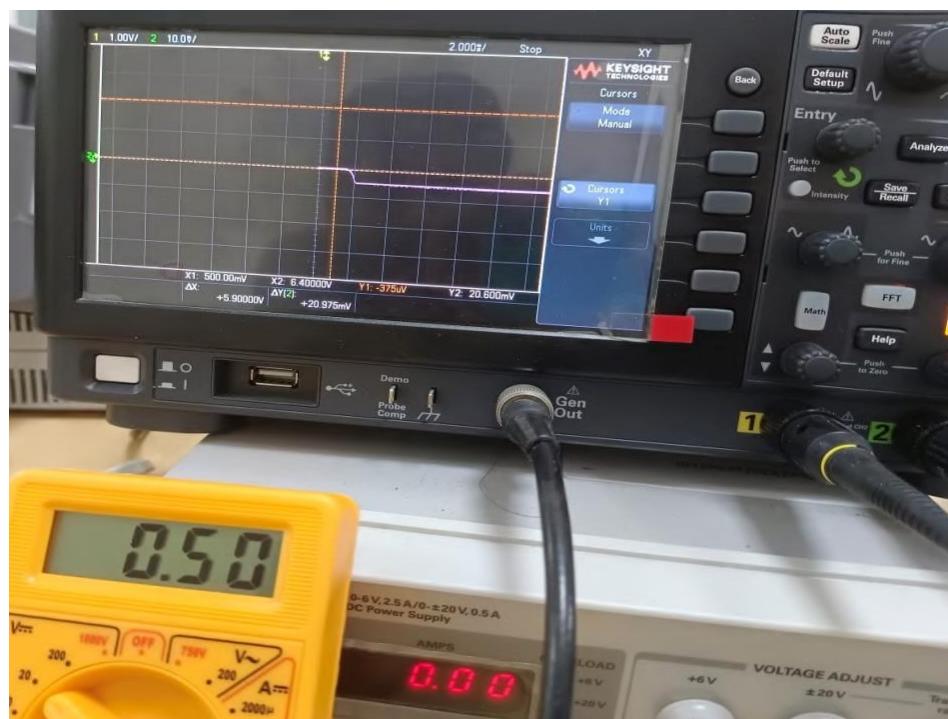


(VGS=500 mV)

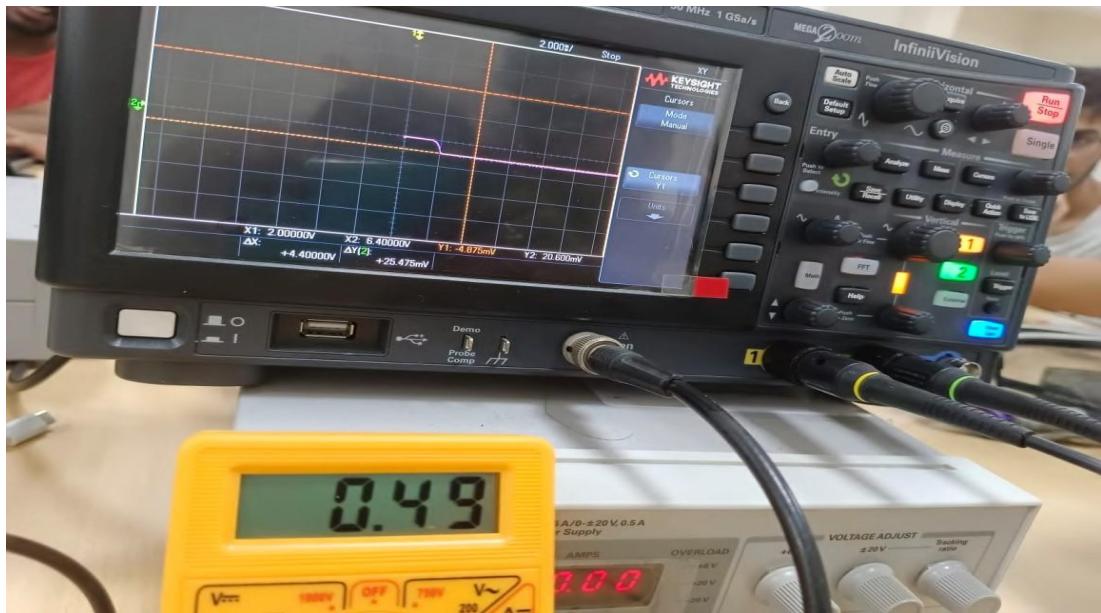


For VDS=0.5V:

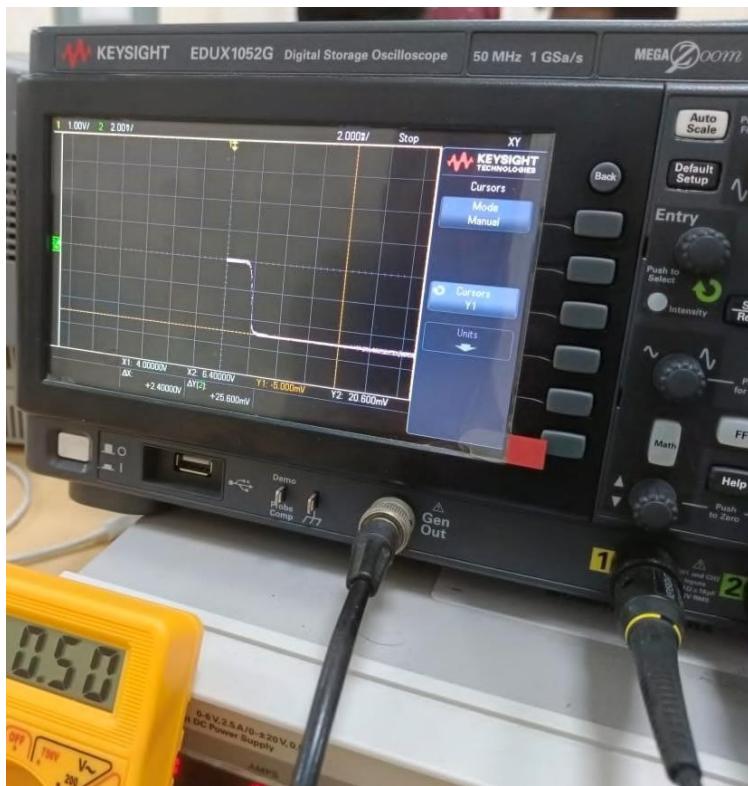
(VGS=500mV)



