

## Analog Electronic Circuits Lab Report - Experiment 9

**Name:** [Chanda Akshay Kumar]

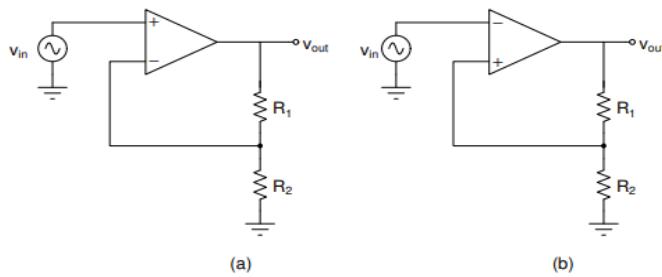
**Roll No:** [2024102014]

**Teammate:** [S V Santhosh Yadav]

**Roll No:** [2024102054]

### Experiment 9: Op-Amp Circuits

#### 1. Voltage Transfer Characteristics (VTC) for Op-Amp in Negative and Positive Feedback Configurations



#### a) Identifying Feedback Type

- **Figure (a):** Negative feedback configuration because the output is connected to the inverting input, causing a fraction of the output to subtract from the input.
- **Figure (b):** Positive feedback configuration because the output is fed back to the non-inverting input, reinforcing the input signal by this output voltage is increased.

#### b) Plotting VTC ( $V_{out}$ vs $V_{in}$ )

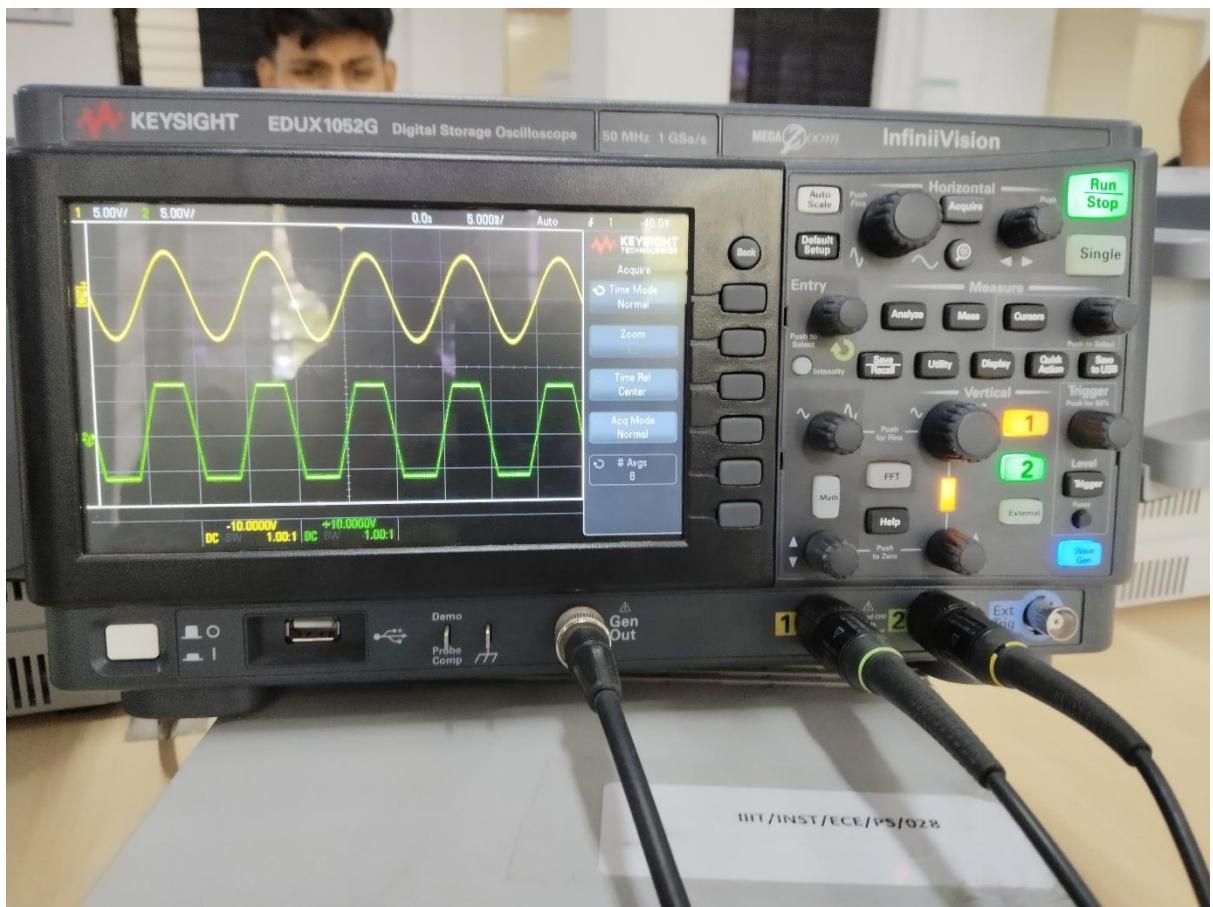
- **Circuit Setup:**

- Resistors:  $R_1=R_2=10\text{ k}\Omega$
- Supply Voltages:  $\pm 8\text{ V}$
- Input: Sine wave,  $V_{in}=\pm 12\text{ V}_{pp}, 100\text{ Hz}$

