

# CMPE 185 Autonomous Mobile Robots

Navigation and Control

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# Control

- Suppose we have a plan:
  - “Hey robot! Move north one meter, then east one meter, then north again for one meter.”
- How do we execute this plan?
  - How do we go exactly one meter?
  - How do we go exactly north?

**How do we control the robots?**

# Control Architectures

- Today, most robots control systems have a mixture of planning and behavior-based control strategies
- To implement these strategies, a control architecture is used
- Control architectures should consider:
  - **Code Modularity**
    - Allows programmers to interchange environment types sensors, path planners, propulsion, etc.
  - **Localization**
    - Embed specific navigation functions within modules to allow different levels of control (e.g., from task planning to wheel velocity control)

# Control Architectures – Decomposition

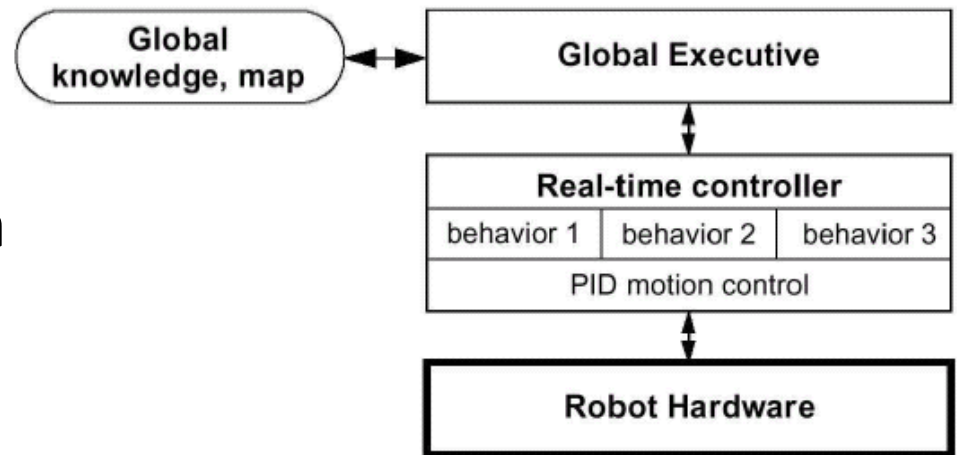
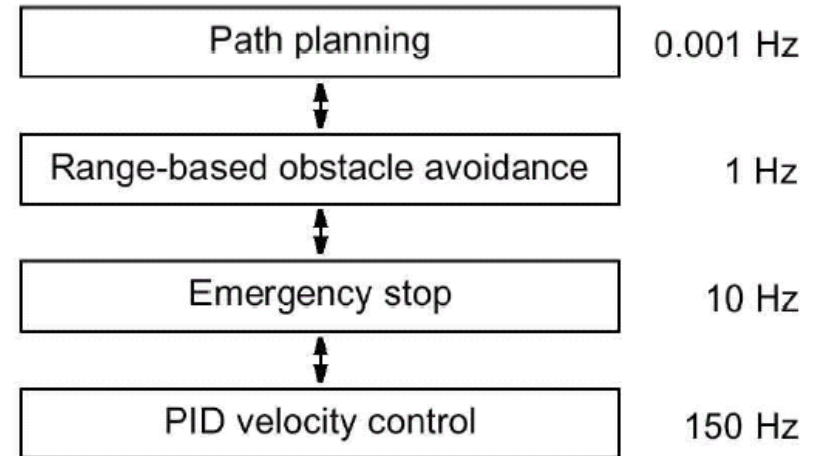
- Decomposition allows us to modularize our control system based on different axes:

- **Temporal Decomposition**

- Facilitates varying degrees of real-time processes

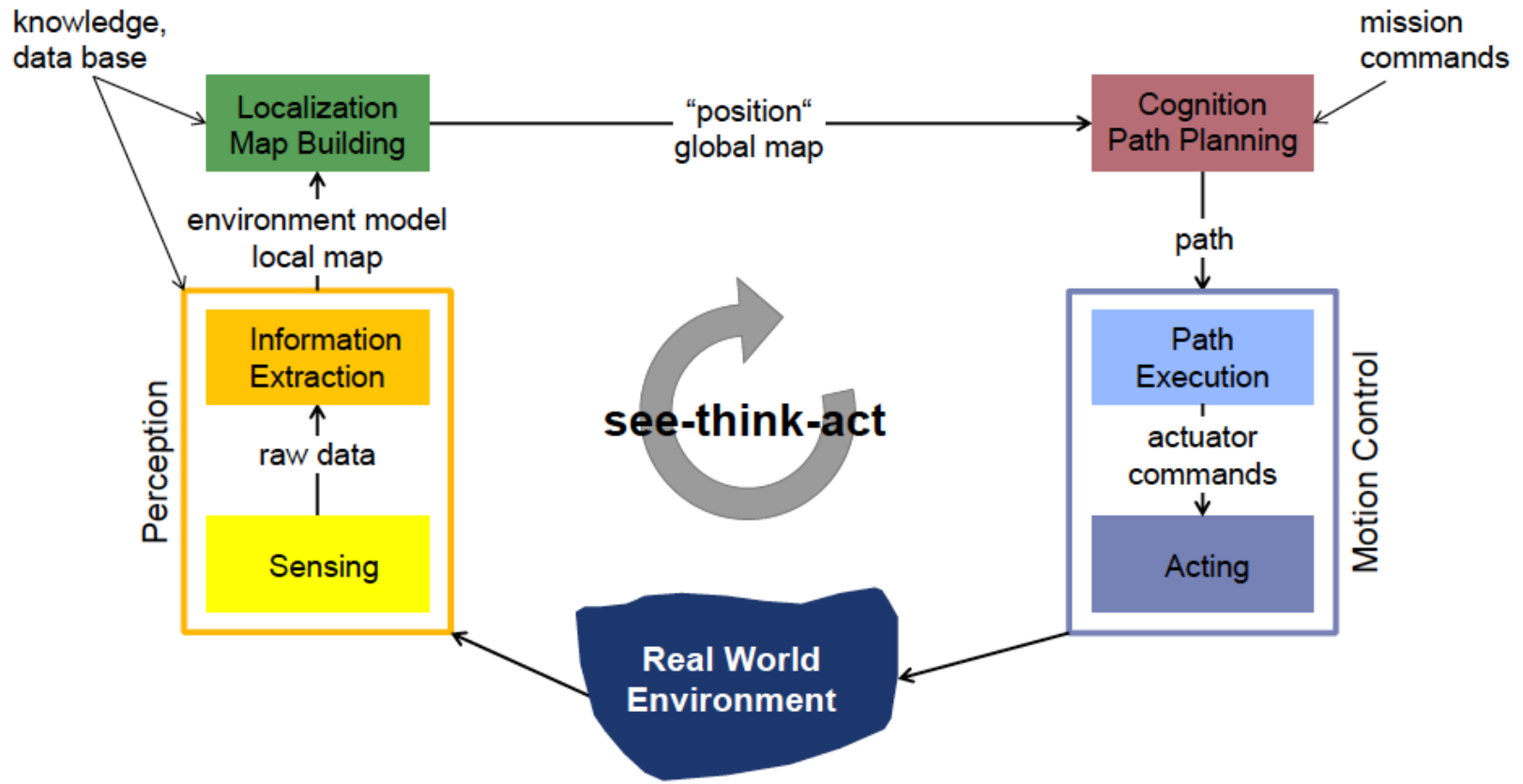
- **Control Decomposition**

- Defines how modules should interact: serial or parallel?



