

### Exercise 1.a

Consider the system

$$\dot{x}_1(t) = -x_1(t) + x_2(t)$$

$$\dot{x}_2(t) = -x_1^3(t) - x_2^3(t)$$

and the Lyapunov function  $V(x) = bx_1^4 + ax_2^2(t)$ . Select proper values of  $a, b$  such that  $V(x)$  can be used to prove the stability of the origin.

$$\dot{V} = -4bx_1^4 + 4bx_1^3x_2 - 2ax_1^3x_2 - 2ax_2^4$$

a.  $a=1, b=1$  ( $\dot{V} = -4x_1^4 + 2x_1^3x_2 - 2x_2^4$ )

b.  $a=2, b=1$  ( $\dot{V} = -4x_1^4 - 4x_2^4 < 0$ )

c.  $a=0, b=1$  ( $V$  is not a Lyapunov function)

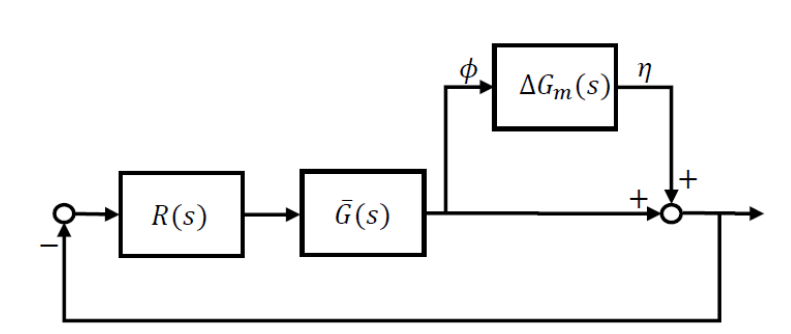
### Exercise 1.b

In view of the previous answer, the origin is (*select the strongest property*)

- a. stable
- b. locally asymptotically stable
- c. globally asymptotically stable

### Exercise 2

Given the following feedback system, assume that in the nominal case ( $\Delta G_m(s)=0$ ) the system is asymptotically stable and that  $\Delta G_m(s)$  is asymptotically stable. Select the sufficient condition guaranteeing that in the perturbed case the asymptotic stability of the closed-loop system is maintained.



- a.  $|T(jw)\Delta(jw)| < 1$ , for any  $w \geq 0$
- b.  $|S(jw)\Delta G_m(jw)| < 1$ , for any  $w \geq 0$
- c.  $|S(jw)R(jw)\Delta G_m(jw)| < 1$ , for any  $w \geq 0$

### Exercise 3.a

Consider the system with the following transfer function  $G(s)$

$$\begin{bmatrix} \frac{a}{(s+1)} & \frac{b}{(s+1)(s+2)} \\ \frac{c}{(s+2)} & \frac{d}{(s+2)} \end{bmatrix}$$

The set of poles (with the proper multiplicity) is

- a. -1,-1,-2,-2,-2
- b. -1,-2,-2
- c. -1, -2

$$\det G(s) = \frac{ad(s+2)-bc}{(s+1)(s+2)^2}$$

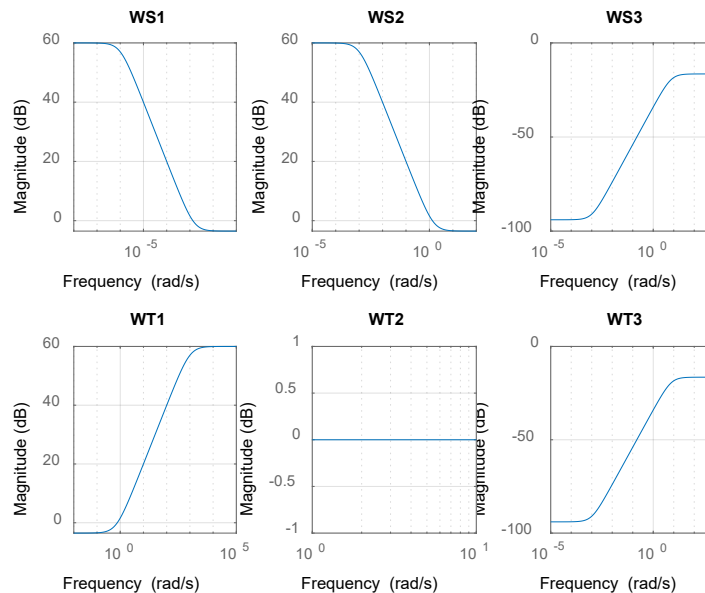
### Exercise 3.b

The system must not have zeros at the origin. The zero is  $s=(2ad-bc)/ad$ . Therefore it must be  $2ad$  not equal to  $bc$

