

ADVANCED AND MULTIVARIABLE CONTROL

16/6/2022

Solutions

Surname and name

Signature

$$V(x) = x^2$$

Exercise 1 (3 marks)

$$\Delta V(x) = (-x \cos^2(x))^2 - x^2$$

Consider the discrete-time system

$$x(k+1) = -x(k) \cos^2(x(k))$$

$$= \underbrace{(\cos^4(x) - 1)}_{<0} x^2$$

Using a quadratic Lyapunov function, select the correct answer among the following ones

- The origin is an unstable equilibrium
- The origin is a locally stable equilibrium
- The origin is a locally asymptotically stable equilibrium
- The origin is a globally asymptotically stable equilibrium
- No answer

$\Delta V(x) < 0$ in a neighborhood of the origin

$\Delta V(x) < 0$ locally.

Exercise 2 (3 marks)

Concerning the use of the Kalman Predictor or Filter for the continuous time system

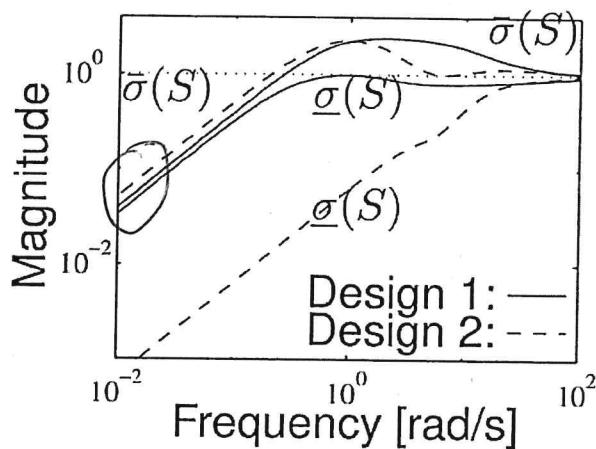
$$\begin{aligned}\dot{x}(t) &= Ax(t) + Bu(t) + v_x(t) \\ y(t) &= Cx(t) + v_y(t)\end{aligned}$$

Select the correct answer

- It can be applied only for asymptotically stable systems
- It can be used only if v_x and v_y are uncorrelated white gaussian noises
- It can be used also when v_x is a stationary stochastic process (with suitable modifications)
- The only condition required to guarantee that the covariance of the state estimation error tends to a limiting value is that the pair (A, C) is observable
- No answer

Exercise 3 (3 marks)

Consider two control designs of a closed-loop system with the following sensitivity functions and select the answer that is surely true



at low frequency
 $\bar{\sigma}(s_1) < \bar{\sigma}(s_2)$

- Design 1 guarantees a faster closed-loop system
- Both designs guarantee closed-loop stability
- Design 1 guarantees slightly more attenuation of high frequency measurement noise
- Design 1 guarantees slightly more attenuation of low frequency process disturbances (d_p)
- No answer

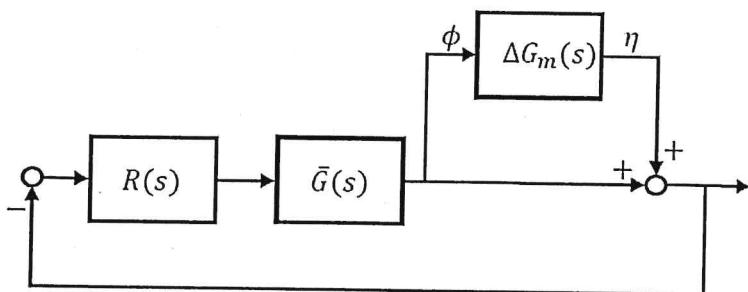
Exercise 4 (3 marks)

In Model Predictive Control of linear systems, it is possible to guarantee robust zero steady state error regulation for constant reference signals y^o also in the case of small model uncertainties or neglected disturbances (assuming that the resulting closed-loop system is asymptotically stable) provided that

- In the cost function to be minimized it is weighted the difference between the predicted state and its asymptotic value corresponding to y^o , in nominal conditions, and the difference between the future input and its asymptotic value corresponding to y^o in nominal conditions (necessary and sufficient condition)
 - The prediction horizon is chosen sufficiently long
 - A model in $\delta x(k) = x(k) - x(k-1)$ and $\delta u(k) = u(k) - u(k-1)$ is used
 - The prediction horizon is selected longer than the control horizon
 - No answer
- not robust
for modeling errors

Exercise 5 (3 marks)