# See-think-act Model of Mobile Robots

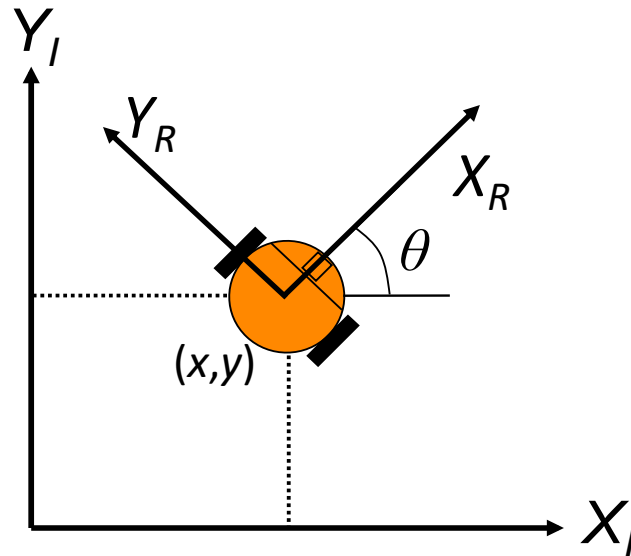
- An example of a decomposition using a mixture of serial and parallel approaches



# Recall: Mobile Robot Kinematics – Two Models

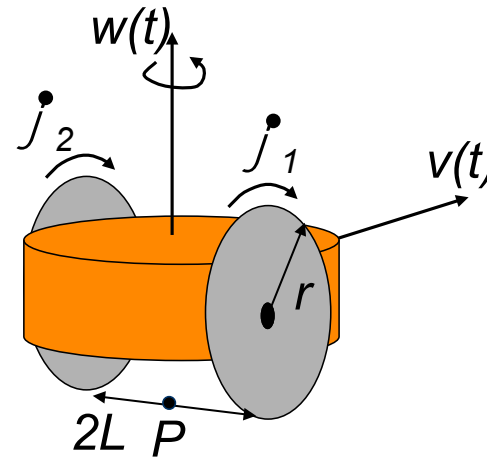
- Two models

How to design  $v$  and  $w$  so that the robot can follow a given trajectory?



$$\begin{cases} \dot{x} = v \cos \theta \\ \dot{y} = v \sin \theta \\ \dot{\theta} = w \end{cases}$$

Design for this model!



$$\begin{cases} \dot{x} = \frac{r}{2} (\dot{\phi}_1 + \dot{\phi}_2) \cos \theta \\ \dot{y} = \frac{r}{2} (\dot{\phi}_1 + \dot{\phi}_2) \sin \theta \\ \dot{\theta} = \frac{r}{2L} (\dot{\phi}_2 - \dot{\phi}_1) \end{cases}$$

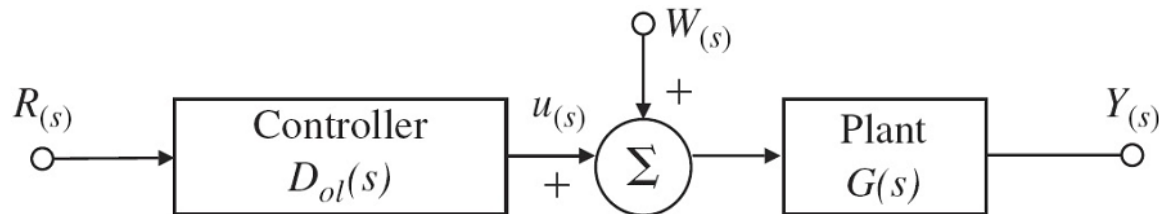
Implement this model

# The Basic Building Blocks

- ***State*** = Representation of what the system is currently doing
- ***Dynamics*** = Description of how the state changes
- ***Reference*** = What we want the system to do
- ***Output*** = Measurement of (some aspects of the) system
- ***Input*** = Control signal
- ***Feedback*** = Mapping from outputs to inputs  
Control Theory = How to pick the input signal  $u$ ?

# Open-loop

- If I command the motors to “full power” for three seconds, the robot probably will go forward one meter
- Open-loop system with
  - Reference  $R$
  - Control  $U$
  - Disturbance  $W$

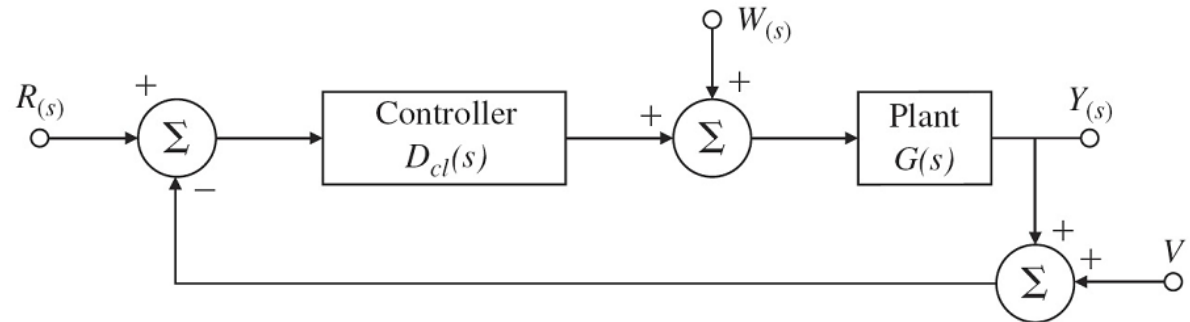


- Recall: Errors in odometry reading



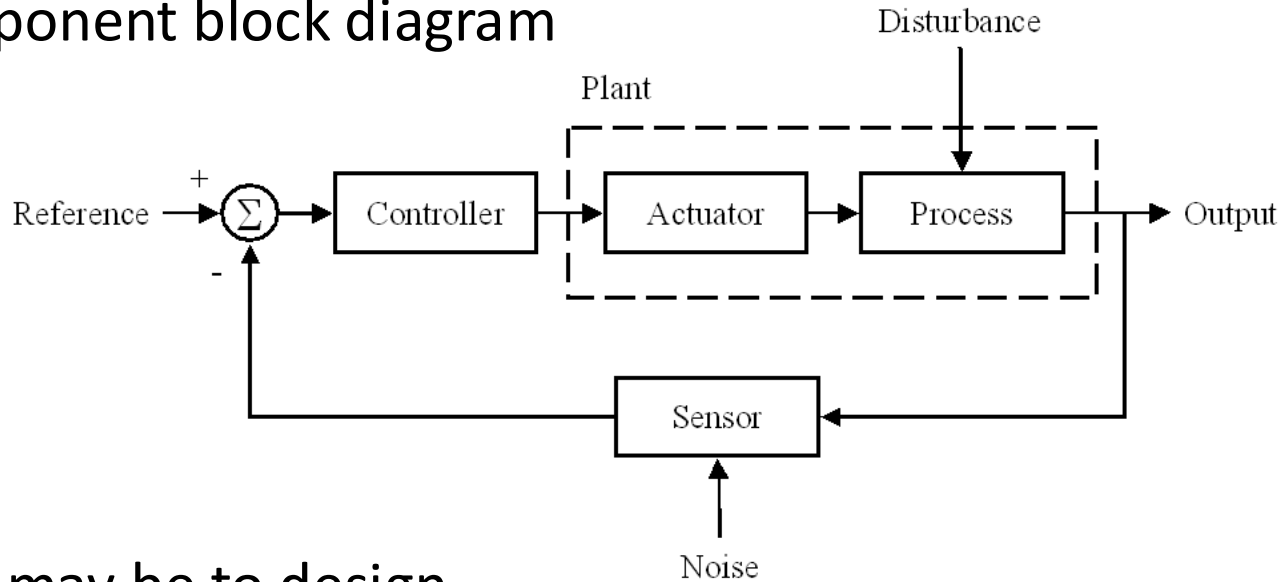
# Closed-loop

- Use real-time information about system performance to improve system performance
- Closed-loop system with
  - Reference  $R$
  - Control  $U$
  - Disturbance  $W$
  - Sensor noise  $V$
- Types:
  - Bang Bang
  - PID



