AP-266 Aerostructural Optimization Homework 02

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Instructions

- Due date: April 5th, 2019. 11:59 PM.
- Send the solutions to ney@ita.br.
- Send the source code as well. The code should have comments.
- You may discuss solution approaches with other students, but you must write your own solution. Do NOT share
 your code.
- Late delivery penalty: 20% of the total score per late day.

1 Newton's Method

Consider the multidimensional quadratic function below:

$$f(\vec{x}) = \frac{1}{2}\vec{x}^T \mathbf{P}\vec{x} + \vec{q}^T \vec{x} + r \tag{1}$$

where \mathbf{P} , \vec{q} , and r are constant, and \vec{x} is a vertical vector. Also, \mathbf{P} is a symmetric positive-definite matrix. Let \vec{x}_0 be the starting point for the Newton's Method. Prove that the Newton's Method converges to the MINIMUM of the quadratic in a single step.

2 Gradient-based Optimization

Let's continue using the Rosenbrock's function from the previous homework assignment:

$$f(\vec{x}) = \sum_{i=1}^{n-1} [100(x_{i+1} - x_i^2)^2 + (1 - x_i)^2]$$
 (2)

where $\vec{x} = [x_1, x_2, \dots, x_n].$

2.1 Part a)

Write Python3 programs to minimize the Rosenbrock's function using analytical gradients for any dimension n using:

- 1. The Conjugate Gradient (CG) Algorithm, starting at the point $\vec{x} = [0, 0, \dots, 0]$
- 2. The BFGS Algorithm, starting at the point $\vec{x} = [0, 0, \dots, 0]$

These two algorithms are already implemented in the scipy.optimize.minimize module, just like the Nelder-Mead Simplex method (see the documentation here).

Remember to create a function that provides analytical gradients to the minimize function. For example, if you have a function named rosen_grad that computes gradients, you should call the minimize function with:

Solve the optimization problem for n = 2, n = 4, and n = 6. Provide the final values of design variables, objective function, and number of function evaluations.

2.2 Part b)

Now let's check how these algorithms scale with the number of design variables. Create a plot showing the number of function evaluations with respect to the number of design variables of the problem for these algorithms. Plot all curves in the same plot. Also add the curves from the Nelder-Mead and Differential Evolution methods. Try reaching at least n=20.

ATTENTION: The cost of computing jacobians with reverse AD is has roughly the same order of magnitude as the function evaluation. Therefore, use the number of functions evaluations (results.nfev) plus the number of jacobian evaluations (results.njev) as the total number of evaluations when comparing CG and BFGS agains the gradient-free methods

Do your best to make a fair comparison between the algorithms, for instance, by using the same solution tolerance. To check that, make another plot with the optimized objective function value versus the number of design variables for all optimization algorithms. Plot all curves in the same plot and use a log scale for the vertical axis.

The computational cost of these methods is roughly proportional to what power of n?

3 Algorithmic Differentiation

This exercise will help you continue coding the lifting-line optimization code that is required for the final report.

In the previous assignment, you implemented a Fortran subroutine to compute the velocity induced at an arbitrary point by a set of linked vortices. Recall that for n_v linked vortices, we get a 3 by n_v matrix of aerodynamic influence coefficients:

The lifting line theory requires that we compute the velocities induced by the linked vortices at a set of control points. Each horseshoe vortex has a corresponding control point at the mid point of the finite vortex segment, as shown in Fig. 1.

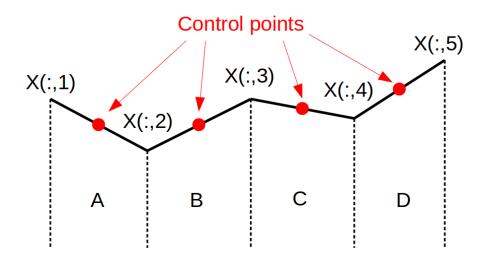


Figure 1: Control points of the horseshoe vortices.

