CL202: Fluid Mechanics

Fluid Statics



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What has been covered till now?

Let us list down

- > Introductory concepts
- Dimensional analysis
 - > Buckingham Pi theorem
 - > Classification of flows
 - > Mach number
 - > Boundary layer
- Similarity/ Scale-up

Fluid Statics: Motivation

- > Also known as 'Hydrostatics' for incompressible fluids
- > Statics: No motion
 - ➤ No momentum change
 - ➤ No shear stress are present
- > Pressure distribution in the atmosphere and ocean
- Force on flat and curved surfaces: vessel / tank walls, dam gates
- **>** Buoyancy
- > Hydraulic actuation
- ➤ Design of manometers, mechanical and electronic pressure instruments

Pressure

- ➤ Thermodynamic property of fluid
- ➤ Defined as force per unit area
 - Force caused by fluid molecules bombarding the surface
- > A scalar quantity
 - > Pressure force acting on a surface is a vector
 - The direction of pressure force is determined by the surface on which it acts
- ➤ Always acts normal (perpendicular) to a surface
- ➤ Pressure is compressive i.e. pushes a surface (not pulls)

Pressure

- ➤ Pressure is isotropic i.e. acts equally is all directions
 - > Has a single value at any point in a fluid
- ➤ Units:
 - ➤ kg/m²; Pascal (Pa), Bar, psi.
- Solution Gage) pressure: Pressure relative to the local ambient pressure (P_{atm}) when $P > P_{\text{atm}}$

$$P(gauge) = P_{abs} - P_{atm}$$

 \triangleright Vacuum pressure: Pressure relative to the local ambient pressure ($P_{\rm atm}$) when $P < P_{\rm atm}$

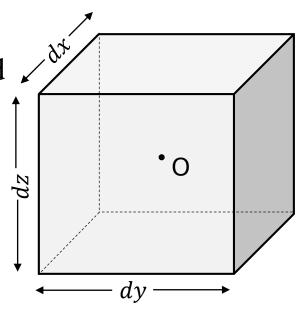
$$P(vacuum) = P_{atm} - P_{abs}$$

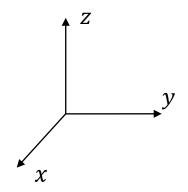
- > We experience that the pressure increases with depth
- Let us derive an expression for pressure distribution in a fluid
- Consider a cuboid fluid element of mass dm
- > Apply Newton's second law of motion on the fluid element

$$\mathbf{F} = \frac{d(m\mathbf{V})}{dt} = m \frac{d\mathbf{V}}{dt}$$
 (for constant m)

- For a stationary fluid $(\frac{dV}{dt})$, F = 0
- Force can be body and surface force
- > Body force is caused by gravity

$$dF_{Body} = dm \, g = \rho \, dV \, g = \rho \, dxdydz \, g$$





- > Surface forces can be caused by pressure and viscous stresses
- ➤ Viscous stresses are zero- stationary fluid
- > We need to find pressure force on each face
- ➤ Recall Taylor series

$$f(x) = f(a) + f'(a)(x - a) + \frac{f''(a)}{2!}(x - a)^2 + \frac{f'''(a)}{3!}(x - a)^3 + \cdots$$

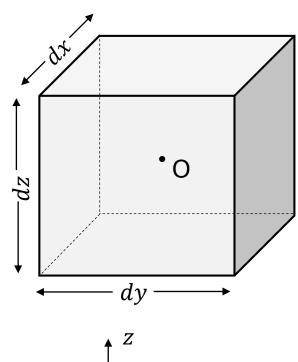
> Pressure on the right face on neglecting high order terms

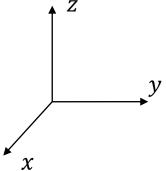
$$p_{Right} = p + \frac{\partial p}{\partial y} \frac{dy}{2}$$