# Feedback Control System Basic Ingredients

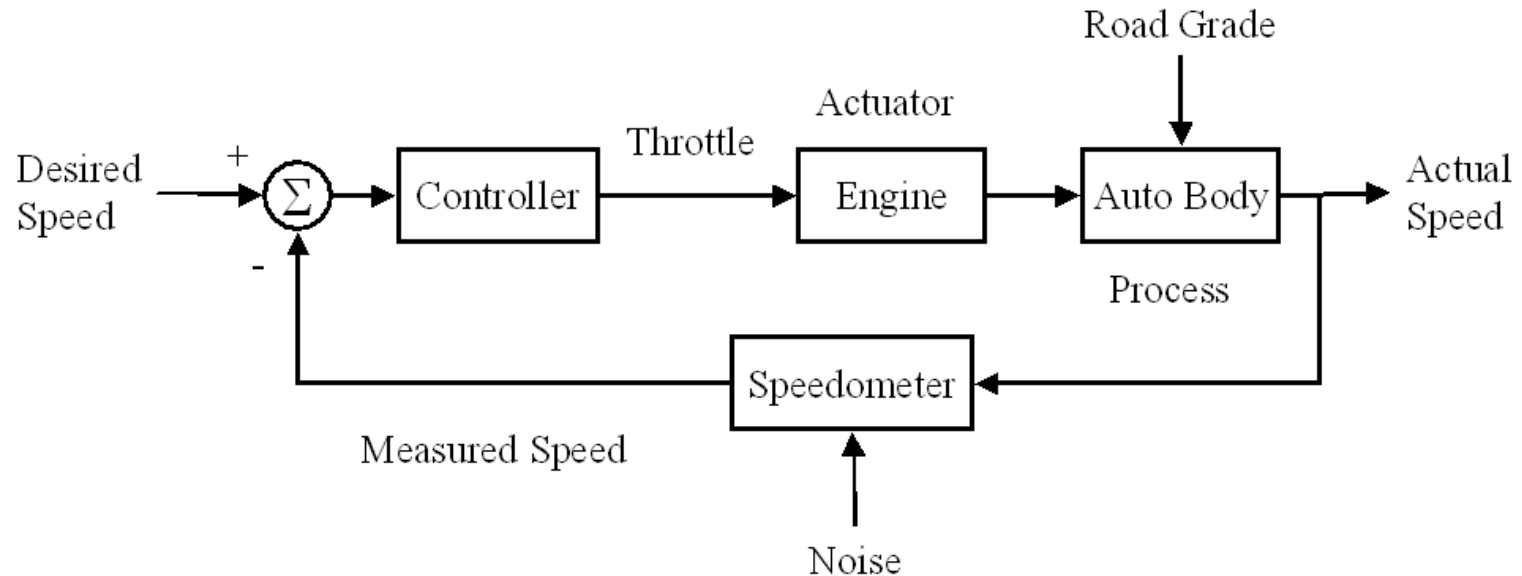
- Component block diagram



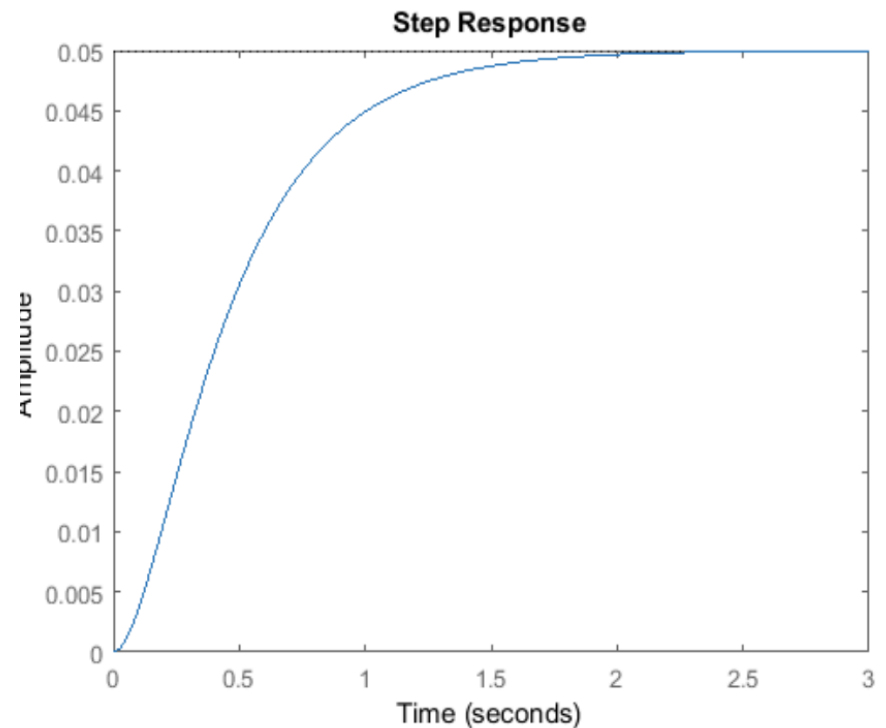
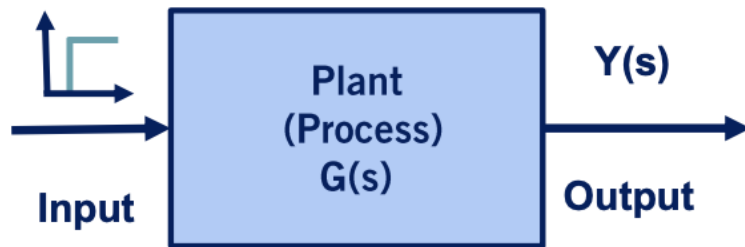
- Goal may be to design
  - **Regulating control**: maintain a fixed output
  - **Servo control**: follow a changing reference
- so that the system
  - is **stable** (e.g., bounded-input-bounded-output)
  - **rejects** disturbances
  - is **robust** to parameter changes

# Control System: Example

- Automobile cruise control



# Open-Loop Step Response



# Time-Domain Specifications

- **Rise time  $t_r$** : how fast the system reacts to a change in its input
- **Setting time  $t_s$** : how fast the system's transient decays
- **Overshoot  $M_p$** : How far the response grows beyond its final value during transients
- **Peak time  $t_p$** : How far the response reaches the peak value

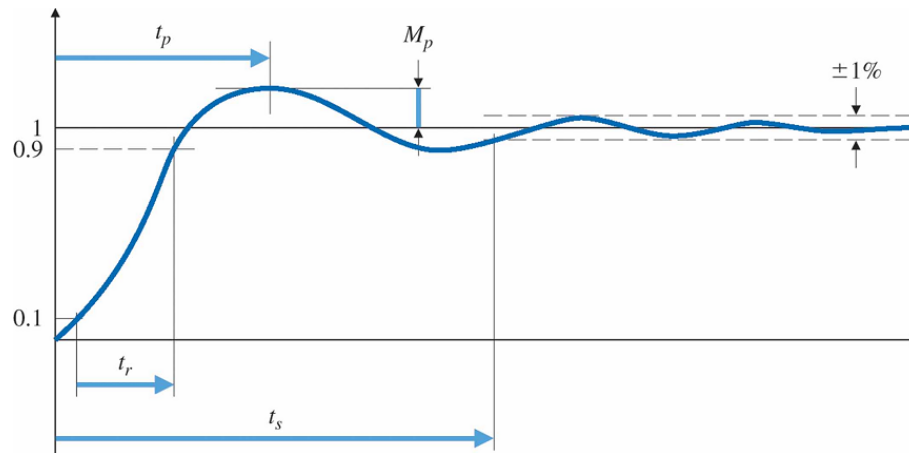


Figure : Definitions of time-domain specifications.

# Dynamic Models

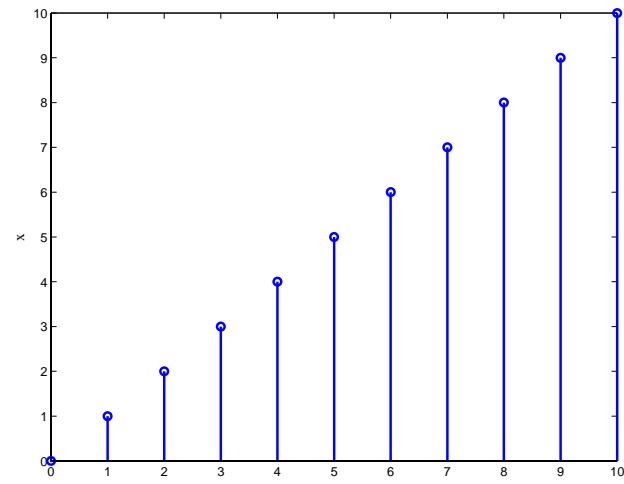
- Effective control strategies rely on predictive models
- **Discrete time:**

$$x_{k+1} = f(x_k, u_k) \quad \leftarrow \text{Difference equation}$$

Example: clock

$$x_{k+1} = x_k + 1$$

**Discrete Time Clock**



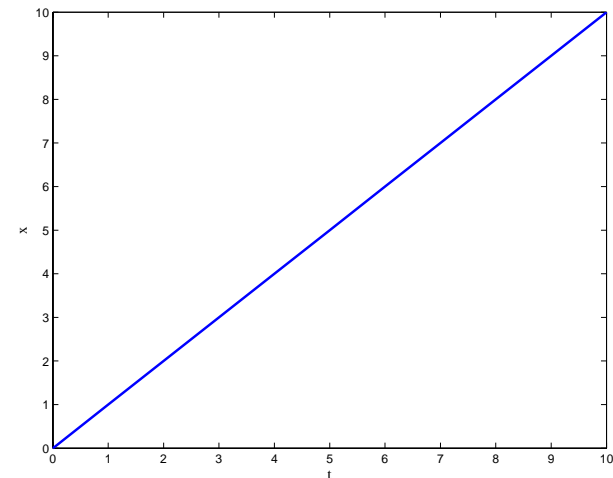
# Dynamic Models

- Laws of Physics are all in continuous time
- Instead of “next” state, we need derivatives w.r.t. time
- **Continuous time:**

$$\frac{dx}{dt} = f(x, u) \sim \dot{x} = f(x, u) \leftarrow \text{Differential equation}$$