- **Observations:**

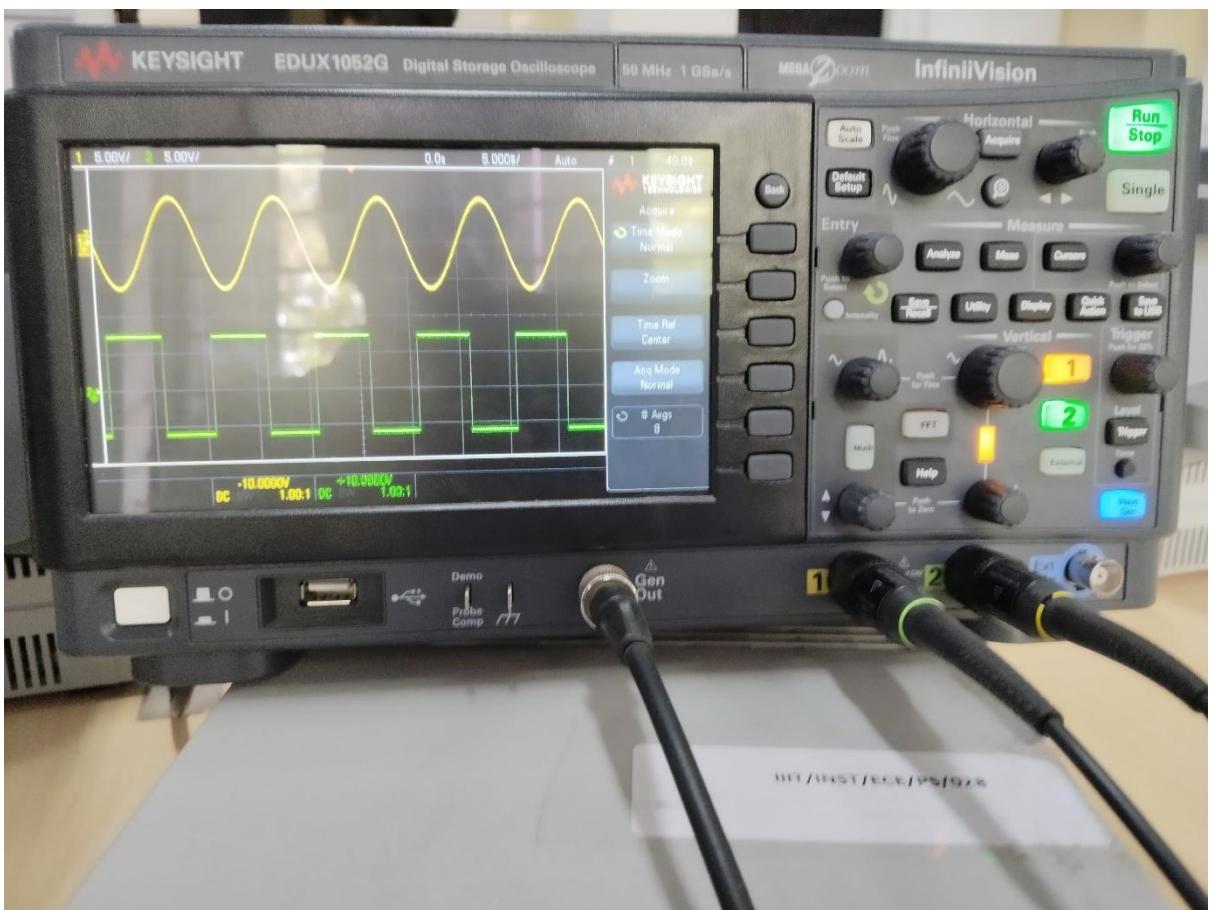
- **Negative Feedback:**

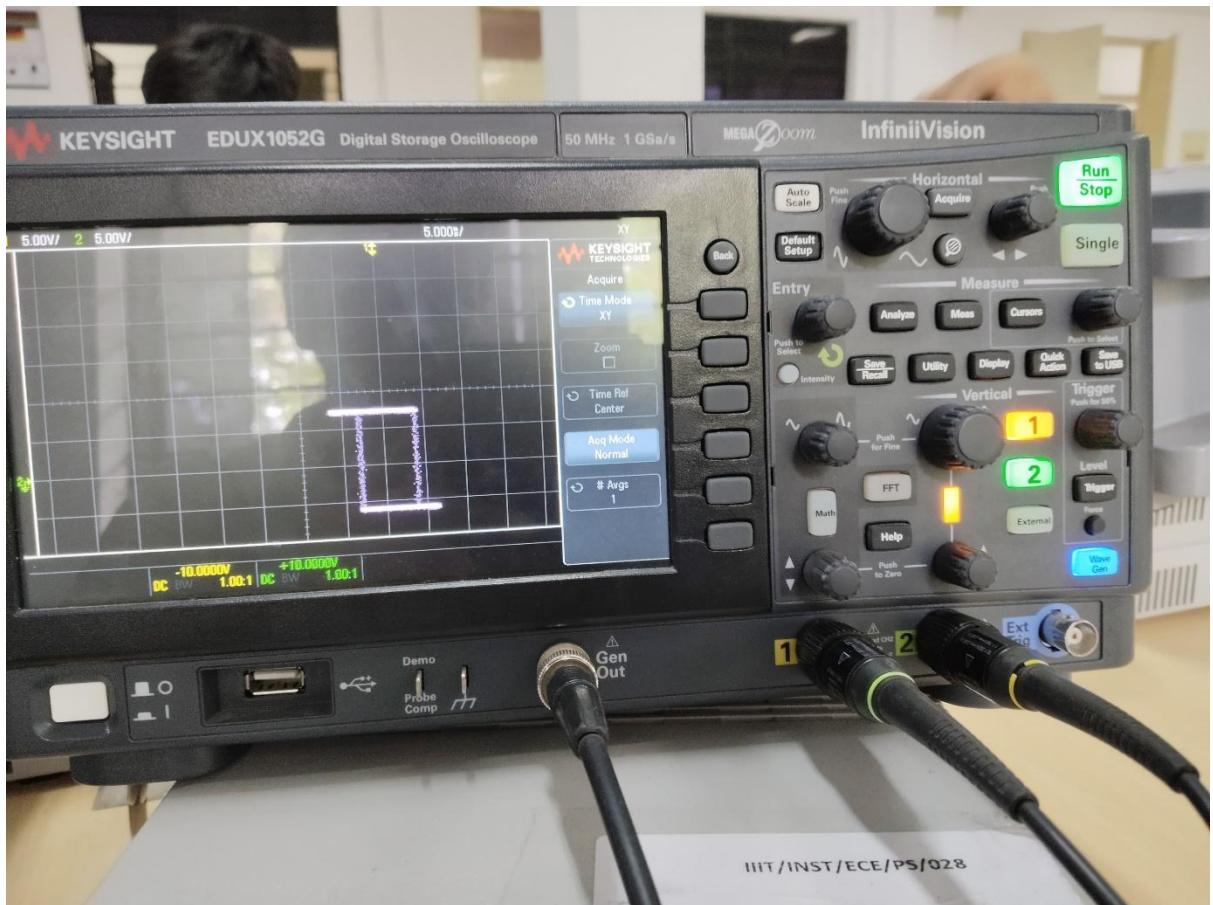
- Output follows input linearly until saturation.
- Smooth transition between positive and negative saturation.



- **Positive Feedback:**

- Output exhibits hysteresis (sudden jumps between  $+VDD$  and  $-VDD$ ).
- Output remains latched at one extreme until input crosses a threshold.

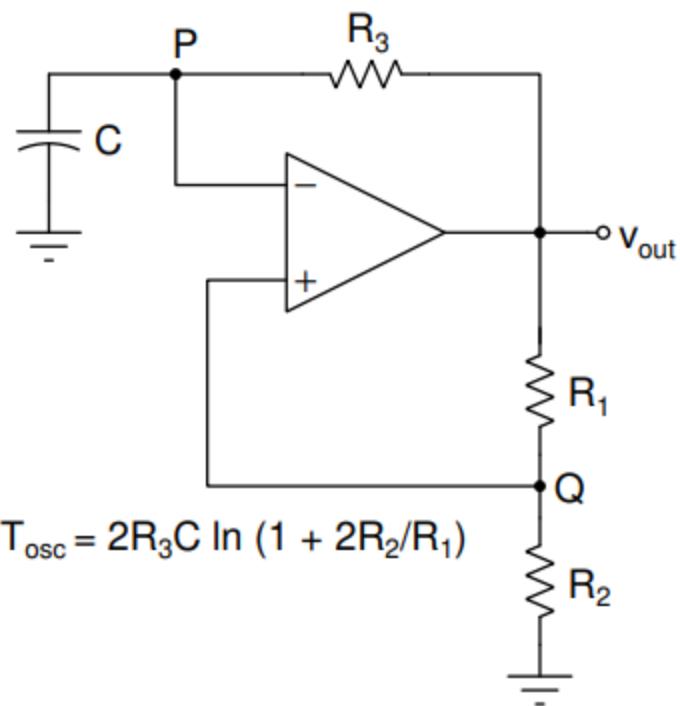




### c) Regeneration/Hysteresis

- **Positive Feedback:** Shows hysteresis because the output reinforces input changes, causing rapid switching between saturation levels. Useful in oscillators and Schmitt triggers.
- the op-amp output is at one extreme, such as the positive supply voltage VDD. As the input voltage crosses the upper threshold, the positive feedback causes a rapid switch in the output to the opposite extreme, such as the negative supply voltage -VDD. With the output now at the opposite extreme, the input voltage must drop below the lower threshold for the output to switch back to the original extreme. This hysteresis characteristic enables the Op-amp positive feedback circuit to provide stable and noise-tolerant switching behaviour.
- The positive feedback reinforces the input signal, resulting in the output regenerating and transitioning to a new state once the input voltage crosses the thresholds.
- **Negative Feedback:** No hysteresis; stabilizes output by counteracting input variations. Used in amplifiers for linear operation.