➤ Similarly, on the left face:

$$p_{Left} = p - \frac{\partial p}{\partial y} \frac{dy}{2}$$

Pressure at O: p





> Surface or pressure force along the y-direction

$$d\mathbf{F}_{P,y} = -\left(p + \frac{\partial p}{\partial y} \frac{dy}{2}\right) dxdz \,\hat{\mathbf{j}} + \left(p - \frac{\partial p}{\partial y} \frac{dy}{2}\right) dxdz \,\hat{\mathbf{j}}$$

$$dF_{P,y} = -\frac{\partial p}{\partial y} dydxdz \,\hat{\mathbf{j}}$$

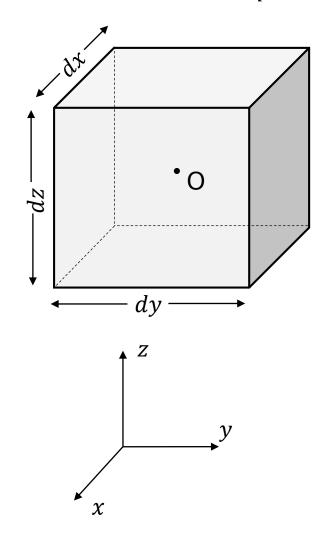
> Similarly, we can obtain:

$$dF_{P,x} = -\frac{\partial p}{\partial x} dy dx dz \,\hat{\mathbf{i}}$$
$$dF_{P,z} = -\frac{\partial p}{\partial z} dy dx dz \,\hat{\mathbf{k}}$$

> Total surface or pressure force will be

$$d\mathbf{F}_{Surface} = -\left(\frac{\partial p}{\partial x} \,\,\hat{\mathbf{i}} + \frac{\partial p}{\partial y} \,\,\hat{\mathbf{j}} + \frac{\partial p}{\partial z} \,\,\hat{\mathbf{k}}\right) dx dy dz$$

Pressure at O is p



$$d\mathbf{F}_{Surface} = -\left(\frac{\partial p}{\partial x}\,\,\hat{\mathbf{i}} + \frac{\partial p}{\partial y}\,\,\hat{\mathbf{j}} + \frac{\partial p}{\partial z}\,\,\hat{\mathbf{k}}\right) dx dy dz$$

➤ Gradient operator

$$\mathbf{\nabla} = \left(\frac{\partial}{\partial x} \,\,\hat{\mathbf{i}} + \frac{\partial}{\partial y} \,\,\hat{\mathbf{j}} + \frac{\partial}{\partial z} \,\,\widehat{\mathbf{k}}\right)$$

> Pressure gradient

$$\nabla p = \left(\frac{\partial p}{\partial x} \,\,\hat{\boldsymbol{\imath}} + \frac{\partial p}{\partial y} \,\,\hat{\boldsymbol{\jmath}} + \frac{\partial p}{\partial z} \,\,\widehat{\boldsymbol{k}}\right)$$

Pressure gradient, not pressure, is important in calculation of surface force

Therefore:

$$d\mathbf{F}_{Surface} = -\nabla p \ dxdydz$$

> Total force

$$d\mathbf{F} = d\mathbf{F}_{Surface} + d\mathbf{F}_{Body}$$

$$d\mathbf{F} = -\nabla p \ dxdydz + \rho \ dxdydz \ \mathbf{g}$$

$$dF = (-\nabla p + \rho g) dxdydz = (-\nabla p + \rho g) dV$$

$$d\mathbf{F} = (-\mathbf{\nabla}p + \rho\mathbf{g}) d\mathbf{\Psi}$$

Using Newton's second law $d\mathbf{F} = (-\nabla p + \rho \mathbf{g}) dV = 0$

$$-\nabla p + \rho \mathbf{g} = 0$$

Net pressure force per unit volume Net body force per unit volume

- > Pressure gradient, not pressure, is important in calculation of surface force
- > The equations can also be written in terms of components in each direction

$$\frac{\partial p}{\partial x} = \rho g_x$$

$$\frac{\partial p}{\partial y} = \rho g_y$$

$$\frac{\partial p}{\partial z} = \rho g_z$$

If the z axis is chosen such that positive z axis points vertically upward,

$$\vec{g} = -g \; \hat{k}$$

because gravity acts vertically downwards.