Example: clock  $\dot{x} = 1$

**Continuous Time Clock**



# Dynamic Models

- Effective control strategies rely on predictive models
- For the unicycle model:

$$\begin{cases} \dot{x} = v \cos \theta \\ \dot{y} = v \sin \theta \\ \dot{\theta} = w \end{cases}$$

- In implementation, **everything is discrete/sampled!**
- From time step  $k$  to time step  $k+1$ , the position changes to

$$\begin{cases} x_{k+1} = x_k + v\Delta t \cos \theta_k \\ y_{k+1} = y_k + v\Delta t \sin \theta_k \\ \theta_{k+1} = \theta_k + w\Delta t \end{cases}$$

$v, w$ : control input!

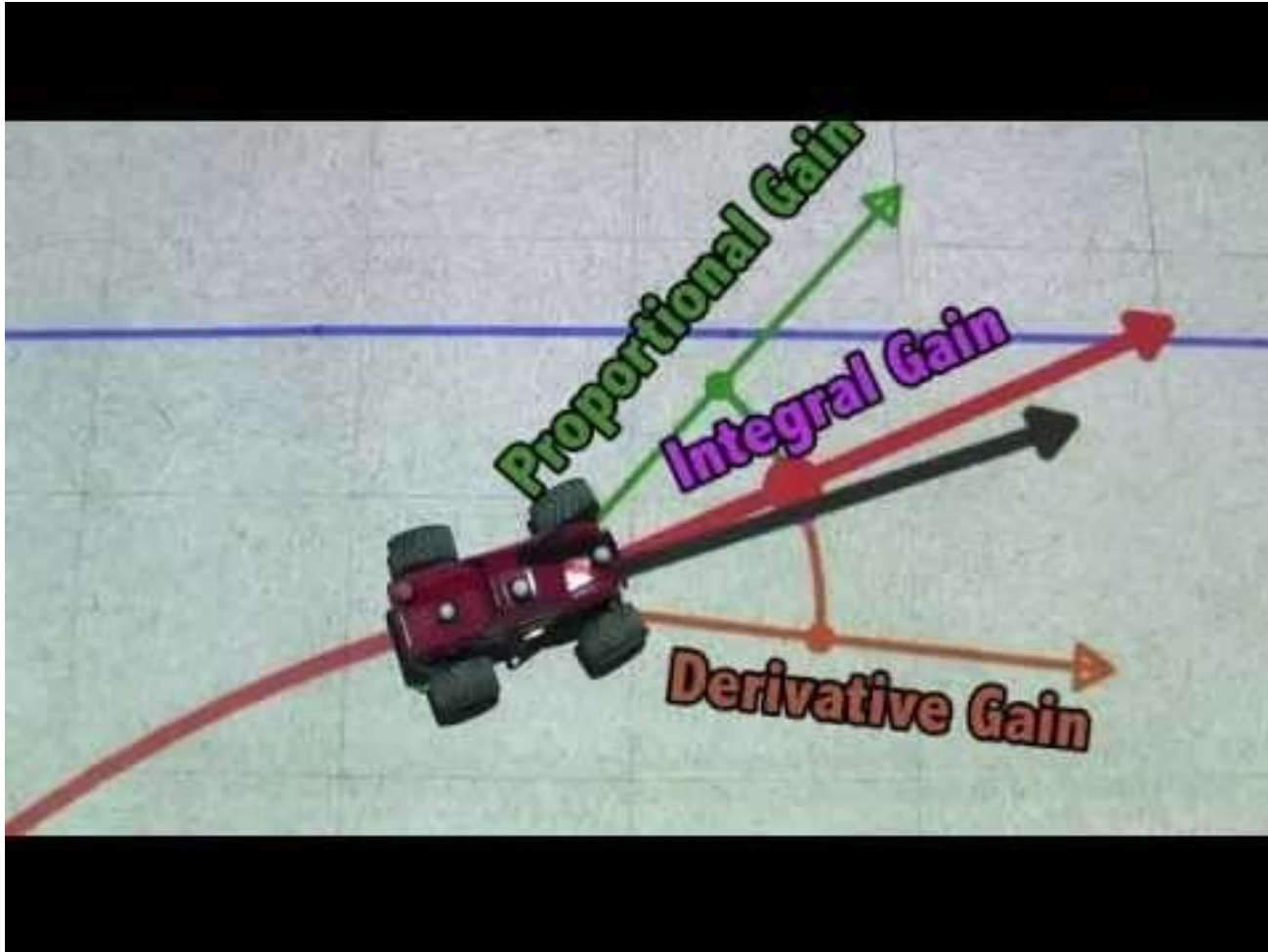


# Next: PID Control

- With the important concepts in feedback control theory, now we are ready to introduce

## PID Control

# PID Controller Explained



# P Control

- Let us start with a simple controller: **P controller**
- Proportional Feedback Control (P Control)
  - Uses the error between the desired and measured state to determine the control signal
- If  $x_{desired}$  is the desired state, and  $x$  is the actual state, we define the error as

$$e = x_{desired} - x$$

- The control signal  $u$  is calculated as  $u = K_p e$

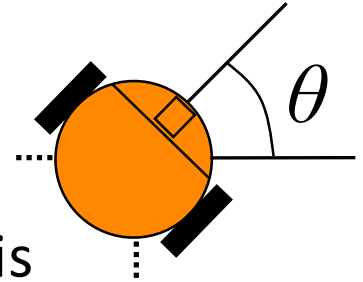
where  $K_p$  is called the proportional gain

# P Control – A Simple Example

- Consider the **orientation control** of a mobile robot

$$\dot{\theta} = w$$

$$\theta_{k+1} = \theta_k + w\Delta t$$



- The control signal  $u$  is the angular velocity  $w$ , and is calculated as

$$u = K_P(\theta_{desired} - \theta)$$

- Note:

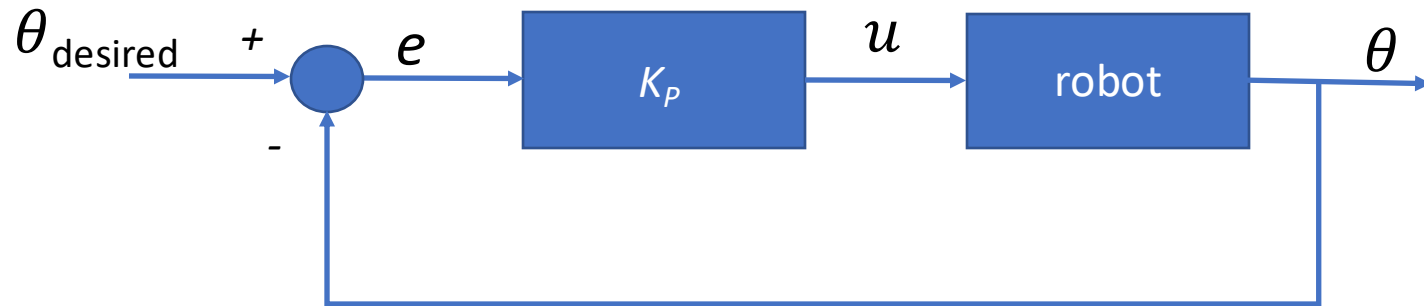
- If  $\theta_{desired} = \theta$ , the control signal is 0
- If  $\theta_{desired} < \theta$ , the control signal is negative, resulting in a decrease in  $\theta$
- If  $\theta_{desired} > \theta$ , the control signal is positive, resulting in an increase in  $\theta$
- The magnitude of the increase/decrease depends on  $K_P$