## 2. RC Oscillator (Positive Feedback Example)

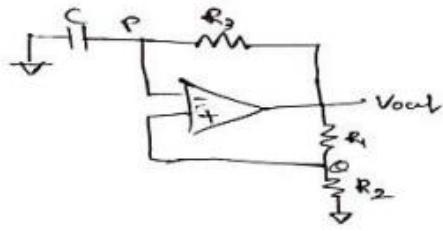


### a) Theoretical Frequency Calculation

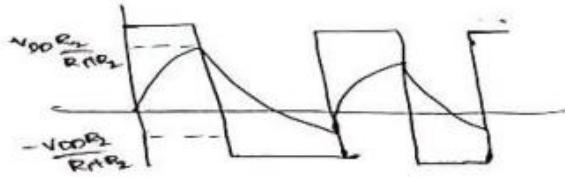
Given:

- $R_1=R_2=10\text{ k}\Omega$
- $R_3=1\text{ k}\Omega$
- $C=1\text{ }\mu\text{F}$

Formula:



$$T_{osc} = 2R_3C \ln(1 + 2R_2/R_1)$$



$$P_C = i R_3$$

$$CD \frac{dV_P}{dt} = \frac{V_{out} - V_P}{R_3}$$

→ for +ve cycle,

$$\int \frac{dt}{R_3 C} = \int \frac{dV_P}{V_{out} - V_P} \quad V_{out} = V_{DD}$$

$$\begin{aligned} \frac{t}{R_3 C} &= \int_{\frac{-VDD R_2}{R_1 + R_2}}^{\frac{VDD R_2}{R_1 + R_2}} \frac{dV_P}{V_{out} - V_P} \\ &= \ln(V_{out} - V_P) \Big|_{\frac{-VDD R_2}{R_1 + R_2}}^{\frac{VDD R_2}{R_1 + R_2}} \\ &= \ln\left(\frac{R_1}{R_1 + 2R_2}\right) \end{aligned}$$

$$T = R_3 C \ln\left(1 + \frac{2R_2}{R_1}\right)$$

→ for -ve & +ve cycle (one period)

$$T = 2R_3 C \ln\left(1 + \frac{2R_2}{R_1}\right)$$

$$T_{osc} = 2R_3 C \ln(1 + 2R_2/R_1)$$

$$\rightarrow T_{osc} = 2 \times 1k \times 1\mu \ln(1+2) = 2.197 \text{ ms} \rightarrow f_{osc} = 1/T_{osc} = 455.12 \text{ Hz}$$

$$\begin{aligned}
 @) T &= 2R_3 C \cdot \ln \left( 1 + \frac{2R_2}{R_1} \right) \\
 &= 2(1\text{K})(10^{-6}) \cdot \ln \left( 1 + \frac{2(10\text{K})}{(10\text{K})} \right) \\
 &= 2(1\text{K})(10^{-6}) \cdot \ln(3)
 \end{aligned}$$

$$T = 0.002197224 \text{ sec}$$

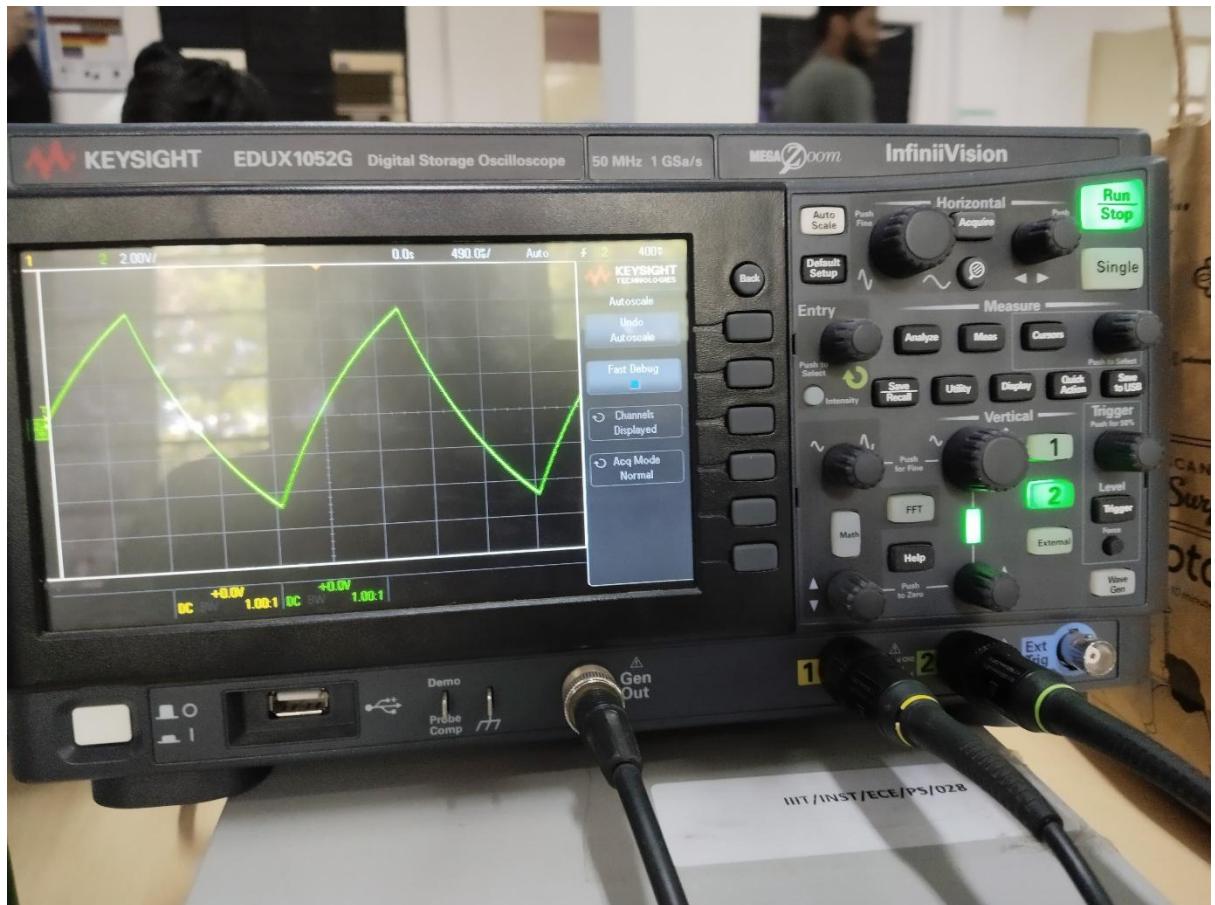
$$f = \frac{1}{T} = \frac{1}{0.002197224}$$

$$f = 455.1199$$

### b) Measured Results

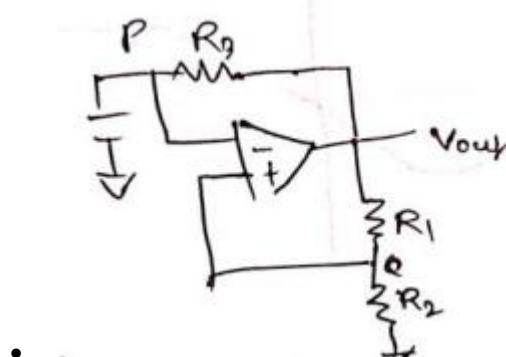
- **Observed Frequency:** 441.03 Hz
- **Comparison:** Close to theoretical value (455.12 Hz). Minor deviation due to component tolerances and other non-ideal reasons.

Plot of VP:



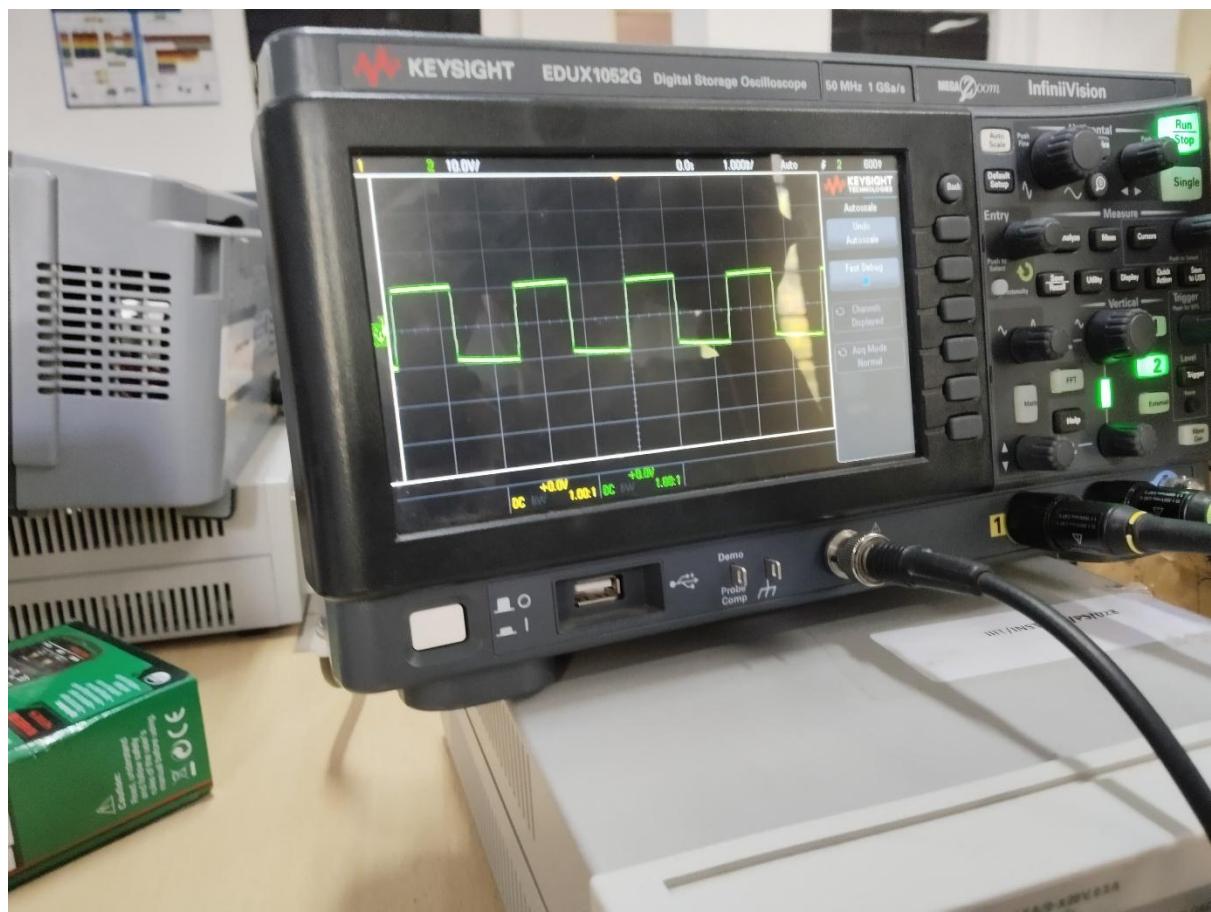
## Why Positive Feedback?

- The RC network introduces phase shift, and positive feedback ensures sustained oscillations by reinforcing the signal.



- Here if  $V_{out}$  changes suddenly  $V_p$  also changes and which is connected to Non inverting terminal
- But  $V_p$  is changing as capacitor is charging and discharging
- By this some fraction is adding to differential input of op-Amp when the input is +ve feedback

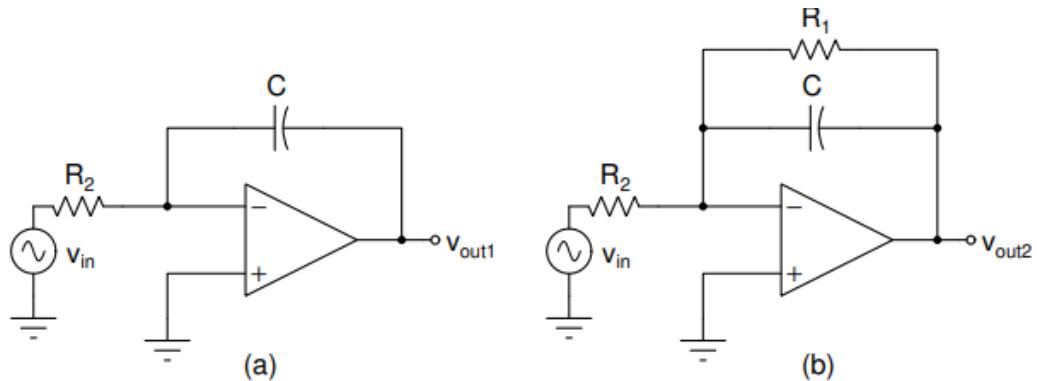
Plot of Vout:



Plot of VQ:



### 3. Integrator (Negative Feedback Example)

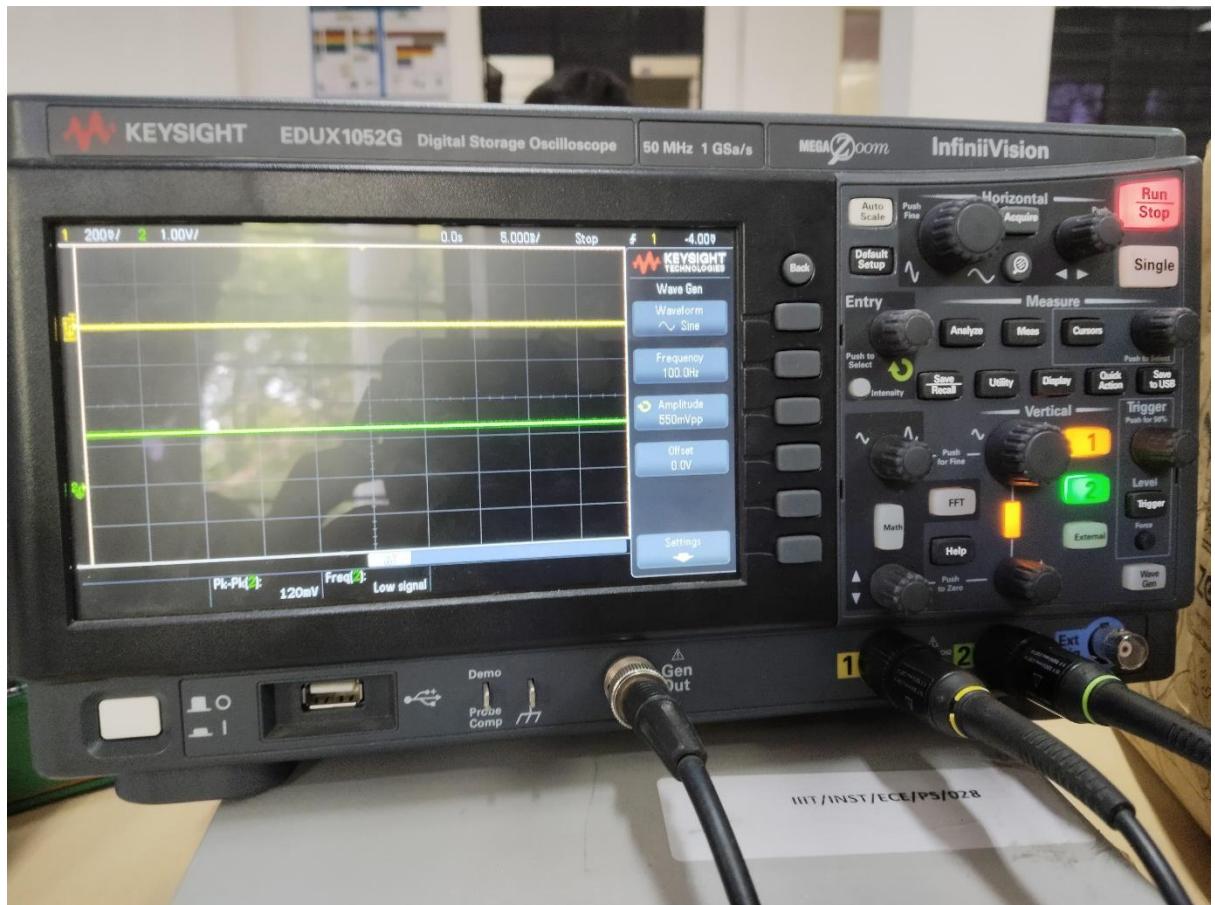


Connecting the circuit above shown and  $C = 10\text{nF}$

And  $R_1=10\text{Kohm}$  and  $R_2 = 1\text{kohm}$

#### a) Output Saturation with DC Input ( $V_{in} = 0V$ )

- Observation:** Output saturates to  $+VDD$  or  $-VDD$  due to op-amp DC offset.