We have,

$$g_x = 0$$

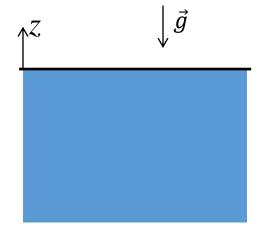
$$g_y = 0$$

$$g_z = -g$$

So,
$$\frac{\partial p}{\partial x} = 0$$

$$\frac{\partial p}{\partial v} = 0$$

$$\frac{\partial p}{\partial z} = -\rho g$$



As pressure is a function of z only in this case, we have

$$\frac{dp}{dz} = -\rho g$$

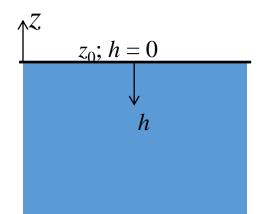
$$\frac{dp}{dz} = -\rho g$$

In general, both ρ and g can vary with z.

However, unless the change in elevation or depth is very large, the change in g can be neglected.

Further, if we are considering an **incompressible liquid**, ρ can also be taken as a constant.

As the z axis is pointing vertically upward, depth increases in the negative z direction.



Let h be the depth of liquid from its surface and let the surface of the liquid be at $z = z_0$.

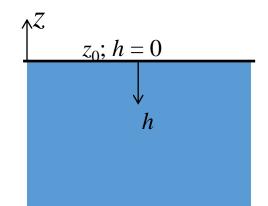
We have, h = 0 at the liquid surface and $h = z_0 - z$, as h is measured positive downward.

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Using the basic equation of fluid statics, we have

$$\frac{dp}{dz} = \rho g_z = -\rho g$$

$$\Rightarrow p - p_0 = -\rho g(z - z_0) = \rho g h$$



where p_0 is the pressure at the liquid surface (i.e., $z = z_0$ or h = 0).

So,

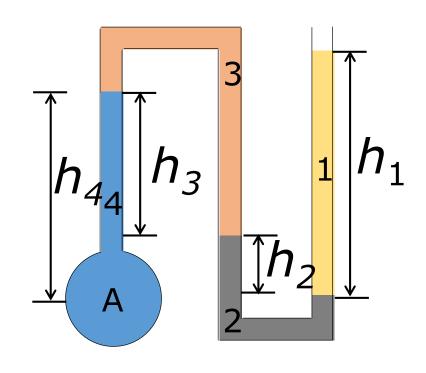
$$p = p_0 + \rho g h$$

Manometer

- ➤ A simple and inexpensive device to measure pressure
- ➤ Note that:
 - Two points at the same elevation in a continuous region of the same liquid are at the same pressure
 - > Pressure increases with increasing depth

Manometer: Example

A manometer has four different fluids as shown in the Figure. Fluid 1 is open to atmosphere. Find the pressure at point A.

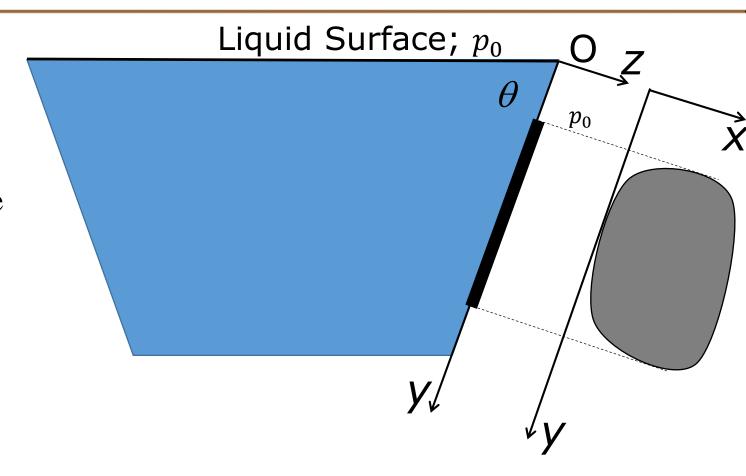


$$p_A = p_{atm} + \rho_1 g h_1 - \rho_2 g h_2 - \rho_3 g h_3 + \rho_4 g h_4$$

➤ Consider a plane submerged surface

Co-ordinates are chosen such that the surface lies in xy plane

- > We would obtain:
 - The magnitude and direction of pressure force on the surface
 - > The line of action of force