- a.  $a=b=c=d=1$
- b.  $a=b=d=1, c=2$
- c. for any value of  $a, b, c, d$

#### Exercise 4

Consider the design of a  $H_2/H_{\infty}$  controller with shaping functions for a SISO system. Which one of the following pairs  $(W_{Si}, W_{Tj})$  of the functions shown in the figure is reasonable and coherent with the goals of the control design procedure?



- a. WS3-WT2    WT2 does not make sense
- b. WS2- WT1    acceptable**
- c. WS1 -WT3    WT3 is not acceptable, small gain at high frequency

#### Exercise 5

Consider the system

$$\begin{aligned}\dot{x}_1(t) &= bu(t) \\ \dot{x}_2(t) &= x_1(t) + u(t)\end{aligned}$$

and assume that you want to design an infinite horizon LQ control with  $Q=\text{diag}(q_1, q_2)$ ,  $R=1$ .

- A. Compute the necessary conditions guaranteeing that the solution of the infinite horizon LQ control is stabilizing.
  - a. any  $b, q_1 > 0, q_2 > 0$  no, lack of reachability if  $b=0$
  - b.  $b \neq 0, q_1 > 0, q_2 \geq 0$  no lack of observability if  $q_2=0$
  - c.  $b \neq 0$ , any  $q_1 \geq 0, q_2 > 0$  yes**

B. With  $Q=I$ ,  $b=1$ , the solution of the steady-state Riccati equation is  $P=I$ . What are the closed-loop eigenvalues? Recall the steady state Riccati equation of LQinf control:  $A'P + PA + Q - PBR^{-1}B'P = 0$

- a. -1,-2
- b. -2,-2
- c. -1,-1

C. Assume now to implement the feedback control law  $u(t) = -\rho Kx(t)$  ( $K$  is again the solution of the LQinf problem), specify the set of values of  $\rho$  guaranteed by LQ control so that the closed-loop system remains asymptotically stable.

- a.  $\rho$  in  $(0, \infty)$
- b.  $\rho$  in  $(0.5, \infty)$
- c.  $\rho$  in  $(-0.5, 0.5)$

A.

$$A = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}, \quad B = \begin{bmatrix} b \\ 1 \end{bmatrix} \rightarrow \text{reachability matrix } M_r = \begin{bmatrix} B & AB \end{bmatrix} = \begin{bmatrix} b & 0 \\ 1 & b \end{bmatrix} \rightarrow \text{condition } b \neq 0$$

$$Q = \begin{bmatrix} q_1 & 0 \\ 0 & q_2 \end{bmatrix} \rightarrow Q^{1/2} = \begin{bmatrix} \sqrt{q_1} & 0 \\ 0 & \sqrt{q_2} \end{bmatrix} \rightarrow \text{observability matrix } M_o = \begin{bmatrix} Q^{1/2} \\ Q^{1/2}A \end{bmatrix} = \begin{bmatrix} \sqrt{q_1} & 0 \\ 0 & \sqrt{q_2} \\ 0 & 0 \\ \sqrt{q_2} & 0 \end{bmatrix} \rightarrow q_2 > 0$$

B.

$$K = R^{-1}B'P = \begin{bmatrix} 1 & 1 \end{bmatrix} \rightarrow A - BK = \begin{bmatrix} -1 & -1 \\ 0 & -1 \end{bmatrix} \rightarrow \text{eigenvalues } -1, -1$$

C.

The loop transfer function is  $K(sI-A)^{-1}B = (2s+1)/s^2$ . In order to compute the gain margin, consider the characteristic equation  $s^2 + 2\rho s + \rho = 0$  with stable roots for any  $\rho > 0$ . The gain margin is  $(0, \infty)$ .

## Exercise 6

EKF: see the notes and the slides

## Exercise 7

MPC: see the notes and the slides