- Integrator continuously accumulates input offset, driving output to saturation.
- In this part of the experiment, the input voltage  $v_{in}$  is kept at a constant 0V. However, due to the inherent DC offset of the Op Amp, the output voltage will continuously increase until the Op Amp reaches saturation

### b) Preventing Saturation with Parallel Resistor (R1)

- **Observation:** Output does not saturate.
- **Reason:** Resistor R1 limits gain at DC, turning the circuit into an inverting amplifier after capacitor charges fully.
- At steady state ( $t = \infty$ ), gain for DC-offset is  $1+R1/R2$
- capacitor gets fully charged, resistor makes the circuit to act as an Inverting amplifier in closed loop configuration

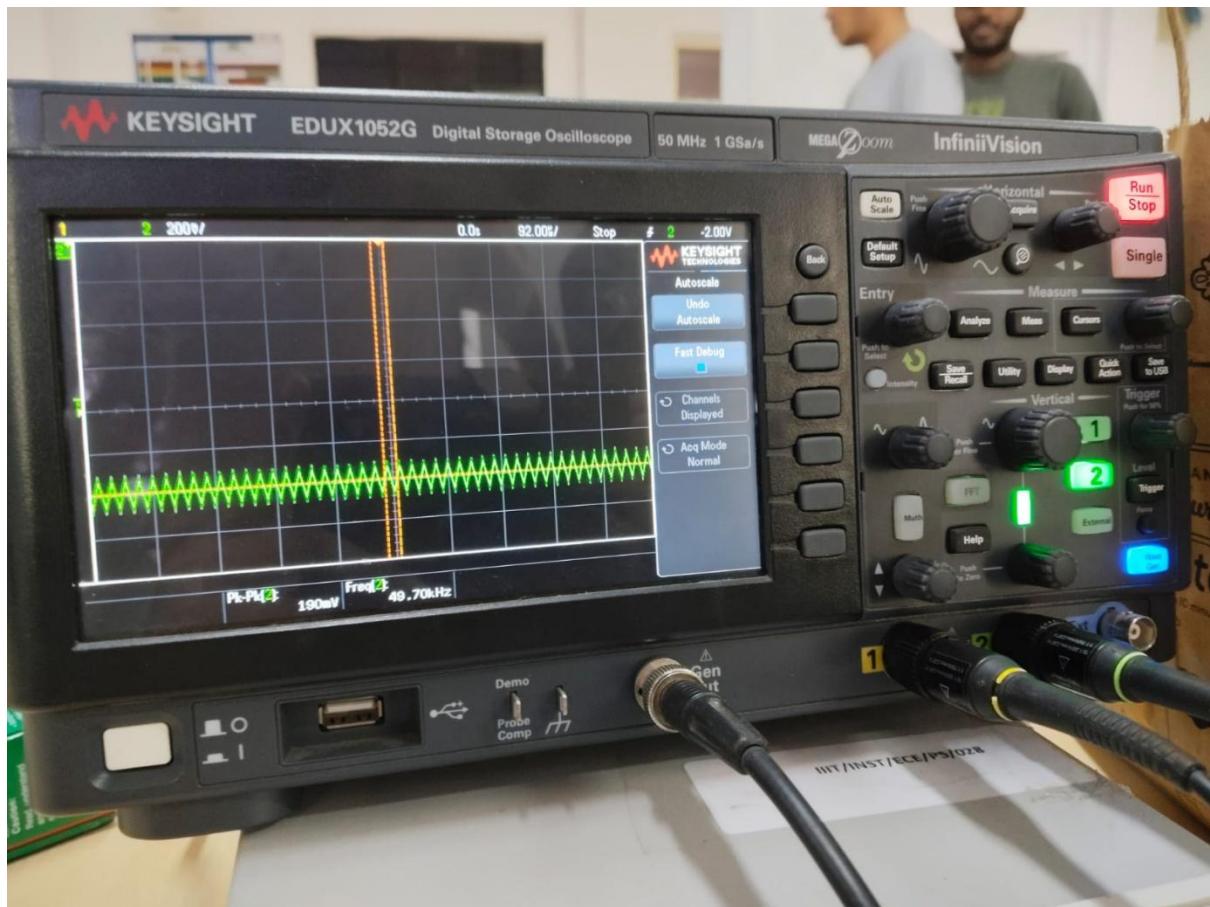
To prevent the op-amp from saturating, a resistor  $R_1$  (with  $10\text{ k}\Omega$ ) is connected across the capacitor in circuit.

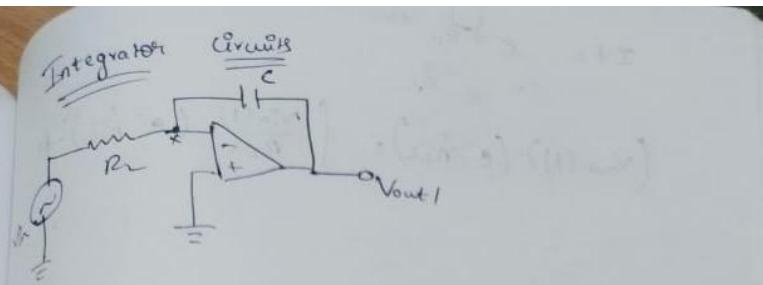
- The resistor avoids excessive voltage build-up & ensures the op-amp operates within its *linear range*.

From the above plot, it is evident that op-amp has not reached saturation. This is due to presence of resistor  $R_1$ , which maintains the negative feedback loop even after capacitor is fully charged.

### c) Integrator Action with Square Wave Input

- **Input:** 0 (low) and 500 mV (high), 50 kHz square wave.
- **Output:** Triangular wave (integrated signal).
- **Verification:**
  - Rising input → Negative ramp output.
  - Falling input → Positive ramp output.





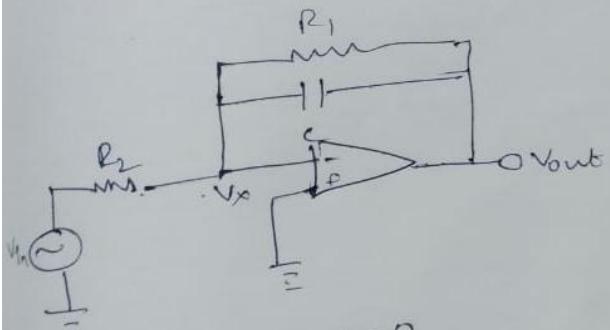
$V_+ = 0 \Rightarrow V_- = 0$  (Approximated because  
out is very higher than  
let us apply KCL at node X)

$$\Rightarrow \frac{V_{in}}{R_L} = -C \left( \frac{d(V_{out})}{dt} \right)$$

$$\Rightarrow \frac{dV_{out}}{dt} = -\frac{1}{R_L C} V_{in}$$

$$\Rightarrow V_{out} = -\frac{1}{R_L C} \int V_{in}$$

$\Rightarrow$  The above circuit acts  
as an integrator circuit



$$V_+ = 0 \Rightarrow V_X = 0$$

$$\Rightarrow C \frac{dV_{out}}{dt} + \frac{V_{out}}{R_1} = \frac{V_{in}}{R_2}$$

$$\frac{dV_{out}}{dt} = \frac{V_{out}}{R_1 C} = \frac{V_{in}}{R_2 C}$$

$$I \cdot t = e^{\int \frac{1}{R_1 C} dt} \\ = e^{-\frac{t}{R_1 C}} \\ (V_{out}(t)) (e^{-\frac{t}{R_1 C}}) = \int \frac{V_{in}(t)}{R_2 C} (e^{-\frac{t}{R_1 C}}) dt$$

for square wave

$$V_{out} = -\frac{1}{R_2 C} \int \frac{A}{2} dt \text{ +ve cycle}$$

$$= \left( \frac{-A}{2 R_2 C} \right) +$$

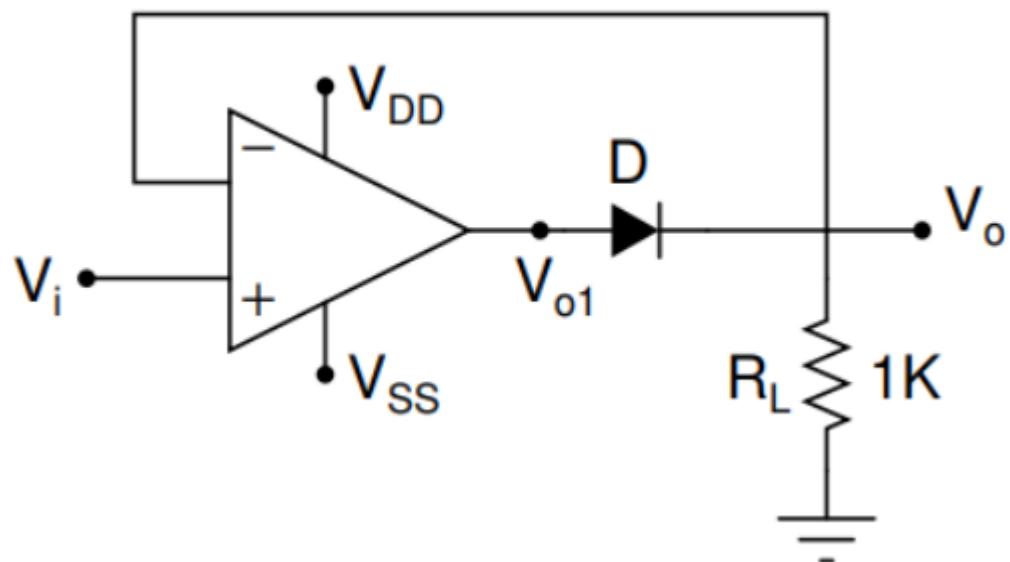
$$V_{out} = -\frac{1}{R_2 C} \int \frac{A}{2} dt \text{ -ve cycle}$$