Consider an element of surface of area dA at a distance y from O

Pressure force on the surface element caused by the liquid

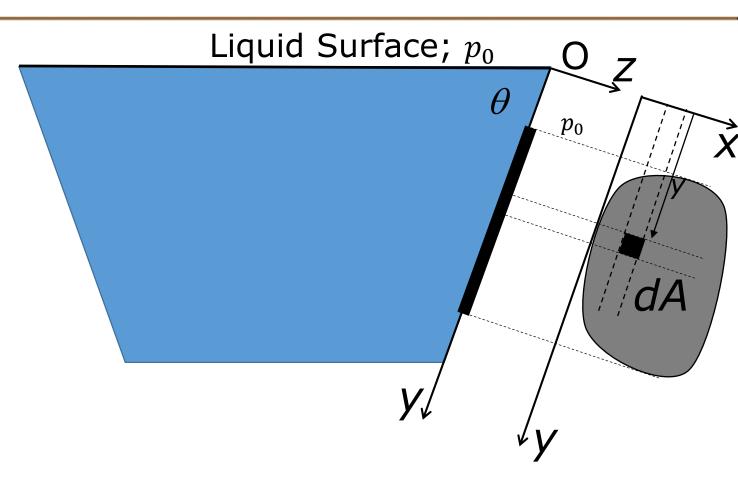
$$dF = p dA$$

Net pressure force on the surface due to liquid

$$\mathbf{F}_{R} = \int_{Area\ of\ plane} p\ dA$$

From hydrostatics,

$$p = p_0 + \rho gy \sin\theta$$



$$\mathbf{F}_{R} = \int_{Area\ of\ plane} (p_{0} + \rho gy\ sin\theta) dA$$

$$\mathbf{F}_{R} = \int_{Area\ of\ plane} (p_{0} + \rho gy\ sin\theta) dA$$

$$\mathbf{F}_{R} = p_{0}A + \rho g \sin\theta \int_{Area\ of\ plane} y\ dA$$

What is $\int_{Area\ of\ plane} y\ dA$?

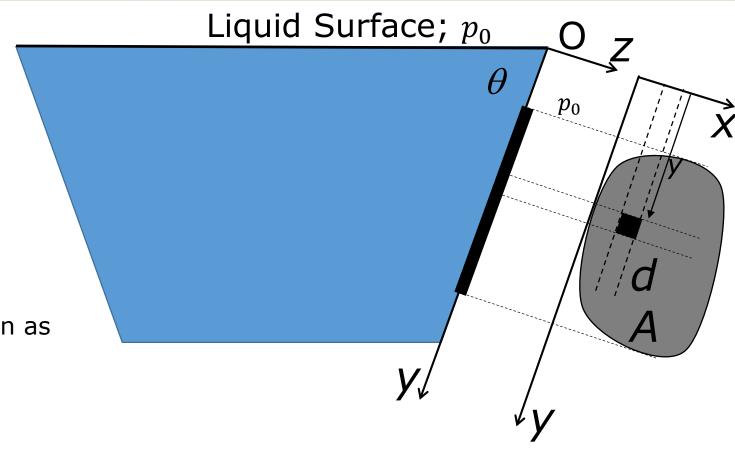
We know that centroid of an area is given as

$$x_C = \frac{\int_{Area} x \, dA}{\int_{Area} dA}; \ y_C = \frac{\int_{Area} y \, dA}{\int_{Area} dA}$$

$$F_R = p_0 A + \rho g y_C \sin \theta A$$

$$\mathbf{F}_R = (p_0 + \rho g y_C sin\theta) A$$

$$\mathbf{F}_R = (p_0 + \rho g h_C) A$$
 where $h_C = y_C sin \theta$ i.e. depth of