(VGS=2V)

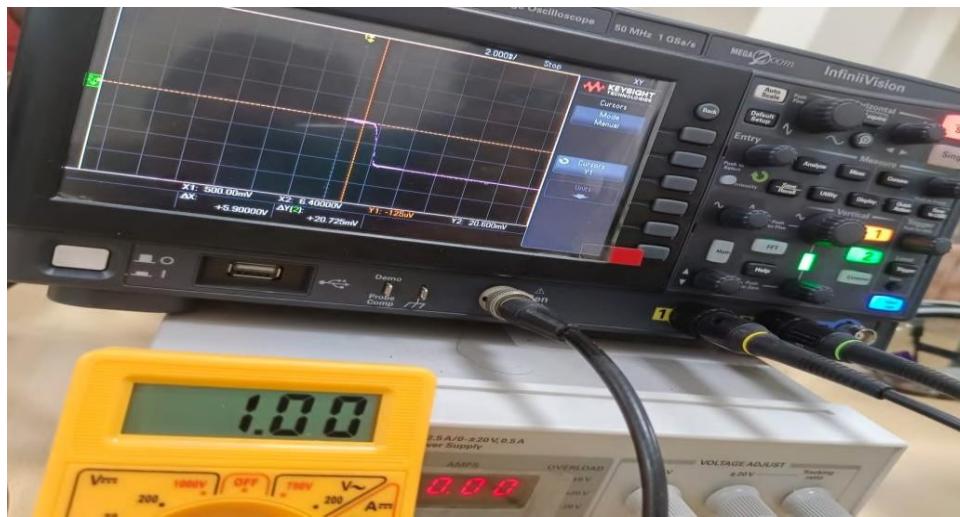


(VGS=4V)

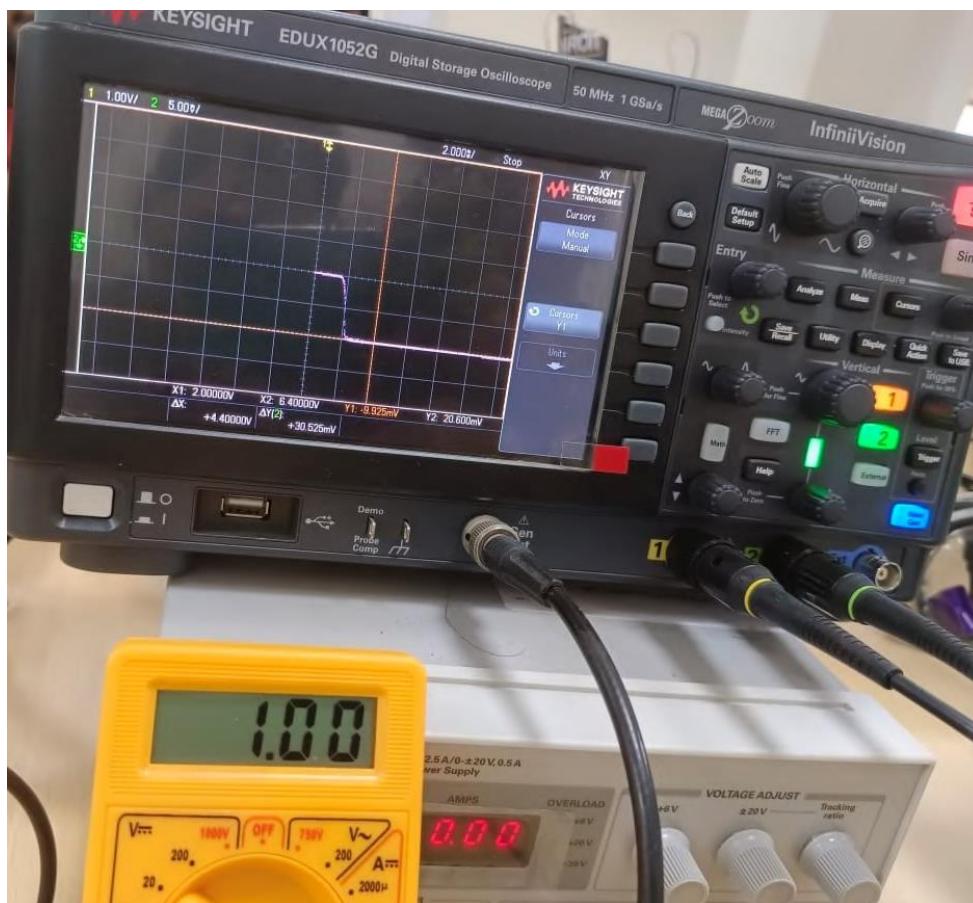


For VDS=1V

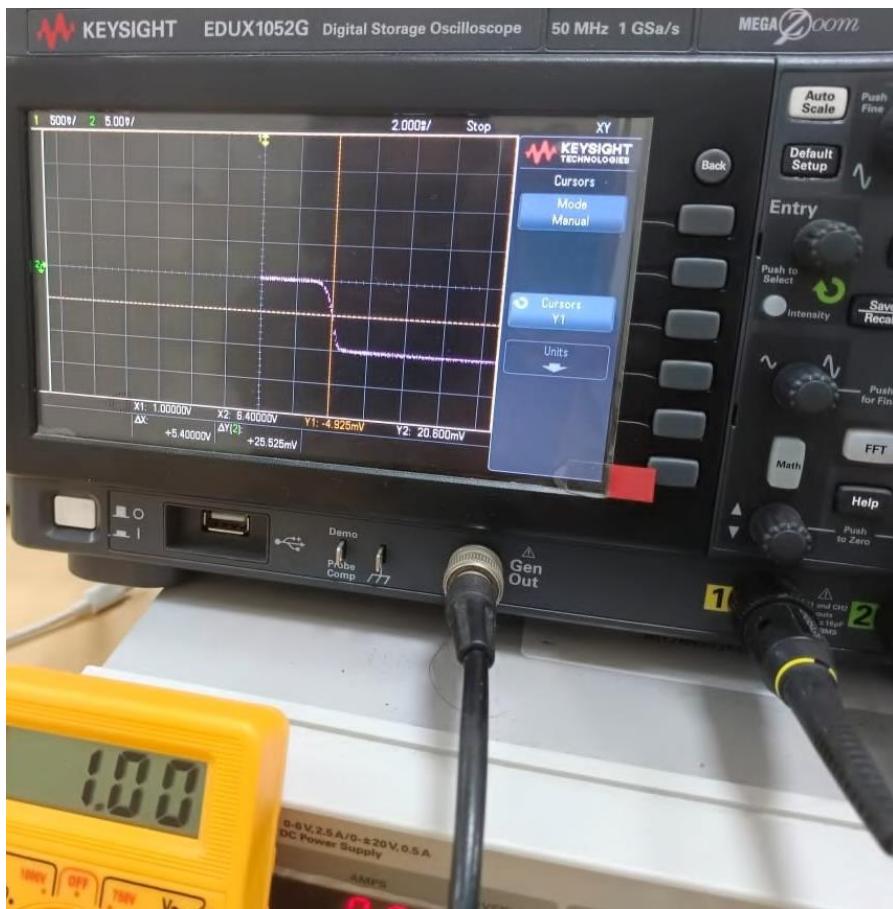
(VGS=500mV)