$$V_{out} = \frac{A}{2 R_2 C} t$$

$\rightarrow$  DC offset  
 $\approx 500m(\tau/2) + o$   
 ↗ Triangular curve  
 $\rightarrow$  we got Integrator.

#### 4. Precision Half-Wave Rectifier (Negative Feedback Example)

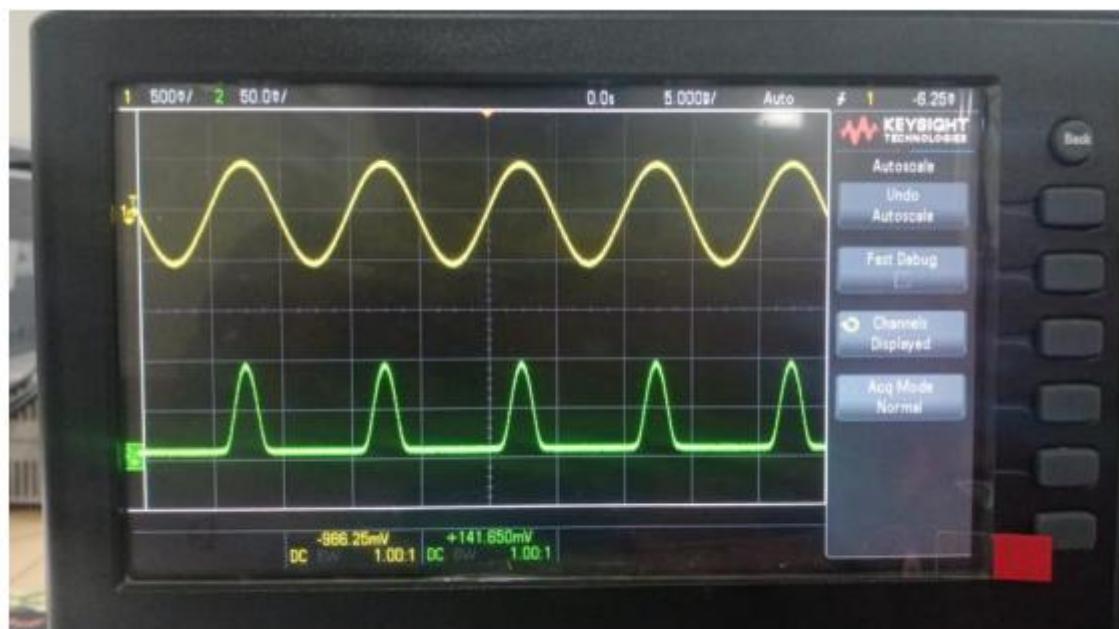
##### a) Circuit Verification



- **Input:** 1 V peak, 100 Hz sine wave.
- **Output:** Half-wave rectified signal.
- **Observation:** No voltage drop (unlike diode rectifiers).

### b) Comparison with Diode Rectifier

- **Diode Rectifier:**
  - 0.7 V drop, distorted output. Because of cutin voltages the voltage is reduced and also no output till the certain voltage





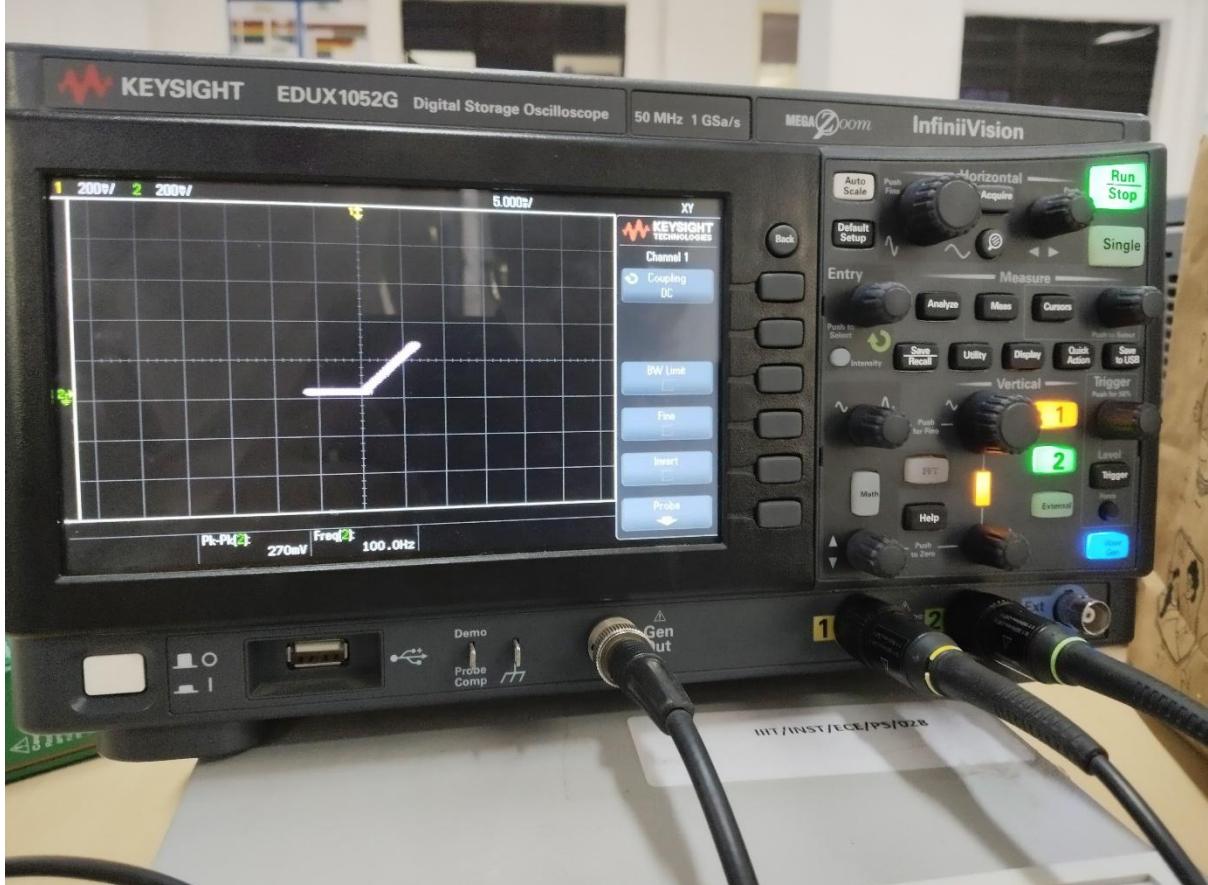
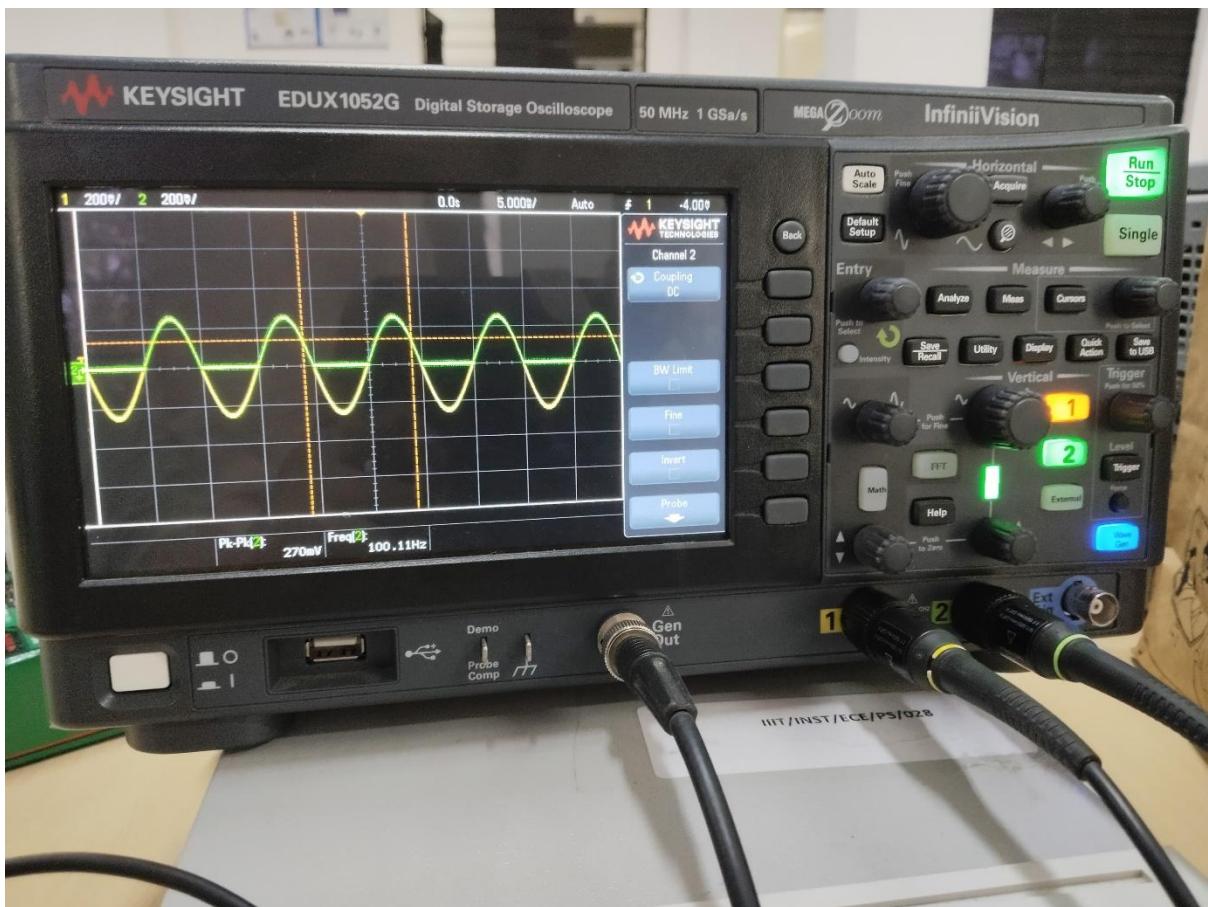
- **Op-Amp Rectifier:**