Consider the following control system with multiplicative uncertainty



where

$$\bar{G}(s) = \frac{m}{1+as}, \quad a > 0, \quad R(s) = \frac{k(1+as)}{s}, \quad \Delta G_m(s) = g$$

Select the sufficient condition required to guarantee the stability of the overall system

$\left\| \frac{mgk}{jw+mk} \right\|_{\infty} < 1$

$\left\| \frac{gk(1+jaw)}{jw+mk} \right\|_{\infty} < 1$

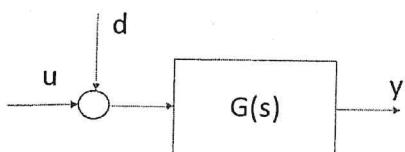
$|g| < 1$

$\left\| \frac{mk}{jw} \right\|_{\infty} < 1$

No answer

Exercise 6 (8 marks)

Consider the following system



$$\text{where } G(s) = \frac{1}{s-1}$$

For this system:

1. Design an observer (full order or reduced order) observer of the disturbance d , assumed to be constant but unknown,
2. Design a compensator of the disturbance
3. Design a feedback regulator with integral action by using the pole-placement approach
4. Show how to implement the regulator in order to avoid that the roots of the polynomial $F(s)$ are zeros of the closed-loop transfer function between the reference and the output.

$$\begin{cases} \dot{x} = x + u + d \\ y = x \end{cases} \rightarrow \begin{cases} \begin{bmatrix} \dot{x} \\ d \end{bmatrix} = \underbrace{\begin{bmatrix} 1 & 1 \\ 0 & 0 \end{bmatrix}}_{\bar{A}} \begin{bmatrix} x \\ d \end{bmatrix} + \underbrace{\begin{bmatrix} 1 \\ 0 \end{bmatrix}}_{\bar{B}} u \\ y = \underbrace{\begin{bmatrix} 1 & 0 \end{bmatrix}}_{\bar{C}} \begin{bmatrix} x \\ d \end{bmatrix} \end{cases}, (\bar{A}, \bar{C}) \text{ observable}$$

Full order observer

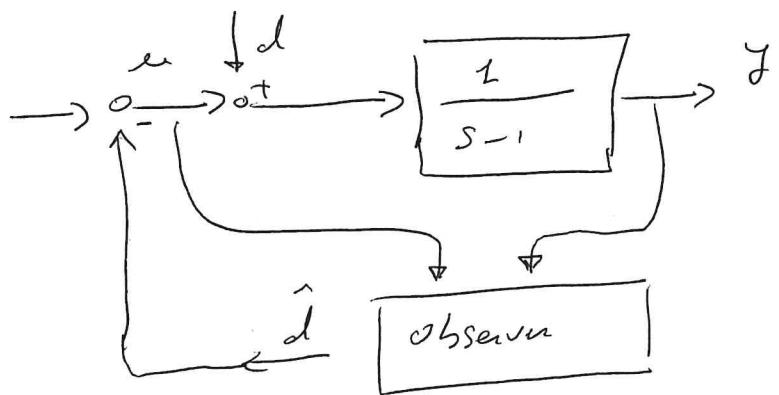
$$\begin{bmatrix} \dot{\hat{x}} \\ \dot{d} \end{bmatrix} = \bar{A} \begin{bmatrix} \hat{x} \\ d \end{bmatrix} + \bar{B} u - L \begin{bmatrix} y - \hat{x} \end{bmatrix}$$

Reduced order observer

$$\begin{bmatrix} \dot{\hat{d}} \\ \dot{\hat{z}} \end{bmatrix} = L \underbrace{\begin{bmatrix} \hat{y} - y - u - \hat{d} \end{bmatrix}}_M \rightarrow \begin{bmatrix} \dot{\hat{d}} \\ \dot{\hat{z}} \end{bmatrix} = -L \hat{y} - Lu - L \hat{d}$$

