

ADVANCED AND MULTIVARIABLE CONTROL

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Surname and Name

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Exercise 1

Consider the system

$$\dot{x}_1(t) = x_2^5(t)$$

$$\dot{x}_2(t) = -x_1(t) - x_2^3(t)$$

- A. Show that the origin is an equilibrium
- B. Show that the equilibrium is asymptotically stable with the Lyapunov theory and the Krasowski La Salle principle using the Lyapunov function $V(x) = 3x_1^2 + x_2^6$.

Solution Exercise 1

a) $0 = \dot{x}_2 \rightarrow \bar{x}_1 = 0$

b)

$$\dot{V}(x) = 6x_1\dot{x}_1 + 6x_2^5\dot{x}_2 = -x_2^8 \leq 0 \rightarrow \text{semidefinite positive}$$

but

$$\dot{V} = 0 \text{ for } x_2 = 0 \text{ and from the first equation } x_1 = \text{const} = \bar{x}_1$$

from the second equation the only possible value is $\bar{x}_1 = 0$

Exercise 2

Given the system

$$\dot{x}(t) = x^3(t) - 2x(t)u(t)$$

$$y(t) = x(t)$$

- Compute the constant input \bar{u} corresponding to the equilibrium $\bar{y} = 2$.
- Compute the linearized model corresponding to the computed equilibrium.
- For the computed linearized system, design a regulator with the pole placement approach guaranteeing closed-loop poles in $s = -1$ and asymptotic zero error for constant reference signals.
- Draw the corresponding control scheme specifying the signals to be used (state and control variables, their variations with respect to the equilibrium values, equilibrium values).

Solution Exercise 2

A.

$$\bar{x}^3 - 2\bar{x}\bar{u} = 0 \rightarrow \bar{u} = 0.5\bar{x}^2 \rightarrow \bar{u} = 2$$

B.

$$\delta \dot{x}(t) = 8\delta x(t) - 4\delta u(t) \rightarrow G(s) = \frac{-4}{s-8}$$

C.

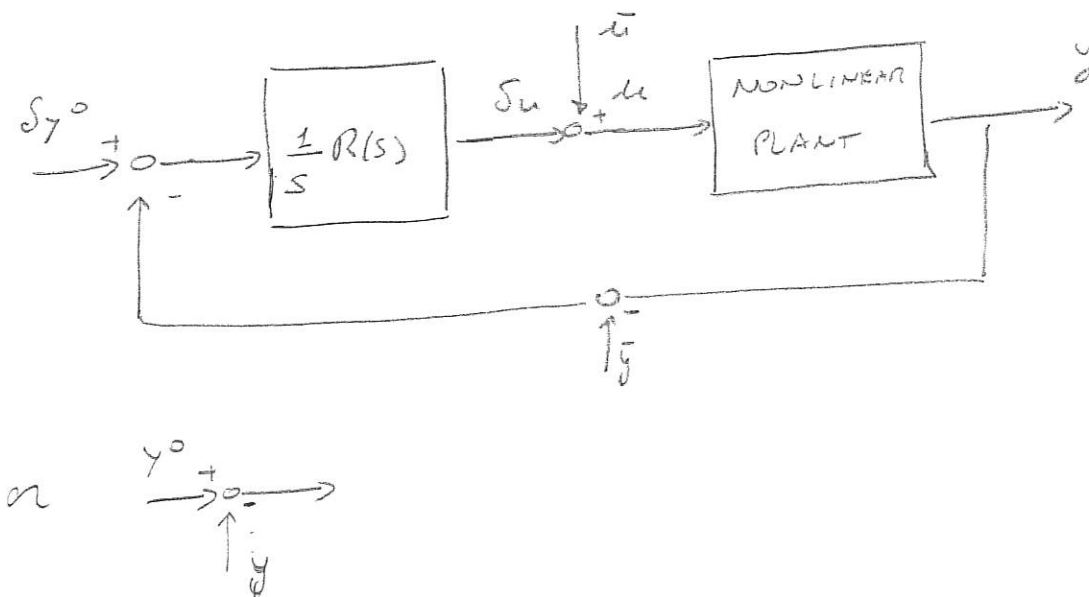
First insert an integrator

$$G'(s) = \frac{-4}{s(s-8)}$$

Then solve the pole placement approach with the solution based on transfer functions (or any other, if you prefer)

$$R(s) = \frac{f_1 s + f_0}{\gamma_1 s + \gamma_0} \rightarrow \begin{bmatrix} 1 & 0 & 0 & 0 \\ -8 & 1 & 0 & 0 \\ 0 & -8 & -4 & 0 \\ 0 & 0 & 0 & -4 \end{bmatrix} \begin{bmatrix} \gamma_1 \\ \gamma_0 \\ f_1 \\ f_0 \end{bmatrix} = \begin{bmatrix} 1 \\ 3 \\ 3 \\ 1 \end{bmatrix}$$

D.



Exercise 3

Given the discrete-time system

$$x(k+1) = -x(k) + u(k)$$

and the cost function

$$J = \sum_{i=0}^{\infty} (0.5x^2(k+i) + u^2(k+i))$$

- A) Compute the solution of the infinite time LQ control ($N=\infty$) and the corresponding closed-loop eigenvalue.
- B) Discuss the robustness properties guaranteed by infinite-horizon LQ control of discrete-time systems.

Discuss the robustness properties guaranteed by infinite-horizon LQ control of discrete-time systems.

$$\text{Riccati equation } P(k) = Q + A'P(k+1)A - A'P(k+1)B(R+B'P(k+1)B)^{-1}B'P(k+1)A$$

Solution Exercise 3

A.

The steady state solution of the stationary Riccati equation with $A=B=R=1$, $Q=0.5$, is $P=1$, which corresponds to $K=(R+B'PB)^{-1}B'PA=0.5$, therefore $A-BK=0.5$.

B.

See the notes, pag 171-172

Anyway, $\bar{r} = \frac{R}{R+B'\bar{P}B} = \frac{1}{2}$, $\gamma = \sqrt{\bar{r}} = 0.7071$

guaranteed gain margin $\left[\frac{1}{1+\gamma}, \frac{1}{1-\gamma} \right] = [0.58, 3.41]$

Exercise 4

$$\dot{x}_1(t) = -x_1(t) + u(t)$$

$$\dot{x}_2(t) = x_1(t) + x_2(t)$$

$$y_1(t) = x_1(t) + x_2(t)$$

$$y_2(t) = x_1(t)$$

A. compute the corresponding transfer function matrix;

B. show how to use, in this case, a static (order zero) observer to estimate the state from the measured outputs;

C. select the output which can asymptotically controlled to an arbitrary constant reference signal;

D. draw the scheme of a feedback controller guaranteeing that the selected output is asymptotically brought to a constant reference.

Solution Exercise 4

A.

$$A = \begin{bmatrix} -1 & 0 \\ 1 & 1 \end{bmatrix}, \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}, \quad C = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix}$$

$$G(s) = C(sI - A)^{-1}B = \begin{bmatrix} \cancel{s}/(s+1)(s-1) \\ (s-1)/\cancel{(s+1)(s-1)} \end{bmatrix}$$

B.

Since matrix C is square and nonsingular, one can set

$$x = C^{-1}y$$

This corresponds to a reduced order observer ($n=p=2, n-p=0$)

C.

By looking at the two transfer functions, it is apparent that from u to y_1 there is a derivative action, so that the zero error regulation for constant references cannot be achieved. On the contrary, it is possible to guarantee it for the second output y_2 .

D.

The corresponding scheme is