(VGS=2V)

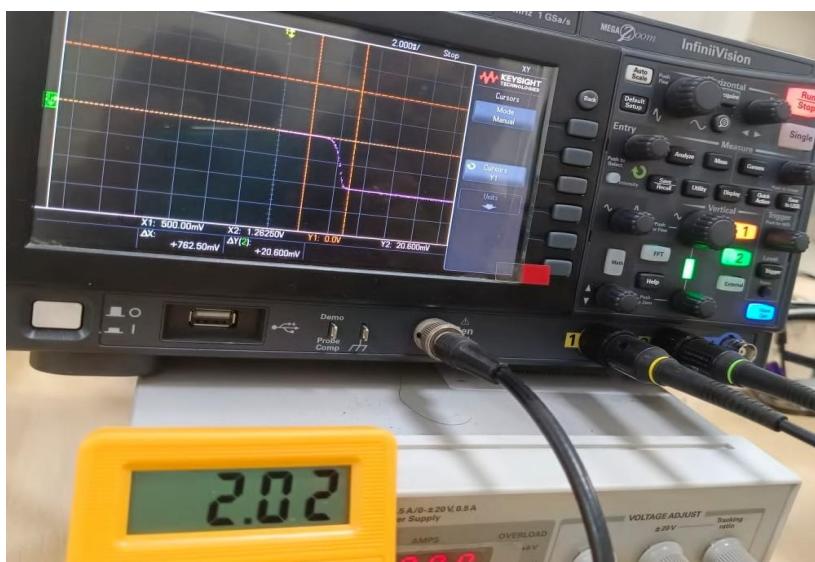


(VGS=1V)

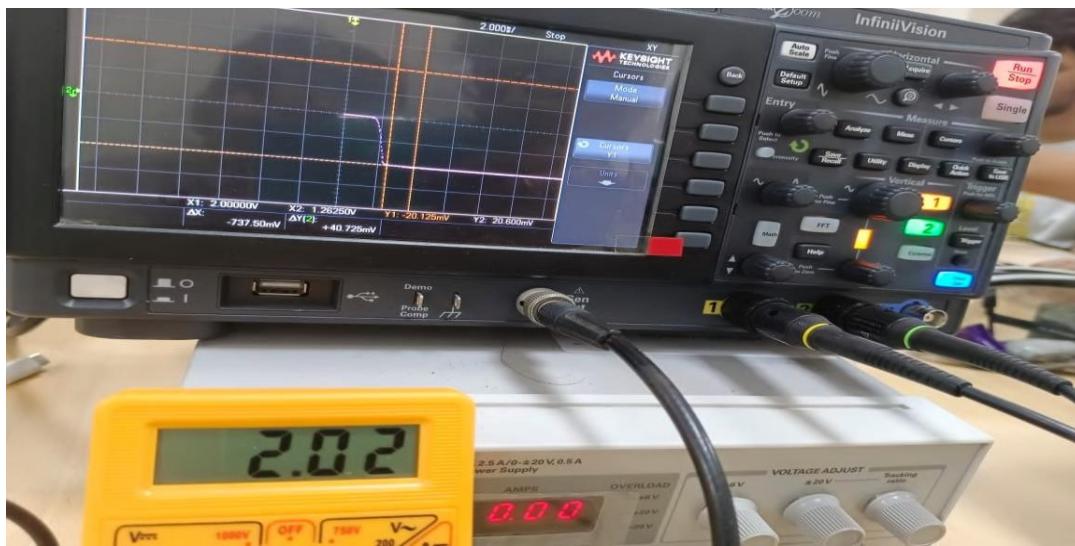


**FOR VDS=2V**

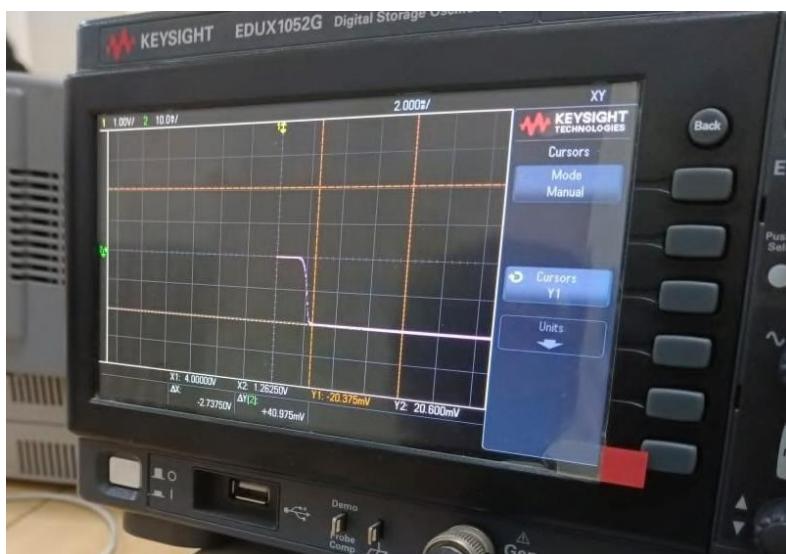
**(VGS=500mV)**



(VGS=2V)