# P Control – A Simple Example

- Block Diagram

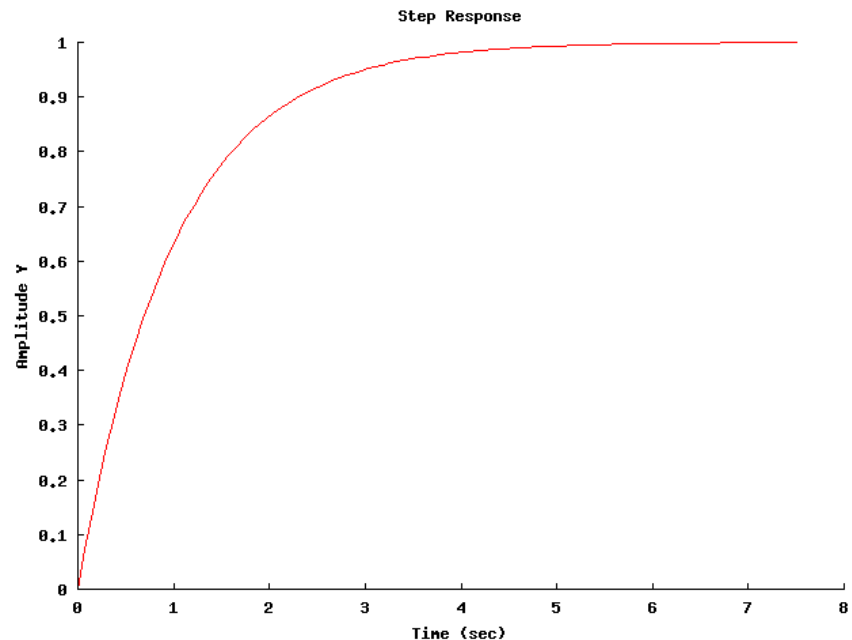
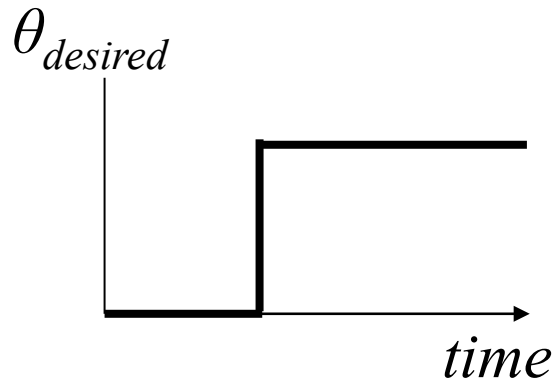
$$u = K_P(\theta_{desired} - \theta)$$

$$\dot{\theta} = w = u$$



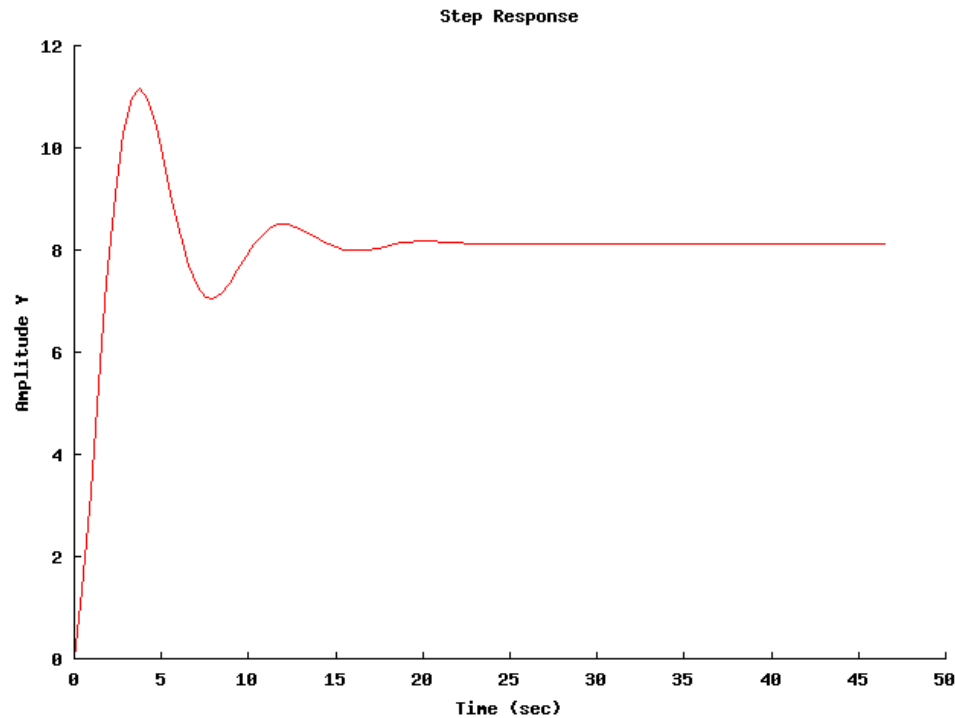
# P Control – A Simple Example

- Time Domain Response of Step Response
- Step from  $\theta_{\text{desired}} = 0$  to  $\theta_{\text{desired}} = 1$



# P Control – A Simple Example

- Time Domain Response of Step Response
- Step from  $\theta_{\text{desired}} = 0$  to  $\theta_{\text{desired}} = 8$



# Another Example: Cruise Controllers

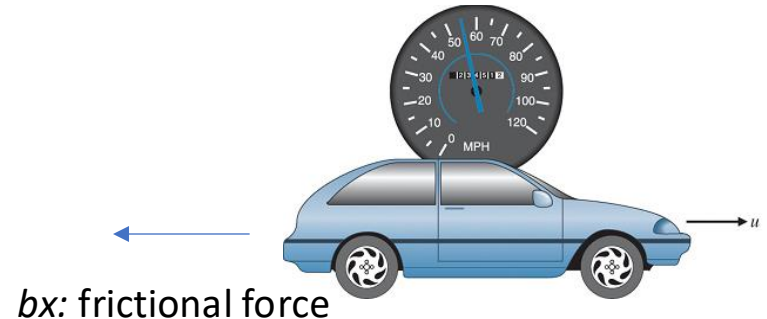
- Make a car drive at a desired, reference speed  $r$
- Newton's Second Law:  $F = ma$
- State: velocity  $x$
- Input: gas/brake  $u$
- Dynamics:

$$m\dot{x} = cu - bx$$

$$\dot{x} = \frac{c}{m}u - \gamma x$$

$$\gamma = \frac{b}{m}$$

$c$  = electro-mechanical transmission coefficient





# Cruise Controllers

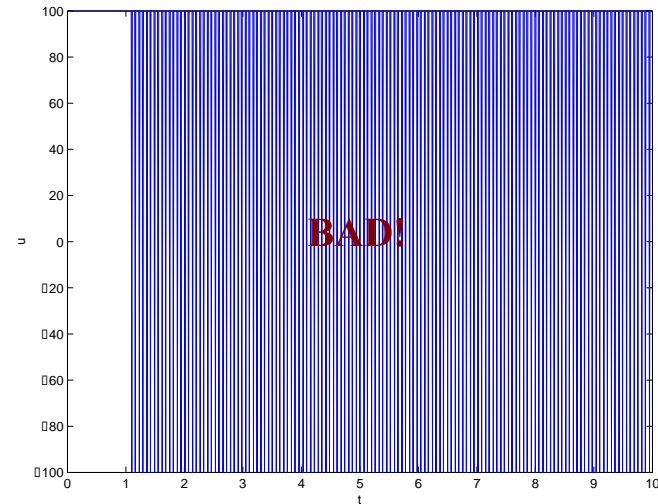
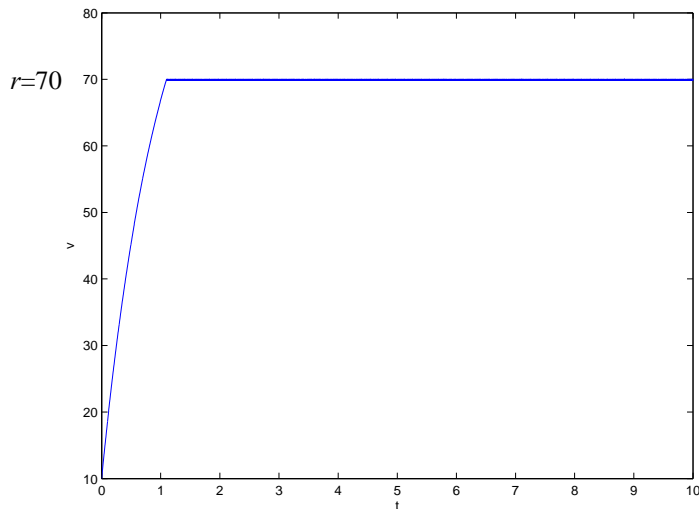
- Assume that we measure the velocity  $y = x$
- The control signal should be a function of  $r - y (= e)$
- What properties should the control signal have?
  - Small  $e$  gives small  $u$
  - $u$  should not be “jerky”
  - $u$  should not depend on us knowing  $c$  and  $m$  exactly
- Car model:  $\dot{x} = \frac{c}{m} u - \gamma x$
- Want:
$$x \rightarrow r \text{ as } t \rightarrow \infty \quad (e = r - x \rightarrow 0)$$