As an example, the control point of the vortex B would be:

$$\vec{X}_B = \frac{\vec{X}_2 + \vec{X}_3}{2} \tag{3}$$

For n_v vortices, there are n_v corresponding control points. Therefore, we will have a set of n_v matrices of size 3 by n_v representing all combinations of vortices and control points. We can gather all these matrices and represent them as a tridimensional matrix **AIC** of size 3 by n_v by n_v as follows:

$$\mathbf{AIC} = \begin{bmatrix} \vec{\gamma}_{1,1} & \vec{\gamma}_{2,1} & \cdots & \vec{\gamma}_{n_v,1} \\ \vec{\gamma}_{1,2} & \vec{\gamma}_{2,2} & \cdots & \vec{\gamma}_{n_v,2} \\ \vdots & \vdots & \ddots & \vdots \\ \vec{\gamma}_{1,n_v} & \vec{\gamma}_{2,n_v} & \cdots & \vec{\gamma}_{n_v,n_v} \end{bmatrix}$$
(4)

where $\vec{\gamma}_{i,j}$ is the aerodynamic influence vector induced by vortex i at the control point of vortex j.

The AIC matrix has three dimensions, as stated previously. The first dimension represents the component (x, y, or z) of the aerodynamic influence vector $(\vec{\gamma})$, the second dimension represents the index of the inducing vortex, and the third dimension represents the index of the induced control point. For example, AIC(2,1,5) should be the y component of the aerodynamic influence vector induced by the first horseshoe vortex over the control point of the fifth horseshoe vortex. Thus, AIC(:,i,j) should be equal to $\vec{\gamma}_{i,j}$.

3.1 Computing the AIC matrix

We will add a new subroutine to the *llt_module.F90* file to compute the matrix **A**. This subroutine should be named get_AIC_matrix and use the following sintax:

```
subroutine get_AIC_matrix(n_vort, X, Uinf, AIC)
! This subroutine computes the Aerodynamic Influence Coefficients (AIC)
! matrix that gives the adimensionalized induced velocities in
! all bound segments in X, that is: Vind = AIC*Gamma.
! Vind(1:3,ii) = AIC(1:3,:,ii)*Gamma(:)
!
! INPUTS
!
! n_vort: integer -> Number of horseshoe vortices.
! X: real(3,n_vort+1) -> Coordinates of the kinks of the horseshoe vortices.
! Uinf: real(3) -> Unitary vector along the free-stream direction.
!
! OUTPUTS
!
! AIC: real(3,n_vort,n_vort) -> Aerodynamic Influence matrix.
```

Here is a pseudo-code to guide you in the implementation:

- 1. for ii varying from 1 to n_v :
 - (a) Extract from the matrix X the coordinates X1ii and X2ii of the kinks of the ii-th vortex.
 - (b) Compute the position of the control point Xc of this vortex by taking the average between X1ii and X2ii.
 - (c) for jj varying from 1 to n_v :
 - i. Extract from the matrix X the coordinates X1jj and X2jj of the kinks of the jj-th vortex.
 - ii. Compute the aerodynamic influence vector gamma_ind between vortices ii and jj using the induced_vel function written in the previous homework assignment.
 - iii. Store the value of gamma_ind at AIC[:,jj,ii].

test you implementation for the following case:

•
$$\vec{u}_{\infty} = [1, 0, 0]$$
 and $\mathbf{X} = \begin{bmatrix} 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 2.0 & 3.0 \\ 0.0 & 0.0 & 0.0 & 0.0 \end{bmatrix}$

The non-zero values of the AIC matrix for this case are:

$$\mathtt{AIC(3,:,:)} = \begin{bmatrix} -0.31830988618379069 & 0.10610329539459691 & 2.1220659078919374E - 002 \\ 0.10610329539459691 & -0.31830988618379069 & 0.10610329539459691 \\ 2.1220659078919374E - 002 & 0.10610329539459691 & -0.31830988618379069 \end{bmatrix} \tag{5}$$

Give the aerodynamic influence matrices **AIC** for the following case:

•
$$\vec{u}_{\infty} = [1, 0, 0]$$
 and $\mathbf{X} = \begin{bmatrix} 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 2.0 & 3.0 \\ 0.0 & 0.1 & 0.2 & 0.3 \end{bmatrix}$

Print AIC(1,:,:), then AIC(2,:,:), and then AIC(3,:,:).

3.2 Testing the LLT method functions

Take your versions of the induced_vel and get_AIC_matrix subroutines and add them to the llt_module_incomplete.f90 file given in the homework folder. Then rename this file as llt_module.f90. You may have to include you dot product, cross product, and norm subroutines into the module as well.