To find net force on the surface, the force on other side should also be accounted for

$$\mathbf{F}_{net} = (p_0 + \rho g h_C) A - p_0 A$$

$$\mathbf{F}_{net} = \rho g h_C A$$

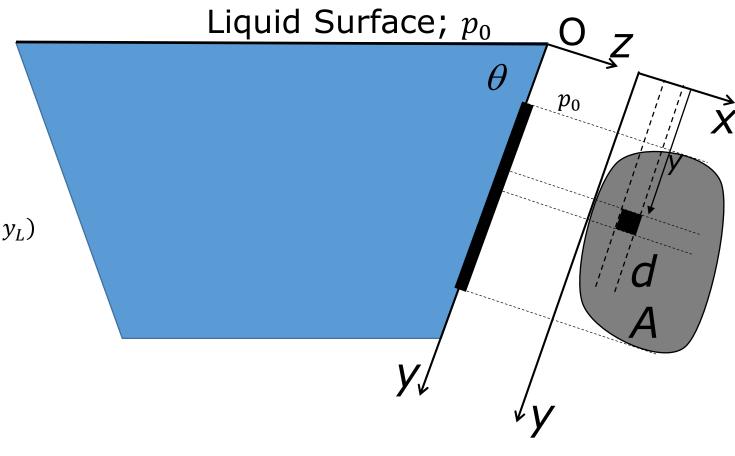
- \triangleright Next, we need to find line of action of F_R
- Remember that the force does not necessarily act at the centroid
 - > Variation of force with y
- \triangleright Let us say the resultant force acts at (x_L, y_L)

Moment of F_R about x-axis = moment of distributed force about x-axis

$$y_L \mathbf{F}_R = \int_{Area\ of\ plane} y\ p\ dA$$

$$y_L = \frac{\int_{Area\ of\ plane} y(p_0 + \rho gysin\theta)\ dA}{\mathbf{F}_R}$$

$$y_{L} = \frac{p_{0} \int_{Area\ of\ plane} y\ dA + \rho g sin\theta \int_{Area\ of\ plane} (y^{2})\ dA}{\mathbf{F}_{R}}$$



Second moment of area:

About x-axis:
$$I_{xx} = \int_A y^2 dA$$

Product moment of area

$$I_{xy} = \int_A xy \ dA$$

Parallel-axis theorem:

$$I_{xx} = I_{xx,centroid} + A y_c^2$$
$$I_{xy} = I_{xy,centroid} + A x_C y_C$$

$$y_{L} = \frac{p_{0} \int_{Area\ of\ plane} y\ dA + \rho g sin\theta \int_{Area\ of\ plane} (y^{2})\ dA}{F_{R}}$$

$$\boxed{F_{R} = (p_{0} + \rho g h_{C})A}$$

$$y_{L} = \frac{p_{0}y_{C}A + \rho g sin\theta \ I_{xx}}{\boldsymbol{F}_{R}} = \frac{p_{0}y_{C}A + \rho g sin\theta \left(I_{xx,centroid} + A \ y_{c}^{2}\right)}{(p_{0} + \rho g y_{C} sin\theta)A}$$

$$y_{L} = \frac{p_{0}y_{C}A + \rho g sin\theta A y_{c}^{2} + \rho g sin\theta I_{xx,centroid}}{(p_{0} + \rho g y_{C} sin\theta)A}$$

$$y_L = y_C + \frac{\rho g sin\theta \ I_{xx,centroid}}{\boldsymbol{F}_R}$$

To find x_L :

Moment of F_R about y-axis = Moment of distributed force

about *y*-axis

$$x_{L}\mathbf{F}_{R} = \int_{Area \ of \ plane} x \ p \ dA$$

$$x_{L}\mathbf{F}_{R} = \int_{Area \ of \ plane} x (p_{0} + \rho gysin\theta) \ dA$$

$$= p_{0} \int_{A} x \ dA + \rho g \sin\theta \int_{A} xy \ dA$$

$$= p_{0}x_{C}A + \rho g \sin\theta I_{xy}$$

$$= p_{0}x_{C}A + \rho g \sin\theta (I_{xy,centroid} + Ax_{C}y_{C})$$

$$x_{L} = x_{C} + \frac{\rho g \sin\theta I_{xy,centroid}}{\mathbf{F}_{R}}$$