# Bang-Bang Control

- **Attempt 1:** Bang-Bang control

$$u = \begin{cases} u_{max} & \text{if } e > 0 \\ -u_{max} & \text{if } e < 0 \\ 0 & \text{if } e = 0 \end{cases}$$

Bumpy ride  
Burns out actuators



- Problem: the controller over-reacts to small errors

# Proportional Control

- **Attempt 2: P Control**

$$u(t) = K_p e(t)$$

- Intuition: if  $e(t) > 0$ , the goal velocity is larger than the current velocity. So, command a larger acceleration
- Small error yields small control signals
- Nice and smooth

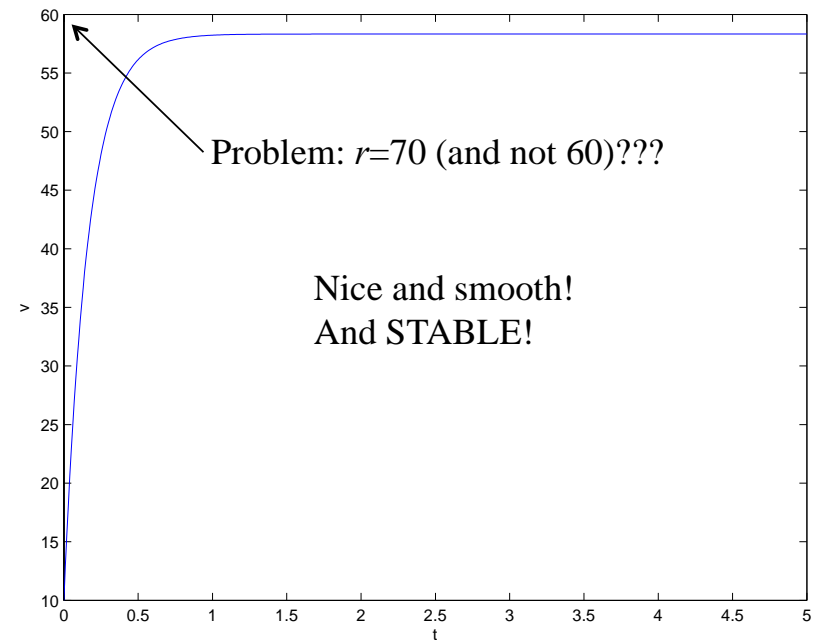
# Proportional Control

- At steady state ( $x$  does not change any more)

$$\begin{aligned}\dot{x} = 0 &= \frac{c}{m}u - \gamma x \\ &= \frac{c}{m}k(r - x) - \gamma x \\ &\rightarrow (ck + m\gamma)x = ckr\end{aligned}$$

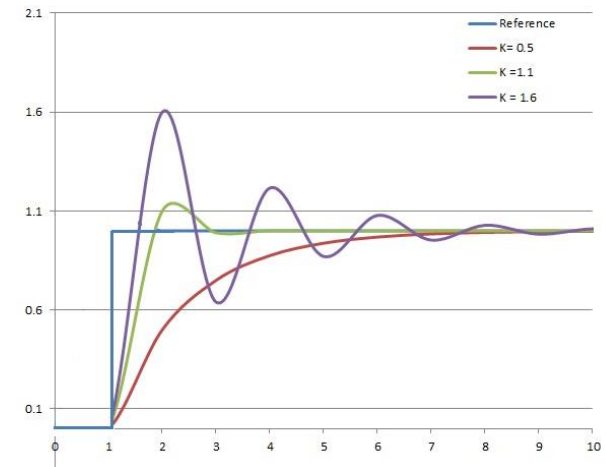
$$x = \frac{ck}{ck + m\gamma}r < r$$

$$\dot{x} = \frac{c}{m}u - \gamma x$$



# Proportional Control

- We want to drive error to zero quickly
  - This implies large gains
- We want to get rid of steady-state error
  - If we're close to desired output, proportional output will be small. This makes it hard to drive steady-state error to zero.
  - This implies large gains.
- What's wrong with really large gains?
  - Oscillations



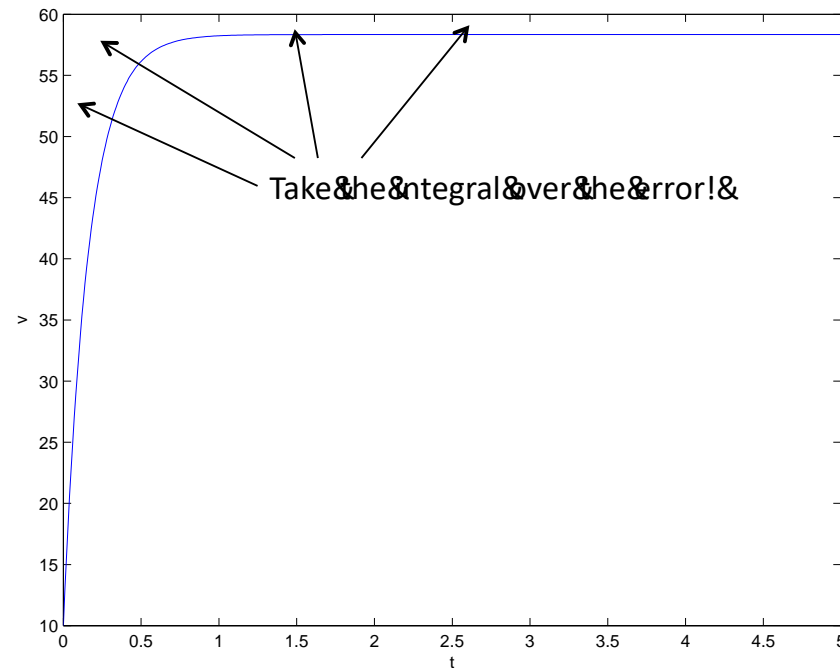
# PI Controller

- **Attempt 3: PI-Controllers**

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau$$

- If we have error for a long period of time, it argues for additional correction
- The integral term in the controller is the sum of the instantaneous error over time and gives the accumulated offset
- Force average error to zero (in steady state)

## P-Regulator



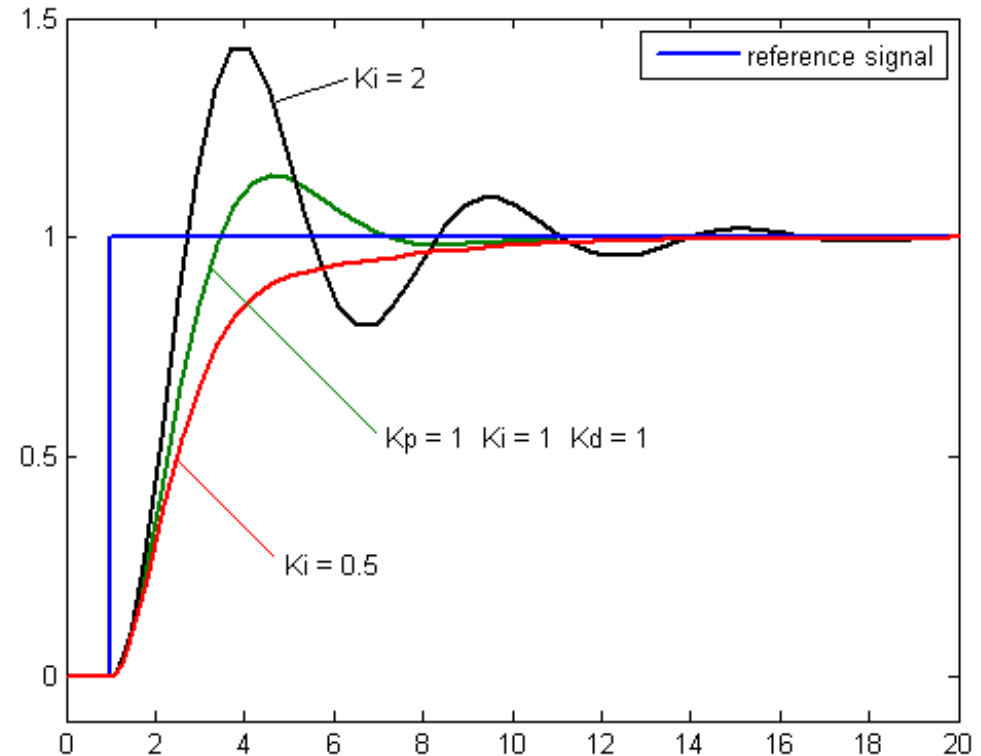
# PI Controller

- Pros:

- accelerates the movement of the process towards setpoint
- eliminates the residual steady-state error

- Cons:

- may result in overshooting the setpoint



# Derivative Controller

- Damping friction is a force opposing motion, proportional to velocity
- Try to prevent overshoot by damping controller response
- Derivative term:

$$K_D \dot{e}(t)$$

- Derivative control is “happy” the error is not changing
  - Things not getting better, but not getting worse either
- Estimating a derivative from measurements is fragile, and amplifies noise
- The Derivative term is rarely used along



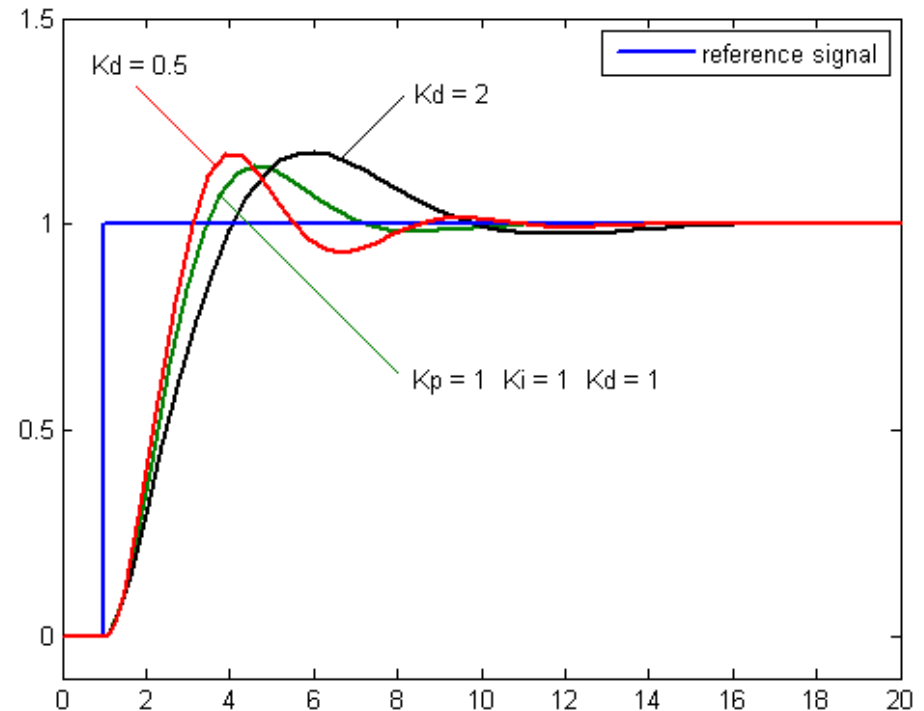
# PD Controller

- **Attempt 4: PD controller**

$$u(t) = K_P e(t) + K_D \dot{e}(t)$$

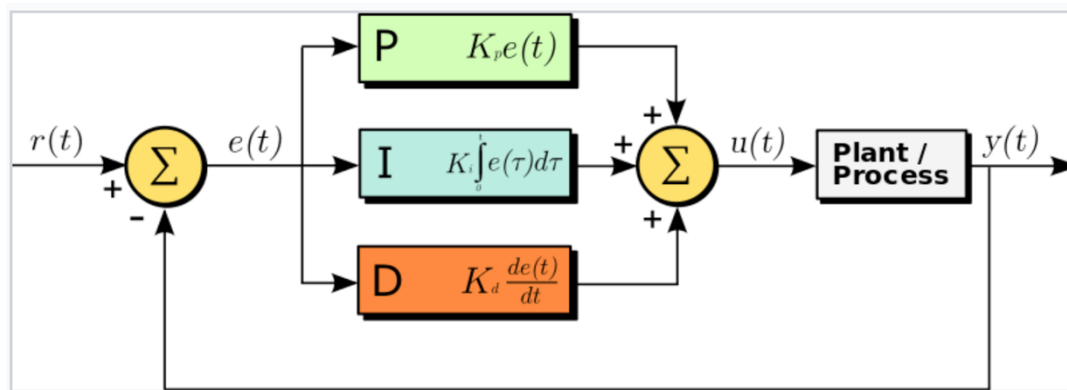
- **Combine P and D terms**

- D term helps us avoid oscillation, allowing us to have bigger P terms
  - Faster response
  - Less oscillation



# PID Control

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$



# PID Control

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

- **P**: contributes to stability, medium-rate responsiveness
- **I**: tracking and disturbance rejection, slow-rate responsiveness. May cause oscillations
- **D**: fast-rate responsiveness. Sensitive to noise
- **PID**: by far the most used low-level controller.
  - However, stability is not guaranteed

# PID Control

- **Note:** we often won't use all three terms
  - Each type of term has downsides
  - Use only the terms you need for good performance
- Feedback has a remarkable ability to fight uncertainty in model parameters!

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

# PID Controller Parameter Tuning

- If the parameters of the PID controller are chosen incorrectly, the controlled process input can be unstable, i.e., its output diverges, with or without oscillation.
- **Where do PID gains come from?**
  - Analysis
    - Carefully model system in terms of underlying physics and PID controller gains
    - Compute values of PID controller so that system is 1) stable and 2) performs well
  - Empirical experimentation
    - Hard to make models accurate enough: many parameters
    - Often, easy to tune by hand.

# PID Controller Parameter Tuning

- Parameter tuning is very important for PID controller
  - **Manual tuning**
    1. Increase P term until performance is adequate or oscillation begins
    2. Increase D term to dampen oscillation
    3. Go to 1 until no improvements possible.
    4. Increase I term to eliminate steady-state error.
  - **Ziegler-Nichols method**
  - **Software**
  - ...

# Characteristics of P, I, and D Gains

Closed Loop Response	Rise Time	Overshoot	Settling Time	Steady State Error
Increase $K_p$	Decrease	Increase	Small change	Decrease
Increase $K_i$	Decrease	Increase	Increase	Eliminate
Increase $K_d$	Small change	Decrease	Decrease	Small change

By properly tuning  
the PID gains

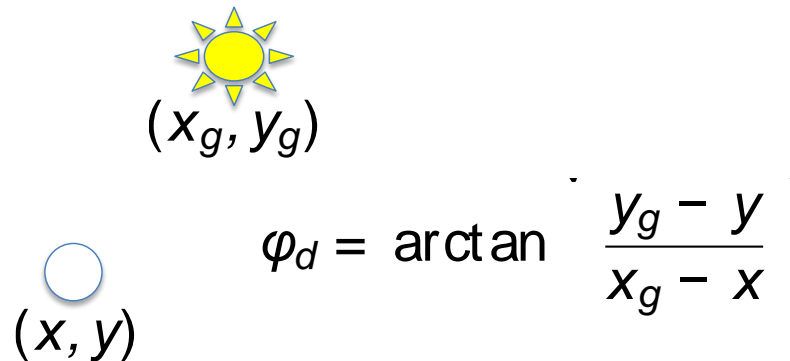
# Example: Go To Goal

- How to drive a robot to a goal location?