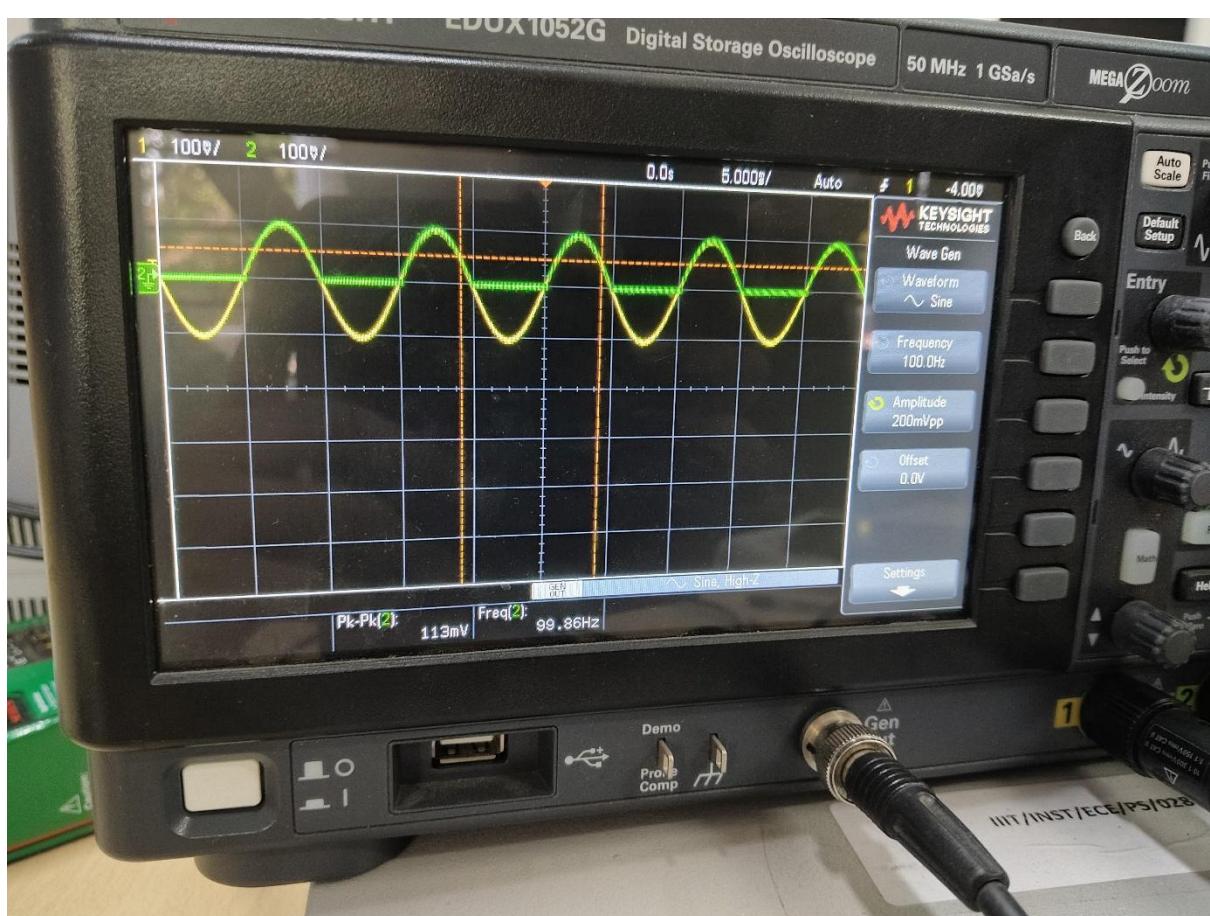
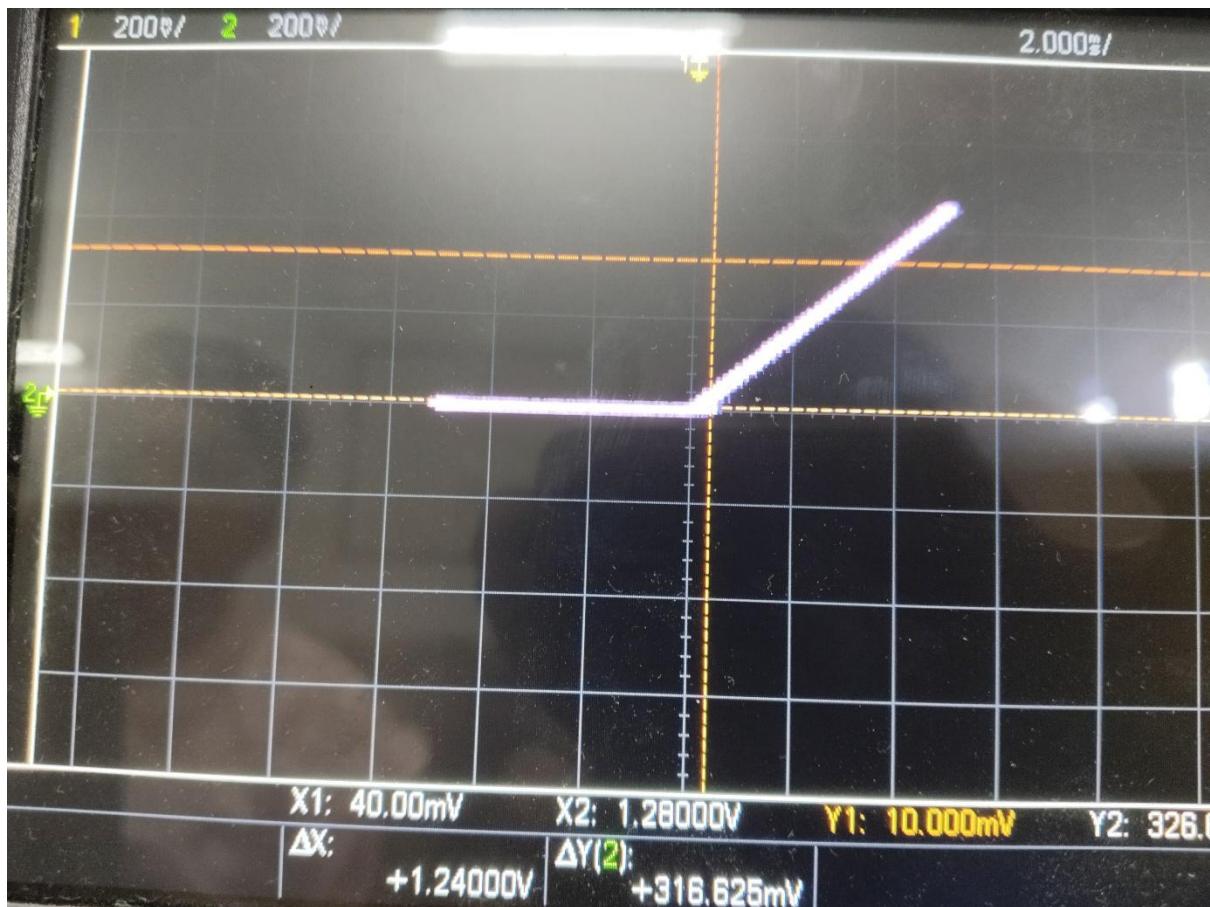
- Near-zero drop, precise rectification.
- Diode conducts only in forward bias (op-amp compensates for reverse bias).