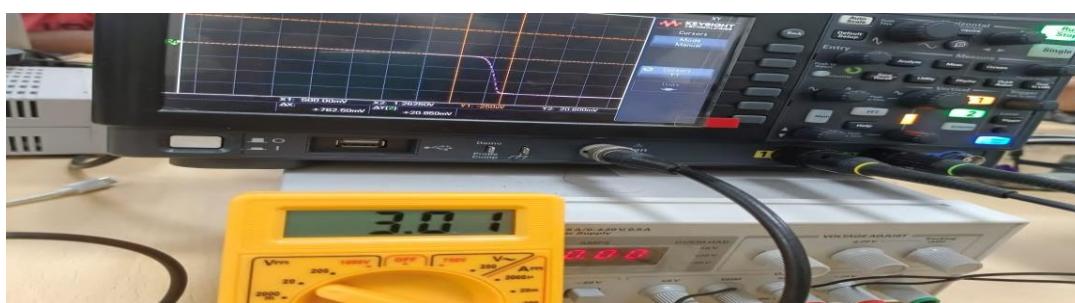


(VGS=4V)

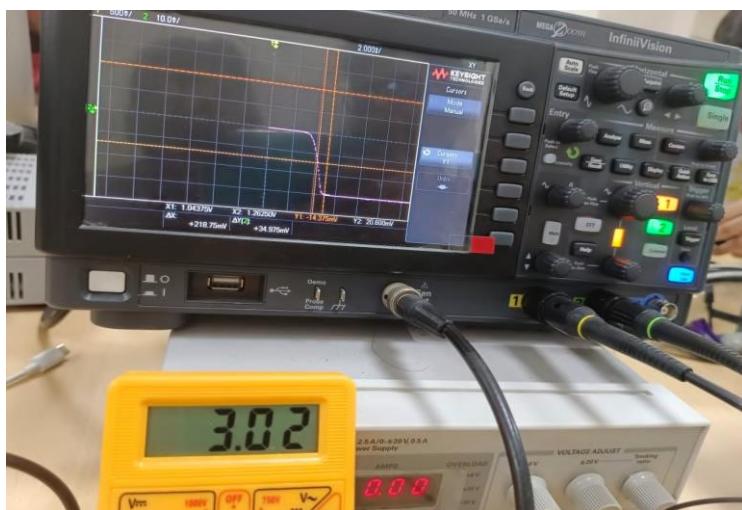


For VDS=3V

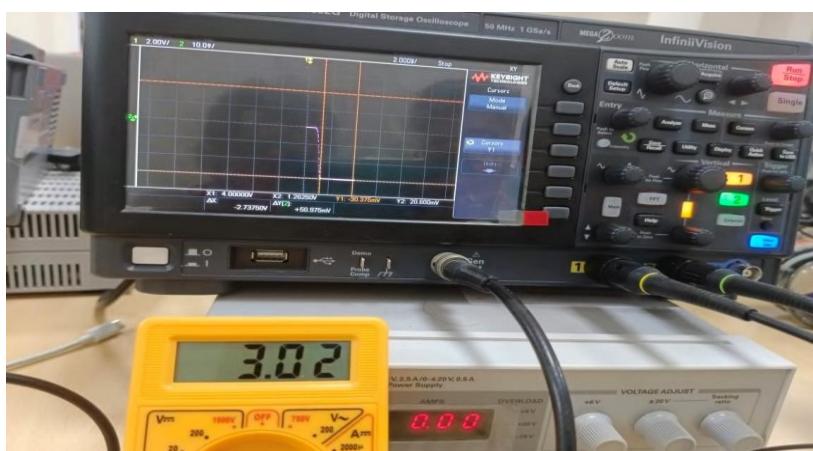
(VGS=500mV)



(VGS=1V)



(VGS=4V)

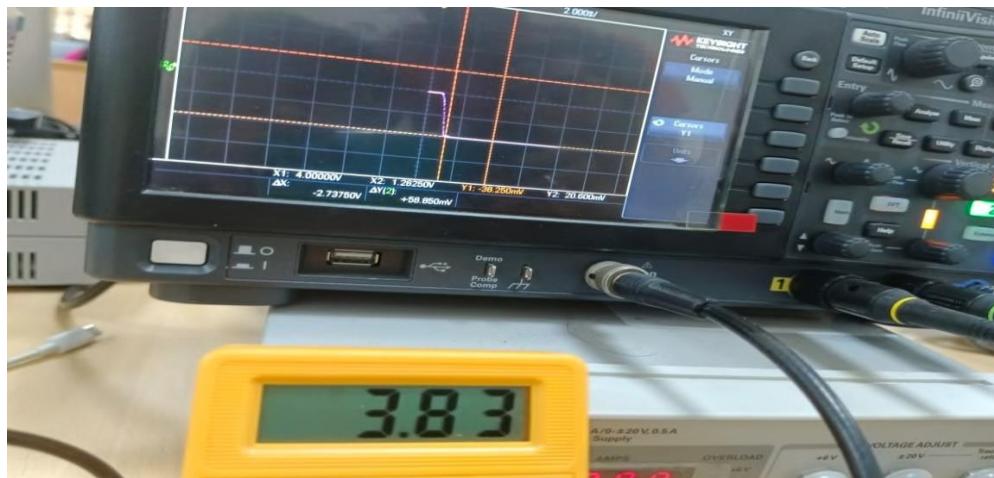


For VDS=4V

(VGS=1V)



(VGS=4V)



VDS	VGS	Vo	I
0.1	775mV	-500uV	0 A
0.1	1.5V	-1.5mV	-1.5uA
0.2	675mV	-200uV	0 A
0.2	2V	-2mV	-2uA
0.5	500mV	-375uV	0 A
0.5	2V	-4.875mV	-4.875uA
0.5	4V	-5mV	-5uA
1	500mV	-125uV	0 A
1	2V	-9.925mV	-9.925uA
1	1V	-4.925mV	-4.925uA
2	500mV	0V	0A
2	2V	-20.125mV	-20.125uA
2	4V	-20.375mV	-20.375uA
3	500mV	-250uV	0 A
3	2V	-30.125mV	-30.125uA
3	1V	-14.375mV	-14.375uA
3	4V	-30.375mV	-30.375uA
4	1V	-20.750mV	-20.750uA
4	2	-38.250mV	-38.250uA
4	4	-38.500mV	-38.500uA

b)

To determine the threshold voltage (VT), we examine the maximum slope of the curve.