This file has all necessary subroutines to compute the residual and functions of interest of the lifting-line theory. These tasks are performed by the get_residuals and the get_functions subroutines, which are already implemented.

Check if the implementation is correct by running the get_residuals for the following case:

$$\bullet \ \mathbf{X} = \left[\begin{array}{cccc} 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 2.0 & 3.0 \\ 0.0 & 0.0 & 0.0 & 0.0 \end{array} \right]$$

- \bullet Gama = [2.0 2.0 2.0]
- \bullet alpha0 = [0.0 0.0 0.0]
- \bullet chords = [0.3 0.3 0.3]
- \bullet cl0 = [0.0 0.0 0.0]
- cla = [6.283 6.283 6.283]
- $Vinf = [1.0 \ 0.0 \ 0.0]$
- rho = 1.0

You should get: res = [6.4261187504344397, 5.0646641230067555, 6.4261187504344388] Now execute the get_functions subroutine for the same set of inputs. You should get:

- Sref = 0.899999999999991
- \bullet CL = 13.333333333333334
- \bullet CD = 4.3384458561346291
- \bullet L = 6.000000000000000
- D = 1.9523006352605827

Rerun the two subroutines for this new set of inputs:

$$\bullet \ \mathbf{X} = \left[\begin{array}{cccc} 0.0 & 0.0 & 0.0 & 0.0 \\ 0.0 & 1.0 & 2.0 & 3.0 \\ 0.2 & 0.0 & 0.0 & 0.2 \end{array} \right]$$

- \bullet Gama = [1.0 2.0 1.0]
- \bullet alpha0 = [0.0 0.1 0.0]
- \bullet chords = $[0.3 \ 0.6 \ 0.3]$
- \bullet cl0 = [0.0 0.0 0.0]
- cla = [6.283 6.283 6.283]
- $Vinf = [1.0 \ 0.0 \ 0.0]$
- rho = 1.0

Provide the values you obtained for: res, Sref, CL, CD, L, and D

3.3 Differentiating the code

We need to differentiate the get_residuals and the get_functions subroutines to apply the adjoint method. The problem is that Tapenade's web interface accepts only a single subroutine as starting point for the differentiation process. Therefore, we need to create a dummy subroutine named tapenade_main that calls the two subroutines we want to differentiate. Create a tapenade_main subroutine at the end of the llt_module.f90 file with the following syntax:

```
subroutine tapenade_main(n_vort, X, Gama, alpha0, chords, cl0, cla, Vinf, rho, &
                         res, Sref, CL, CD, L, D)
! Dummy subroutine to allow differentiation of get_residuals and
! get_functions in a single Tapenade call.
! INPUTS
! n_vort: integer -> Number of horseshoe vortices.
! X: real(3,n_vort+1) -> Coordinates of the kinks of the horseshoe vortices.
! Gama: real(n_vort) -> Circulation intensity of each horseshoe vortex.
! alpha0: real(n_vort) -> Array of local incidence angles.
! chords: real(n_vort) -> Array of local chords.
! cl0: real(n_vort) -> cl0 of each 2D section
! cla: real(n_vort) -> lift curve slope of each 2D section [1/rad]
! Vinf: real(3) -> Free-stream velocity vector
! rho: real -> Air density
Ţ
! OUTPUTS
! res: real(n_vort) -> Residuals of the LLT method
! Sref: real -> Area of all panels
! CL: real -> Lift coefficient (adimensionalized by Sref)
! CD: real -> Drag coefficient (adimensionalized by Sref)
! L: real -> Lift force
! D: real -> Drag force
```

Once the subroutine is implemented, use the send_to_tapenade.py script to generate differentiated versions of the llt_module.f90 file in forward and reverse modes. The differentiation should be done with respect to the following variables:

- Input variables: X, Gama, alpha0, chords.
- Output variables: res, Sref, CL, CD, L, D.

3.4 Finite difference test

Let's use the finite difference method to compute the directional derivative of the residuals res with respect to the inputs variables.

