

# Lecture 38 - Nonlinear Control

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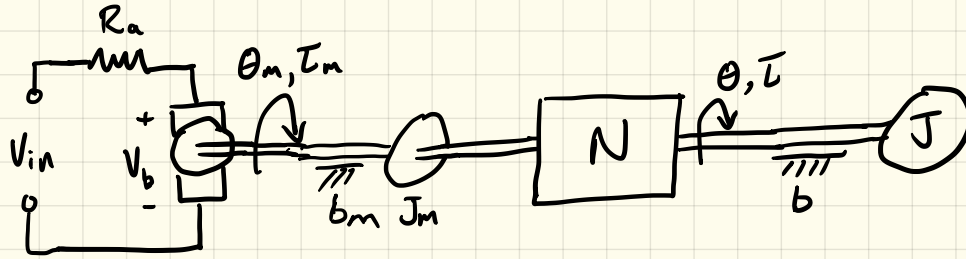
## Announcements:

- HW 10: Online, never due. Turn into my mailbox by Thursday  $\Rightarrow$  I'll replace your 2nd lowest HW w/ a 10
- Final Review: Friday 7th, 4-6 PM, Fitz 356

## Today:

- Wrap up: Motor modelling
- Introductory Nonlinear Control
  - $\Rightarrow$  Computed Torque
  - $\Rightarrow$  PD+ control

## DC Motor Model: Adding a Gearbox



Torque @ output of Gearbox:

$$T = [T_m - \dot{\theta}_m b_m - J_m \ddot{\theta}_m] N = b \ddot{\theta} + J \ddot{\theta}$$

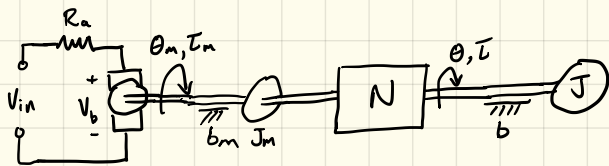
$$N T_m = N \dot{\theta}_m b_m + N J_m \ddot{\theta}_m + b \ddot{\theta} + J \ddot{\theta} \quad N \theta = \theta_m$$

$$= (b + N^2 b_m) \ddot{\theta} + (J + N^2 J_m) \ddot{\theta}$$

inertia felt @ output

Or in terms of motor angles:

$$T_m = \left(b_m + \frac{b}{N^2}\right) \ddot{\theta}_m + \left(J_m + \frac{J}{N^2}\right) \ddot{\theta}_m$$



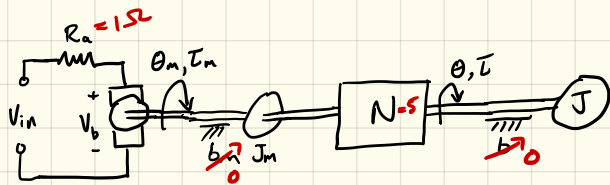
$$T_m = \underbrace{\left(b_m + \frac{b}{N^2}\right)}_{b'_m} \dot{\theta}_m + \underbrace{\left(J_m + \frac{J}{N^2}\right)}_{J'_m} \ddot{\theta}_m$$

Comments:

- In a multi joint robot  $J$  is not fixed
- When  $N$  is large motor components dominate dynamics
- Industrial robots  $N > 100$  not uncommon
- Design a critically damped control for maximum  $J$   
 $\Rightarrow$  Then at least critically damped all the time

Aside:

- $a\ddot{x} + b\dot{x} + cx = 0$  Overdamped when  $b^2 > 4ac$
- if  $a_{\min} \leq a \leq a_{\max}$  System overdamped if  $b^2 > 4a_{\max}c$



$$N=5$$

$$b=b_m=0$$

$$R=1 \Omega$$

$$K_b = \frac{1}{2} \text{ Vs/rad}$$

$$J_m = 2 \text{ Kg cm}^2$$

If  $J$  ranges from 100 to 300  $\text{Kg cm}^2$ , and  $V_{in} = -K_p \theta_m$  what is maximum  $K_p$  such that the system is always critically or over damped?

$$\frac{R_a}{K_L} J_m' \ddot{\theta}_m + \left( K_b + \frac{R_a b_m'}{K_L} \right) \dot{\theta}_m + K_p \theta_m = 0$$

$$\left( K_b + \frac{R_a b_m'}{K_L} \right)^2 \rightarrow 4 \frac{R_a}{K_L} J_m' K_p$$

$$K_p < \frac{K_b^2 K_L}{4 R_a J_m'} = \frac{\left( \frac{1}{2} \text{ Vs/rad} \right)^2 \left( \frac{1}{2} \text{ Nm/A} \right)}{4 \cdot 1 \cdot \left( 2 \times 10^{-4} + \frac{300}{25} \times 10^{-4} \right) \text{ Kg m}^2} = 22.3 \text{ V/rad}$$

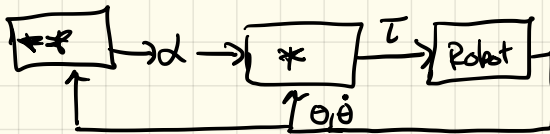
A simple Nonlinear control law: Goal  $\theta \rightarrow 0$  as  $t \rightarrow \infty$

Dynamics:  $\tau = M(\theta) \ddot{\theta} + V(\theta, \dot{\theta}) + G(\theta)$

- Nonlinear dynamics are difficult to work with
- Let's design a feedback controller to turn this system into a linear one  
"Feedback linearization"

$$\tau = M(\theta) \alpha + V(\theta, \dot{\theta}) + G(\theta) \quad (*)$$

$$\cancel{M} \alpha + \cancel{V} + \cancel{G} = \cancel{M} \ddot{\theta} + \cancel{V} + \cancel{G} \Rightarrow \ddot{\theta} = \alpha$$



- Try PD control:  $\alpha = -k_p \theta - k_d \dot{\theta}$  (\*\*)
- Closed loop:  $\ddot{\theta} + k_d \dot{\theta} + k_p \theta = 0$

# Computed Torque Tracking Control

- Desired Trajectory  $\theta_d(t)$
- $\tau = M\alpha + V + G$
- $\alpha = \ddot{\theta}_d + K_p(\theta_d - \theta) + K_d(\dot{\theta}_d - \dot{\theta})$
- Consider  $e = \theta_d - \theta$

$$\ddot{e} + K_p e + K_d \dot{e} = 0$$

Stable if and only if  $K_p > 0$  and  $K_d > 0$

(Project 2)