This occurs at the point (VGS, VOUT) = (2, -1.95).

By considering the points (2, -1.95) and (1.95, -2), we calculate the approximate slope to be -1.8V.

The next step involves drawing a tangent at the point of maximum slope and determining its intersection with the x-axis (VGS). This intersection point represents the threshold voltage (VT). Therefore, in this case, the threshold voltage is approximately 0.75V.

c)

Given the following known parameters:

$$VDS = 0.1V$$

$$VGS = 2V$$

$$Vout = -1.95V$$

$$VT = 0.75V$$

$$ID \approx 2mA$$

To determine the mode of operation of the MOSFET, we calculate:

$$VGS - VTH = 2 - 0.75 = 1.25V$$

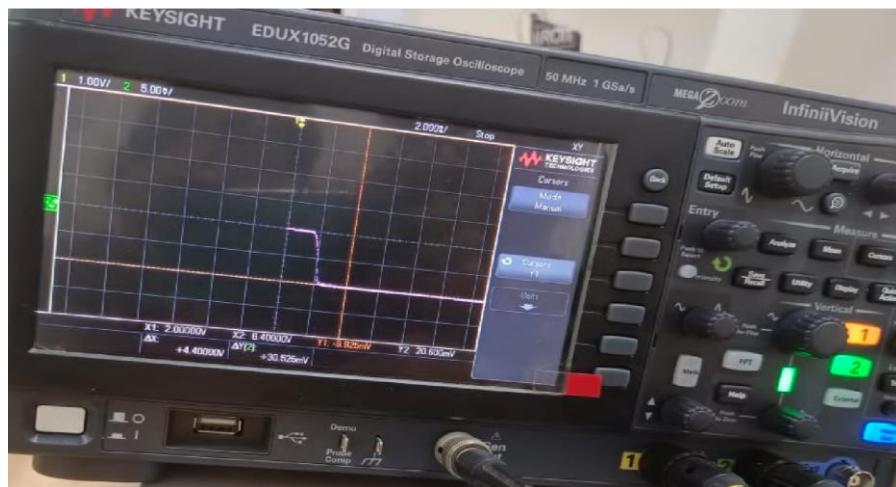
Since VDS is less than 1.25V, the MOSFET is operating in the triode or linear region.

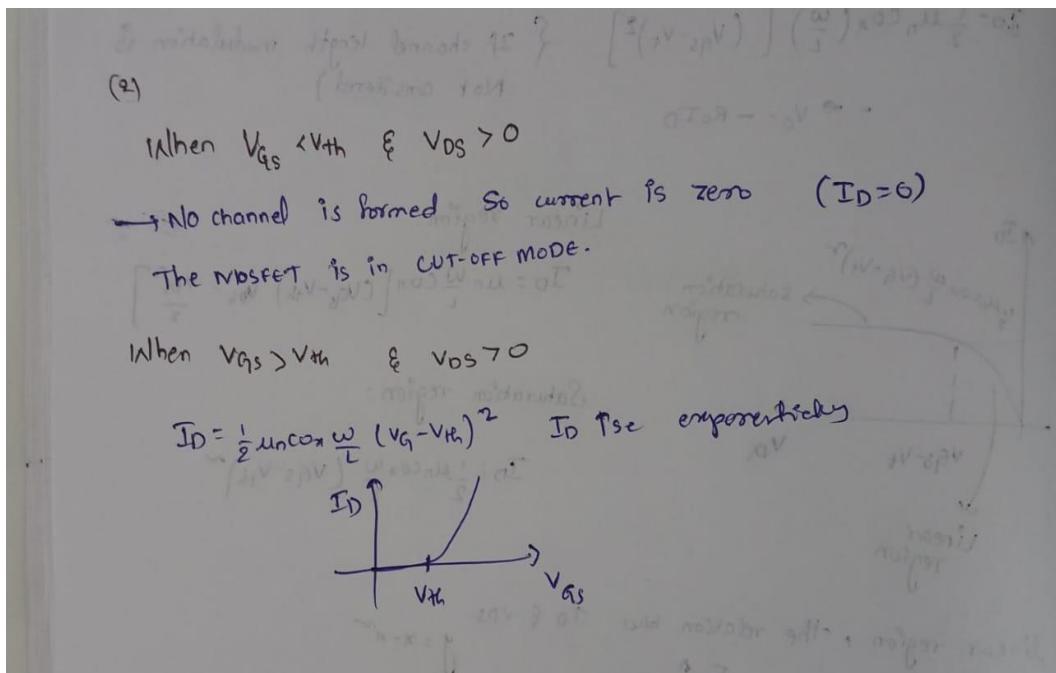
To further analyze the MOSFET's behavior, we can utilize the characteristic equation:

$$I_D \approx \mu C_{ox} \frac{W}{L} (V_{GS} - V_T) V_{DS}$$

$$ID = (\mu nCox/2) * [(VGS - VTH) * VDS - (VDS^2 / 2)]$$

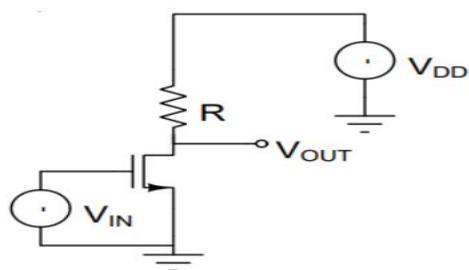
Using the above equation we got  $\mu nCox(W/L) = 18 mS/V$





### 3) Large signal Analysis and other Voltage Transfer Characteristics of MOS based Amplifier :

Consider the NMOS based amplifier with a resistive load as shown below:

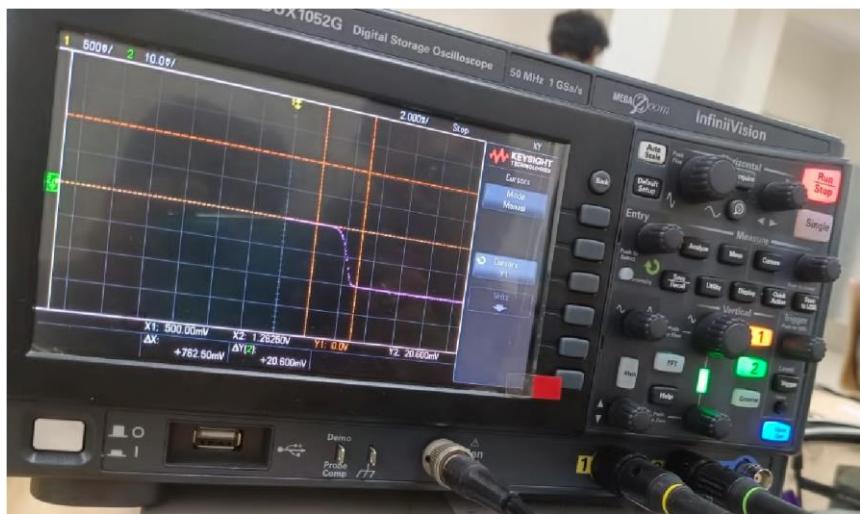


#### Modes of Operation of MOSFET:

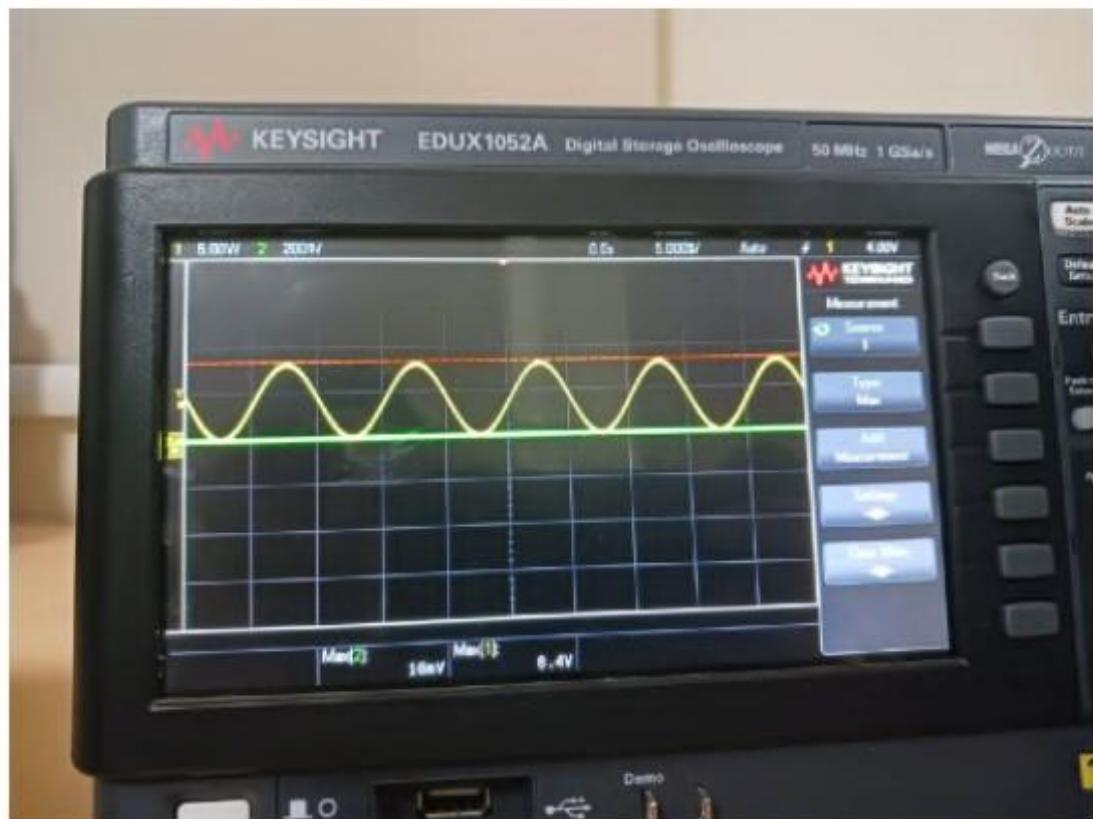
$V_{in} = 500\text{mV}$  => cut off mode