- Heading error:  $e = \theta_d - \theta$

$$\begin{cases} \dot{x} = v \cos \theta \\ \dot{y} = v \sin \theta \\ \dot{\theta} = \omega \end{cases}$$

- In this case, the desired heading  $\theta_d$  is time-varying



- Control:  $\omega = \text{PID}(e)$



# Cruise Controller

- Let's consider the simplified model with the PID controller

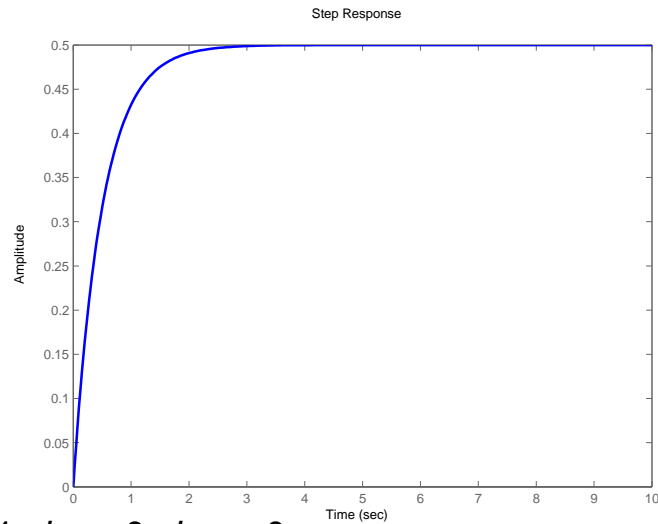
$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

$$\dot{x} = \frac{c}{m} u - \gamma x$$

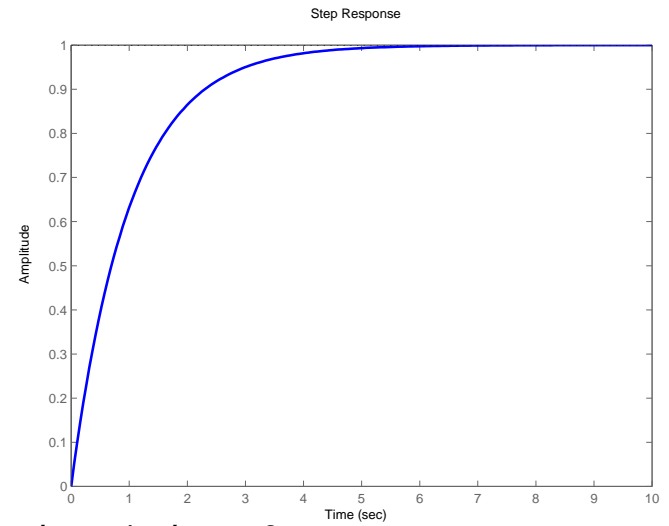
$$c = 1, m = 1, \gamma = 0.1, r = 1$$



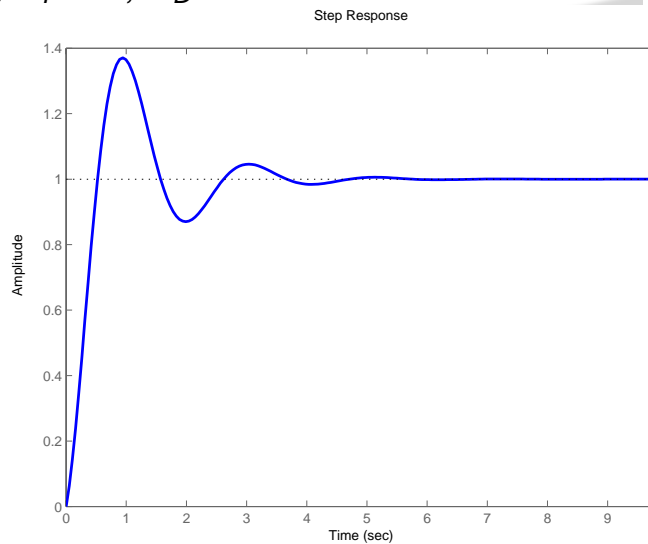
# Cruise Controller



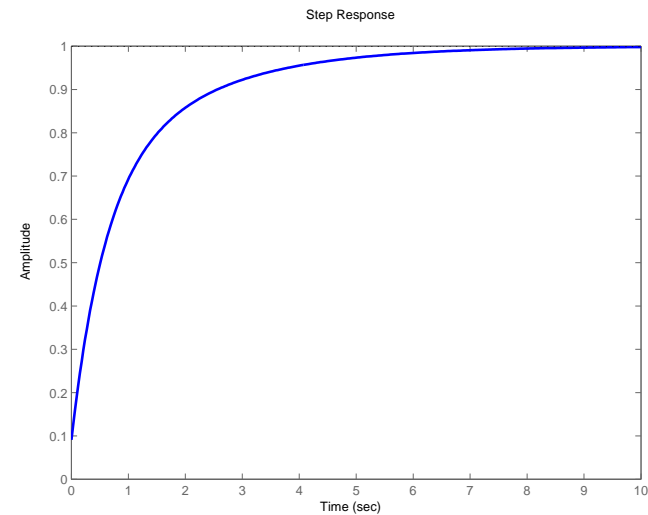
$$k_P = 1, k_I = 0, k_D = 0$$



$$k_P = 1, k_I = 1, k_D = 0$$



$$k_P = 1, k_I = 10, k_D = 0$$



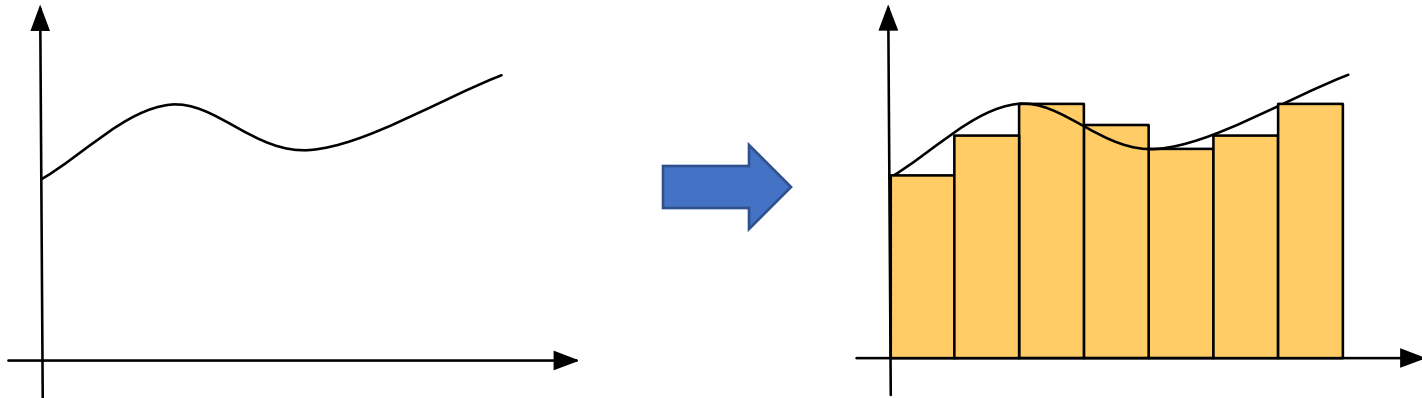
$$k_P = 1, k_I = 1, k_D = 0.1$$

# PID Controller Implementation

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

$\Delta t$  (sample time)

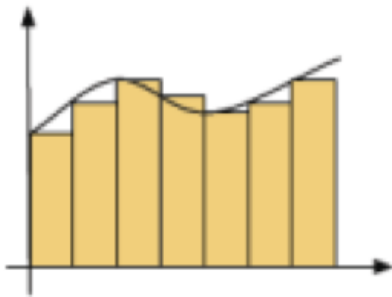
$$\dot{e} \approx \frac{e_{new} - e_{old}}{\Delta t}$$



# PID Controller Implementation

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

$$\Delta t \text{ (sample time)} \quad \dot{e} \approx \frac{e_{new} - e_{old}}{\Delta t}$$



$$\int_0^t e(\tau) d\tau \approx \sum_{k=0}^N e(k\Delta t) \Delta t = \Delta t E$$

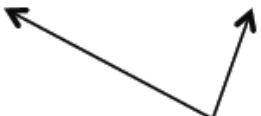
$$\Delta t E_{new} = \Delta t \sum_{k=1}^{N+1} e(k\Delta t) = \Delta t e((N+1)\Delta t) + \Delta t E_{old}$$

$$E_{new} = E_{old} + e$$

# PID Controller Implementation

- Each time the controller is called

```
read e;  
e_dot=e-old_e;  
E=E+e;  
u=kP*e+kD*e_dot+kI*E;  
old_e=e;
```



Note: The coefficients now include the sample time and must be scaled accordingly

- Thank You!