In our case, since we have 4 input variables (X, Gama, alpha0, and chords), we need to define 4 perturbation directions (Xd, Gamad, alpha0d, and chordsd) to compute a direction derivative. For this exercise, use the first set of inputs from Sec. 3.2 and the following perturbation directions:

$$\bullet \ \mathbf{Xd} = \left[\begin{array}{cccc} -0.1 & 0.5 & 0.2 & 0.0 \\ 1.0 & -0.7 & 0.1 & -0.9 \\ 0.3 & 0.0 & -0.6 & 0.2 \end{array} \right]$$

- $Gamad = [-1.0 \ 0.5 \ 0.3]$
- $alpha0d = [0.0 \ 0.1 \ -0.1]$
- chordsd = [1.0 -0.2 0.7]

You should perturb each input variable in a small amount along these direction, compute the residuals at this new location, and use finite differences to estimate the directional derivative:

directional deriv. of
$$res = \frac{1}{h} [res1 - res]$$
 (8)

NOTE: the directional derivative of res should have the same number of elements as the variable res.

We can also use the forward AD version of the get_residuals subroutine to get the directional derivative by using the perturbation directions as derivative seeds:

Test different values of $h = 10^n$ and find the step size magnitude (n) that gives the smallest difference between the directional derivatives estimated with these two methods. You do not need to run an optimization to find the best h, just give the order of magnitude. Use the norm of the difference between arrays as metric:

$$difference = |FD directional deriv. - AD directional deriv.|$$
 (10)

Give the values of the directional derivative computed by the AD code.

Repeat the same process to verify the directional derivatives of the $get_functions$ subroutine. Use the same set of perturbation directions and step size h from the previous test. Compute the difference between directional derivatives estimated with the finite difference method and the forward AD code. Also give the directional derivatives of: Sref, CL, CD, L, and D.

3.5 Dot product test

Now we will use the dot product test to verify the reverse AD code.

Run the forward AD version of the get_residuals subroutine with this set of arbitrary derivative seeds:

$$\bullet \mathbf{Xd} = \begin{bmatrix} -0.1 & 0.5 & 0.2 & 0.0 \\ 1.0 & -0.7 & 0.1 & -0.9 \\ 0.3 & 0.0 & -0.6 & 0.2 \end{bmatrix}$$

- $Gamad = [-1.0 \ 0.5 \ 0.3]$
- $alpha0d = [0.0 \ 0.1 \ -0.1]$
- chordsd = [1.0 0.2 0.7]

Give the derivative seeds of the outputs: resd.

Next, execute the reverse AD version of get_residuals subroutine with this set of arbitrary derivative seeds:

• resb = [0.1 - 0.2 0.3]

Give the derivative seeds of the inputs: Xb, Gamab, alpha0b, chordsb.

Now do the dot product test by adding the contributions of the input variables and by subtracting the contributions of the output variables:

Write the value you obtained for dotprod. The final value of the dot product should be zero (to machine precision). Now we will repeat the same process for the get_functions subroutine. Use the same input derivative seeds and give the corresponding derivative seeds you got for Srefd, CLd, CDd, Ld, and Dd.

Then execute the reverse AD version of get_functions subroutine with this set of arbitrary derivative seeds:

- Srefb = 0.6
- \bullet CLb = -0.2
- \bullet CDb = 0.1

- Lb = -0.3
- \bullet Db = 0.7

Give the derivative seeds of the inputs: Xb, Gamab, alpha0b, chordsb.

Now do the dot product test by adding the contributions of the input variables and by subtracting the contributions of the output variables:

Write the value you obtained for dotprod. The final value of the dot product should be zero (to machine precision).

3.6 Troubleshooting

If the dot product is not zero, it may due to a couple of things:

- If you are using the -fdefault-real-8 flag when compiling Fortran code, you should also set the real4toreal8 flag to True in the send_to_tapenade.py script.
- The reverse AD code modifies the content of the reverse AD seeds of the output variables. Therefore, make a copy of these derivative seeds before calling the reverse AD code, so that you still have the original seeds for the dot product test.
- Remember to set the reverse AD seeds of the input variables to 0.0 before calling the reverse AD code, since the code just accumulate values to these seeds. Previous values stored in the memory will interfere with your results if you do not initialize the seeds.
- Sometimes the differentiation does not work when you use the same variable twice as arguments of a function. For instance, assume that you have a subroutine dot(a,b,adotb) that computes the dot product of the vector a and b. You can use this same subroutine to compute the square of the norm of vector a by calling: dot(a,a,norma2). The reverse differentiation may not work well because Tapenade may not recognize that the two arguments of dot are in fact the same variable. To get around this case, it is better to define a new dedicated subroutine norm(a,norma2) to compute the norm of a vector.