$V_{in} = 2.5\text{v}$  => saturation mode

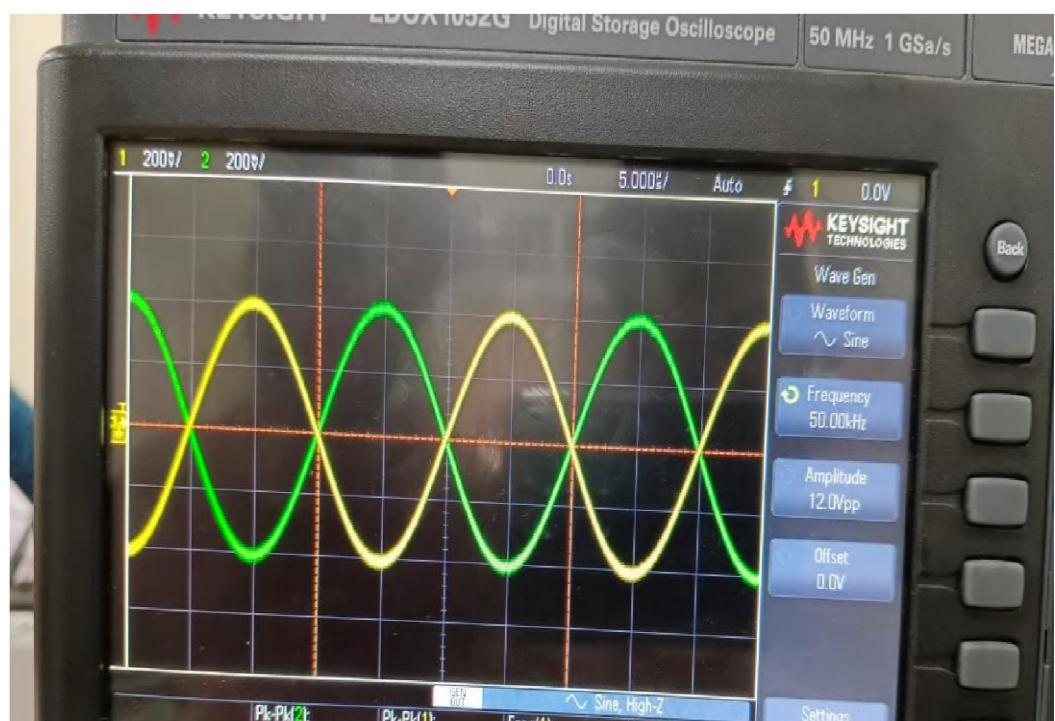
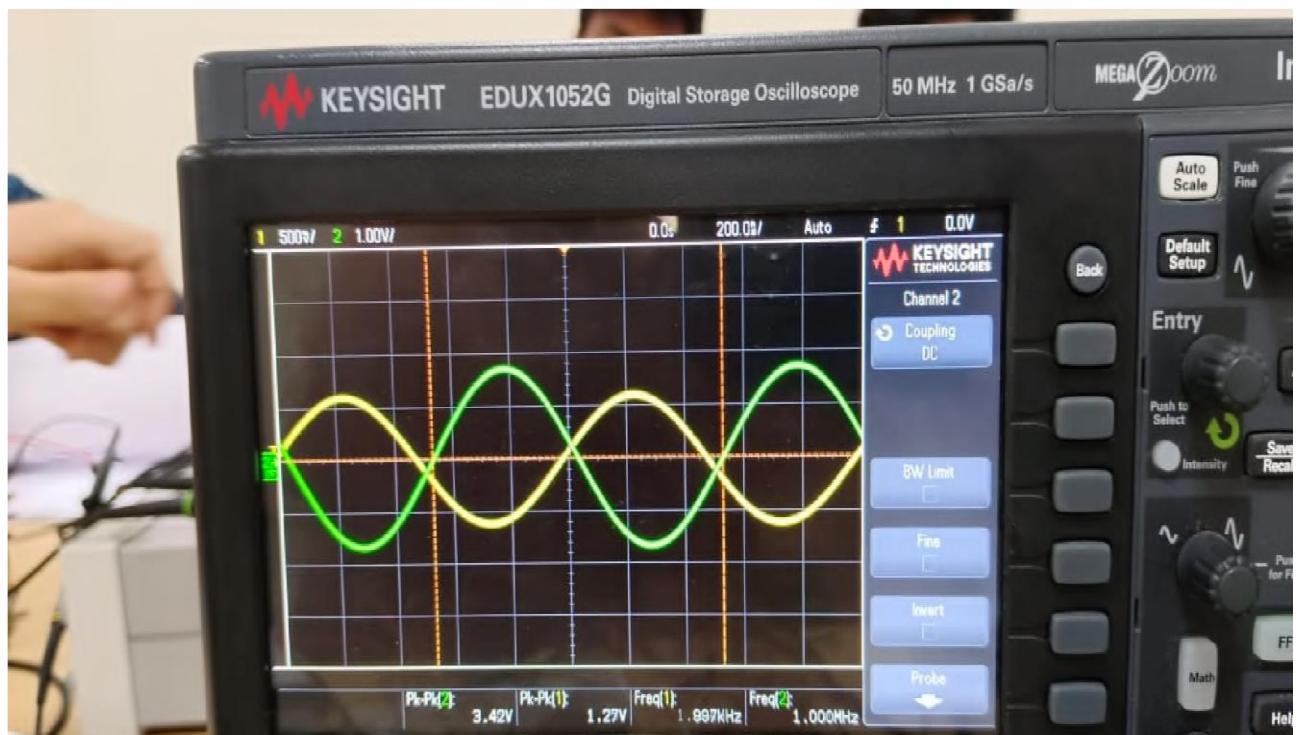
$V_{in} = 4\text{v}$  => Linear/Triode mode



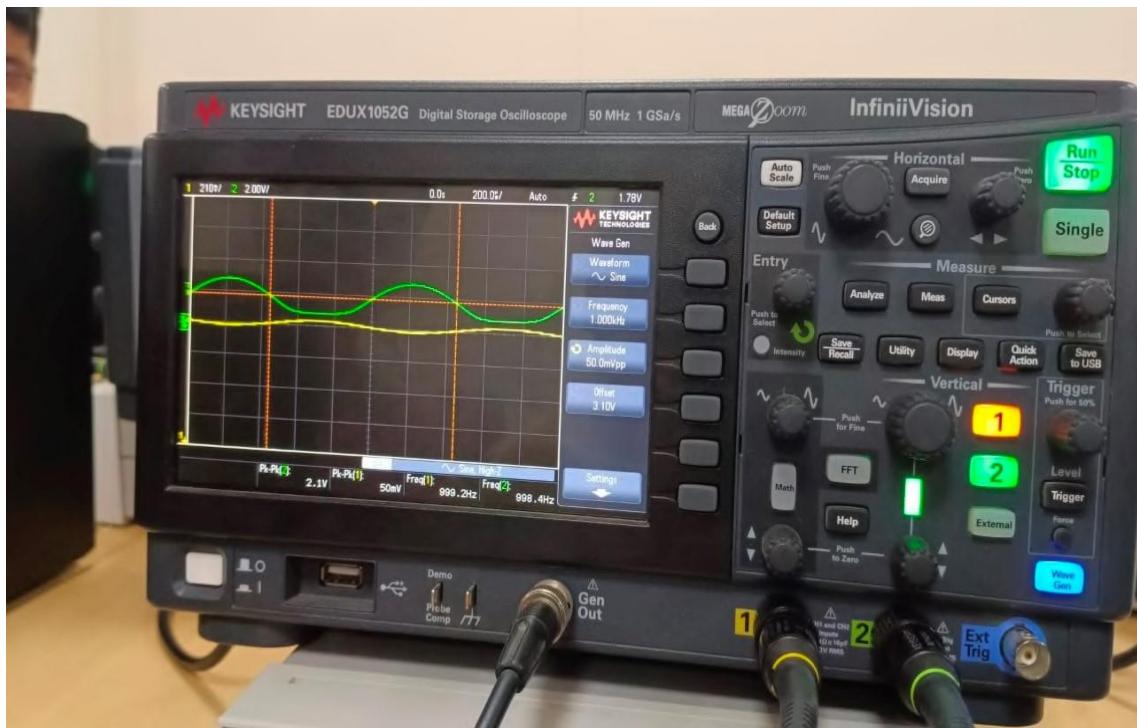
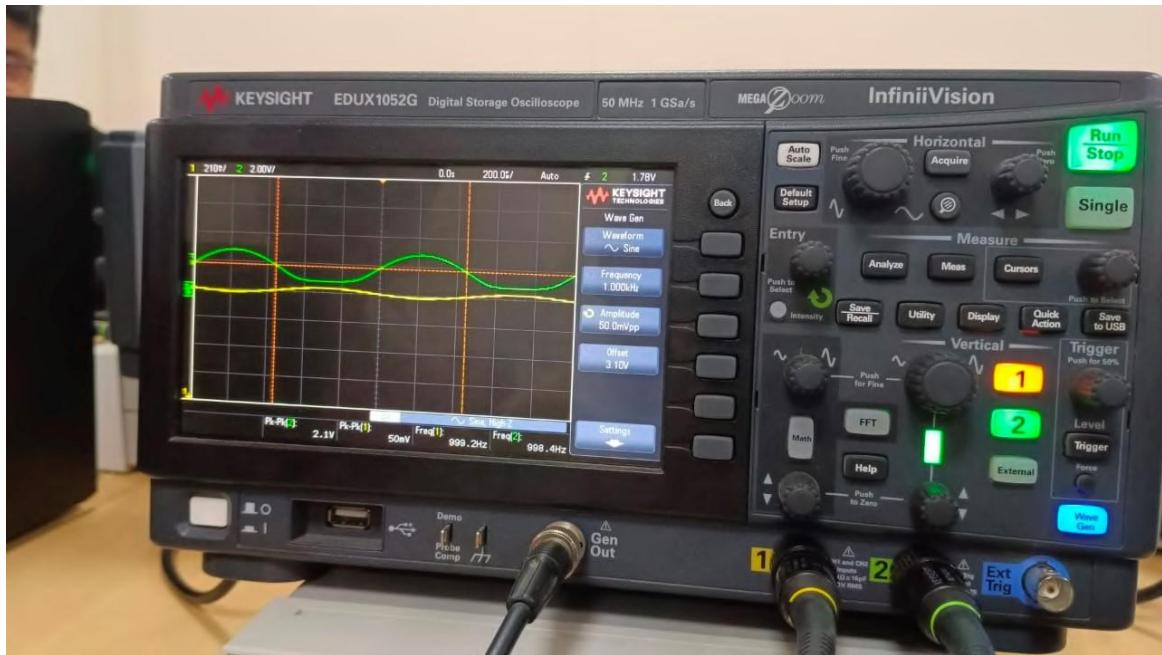
At Vin=500mV



