

Lecture 18 - The Jacobian & Static Force Analysis

- Jacobian for Velocity Analysis

$$\textcircled{1} \begin{bmatrix} {}^A\omega_B \\ {}^A\nu_B \end{bmatrix} = {}^A J_B \dot{\theta}$$

↖ Frame being described
↙ Frame of expression

Jacobian for the velocities of $\{B\}$ expressed in $\{A\}$

$$\textcircled{2} \begin{bmatrix} {}^c\omega_c \\ {}^c\nu_c \end{bmatrix} = {}^c X_A \begin{bmatrix} {}^A\omega_A \\ {}^A\nu_A \end{bmatrix} \quad \text{when } \{C\} \text{ and } \{A\} \text{ rigidly attached}$$

Today:

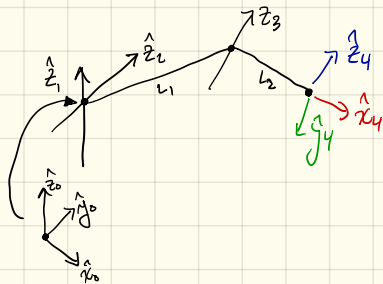
- Jacobian wrap-up
 - Spatial reasoning
 - Changing Frames
- Statics analysis for end-effector forces

$${}^4\omega_4 = {}^4J_4 \dot{\theta} = [{}^4v_{4,1} \ {}^4v_{4,2} \ {}^4v_{4,3}] \dot{\theta} \quad {}^tV_{t,i} = {}^tX_i \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} {}^iR_t^T \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\ -{}^iR_t^T \begin{bmatrix} p_t x \\ 0 \\ 1 \end{bmatrix} \end{bmatrix}$$

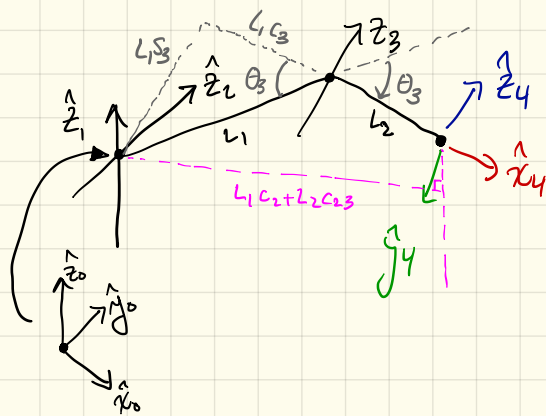
$${}^1T_4 = \begin{bmatrix} c_{23} & -s_{23} & 0 & L_2 c_{23} + L_1 c_2 \\ 0 & 0 & 1 & 0 \\ -s_{23} & -c_{23} & 0 & -L_2 s_{23} - L_1 s_2 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^2T_4 = \begin{bmatrix} c_3 & -s_3 & 0 & L_1 + L_2 c_3 \\ s_3 & c_3 & 0 & L_2 s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad {}^3T_4 = \begin{bmatrix} 1 & 0 & 0 & L_2 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Compute the Second Column of the Jacobian 4J_4 : ${}^4v_{4,2}$

$${}^4v_{4,2} = {}^4X_2 \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} = \begin{bmatrix} {}^2R_4^T \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\ {}^2R_4^T \left(\begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times {}^2p_4 \right) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \frac{1}{L_1} s_3 \\ L_2 + L_1 c_3 \\ 0 \end{bmatrix}$$



Spatial Reasoning:



Warm Up: Third column of the Jacobian ${}^4\bar{J}_4$

$$\begin{bmatrix} {}^4\omega_4 \\ {}^4\nu_4 \end{bmatrix} \bigg|_{\dot{\theta}_2=1, \dot{\theta}_1=\dot{\theta}_3=0} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ \hline 0 \\ L_2 \\ 0 \end{bmatrix}$$

Since \hat{z}_3 and \hat{z}_4 aligned
Since rotation about \hat{z}_3 creates velocity along \hat{y}_4

First Column of ${}^4\bar{J}_4$:

$$\begin{bmatrix} {}^4\omega_4 \\ {}^4\nu_4 \end{bmatrix} \bigg|_{\dot{\theta}_1=1, \dot{\theta}_2=\dot{\theta}_3=0} = \begin{bmatrix} -s_{23} \\ -c_{23} \\ \hline 0 \\ 0 \\ 0 \\ L_1c_2 + L_2c_{23} \end{bmatrix}$$

when $\theta_{23} = 0^\circ$, ${}^4\omega_4 = \begin{bmatrix} 0 \\ -1 \\ 0 \end{bmatrix}$

when $\theta_{23} = 90^\circ$, ${}^4\omega_4 = \begin{bmatrix} -1 \\ 0 \\ 0 \end{bmatrix}$