These op-amp based rectifiers are better than diode and resistor based rectifiers. Op-amp based rectifiers are better in terms of accuracy, precision, speed, input impedance, temperature stability, and linearity. Conventional diode-based rectifiers have a voltage drop across the diode, typically around 0.7 volts for silicon diodes. In these rectifiers, the output waveform has a lower amplitude due to the cut in voltage of the diode.

Op-amp rectifiers, on the other hand, can achieve nearly zero voltage drop during rectification. The diode acts as a DC voltage source with reversed polarities, resulting in a decreased output sinusoid amplitude.

In contrast, the Op Amp-based rectifier circuit behaves differently. When the input sinusoid is positive, the Op Amp amplifies it, causing the diode to be forward biased and act as a short circuit

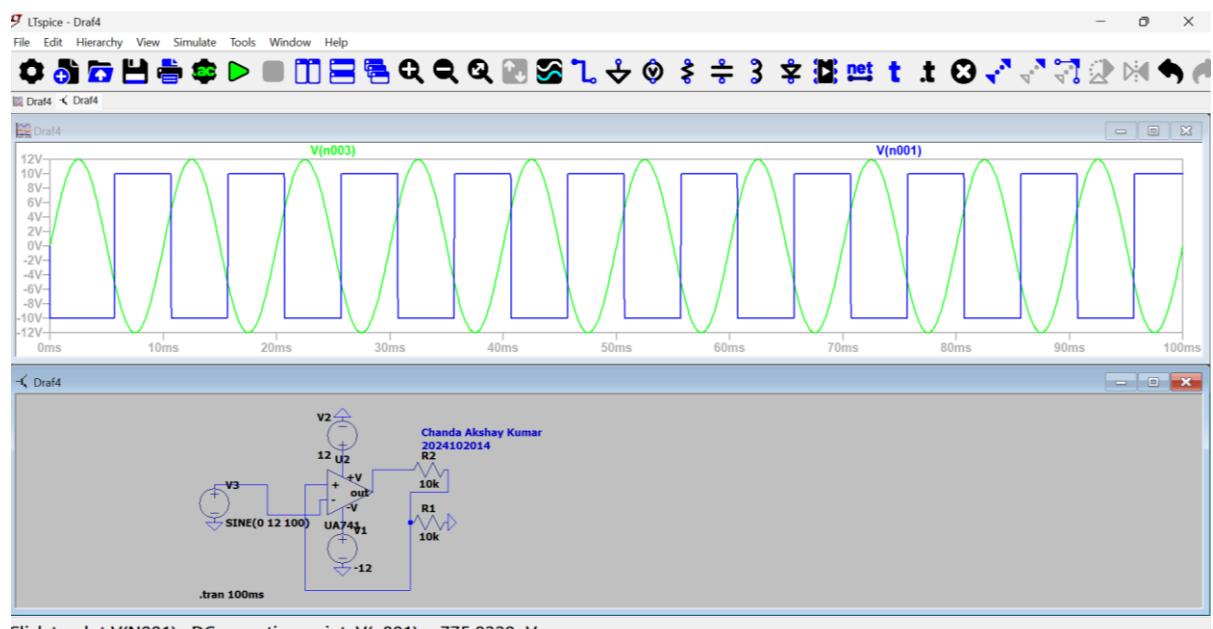
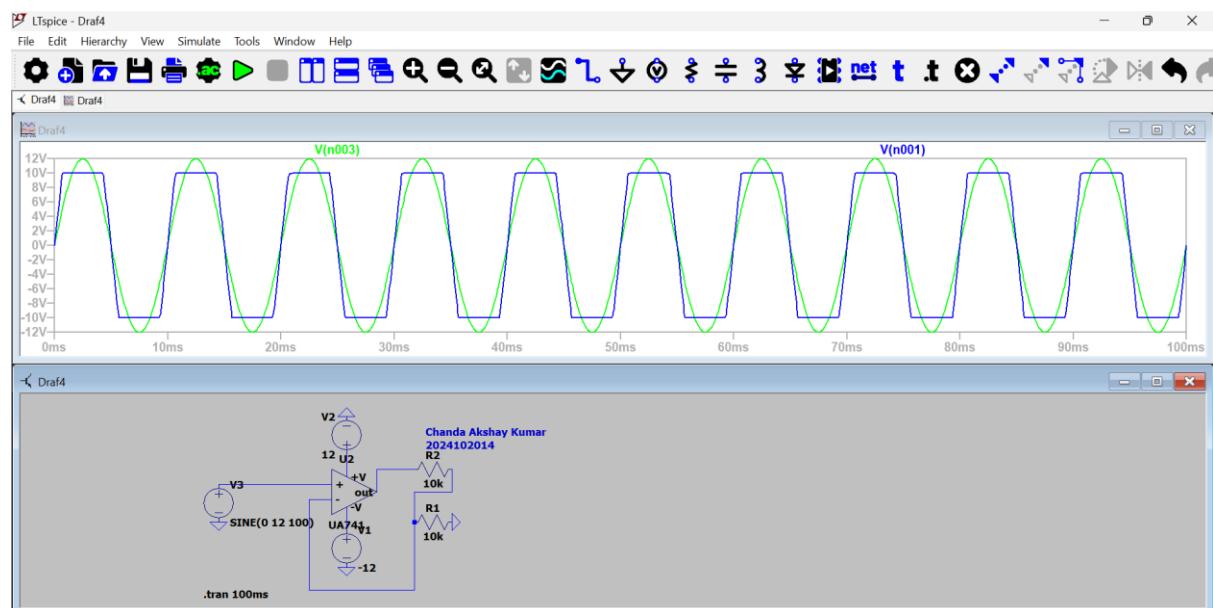




## Conclusion

- **Negative Feedback:** Improves stability (integrator, rectifier).
- **Positive Feedback:** Causes hysteresis (oscillators).
- Op-amp circuits outperform passive components in precision applications.

## LTSPICE



Click to plot V(N001). DC operating point: V(n001) = 775.0229 $\mu$ V