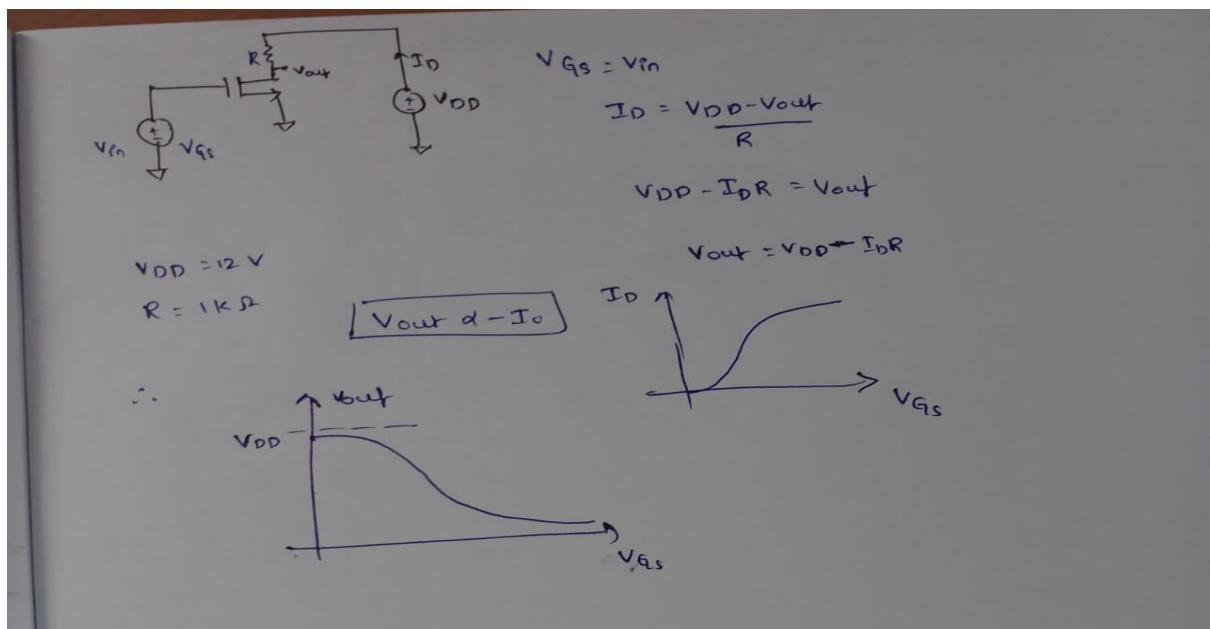
At Vin=2.5mV



At Vin=4V



MODE	VDS	Vin	Vout	Gain
<b>Cutoff-mode</b>	500mv	40mv	22mv	~0.5
		120mv	15mv	0.125
		1v	40mv	0.04
		500mv	16mv	0.032
<b>Linear/Triode</b>	4v	40mv	21mv	~0.5
		19.7mv	19mv	0.96
		120mv	45mv	0.375
		500mv	120mv	0.24
		1v	300mv	0.3
<b>saturation</b>	2.5	27mv	38mv	1.407
		120mv	155mv	1.2917
		570mv	765mv	1.34
		1 V	1.42V	1.42



When the input voltage ( $V_{in}$ ) is significantly smaller than  $2(V_{GS}-V_{TH})$  and much smaller than  $V_{DS}$ , we can observe a proper gain in the MOSFET.

However, when  $V_{in}$  becomes comparable to  $V_{DS}$ , the MOSFET enters the triode mode on one side of the operational point.

As a result, the gain is not uniform and varies. This occurs because the MOSFET's behavior changes as the input voltage crosses the operational point, leading to non-uniform amplification characteristics.

Gain is greater than 1 only in saturation region.

MOSFET acts as closed switch in cut off region. MOSFET acts as an amplifier only in Saturation region because a voltage dependent current source can be obtained in this region. MOSFET acts as a voltage dependent resistor in Linear region.