$$\dot{\hat{z}} = -L \hat{z} - L^2 y - Lu$$

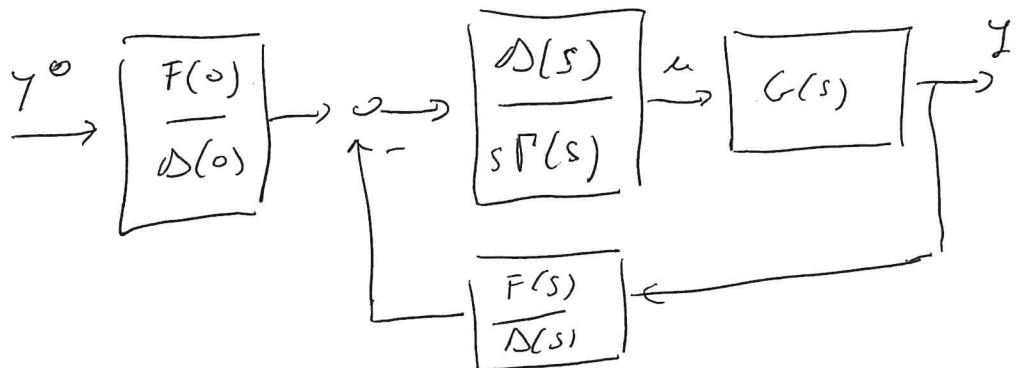
disturbance compensation



Feedback regulator + integral action

$$\tilde{G}(s) = \frac{1}{s(s-1)}, \quad R(s) = \frac{f_1 s + p_0}{g_1 s + g_0}, \quad P(s) = s^3 + p_2 s^2 + p_1 s + p_0$$

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ -1 & 1 & 0 & 0 \\ 0 & -1 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} g_1 \\ g_0 \\ f_1 \\ f_0 \end{bmatrix} = \begin{bmatrix} 1 \\ p_2 \\ p_1 \\ p_0 \end{bmatrix}$$

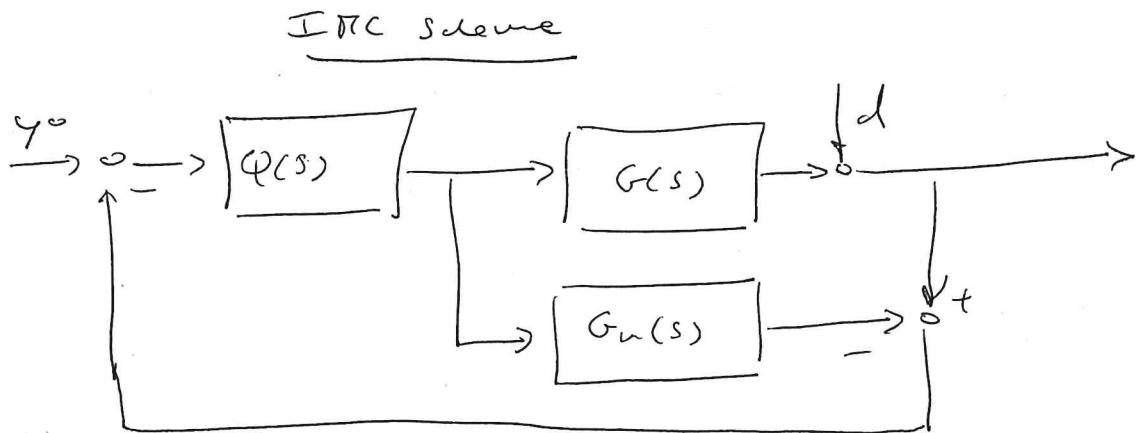


$$\Delta(s) = \sigma_2 s^2 + \sigma_1 s + \sigma_0 \quad (\text{with roots } \tau \text{ as. stable})$$

Exercise 7 (5 marks)

Consider a system described by the transfer function $G(s) = \frac{1-s}{(1+2s)(1+5s)}$

For this system design an Internal Model Controller.



$$Q(s) = G_m^{-1}(s) G_f(s), \quad G_m(s) = \frac{1}{(1+2s)(1+5s)} \cdot (1-s)$$

\downarrow \downarrow
 $G_m(s)$ $G_m(s)$

$$Q(s) = \frac{(1+2s)(1+5s)}{(1+sT)^2}, \quad T > 0,$$

$$G_f(s) = \frac{1}{(1+sT)^2}$$

Exercise 8 (5 marks)

Explain the Loop Transfer Recovery, and in particular:

- Its goal
- Its applicability conditions
- The required choice of the design parameters

a) to recover the robustness properties of LQ control (continuous time) also when an observer is used

b) ~~the~~ conditions for stability of LQ control

and

- $W = P$
- no invariant zeros with $\text{Re}(z) \geq 0$

c) Solution 1

$$L = \rho B, \quad \rho \rightarrow \infty \quad (\text{L is the observer gain})$$

Solution 2

solve KF with
$$\begin{cases} \tilde{Q} = \alpha BB^T, & \alpha \rightarrow \infty \\ \tilde{R} = I \end{cases}$$