Second column of ${}^4\bar{J}_4$

$$\begin{bmatrix} {}^4\omega_4 \\ {}^4\nu_4 \end{bmatrix} \bigg|_{\dot{\theta}_2=1, \dot{\theta}_1=\dot{\theta}_3=0} = \begin{bmatrix} 0 \\ 0 \\ 1 \\ \hline L_1s_3 \\ L_2 + L_1c_3 \\ 0 \end{bmatrix}$$

Changing Frames of Expression:

$${}^4\bar{J}_4 \stackrel{?}{\Longleftrightarrow} {}^0J_4$$

$${}^0R_4, {}^0P_4$$
$${}^0X_4, {}^4X_0$$

$$\begin{bmatrix} {}^0\omega_4 \\ {}^0\dot{N}_4 \end{bmatrix} = {}^0\bar{J}_4 \dot{\Theta}$$

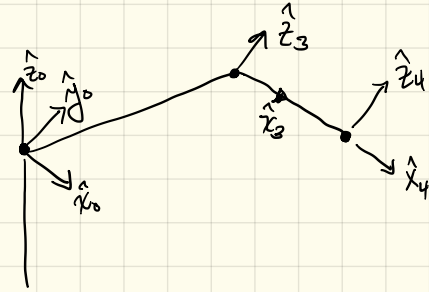
$$= \begin{bmatrix} {}^0R_4 {}^4\omega_4 \\ {}^0R_4 {}^4\dot{N}_4 \end{bmatrix} = \begin{bmatrix} {}^0R_4 & 0 \\ 0 & {}^0R_4 \end{bmatrix} \begin{bmatrix} {}^4\omega_4 \\ {}^4\dot{N}_4 \end{bmatrix} = \begin{bmatrix} {}^0R_4 & 0 \\ 0 & {}^0R_4 \end{bmatrix} {}^4\bar{J}_4 \dot{\Theta}$$

$$\boxed{{}^0\bar{J}_4 = \begin{bmatrix} {}^0R_4 & 0 \\ 0 & {}^0R_4 \end{bmatrix} {}^4\bar{J}_4}$$

Can we also change the frame of description?

what is ${}^4\bar{J}_4$?

(a) $\begin{bmatrix} {}^4P_3 & 0 \\ 0 & {}^4P_3 \end{bmatrix} {}^3\bar{J}_3 = {}^4\bar{J}_3$



(b) ${}^4X_3 {}^3\bar{J}_3$ ✓

(c) $(6 \times 6) \cdot (6 \times n) \cdot (6 \times 6)$ (x)
 ${}^4X_3 {}^3\bar{J}_3 {}^3X_4$

(d) None of the above

• Yes when two frames are rigidly attached to the same body.

$$\begin{bmatrix} {}^4\omega_4 \\ {}^4\dot{\theta}_4 \end{bmatrix} = {}^4\bar{J}_4 \dot{\theta}$$

$$= {}^4X_3 \begin{bmatrix} {}^3\omega_3 \\ {}^3\dot{\theta}_3 \end{bmatrix} = {}^4X_3 {}^3\bar{J}_3 \dot{\theta}$$

Static Force Propagation

Force Balance on Body 3:

$${}^3f_3 = {}^3R_t {}^t f_t$$

Moment Balance on Body 3
about origin ξ_3 :

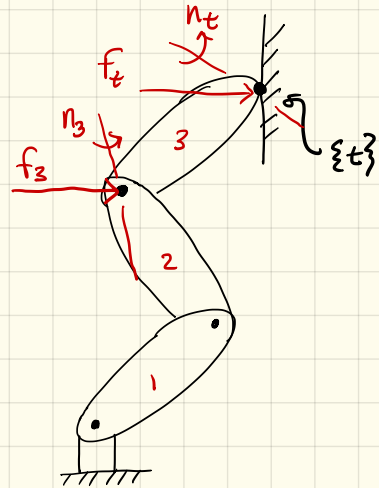
$${}^3n_3 = {}^3R_t {}^t n_t + {}^3p_t \times {}^3R_t {}^t f_t$$

f_t : Force applied by tool
onto the wall

n_t : Moments applied by tool
onto the wall (about ξ_t)

f_i : Force applied at ξ_i onto
body ξ_i

n_i : moment about ξ_i onto
body ξ_i



$$\begin{bmatrix} {}^3n_3 \\ {}^3f_3 \end{bmatrix} = \begin{bmatrix} {}^3R_t & S({}^3p_t) {}^3R_t \\ 0 & {}^3R_t \end{bmatrix} \begin{bmatrix} {}^t n_t \\ {}^t f_t \end{bmatrix}$$

$$= \begin{bmatrix} {}^tR_3 & 0 \\ -{}^tR_3 S({}^3p_t) & {}^tR_3 \end{bmatrix}^T \begin{bmatrix} {}^t n_t \\ {}^t f_t \end{bmatrix} = \begin{matrix} t \\ 3 \end{matrix} \begin{bmatrix} {}^t n_t \\ {}^t f_t \end{bmatrix}$$